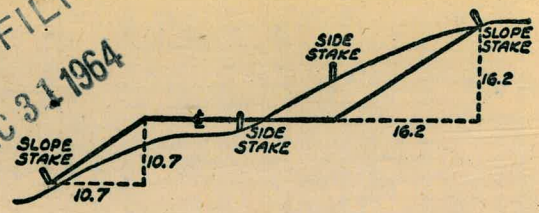


2067

EMERSON

MICROFILMED
DEC 31 1964



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

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to page 457

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE															
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°		
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46		
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68		
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90		
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14		
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39		
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66		
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94		
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21		
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48		
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77		
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07		
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39		
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72		
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09		
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46		
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89		
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32		
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83		
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34		
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60		
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22		

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE															
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°		
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020		
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051		
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083		
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135		
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188		
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264		
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341		
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445		
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550		
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700		
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851		
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01		
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17		
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	1.07	1.18	1.29	1.39		
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62		
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91		
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20		
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58		
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96		
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96		
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32		

Pages

1-5 - Prelim. Sewer - LaJolla Shores - + Frescotu

6-19X Sec Elizabeth St - Logan to "T" St

20-26 - Logan - Elizabeth to 45th

26 - X-Sect. Thomas - Reed - Jewell - + Alley's Blk 270

51 X-Sect Arista Dr. ^{Jefferson} Congress & LaJolla

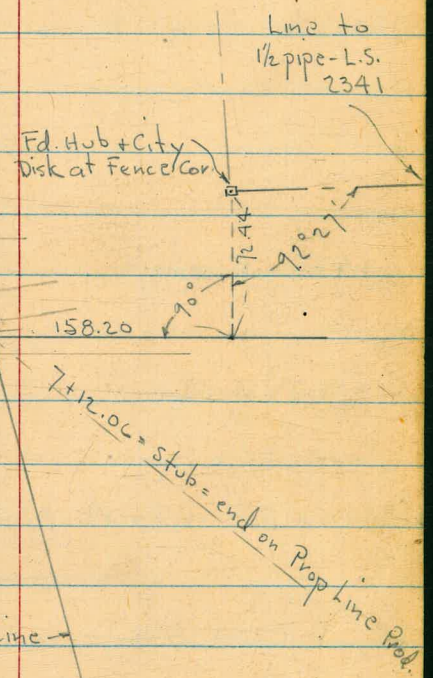
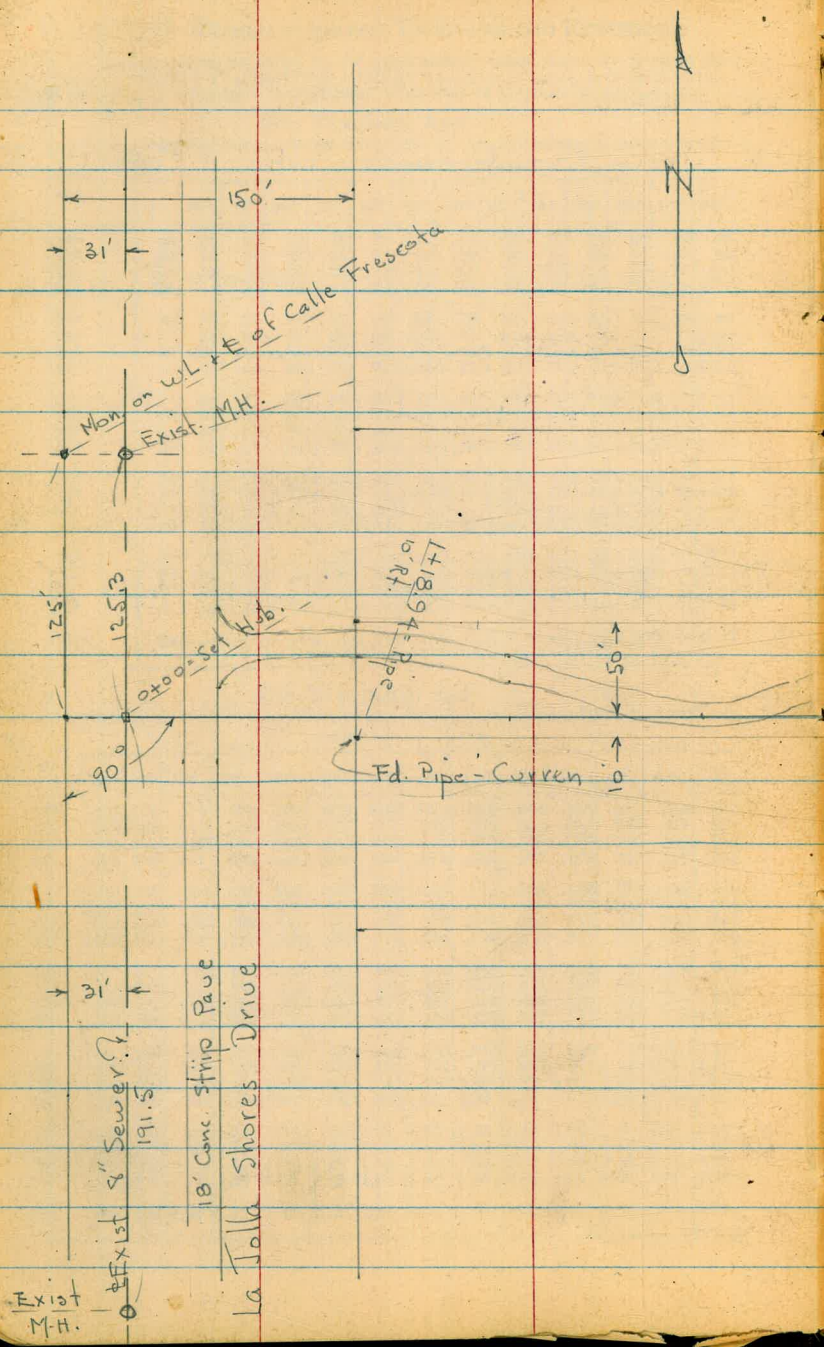
58-⁷³⁻⁷⁸ Pro. Drain Marena Blu & Milton St.

74 Pt. Loma Ave Santa Barbara east ✓

78 Levels on Milton also Marena Blu

Survey for Prop. Sewer
Notes - P. 2

INDEXED
W.K.
FEB 6 1950



Survey for Prop. Sewer in 60' Easment. E. of La Jolla Shores Dr.

Sec sketch - P. 1.

4186 Osborne 2-3-50
W.O. 62175 Haydin Hatch Shepard.

Levels along. #

0+55 21.5
4.4

0+47.7 = E. edge 21.61
4.33

0+29.7 = w. edge Conc. Pave - 18' strip 21.57
4.37

0+00 = Hub. on Exist. 8" Line 20.51
5.43
on Hub.

191.5 to S. I.E. of Exist. M.H. 15.54

125.3 to N. I.E. of Exist M.H. 10.12

B.M. 329 25.94 22.65 = 25.94
Chisel \square on cb. - \pm Ret. - S.W. Cor. Calle Frescota & La Jolla Shores Dr.

2+75 = ± at sly. of Rd.

Lt.	F	Rt.
34.6	34.8	33.7
3.0	2.8	3.7
13 = edge		15

3+30

31.8	31.8	31.9
5.8	5.8	5.7
9.5 = edge		3 = edge

2+90 = Sly. of Rd.

29.6	29.4	29.5	28.8	27.5
8.0	8.2	8.1	8.8	10.1
12	6		10	75 = Vac. Lot.

2+45 - 117' Lt. = Nearest to House (Pool) (Large + Swimming)

29.9	30.86	26.4
7.7	6.70	11.2
117	117	
ground	floor	

2+00

25.6	24.6
12.0	13.0
18	

T.P. 12.11 37.56 149 24.45

5. edge	37.56
Rd.	

1+70 - 34.7 Rt. = ^{86' Rt.} House - Tank at South end

23.2	24.17	22.2
2.7	1.77	3.7
	34.7 = floor	86 - ground at Tank

1+18.94 = 10' Rt. = Pipe - 31.5 Lt. = Sly. of Road. Cold Lay

23.1	22.2	21.6	21.4
2.8	3.7	4.3	4.5
31.5	25		10
Sly. of Rd.			

0+80

20.8
5.1

0+65 = ± Drain

20.3	19.6	18.7
5.6	6.3	7.2
25		25
in Drain	25.94	Drain

floor level - 150' Rt. = Sly.
 - 38.5' Rt. = Near Cor. of Large House
 6+70 = ± at wly. of C.L. Dr. to Rt

6+50

6+00

T.P. 13.19 62.26 0.51 49.08

5+50

5+00

floor level 150 Rt. = S. end.
 4+55 - 40' Rt. = ± at N. end of Long House

T.P. 12.52 49.59 0.49 37.07

4+21 = Ely. of Dr.

3+91 = wly. of C.L. Dr. to Rt.

Lt. Rt. 4

55.8 54.7

6.5 7.6

38.5' ground 38.5' floor.

54.8 54.4

7.3 7.9

13.5
edge Rd.

51.5 50.3 50.4 49.9

10.8 12.0 11.9 12.4

2.5 13 10

edge Rd.

62.26

47.1

2.5

43.6 43.0 42.6

6.0 6.6 7.0

25.5 15

edge Rd.

39.5 39.6 38.2 38.19

10.1 10.0 11.4 11.40

1.5 4.0 4.0

edge Rd. ground floor

49.59

37.2

0.4

35.8

1.8

37.56

Lt.

#

Rt.

opp. end.

Set B.M. on Cor. Pipe 344 58.82

owner says he is not interested, at present
Road continues on to House on Hill

7+12 :06 = Stub = end

58.6

3.60

on Stub

7+10 = Ely. of C.L. Dr.

59.0

58.6

58.1

58.9

3.3

3.7

4.2

3.4

35'

4

10

edge

Rd.

62.26

along

wall

Elizabeth St X Section
from Logan to T St

Moore 4/4/50 W031577

Begg notes

INDEXED

Sherman

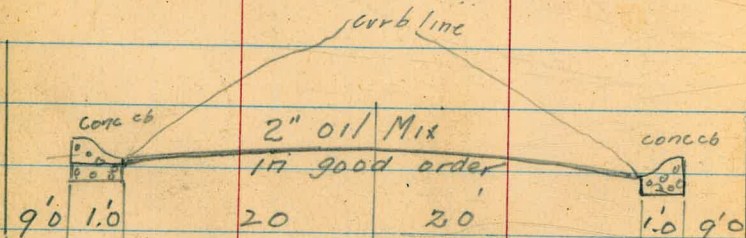
M.R.

APR 7 1950

Crawford

Drawings 6146 L Map 1886 #2

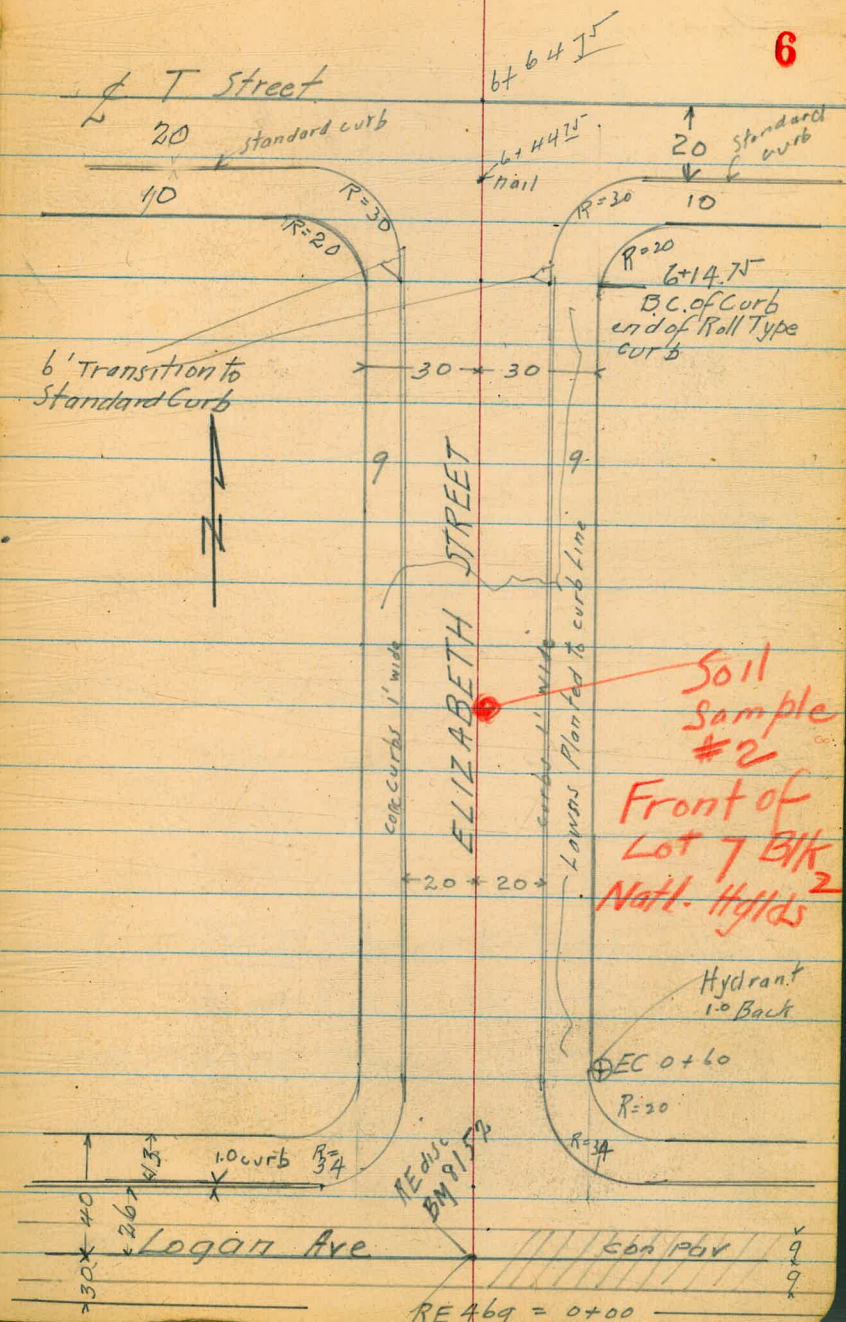
TP 3430 Profile 3683, 2892 Map 2265 #



X Section of Elizabeth

Prop Line

Clear View Blvd



BM		8.75	85.43	85.44 ₀₁
TP	6.42	94.18	2.62	87.76
TP	4.41	90.38	5.61	85.97
TP	5.63	91.58	2.71	85.95
TP				
set BM.	7.14	88.66	3.96	<u>81.52</u>
T.P.	5.38	85.48	4.48	80.10
BM set		4.74	<u>79.84</u>	set BM.
TP	0.82	<u>84.58</u>	6.47	83.76
T.P.	2.94	90.23	6.73	87.29
B.M.	8.58	94.02		85.44

BM starting Ocean Blvd & 45th

Disk REH 69 of Elizabeth & Logan

chis □ center S. E return T & Elizabeth

BM leads copper track of Ocean View Blvd to West of 45th

Elizabeth

0+875 30 Walk 21 Rt

0+70 Palm

2.5 Lt 6" Palm

2.5 Rt 12" Palm

460 86.12 5.78 81.52

0+60

0+40 contd.

0+40

0+26 gutter Line

87.30

80.68
662
160

80.34
696
1009

BC
54
see sketch

80.88
648
30

80.99
631
20

81.14
616
10

81.24
606
87.30

81.31
599
10

81.33
597
20

81.42
588 BC
30 54
see sketch

81.30
60
30

81.24
606
377

80.94
636
265

80.71
639
20

81.04
626
10

81.19
611
10

81.26
594
20

81.39
591
20

81.60
570
26.5

81.92
538
37.7

81.04
5.9
30

EC
20
see sketch

81.04
626
10

86.12
81.29
6.07

81.84
5.96
10

EC
20
see sketch

81.01
5.3
30

81.01
5.3
30

81.88
474
20

81.72
439
21

81.21
434
30

9

1+46 25 L 8" Palm

1+37 25 R Palm 14"

1+32 5 Eug Hedge E & W bog 21 RT

1+17 ϕ 2.0 wide conc Rib R1+11 ϕ 4.0 wide conc Ribbon R1+05 ϕ 2.0 wide conc Ribbon R

1+00 25 R 12" Palm

81	81	81
27	61	76
4.85	4.51	4.34
20	21	30

81	81	81
29	62	76
4.83	4.50	4.36
20	21	30

81	81	81
30	63	79
4.82	4.49	4.33
20	21	30

80	81	80	80	81	81	81	81	
2	15	80	74	11	23	34	64	82
5.2	4.97	5.32	5.18	5.01	4.89	4.78	4.68	4.3
30	21	20	10		10	20	21	30

86.12

86.12

Elizabeth

L

D

R

11

1+96 2.0 Rib R

$\frac{80}{80} \frac{23}{23}$	$\frac{81}{81} \frac{24}{24}$	$\frac{81}{81} \frac{25}{25}$
5.19	4.88	4.64
20	21	30

1+91 2.0 Rib Rt

$\frac{81}{81} \frac{20}{20}$	$\frac{81}{81} \frac{21}{21}$	$\frac{81}{81} \frac{22}{22}$
5.16	4.84	4.71
20	21	30

1+87 2.5 Palm 12" diam

1+77 2.0 Rib

$\frac{81}{81} \frac{20}{20}$	$\frac{80}{80} \frac{23}{23}$	$\frac{80}{80} \frac{24}{24}$
5.12	5.29	5.56
30	21	20

$\frac{81}{81} \frac{20}{20}$	$\frac{81}{81} \frac{21}{21}$	$\frac{81}{81} \frac{22}{22}$
5.10	4.82	4.60
20	21	30

1+72 2.0 Rib R & L

$\frac{81}{81} \frac{20}{20}$	$\frac{80}{80} \frac{23}{23}$	$\frac{80}{80} \frac{24}{24}$
5.12	5.24	5.53
30	21	20

$\frac{81}{81} \frac{20}{20}$	$\frac{81}{81} \frac{21}{21}$	$\frac{81}{81} \frac{22}{22}$
5.09	4.80	4.57
20	21	30

1+55 21 R 3.0 walk

$\frac{81}{81} \frac{23}{23}$	$\frac{81}{81} \frac{24}{24}$	$\frac{81}{81} \frac{25}{25}$
4.99	4.49	4.55
20	21	30

1+51 21 Lt 3.0 Walk

86.12

$\frac{81}{81} \frac{20}{20}$	$\frac{80}{80} \frac{24}{24}$	$\frac{80}{80} \frac{25}{25}$	$\frac{80}{80} \frac{26}{26}$
5.09	5.18	5.46	5.33
30	21	20	10

$\frac{80}{80} \frac{21}{21}$	$\frac{81}{81} \frac{20}{20}$	$\frac{81}{81} \frac{21}{21}$	$\frac{81}{81} \frac{22}{22}$	$\frac{81}{81} \frac{23}{23}$
5.21	5.06	4.96	4.66	4.4
10	20	20	21	30

86 12

Elizabeth

L F R

12

2+55 2.0 Rib RT

80 60	80 54	80 21	80 38	80 53	80 67	80 21	80 24
5.52	5.58	5.91	5.74	5.53	5.43	5.11	4.88
30	21	20	10	10	20	21	30
walk							

2+50 2.0 Rib RT ~~RT~~ 3.0 walk LT

2+30 2.1R E & W Hedge Eug

2+28 2.0 R LT

2+23 2.0 Rib LT

2+14.5 3.0 walk 2.1 R

2+07 3.0 walk 2.1 Left

2+00

86:12

80 60	80 54	80 21	80 38	80 53	80 67	80 21	80 24
5.52	5.57	5.85		5.39	5.30	5.23	4.96
30	21	20	10	10	20	21	30
walk							

80 72	80 54	80 21	80 49	80 25	80 82	80 87	80 16	80 50
5.72	5.48	5.75	5.63	5.39	5.30	5.23	4.96	4.82
30	21	20	10	10	20	21	30	walk

80 62	80 72	80 45	80 56	80 25	80 84	80 72	80 23	80 52
5.71	5.40	5.67	5.54	5.34	5.24	5.20	4.89	4.6
30	21	20	10	10	20	21	30	

86:12

TP 4.13 84.59 5.66 80.46

84.59 50 80 20

3+04 3.0 Walk R 21

80 80 81
5.62 5.32 4.92
20 21 30

3+00

30 21 20 10 80 80 80 81
5.8 5.81 6.09 5.94 5.73 5.62 5.64 5.32 4.8
30 21 20 10 10 20 21 30

2+975 2.0 Rib Lt

80 80 80
5.39 5.81 6.10
30 21 20

2+96 12" Palm 25 R

2+93 20 Rib 21 Lt

80 80 80
5.88 5.76 6.06
30 21 20

2+85 21 Rt Eug Hed

2+76 2" Rib Lt

5.84 5.71 6.01
30 21 20

2+71 3.0 Walk R 2.0 Rib Lt

80 80 80
5.78 5.65 5.98
30 21 20

57 20 20
5.53 5.19 5.03
20 21 30

2+59 25 R 14" Palm

86.12

86.12

Elizabeth

3+85 E+W Evg Her 73 RT.

3+79

3+74 2.0 Rib Lt

3+55 3.0 walk Lt

3+53 2.0 Rib RT.

3+48 2.0 Rib 21 RT

3+35 E+W Hedge Evg 22. RT

3+33 2.5 RT Palm 6"

3+27 2.0 Rib

3+22 2.0 Rib 21 RT

3+20

84.59

01	01	57
20	20	29
4.89	4.62	4.92
30	21	20
29 2/3	80 5/1	79 2/1
4.86	4.59	4.88
30	21	20
80 0/1	80 0/1	79 2/2
4.57	4.57	4.81
30	21	26

80 2/2	80 6/1	81 0/1
4.27	3.98	3.58
20	21	30

29 2/2	13	83	80 0/1	80 1/1	80 3/1	80 5/1	81 0/1
4.6	4.46	4.76	4.53	4.42	4.26	4.25	3.95
30	21	20	10	10	10	20	21
							30

80 5/3	20	13
4.16	3.86	3.46
20	21	30
80 4/4	80 2/1	81 1/1
4.15	3.86	3.41
20	21	30

84.59

Elizabeth

15

4+55 3.0 Walk RT

79	80	80
79	80	80
4.70	4.42	3.95
20	21	30

4+51 3.0 Walk LT

26	23	23	58	79	85	91	17	79
79	79	79	79	79	79	79	80	80
4.83	4.86	5.16	5.01	4.82	4.74	4.68	4.42	3.8
30	21	20	10	10	20	20	21	30
Walk								

4+32 12" Palm 25 LT

4+28 3.0 Rib LT

56	81	59
79	79	79
5.03	4.78	5.10
30	21	20

4+22 3.0 Rib LT

58	81	50
79	79	79
5.01	4.78	5.09
30	21	20

4+14 3.0 Walk RT

80	80	80
80	80	80
4.57	4.27	3.86
30	21	30

4+09 12" Palm 25 RT

4+06 3.0 Walk LT

4.70	4.68	5.01
30	21	20

4+00

81	84	81	25	85	80	80	80	79
79	79	79	79	79	80	80	80	80
4.7	4.65	5.00	4.84	4.64	4.55	4.52	4.22	3.8
30	21	20	10	10	20	20	21	30

3.94 4.70 Drive RT 12" Palm Lt 25

84.59

84.59

Elizabeth

5443 2.0 Rib Rt
 5+28 2.0 Rib Lt
 5+26 15" Palm 25 R
 5+23 2.0 Rib Lt
 5+21 3.0 Walk Rt
 5+14 2" Oleander 25 Lt
 5+05 3.0 Walk Lt 2.0 Rib Rt

5+00 2.0 Rib R
 4+91 4" Oleander 25 Lt
 4+84 25 R 12 Palm
 4+78 2.0 Rib R
 4+77 2.0 Rib Lt
 4+73 2.0 Rib Rt
 4+72 2.0 Rib Lt
 4+67 2" Tree 25 Lt

84.59

14
 $\begin{array}{r} 79 \\ 5.45 \\ 30 \end{array}$ $\begin{array}{r} 26 \\ 79 \\ 5.23 \\ 21 \end{array}$ $\begin{array}{r} 01 \\ 79 \\ 5.53 \\ 20 \end{array}$

12
 $\begin{array}{r} 79 \\ 5.42 \\ 30 \end{array}$ $\begin{array}{r} 23 \\ 79 \\ 5.16 \\ 21 \end{array}$ $\begin{array}{r} 11 \\ 79 \\ 5.48 \\ 20 \end{array}$

25
 $\begin{array}{r} 79 \\ 5.14 \\ 30 \end{array}$ $\begin{array}{r} 21 \\ 79 \\ 5.07 \\ 21 \end{array}$ $\begin{array}{r} 24 \\ 79 \\ 5.35 \\ 20 \end{array}$

49
 $\begin{array}{r} 79 \\ 5.1 \\ 30 \end{array}$ $\begin{array}{r} 51 \\ 79 \\ 5.02 \\ 21 \end{array}$ $\begin{array}{r} 21 \\ 79 \\ 5.32 \\ 20 \end{array}$ $\begin{array}{r} 31 \\ 79 \\ 5.22 \\ 10 \end{array}$

04
 $\begin{array}{r} 30 \\ 5.04 \\ 30 \end{array}$ $\begin{array}{r} 92 \\ 21 \\ 4.92 \\ 21 \end{array}$ $\begin{array}{r} 20 \\ 20 \\ 5.20 \\ 20 \end{array}$

61
 $\begin{array}{r} 79 \\ 4.98 \\ 30 \end{array}$ $\begin{array}{r} 69 \\ 79 \\ 4.90 \\ 21 \end{array}$ $\begin{array}{r} 20 \\ 79 \\ 5.19 \\ 20 \end{array}$

51
 $\begin{array}{r} 79 \\ 5.00 \\ 20 \end{array}$ $\begin{array}{r} 25 \\ 79 \\ 4.74 \\ 21 \end{array}$ $\begin{array}{r} 08 \\ 80 \\ 4.51 \\ 30 \end{array}$

16

36
 $\begin{array}{r} 79 \\ 4.93 \\ 20 \end{array}$ $\begin{array}{r} 94 \\ 79 \\ 4.65 \\ 21 \end{array}$ $\begin{array}{r} 41 \\ 80 \\ 4.18 \\ 30 \end{array}$

51
 $\begin{array}{r} 79 \\ 4.90 \\ 20 \end{array}$ $\begin{array}{r} 21 \\ 79 \\ 4.61 \\ 21 \end{array}$ $\begin{array}{r} 44 \\ 80 \\ 4.15 \\ 30 \end{array}$

55
 $\begin{array}{r} 79 \\ 5.04 \\ 10 \end{array}$ $\begin{array}{r} 57 \\ 79 \\ 4.92 \\ 20 \end{array}$ $\begin{array}{r} 59 \\ 79 \\ 4.90 \\ 20 \end{array}$ $\begin{array}{r} 89 \\ 79 \\ 4.60 \\ 21 \end{array}$ $\begin{array}{r} 42 \\ 80 \\ 4.17 \\ 30 \end{array}$

29
 $\begin{array}{r} 79 \\ 4.80 \\ 20 \end{array}$ $\begin{array}{r} 80 \\ 79 \\ 4.48 \\ 21 \end{array}$ $\begin{array}{r} 31 \\ 80 \\ 4.06 \\ 30 \end{array}$

25
 $\begin{array}{r} 79 \\ 4.78 \\ 20 \end{array}$ $\begin{array}{r} 72 \\ 80 \\ 4.47 \\ 21 \end{array}$ $\begin{array}{r} 50 \\ 80 \\ 4.05 \\ 30 \end{array}$

84.59

Elizabeth

18

6 + 4475 Scurb. T 9.36 10.00 678
 100 100 50
 6 9 6

Check to BM chns 9
 Sec P7 462 84.47 449 79.85 79.84
 see P7

6 + 3475 5 Line "T" St

6 + 2075 end of transition bag regular type curb

6 + 19 3-0 Walk Rt

6 + 14.75 Curb BC end of Roll Type Curb

6 + 04 2-0 Rib Lt
 84.59

79 02 61 85 19
 79 51 78 27 25 03
 74 5 686 659 628 5.96 5.68 5.44 5.19 4.45 38.3
 50 30 20 10 84 47 10 20 30 50 50
 EC EC EC

79 81 85 85 82
 79 15 79 30 25 83 25 60 80 81 14
 5.8 5.72 6.24 6.05 5.70 5.44 5.29 5.16 4.99 4.50 4.5
 30 27 37.8 20 10 10 20 27.9 27.9 30

79 29 79 01 78 22 79 10 79 20 79 82 79 85 79 80 80 2
 5.6 5.55 5.87 5.49 5.29 5.12 5.14 4.69 4.4
 30 6 20.7 10 10 10 20.7 20.7 30

79 46 79 85 84 77 85
 79 79 79 80 80 77 81 35
 5.13 4.74 4.35 3.82 3.4
 20.3 20.7 30 30 31
 steps

79 27 79 20 79 21 79 15 79 35 79 82 79 50 79 86 80 57
 5.6 5.39 5.68 5.44 5.34 5.07 5.09 4.73 4.1
 30 21 20 10 10 10 20 21 30
 BC BC BC BC

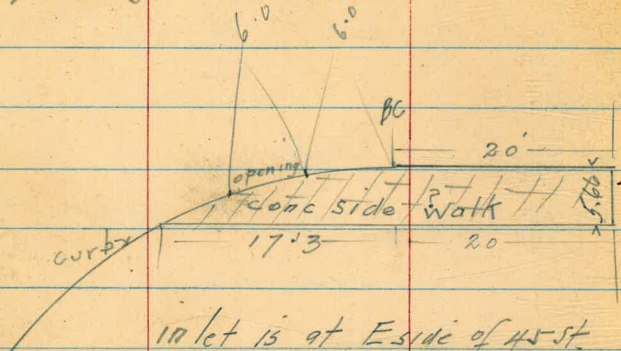
79 00 79 25 79 21
 5.59 5.31 5.61
 30 21 20
 84.59

1.86 2.56
 100 100
 26 5
 29 24 80 81
 29 80 80
 25 28 50 50
 EC EC

Elizabeth St

19

opening 0.4 high



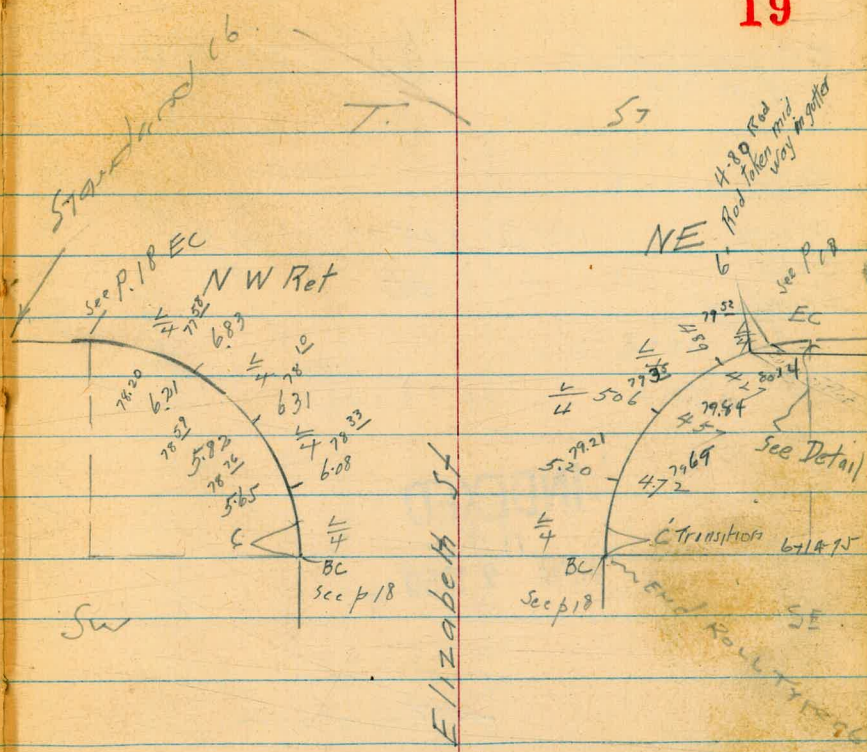
inlet is at E side of 45th St.

& connects as a corrugated

Pipe

Sketch of out-let NE

Return



6 + 64 75

TP. 4.56 84.41 4.62 79.85
chisel sg
P. 7

6 + 47 75

end of block Pav

~~84.59~~
84.47

74.21	76.21	75	75	78.05	78.04	76.20	75.21	79.51	79	80.51	82
9.8	7.5	6.9	6.35	5.87	5.51	5.17	4.86	4.52	3.9	2.2	
100	50	30	20	10	0.11	84.41	oil	20	30	50	100
										dir	

2.21	7.21	78.01	78	78.01	78.01	78.20	78.21	79	78.47	82
7.33	6.76	6.46	6.16	5.83	5.55	5.26	4.98	4.35		
50	30	30	10		10	20	30	50		

~~84.59~~
84.47

X Section Logan Ave
Elizabeth to 45th

0 + 24 Curb BC

$\frac{82}{25}$	$\frac{82}{15}$	$\frac{81}{25}$	$\frac{81}{1}$	$\frac{81}{25}$	$\frac{81}{25}$	$\frac{81}{25}$	$\frac{81}{25}$
5.7	5.80	6.10	6.14	6.20	5.90	5.96	6.6
40	27	26	18	9		9	30

0 + 0 F line Eliz

$\frac{81}{31}$	$\frac{81}{27}$	$\frac{81}{23}$	$\frac{81}{20}$	$\frac{81}{25}$	$\frac{81}{25}$
6.60	6.38	6.22	6.15	6.20	6.9
26	18	9		9	30

0 - 30

$\frac{81}{21}$	$\frac{81}{20}$	$\frac{81}{25}$	$\frac{81}{23}$	$\frac{81}{20}$	$\frac{81}{25}$
6.74	6.65	6.57	6.42	6.45	6.6
26	18	9		9	30

0 - 33 Pole 25A P7583

0 - 60

$\frac{81}{20}$	$\frac{81}{25}$	$\frac{81}{21}$	$\frac{81}{25}$	$\frac{81}{21}$	$\frac{81}{25}$
7.05	6.89	6.74	6.60	6.71	6.6
26	18	9		9	30

87.95

6.43 87.95

81.52

RE disc #69 Elizabeth & Logan

X Section Logan

1 + 52.61

E line Alley

83 21
4.24
40

83 25
4.6
40

1 + 32.61

W line Alley

83 20
4.57
40

83 25
4.9
40

1 + 33.5 d 14' Drive Lt

1 + 00 W edge 3' con walk

83 18
4.77
40

0 + 74 10" Palm 31 Lt

0 + 78 Nos hedge 28 Lt

0 + 50

82 31
5.5
40

82 40
5.55
27

87.95

83 52
4.43
27

83 15
4.80
26

83 15
4.80
18

83 17
4.76
9

83 25
4.70

83 4
4.64
9

83 20
5.1
20

83 25
6.4
30

83 25
6.4
30

22

83 20
4.75
27

83 25
5.09
26

83 25
5.10
18

83 25
4.99
9

83 08
4.87

83 05
4.90
9

83 25
5.4
20

83 25
6.6
30

83 25
6.6
30

83 31
4.54
40

83 15
4.80
27

83 17
5.14
26

82 27
5.06
27

82 51
5.40
26

82 57
5.36
18

82 22
5.83
9

82 29
5.16

82 28
5.27
9

82 15
5.8
20

82 18
6.4
30

82 18
6.4
30

82 09
5.86
26

82 11
5.84
18

82 20
5.75
9

82 30
5.65

82 22
5.79
9

82 15
6.1
20

82 18
6.8
30

82 18
6.8
30

87.95

8+00

84 55
3.4
40

84 03
3.92
27

84 51
4.30
26

84 22
4.16
18

84 55
4.10
9

84 22
4.03

84 03
3.92
9

84 55
4.15
20

84 55
4.57
22

84 25
4.30

1+89 $\frac{d}{3}$ Walk

84 55
3.60
40

84 20
4.05
27

84 54
4.41
26

1+71 25A P Rib 75837

1+68 $\frac{d}{2.0}$ Rib

84 02
3.94
40

84 56
4.27
27

84 34
4.61
26

1+62 $\frac{d}{4.0}$ Rib

84 27
3.98
40

84 57
4.36
27

84 31
4.64
26

1+56 $\frac{w}{2.0}$ Rib drive

84 24
4.01
40

84 52
4.43
27

84 20
4.76
26

87-95

87 95

	85 ¹⁵	84.55	01
B + 85 ² WL 45 St	42.8	461	439
	61	60	50
	cb	cut	

B + 50		84 ⁷⁶	
		4.7	
		40	

B + 4 2 10" Palim 335 Lt

T.P. H-90 89.46 339 84.56

B + 362 Prop BC	84 ⁸¹		
	3.2		
	40		

B + 25 ² Curb BC	84 ²¹		
	3.2		
	40		

87.95

21	21	51	51	21	82	7	15
85	85	85	85	85	84	88	88
4.15	3.99	3.79	3.77	4.25	4.64	4.8	5.3
40	30	20	10		12	20	30

61	30	62	85	21	61	7	81	90
84	84	84	84	84	84	84	84	84
4.85	5.16	4.84	4.58	4.55	4.85	5.4	6.0	6.1
314	304	18	9		9	18	20	30

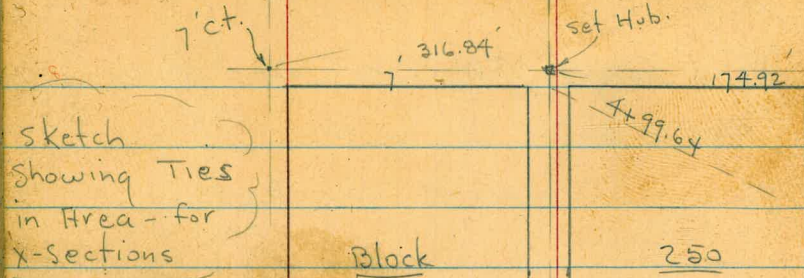
				89.46				
21	02	21	55	84	21	58	50	51
84	84	84	84	84	84	84	84	84
3.57	3.88	3.63	3.40	3.27	3.47	4.1	4.9	4.8
27.7	26.7	18	9		9	19	21	30
urb	cut							

21	21	12	21	21	01	508	50	2
84	84	84	84	84	84	84	84	84
3.69	3.97	3.87	3.64	3.59	3.55	4.4	5.0	4.8
27	26	18	9		9	20	22	30
cb	cut							

87.95

E. 7' line
Kendall

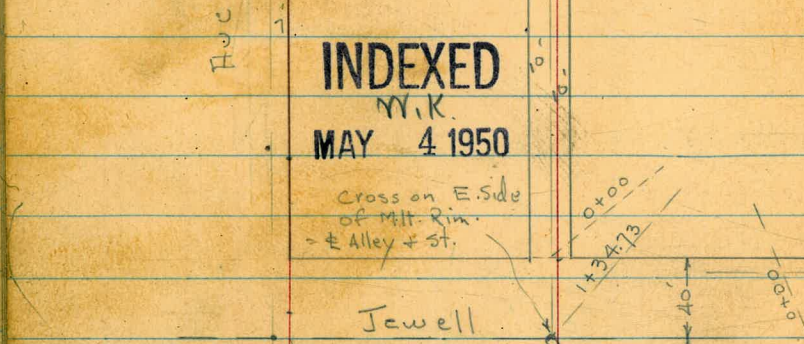
st



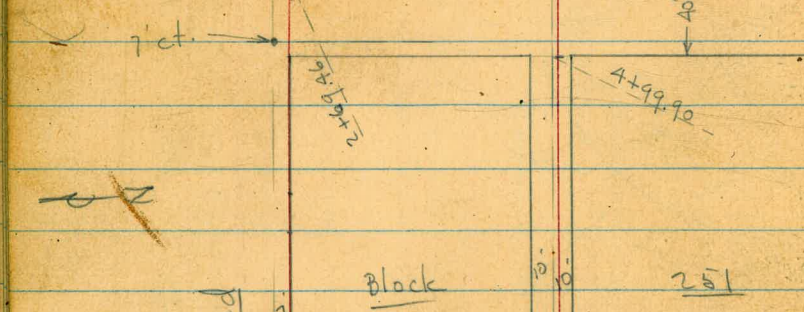
Sketch
Showing Ties
in Area - for
X-Sections

INDEXED
M.K.
MAY 4 1950

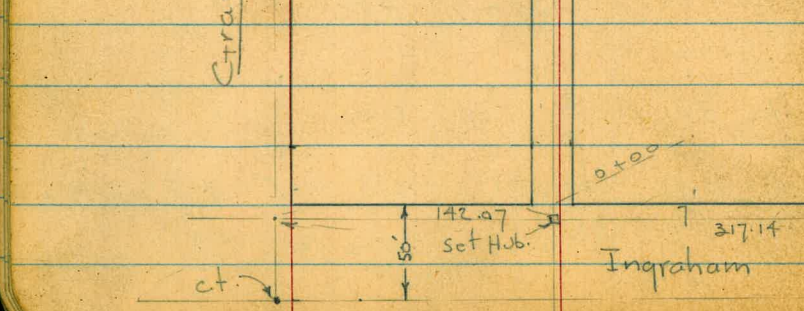
Cross on E. Side
of Mt. Rim.
- E Alley + St.



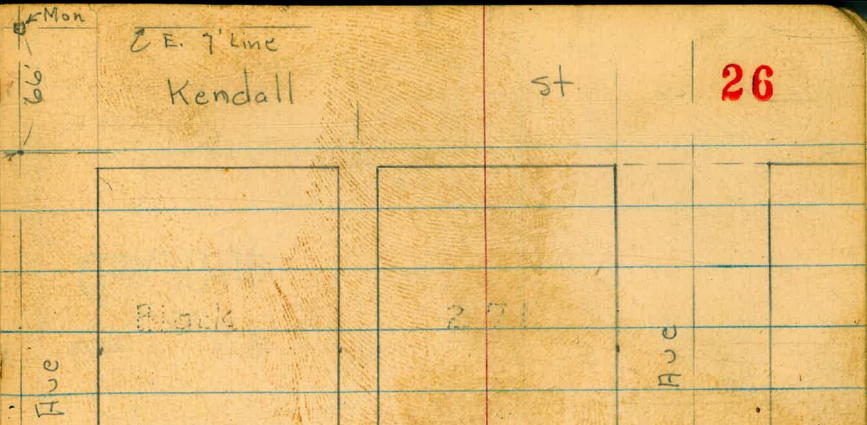
Jewell



Grand



Ingraham



Hub

Block

271

Hub



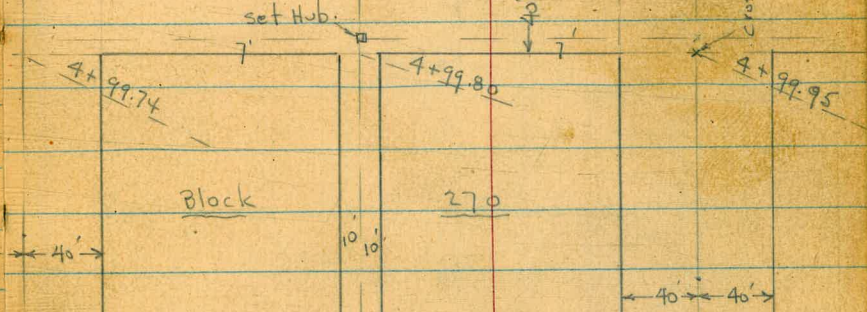
Mon

st

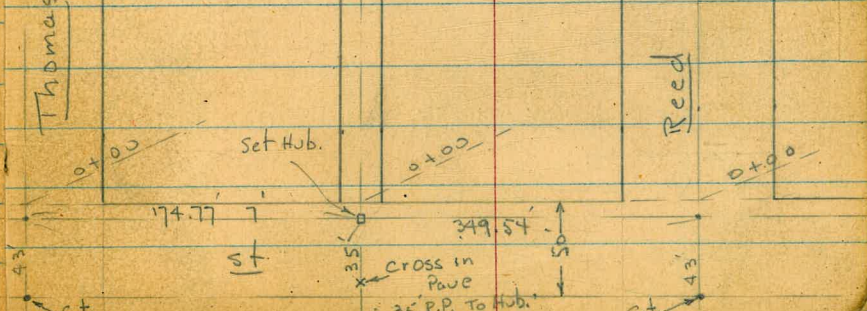
set Hub.

Block

270



Thomas



Reed

Cross in Pave
35' R.P. to Hub.

Topo. of Block 270

Ties - P. 26

Vac Lot

INDEXED
MAY 4 1950
W.K.

2+02

1+79-63.8 Rt.

1+45-55 Rt.

1+25

40' 40'

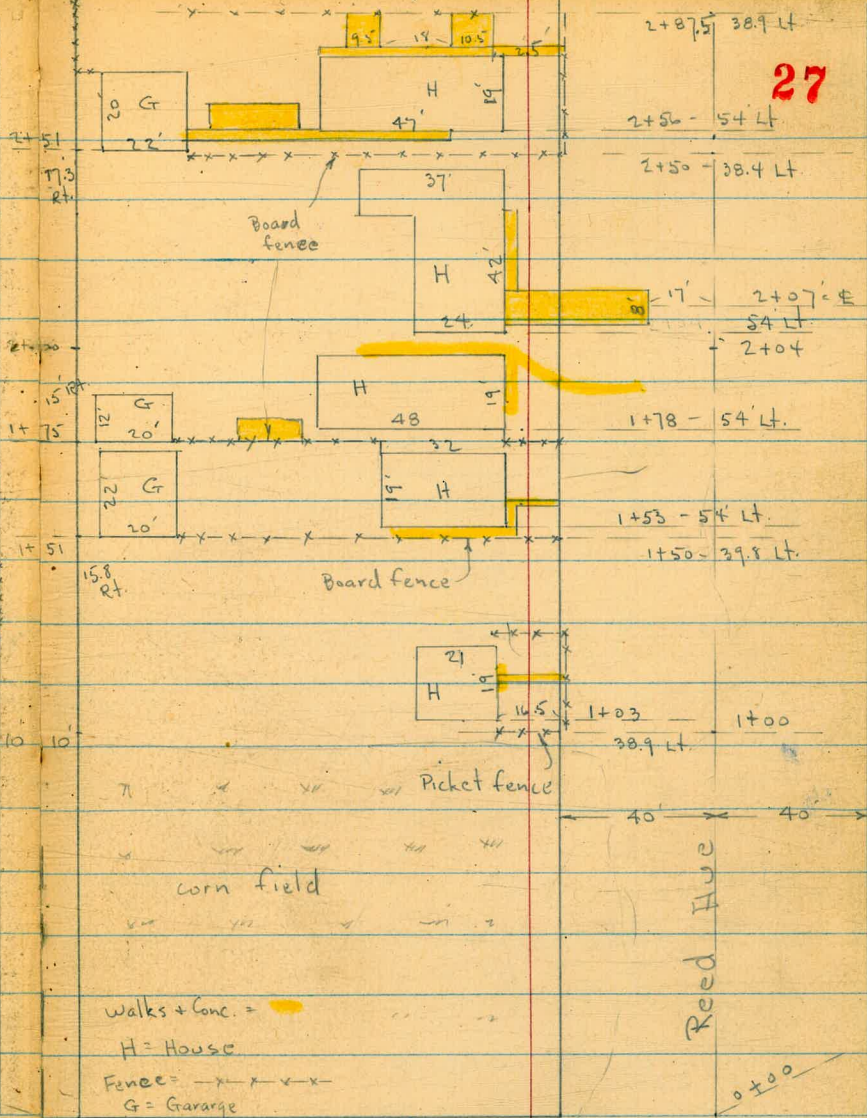
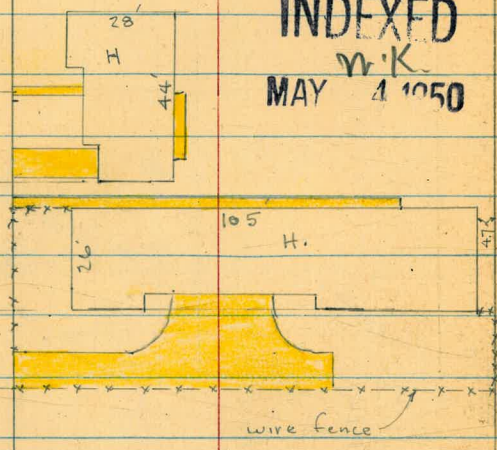
Thomas

Corn field

0+00

ct.

Ingraham



27

2+87.5 38.4 Lt

2+56-54 Lt

2+50-38.4 Lt

2+07-54 Lt

2+04

1+78-54 Lt.

1+53-54 Lt.

1+50-39.8 Lt.

1+03 38.9 Lt.

1+00

40' 40'

Reed Ave

0+00

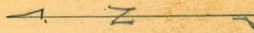
walks + Conc. =
H = House
Fence = - x - x - x -
G = Garage

Hub.

cross.

St. - Conc. Pave

ct. - E



Jewell St.

Conc Pave

Reed Hue

4+99.74

4+99.80

4+99.95

4+55 55' Rt

4+50

4+25, Walk?

4+15-55' Rt

3+89

3+78-55' Rt

AUC

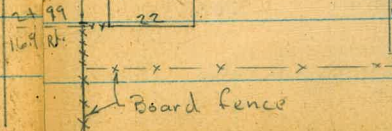
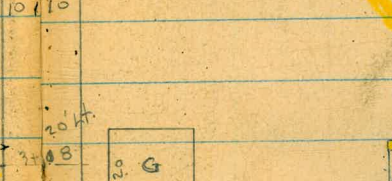
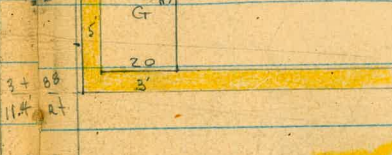
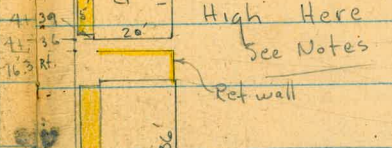
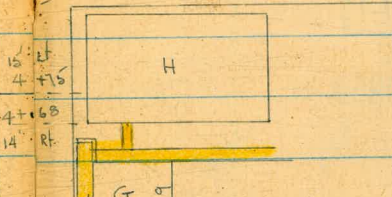
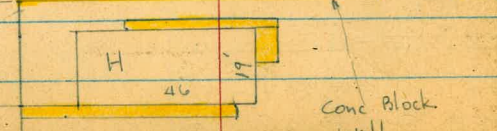
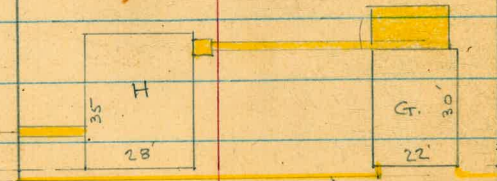
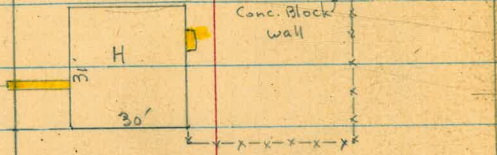
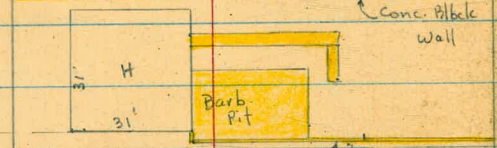
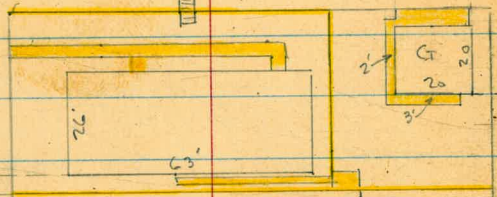
3+18

3+09-57' Rt

3+00

I

2+77-55' Rt



High Here See Notes

Ret wall

Conc Block wall

Board fence

3+28-54' Lt.

2+91-54' Lt.

2+87.5

3+00

Beq. X-Section of Reed St. from Ingraham
to Jewell - for Grade est. + showing
Topography of Block 270 - to N. for
Drainage problem - Sketch - P. 27

4427

W.O. 25020

5-1-50

Osborne
Hardin
Hatch

INDEXED
M.K.
MAY 4 1950

0+50

Trees about 15' apart.

0+17 - 26 Rt. = Beg. of Row of 24" Cypress Trees

0+00 = EL. Ingraham

Reduced to 1950
May 4, 1950
gms

0-40 = edge of Conc. Pavc.

5.45 49.61 4.68 44.16 - 44.15 = ± Id + ct. Reed + Ingraham

13.6 48.84 8.44 47.48

B.M. 0.07 55.92

55.85 = N.E. B.P. Grandt Ingraham

L. = N. †

Rt. = 5.28

A5 ¹	A3 ⁸	A3 ⁶	A3 ⁶	A3 ²	A2 ¹	A3 ⁴	A2 ⁶	A4 ²
4.5	5.8	6.0	6.0	6.4	7.5	6.2	7.0	5.4
100	40	20		20	35	40	55	65
Cornfield								

A5 ³	A5 ¹	A4 ¹	A3 ⁹	A4 ⁰	A4 ⁵	A5 ¹
4.3	4.5	4.9	5.7	5.6	5.1	4.5
100	40	20		20	40	80
Corn field						

A5.61	A4.90	A4.56	A4.12	A3.83	A4.10	A5.29
4.00	4.71	5.05	5.49	5.78	5.51	4.32
100	40	20		20	40	100

49.61

Reed

29

1+87- 19.1 Lt. = ± of 3' Conc. walk

LT

7.13	8.25	8.16	7.70
floor at House	54	40	19.1 = walk
		walk - To E. See sketch	

1+75

9.1	8.9	8.5	8.3	7.1	6.6	4.5	2.7
100	100	40	20	20	20	40	80
hit to E.	High lot To W.						

1+59- 40' Lt. = ± of 2' Conc. walk

6.96	8.24	8.8	8.50	8.3	8.5
54	51.7	100	60	40	20
floor at House	at Porch		on walk		

1+51 - to Show lot filled in

1+50

9.6	9.3	8.9	8.5	7.5	7.1	6.0	3.7
100	60	40	20	20	20	40	80

1+25- 67.5 Lt. - sly. + Ely. of 3'x6' Conc. porch

9.5	7.12	9.0	9.1	8.4	7.3	7.2	6.5	4.8
100	67.5	67.5	40	20	20	20	40	80
	Top Conc.	ground						

1+12- 38.6 Lt. = ± 3' Conc. walk

7.00	8.91	9.02
56.5	51.5	38.6 = walk
floor at House	at Porch	

1+00

9.0	8.5	7.7	7.1	7.1	7.1	5.1
100	40	20	20	20	40	80
end of field			49.61			

Reed

2+94 - 41.2 Rt = ± 8' Conc. Dr.

2+87.5 38.9 Lt = Beg. 8" Conc. wall = Cor.

2+78 - 39.6 Rt = ± 3' Conc. walk

Slabs to E. are level

2+75 - 41.2 Lt = wly of 2.5' Conc. walk along House

2+70 - 37.5 Rt = end Row of Trees

2+58 - 41.5 Rt = ± 8' Conc. Dr.

2+54 = ± 2.5' walk along House on Lt.

is Low + Level with top to E.

2+50 - 48.4 Lt = Cor. Conc. wall - ground to w.

2+07 - 17 Lt = ± of 8' Conc. Drive

T.P. 8.00 54.13 3.48 46.13

2+00

Lt

Rt

42.2

11.9
100

44.3

9.8

ground Top
end wall

46.86

7.27

55.5
40

45.1

9.0

40

47.93

6.20

38.9
20

46.6

7.5

20

48.3

5.8

49.3

4.8

20

51.3

2.8

40

51.6

2.5

50

51.83 Rt.
2.30
41.2
Dr.
52.21
1.92
55
Dr.
30
50.94
3.19
39.6
walk
51.20
2.93
52.5
at Porch

43.08

11.05

94 =
end

43.75

10.38

floor
House

44.08

10.05

54
at Cor. House

44.77

9.36

41.2

42.27

11.76

100

goes to
Cor.

43.41

10.72

68.2 = Beg. walk

50.53

3.60

41.5
Dr.

50.93

3.20

55
Dr.

42.0

12.1

100

42.1

12.0

ground Top
to w. end.

43.19

12.9

91
91

41.2

11.03

ground
to N. + w.
wall

43.10

11.0

48.4
40

43.1

11.0

40

44.3

9.8

20

45.9

8.2

20

46.6

7.5

20

49.8

4.3

40

50.2

3.9

50

41.75

12.38

54
Floor

also
House

41.89

12.24

40
Dr.

42.59

11.54

17
Dr.

54.13

40.5

9.1

100

41.4

8.2

40

42.1

7.5

20

43.3

6.3

49.61

43.8

5.8

20

45.1

3.9

40

48.4

1.2

80

Reed

4+17 - 40.7' Rt. = ± Conc. apron to Dowb. Gar.

4+00

3+92 - 40.5' Lt. = ± 3' Conc. Walk

3+70 - 40' Lt. = on 9' Conc. Dr.

3+51 - 41' Rt. = ± 8' Conc. Dr.

3+40 -

T.P. 8.40 60.94 159 52.54

3+25 - 39.5' Lt. = Cor. Conc. wall

3+14 - 38' Rt. = ± 3' Conc. Walk

3+07 - 19' Lt. = ± 3' Conc. walk

56.64
4.30
40.7
56.77
4.17
45.5
floor
Gar.

31

55⁹ 55⁷ 55³ 55⁴ 55⁴ 56⁰ 56⁰
5.0 5.2 5.6 5.5 5.5 4.9 4.9
50 40 20 20 40 42
along
House

55.46 55.41
5.48 5.53
50 40.5
walk walk

51⁴ 53.73 53.67 53⁵ 54³ 54⁵ 55³
9.5 7.21 7.27 7.4 6.6 6.4 5.6
100 54 40 20 20 40
floor
Gar.
in House

48.14 54.40 54.18 53⁴ 52⁰ 53¹ 53⁰ 54⁰ 54.46 55.12
13.80 6.54 6.76 7.5 8.9 7.8 7.3 6.9 6.48 5.82
54 49.5 40 20 20 40 40 41 55
Base
ment
floor
House
Conc.
Porch
Dr.
floor
Gar.

46.93 45⁶ 49.93 49⁰ 50⁶ 51⁹ 52⁵ 53⁵ 53⁵
7.20 8.5 4.20 5.1 3.5 2.2 1.6 0.6 0.6
80 80 39.5 39.5 20 20 40 50
TOP
end
wall
ground
Top
wall

46.53 45.82 46.22 47.71 48.75 53.14 53.34
7.60 8.31 7.91 6.42 5.38 0.99 0.79
floor 54 40 38 19 38 54
House at house Bot. at step walk at Porch
54:13

Check - N.E. B.P. Jewell & Reed 2.47 58.47 - 58.43 = Book

0.5 w. - Rods on edge

4+99.95 = W.L. Jewell - edge of Conc. Pav. is

58.35	58.30	57.85	57.27	57.92	57.43	58.00	58.1
2.59	2.64	3.09	3.67	3.02	3.51	2.94	2.8
37.3	32.3	26.3	20.3		27.6	27.6	40
'walk'		Top	90'		90'	Top	
end		end cb.				end cb.	

4+61 - 40.3 Lt = ± 3' Conc. walk

58.10	58.04
2.84	2.90
50	40.3
walk	walk

4+50 - 55 Lt = ± Doub. Grav.

58.14	57.8	57.3	57.0	56.8	57.4
2.80	3.3	3.6	3.9	4.1	3.3
55	40	20.		20	40
floor					
Grav.					

4+31 - 40 Lt = ± 3' Conc. walk

57.65	57.18
3.29	3.46
50	40
walk	walk
	60.94

X-Sect Jewell for Grade Est.

Reed to Grand - See sketch - P. 26 + 27-A

W.O. 25020

5-1-50

7.0

INDEXED

MAY ^{W.K.} 4 1950

1+00 - 40' Lt. Nly. of 4' Conc. walk

0+65-22 Rt. = on 15' Conc. Dr. - No Gar. (Now House)

0+49- 39.7 Lt. = 4' Conc. walk

0+30- 39.7 Lt. = Nly. of 4' Conc. walk

See FB 2202 - P 45

Rods on edge

0+00 = N.L. Reed - edge of Conc. pave is 0.3' N.

634

64.81

58.47 = NE. B.P.

Used our Elev.

58.31	58.27	57.2	58.2	60.3	60.5
6.50	6.54	7.1	5.9	4.5	4.3
4.8	4.0	2.0		2.0	4.0
along	walk				
House					

58.4	58.5	58.5	59.4	60.4	60.44	61.03	61.22
6.4	6.2	6.3	5.4	4.4	4.37	3.78	3.59
5.0	4.0	2.0		2.0	2.2	4.0	4.4
					Dr.	Dr.	at House

60.23	58.84
4.58	5.97
4.4	39.7 = walk
Top	
Porch	

60.27	58.83	58.3	58.9	60.6	60.5	60.8
4.54	5.98	6.5	5.9	4.2	4.0	4.0
4.4	39.7	2.0		2.0	4.0	47.5
Top	walk					along
Porch						House

57.41	58.39	58.21	57.48	58.28	58.09	58.64	58.72	58.75
6.40	6.42	6.60	7.33	6.53	6.72	6.17	6.09	6.06
35.3	30.3	20.3	20.3		2.0	2.0	3.0	3.5
end walk		Top	gut.		gut.	Top	Con.	walk

See P. 32.

64.81
mmmm

Lt. † Rt

2+30

46.8	46.78	46.9	50.20	51.2	51.7	52.5	55.1	55.6
10.5	10.48	10.4	7.06	6.1	5.6	4.8	2.2	1.7
56.5	57.2	41	40.3	20		20	40	50
along House	E. edge Conc walk		Top wall					

2+22 - 35.3 Lt. = † 4' Brick steps thru wall

46.79 50.32

10.47 6.94

41.0 35.3 = Top of Steps

T.P.

4.85 57.26 12.40 52.41 = Na

Thomas in S.W. Pole

57.26

1+85 - 40.1 Lt. = Beg. 8' Conc. wall - also to W.

46.8	52.54	46.9	52.50	54.2	54.8	55.5	57.0
18.0	12.27	17.9	12.25	10.8	10.0	9.3	7.2
89.2	89.2	ground	40.1	20		20	40
ground. end at N.W. wall	Top. 89.2	To N.W.	Top wall				

1+69 - 39.9 Lt. = end Conc. apron

53.77

11.10

45 floor.

53.60

11.21

39.9 = apron

1+50 - 39.9 Lt. = Beg. Conc. apron to Doub. Grav.

53.72

11.09

45 floor Grav.

53.67

11.14

39.9 = apron

1+44.84 = N.L.

55.5	56.3	57.1	57.5	59.5
9.3	8.5	7.7	7.3	5.0
40	20		20	40

1+24.84 = S.L. Alley

57.3	57.2	58.0	59.6	59.9
7.5	7.6	6.8	5.2	4.9
40	20		20	40
		64.81		

Jewell

w. side - at Alley
Set B.M. - Nail in Pole

9.40 47.86

1+24.73 = S.L. Alley

INDEXED

MAY 4 1950

1+10 - 40.1 H. = 15' Conc. Dr. to Doub. Gar.

0+85

0+50

80 N. = 0+00 ahead = N.L. Thomas

40' N. = 4

2+69.68 - S.L. Thomas - 40.1 H. = end wall

Lt.

±

Rt.

35

46.4	46.6	46.6	46.2	46.2
10.9	10.7	10.7	11.1	11.4
40	20	40	20	40

46.76	46.49
10.50	10.77
50	40.1 = Dr.

floor
Gar.

46.3	46.3	46.1	45.9	45.9
11.0	11.0	10.9	11.4	11.4
40	20	40	20	40

46.5	46.3	46.2	46.0	45.7	45.5
10.8	11.0	11.1	11.3	11.6	11.8
40	20	40	20	40	80

Low
Point

46.4	46.5	46.5	47.0	47.0
10.9	10.8	10.8	10.3	10.3
40	20	40	20	40

46.5	47.1	47.5	48.1	48.5
10.7	10.2	9.7	9.2	8.7
40	20	40	20	40

46.86	47.9	48.7	49.1	49.5	52.3
8.40	9.4	8.6	8.2	7.8	5.0
40.1	40	20	40	20	40

Top
wall

57.26

20' cbs in on Grand - + walks

2+69.46 = S.L. Grand = end of cbs

2+35

2+00

1+44.73 = N.L. Alley

50.90	50.71	50.1	49.1	50.0	50.66	50.91
6.36	6.55	7.2	8.2	7.3	6.60	6.35
40.3	20.1	20.1		19.8	19.8	40
Cor. Ret.	Top end cb.	94.		94.	Top end cb.	Cor. Ret.
	47.8	48.1	48.1	47.9	46.9	
	9.5	9.2	9.2	9.4	10.4	
	40	20		20	40	
48.1	47.3	47.5	47.0	47.1	46.3	45.5
9.2	10.1	9.8	10.3	10.2	11.1	11.8
100	40	20		20	40	100
	46.3	46.6	46.1	46.4	45.9	
	11.1	10.7	10.6	10.9	11.4	
	40	20		20	40	

57.26

X-Sect Thomas - from Ingraham to
 200' E. of Jewell. 5-2-50
 W.O. 25020 7.0.

INDEXED
 N.K.
 MAY 4 1950

1+30 - 39.8 ft. = ± 8' Conc. Dr.

1+00

0+86 - 39.3 ft. = ± 2' Conc. walk

0+50

0+00 - E.L. Ingraham

0-40 - edge Conc. Pavc

49.4 52.42

47.48 - T.P. - P. 28

H. \$ Rt. 37

43.09
 9.33 10.23 10.93
 398 71 123 =
 Dr. Dr. end

46.09 46.02 45.4 44.7 44.3 43.9 43.1 42.8
 7.0 7.7 8.1 8.5 8.7 10.2
 40 20 20 40 100

6.33 6.40
 54 at Porch 38.3 walk

46.2 46.1 46.4 45.9 45.4 45.8
 6.2 6.3 6.0 6.5 7.0 8.6
 40 20 20 40 100

48.8 47.5 47.5 47.1 47.4 46.2
 3.6 4.9 4.9 4.7 5.0 5.7
 40 20 20 40 100

50.37 49.30 48.99 48.77 48.48 48.24 47.48
 2.05 3.12 3.43 3.65 3.94 4.18 4.94
 100 40 20 20 40 100
 52.42

Thomas

4+50

4+25- 40' Rt. = ± 3' Conc. walk

4+22- 39.8' Lt. = ± 3' Conc. Walk

4+00

3+94- 40' Lt. = ± 7' Dr. - 2' - 2' Conc. strips

3+89- 38.4 Rt. = ± 2.3' Conc. walk

3+50

3+26- 40.7 Lt. = ± 3' Conc. walk

3+17- 39.2 Rt. = ± 3' Conc. walk

3+00

Lt.

±

Rt.

39

~~46.6~~

~~46.9~~

~~46.1~~

~~46.3~~

~~46.4~~

~~46.5~~

6.4
40

7.0
20

6.9

6.7
20

6.6
40

6.5
55

47.07

46.87

46.34

46.34

48.59

5.95
55
walk

6.15
39.8
walk

6.68
40
walk

6.68
52
at Porch

4.43
55
floor
House

~~46.5~~

~~45.9~~

~~46.1~~

~~45.9~~

~~45.6~~

~~45.5~~

6.5
40

7.1
20

6.9

7.2
20

7.4
40

7.2
55

46.87

46.69

45.67

45.74

47.64

6.15
55
Dr.

6.33
40
Dr.

7.35
38.4
walk

7.28
53
at Porch

5.38
55
floor
House

~~46.6~~

~~45.6~~

~~45.3~~

~~45.0~~

~~44.7~~

~~44.3~~

6.4
40

7.4
20

7.7

8.0
20

8.3
40

8.7
65

46.92

46.61

44.62

44.85

46.44

6.10
53
at Porch

6.41
40.7
walk

8.40
39.2
walk

8.17
53
at

6.58
55
floor
House

~~45.9~~

~~45.9~~

~~44.3~~

~~44.3~~

~~44.0~~

~~43.7~~

7.1
40

7.7
20

8.2

8.7
20

9.0
40

9.3
60

53.02

Thomas

1+00

0+50

T.P. 9.13 60.75 1.40 51.62

0+00 = E.L. Jewell

check B.M. in Pole 0.62 52.40 52.41 -P.34

4+99 = 74 - w.l. Jewell

4+86 - 40 Rt = 3' Conc. walk

4+86 - 39.9 Lt = 3' Conc. walk

4+55 - 55 Rt = NW Cor. House

Lt.

±

Rt.

40

46.9	50.1	52.5	54.1	55.0	57.2	57.9
13.9	10.1	8.3	6.7	5.8	3.6	2.9
100	40	20		20	40	50

47.8	49.2	51.1	52.2	55.0	56.1
13.0	11.6	9.7	8.6	5.8	4.7
40	20		20	40	50

46.9	47.4	48.5	49.4	52.0
6.1	5.6	4.5	3.6	1.0
40	20		20	40

46.4	46.4	46.6	46.8	47.1
6.6	6.6	6.4	6.2	5.9
40	20		20	40

46.81	46.59
6.21	6.45
53.5	39.9
at porch	walk

46.72	46.82
6.30	6.20
40	55
walk	walk
46.8	47.44
6.2	5.58
55	55
ground	floor House

53.02

2+50 - end - 40.3' Lt. = Ely of 2.5' Conc. walk

56.99 57.12 57.3 57.8 57.9 58.1
 3.76 3.63 3.5 3.0 2.9 2.7
 53 40.3
 walk walk 20 20 40

2+33 - 39.2 Lt. = ± 6.3 Conc. Dr.

56.49 56.31
 4.26 4.44
 56.3 39.2
 floor Dr.
 Grav.

2+30 - 40.3' Rt. = ± 6.5' Dr. - 2 - 1.5' Conc. strips

58.10 58.11
 2.65 2.64
 40.3 65
 Dr. Dr.

2+00

56.5 57.0 57.6 58.0 58.4 58.8
 4.3 3.8 3.2 2.8 2.4 2.0
 40 20 20 40 60

1+96 - 39.6' Lt. = ± 3' Conc. walk

56.42 56.49
 4.33 4.26
 59 39.6 = walk
 walk

1+77 - 40' Lt. = ± 3' Conc. walk

56.26 56.47
 4.49 4.28
 59 40 = walk
 walk

1+50 - 40' Rt. = Ely. of 3' Conc. walk

56.0 56.5 56.7 57.2 58.2 58.75 59.01
 4.8 4.3 4.1 3.6 2.6 2.00 1.74
 40 20 20 40 40 51
 59.81 walk 56.17 walk 58.53
 Top 51

1+30 - 36.8' Rt. = ± 8' Conc. Dr.

60.75 2.94 2.58 2.22
 36.8 40 60
 Dr. Dr. Dr.

X-Sect 20 Alley in Block 270

for Grade est. & Drainage - See sketch - P. 29

w.o. 25020.

5-2-50 - 70.

PROFILE No 4156

INDEXED

W.K.
MAY 4 1950

1+25

1+00

0+50

0+00 = E.L. Ingraham

0-40 = edge Conc. Pave

B.M. 535 49.51

44.16 = c.t. Reel.
P. 28

A14	A10	A05	A06	A03
8.1	8.5	9.0	8.9	9.3
40	10		10	40

A14	A12	A11	A11	A02
8.1	8.3	8.4	8.4	8.8
40	10		10	40

A32	A26	A31	A38	A49
6.3	6.9	6.4	5.7	4.6
40	10		10	40

A62	A59	A60	A60	A51
3.3	3.6	3.5	3.5	3.8
40	10		10	40

A7.04	A6.64	A6.53	A6.40	A6.02
2.47	2.87	2.94	3.11	3.49
40	10		10	40

49.51

GMT

3+00

~~X2.4~~ ~~X2.0~~ ~~X1.8~~ ~~X2.2~~ Rt.
 $\frac{4.4}{40}$ $\frac{4.9}{10}$ 5.1 $\frac{4.7}{10}$

2+87.5

~~X2.2~~ ~~X1.6~~ ~~X1.8~~ ~~X1.8~~ ~~X2.2~~
 $\frac{4.7}{40}$ $\frac{5.3}{10}$ 5.1 5.1 $\frac{4.7}{40}$

2+62 - 17.3 Rt. = \pm Doub. Gar.

~~X1.45~~
 5.45
 17.3
 floor.

2+50

~~X1.4~~ ~~X0.8~~ ~~X0.8~~ ~~X0.8~~ ~~X0.8~~
 5.5 6.1 6.1 6.1 6.1
 40 10 10 10 20

2+00

~~X1.4~~ ~~X0.8~~ ~~X0.8~~ ~~X0.8~~ ~~X0.6~~
 5.5 6.1 6.1 6.1 6.3
 40 10 10 10 40

1+80 - 15' Rt. = \pm Sing. Gar.

1+75

~~X1.3~~ ~~X0.7~~ ~~X0.6~~ ~~X0.6~~ ~~X0.7~~ ~~X1.13~~
 5.6 6.2 6.3 6.3 6.2 5.75
 40 10 10 10 40 15
 floor.

T.P. 6.19 46.88 8.82 40.69

46.88

1+62 - 15.8 Rt. = \pm Doub. Gar.

~~X1.21~~
 8.30
 15.8
 floor
 Gar.

1+50

~~X0.9~~ ~~X0.8~~ ~~X0.5~~ ~~X0.5~~ ~~X0.3~~
 8.6 8.7 9.0 9.0 9.3
 14.7 10 10 10 40
 along House 49.51

4+09 = Beg. High Slab.

4+06 = Ely. of Level Slab.

4+00

3+88 = 11.4 Rt. = Beg. Conc. apron to Row of Gar.

3+70

T.P. 10.69 56.91 0.66 46.22 - Nail in pole 3+75'

3+50

3+43 = 22' Lt. = 11' Conc. Slab.

3+25

3+18 = 20' Lt. = 2' Doub. Gar. - Conc. floor.

3+09 = 16.9 Rt. = 2' Doub. Gar. - Conc. floor.

4841 Rt. 44
 8.50 8.29
 11.4 16.4
 Conc. 17.42
 9.49 9.29
 11.4 16.4
 Conc. 17.62

A5⁶ 11.3 40
 A6⁶ 10.3 10
 A6⁹ 10.0
 A7² 9.7 10
 A9.23 9.68 11.4
 Conc. 16.4
 16.4 Floor Gar.
 A6.96 9.95 11.4
 Cor. 17.05 9.86 16.4
 Line of Gar.

A4¹ 12.8 40
 A4⁶ 12.3 10
 A4⁷ 12.2
 A5⁰ 11.9 10
 A6² 10.7 40

56.91
 A3⁶ 3.1 40
 A3⁸ 3.1 10
 A4⁰ 2.9
 A4² 2.7 10
 A5⁰ 1.3 40

3.19 22 Conc.
 A3⁰ 3.9 10
 A2⁸ 4.1
 A3⁰ 3.9 10
 A3¹ 3.8 40
 To W. 4.05
 To E. 16.9 floor

46.88

4.05
16.9
floor

Thomas + Jewell - P. 34
Check. B.M. = spike in Pole: 4.51 52.40 - 52.41

4+99.80 - W.L. Jewell - end.

55.4
1.5
10
55.9
1.0
57.3
+ 0.4
10

4+70

51.6
5.3
40
52.8
4.1
10
53.4
3.5
54.0
2.9
10
54.2
2.2
13.8
along House

4+64 - 10.9 Rt. = end Conc. apron

52.72
4.19
10.9
52.07 Cor.
4.84
11
Cor.
54.32
2.59
10.9
Top of Ret wall
52.71
4.20
15 on walk
52.68
4.23
15 = floor
Grav.

4+40.5 - 11' Rt. = Beg. Conc. apron to Doub. Crar.

4+30

48.4
8.5
40
48.9
8.0
10
49.5
7.4
50.1
6.8
10
52.1
4.8
36
49.15
7.73
11.4
49.48 Cor.
8.43
11.4
To W.
54.86
2.08
36
Top Ret wall
49.49
7.42
16.4 =
Floor
Grav.

4+26 - 11.4' Rt. = end Conc. Slab

49.11
7.80
11.4
To E.

4+17 - Vert. Rise in Conc. Slab.

56.91

X-Sect. 20' Alley in Blocks - 251 + 250
 for Grade Est. - sketch - P. 26
 w.o. 250 20 (PROFILE # 4155) 5-3-50 - 70

T.P. 5.87 53.98 9.11 48.11
 1+25- 10.3' Rt. = E 2' Conc. Walk Thru Conc. wall

0+80- 12.2 Rt. = wly of Conc. apron - to Doub. Gar.

INDEXED

MAY 4 1950
 W.K.

Sec 110 # 33128 - Loose Leaf
 # 23/60 - ALLEN -

0+00 = E.L. Ingraham.
 Beg. Block 251

0-40 = Edge of Conc. Pavc.

B.M. 137 57.22

55.85 N.E. B. P. Grand + Ingraham

57.22

Lt. Rt. 46

	493	482	480	4788	47.70
	7.9	9.0	9.2	9.34	9.52
	10		10	10.3	10
				walk	
	525	512	502	50.79	50.85
	4.7	6.0	6.5	6.43	6.37
	10		10	12.2	14.9
				apron	floor
					Gar.
	522	518	519		
	5.0	5.4	5.3		
	10		10		
	521	519	516		
	5.1	5.3	5.6		
	10		10		
	5267	5192	5174	51.57	50.82
	4.55	5.30	5.48	5.65	6.40
	50	10		10	50

4+00

3+50

3+13 - 10.1' Rt. = ± Conc. apron to Doub. Grav.

2+00

2+63 - 10.1' Rt. = ± Conc. apron to Doub. Grav.

2+50

2+00

1+65

Lt.

#

Rt.

A76

6.4
10

A75

6.5
10

A73

6.7
10

A85

5.5
10

A82

5.8
10

A72

6.2
10

A8.11

5.47
10.1
apron

A8.38

5.60
14' = floor

A86

5.4
30

A88

5.2
10

A84

5.6
10

A83

5.7
10

A79

6.1
30

A8.47

5.51
10.1
apron

A8.56

5.42
14
floor
Grav.

A88

5.2
10

A84

5.6
10

A82

5.8
10

A88

5.2
30

A86

5.4
10

A84

5.6
10

A78

6.2
10

A75

6.5
30

A94

4.6
10

A86

5.4
10

A80

6.0
10

53.98

1+50

LT	A5 ⁸	A6 ²	A6 ⁴	RT
	9.1	8.7	8.5	
	10		10	

1+00

A5 ⁷	A5 ²	A5 ¹	A5 ⁴	A5 ³
9.2	9.7	9.8	9.5	9.6
50	10		10	30

0+50

A5 ²	A5 ¹	A5 ³
9.7	9.5	9.6
10		10

0+00 = E.L. Jewell

A5 ⁹	A5 ⁹	A5 ⁸
9.0	9.0	9.1
10		10

Req. X-Sect. of Alley in Block 250

T.P. 709 54.94 6.13 47.85 on N. in pole - P 35

54.94

4+99.90 = W.L. Jewell

A6 ⁴	A6 ²	A6 ³
7.6	7.8	7.7
10		10

4+50

A6 ⁸	A6 ⁸	A6 ⁵
7.2	7.2	7.5
10		10

Converted to House 4/23/60

4+12 - 10' Rt. = E Conc. apron to Doub. Gar.

53.98

A7.50
6.48
10
apron
A7.68
6.30
14
floor

4+99.64 = w.L. Kendall

4+88- 9.8' Lt. = end House

4+68- 10' Lt. = Beg Stucco House (far.)

4+50

51.9	53.38	53.3	53.4	53.8	53.4
8.4	7.34	7.4	7.3	6.9	7.3
50	11.7	10		10	50

edge Conc.
Apron

54.1	54.1	54.5	55.2
6.6	6.6	6.2	5.0
9.8		10	20

at House

54.72
54.5

6.00 6.2
10 10
floor along
House

55.2	55.5	55.5
5.5	5.2	5.2
10		10

60.72

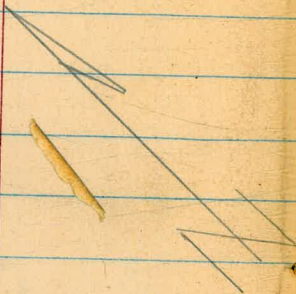
D. Smith
Wm. Fay
E. Sherman
R. Lockwood

Cross Sec Arista (Dr) Street

Jefferson Ave to La Jolla Ave.

INDEXED

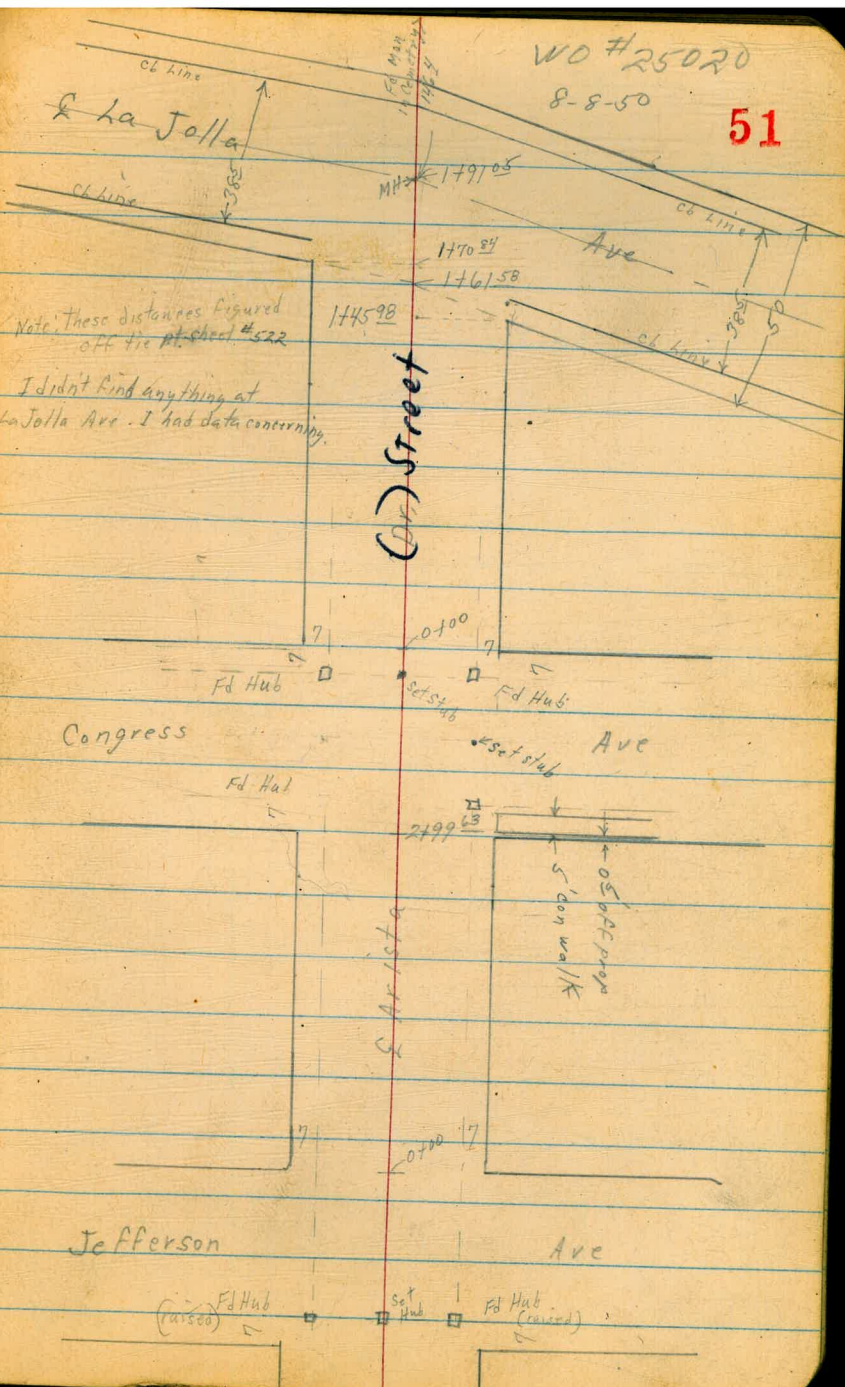
Y.P.K.
AUG 9 1950



WO #25020

8-8-50

51



Note: these distances figured off the pt. ch. #522
I didn't find anything at La Jolla Ave. I had data concerning.

Jefferson Ave

(raised) Fid Hub set slab Fid Hub (raised)

D. Smith
Wm. Fay
E. Sherman
R. Lockwood

Index

Cross Sec Arista Dr

Jefferson Ave to La Jolla Ave

Lt. North

Rt. South

WO # 25020

Volume 8-50

52

0+00 East line Jefferson

21.7	23.2	22.8	21.9	22.7	22.7	25.6	26.9	27.4
62	54	58	62	52	52	30	17	12
50	25	20	15		11	15	25	50

0-15'

20.7	22.2	21.1	21.6	21.6	22.4	25.4	26.2
72	64	75	70	71	62	32	24
50	25	15		10	15	25	50

0-25' E Jefferson E. edge Cold hay

17.8	19.7	20.4	21.0	21.6	21.8	22.0
102	82	82	76	70	68	66
50	25	15		15	25	50

0-40' W edge cold hay

20.1	20.1	20.6	21.2	21.8	22.5
85	85	80	74	68	64
25	15		10	15	25

0-50' West line Jefferson

18.4	16.9	19.6	19.8	20.2
102	92	90	88	84
25	15		15	25

TP, 138 2858 952 2720

BM, 124 3672

SEBP Arista
La Jolla Ave
FB 1459-47

28.6

2858

Lt = North

£

Rt = South

53

1467 25⁵ Rt £ 6" cast iron drain outlet

1450

1404 21° Rt £ Deadman

TP₂ 5⁰² 31³⁰ 24⁰ 26¹⁸

1400

0498 21° Rt £ Deadman

0495 26° Rt £ 12" Pepper tree

0466 20⁸ Rt £ 12" Guy pole #3909

0462 24⁵ Rt £ 14" Pepper tree

0450

0425

234
FK 20⁵
26.2 26.5 27.2 26.5 29.1
5⁰ 42 4⁰ 32 21
25 15 15 25

3/20

25.8 25.6 26.1 26.4 27.0 28.6
2⁸ 3⁰ 2⁵ 2³ 1⁶ 0⁰
25 15 12 15 25

25.3 29.0 25.0 25.3 27.1 27.6
3³ 4⁶ 3⁶ 3³ 1⁵ 1⁰
25 15 15 21 25

26.2 25.5 23.3 24.3 24.2 25.8 27.2 27.7 28.3
3⁴ 3¹ 5³ 4³ 4⁴ 2⁸ 1⁴ 0² 0³
50 25 15 12 15 20 25 50

28⁵⁸

LT = North E RT = South

3+09⁶³

3+05¹³ con walk end
 (3+00¹³ con walk end (on congress))

2+99⁶³ West Line Congress

21 A3
 322 End
 27 59
 3 62 End
 30 08
 12
 50 up walk
 congress

25.8	26.0	25.0	25.9	26.3	27.8	28.6
54	57	62	53	49	38	26
50	25	15		15	25	50
25.6	26.0	25.7	25.8	26.3	27.2	28.9
56	52	55	58	55	42	40
50	25	15	12	15	25	50

2+77 27⁵ RT & 12" pepper tree

2+75

2+62 17⁵ LT & 12" gay pole # gone

2+53 17² RT & Dead man

2+50

2+17 27⁸ RT & 18" pepper tree

2+00

25.6	26.1	25.9	26.2	26.7	29.6	30.8
56	51	53	50	45	16	04
50	25	15		15	25	50

25.8	27.0	27.0	26.7	27.1	29.9	31.5
54	42	42	45	41	13	10.3
50	25	15		15	25	50

26.4	26.6	27.2	27.8	29.7
48	46	40	34	15
25	15		15	25

3/20

0+25^s 35° Lt SE cor House

0+25

0+100 = s 23° Lt Begin Flower Hedge
3+49⁶³ East Line Congress

3+39⁶³

3+35⁶³

3+24⁶³ & Congress

3+10⁶³

Lt = North

qt = South

55

29.16

204

Floor
of house

26.1	26.6	26.9	26.6	26.4	28.5	29.2	29.8
51	44	43	46	48	22	20	14
35	25	15		9	15	25	50
25.6	26.2	26.5	26.1	26.2	27.5	28.0	28.2
56	50	42	52	50	37	32	30
50	25	15	13	11	13	15	20
25.9	26.1	26.3	25.7	26.1	26.9	27.8	28.6
58	51	42	55	51	43	34	26
50	25	17	15	15	25	50	
23.6	24.9	25.4	26.3	26.6	26.8	27.6	
76	63	58	42	46	44	35	
50	25	15	15	15	25	50	
24.1	25.1	25.6	26.0	26.7	27.1	27.8	
74	64	56	48	45	44	34	
50	25	15	on	15	25	50	
23.6	25.2	25.9	26.3	26.6	27.6		
74	66	53	42	45	36		
50	25	15	15	25	50		

3/20

1446 24² Lt End 4' picket fence

1445⁹⁸ SW Cor La Jolla Ave

1425

1417 16° RT & 14" Power Pole #3975

1400

0494 58° Lt SE Cor House

0486 24² Lt & Single garage con floor + driveway ^{11 1/2 wide}

0478 24⁵ Lt End Flower Hedge

TP₃ 1131 39⁰⁵ 34⁶ 27⁷⁴

0450

0430 24² Lt Begin 4' picket fence

Lt = North

RT = South

30.2	31.3	31.6	31.7	32.8	33.4
82	75	75	74	63	47
50	25	15	15	15	25

28.9	29.5	29.4	28.9	38.4	30.4	35.1
102	96	92	103	92	82	40
50	25	15	15	15	25	50

28.1	28.2	28.3	27.6	24.3	29.0	30.2
110	102	108	115	108	101	82
50	25	15	15	15	25	50

30 24
8 81
580
Floor

27 29
11 56
45 Floor
27 05
11 10
242
Floor drive end

39 05

222	274	274	272	29.5	30.1
40	38	46	40	12	11
25	15	15	8	15	25

31 20

BM starting

35⁵⁸ 35⁴⁹ 35⁴⁸

1491⁰⁵ Int E LaJolla Ave & Arista Ave
Taken along LaJolla Ave

1470⁸⁴ NW cor LaJolla Ave

1468^E Int West E Line LaJolla Blvd extended &
E Arista Also edge A.C. paving
Taken along LaJolla Ave lines

1461⁵⁸ Int West Propinas LaJolla Blvd and
E Arista Ave

Reduced
J.T. Lando 87

33.81	33.95	34.21	34.39	34.68	34.99	35.23	35.75	36.41
5 ²⁴	5 ¹⁰	4 ⁸⁴	4 ⁶⁶	4 ³⁷	4 ⁰⁶	3 ⁸²	3 ³⁰	2 ⁵⁸
69E	50	25	15	14 rim	15	25	30	84

33.5	33.9	34.25	34.5	34.82	35.25	35.5	35.51	36.11	36.77
5 ⁶	5 ²²	4 ⁷⁶	4 ²⁶	3 ²¹	3 ⁸⁵	3 ⁵¹	3 ⁵¹	3 ⁵¹	3 ⁵¹
69E	69E	19E	19E	15	15	25	34E	34E	84
06	94	06	94	end.	end.	94	06	94	06

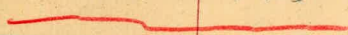
39⁰⁵

LOCATION PROPOSED DRAIN

111 MORENA BLVD. AND MILTON ST.
Walker
Pape 10-22-51 410 20897
Huffman

Also see F.B. 2190

1+3



8" line

7" line Cont. P. 59

1+59.10 = Δ 90°23' RT

1+67.3 = East end Wooden Bridge

0+98.22 = East Track Santa Fe RR.

0+84.15 = Main line Santa Fe RR Track

0+74.5 = West end Wooden Bridge

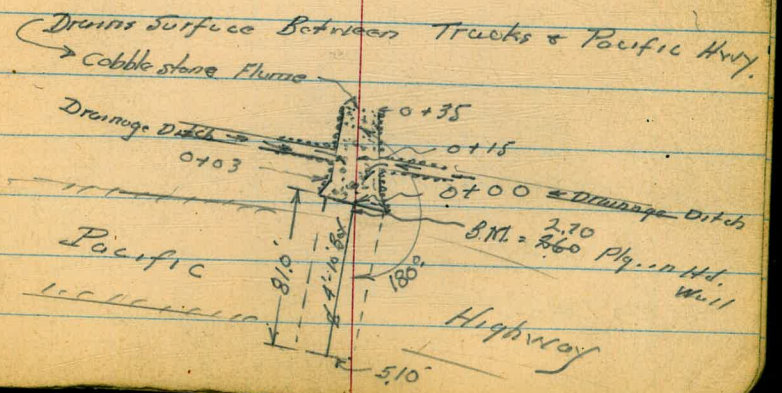
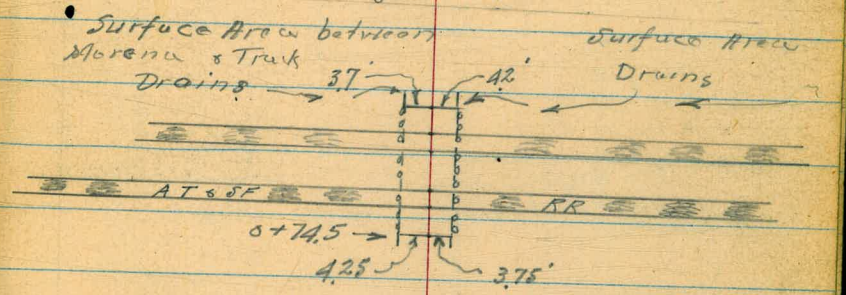
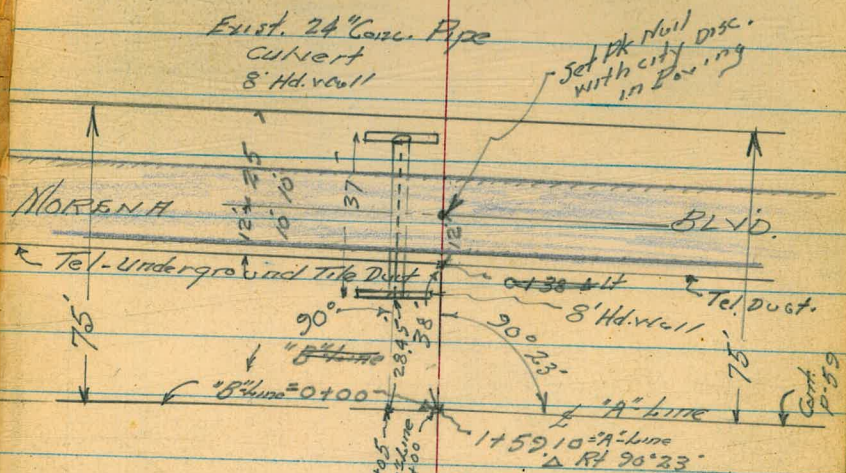
0+00 "A" line = East End Existing 4'x10' Box Culvert

INDEXED

LOW

NOV 27 1951

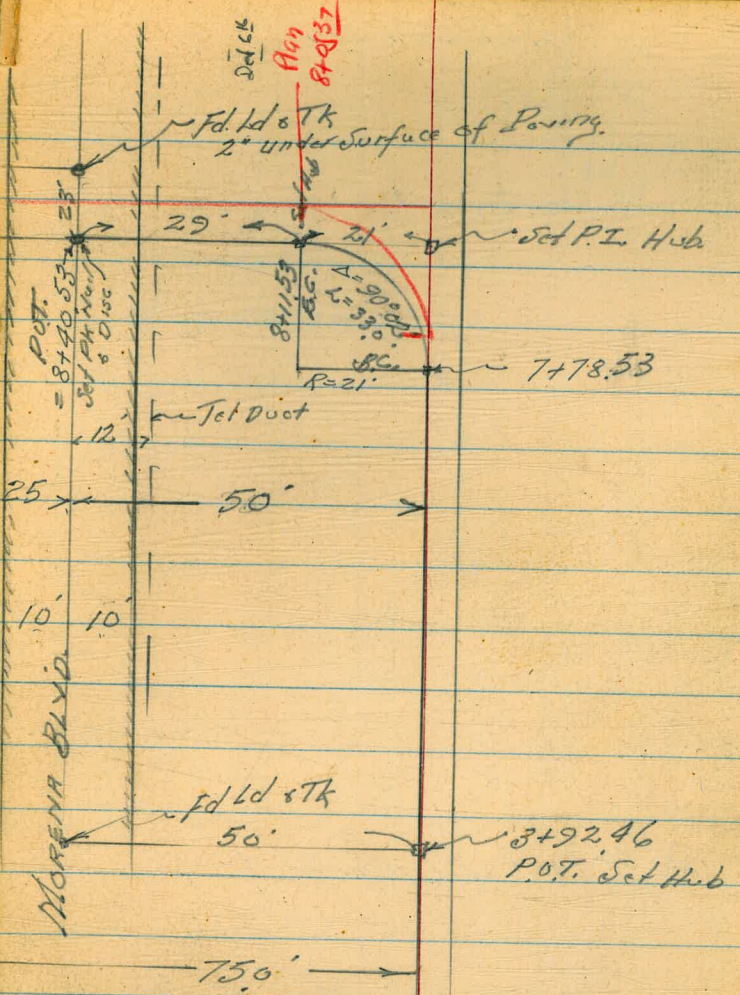
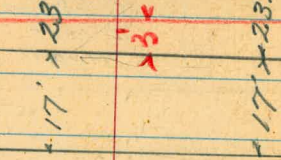
58



Location Proposed Drain
"A" line

See 9355-L

MILTON



3+92.46 = POT. Hub

Water

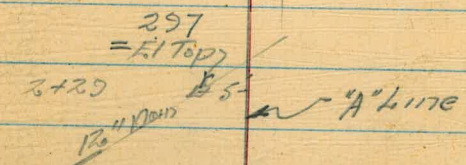
Fol. Ld & Tk
50'

3+92.46
POT. Set Hub

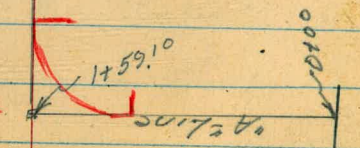
750'

2+29 (5'4") Top	1016	2.97	
on 12" Water Main			
5.61	13.13	7.52	1459.10
1+59.10			

Mon Hub
P-62



See 9355-L



Location
"A" Line

60

Vol. Pipe
L.S. #2317

17' x 63'

GALVESTON

MILTON

17' x 63'

23494.65 - Sec F.B. 2180-5 C.H.S. 1/3/52

22 + 40.54 = P.O.T. Set Hub. Plan Sta = 22224.37

16 + 00.08 = P.O.T.

"A" line
Levels for Culvert.
Location P-58-60

Lt

Rt

Rt

61

0+50

2.5
2.0
2.5
15

0+35 = End Cobble Flume

2.90
8.59
5.0
Top
1.05
10.46
4.5
Flow
0.86
10.63
Flow
1.22
10.27
2.5
Flow
2.86
8.63
3
Top Wall

0+15 = North & South Ditch

1.08
10.41
19
End Cobble
Ditch
0.67
10.82
4.5
Cobble
Flow
-0.20
11.69
cobble
Flow
0.90
11.09
4.5
cobble
Flow
0.78
10.71
17
End
Cobble
Ditch

0+03

1.95
9.54
4.5
Top Wall
-0.97
12.46
4.5
Flow
Cobble
-1.17
12.66
Flow
Cobble
-0.66
12.15
4
Flow
Cobble
2.19
9.30
4.5
Top Wall

0+00

9.06
14.55
invert

0-81.0

-2.57
15.00
invert

8.79

11.49
H. 39

2.70 P. 78
4.00

Starts Hwy.
B.M. Steel Plg End Box Culvert 0-00.40

11.49

3+00

2+49 15³ Rt. = Top of water main + 1.95 = EL.

2+29 5² Lt. = " " " " Top of pipe 2.96 = EL.

2+00

1+59.10 = Rt 90° 23'

1+25

1+07.3

0+96.5 = Rt Rail of E. Truck 2.93

0+81.73 West Rail Main line 2.27

0+74.5

11.49
~~11.79~~
2

Lt.

Rt.

5.7	6.0	7.5	8.3	8.4
5.8	5.5	4.0	3.2	3.1
16	10	6		15
Ditch				

5.7	6.0	7.9	8.8	8.1
5.8	5.5	3.6	3.5	3.4
16	13	5		15
Ditch				
North				
South				

7.52 = Flange Hub
3.97 = Rod on Hub.

5.2	4.8	4.3	5.0	5.2	5.2
6.3	6.7	7.2	6.5	6.3	6.3
15	5	4	3		15
Ditch					

2.4	2.4	6.06
8.1	4.15	5.43
	0	0
	Top Deck	Top Deck
		Bottom

2.4	6.24	2.33
8.1	5.25	4.16
	0	0
	Bottom Deck	Top Deck
11.49		

8+1153 = E.C.

7+7853 = J.G. 21' R

7+00

6+00

5+00

4+00

TR

9.06

18.41 ✓

18.31

2.14

9351

925

1149

Lt.

Rt.

9.2

9.56

10.0

9.2

885

8.4

20
Ditchon Hub
Ditch.15
Ditch

9.2

9.0

12.1

12.65

13.4

9.2

9.4

6.8

5.76

5.0

20
L Ditch

12

5

on Hub.

15

9.2

8.4

11.2

12.7

12.9

10.2

10.0

7.0

57

5.5

20

15

8

57

15

L Ditch

7.3

7.6

10.6

11.3

11.8

11.1

10.8

7.8

7.1

6.6

17
L Ditch

11

5

7.1

15

6.7

7.3

9.5

10.5

10.6

11.7

11.1

8.9

7.9

7.8

18

12

6

7.9

15

L Ditch

6.0

6.4

9.1

9.5

9.8

12.4

12.0

9.3

8.9

8.6

17

12

7

8.9

15

L Ditch.

992

992

RM

MH

18.41 ✓

8+65

$$\begin{array}{r} 13.8 \\ 4.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 13.8 \\ 4.6 \\ \hline 8 \end{array}$$

$$\begin{array}{r} 11.2 \\ 7.2 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 11.2 \\ 7.2 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 11.2 \\ 7.2 \\ \hline 15 \end{array}$$

8+60

$$\begin{array}{r} 11.1 \\ 7.3 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 11.1 \\ 7.3 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 11.1 \\ 7.3 \\ \hline 15 \end{array}$$

8+50.53 = Fast edge

$$\begin{array}{r} 10.92 \\ 7.49 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 10.98 \\ 7.43 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 11.07 \\ 7.34 \\ \hline 15 \\ \text{Por.} \end{array}$$

8+40.53 = Por.

$$\begin{array}{r} 11.10 \\ 7.31 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 11.16 \\ 7.25 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 11.21 \\ 7.20 \\ \hline 15 \\ \text{Por.} \end{array}$$

8+30.53 = West edge Poring

$$\begin{array}{r} 10.91 \\ 7.50 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 10.95 \\ 7.46 \\ \hline 15 \\ \text{Por.} \end{array}$$

$$\begin{array}{r} 11.00 \\ 7.41 \\ \hline 15 \\ \text{Por.} \end{array}$$

8+22

$$\begin{array}{r} 10.9 \\ 7.5 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 11.1 \\ 7.3 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 10.8 \\ 7.6 \\ \hline 15 \end{array}$$

8+18

18.41

$$\begin{array}{r} 9.2 \\ 9.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 9.6 \\ 8.8 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 10.4 \\ 8.0 \\ \hline 15 \end{array}$$

18.41 ✓

"A" Line

13+00

12+00

11+00

10+88.7 = East Side Ribbon Drive

10+79 = West Side Ribbon Drive

TR 11.84

10+00

9+00

18.41

18.34

7

2' wide Ribbons

17.92

17.82

Lt.

f

Rt.

25.7
41
15

22.8
7.0
15

20.0
9.8
15

26.4
3.4

22.8
7.0

20.0
9.8

19.40
10.36
DRIVE

19.44
10.32

39.76

17.3
1.1
15

14.2
4.2
15

14.2
4.2
3

12.4
6.0
18.41

25.0
4.8
8

22.4
7.4
15

19.4
9.9
5

19.4
10.4
6

19.38
10.38
3'
on End
DRIVE

19.39
10.37
3'
End
DRIVE

17.0
1.4
15

13.0
5.4
15

65

4.2
15

25.6

19.7
10.1
15

"A" line

17+30

16+23

16+81 64' Pole Tel # H- 988067

16+00 08 = POT.

15+50

15+05

15+00

TR 12.98

14+00

42.67

~~42.57~~

29.76
29.66

007

29.69
29.59

14

33.09
15 33.2

4.2
15 38.5

7.2
15 35.5

84
15 34.3

9.7
15 33.0

10.32.7
15 32.8

0.220
15 31.7

28.8
15 31.0
29.76

33.09
33.2

4.5
38.2

7.41
on Hub 35.26

82
34.5

9.0
33.7

11.0
42.67
31.7

28.8
15 31.0
29.76

TH

4.5
9 38.2

5.8
9 36.9

8.7
8 34.0

9.7
7 33.0

9.9
15 32.8

11.2
7 31.5

2.1
27.7

4.2
15 34.5
66

5.2
15 37.5

8.0
15 34.7

9.0
15 33.7

9.9
15 32.8

10.2
15 32.5

15.6
28.8

*A^c Line

20+13

20+00

19+92 = East edge Drive

19+77 = West Edge ^{Cont.} Diner Way

19+28 17' Lt = Tel Pole # 90844-H

19+15 = ^{Top Box 970} Two Water Meter Boxes 1' Lt = South edge Box.

19+00

~~57.98~~

54.08¹

~~53.98~~

12.04

0.37

42.04¹

~~41.94~~ 42.03

42.30¹

~~42.20~~

T.P. 11.78

18+19 = Tel Pole 7' Lt # 488068-H

18+00

42.67

~~42.57~~

H.

7.47.1
15

46.4
7.7
15

46.10
7.98
7
DRIVE

46.15
7.93
7
DRIVE

43.2
10.9
15

43.0
11.1

5408¹
~~53.98~~

BM

SW. BR Erie + Milton St - P-78

Nail

SW Pole Erie + Milton

41.1
1.6
15

41.1
1.6
42.67¹

38.7
3.0
9

40.2
2.5
15

45.5
8.6
9

45.1
9.0
9

46.2
7.9
15

45.8
8.3
15

67

A^c Line

22+20

22+16 = Air channel

TR 1070

22+00

21+50

21+00

20+70 = Bag channel

20+46 = 7' Lt = Pale 90845-H

54.08

Tel

~~53.98~~

Lt.

Rt.

Rt.

68

50.4

49.3

50.4

54.6

54.6

54.2

12.8
15

13.9
8

12.8
9

8.6
9

8.6
15

10.0
17

L Wash

50.4

12.8
15

50.0

13.3
10

48.9

14.3
3
ch

45.9

14.3
3
in ch

48.9

55.5

53.1

7.7
10
Bank

10.1
15

63.18

67.08

1.60

52.98

52.38

53.1

1.0
15
Bank ch.

50.1

1.0
10
ch

50.2

3.9
ch.

49.1

5.0
9
ch.

52.5

1.6
16
Bank ch.

53.1

1.0
15

53.0

1.1
9
Bank ch.

48.8

5.3
5
ch.

49.0

5.1
ch

48.0

6.1
ch

50.9

3.2
15
Bank ch.

51.7

2.4
15

51.5

2.6
4
Bank ch.

49.4

4.7
ch

47.4

6.7
15
ch

44.1

5.0
13

50.0

4.1
15

49.0

6.1
ch

48.5

5.6
15

49.6

4.5
15

48.5

5.6
15

47.3

6.8
ch

47.6

6.5
15

~~54.28~~
~~53.98~~

"A" Line

24+40 = 1 in ch on Lt.

24+00

23+80 9' Lt = 24' Tree (Dead)
8' Lt

23+68 = 8' 4' Tree cluster (Dead)

23+62 8' Lt & 2' Stump

23+40 9' Lt = 3' Euc Tree

23+31 6' Lt 3' Euc Tree

23+20 7' Lt = 8' cluster 4 Trees

23+00

22+84 = 9' Lt & 4' Euc Tree
8' Lt

22+78 9' Lt = 4' Euc Tree
8' Lt

22+60

22+46 6.5 Lt = Pola # 90846-H
Tel.

22+40.54 - P.O.T.

22+30

63.18

52.3 Lt
9.9 54.2
80 4.0
66 3.1
50 60.1
6.9
1.8
62.2 Rt
1.0
15

52.2
11.0 57 4.5 3.7
58 40 17
E. Bank
ch

56.8 50.4 56.4 56.8 55.4
6.8 12.8 6.8 7.4 7.8
37 31 20 15
N Bank ch E. Bank ch Bank ch

49.9 49.9 55.0 54.7 55.1 54.3 54.3
13.3 13.3 8.2 8.5 8.1 8.9 8.9
45 36 30 12 13 20
N Bank ch E. Bank ch South Bank ch

55.04
8.14
0.1
Hub.

57.4
11.8
25

50.4 49.2 55.3 55.3
12.8 14.0 7.9 7.9
17 12 2 63.18
ch ch

8.54.9
8.3
15

U.S.G.S Mon Tallett & Morera

chk

2.71

$\frac{.05}{11.673 = \text{Moore}}$
11.72

→ FB 1647-80

11.73 14.43

2.70

→ B.M. Hd Wall P. 78 P. 61

Diff = ~~0.05~~

chk starting B.M.

4.73

~~2.70~~
~~2.65~~
2.65

→ B.M. Hd Wall
→ This B.M. Given 2052 = U.S.C. & G. in My Field B.M. Book
 $\frac{2.61}{11.51} = \text{city Datum}$

~~2.71~~ 14.38

~~4.673~~

U.S.G.S B.M. Mon SW Cor Tallett & Morera Blvd
FB 1647-80

chk. starting B.M. P-61 10.10

$\frac{0.014}{2.70}$
~~2.60~~
2.71

→ B.M. in Hd Wall 0-00.4

T.P. 3.44 12.81 6.76

9.37

T.P. 1.94 16.13 12.57

14.19

T.P. 0.19 26.76 12.21

26.57

T.P. 0.33 39.48 12.87

39.15

T.P. 0.88 52.02 8.52

51.14

Diff. $\frac{0.06}{55.13 = \text{B.M.}}$

T.P. 6.45 59.66 2.97

53.11

chk. N.V.I. B.P. Napier & Frankfurt FB 1590-48

59.56
53.18
63.48

Levels - Proposed Culvert
 ~ "B" Line ~
 Location P-58

0+45

0+20

0+15

0+05 Cont.

0+05

0+00 Cont.

- 0+00 "B" Line
 1+59.10 "A" Line

5.24 13.46 ✓
 13.36 -
 7.52 ✓
 7.42

Lt.	R.	1st.
6.6	8.1	6.9
15	13	6.6
		7.5
		8
		7.8
		22
		6.0
		5.7
		4.8
		7.0

Lt.	R.	1st.
6.1	5.9	5.0
7.4	7.6	8.5
15	9	
		5.3
		6.1
		7.3
		24
		7.3

8.21	9.03	9.19	6.34
825	543	427	7.12
2845	2845	6545	6545
Invert	Hub	Hub	Invert.

Lt.	R.	1st.
7.8	7.42	
5.7	6.04	
12	Hub	
		7.5
		10
		6.0

9.06	8.61	8.8	7.0
4.40	4.65	4.7	6.5
50	6.0	87	7.0
Hub	East Edge	Post	

Lt.	R.	1st.
7.8	7.52	
5.1	5.24	
12	13.46	
	13.36	
		7.2
		10
		6.9
		24
		48
		30
		46.5
		50
		Post
		W. edge

B. Mon Hub 1+59.10 "A" Line P-62

2+21 30' RT Tel Pole 415021-H

2+00 Cont.

(Station Not Taken in order) 36"
2+07 - E.M.A 10' RT, E. Euc Tree 31.5' RT

2+00

1+82

17' RT - Pole Anchor 31.5' RT # P-3199
Elec. Pole

1+70

1+50

1+33 ~24" Euc Tree 31.5' RT

1+00 Cont.

1+00

13.46

0+94 = Tel Pole 415022-H 31.5' RT

0+31.5 - 10" Euc Tree 31.5' RT

13.46
~~13.96~~

4 2 RT 72

9.63
383 395 36
50 60 70
Elev. Elev.
8.76

9.5
4.7 4.2
15 17 34
5.2 4.1 4.03
8.3 9.4 9.43
470
10
Rim
774

9.1 9.2
4.4 4.3
15 10 13
8.9 7.6
7.3 8.3
6.2 4.2
2.2 2.8

9.09
437 413 433 39
40 50 60 70
Pov Pov Pov

7.8 7.7
15 18
5.7 5.8
6.1 6.0 8.5 8.9
7.4 7.5 5.0 4.6
12 18 25 33

Drum
"B" Line

Reduced By
C.Rh. 12-3-51

S.V. Cor Jellott & Morano

Ch. B.M. USGS P-70

TP	7.16	16.03 ^v	4.59	8.87 ^v
		15.93		8.77

3+00 Cont.

3+00

13.46

2+80 31' RH = 8" Euc Tree

2+57 63' RH = 32" " "

13.36

73

N ←

Morano

Blvd.

Elev. 11,673-city data Mon About 2' Deep.

USGS B.M. Mon.

Siding AT & SF

27.20'

Christed cross
in Conc. Base

Digital Block

AT & SF

Christed cross
in Conc. Base
Santa Fe Signal Block

6.27'

14

15

16

9.79	10.06	9.92	10.4
3.67	3.40	3.54	3.1
38.3	48.3	58.3	68.3
Par. edge	Par. edge	Edge Par.	

14.4

14.87

14.2

14.5

14.53

5.1

4.59

4.3

3.0

3.23

15

on Hub

15

27

30

13.46^v

13.36

Cross Sec. Pt Loma Ave.
Santa Barbara Ely.

W.O. 25020

9-24-52
C.H.S.
Be99
altman
Johns

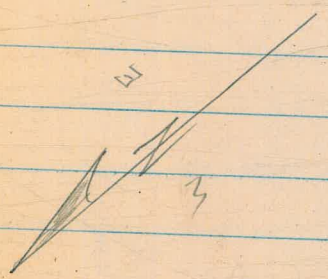
Nly. cl. line
Point Loma Ave

-- 1+35.7

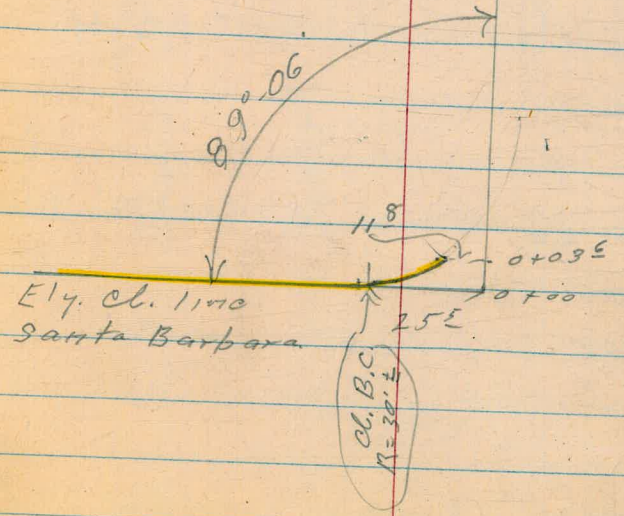
Ely. cl. line Santa Barbara = 0+00
Nly. cl. line Pt. Loma Ave = Base line

E.P. = edge of good A.C. pave. to
be met for grade.

23' At. = $\frac{1}{2}$ Pavement to East.



INDEXED
Law
OCT 27 1952



Pt. Loma Ave
 Santa Barbara East.

T.P. 12.70 205.94 0.18 193.24

0+20

0+10² = leave pavement

0+03^e 11⁸ Lt. = end existing cl.

0+00 25⁵ Lt. = B.C. 30' Rad cl. Ret.

E.P. denotes edge of good A.C. Pavc.
 Nly. cl. line Pt. Loma. = Base line

4.90 193.42 - 188.52

B.L.

75

261.91	85.06	190.78	190.71
2.0	2.74	2.64	2.71
	7	10	23
	E.P.		

199.71
 8.70

3.88	4.48	4.12	3.95	4.15
11.8	11.8		10	23
cl.	cl.			
	also E.P.			
189.28	189.53	189.11	189.17	189.02
4.14	4.89	4.31	4.25	4.40
25 ⁵	25 ⁵		10	23
cl.	cl.			

193.42

S.E.B.P. Santa Barbara + Pt. Loma Ave.

L+T. Marked
M.E. Cor. PL 172 8.29 206.30

1+60

J.P. 9.58 214.59 0.93 205.01

Start Conc. Cl. on B.L.
1+35.7 = start full width A.C. Pavc.

1+20

1+00

0+70

0+40

B.L.

206.98	206.48	206.79	207.01
7.61	8.11	7.80	7.58
B.L.	B.L.	10	23
Cl.	G		
214.59			
10.25	204.44	204.59	204.71
0.93	1.50	1.35	1.23
B.L.	B.L.	10	23
Cl.	G		
202.5	202.69	202.84	203.04
3.4	3.25	3.10	2.90
	5	10	23
	E.P.		
200.2	200.34	200.49	200.64
5.7	5.60	5.45	5.32
	5.5	10	23
	E.P.		
177.69	177.02	176.69	
8.25	8.92	9.25	
	10	23	
	E.P.		
193.94	192.94	192.84	
12.0	13.00	13.10	
	10	23	
	E.P.		

205.94

77

Check Levels on B.M.s

for Drain Project ~ Milton St
And Morena Blvd.

Walker
Page
Huffman
12-1-51

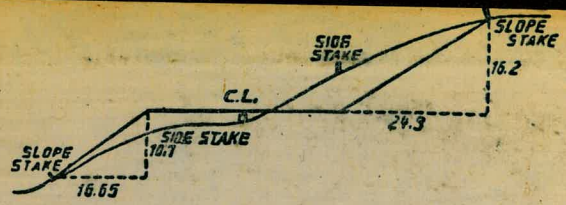
INDEXED
Law
OCT 27 1952

chk. starting B.M. P.61	10.43	2.60	2.70 [✓]
T.P. #6	3.77	13.13 [✓]	8.46
T.P. #5	5.11	17.82 [✓]	2.34
T.P. #4	1.73	15.05 [✓]	10.30
chk B.M.		5.23	17.62 [✓]
T.P. #3	4.23	23.62 [✓]	10.92
T.P. #2	0.36	30.31 [✓]	3.18
T.P. #1	1.59	33.13 [✓]	12.55
	2.06	44.09 [✓]	42.03

> Pct = ~~2.60~~ P.70
 > Use this = Per Inst. Ed Gabrielson 12-1-51 } Agrees with
 on Hub 3+92.46 P.59 } Filications
 in FB 2038
 Chisled cross
 on Rim, M.H. Trunk Sewer, West Side Morena Blvd.
 Approx 200' South of Milton
 Nail in Pole, Alley
 > FB 2038-1
 N.W. B.P. NAPIER Had Chicago
 S.W. B.P. Milton & Erie

31.20
27.00
3 42 397

30.08
1.12
29.90
1.30



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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