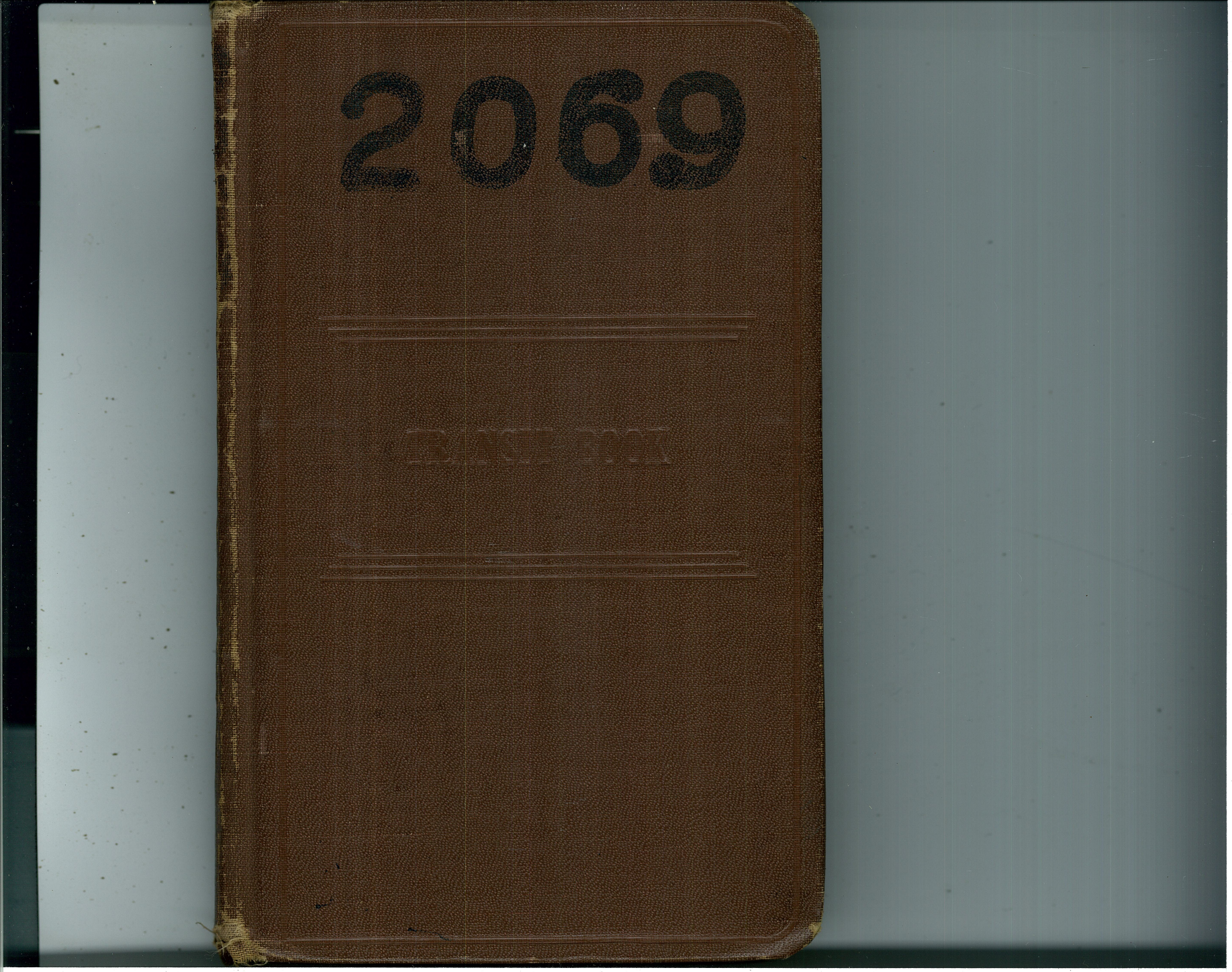
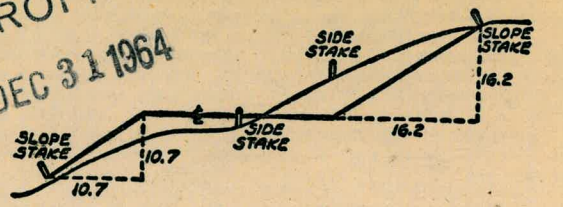

2069



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34 20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35 10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36 00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

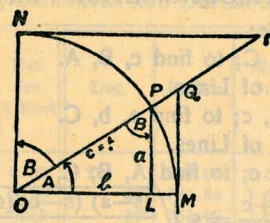


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$\sin A = \frac{a}{c} = \frac{a}{1} = a = \text{sos } B = LP$

$\text{sos } A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$

$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$

$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$

$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$

$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$

$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$

$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$

$\text{exsec } A = PQ = \text{coexsec } B$

$\text{coexsec } A = PT = \text{exsec } B$

$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$

$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$

Law of Lines $\frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C^1}{C}$

Law of Cosines $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents $\frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$

TABLE II — Continued
TRIGONOMETRIC FORMULÆ (continued)

in any triangle:

Given a, b, C; to find c, B, A.
Use Law of Lines.

Given A, B, c; to find a, b, C.
Use Law of Lines.

Given a, b, c; to find A, B, C.

Let $\frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$

$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$

$\tan \frac{1}{2} A = \frac{r}{s-a}$

$\tan \frac{1}{2} B = \frac{r}{s-b}$

$\tan \frac{1}{2} C = \frac{r}{s-c}$

Area of a triangle:

Area $= \frac{1}{2} ab \sin C$

Area $= \sqrt{s(s-a)(s-b)(s-c)}$

PRISMOIDAL FORMULA.

$\text{Vol.} = \frac{h}{6}(B+b+4M)$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/16
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	3/16
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	1/4
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	5/16
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	3/8
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	7/16
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	1/2
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	9/16
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	5/8
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	11/16
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	3/4
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	13/16
7/8	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	7/8
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	15/16
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV — RADII, ORDINATES AND DEFLECTIONS

Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot
0° 10′	34377.5	.036	.145	0.05′	7°	819.02	1.528	6.105	2.10′
20	17188.8	.073	.291	0.10	20′	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25	8	716.78	1.746	6.976	2.40
1	5729.65	.218	.873	0.30	20	688.16	1.819	7.266	2.50
10	4911.15	.255	1.018	0.35	30	674.69	1.855	7.411	2.55
20	4297.28	.291	1.164	0.40	40	661.74	1.892	7.556	2.60
30	3819.83	.327	1.309	0.45	9	637.28	1.965	7.846	2.70
40	3437.87	.364	1.454	0.50	20	614.56	2.037	8.136	2.80
50	3125.36	.400	1.600	0.55	30	603.80	2.074	8.281	2.85
2	2864.93	.436	1.745	0.60	40	593.42	2.110	8.426	2.90
10	2644.58	.473	1.891	0.65	10	573.69	2.183	8.716	3.00
20	2455.70	.509	2.036	0.70	30	546.44	2.292	9.150	3.15
30	2292.01	.545	2.181	0.75	11	521.67	2.402	9.585	3.30
40	2148.79	.582	2.327	0.80	30	499.06	2.511	10.02	3.45
50	2022.41	.618	2.472	0.85	12	478.34	2.620	10.45	3.60
3	1910.08	.655	2.618	0.90	30	459.28	2.730	10.89	3.75
10	1809.57	.691	2.763	0.95	13	441.68	2.839	11.32	3.90
20	1719.12	.727	2.908	1.00	30	425.40	2.949	11.75	4.05
30	1637.28	764	3.054	1.05	14	410.28	3.058	12.18	4.20
40	1562 88	.800	3.199	1.10	30	396.20	3.168	12.62	4.35
50	1494.95	836	3.345	1.15	15	383.07	3.277	13.05	4.50
4	1432.69	.873	3.490	1.20	30	370.78	3.387	13.49	4.65
10	1375.40	.909	3.635	1.25	16	359.27	3.496	13.92	4.80
20	1322.53	.945	3.718	1.30	30	348.45	3.606	14.35	4.95
30	1273.57	.982	3.926	1.35	17	338.27	3.716	14.78	5.10
40	1228.11	1.018	4.071	1.40	18	319.62	3.935	15.64	5.40
50	1185.78	1.055	4.217	1.45	19	302.94	4.155	16.51	5.70
5	1146.28	1.091	4.362	1.50	20	287.94	4.374	17.37	6 00
10	1109.33	1.127	4.507	1.55	21	274.37	4.594	18.22	6.30
20	1074.68	1.164	4.653	1.60	22	262.04	4.814	19.08	6.60
30	1042.14	1.200	4.798	1.65	23	250.79	5.035	19.94	6.90
40	1011.51	1.237	4.943	1.70	24	240.49	5.255	20.79	7.20
50	982.64	1.273	5.088	1.75	25	231.01	5.476	21.64	7.50
6	955.37	1.309	5.234	1.80	26	222.27	5.697	22.50	7.80
10	929.57	1.346	5.379	1.85	27	214.18	5.918	23.35	8.10
20	905.13	1.382	5.524	1.90	28	206.68	6.139	24.19	8.40
30	881.95	1.418	5.669	1.95	29	199.70	6.360	25.04	8.70
40	859.92	1.455	5.814	2.00	30	193.18	6.583	25.88	9.00

Note. Chord Deflection = 2 times tangent deflection.

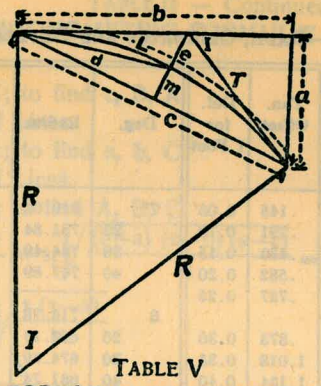


TABLE V

CURVE FORMULÆ FOR SIMPLE CURVES

COMPILED BY J. CALVIN LOCKE, C. E.

(1) $c = \sqrt{2Ra}$ (2) $c = \sqrt{a^2+b^2}$

(3) $c = \sqrt{2R\,(R-\sqrt{(R+b)\,(R-b)}} = \sqrt{2R\,(R-\sqrt{R^2-b^2})}$

(4) $c = 2\sqrt{m\,(2R-m)}$

(5) $c = 2R \sin {}^1/_2\, I$ (6) $c = 2T \cos {}^1/_2\, I$

(7) $e = R \operatorname{exsec} {}^1/_2\, I$

(8) $e = R \tan {}^1/_2\, I \tan {}^1/_4\, I$ (9) $e = T \tan {}^1/_4\, I$

(10) $b = \sqrt{a\,(2R-a)}$

(11) $b = \sqrt{\left(c+\frac{c^2}{2R}\right)\left(c-\frac{c^2}{2R}\right)} = \sqrt{c^2-\frac{c^4}{4R^2}}$

(12) $b = R \sin I$ (13) $b = a \cot {}^1/_2\, I$

(14) $R = \frac{a^2+b^2}{2a} = \frac{c^2}{2a}$ (15) $R = \frac{d^2}{2m} = \frac{c^2+4m^2}{8m}$

(16) $d = \sqrt{R\,(2R-\sqrt{(2R+c)\,2R-c})} = \sqrt{R\,(2R-\sqrt{4R^2-c^2})}$

(17) $d = \sqrt{2Rm}$ (18) $d = 2R \sin {}^1/_4\, I$ (19) $m = \frac{d^2}{2R}$

(20) $m = R \mp \sqrt{\left(R+\frac{c}{2}\right)\left(R-\frac{c}{2}\right)} = R \mp \sqrt{R^2-\frac{c^2}{4}}$

(21) $m = R \operatorname{vers} {}^1/_2\, I$ (22) $m = R \sin {}^1/_2\, I \tan {}^1/_4\, I$ (23) $m = {}^1/_2\, c \tan {}^1/_4\, I$

(24) $a = \frac{c^2}{2R}$ (25) $a = R - \sqrt{(R+b)\,(R-b)} = R - \sqrt{R^2-b^2}$

(26) $a = 2R\,(\sin^2 {}^1/_2\, I)^2$ (27) $a = R \operatorname{vers} I$ (28 $a = R \sin I \tan {}^1/_2$

(29) $a = b \tan {}^1/_2\, I$ (30) $a = T \sin I$ (31) $T = R \tan {}^1/_2\, I$

(32) $I = \frac{L}{R} \times 57.295780$ (33) $R = \frac{L}{I} \times 57.295780$

(34) $L = IR \times 0.01745329$ (35) $L = \frac{8d-c}{3}$

36 Area Seg. $= \frac{LR-R^2 \sin I}{2} = \frac{LR-Rb}{2}$

TABLE VI

SINES, COSINES, TANGENTS, COTANGENTS

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0175	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	670	86
4	698	699	727	729	756	758	785	787	814	816	843	846	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	190	198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	939	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	827	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20′ cot	10′ cos	10′ cot	deg.

TABLE VI (continued)

SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	932	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60 cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20′ cot	10′ cos	10′ cot	deg.

TABLE VII Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 / sin. ½ def. ang.	½ sub chord / R = sin of ½ def. angle — 12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	Length of arc for 100 ft.
30°	193.18	1° 51′	2° 17′	2° 58′	3° 43′	101.15
32°	181.39	1° 59′	2° 25′	3° 10′	3° 58′	101.33
34°	171.01	2° 06′	2° 33′	3° 21′	4° 12′	101.48
36°	161.80	2° 13′	2° 41′	3° 33′	4° 26′	101.66
38°	153.58	2° 20′	2° 49′	3° 44′	4° 40′	101.85
40°	146.19	2° 27′	2° 57′	3° 55′	4° 54′	102.06
42°	139.52	2° 34′	3° 05′	4° 07′	5° 08′	102.29
44°	133.47	2° 41′	3° 13′	4° 18′	5° 22′	102.53
46°	127.97	2° 48′	3° 21′	4° 29′	5° 36′	102.76
48°	122.92	2° 55′	3° 29′	4° 40′	5° 50′	103.00
50°	118.31	3° 02′	3° 38′	4° 51′	6° 04′	103.24
52°	114.06	3° 09′	3° 46′	5° 02′	6° 17′	103.54
54°	110.11	3° 16′	3° 54′	5° 13′	6° 31′	103.84
56°	106.50	3° 22′	4° 02′	5° 23′	6° 44′	104.14
58°	103.14	3° 29′	4° 10′	5° 34′	6° 57′	104.43
60°	100.00	3° 35′	4° 18′	5° 44′	7° 11′	104.72

$T = R \tan \frac{1}{2} I$

$T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } \frac{1}{2} D}$

$\text{Sin. } \frac{1}{2} D = \frac{50}{R}$

$\text{Sin. } \frac{1}{2} D = \frac{50 \tan \frac{1}{2} I}{T}$

$R = T \cot. \frac{1}{2} I$

$R = \frac{\text{Sin. } \frac{1}{2} D}{50}$

$E = R \text{ ex. sec } \frac{1}{2} I$

$E = T \tan \frac{1}{4} I$

$\text{Chord def.} = \frac{\text{chord}^2}{R}$

$\text{No. chords} = \frac{I}{D}$

Tan. def. = ½ chord def.

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft. see Table II.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance. Multiply the angle by .01745, and the product by the distance.

GENERAL DATA

RIGHT ANGLE TRIANGLES. Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. $10.10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. $25.25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875$ = Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

LEVELING. The correction for curvature and refraction, in feet and decimals of feet is equal to $0.574\,d^2$, where d is the distance in miles. The correction for curvature alone is closely, $\frac{2}{3}d^2$. The combined correction is negative.

PROBABLE ERROR. If d_1, d_2, d_3, etc. are the discrepancies of various results from the mean, and if Σd^2 = the sum of the squares of these differences and n = the number of observations, then the probable error of the mean = $\pm 0.6745 \sqrt{\frac{\Sigma d^2}{n(n-1)}}$

TABLE VIII TANGENTS AND EXTERNALS TO A 1° CURVE.

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2		71°	4086.9	1308.2		81°	4893.6	1805.3	
10′	3386.3	925.9		10′	4099.5	1315.6		10′	4908.0	1814.7	
20′	3397.5	931.6	+	20′	4112.1	1322.9	+	20′	4922.5	1824.1	+
30′	3408.8	937.3	5° C.	30′	4124.8	1330.3	5° C.	30′	4937.0	1833.6	5° C.
40′	3420.1	943.1	T	40′	1137.4	1337.7	T	40′	4951.5	1843.1	T
50′	3431.4	948.9	.25	50′	4150.1	1345.1	.30	50′	4966.1	1852.6	.36
62°	3442.7	954.8	E	72°	4162.8	1352.6	E	82°	4980.7	1862.2	E
10′	3454.1	960.6	.080	10′	4175.6	1360.1	.110	10′	4995.4	1871.8	.149
20′	3465.4	966.5		20′	4188.5	1367.6		20′	5010.0	1881.5	
30′	3476.8	972.4		30′	4201.2	1375.2		30′	5024.8	1891.2	
40′	3488.3	978.3		40′	4214.0	1382.8		40′	5039.5	1900.9	
50′	3499.7	984.3		50′	4226.8	1390.4		50′	5054.3	1910.7	
63°	3511.1	990.2		73°	4239.7	1398.0		83°	5069.2	1920.5	
10′	3522.6	996.2	10° C.	10′	4252.6	1405.7	10° C.	10′	5084.0	1930.4	10° C.
20′	3534.1	1002.3	T	20′	4265.6	1413.5	T	20′	5099.0	1940.3	T
30′	3545.6	1008.3	.51	30′	4278.5	1421.2	.61	30′	5113.9	1950.3	.72
40′	3557.2	1014.4	E	40′	4291.5	1429.0	E	40′	5128.9	1960.2	E
50′	3568.7	1020.5	159	50′	4304.6	1436.8	.220	50′	5143.9	1970.3	.299
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10′	3591,9	1032.8		10′	4330.7	1452.5		10′	5174.1	1990.5	
20′	3603.5	1039.0		20′	4343.8	1460.4		20′	5189.3	2000.6	
30′	3615.1	1045.2		30′	4356.9	1468.4		30′	5204.4	2010.8	
40′	3626.8	1051.4		40′	4370.1	1476.4		40′	5219.7	2021.1	
50′	3638.5	1057.7	15° C.	50′	4383.3	1484.4	15° C.	50′	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10′	3661.9	1070.2	.76	10′	4409.8	1500.5	.91	10′	5265.6	2052.1	1.09
20′	3673.7	1076.6	E	20′	4423.1	1508.6	E	20′	5281.0	2062.5	E
30′	3685.4	1082.9	.240	30′	4436.4	1516.7	.332	30′	5296,4	2073.0	.450
40′	3697.2	1089.3		40′	4449.7	1524.9		40′	5311.9	2083.5	
50′	3709.0	1095.7		50′	4463.1	1533.1		50′	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10′	3732.7	1108.6		10′	4489.9	1549.7		10′	5358.6	2115.3	
20′	3744.6	1115.1		20′	4503.4	1558.0		20′	5374.2	2126.0	
30′	3756.5	1121.7	20° C.	30′	4516.9	1566.3	20° C.	30′	5389.9	2136.7	20° C.
40′	3768.5	1128.2	T	40′	4530,4	1574.7	T	40′	5405.6	2147.5	T
50′	3780.4	1134.8	1.02	50′	4544.0	1583.1	1.22	50′	5421.4	2158.4	1.45
67°	3792.4	1141.4	E	77°	4557.6	1591.6	E	87°	5437.2	2169.2	E
10′	3804.4	1148.0	.321	10′	4571.2	1600.1	.445	10′	5453.1	2180.2	.603
20′	3816.4	1154.7		20′	4584.8	1608.6		20′	5469.0	2191.1	
30′	3828.4	1161.3		30′	4598.5	1617.1		30′	5484.9	2202.2	
40′	3840.5	1168.1		40′	4612.2	1625.7		40′	5500.9	2213.2	
50′	3852.6	1174.8		50′	4626.0	1634.4		50′	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10′	3876.8	1188.4	25° C.	10′	4653.6	1651.7	25° C.	10′	5549.2	2246.7	25° C.
20′	3889.0	1195.2	T	20′	4667.4	1660.5	T	20′	5565.4	2258.0	T
30′	3901.2	1202.0	1.28	30′	4681.3	1669.2	1.53	30′	5581.6	2269.3	1.83
40′	3913.4	1208.9	E	40′	4695.2	1678.1	E	40′	5597.8	2280.6	E
50′	3925.6	1215.8	.403	50′	4709.2	1686.9	.558	50′	5614.2	2292.0	.756
69°	3937.9	1222.7		79°	4723.2	1695.8		89°	5630.5	2303.5	
10′	3950.2	1229.7		10′	4737.2	1704.7		10′	5646.9	2315.0	
20′	3962.5	1236.7		20′	4751.2	1713.7		20′	5663.4	2326.6	
30′	3974.8	1243.7		30′	4765.3	1722.7		30′	5679.9	2338.2	
40′	3987.2	1250.8		40′	4779.4	1731.7		40′	5696.4	2349.8	
50′	3999.5	1257.9	30° C.	50′	4793.6	1740.8	30° C.	50′	5713.0	2361.5	30° C.
70°	4011.9	1265.0	T	80°	4807.7	1749.9	T	90°	5729.7	2373.3	T
10′	4024.4	1272.1	1.54	10′	4822.0	1759.0	1.84	10′	5746.3	2385.1	2.20
20′	4036.8	1279.3	E	20′	4836.2	1768.2	E	20′	5763.1	2397.0	E
30′	4049.3	1286.5	.485	30′	4850.5	1777.4	.671	30′	5779.9	2408.9	.910
40′	4061.8	1293.6		40′	4864.8	1786.7		40′	5796.7	2420.9	
50′	4074.4	1300.9		50′	4879.2	1796.0		50′	5813.6	2432.9	

$E = R \tan \frac{1}{2} I$ $E = R \operatorname{exsec} \frac{1}{2} I$

TABLE VIII TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9		101°	6950.6	3278.1		111°	8336.7	4386.1	
10′	5847.5	2457.1	+	10′	6971.3	3294.1	+	10′	8362.7	4407.6	+
20′	5864.6	2469.3	5° C.	20′	6992.0	3310.1	5° C.	20′	8388.9	4429.2	5° C.
30′	5881.7	2481.5	T	30′	7012.7	3326.1	T	30′	8415.1	4450.9	T
40′	5898.8	2493.8	.43	40′	7033.6	3342.3	.51	40′	8441.5	4472.7	.62
50′	5916.0	2506.1	E	50′	7054.5	3358.5	E	50′	8468.0	4494.6	E
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10′	5950.5	2531.0		10′	7096.6	3391.2		10′	8521.3	4538.8	
20′	5967.9	2543.5		20′	7117.8	3407.7		20′	8548.1	4561.1	
30′	5985,3	2556.0		30′	7139.0	3424.3		30′	8575.0	4583.4	
40′	6002.7	2568.6		40′	7160.3	3440.9		40′	8602.1	4606.0	
50′	6020.2	2581.3		50′	7181.7	3457.6		50′	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10′	6055.4	2606.8	T	10′	7224.7	3491.3	T	10′	8684.0	4674.2	T
20′	6073.1	2619.7	.86	20′	7246.3	3508.2	.103	20′	8711.5	4697.2	1.25
30′	6090.8	2632.6	E	30′	7268.0	3525.2	E	30′	8739.2	4720.3	E
40′	6108.6	2645.5	.401	40′	7289.8	3542.4	.536	40′	8767.0	4743.6	721
50′	6126.4	2658.5		50′	7311.7	3559.6		50′	8794.9	4766.9	
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10′	6162.2	2684.7		10′	7355.6	3594.2		10′	8851.0	4814.1	
20′	6180.2	2697.9		20′	7377.8	3611.7		20′	8879.3	4837.8	
30′	6198.3	2711.2		30′	7399.9	3629.2		30′	8907.7	4861.7	
40′	6216.4	2724.5		40′	7422.2	3646.8		40′	8936.3	4885.7	
50′	6234.6	2737.9	15° C.	50′	7444.6	3664.5	15° C.	50′	8965.0	4909 9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10′	6271.1	2764.8	1.30	10′	7489.6	3700.2	1.56	10′	9022.7	4958.6	1.93
20′	6289.4	2778.3	E	20′	7512.2	3718.2	E	20′	9051.7	4983 1	E
30′	6307.9	2792.0	.604	30′	7534.9	3736.2	.806	30′	9080.9	5007.8	1 09
40′	6326.3	2805.6		40′	7557.7	3754.4		40′	9110.3	5032.6	
50′	6344.8	2819.4		50′	7580.5	3772.6		50′	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10′	6382.1	2847.0		10′	7626.6	3809.4		10′	9199.1	5107.9	
20′	6400.8	2861.0		20′	7649.7	3827.9		20′	9229.0	5133.3	
30′	6419.5	2875.0	20° C.	30′	7672.9	3846.5	20° C.	30′	9259.0	5158.8	20° C.
40′	6438.4	2889.0	T	40′	7696.3	3865.2	T	40′	9289.2	5184.5	T
50′	6457.3	2903.1	1.74	50′	7719.7	3884.0	2.08	50′	9319.5	5210.3	2.52
97°	6476.2	2917.3	E	107°	7743.2	3902.9	E	117°	9349.9	5236.2	E
10′	6495.2	2931.6	.809	10′	7766.8	3921.9	1.08	10′	9380.5	5262.3	1.46
20′	6514.3	2945.9		20′	7790.5	3940.9		20′	9411.3	5288.6	
30′	6533.4	2960.3		30′	7814.3	3960.1		30′	9442.2	5315.0	
40′	6552.6	2974.7		40′	7838.1	3979.4		40′	9473.2	5341.5	
50′	6571.9	2989.2		50′	7862.1	3998.7		50′	9504.4	5368.2	
98°	6591.2	3003.8		108°	7886.2	4018.2		118°	9535.7	5395.1	
10′	6610.6	3018.4	25° C.	10′	7910.4	4037.8	25° C.	10′	9567.2	5422.1	25° C.
20′	6630.1	3033.1	T	20′	7934.6	4057.4	T	20′	9598.9	5449.2	T
30′	6649.6	3047.9	2.18	30′	7959.0	4077.2	2.61	30′	9630.7	5476.5	3.16
40′	6669.2	3062.8	E	40′	7983.5	4097.1	E	40′	9662.6	5504.0	E
50′	6688.8	3077.7	1.02	50′	8008.0	4117.0	1.36	50′	9694.7	5531.7	1.83
99°	6708.6	3092.7		109°	8032.7	4137.1		119°	9727.0	5559.4	
10′	6728.4	3107.7		10′	8057.4	4157.3		10′	9759.4	5587.4	
20′	6748.2	3122.9		20′	8082.3	4177.5		20′	9792.0	5615.5	
30′	6768.1	3138.1		30′	8107.3	4197.9		30′	9824.8	5643.8	
40′	6788.1	3153.3		40′	8132.3	4218.4		40′	9857.7	5672.3	
50′	6808.2	3168.7		50′	8157.5	4239.0		50′	9890.8	5700.9	
100°	6828.3	3184.1	30° C.	110°	8182.8	4259.7	30° C.	120°	9924.0	5729.7	30° C.
10′	6848.5	3199.6	T	10′	8208.2	4280.5	T	10′	9957.5	5758.6	T
20′	6868.8	3215.1	2.62	20′	8233.7	4301.4	3.14	20′	9991.0	5787.7	3.81
30′	6889.2	3230.8	E	30′	8259.3	4322.4	E	30′	10025.0	5817.0	E
40′	6909.6	3246.5	1.22	40′	8285.0	4343.6	1.63	40′	10059.0	5846.5	2.20
50′	6930.1	3262.3		50′	8310.8	4364.8		50′	10093.0	5876.1	

$T = R \tan \frac{1}{2} I$ $E = R \operatorname{exsec} \frac{1}{2} I$

TABLE IX

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE X

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5 58	2-59	7.2
250	25	5 44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9 -32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XI

INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL.

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XII

MINUTES IN DECIMALS OF A DEGREE.

0′30″	.00833	10′30″	.17500	20′30″	.34167	30′30″	.50833	40′30″	.67500	50′30″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

Table XIII—Corrections for Tangents and Externals

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

For Tangents Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

For Externals Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Index

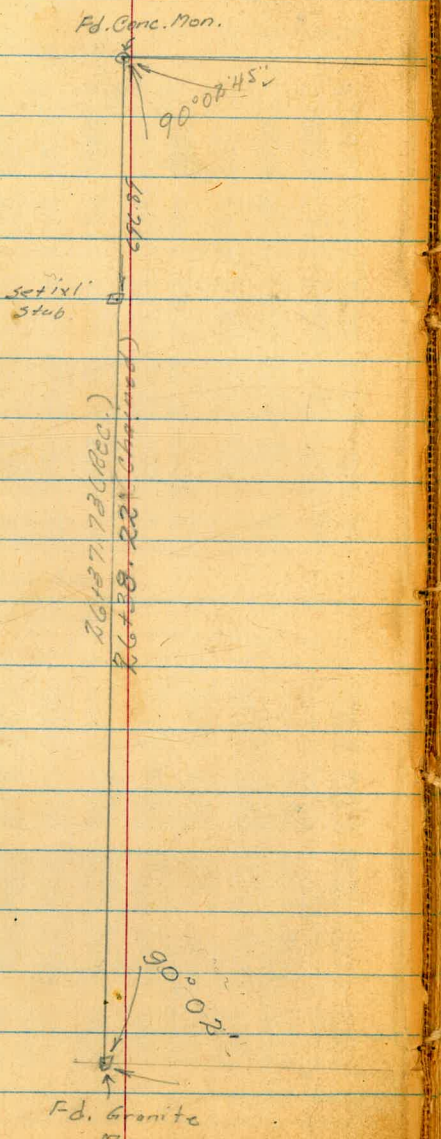
Pg

Alley Blk 69 O.B. X-Sec. for payment 50-52

Johnson
Greer
Cota
Fay
1-27-50.
W.O. 20638

Survey of Pueblo Lot #1203

Roberts x643.5



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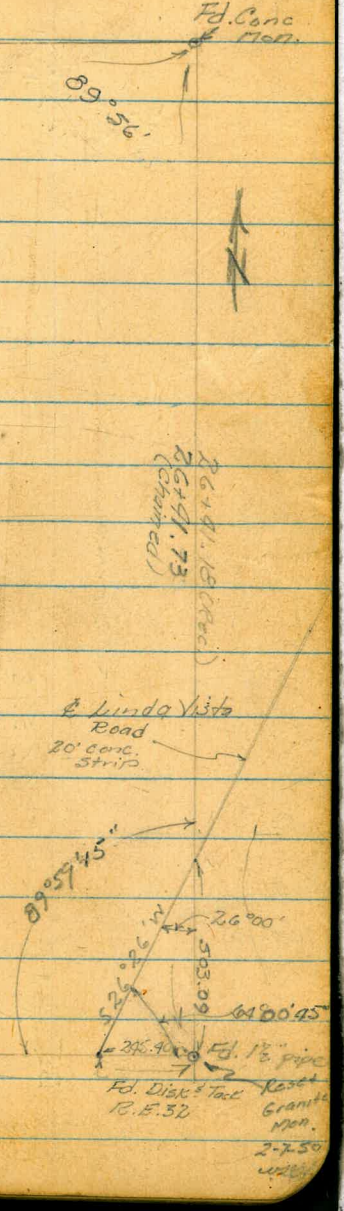
P.L. 1203

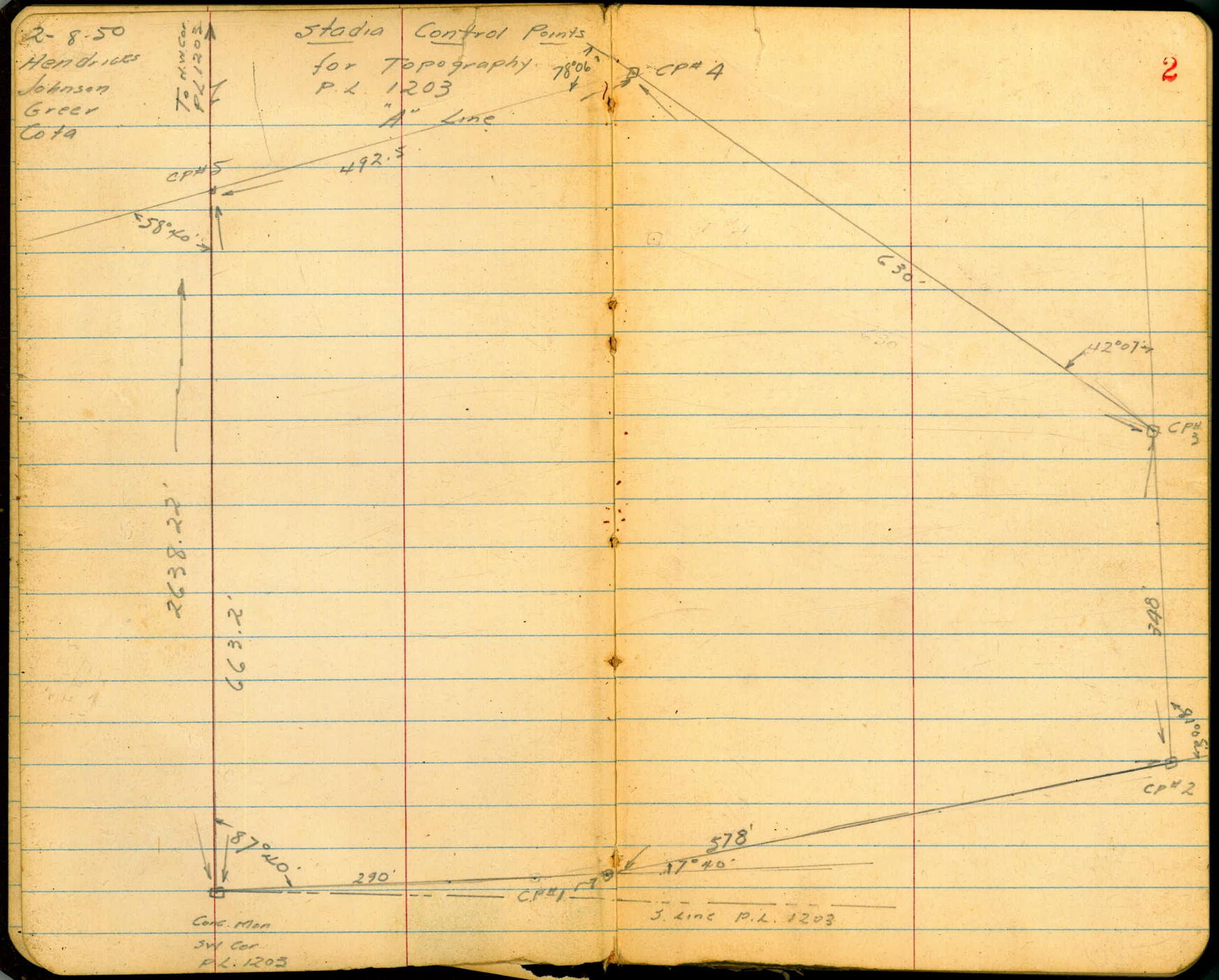
26+40.23 (Rec.)
26+41.76 (Chained)



2-8-50
Hendricks
Johnson
Greer
Cota

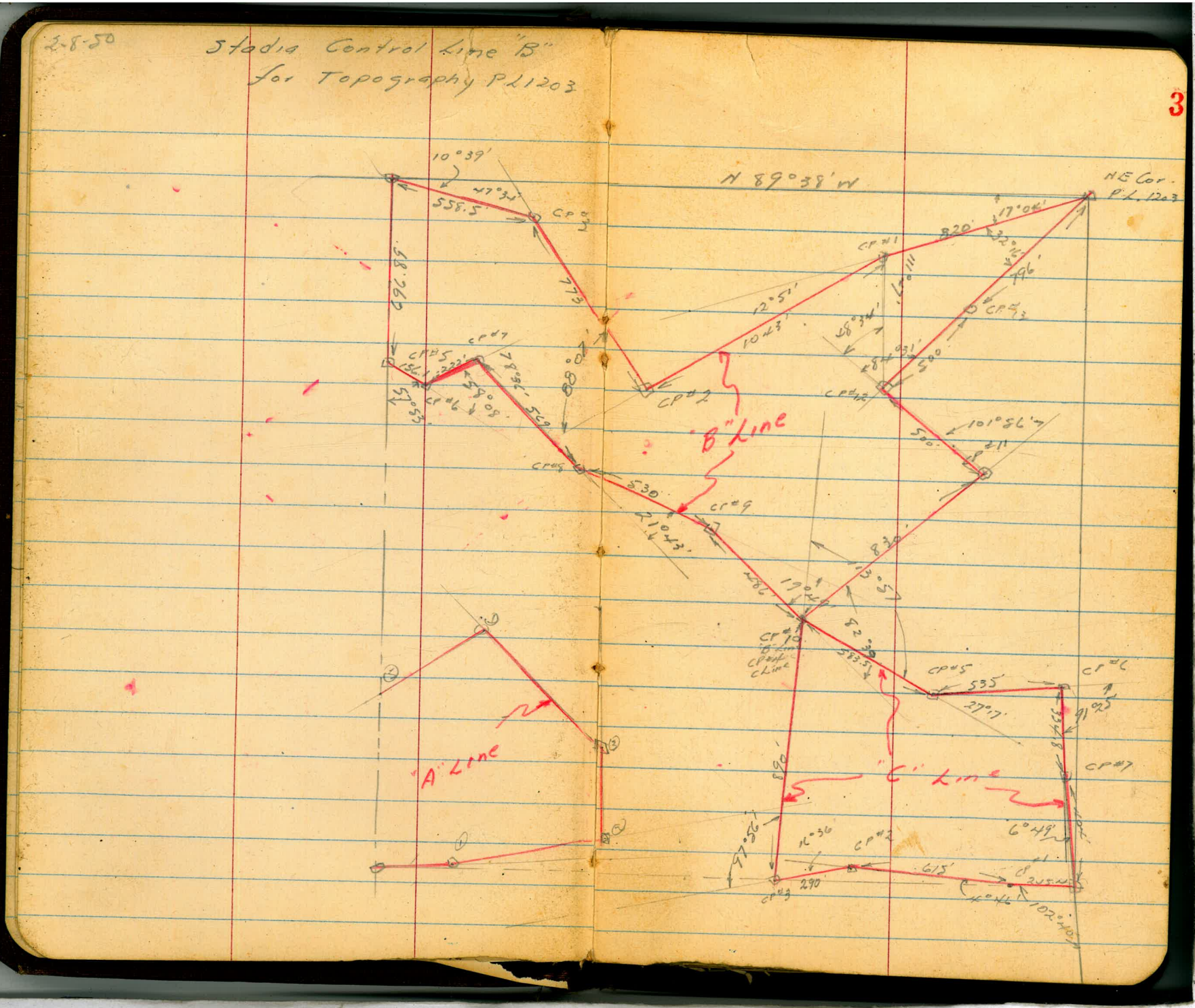
Stadia Control Points for Topography P.L. 1203

"A" Line



2-8-50

Stadia Control Line "B" for Topography PL1203



Coordinates of Control Points

Base Line Outer Boundary

	North	East
SW Cor. PL 1203	00	00
N.W. " " "	2638.15 N.	18.99
NE " " "	2621.24 N	2661.79
SE " " "	20.41 South	2641.81

"A" Line

	North	East
CP #1	9.70	289.84
CP #2	105.92	859.77
CP #3	453.90	855.72
CP #4	916.27	427.81
CP #5	663.47	815.14

"C" Line

CP #1 LE Disc & Land Vista Rd.	18.49 So.	2396.42
#2	37.43 N.	1783.96
#3	19.81 S	1499.66
#4 = #10 "B" Line	848.52 N	1447.30
#5	644.35	1991.63
#6	707.54	2522.89
#7	374.01	2554.21

"B" Line

	North	East
CP #1	2385.60	1876.38
CP #2	1871.29	969.04
#3	2530.77	565.91
#4	2638.15	1899.00
#5	1941.17	1392.00
#6	1857.24	1425.42
#7	1953.16	345.63
#8	1498.73	688.07
#9	1223.52	1141.00
#10	845.30	1446.19
#11	1279.89	2153.51
#12	1642.37	1809.44
#13	2019.53	2137.69
NW Mon.	2621.24	2661.79

2-10-50
Hendricks
Johnson
Greer
Cota

Levels for Topography of P.L. 1203

. These Levels are USGS Datum
Subtract 6.12 for city Datum

TP	5.22	358.14	8.14	352.92	CP # 6 "B" Line
TP	4.71	361.06	8.74	356.35	CP # 5 "B" Line
B.M.	7.37	365.09	6.31	357.72	Conc. Mon N.W. Cor. P.L. 1203
TP	7.99	364.03	7.67	356.04	CP # 3 "B" Line
TP	8.83	363.71	10.46	354.88	CP # 2 "B" Line
TP	2.14	365.34	10.70	363.20	
TP	1.34	373.90	13.07	372.56	
TP	1.12	385.63	3.96	384.51	CP # 1 "B" Line
TP	7.84	388.47	10.15	380.63	
B.M.	0.92	390.78	5.88	389.86	Conc. Mon N.E. Cor. P.L. 1203
TP	0.00	395.74	12.45	395.74	
TP	1.26	408.19	12.65	406.93	
TP	0.27	419.58	11.78	419.31	
TP	0.50	431.09	13.21	430.59	
TP	10.02	443.80	0.16	433.78	
	11.77				
BM # 2A (State Highway BM)		433.94		422.17	U.S.G.S. Datum Conc. Mon. Int. of E. Line Linda Vista Rd. & Northerly Boundary of San Diego

T.P.	4.42	368.87	10.66	364.45	CP # 6 "C" Line
T.P.	4.05	375.11	1.93	371.06	CP # 7 "C" Line
B.M.	9.95	372.99	3.12	363.04	Conc Mon. S.E. Cor P.L. 1203 CP #1 "B" Line
T.P.	3.43	366.16	0.81	362.73	L.S. Disc & Linda Vista Rd & 50 Line P.L. 1203
T.P.	9.10	363.54	4.50	354.44	CP # 2 "C" Line
T.P.	6.62	358.94	3.39	352.32	CP # 3 "C" Line
T.P.	7.49	355.71	6.59	348.22	CP # 2 "A" Line
T.P.	7.44	354.81	7.06	347.37	C.P. # 1 "A" Line
B.M.	2.37	354.43	8.12	352.06	Conc. Mon. S.W. Cor. P.L. 1203
T.P.	6.43	360.18	9.00	353.75	CP # 5 "A" Line
T.P.	0.26	362.75	1.85	362.49	CP # 4 "A" Line
T.P.	13.10	364.34	8.94	351.24	C.P. # 3 "A" Line
T.P.	3.36	360.18	11.51	356.82	
T.P.	0.35	368.33	2.41	367.98	CP # 10 "B" Line
T.P.	7.89	370.39	2.93	362.50	C.P. # 9 "B" Line
T.P.	2.47	365.43	1.18	362.96	CP # 8 "B" Line
T.P.	12.77 ~~10.94~~	364.14	6.77	351.37	CP # 7 "B" Line
		358.14			

B.M.			12.75	422.15	422.17	CK Starting BM P.S
T.P.	1.16	434.90	8.20	433.74		
T.P.	10.64	441.94	0.30	431.30		
T.P.	13.28	431.60	0.65	418.32		
T.P.	11.03	418.97	0.15	407.94		
T.P.	12.83	408.09	0.71	395.26		
B.M.	6.13	395.97	0.84	389.84		Conc. Mon N.E. Cor P.L. 1203
T.P.	8.77	390.68	1.88	381.91		
T.P.	3.85	383.79	6.62	379.94		C.P. #13 "B" Line
T.P.	1.21	386.56	3.35	385.35		C.P. #12 "B" Line
T.P.	8.72	388.70	2.62	379.98		C.P. #11 "B" Line
T.P.	6.46	382.60	0.64	376.14		
T.P.	11.25	376.78	3.34	365.53		C.P. #5 "C" Line
		368.87				

Hendricks
Johnson
Greer
Cota
3-10-50
W.O. 20639

Levels Around Boundary of P.L. 1781

T.P.	12.61	369.74	0.26	357.13	
T.P.	13.17	357.39	0.20	344.22	
T.P.	13.29	344.92	0.38	331.18	
T.P	12.09	331.56	5.92	319.47	
T.P.	12.81	324.89	11.98	312.08	
T.P.	4.87	324.06	2.38	319.19	P.O.T. 2"x2" Rwd Station 11426.89 So. Line P.L. 1781
T.P.	6.32	321.57	0.28	315.25	
T.P.	12.34	315.53	0.15	303.19	
T.P.	12.85	303.34	0.40	290.49	
T.P	13.25	290.89	1.90	277.64	
T.P.	12.31	279.04	0.15	266.73	
T.P.	12.14	266.88	1.00	254.74	
T.P.	12.97	255.74	3.13	242.77	Conc. Mon. S.W. Cor Pueblo Lot 1781
T.P.	13.36	245.90	1.01	232.54	
T.P.	13.17	233.55	0.24	220.38	
T.P	12.55	220.62	0.51	208.07	
T.P.	12.16	208.58	0.13	196.42	
T.P.	13.06	196.55	0.32	183.49	
B.M.	12.99	183.81		170.82	S.W. 7' Conc. Mon. Cass & Van Nuys

Levels Around Boundary of P.L. 1781

T.P	0.01	424.14	13.06	424.13	
T.P	2.25	437.19	13.19	434.99	
T.P	0.33	448.13	12.80	447.80	
T.P.	0.29	460.60	7.44	460.31	Conc. Mon. N.W. Cor. Pueblo Lot 1781
T.P	8.17	467.75	0.38	459.58	
T.P.	13.10	459.96	12.37	446.86	on North Line P.L. 1781 Conc. Mon S.E. Cor. Pueblo Lot 1774
T.P.	5.35	459.23	12.92	453.88	
T.P.	0.99	466.80	3.94	466.31	Conc. Mon. N.E. Cor. Pueblo Lot 1781
T.P.	4.92	470.75	1.61	465.83	
T.P	11.34	467.44	2.94	456.10	2"x2" Rwd. P.o.t. Sta. 16+37 Lt on East Line P.L. 1781
T.P	11.11	459.04	2.95	447.93	2"x2" Rwd P.o.t. Sta. 12+40 Lt on East Line P.L. 1781
T.P.	13.17	450.38	0.38	437.21	
T.P	12.24	437.59	0.05	425.35	
T.P.	13.00	425.40	0.03	412.40	
T.P.	13.10	412.43	0.49	399.33	
T.P.	13.35	399.82	1.09	386.47	
T.P.	13.34	387.56	8.51	374.22	Conc. Mon. S.E. Cor. Pueblo Lot 1781
T.P.	13.29	382.73	0.25	369.44	

Levels Around Boundary of 1781

T.P.	0.27	205.14	12.84	204.87		
T.P.	0.32	217.71	12.63	217.39		
T.P.	0.09	230.02	13.00	229.93		
T.P.	0.04	242.93	12.65	242.89	S.W. Conc. Mon — P.L. 1781	
T.P.	0.23	255.54	11.25	255.31		
T.P.	0.13	266.56	12.56	266.43		
T.P.	1.27	278.99	12.59	277.72		
T.P.	0.26	290.31	12.97	290.05	Conc. Mon Sta 6+55.60	0.26 East West Line P.L. 1781
T.P.	0.87	303.02	13.27	302.15		
T.P.	0.35	315.42	13.32	315.07		
T.P.	1.12	328.39	13.10	327.27		
T.P.	0.17	340.37	12.98	340.20		
T.P.	0.45	353.18	13.30	352.73		
T.P.	1.67	366.03	11.80	364.36	2"x2" Rwd. Pot. Sta. 13+15.67	on West Line P.L. 1781
T.P.	1.39	376.16	12.80	374.77		
T.P.	0.60	387.57	12.88	386.97		
T.P.	1.24	399.85	13.16	398.61		
T.P.	0.69	411.77	13.06	411.08		

Levels Around Boundary of P.L. 1781

				0.12	
				170.87	
			9.63	170.99	S.W. 7' Conc. Mon - Cass & Van Nuys
T.P.	1.69	180.62	13.19	178.93	
T.P.	0.29	192.12	13.31	191.83	

Levels West Half PL 1780 for Topography

		325.90		313.08	
TP.	13.82	324.90	0.03	312.08	
		313.11		299.94	
TP.	13.17	312.11	0.08	298.94	
		300.02		286.76	
TP.	13.26	299.02	0.47	285.76	
		287.23		274.40	
TBM.	12.83	286.23	8.96	273.40	Conc. Mon. Center Point of So Line PL 1780
		283.36		277.46	
TP.	5.90	282.36	13.22	276.46	
		290.68		290.64	
TP.	0.04	289.68	13.09	289.64	
		303.73		303.41	
TP.	0.32	302.73	12.63	302.41	
		316.04		316.00	
TP.	0.04	315.04	12.95	315.00	
		328.95		329.09	
TP.	-0.14	327.95	12.69	328.09	
		341.78		341.58	
TP.	0.20	340.78	12.94	340.58	
		354.52		354.69	
TP.	-0.17	353.52	13.08	353.69	
		367.77		367	
TP.	0.53	366.77	11.21	366.24	10+76.5 C POT (30' North)
		378.45			
TP.	4.33	377.45	3.94	374.12	
TP.	0.33	378.06	12.43	377.73	
TP.	4.14	390.16	0.75	386.02	
BM.	12.55	386.77		374.22	SE Cor. Mon PL 1781 (P 9)

Levels P.L 1780 Cont'd.

T.P.	13.04	481.47 ~~480.47~~	0.15	468.43 ~~467.43~~		
T.P.	12.89	468.55 ~~467.55~~	0.11	455.69 ~~454.69~~		
			4.15	451.65 ~~450.65~~	on Stub	11+61.08 East Line
T.P.	12.68	455.80 ~~454.80~~	0.80	443.12 ~~442.12~~		
			10.08	433.84 ~~432.84~~	on Stub	14+20.02 East Line
T.P.	12.35	443.92 ~~442.92~~	0.68	431.57 ~~430.57~~		
T.P.	12.83	432.25 ~~431.25~~	0.32	419.42 ~~418.42~~		
T.P.	13.16	419.74 ~~418.74~~	0.00	406.58 ~~405.58~~		
T.P.	13.12	406.58 ~~405.58~~	0.39	393.46 ~~392.46~~		
			5.34	388.51 ~~387.51~~	on Stub	16+98.58 East Line
T.P.	13.26	393.85 ~~392.85~~	0.21	380.59 ~~379.59~~		
T.P.	12.51	380.80 ~~379.80~~	0.21	368.29 ~~367.29~~		
T.P.	13.06	368.50 ~~367.50~~	5.22	355.44 ~~354.44~~	on Stub	19+03.53 East Line
T.P.	9.55	360.66 ~~359.66~~	0.05	351.16 ~~350.16~~		
T.P.	13.03	351.16 ~~350.16~~	0.32	338.13 ~~337.13~~		
T.P.	12.65	338.45 ~~337.45~~	0.10	325.80 ~~324.80~~		
		325.90 ~~324.90~~				

Levels PL 1780 Contd.

T.P.			13.31	466.29 (466.31)	NE Mon P.L. 1781 (P-9)
T.P.	0.72	479.60 ~~478.60~~	13.14	478.88 ~~477.88~~	
T.P.	0.00	492.02 ~~491.02~~	12.72	492.02 ~~491.02~~	
T.P.	0.35	504.74 ~~503.74~~	13.12	504.39 ~~503.39~~	
T.P.	1.89	517.51 ~~516.51~~	13.02	515.62 ~~514.62~~	
TBM	1.51	528.64 ~~527.64~~	3.28	527.13 ~~526.13~~	Conc Mon. Center Point North Line PL 1780
			4.52	525.89 ~~524.89~~	on Stub 2+37.15 East Line
T.P.	12.54	530.41 ~~529.41~~	0.06	517.87 ~~516.87~~	
			8.64	509.29 ~~508.29~~	on Stub 4+51.55 East Line
T.P.	11.76	517.93 ~~516.93~~	0.41	506.17 ~~505.17~~	
T.P.	13.20	506.58 ~~505.58~~	0.14	493.38 ~~492.38~~	
T.P.	12.63	493.52 ~~492.52~~	0.58	480.89 ~~479.89~~	
			8.35	473.12 ~~472.12~~	On Stub 7+49.96 East Line
		481.47 ~~480.47~~			

11-10-50
Hendricks
Sherman
Shepard
Crawford
W O # 31812

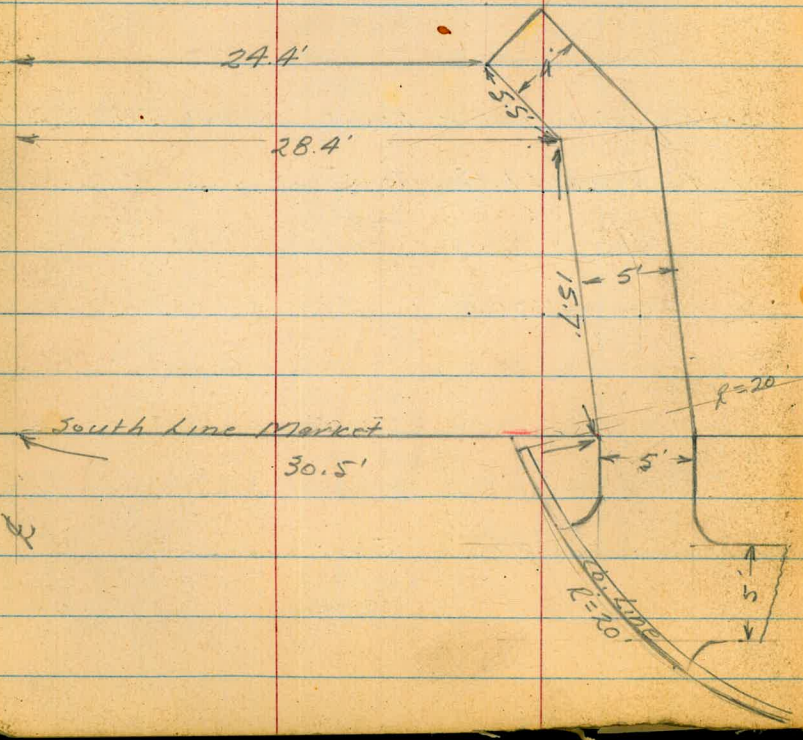
X SECTION DODSON ST.
MARKET to K ST.

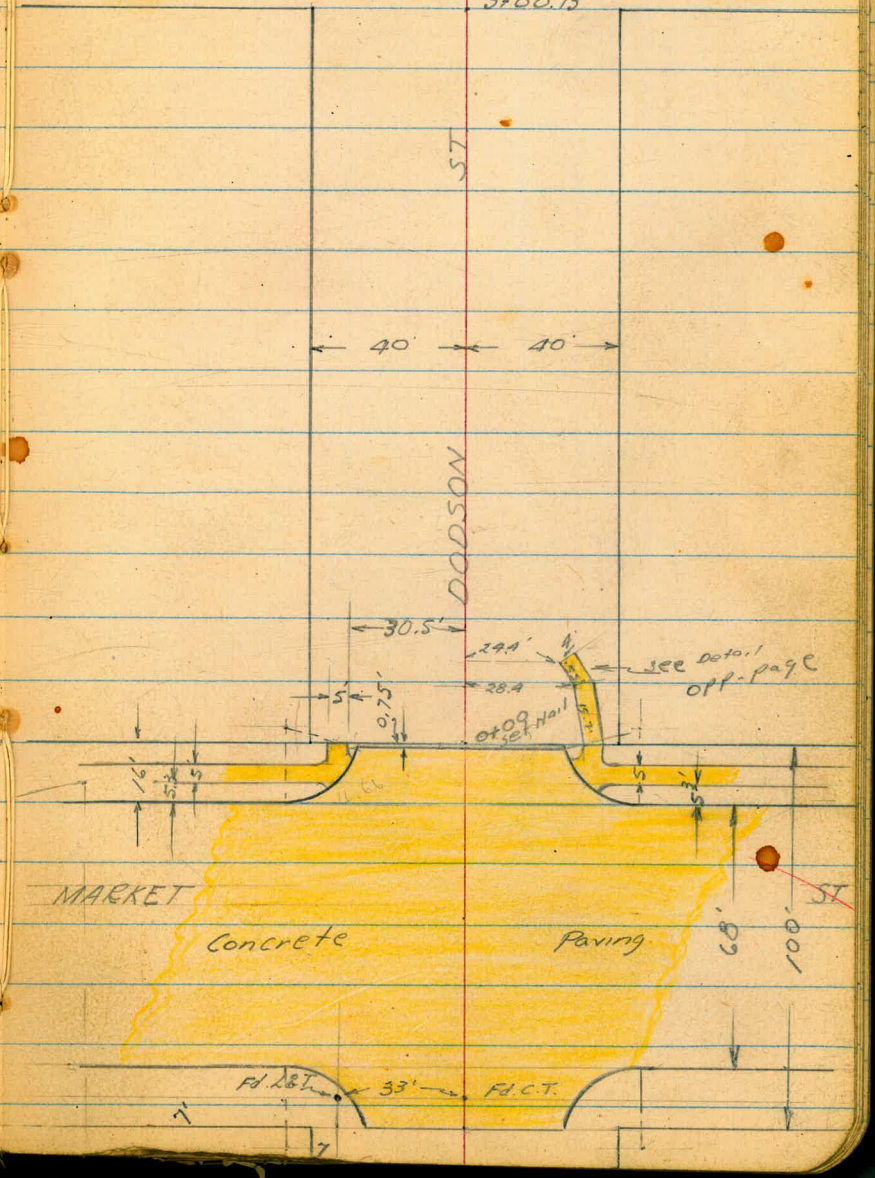
ISLAND

Contd. P-15

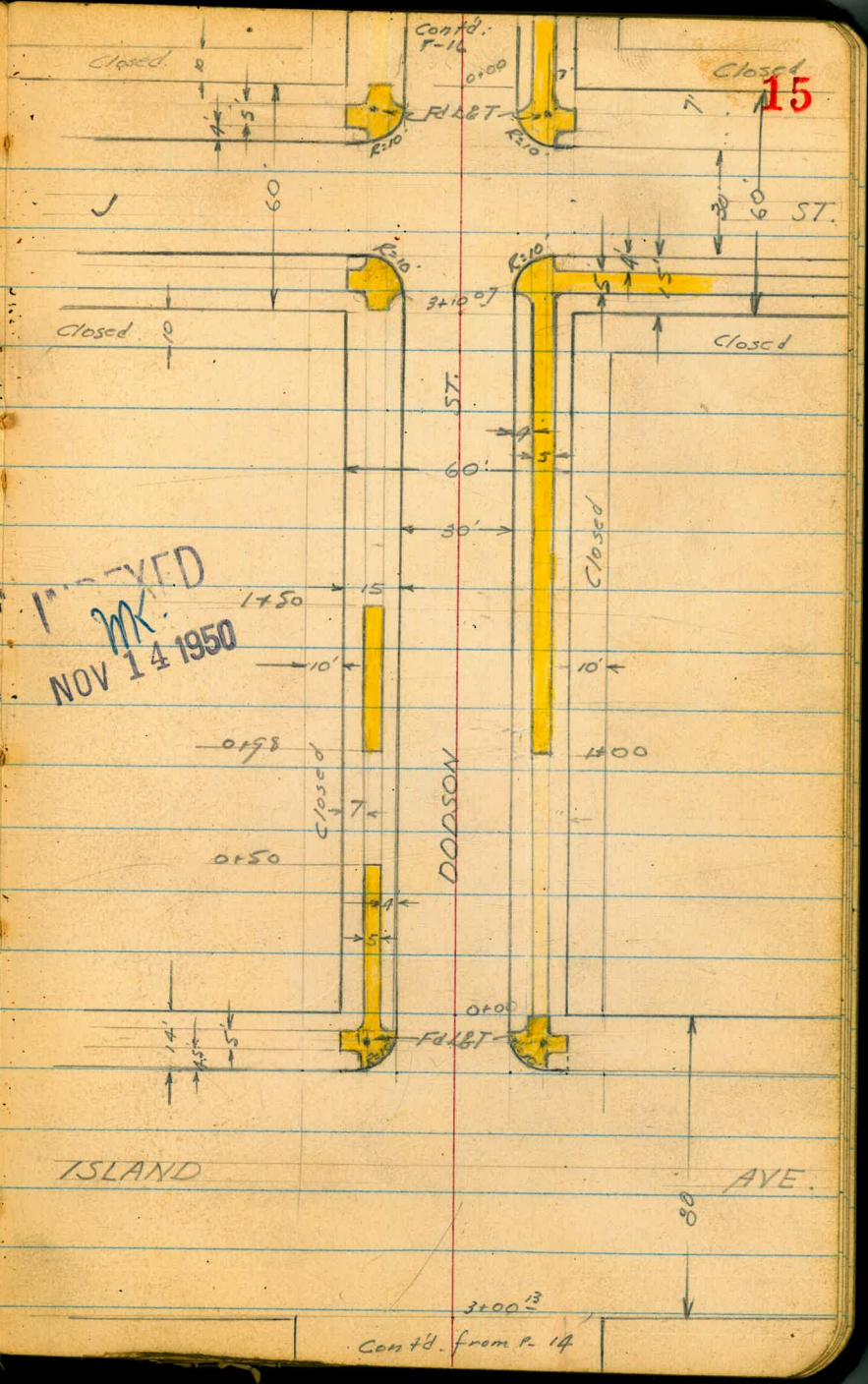
3+00.13

Detail of Sidewalk
S.W. Cor. Market & Dobson.

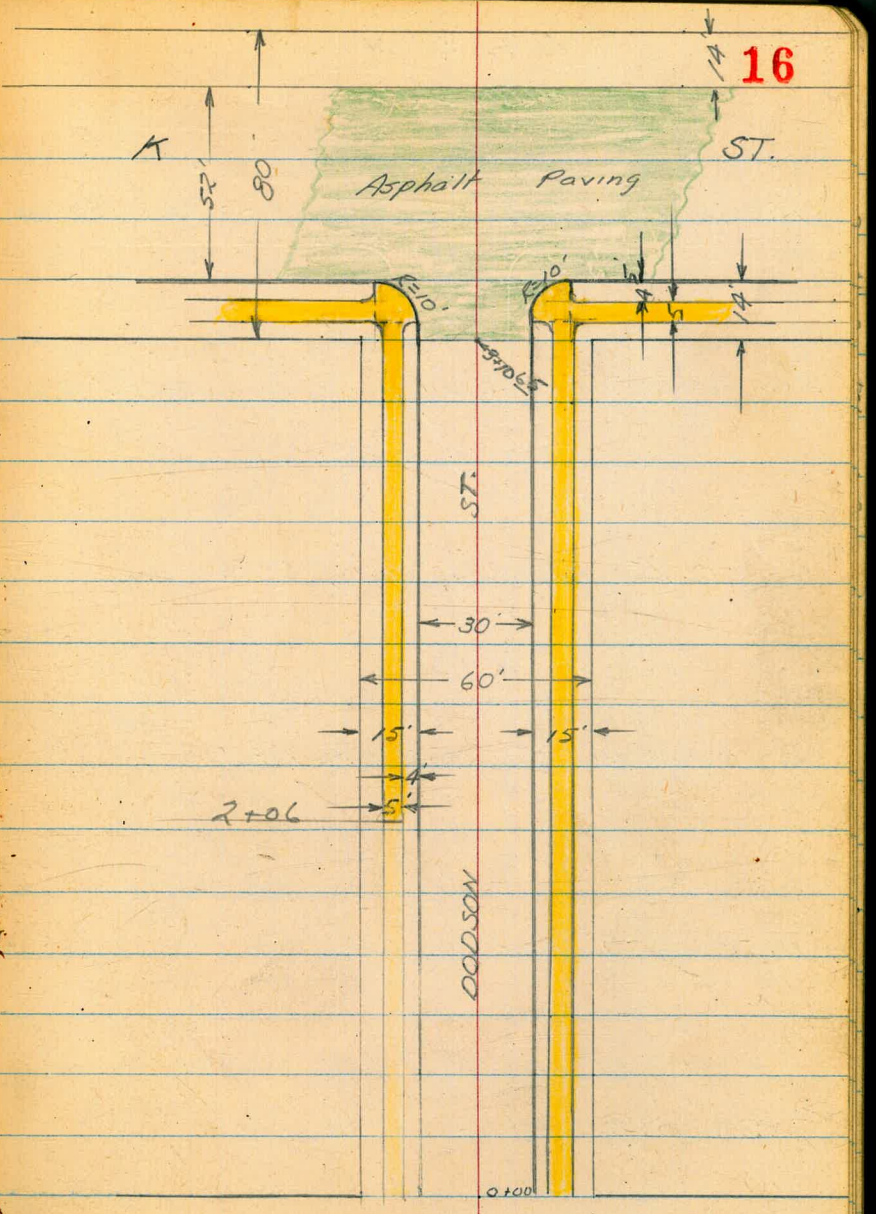




DODSON ST. Cont'd.



DODSON ST. Cont'd



Levels Dodson 57

BC on Market

SE Cb Rot. Market & Dodson (L = 26.5 3 parts)

BC on Market.

SW Cb Rot. Market & Dodson L = 26.4 3 pts

0 - 00.75 Edge Conc. Paving 6" End Cbs.

P. Hom 11-13-50

0-16 South Cb. Line Market

Reduced by

0.50 ℄ Market

T.B.M. 1.83	138.66 ✓	1.83	136.83
T.P. 8.78	138.66	2.30	129.88
T.P. 10.04	132.18	0.82	122.14
B.M. ℄ 13	122.96		11383

℄

134.52 135.09 134.28 134.99 134.13 134.89 134.20 134.81

4-14 3-57 4-38 3-67 4-53 3-77 4-45 3-85

G Cb G Cb G Cb G Cb

BC Market ① ② EC

131.65 132.23 131.92 132.47 132.07 132.65 132.20 132.80 Dodson

7-01 6-43 6-74 6-19 6-59 6-01 6-45 5-86

G Cb G Cb G Cb G Cb

BC Market ① ② EC Dodson

134.20 134.81 133.87 133.41 132.89 132.20 132.80

4-46 3-85 4-79 5-25 5-77 6-45 5-86

26.7 26.7 13 13 26.7 26.7

Cb G G Cb 8-73 9-12

136.78 136.21 135.09 134.52 134.36 134.03 133.26 132.42 131.85 131.65 132.23 130.46

1-88 2-45 3-57 4-14 4-30 4-63 5-40 6-24 6-81 7-01 6-43 8-25 7-80

90 90 46 46 40 26 26 40 46 46 74 74

Cb G 90 G G Cb G Cb

137.86 136.00 135.37 134.70 133.90 133.54 132.90 132.14 131.32

0-80 2-66 3-07 3-96 4-76 5-12 5-79 6-53 7-44

90 40 26 26 40 56 72 90

NE ℄ L&T Market & Dodson 138.66 ↑

SW BP Island & 30th

Dodson St. Contd.

0+35

0+29

0+19.5 ± End S.W. on Rt.

0+14

0+05 Fire Hydt. 28.6' Rt.

0+00 S. Line Market.

138.66

138.66

Dodson Cont'd

1+38 ℄ 3.7' Conc. Walk on Lt.

T.P. 3.98 137.57 5.07 133.59

1+33

1+25

1+24 Power Pole # WAL-52 16.9' Rt

1+00

0+70

138.66

134.01 133.88 ℄
3.5 3.69
40 36.0
Beg. Stairway

137.57

143.6	142.5	135.1	134.8	132.4	132.2	132.2	133.6	133.6	132.7	132.2
4.9	3.8	3.6	4.9	6.3	6.5	6.5	5.1	5.1	6.0	6.5
50	41	32	26	21		9	17	26	40	46

143.6	142.5	135.1	133.6	132.4	132.2	132.3	135.3	135.5	132.8	131.9
4.9	3.8	3.6	5.1	6.3	6.5	6.4	3.4	3.2	5.9	6.8
50	41	32	25	21		9	12	18	40	50

142.1	139.4	134.3	133.0	132.5	132.4	132.4	134.6	133.8	133.2	133.2
3.4	1.7	4.4	5.2	6.3	6.2	6.2	4.0	4.9	5.5	5.5
50	40	31	23	20		10	12	23	40	47

142.0	139.6	138.4	135.2	132.6	132.6	132.6	133.1	133.2	133.2	133.3
3.3	0.9	0.3	5.5	6.1	6.1	6.1	5.6	5.5	5.5	5.4
50	40	35	27	15		9	13	25	40	47

138.66

Dodson St Cont'd

℄

Station	Note	Elevations	Rod readings	Distances
2+30		144.7, 144.3, 138.2, 133.6, 131.3 | 130.3, 130.2, 130.6, 131.7, 131.9, 136.3, 136.7?, 135.3?	+7.1, +6.7, +0.6, 4.0, 6.3, 7.3 | 7.4, 7.0, 5.9, 5.7, 1.3, 0.9, 2.3	60, 48, 36, 34, 21 | 5, 7, 17, 31, 36, 40, 50
2+00		145.4, 145.0, 137.6, 133.3, 131.7, 131.3 | 131.3, 131.4, 132.8, 133.2, 135.6, 134.8?, 134.7?	+7.8, +7.4, 0.0, 4.3, 5.9, 6.3, 6.3 | 6.2, 4.8, 4.4, 2.0, 2.8, 2.9	50, 45, 35, 34, 20, 7 | 5, 10, 24, 27, 40, 50
1+70		145.6, 144.6, 133.9, 132.2, 131.8 | 132.0, 132.1, 133.3, 133.3, 132.8	+8.0, +7.0, 3.7, 5.4, 5.8, 5.6 | 5.5, 4.3, 4.3, 4.8	50, 43, 34, 21, 8 | 4, 13, 40, 50

Station	Note	Elev.	Rod	Dist.	Elev.	Rod	Dist.	Remarks
1+61	℄ 3.7' Conc. walk on Lt	134.07	3.50	39.9	133.90	3.67	35.9	Beg. Stairway
1+54.5	℄ Garage Conc. Ramp. Lt.	133.88	3.69	40	133.78	3.79	38	floor / Ramp
1+44.5	℄ Garage Conc. Ramp. Lt.	133.90	3.67	40	133.81	3.76	37.9	floor / Apron

137.57 (height of instrument; written at the foot of the left page and repeated on the right page)

Dodson St. Contd.

3+40.13 (Sewer MH) ℄ Island

3+16

3+14

3+00.13 North Line Island St

TP 385 131.90 9.52 128.05

2+92

2+60

137.57

127.2 128.0 128.3 128.57 128.4 128.1 127.4
4.2 3.9 3.6 3.3 3.5 3.8 4.5
50 30 15 Rim 15 30 50

126.6 127.4 127.9 128.2 128.9 128.0 127.8 127.3 126.9
5.3 4.5 4.0 3.7 3.0 3.9 4.4 4.8 5.0
50 40 26 19 12 20 40 50

127.5 128.1 128.5 128.1 128.9 128.0 128.5 127.9 127.4
4.4 3.8 3.4 3.8 3.0 3.9 3.4 4.0 4.5
50 40 26 19 12 20 40 50

129.3 129.6 129.1 128.6 128.9 128.4 128.9 128.7 128.9
2.6 2.3 2.8 3.3 3.0 3.5 3.0 3.2 3.0
50 40 22 20 9 11 24 40 50

131.90

SE 7' K&T Island & Dodson

137.6 137.1 136.5 130.7 129.2 128.6 128.9 128.6 129.1 128.9 132.1 136.6 136.0
0.0 0.5 1.4 6.9 8.4 9.0 8.7 9.0 8.5 8.7 5.5 2.0 1.6
50 40 35 32 22 20 8 10 24 38 40 50

141.3 141.1 138.9 132.1 130.8 129.8 129.5 129.4 129.7 130.4 136.4 137.1 137.6
+3.7 +3.5 +1.3 5.5 6.8 7.8 8.1 8.2 7.9 7.3 1.4 0.5 0.0
50 41 37 35 27 20 6 9 33 35 40 50

137.57

Dodson St. Cont'd.

1+00 Beg. Sidewalk on Rt

TP 2.35 121.50 12.75 119.15

0+98 Beg Sidewalk on Lt

0+50 End. Sidewalk on Lt

0+00
3+80.13 = So. Line Island

3+76.13 EC Cb Rets.

3+66.13 So. Cb Line Island

131.90

115.04 114.3 114.7 114.8 116.31 115.7 115.18 116.21 115.55
6.46 7.3 6.8 6.7 6.19 5.8 6.02 5.3 5.25
15 15 15 15 19 19 24 24
Cb Cb Dist Sw Dist Sw

116.51 115.40
5.98 6.10
24 19
Sidewalk

121.50

121.53 121.56 121.38 121.0 121.1 120.8 121.69 121.8
10.37 10.33 10.52 10.9 10.8 11.1 10.21 10.1
(24 19) 15 15 15 15 24
Sidewalk Cb Cb

127.90 126.4 126.6 126.4 127.45 127.96 128.04
4.00 5.5 5.3 5.5 4.15 3.94 3.80
15 15 15 15 (19 24
Cb. Cb. Sidewalk

127.95 126.7 126.8 126.7 127.84
3.95 5.2 5.1 5.2 4.06
15 15 15 15
Cb Cb

126.8 127.0 127.92 127.4 127.90 127.8 127.5 127.3 127.3 127.90 127.2 127.96 126.4
5.6 4.8 3.98 4.2 3.98 4.6 4.4 4.6 4.6 4.00 4.2 3.94 5.5
50 30 30 25 25 15 15 25 25 30 30 50
Cb Cb Cb Cb

131.90

Dodson St. Cont'd

2+00

1+93 ℄ 12' Drive on Lt

1+74 ℄ 13' Drive on Rt

TP 0.64 109.01 13.13 108.37

1+50 End SW, on Lt

(1+28 to 1+48 sidewalk on Rt. is warped & broken)

1+41 ℄ 10' Drive on Lt

1+22 ℄ 8' drive on Rt.

121.50

102.0 102.01 101.3 101.6 101.8 102.12
7.0 7.0 7.7 7.4 7.3 6.39
25 15 15 15 15
CB CB

102.78 102.84 102.37
6.23 6.17 6.64
24 18.5 15
Drive

105.53 106.27
3.48 2.74
15 19
Drive SW

109.01

108.83 108.77 108.71 108.1 108.1 108.2 109.08
12.65 12.73 12.71 13.4 13.4 13.3 12.42
24 19 15 15 15 15
(sidewalk) CB CB

109.74 109.26
11.76 12.24
19 15
SW Drive

111.98 112.86
9.52 8.64
15 19
Drive SW

121.50

Dodson St. Cont'd

3+45.07 BC Cb. Rds

3+10.07 North Line "J" St.

2+88

2+81.5 @ 12' Conc Drive on Rt.

T.P. 0.26 96.45 12.82 96.19

2+50

2+15 Rt 12' Drive on Rt.

109.01

℄

87.93 88.3
8 52 8 2
15 15
Cb. Dirt

88.6 88.87
7 2 7 58
15 15
Dirt Cb.

88.6 87.89 88.6 89.1 88.8 88.91
7 2 8 56 7 9 7 4 7 7 7 54
25 15 15 15 15
Cb Dirt Cb

91.1 90.82 90.5 91.1 91.0 91.74
5 4 5 63 6 0 5 4 5 5 4 71
25 15 15 15 15
Cb G Cb

91.84 92.56
4 21 3 20
15 19
Drive SWK

96.45

95.6 95.53 94.7 95.4 95.6 96.45
13 4 13 48 14 3 13 16 13 4 12 56
25 15 15 15 15
Cb Cb

100.15 100.83
8 86 8 18
15 19
Drive

109.01

Dodson St. Cont'd.

0+07 ℄ 12' Conc. Drive

0+00 Beg. 8' Woven Wire fence 25' Lt.
3+70.07 = 50 Line of St.

3+65.07 EC Cb Rets.

3+55.07 50 Cb Line

3+40.07 ℄ of St.

3+25.07 No. Cb. Line of St.

96.45

85.44 86.23
11.0 10.2
15 15
Drive S.W.

85.98 85.90 85.80 85.0 85.1 85.5 86.78
10.9 10.5 10.6 11.5 11.4 11.0 9.6
(24 19) 15 15 15 15
Sidewalk Cb. Cb

85.83 85.4 85.8 86.18
10.6 11.- 10.2 9.6
15 15 15 15
Cb Cb

85.03 84.5 85.81 85.5 85.86 85.6 86.0 86.2 86.2 86.9 86.82 87.3 86.94 88.0
11.4 12.0 10.6 11.0 10.5 10.2 10.5 10.3 10.3 10.3 9.6 9.6 9.3 9.1 7.5
50 50 30 30 25 25 15 15 25 25 30 30 50
Cb Cb Cb Cb Cb

85.7 86.4 87.0 87.2 87.1 87.6 88.0 89.3
10.8 10.1 9.5 9.3 9.0 8.5 7.2
50 30 15 15 30 50

86.93 86.0 87.80 87.0 87.85 87.1 87.5 88.1 88.0 88.3 88.90 88.6 88.91 88.9 89.10
9.5 10.5 8.6 9.5 8.6 9.4 9.0 8.4 8.5 8.3 7.55 7.3 7.3 6.5 5.5
50 50 30 30 25 25 15 15 25 25 30 30 50 50
Cb. Cb Cb Cb Cb Cb

96.45

Dodson St. Contd.

1+95 ℄ 11' Conc. Drive on Rt.

1+50

1+22.5 ℄ 15' Conc. Drive

1+00

0+84 ℄ 12' Conc. Drive on Rt.

0+50

T.P. 0.99 86.96 10×8 85.97

96.45

℄

75.07 11 89 15 Drive S.W.

75.80 11 15 19

76.6 10 25 Cb

76.22 10 74 15

75.9 11 15

76.5 10 5

76.5 10 5 15

77.01 9 25 15 Cb.

77.30 8 Cb 15

76.15 8 81 19 Drive S.W.

78.5 8 25 Cb

78.33 8 63 15

78.0 9 15

78.5 8 5

78.4 8 5 15

79.03 7 93 15 Cb

79.28 7 28 15

80.02 6 94 19 Drive S.W.

82.0 5 25

81.70 5 26 15 Cb

81.1 5 2 15

81.5 5

81.6 5 4 15

80.45 4 51 15 Cb

86.96

2E 7' Lt. Dodson & J St.

Dodson St Cont'd

3+10.65 Edge Asph. Paving No. Line K" St.

2+70 End Woven wire fence 25' Lt.

2+50

2+06 Beg S.W. on Lt.

2+17 & 12' Conc Drive on Lt.

2+12 & 13' Conc Drive on Lt.

TP 5.62 79.80 12.78 74.18

2+00

86.96

℄

73.90 73.44 73.80 72.71 74.36
5.90 6.36 6.00 6.09 5.44
15 15 15 15
Cb G G Cb

74.50 74.1 74.4 74.3 74.95
5.30 5.7 5.4 5.5 4.85
15 15 15 15
Cb SWK Cb

75.11 75.19
4.69 4.61
27 19
(Sidewalk)

74.62 75.42
3.8 4.38
15 19
Drive SWK

75.05 74.36
4.75 5.44
19 15
SWK Drive 79.80

75.5 75.11 74.7 75.3 75.0 75.54
11.5 11.85 12.3 11.7 12.0 11.42
25 15 15 15 15
Cb Cb

86.96

Dodson St Cont'd

BM			2.49	113.83	113.83
TP	6.72	116.32	0.66	109.60	
TP	10.31	110.26	0.13	99.95	
TP	12.62	100.08	0.43	87.46	
B.M.	11.05	87.89	2.02	76.84	77.01
TP	6.68	78.86	7.62	72.18	
BM	0.46	79.80	0.46	79.34	79.47

3+50.65 ℄ K St.

3+24.65 No Cb Line "K" St.

3+14.65 BCs Cb. Rets

79.80

℄

SWBP 30th & Island (Starting B.M.)

SWBP 30th & J Sts.

SEBP 29th & "K"

73.34 73.50 73.63 73.77 73.75 73.89 74.29 74.67 74.01

6^{46} 6^{30} 6^{17} 6^{03} 6^{05} 5^{91} 5^{57}) 5^{13} 5^{79}

50 30 15 15 30 50) 50 50

Cb G

73.83 73.12 73.86 73.22 73.86 73.25 73.29 73.46 73.64 73.72 74.38 73.79 74.43

5^{97} 6^{68} 5^{94} 6^{58} 5^{94} 6^{55} 6^{51} 6^{34} 6^{16} 6^{08} 5^{42} 6^{01} 5^{37}

50 50 30 30 25 25 15 15 25 25 41 41

G Cb G Cb G G Cb G Cb

73.87 73.43 73.69 73.76 74.32

5^{93} 6^{37} 6^{11} 6^{04} 5^{48}

15 15 15 15

Cb. G G Cb.

79.80

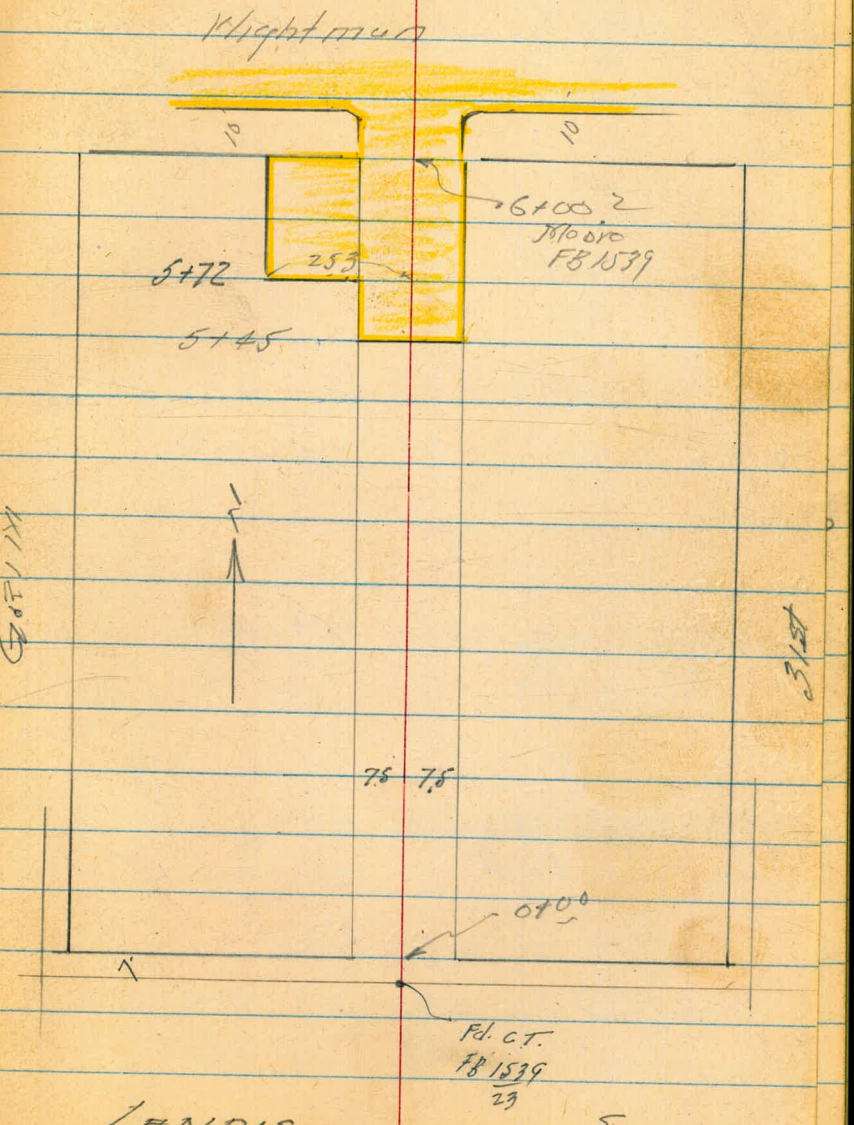
Cross Section Alley Block 8
McFadden & Buxton
Block 7 - North Park
Between Griffin & 31st
From Landis to Wightman
Orig. Sections in FB 1539-23
WO 25020

(Direct Elev. Rod used)

INDEXED
MAR 13 1951

Walker 3-12-51
Pope
Clark
Huffman

29



Alley — Cont.

0+59. ℄ Gurage on Rt. St. Entrance

0+57 ℄ Gurage on Lt.

0+50

0+24 6.2' Rt = ℄ Tel Pole 307187-H

0+15

0+00 = N.W. Landis

0-10

0-30' = ℄ Landis

T.P. 341.08

SE.B.P. Roy + Landis 340.91

℄

345.40
22.8

344.59
18.2
on Conc. Floor.

344.5 344.6 344.6 344.5 345.0
15 7.5 7.5 15

343.5 343.1 343.1 343.5 344.1
20 7.5 7.5 15
on Ground

341.20 341.11 340.88 341.10 341.18
7.5 7.5 7.6 7.6
Cb Gut. Gut Cb

340.50 340.21 340.94 340.82 340.82 341.07 340.71 341.26 340.97
50 50 95 95 10 10 50 50
Cb. Gut Cb. Gut Cb Gut Cb. Gut

340.42
50
on Pav.

340.72
Rim
MH

341.27
50
on Pav.

Alley

4.5' High 8" wide

1+50 = Beg. Conc. Tile 14611 7.2' Rt.

Tel.

1+50 = ℄ Pole on Rt. 2' Rt. # JPH 3722

1+47 = End Dble Gurage

1+33 = Beg. Dble Gurage

1+25 = Beg. Conc. Apron on ℄

1+24 = Beg. Board Fence 7' Rt.

1+21 = End Dble Gurage on Rt. St Entrance

1+01 = Beg. Dble Gurage on Rt. St. Entrance

T.P 345.89

1+00 = End 4' Picket Fence 7.2' Rt.

1+00 7.3' Lt. = Elec Pole # 83715

4' Picket

0+67 = Beg Fence on Rt. 7.4' Rt.

0+69 = ℄ 2' Conc. 14614

Lt. ℄ Rt.

30

346.3 346.3 346.4
7.5 7.2
at wall

346.33 346.27
11.2 8
Conc. Floor Apron

346.21 346.15
11.2 8
Floor. Conc. Apron

346.14
8
Conc. Apron

346.59
8.7
Floor

346.38
8.7
Floor.

345.4 345.4 345.6 345.2
12.5 7.5 7.5

345.05
7.5

Alley	Lt.	℄	Rt.
2+50 = Beg. Dble. Garage on Lt. St. Entrance	347.98 8.3 Floor		
2+50 = End 4' Picket Fence 7.5'R	346.6 15 Yard; 346.8 8; 348.0 7.5	347.7	347.6 7.5; 347.4 15 Yard; 347.4 35 Yard
2+25 Note: Water Stands in these Yards. Be sure to Lay Grade below Yards.	347.0 20 Yard; 347.3 7.5	347.4	347.4 7.5; 347.1 15 Yard
2+15 6.8' Lt = Elec. Pole; Beg. 4' Picket Fence 7.2' Rt.			
2+00 = End 8" Conc. Tile Wall 7.4' Rt	346.6 15 Yard; 347.0 7.5	347.0	347.1 7.5
1+99 = End 6" Conc. Wall	347.00 82 Wall; (Drain This)		
1+77 = ℄ Gate to yard			346.8 10 Lawn; 346.7 20 Lawn
1+70 = Step up in Conc. Wall	347.00 8.2 Wall		
1+66 = Beg. 6" Conc. Wall	346.60 8.2 Wall		
1+66 = End Dble Garage	346.56 89 Floor		
1+51 = Beg. Dble. Garage on Lt. St. Ent.	346.56 8.9 Floor		

Alley

	Lt.	℄	Rt.
3+45 = Elec. Pole 6.5' Lt # A-3765			
3+20 = Beg. 5' Picket Fence 7' Rt	349.0 15 Yard	348.9 7.5	349.1 7.5 / 349.3 15 Lawn / 349.0 35 Lawn Yard.
3+08 = ℄ Gurage on Rt St. Entrunce			348.75 9 Floor.
6.2' Lt = 3" Popper Tree #			
3+18 6.3' Rt = Telpole 84367-H			
TP	349.19		
3+00 = End Fence 7.3' Lt	348.5 20 Yard	348.7 7.5	348.8 7.5 / 348.7 25 Yard Lawn
2+70	348.2 15 Yard. Lawn	348.5 7.5	348.2 7.5 / 348.0 9 Drainage Ditch. to yard / 347.6 20
2+68 = End Gurage on Rt. St. Entrunce			347.60 9.4 Floor.
Beg. Fence 7.3' Lt.			
2+66 = End Dble Gurage on Lt St Ent	347.98 8.3 Floor		
2+52 = Beg. Gurage on Rt. St. Ent.			347.60 9.4 Floor.

				Alley	Lt.	℄	Rt.
4+75			Lay Grade to Drain Yards		352.3 15 Yard	352.7 7.5	352.5	352.0 7.5	351.9 20 Yard
4+50									
4+45	6.5 Rt	#82310 H	Tel Pole		351.7 20 Yard (Drain This)	352.2 7.5	352.1	352.0 7.5	351.8 20 Yard.
4+00					351.0 12	350.9 7.5	350.8	350.9 7.5	350.7 15
3+99								350.71 7.5 Flour.	
3+73 = Beg. Work Shop & Gurage on Rt St. Entrance								350.44 7.5 Flour.	
3+68 = End Dble. Gurage St. Entrance					350.10 7.4 Floor.				
3+50 = Beg. Dble. Gurage on Lt. St. Entrance					349.8 8 Yard	350.20 7.4 Floor.	349.9 7.5	349.9 0	349.9 7.5	349.7 10 Yard

	Alley		Lt.	℄	Rt.
5+70			35280 35220 35194 351.79		35220 352.80
T.P.		351.63	4 6 7.5 Edge Pov. Brk Edge Pov		6 7 Brk Edge Pov
5+50	6.4' Rt = Pole # 82309-H		353.14 352.81		353.20 353.89
			7.5 Pov	Pov	6.3 7.3 Brk Pov. Edge
5+45 = Beg. Exist Pov.			35327 353.08		35328
			7.5 Pov.		6.5 Edge Pov
5+36 = ℄ Shop or Shed on Rt. Conc. Floor, Dble on Lt. Conc. Floor					
5+36	℄ Gurage Alley Entrance		35307 353.2	353.2	353.5 353.26
			11.2 Conc. Floor		7.5 11.4 Conc. Floor-Shed
5+09 = ℄ 16' Dble Gurage St. Entrance.					35323
5+01 62' Lt. = Pole Anchor, Gurage = St					10.8 Conc. Floor
4+94 = ℄ Conc. Apron Not used		Entrance	35278 35277 352.96 353.0		352.7 352.4 352.3
			17 12.4 7.8 Floor Brk Apron Apron		7.5 10 25 Yard Yard Lawn
T.P.		352.80			
4+78 = ℄ Pole 6.4 Lt.		A-3773			

	Alley		Lt.	℄	Rt.
B.P.		0.05			
S.E. Roy & Landis		340.91			
Chk. Starting B.M.		340.86			
T.P.		344.70			
		0.06			
S.E. B.P. Roy & Wightman		351.66			
Chk B.M.	FS. 1539 = 25'	351.72			
T.P.		350.74			
6+10.2 = 5 curb W		351.11 75' Cb.	350.64 75 Gut.	350.91 25 Gut. in Drive	350.98 10 Gut. in Drive
			350.98	350.98 10 Gut. in Drive	351.02 25 Gut. in Drive
6+00.2 = ℄ Line			351.51 28.7 Pav.	351.76 7.5 Walk & Pav. Some	351.20
			351.52 7.4 Pav. & Curb Some		
5+72 - Beg. Ramp			351.97 25.3 Conc. Deck	351.72 28 Black Pav.	351.80 75 Pav.
			351.45	352.02 6 Brk	352.63 7.2 Edge Pak

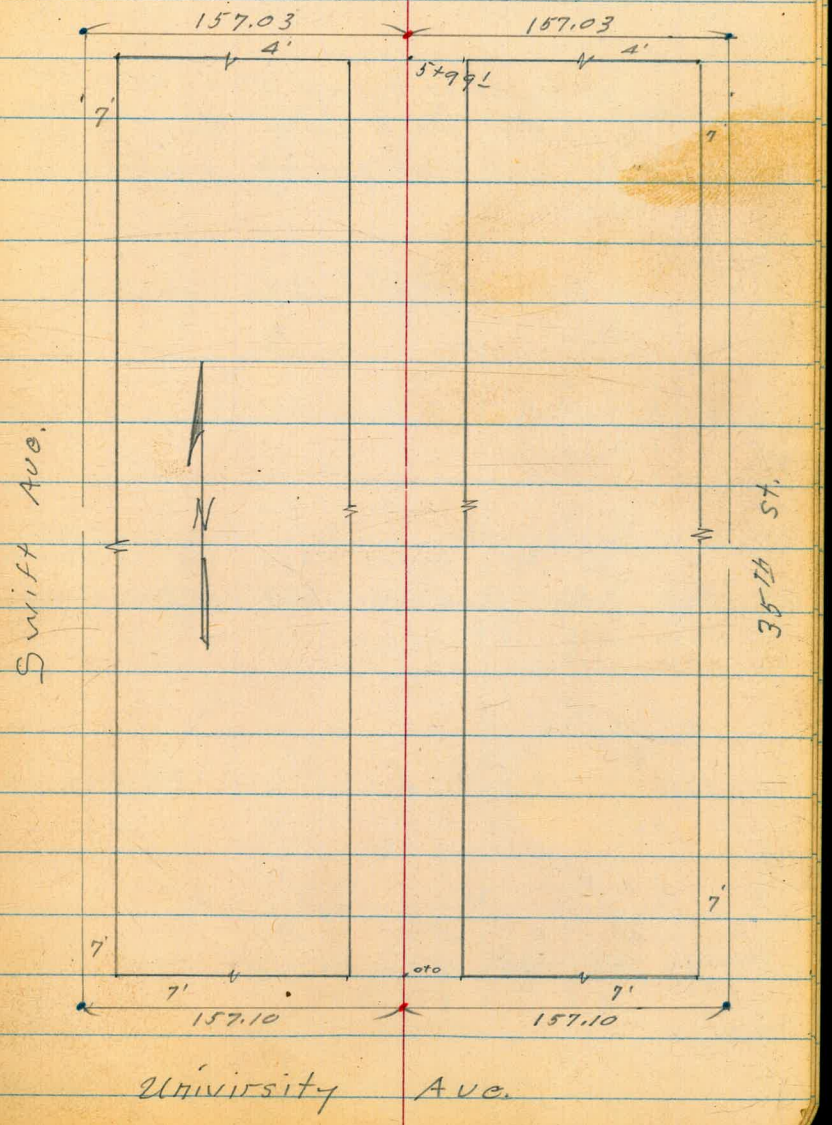
Cross Section Alley Blk. 197 City Hgts.
Univ. to Polk - between 35th & Swift.

5-Apr. 1951
W.O. 25020

Sommermeyer
Begg
Wierciszewski.

• = Fd. L.47. C.T.P. Sheet # 3556

• = Set Conc. Nail in pave.



Alley Blk. 197 City Hgts

Levels.

Reduced by R.W. McHarg 5-3-51

1+00

14' Rt. = Start Repair Shop - Conc. Floor Shop.
11½ Rt. = Start. conc. Apron To Repair Shop.
0+81 10' Rt. = end paved parking lot.

Pole A 4015.
Tip 5.61 369.80 1.80 364.19

0+50

10' Rt. = start Cold lay in parking lot.
0+00 = Nly. line Univ. = end E.C. Pave. end A.C. Pave.

0-12 10' Rt. } = E.C. 2' Rad. cl. Rct.
10' Lt. }

0-14 = Nly cl. line Univ.

7.13 365.99 — 358.86

363.70 6.1 / 85
363.50 6.3 / 50
364.10 5.7 / 10
363.70 6.1
364.0 5.8 / 10
363.90 5.9 / 11½ Apron
364.1 5.66 / 14' Shop Floor

363.6 6.2 / 10
363.6 6.2
363.90 5.9 / 10 end + plant mix
363.87 5.93 / 11½ Apron
363.97 5.83 / 14

369.80

362.9 3.1 / 10 / 1
362.6 3.4 / 1
363.09 2.90 / 10 = paved lot
363.6 2.4 / 25

360.63 5.36 / 10 / end cl.
360.61 5.38 / 10 / G
360.48 5.51
360.83 5.16 / 10 / G
360.84 5.15 / 10 / end cl.
360.95 5.04 / 10 / paved lot
361.01 4.98 / 10

360.24 5.75 / 10 / cl. E.C.
360.04 5.95 / 10 / G
364.29 5.70 / 10 / G
360.61 5.38 / 10 / cl. E.C.

360.21 5.78 / 12 / A.B.C. 2' Rad.
357.85 6.14 / 12 / G.
357.85 6.14 / 10
355.94 6.05
365.99
360.03 5.96 / 10
360.09 5.90 / 12 / G
360.46 5.43 / 12 / A.B.C. 2' Rad.

N.W.B.P. Swift + University.

Alley

10' Lt. = ℄ Conc. Apron 8' wide.
3+45 14⁶ Lt. = ℄ Sing Gar. Conc. floor.
Pole # 406933H

T.P.	5.55	373.42	1.93	367.87

3+00

2+50

2+00

1+65 14⁷ Lt. = ℄ Sing. Gar. (Not in use) dirt floor

1+50

1+25 14⁹ = end Repair shop
11⁵ Rt. = end conc. Apron

℄

367.43 — 5.99 / 14⁶ Floor
367.44 — 5.98 / 10 Apron + end

3 13.42

363.50 — 6.0 / 150
366.40 — 3.4 / 10
366.70 — 3.1
366.70 — 3.1 / 10

365.80 — 4.0 / 75
365.80 — 4.0 / 50
366.0 — 3.8 / 10
366.30 — 3.5
366.50 — 3.3 / 10

364.90 — 4.9 / 75
365.0 — 4.8 / 50
364.80 — 5.0 / 10
365.30 — 4.5
365.40 — 4.4 / 10

364.60 — 5.2 / 14⁷ Floor
364.70 — 5.1 / 14

364.50 — 5.3 / 10
364.70 — 5.1
364.80 — 5.0 / 10

364.40 — 5.4 / 10
364.60 — 5.2
364.20 — 5.6 / 10
364.05 — 5.75 / 11⁵ Apron
364.16 — 5.64 / 14 Floor Repair shop

369.80

Alley Blk 197 C.Ty Hgts.

5+00

4+50

4+33 $14\frac{5}{}$ Lt. = end triple Gar. Bldg.

4+28 = ℄ 3rd door. } Conc floor

4+18 = ℄ 2nd door } No Apron

4+08 = ℄ 1st door }

4+04 - $14\frac{6}{}$ Lt. = start triple Gar. Bldg.

4+00

3+50

℄

368.72 — 4.5 / 10

369.12 — 4.3

369.22 — 4.2 / 10

368.32 — 5.1 / 50

368.52 — 4.9 / 10

368.72 — 4.7

368.92 — 4.5 / 10

368.79 — 4.63 / $14\frac{5}{}$ Floor

368.62 — 4.60 / $14\frac{5}{}$ Floor

368.09 — 4.63 / $14\frac{5}{}$ Floor

368.32 — 5.1 / 10

368.22 — 5.2

368.52 — 4.9 / 10

367.42 — 6.0 / 10

367.72 — 6.2

367.42 — 6.0 / 10

373.42

Alley Blk. 197 City Hgts.

Orig B.M.			6.73	358.88	(358.86)
	3.90	365.61	10.64	361.71	(361.55)
T.P.	4.76	372.35	7.62	367.59	
T.P.	5.13	375.21	4.77	370.08	

also = sly el. line Polk.

6+05 — 12' Rt. } = el. E.C.
12' Lt. }

6+03 — 10' Lt. } el. B.C. 2' el. Rad.
10' Rt. }

5+99 — = Sly. line Polk.
= start A.C. Pave
10' Rt. }
10' Lt. } start alley els.

(walk to porch.)

5+64 — 11½ Lt. = ± 5' wide conc. slab.

5+50

18' Rt. = ± sing Gar. Conc. floor.
16 Rt. = ± 8' wide apron

5+34 — 18 Lt. = ± sing Gar. Conc. floor apron. No

T.P.	5.21	374.85	3.78	369.64	

N.W.B.P. Unio + Swift.

N.W.B.P. Unio + 33-Ht

369.14 — 5.71 / 60 G

369.74 — 5.09 / 12 el. E.C.

369.25 — 5.60 / 12 G

369.35 — 5.50 / 10

369.34 — 5.51 / 10

369.33 — 5.52 / 12 G

369.84 — 5.01 / 12 el. E.C.

369.49 — 5.36 / 60 G.

369.80 — 5.03 / 10 el. B.C.

369.51 — 5.34 / 10 G

369.55 — 5.30 / 10 G.

369.90 — 4.95 / 10 el. B.C.

369.86 — 4.99 / 10 el

369.65 — 5.20 / 10 G

369.55 — 5.30

369.73 — 5.12 / 10 G

370.02 — 4.83 / 10 el

370.33 — 4.52 / 11½ ± slab.

370.05 — 4.8 / 10

369.95 — 4.9

369.95 — 4.9 / 10

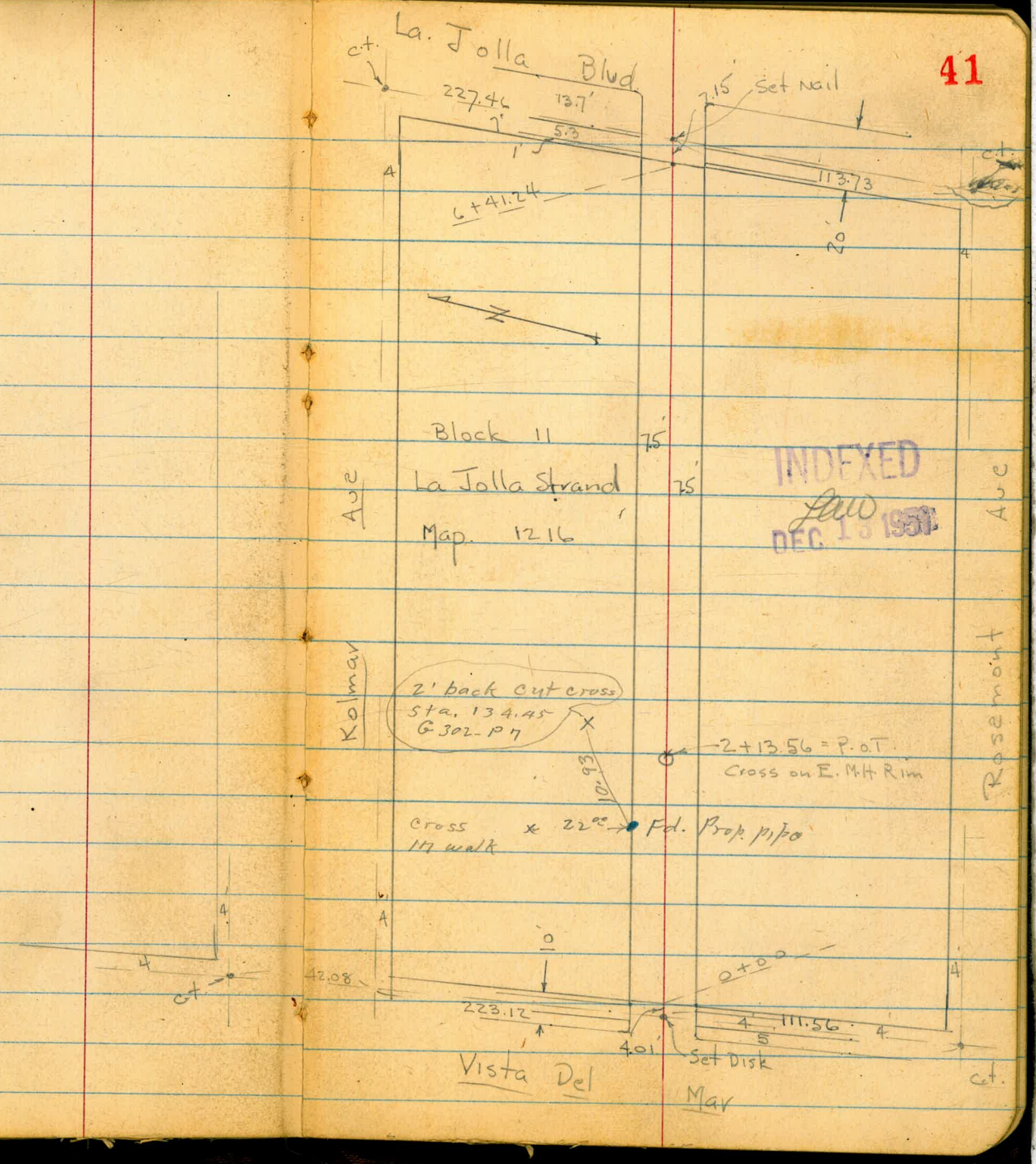
370.03 — 4.82 / 18 Floor

369.98 — 4.87 / 16 Apron

370.52 — 4.33 / 18 Floor

374.85

~~373.42~~



X-Sect 15' Alley - Block 11 - La Jolla Strand
for Paving.

5721 9-18-51 - 7.0.

W.O. 31346

7.8 - Lt. = Sly of 3' Conc walk along House
0+50 - 6.7 Lt. = Beg. ℄ of 8' Hedge - 16' High
Ave. 6" Trunks

0+47 - 6.8' Lt. = ℄ 3.5' Conc. walk

0+28 - 7.9 Lt. = Cor. steps - (wood)

0+10

Produced & Plotted by A. Mills 9-20-51

0+00 = E.L. Vista Del Mar. + edge Conc. Pave +

0-10 = E. cb.

B.M. 10.75 41.17 30.42 = S E.BP. Kolmar & Vista Del Mar.

	Lt.		℄		Rt
	39.76	39.8	35.5	37.5	39.7
	1.41	1.4	1.7	1.7	1.5
	7.8 walk	7.5		7.5	15
	38.65	39.53			
	1.52	1.64			
	10.8 at House	6.5 walk			
37.0					
4.7					
7.9 = along Cor					
	34.6	34.0	33.7	33.9	34.7
	6.6	7.1	7.5	7.3	6.5
	8.8 along steps	7.5		7.5	15
	31.40	31.55	31.47	31.47	31.81
	9.57 Top= end	9.62 7.5 gut.	9.70	9.70 7.6 gut.	9.36 Top= end.
30.95	30.85	31.41	30.84	30.91	30.95	31.72	31.42	32.14
10.22	10.82	9.76	10.33	10.26	10.22	9.45	9.75	9.03
Top	5.7 gut.	Top 2' Rad.	7.5 gut.	41.17	7.5 gut	Top 2' Rad.	5.0 gut.	Top

Lt. ℄ Rt.

1+75

1+66 - 7.1 Lt. = end Conc. wall

T.P. 12.79 66.56 0.12 53.77

1+50

1+17 - 7.4' Lt. = Beg. 6" Conc. Wall - stepped.

1+15 - 7.1 Lt. = end ℄ Hedge

1+00 - 7.5 Lt. = ℄ Hedge

at Cor. Beg. Wall is 7.8 Rt.

0+93 - 7.5' Rt. = Beg. Conc. Wall - Brick Collaum

0+82 - 6' Rt. = ℄ P. pole # A210

T.P. 13.23 53.89 0.51 40.66

0+62 - 7.5 Lt. = end - Cor. Walk

Lt.		℄		Rt.
55.76	56.1	56.0	56.2	56.6
11.0	10.5	10.6	10.4	10.0
15	7.5		7.5	7.9 = wall
54.70	54.05	54.8		
11.86	12.51	11.8		
Top wall	Bottom wall	7.1 ground		66.56
53.70	52.5	52.1	52.6	52.6
0.19	1.4	1.8	1.3	1.3
7.1	7.1 =		7.5	7.7 = wall
Top wall				
49.37	47.49	48.2		
4.52	6.40	5.7		
7.4	Bottom	7.4 = ground		
Top wall				
45.3	45.9	45.7	46.00	46.1
8.6	8.0	8.2	7.9	7.8
15	7.5		7.5	7.8 = along wall
			45.1	44.14
			8.8	9.75
			7.5	Bottom
			ground	
				53.89
41.42	41.32			
+0.25	+0.15			
15	7.5			
	Cor. walk			
				41.17

Conc. floor

2+84 - 8.4' Rt. = end wall + Beg. Doub. Gar.

2+80 - 6.3' Lt. = end fence

2+67 - 8.8' Rt. = end House + Beg. Stucco wall

2+66 - 5.8' Lt. = Beg. Wire fence

2+50 - 24.5' Lt. = ℄ Doub. Gar.

2+38 - 6.8' Rt. = ℄ P. pole PA 260

2+37 - 8.3' Rt. = end wall + Beg. Stucco House

2+25

Sewer

2+13.56 = Cross on MH. 7.02

Beg. Rough Cold Lay Pave

2+10 - 10.5' Lt. = ℄ Conc. apron to Doub. Gar.

2+04 - 8.2 Rt. = ℄ 3' Conc walk Thru wall

2+01 - 7.6' Lt. = end wall

2+00

1+80 - 7.6' Lt. = Beg. Rock & Conc. wall to Greenhouse

Lt. ℄ Rt.

63.59 2.97 8.4 floor Gar.

62.16 4.0 8.5 = ground

61.99 4.57 24.5 floor Gar.

61.6 5.0 7.5

61.4 5.2 5

61.7 4.9

61.7 4.9 7.5

61.9 4.7 8.4 = House

61.7 4.9 8.3 ground

60.65 5.91 Bottom

60.7 5.9 15 ℄ C.L.

60.6 6.0 7.5

60.3 6.3 6

61.5 6.1

60.4 6.2 7.5

60.8 5.8 8.2 = wall

60.29 6.48 22.5 floor Gar.

59.76 6.80 10.5 = apron

59.58 6.98 8.2 = walk

60.26 6.30 Top

59.25 7.31 Bottom

59.5 7.1 7.6 = ground

59.3 7.3 7.6 at wall

59.50 7.6 7.5

59.5 7.7

59.50 7.6 7.5

59.35 7.1 8.1

59.04 7.52 8.1 Bottom wall

59.28 7.28 Top

59.16 10.40 Bottom

59.0 10.0 7.6 ground

66.56

3+68 - 13.2' Rt. = Conc. apron to Doub. Gar. - Beg.

3+50

3+47 - 8' Lt. = ℄ 11' Conc. Slab. - for Garbage Cans

3+37 - 12.5' Lt. = ℄ Sing. Gar. - Conc. floor

3+36 - 18.1' Rt. = ℄ Sing. Gar. - Conc. floor

T.P.	5.66	71.27	0.95	65.61
Set B.M. = Nail in Pole - Below			0.95	65.61

3+19 - 8' Rt. = ℄ P. pole # P.P. 316

3+18 - 8.7' Rt. = end wall

3+12 - 5.8' Lt. = end Conc. Slab - apron

3+05 - 8.6' Rt. = end Gar. & Beg. stucco wall

3+03 - 8.9' Lt. = Beg. Conc. apron to Shed.

3+00 = ℄ Sing Gar. on Lt. - Conc apron

2+91 - 7' Lt. = ℄ 5' Conc. slab.

Lt. ℄ Rt.

66.78 4.49 13.2 apron — 67.24 4.03 16.2 = floor Gar.

64.57 6.30 8 Conc slab — 64.5 6.4 7.5 — 6.4 — 64.51 6.2 7.5 — 65.05 5.5 13.2 — 66.81 4.46 13.2 Top Conc. step

64.95 6.28 12.4 at House — 64.97 6.30 8 = Conc. — 64.79 6.48 12.5 floor

65.33 5.94 18.1 = floor.

71.27

64.3 2.3 8.7 ground — 63.2 3.32 Bottom

63.74 2.82 11 floor shed — 63.74 2.82 5.8 = Cor. apron

63.61 2.95 8.6 = floor Gar.

63.71 2.85 11.1 floor shed — 63.44 3.12 8.9 = apron

63.29 3.27 10.7 floor — 63.18 3.38 9.1 apron — 63.3 3.3 7.5 C.L. — 63.3 3.3 — 63.5 3.1 7.5 — 63.64 2.92 8.6 floor Gar.

63.20 3.26 11.1 Gar. — 63.04 3.52 7 Conc.

66.56

T.P. 8.04 79.17 0.14 71.13

5+00 = end Cold Lay

4+80 - 7.5' Lt. = end apron

4+56 - 7.5' Lt. = end slab. + Beg. Conc. apron

4+50

4+43 - 7.5' Lt. = Beg. Conc. Slab.

4+27 - 7.8' Rt = Beg. Conc. apron to Line of Gar.

4+17 - 7.4' Rt. = ℄ P.pole - # P.A.366

4+00 Rt. = Conc. apron to Doub. Gar.

3+84 - 13.2' Rt. = end apron

Lt. ℄ Rt.

71.2
0.1
15

70.7
0.6
7.5

70.7
0.6

70.85
0.42
7.5
apron

70.92
0.35
15 = floor
Gar.

69.91
1.36
14.3
floor

69.81
1.46
7.5 = apron

69.87
1.10
10.1
floor
Gar.

69.33
1.94
7.5 = apron

69.87
2.30
7.5 = slab.

68.92
2.35
7.5
Conc.
slab

68.73
2.54
7.5 = Conc.

68.86
2.7

69.0
2.3
7.5

69.08
2.19
7.7
apron

69.97
1.30
15 = floor
Gar.

68.25
3.02
7.8
apron

70.02
1.25
15.8
floor
Gar.

66.9
4.4
15

66.5
4.8
7.5

66.5
4.8

66.7
4.6
7.5

67.12
3.85
11.9
apron

67.28
3.59
15
floor
Gar.

66.97
4.30
13.2
apron

67.25
2.98
16.2
floor

71.27

6 +00

Laid on ground.
5+95 - 7' Lt. = Beg. 6" Conc. Block wall - No Mortar

.5+94 - 7.1' Lt. = ℄ 2' Conc. walk

5+91 - 7.4' Rt. = end steps

5+82 - 7.4' Rt. = Beg. Conc. Steps along House

5+66 - 7.4 Rt. = end apron

5+57 = 7.5' Lt. = end apron

5+50

5+46 - 7.5' Lt. = Beg. Conc. apron to House - was Gar.

5+32 - 7.6' Rt. = Beg. Conc. apron to 3 Car. Gar.

5+25 = 7.2' Rt. = ℄ P. pole - # P.A. 386

5+08 - 7.6' Rt. = end Conc. apron

Lt.	℄	Rt
74.91 4.26 10 on Conc. walk	76.59 2.58 7 = Top wall	74.9 4.3 7
76.53 2.64 7 Top wall	74.8 4.4 7 = ground	
74.77 4.40 13.5 at steps	74.92 4.25 7.1 = walk	
73.16 6.01 11.1 at House	73.01 6.10 7.5 = apron	
73.04 6.13 7.5 apron	72.9 6.3	73.21 5.96 7.4 apron
73.12 6.05 11.1 House	72.98 6.19 7.5 = apron	
		72.50 6.67 7.6 apron
		71.11 8.06 7.6 apron

Lt.	℄	Rt
74.5 4.2 7.4 = ground	75.0 4.2 7.4 = ground	75.2 4.0 7.5
74.5 4.7 7.4 ground	76.57 2.60 7.4 Top steps = Porch	74.48 4.69 7.4 Bottom found.
	74.54 3.73 7.4 = Top of Bot. step	
	73.70 5.47 7.4 apron	73.79 5.38 13.9 floor Gar.
		73.79 5.38 13.9 floor
		73.14 5.39 13.9 = floor
		70.84 8.29 15 = floor.

Lt.	℄	Rt
		75.3 3.9 9.4 = along House
		76.57 2.60 9.4 = at House

79.17

Note: Something Wrong with Benches
See P. 49

check B.M. 6.19 74.89

6+61.9 = w.cb.

T.P. 4.96 81.08 3.05 76.12
Sect along W.L.
on curb on Rt. - for 2.1' from W.L.
+ curbs. - Top Broken

6+41.24 = W.L. La Jolla Blvd. = edge A.C. Pave

6+41 - 7' Lt. = Near edge of 30" Cypress

6+38 - 6.5' Lt. = Near edge of 30" Cypress Tree

6+34 - 6.9' Lt. = end wall

Note: Prop Owners want Trees out

6+30

6+16 - 7.3' Rt. = end Conc. Porch

6+08 - 7.3' Rt. = Beg. Conc. steps + porch

Lt. # Rt

74.90 in Office Book
Must be wrong.

48

S.W. Kolmar & La Jolla = 75.27 = Book

75.67	75.20	76.23	75.80	75.90	75.98	76.42	76.40	76.94
5.41	5.88	4.85	5.28	5.18	5.10	4.66	4.68	4.14
50	50	Top	7.5		7.5	Top	50	
Top	gut.	2' Rad.	gut.		gut	2' Rad.	gut.	Top.

81.08

76.54	76.35	76.19	76.45	76.53	76.68	
2.63	2.82	2.98	2.72	2.64	2.49	
7.6	7.6		7.5	7.8	walk	
Top: ok	gut		gut.	Top - Broken off	opp.	

76.23	76.0	
2.44	3.2	
6.9	6.9	
Top - end wall	ground	

76.61	76.63	75.7	75.9	76.0	76.45	
3.16	2.54	3.5	3.3	3.2	2.7	
10.1	6.8	6.8		7.5	15	
edge walk	Top wall					

75.6	75.96	76.65	76.65	
3.6	3.81	2.52	2.52	
7.3	Bottom	7.3	9.4 - at	
ground		Top	House	

75.4	75.17	76.07	
3.8	4.00	3.10	
7.3	7.3	7.3 = Top	
ground	Bottom	Bot step.	

79.17

6.07	80.96		74.89 = S.W.B	P. Kolmar + La Jolla Blvd.
0.28	68.16	13.08	67.88	
0.68	55.89	12.95	55.21	
0.39	43.09	13.19	42.70	
1.45	36.07	8.47	34.62	
		5.64	30.43	30.42 = starting B.M.
10.83	85.72		74.89	
		1.93	83.79 - 83.80	= S.E. B.P. Rosemont + Electric = check

My Book Elev. of 75.27 Must be wrong

use 74.89

Cross Sec. Portion of
Alley Blk. 69-Ocean Beach

For payment of excavation.
W.O. 31392 12-18-51
C.H.S.

B.L. = ± original alley before opening of S'ly. + W'ly. additional 10'

T.P.	10.18	5 4.33	4.96	44.15
2+75				
2+35				
T.P.	11.28	49.11	5.83	37.83
2+15				
1+90				
0+00 = W'ly. line Bacon				
T.P.	11.96	43.66	1.14	31.70
	8.80	32.84	—	24.04

B.L.

50

39.3 39.4 46.0 46.6
9.8 9.7 3.1 2.5
15 6 10

38.0 38.8 41.6 43.4
11.0 10.3 7.5 5.7
8 12 13 20

49.11

37.4 37.6 40.7 42.6
6.3 6.1 3.0 1.1
10 12 14 20

36.1 36.7 37.4 37.4
7.6 7.0 6.3 6.3
10 17 19 25

43.66

N.W.B.R. Bacon & Del Monte

E & W. Alley Blk 69 · O. B.

T.P. 1.50 43.55 12.28 42.05

Alley to north - P. 52

4+00

3+75

3+60

3+35

2+95

B. L.

42.1 42.1 43.4 43.5

12.2 12.2 10.9 10.8

1 2 10

41.7 41.7 44.3 49.3 49.4

12.6 12.16 10.0 5.0 4.9

1 2 5 8

41.3 41.7 47.8 50.1 52.0

13.0 12.6 6.5 3.8 2.0

3 4 5 10

40.1 40.1 45.6 49.7 52.0 52.0

13.5 13.5 8.7 4.6 2.3 2.2

1 3 7 8 10

39.9 39.9 46.0 52.0 52.1

14.5 14.4 8.3 2.3 2.2

1 3 9 10

54.83

Alley to north Blk 69. O.B.
B.L. = ℄ original alley

1+70 = Sly line Del Monte

1+60

1+30

1+00

0+59

0+41 to 0+59 is now conc. drive

0+41

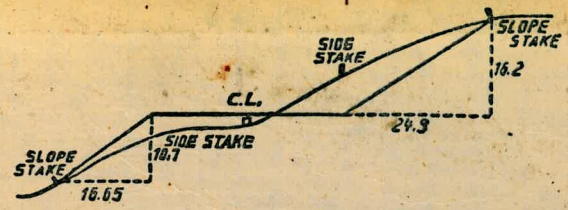
0+30

0+00 = Sly line E+W. Alley

B.L.

6.6.	37.0		37.0		
			6.6		
			10		
6.0	37.6	38.3	38.3		
		5.3	5.3		
		5	10		
4.8	37.5	39.6	40.0	40.6	42.0
		4.0	3.6	3.0	1.6
		2	8	10	13
3.7	39.9	41.2	41.6	42.4	43.6
		2.4	2.0	1.2	.00
		3	8	10	13
2.3	41.3	42.6	43.0		
		1.0	0.6		
		2	10		
1.7	41.9	43.1	43.5		
		0.5	0.1		
		3	10		
1.5	42.1	43.0	43.6		
		0.6	0.0		
		2	10		

43.55



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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