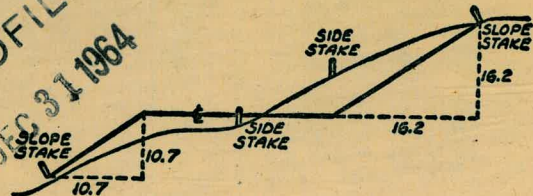


2077

TRANSIT BOOK

MICROFILMED  
 DEC 31 1964



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

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Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

## DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

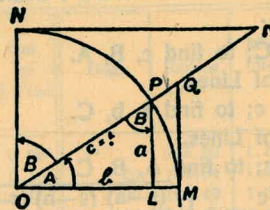


TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \neq$$

$$\text{covers } A = \frac{OP-LP}{OP} = OP-LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1-\cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1+\cos A}{2}}$$

$$\sin 2 A = 2 \sin A \cos A \quad \cos 2 A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2 ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2} (A+B)}{\tan \frac{1}{2} (A-B)}$$

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Page -

- 2-9 - X-Sept - Pac Hwy. + Ash.
- 10-21 - X-Sept - 49th + Ontario
- La Mesa Colony Sewers.
- 53 -
- 22-27 Reservoir Dr. to 67<sup>th</sup>
- 49-52
- 28 - Lots 36 + 37
- 22 + 33 " B + 32
- 22 + 35 Lot B - Easement 8/11/50
- 47 Locate gas line North of Saramac on 68th

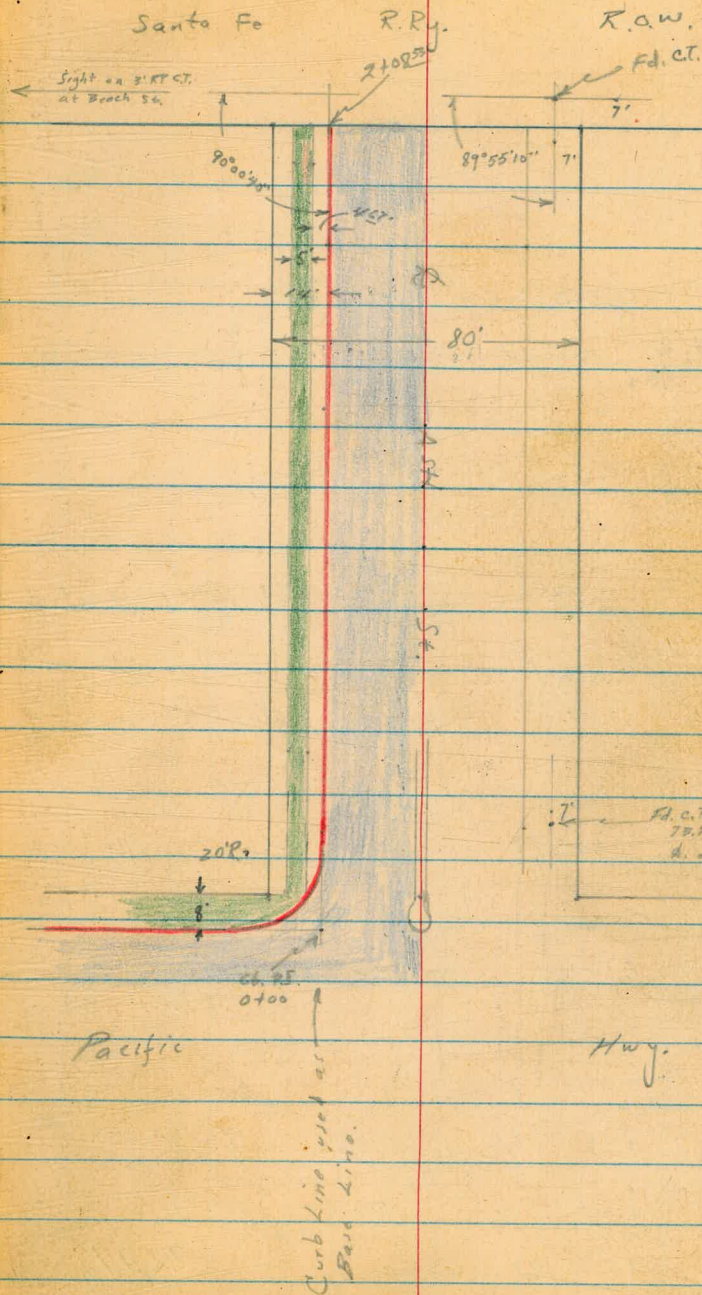
Roberts  
Garber  
Moore  
Clark  
342-50  
W.O. 20364.

Survey North Half Ash Street  
Pac. Hwy. to Santa Fe R.R. R.O.W.  
T.P. Sheet

INDEXED

MAR 28 1950  
W.K.

Reduced 3-3-50  
H. Remington



Cont'd From Page 2

Lt.

Rt

3

Base line

0+10

1.44	4.11	1.83
7.97	8.00	8.58
9.57	7.2	2.4
Edge walk	Brk	Gutter No Cb.

0+08<sup>2</sup>

{ 29' Lt to Canopy Pillar 145',  
20' wide  
14' Lt to Gas Station Island for Pumps

15' Lt to Station Light 27' Lt to Solid Conc. Island

0+08<sup>6</sup>

65' Lt to Street # Stop Sign

0+07<sup>5</sup>

Begin opening in curb for Drive  
7' Lt to Center Traffic Signal

4.31	3.65	3.79	3.79
8.10	8.76	8.62	8.12
4.2	4.2	0.4	
cb	Gutt	End conc Gutter	

0+02<sup>4</sup>

{ 26' Rt to Center Traffic Light  
17<sup>35</sup>' Lt. to Center Traffic Signal

0+02

34' Lt to Center Street Light

0+00

E. Curb Line Pac. Hwy.

3.93	4.37	3.61	3.62	3.69	3.76	3.77	4.34
8.48	8.04	8.20	8.79	8.72	8.65	8.64	8.07
7.0	2.0	2.0	7'		13	26	26
Gutt	cb	Gutt	conc Gutt			Gutt	cb

T.P.

5.73

12.41

8.44

8.68

12.41

T.P.

2.41

17.12

10.55

12.71

BM

2.29

25.26

22.97

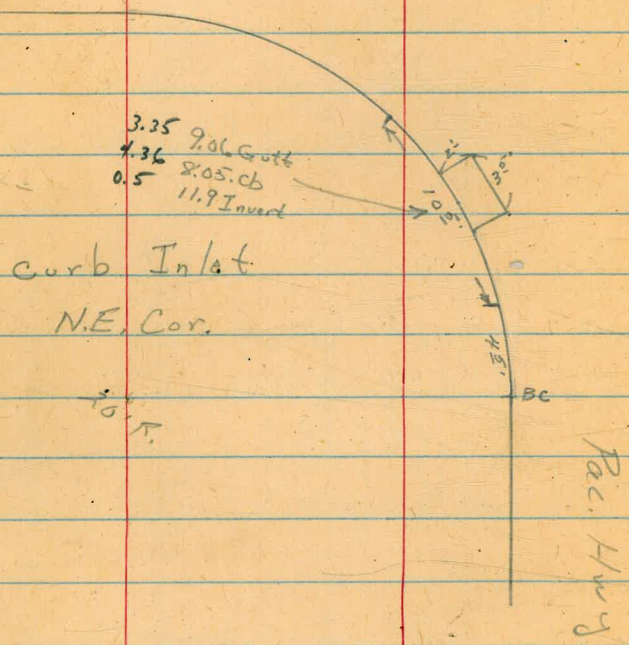
SWBP  
Ash & India

E. Cb. Int.  
Blank & offset

Contd From Page 3

4

Ash



12.41

Contd From Page 4

Lt

Base Line

Rt

5

0+56<sup>1</sup> 28<sup>5</sup> Lt End. Bldg.

0+53 17' Lt to Center T. Pole #505717H # JP880

0+48 Normal Curb

4.81 5.32  
7.60 7.09  
(Gut. cb)  
4.73  
7.68

0+46 End. Drive opening

0+44<sup>6</sup> 28<sup>6</sup> Lt. to Cor. Bldg

	5.16	5.37	4.59	5.15	5.25	5.73
0+40	7.25	7.04	7.82	7.26	7.16	6.68
	25	9.61		13	24.8	24.75
	Drive	Edge			Gut	cb
		walk				

0+29<sup>2</sup> 29<sup>8</sup> Lt. to Conc. Island 3 pumps

	4.93	4.48	4.10		4.77	5.25
0+23	7.48	7.53	8.31	7.25	7.64	7.16
	25	9.61		13	24.8	24.75
	Drive	Edge			Gut	cb
	AC.	walk				

0+20 EC of Curb

12.41

12.41



Cont'd From Page 5

Lt

Rt

6

0791

6.10  
6.31  
Gutt  
6.65  
5.76  
cb

0789

End Drive Opening

6.84  
5.57  
14  
walk  
6.88  
5.53  
921  
walk  
6.06  
6.35

0788

Begin solid walk to property.  
15<sup>s</sup> Lt station light

0787<sup>5</sup>

14' Lt Begin Board Fence

0780

6.05  
6.36  
25  
6.54  
5.87  
951  
walk  
5.77  
6.14  
6.25  
6.31  
6.16  
13  
6.10  
26

0764<sup>5</sup>

6.11  
6.30  
951  
walk  
5.27  
7.14

0762<sup>5</sup>

5.20  
7.21  
Gutt  
5.80  
6.61  
cb

0760<sup>3</sup>

End Center Island

5.57  
6.84  
25  
5.97  
6.44  
987  
walk  
5.10  
7.31  
Gutt  
5.74  
6.67  
cb  
5.62  
6.79  
13  
5.77  
6.64  
242  
Gutt  
6.24  
6.17  
253  
cb

12.41

12.41

Cont'd From Page 6

Lt

Rt

7

1742<sup>1/2</sup>

13<sup>1/2</sup> Lt Begin Bldg.

9.0	8.66	8.46	7.93	8.13	8.2 <sup>v</sup>
3.4	3.75	3.25	4.68	4.28	4.19
25	135	95 <sup>v</sup>		13	26
		walk			

1723

Drive Opening

7.1<sup>v</sup>  
5.29

1722

14<sup>1/2</sup> Lt End Conc. Ret. Wall

9.4	9.7 <sup>v</sup>	8.4	7.8 <sup>v</sup>	7.74	7.07	7.68	7.41	7.50
3.0	2.69	4.0	4.59	4.67	5.34	4.73	5.00	4.91
25	142	143	98	48 <sup>v</sup>	Gutt	CB	13	26
	Top	Grd	walk	walk				
	walk							

1710

15<sup>1/2</sup> Lt to Center T. Pole # 93779H

9.6 <sup>v</sup>	7.48	7.48	7.35	6.6 <sup>v</sup>	7.2 <sup>v</sup>
2.79	4.83	4.93	5.06	5.79	5.19
142	14	98	48	Gutt	CB
Top	walk	walk	walk		
walk					

1708

End solid walk CB to Property  
14<sup>1/2</sup> Lt End Fence Begin 8" Conc. Ret. Wall

1707<sup>1/2</sup>

16<sup>1/2</sup> Lt to Large Sign board

6.7 <sup>v</sup>	7.24	7.24	6.77	6.96	6.87	6.97
5.69	5.15	5.17	6.04	5.45	5.54	5.44
25	14	98	Gutt	CB	13	26
	walk	walk				

1700

12.41

12.41

T.P. 6.21 16.92 1.80 10.61

1780

1769<sup>3</sup>

135 to Bldg.  
End. Conc. Walk on Steps

1765

10° Lt to End conc. Steps

1757<sup>3</sup>

2' x 12' Motor box next to cb.

1756<sup>1</sup>

10° Lt Begin Conc. Patch & Steps

1752<sup>5</sup>

2° Lt. No Parking Sign

1749<sup>6</sup>

Normal cb.

1747

End Drive Opening

12.41

Lt

Base Line

Rt

8

9.7	9.61	9.64	8.93	9.56	9.27	9.43
2.7	2.20	2.71	3.48	2.85	3.14	2.98
135	967	961	Gutt	cb	13	2C
	walk	walk				

12.36	8.95
0°E	3.46
10°E	10°
Top	Bottom
Landing	Landing

7.93	8.64
4.48	3.77
Gutt	cb

7.90  
4.51

12.41

Cont'd From Page 8

Lt.

R2

9

check 2.62 22.78 = 22.97 Start. BU

T.P. 11.40 25.60 2.62 14.20

2710<sup>1</sup> 132' Lt to Drain Inlet

9.15

7.67

132'  
Invert

was 25' corr. Pipe Filled with  
conc. to within 0.8' of top.

2708<sup>33</sup> Santa Fe R.Ry. R.O.W.

10.69	10.67	10.62	10.59	10.35	10.31
6.13	6.15	6.20	6.23	6.47	6.51
132' End cb	92' walk	487 walk	cb & Gutt	13	26

2704<sup>2</sup> 16' Lt. to Center T. Pole # D5408T

1799 End Curb Outlet

10.4	10.27	10.26	9.26	10.21	9.95	10.02
6.4	6.55	6.56	7.56	6.61	6.87	6.80
132'	92' walk	482 walk	Gutt	cb	13	26

1496<sup>5</sup> 132' End Bldg. Begin Conc. Plat form

1491<sup>5</sup> Begin Curb ~~Inlet~~ or Outlet?

9.10	9.93
7.72	6.89
Gutt	cb

1682

16.82

Fd. stub

13

7+11.51

20' 20'

st.

AVBURN DRIVE

49+15

S.L. Fairhaven Acres

7' 13'

0+00

Fd. Mon.

st.

10+00.60

52° 53' 30"

Ontario Ave

0+90.18

25' 10' 25'

9+10.42 = 0+00 on Ontario

Ang. = 15° 07' 30"

Fd. Mon.

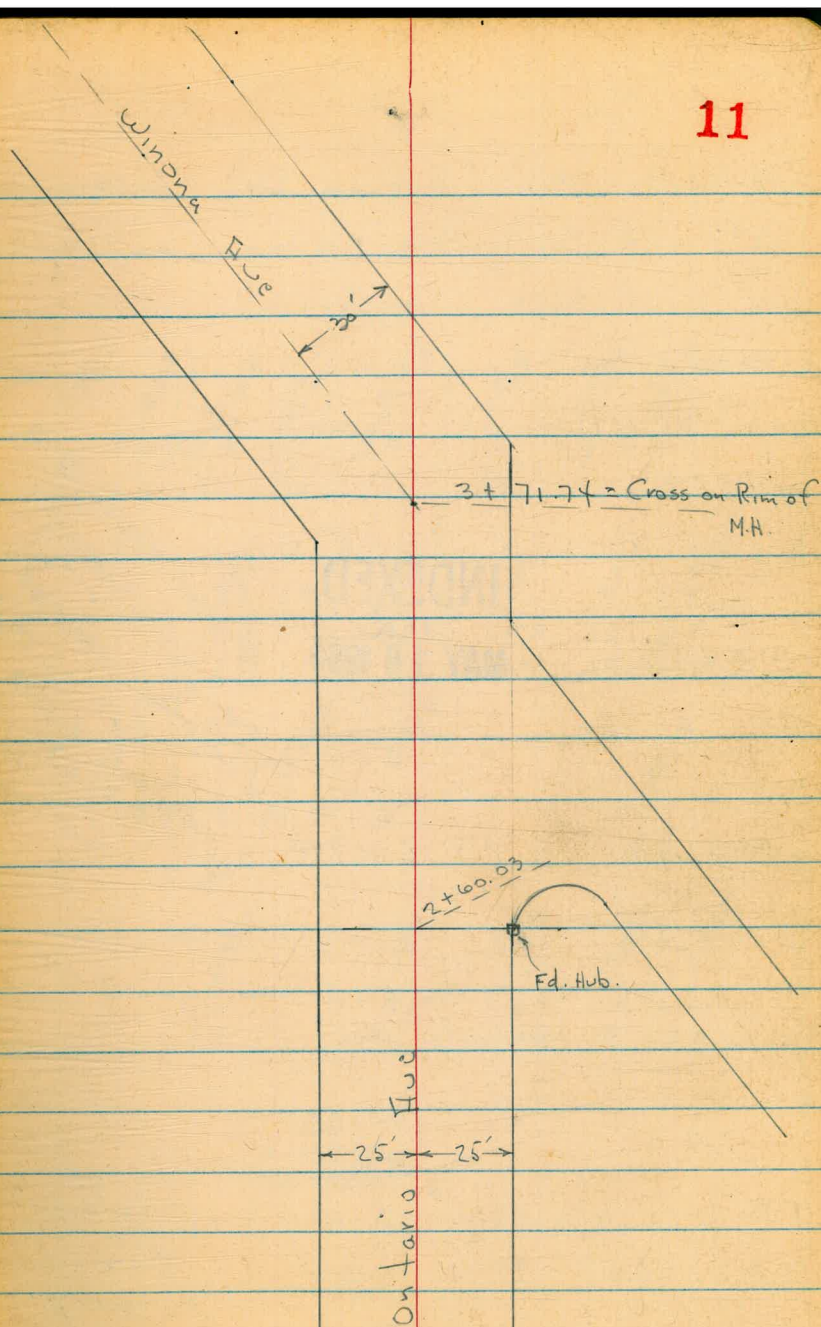
3' Deep  
Set Hub on top.

8+59.76

25' 25'

49+15

7+11.51



X-Section 49<sup>th</sup> (Huburn Dr) from  
S.L. of Fairhaven Acres to  
200' N. of Pave. - See sketch

± Ontario - 49<sup>th</sup> to Winona Ave.

Begin X-Sections of Ontario

1+00

Party?  
Date?

**INDEXED**  
M.K.  
**MAY 16 1950**

0+50

Reduced May 16, 1950  
John Firebaugh  
Elevations come off  
of st. on PC. - 5.00  
Wightman & 49<sup>th</sup>  
El. 311.63

0+21.62

P.I. CURVE

0+00

± Ontario Mon

T.P. +10.73

~~261.08~~  
~~261.20~~ - 5.44

~~250.35~~  
~~250.47~~

T.P. +6.68

~~255.79~~  
~~255.91~~ - 0.66

~~249.11~~  
~~249.23~~

+10.19

~~249.77~~  
~~249.89~~

Disregard 2  
~~239.58~~ - 239.70

Note: See check to other B.M. on P. 21 - Before

252 <sup>L</sup>	249 <sup>S</sup>	256 <sup>2</sup>	252 <sup>L</sup>	252 <sup>2</sup>	251 <sup>3</sup>	253 <sup>2</sup>	256 <sup>7</sup>
9.0 65 Top	11.6 95 ± Work	4.9 25	9.0 18 Top	8.9	9.8 25	7.9 50	4.4 80

251 <sup>L</sup>	251 <sup>5</sup>	251 <sup>3</sup>	251 <sup>L</sup>	251 <sup>3</sup>	252 <sup>9</sup>
10.0 35	9.6 25	9.6 ..	10.0 25	9.8 50	8.2 65 Top of slope

251 <sup>5</sup>	251 <sup>3</sup>	250 <sup>A</sup>	251 <sup>2</sup>	251 <sup>A</sup>
9.6 25	9.3 16	10.7 9	10.1	9.7 25

251 <sup>2</sup>	251 <sup>7</sup>	251 <sup>6</sup>	249 <sup>2</sup>	250 <sup>3</sup>
9.4 25	9.4	9.5 10	11.4 17	10.8 25

~~261.08~~  
~~261.20~~

Nail in pole - 7+35 - Lt

B.M. nails in pole 2+38 15' Lt  
Reducing Book 1561 - P. 46

T.P. 10.04 266.80 256.76  
266.92 432 256.88

3+00

2+60.03 = P.C. Prop. on Rt.

2+30

2+00

1+80

1+50

Lt. £ Rt.  
266.80

254<sup>0</sup> 250<sup>3</sup> 254<sup>0</sup> 255<sup>1</sup> 256<sup>1</sup> 259<sup>0</sup> ~~261<sup>2</sup>~~  
 7.1 106 7.1 6.0 5.0 2.1 + 0.9  
 60 50 46 25 25 25 50  
 Wash

253<sup>1</sup> 249<sup>6</sup> 253<sup>1</sup> 253<sup>3</sup> 256<sup>0</sup> 258<sup>5</sup>  
 8.0 11.5 8.0 8.0 7.8 5.1 2.6  
 5.5 46 40 25 25 25 50  
 Wash

252<sup>9</sup> 249<sup>6</sup> 252<sup>9</sup> 253<sup>2</sup> 252<sup>1</sup> 254<sup>2</sup> 257<sup>8</sup>  
 8.2 11.7 8.2 7.9 8.4 6.8 3.3  
 50 41 36 25 25 25 50  
 Wash

253<sup>2</sup> 248<sup>9</sup> 252<sup>6</sup> 252<sup>9</sup> 252<sup>1</sup> 252<sup>9</sup> 256<sup>3</sup>  
 7.8 12.2 8.5 8.2 9.0 8.2 4.3  
 47 37 28 25 25 25 50  
 Wash

253<sup>2</sup> 248<sup>9</sup> 251<sup>9</sup> 253<sup>3</sup> 252<sup>1</sup> 252<sup>2</sup> 253<sup>1</sup>  
 7.6 12.2 9.2 7.8 9.0 8.9 8.0  
 40 32 25 20 11 25 25  
 Wash

252<sup>5</sup> 249<sup>0</sup> 252<sup>9</sup> 255<sup>0</sup> 252<sup>2</sup> 251<sup>9</sup> 252<sup>6</sup> 255<sup>4</sup> 258<sup>2</sup>  
 8.6 12.1 9.1 6.1 8.9 9.2 8.5 5.7 2.3  
 43 32 25 20 13 25 25 50 70  
 Wash

261.20  
261.08



3 + 71.74 = end.

3 + 40

255 <sup>2</sup>	252 <sup>2</sup>	256 <sup>2</sup>	260 <sup>2</sup>	262 <sup>2</sup>	265 <sup>2</sup>	269 <sup>2</sup>
11.6	14.8	10.6	6.1	4.7	0.9	+2.6
88	73	63	25		25	50
wash						
255 <sup>2</sup>	251 <sup>2</sup>	255 <sup>2</sup>	259 <sup>2</sup>	259 <sup>2</sup>	264 <sup>2</sup>	266 <sup>2</sup>
10.9	14.9	10.9	7.4	7.3	2.4	0.0
66	58	50	25	7.3	25	50
wash						
					266.80	

Req. X-Sect. of 49<sup>th</sup> - from S.L. Fairhaven  
to 200 N. of Pauc. - Sketch - p. 10

T.P. 6.87 ~~246.57~~ <sup>246.45</sup> 386 ~~239.70~~ <sup>239.58</sup>

2+00

INDEXED  
MAY 16 1950

1+50

1+00

0+50

show both sides of graded Road.

0+00 -  $\pm$  S.L. Fairhaven Acres. - Sect along S.L.

B.M. 3.86 ~~243.56~~ <sup>243.44</sup> 239.58 ~~239.70~~ = Nails in Pole.

4.

#

Rt.

15

246.45

2399 4.5  
30  
2383 5.1  
20  
2359 7.5  
13  
2357 7.7  
7  
 $\pm$ wash  
2367 6.7  
2397 3.7  
5  
2396 3.8  
20  
Rd.  
2382 5.2  
30

2387 4.7  
30  
2365 6.9  
20  
2352 8.2  
5  
 $\pm$ wash  
2356 7.8  
2396 4.8  
7  
2386 4.8  
20  
Rd.  
2386 4.8  
25

2379 5.5  
30  
2368 6.6  
20  
2350 8.4  
 $\pm$ wash  
2355 7.9  
11  
2380 5.4  
15  
Rd.  
2381 5.3  
30

2390 4.4  
30  
2385 4.9  
20  
2353 8.1  
11  
 $\pm$ wash  
2344 9.0  
20  
2352 8.1  
20  
2371 6.3  
25  
Road  
2369 6.5  
40

2389 4.5  
30  
2380 5.4  
20  
2369 6.5  
20  
2359 7.5  
20  
2349 8.6  
30

243.44

~~243.56~~

4+50

4+41 - 15' Lt. = ± 3.5 Conc. walk

4+15 - 41' Lt. = ± House

4+00

3+50

3+12 - 3.3' Lt. = ± Sewer M.H.

3+00 - = end Rubble wall

Wash goes to W.

2+90 = ± 8' Wood Bridge (single span)

2+50

2+14 - 282' Rt. = ± House

2+16 - 2' Rt. = Beg. Rubble wall

243.50

2.95  
41  
floor.

2419

4.6  
41  
ground.

2421

4.4  
30

2422 Lt

4.2  
30

242.59

3.88  
50  
walk

2436

2.9  
20

242279

4.18  
20

24226 Rd

4.19  
15.7 = walk

2435

3.0  
14

2434

3.1  
20

2434 Rt

3.1  
20

2442 16

2.3  
30

240.89

5.56

enlim

2404

6.1  
35

2373

9.2  
26

2373

9.2  
20

2373

9.2  
15  
± wash

2371

9.4  
9

240.54

5.91  
Top wall

2409

5.6  
3

2411

5.4  
18

2403

6.2  
20

2399

6.6  
30

2408

5.7  
50  
Dirt Dr.

241.20

5.25  
19  
w. end.

240.59

5.86

240.63

5.82  
2 end

2401

6.4  
30

2402

6.5  
20

2371

9.4  
12

2361

10.4  
7  
± wash

2375

9.0  
1

2377

8.8  
1  
Top wall

23999

6.46  
1  
Rd

2404

6.1  
20

2392

7.2  
30

2391

7.1  
282  
ground.

240.15

6.30  
282  
floor.

246.45

246.57

9.3  
2  
ground

6.79  
2  
Top

49<sup>th</sup>

7+31- 16' Lt. - Beg. 6" Rock + Conc. wall

7+00

6+94- 477 Lt. - House

6+50

6+14- Sewer Mt.

6+00

5+82- 20.7 Lt. - 2' Conc. walk

5+50

5+30- 20' Lt. - 3' Conc. walk

T.P.

5+00

249.36

Lt.

±

Rt.

17

5.42  
16  
Top  
wall

247<sup>6</sup>

248<sup>3</sup>

249<sup>2</sup>

249<sup>4</sup>

249<sup>5</sup>

249<sup>6</sup>

249<sup>5</sup>

7.2  
30

6.5  
20

5.6  
10

5.4  
Rd.

5.0  
11

5.2  
20

5.3  
30

248.57  
6.21  
floor

247<sup>1</sup>

77  
47.7  
ground

247<sup>1</sup>

247<sup>2</sup>

248<sup>5</sup>

248<sup>2</sup>

249<sup>1</sup>

249<sup>3</sup>

250<sup>9</sup>

7.7  
30

7.0  
20

6.3  
11

6.0  
Rd.

5.7  
10

5.5  
20

5.9  
30

248.10  
6.68  
on Rim

246<sup>1</sup>

246<sup>9</sup>

247<sup>6</sup>

247<sup>2</sup>

248<sup>2</sup>

248<sup>6</sup>

249<sup>4</sup>

8.7  
30

7.9  
20

7.2  
11

7.0  
Rd.

6.8  
9

6.2  
20

5.4  
30

245.66  
9.12  
38  
at  
porch

245.85  
8.93  
20.7  
walk

245<sup>2</sup>

245<sup>2</sup>

246<sup>2</sup>

246<sup>5</sup>

246<sup>6</sup>

246<sup>5</sup>

247<sup>3</sup>

9.6  
30

8.9  
20

8.6  
12

8.3  
Rd.

8.2  
11

8.3  
20

7.5  
30

244.02

244.49

10.76  
50

10.31  
20

walk

254.78

~~254.90~~

243<sup>3</sup>

243<sup>5</sup>

244<sup>8</sup>

245<sup>2</sup>

245<sup>3</sup>

245<sup>2</sup>

245<sup>6</sup>

3.2  
30

3.0  
20

1.7  
11

1.5  
Rd.

246.45

1.7  
11

1.3  
20

0.9  
30

~~246.57~~

49th

9+45

9+10.42 = 0+00 to E. (Ontario) - Sect. at 90°

8+59.76 = Ang. 15° 07' 30" Lt - Sect. 90° to back

8+30

7+P

7.61

257.94

~~258.06~~

4.45

250.33

~~250.45~~

Nail

in Pole

250.47 - P 12

257.94

~~258.06~~

8+00

7+70 = 18' Lt. - end wall

7+50

7+41 = 15.1' Lt. = 3.5' Conc. walk + step Thru wall

2490

6.8  
30

6.88  
45.9  
at porch

6.13  
16.2  
walk

5.32  
15.1  
top step

254.78

~~254.90~~

2486

6.2  
30

6.4  
20

6.0  
17

5.09  
16.5  
wall

2495

5.3  
20

5.09  
16.5  
wall

2503

4.5  
15

5.0  
12

2506

4.2  
Rd

4.9  
9

2507

4.1  
6

4.6  
7

2514

3.4  
20

5.1  
13

2525

3.3  
30

5.2  
20

2519

3.8  
30

3.9  
30

2495

8.4  
115

2461

11.8  
100  
wash

2516

6.3  
82

2509 Lt.

7.2  
35

2521

5.8  
25

2513

6.6  
14

2513

6.6  
Rd. - 9

2514

6.5  
9

2515 Rt.

6.4  
25

2516

6.3  
50

2458

12.1  
129  
wash

2487

9.2  
40

2492

8.7  
50

2502

7.7  
25

2514

6.5  
18

2516

6.3  
Rd - 6

2516

6.3  
25

2519

6.2  
25

2509

7.0  
50

2487

9.2  
40

2491

8.8  
30

2501

7.2  
23

2508

7.1  
Rd.

2506

7.3  
5

2506

7.3  
25

2501

7.8  
25

2519

6.0  
35

2495

8.4  
35

2496

8.3  
25

2505

7.4  
19

2506

7.3  
Rd.

2507

7.2  
3

2515

6.4  
25

2522

5.7  
35

49+2

10+12.7 - 14.7 Lt. = Beg. cb.

10+13.5 - 15.4 Rt. = Beg. cb. on Rt.

10+14 - 25 Lt. = ± 30" Euc. Tree

10+06 Lt. = end Ely. of Bridge

+ ± wash

10+00.60 P.C. on Rt. - Beg. Cold Lay Pave

10+00 - Brk in Deck

9+90

9+79 - Brk. in Deck of Bridge

9+76 - 16.5 Lt. = ± P. pole # P 3640

9+74 - 18 Lt. = Beg. Ely. of 3' Wood Footbridge

Lt.

Rt.

255.5  
251.8  
254.4  
253.9  
252.80  
249.40  
251.42  
250.69  
249.11  
249.09  
249.73  
250.319  
249.6

6.52 7.25  
1.47 1.7  
Top. 9.7

8.21 7.63  
15.4 15.4  
Top. Top.

2.4 6.1 3.5 4.0 5.14 8.54 8.83 8.85 9.0 8.8 8.3  
100 38 30 25 18 14 Rd. CL 8 25 35 50

Top Bridge  
± wash

251.6 252.9 250.0 248.8 248.4 248.6 248.5 249.3  
6.3 5.0 7.9 9.1 9.5 9.3 9.4 8.4  
40 27 23 15 Rd. 9 25 50

253.58  
4.36  
Top

254.5  
3.4  
100

250.9 250.8 248.0 248.2 248.5 248.5 248.8 249.4 254.3 255.9  
7.0 7.1 9.9 9.7 9.4 9.4 9.1 8.5 3.2 2.0  
75 42 35 25 14 Rd. 9 7 25 50

± wash  
Top of Deck  
Top - fill from wash

249.9 246.9 248.1 252.0 253.1 252.83 249.1 249.4 249.9 251.2 251.9  
8.0 11.0 9.5 5.9 4.8 5.11 8.8 8.5 8.0 6.7 6.0  
70 63 50 35 25 18 14 Rd. 9 25 50

± wash  
Bridge Top.

257.94  
~~258.05~~

11+92

2630	262.41	261.62	262.27	260.73	261.28	261.4
5.3	5.92	6.71	6.06	7.60	7.05	6.9
25		14.9		15.2		25
	Top	9.4		9.4	Top	

11+78

2612	260.62	259.89	260.70	259.78	259.78	259.4
7.1	7.71	8.44	7.63	9.05	8.55	8.9
25		14.8		15.2		25
	Top	9.4		9.4	Top	

11+40

2582	258.27	257.66	257.95	256.81	257.33	257.0
9.6	10.06	10.67	10.38	11.52	11.00	11.3
25		14.7		15.2		25
	Top	9.4		9.4	Top	

11+05

2571	256.34	255.76	255.95	254.84	255.38	255.2
11.2	11.99	12.57	12.38	13.49	12.95	13.1
25		14.7		15.4		25
	Top	9.4		9.4	Top	

T.P.

12.33

268.33

~~268.45~~

1.94

256.00

~~256.12~~

10+65

2549	254.15	253.44	253.69	252.61	253.11	253.4
3.0	3.79	4.50	4.25	5.33	4.83	4.5
25		14.6		15.4		25
	Top	9.4		9.4	Top	

10+30 - wire fence behind cb.

2529	252.18	251.53	251.52	250.79	251.24	251.5
5.0	5.79	6.41	6.42	7.15	6.70	6.4
25		14.6		15.4		25
	Top	9.4		9.4	Top	

check B.M.

	312.37	0.74	<del>311.75</del> = 311.63
12.96	<del>312.49</del>	0.14	<del>299.41</del>
	299.55		<del>299.53</del>
13.18	<del>299.67</del>	0.03	<del>286.37</del>
	286.40		<del>286.49</del>
13.24	<del>286.52</del>	0.34	<del>273.16</del>
	273.50		<del>273.28</del>
T.P.	13.37	8.20	<del>260.25</del>
	<del>273.62</del>		260.13

311.63 = c.t. on PC. - S. cb. Wightman + Auburn Dr.

12 + 80

267.92	267.28	267.20	266.41	266.97
0.41	1.05	1.13	1.92	1.36
Top	14.9	268.33	15.1	Top
	904	<del>268.33</del>	904	



La Mesa Colony Sewers  
Reservoir Dr. to 67th St.

Sammermeyer

B099  
Aouña

7-7-50

INDEXED  
MK  
JUL 12 1950

FB 2040-36

1762-38

1376

1665-25

T.P. 29

□ = fd hub

■ = set hub

Blue line = Final location

Reservoir Drive line



67th

7+06.12

22

Saravac.

+ 67th

7 06.12  
5 52.71  
1 53.81

8-11-50

2+17.36

Δ 24°-17' Lt

Easement to  
serve Lot # B

5+52.71  
Δ 52°-10' Rt

See P. 53

10-26-50

line change  
see p 44

levels - P. 22

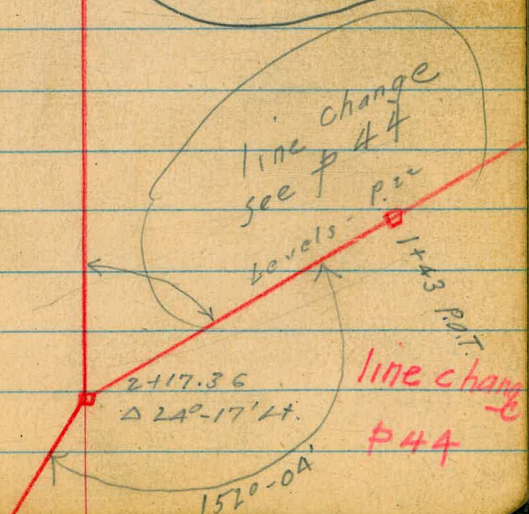
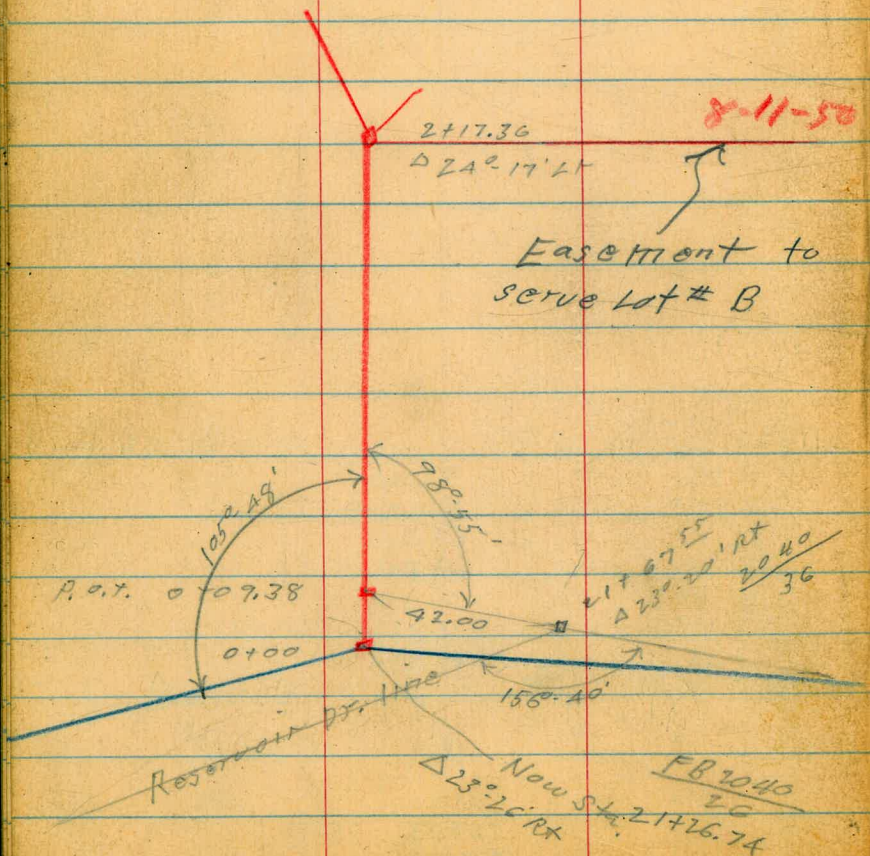
1+43 POT

2+17.36

Δ 24°-17' Lt

line change  
P 44

152°-04'



Reservoir Dr. to 67<sup>th</sup>

7-7-50

23

1+00

388.2  
15.7  
12  
w

390.9  
13.0

393.0  
10.9  
10

403.92

T.P. 11.34 403.92 0.34 392.58

+50

384.5  
8.4  
12  
w

386.3  
6.6

387.5  
5.4  
10

+25

382.9

10.0  
w

w. = wash

0+17

381.6

11.3  
w

0+09<sup>38</sup> = p.o.t. + Tic

382.0

10.9  
10

383.0

9.9

383.3

9.6  
10

0+00=

383.22

9.70  
Hub

B.M. = 21+67.55

2040  
39

9.06 392.92 - 383.86

392.92

2+90

$$\begin{array}{r} 408.6 \\ 5.6 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 406.0 \\ 8.2 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 402.6 \\ 11.6 \\ \hline 17 \\ \hline w \end{array}$$

2+50

$$\begin{array}{r} 405.4 \\ 8.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 400.7 \\ 13.5 \\ \hline 13 \\ \hline w \end{array}$$

$$\begin{array}{r} 400.2 \\ 14.0 \\ \hline 13 \\ \hline w \end{array}$$

2+30

$$\begin{array}{r} 401.2 \\ 13.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 398.7 \\ 15.5 \\ \hline w \end{array}$$

$$\begin{array}{r} 400.2 \\ 14.0 \\ \hline 10 \end{array}$$
T.P. 11.90 414.19 1.63 402.29

E.L. 1/2 = 398.33

2+17<sup>36</sup> Δ 2A° - 17' Lt. (Sec. on split of Δ)

414.19

see p 45

$$\begin{array}{r} 397.3 \\ 6.6 \\ \hline 7 \\ \hline w \end{array}$$

$$\begin{array}{r} 398.33 \\ 5.59 \\ \hline \text{Hub.} \end{array}$$

$$\begin{array}{r} 399.7 \\ 4.2 \\ \hline 10 \end{array}$$

2+00

$$\begin{array}{r} 396.2 \\ 7.7 \\ \hline 5 \\ \hline w \end{array}$$

$$\begin{array}{r} 397.1 \\ 6.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 399.4 \\ 4.5 \\ \hline 10 \end{array}$$

1+50

$$\begin{array}{r} 394.0 \\ 9.9 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 393.2 \\ 10.7 \\ \hline w \end{array}$$

$$\begin{array}{r} 395.7 \\ 8.2 \\ \hline 10 \end{array}$$

1+28

$$\begin{array}{r} 389.9 \\ 14.0 \\ \hline w \end{array}$$

$$\begin{array}{r} 396.6 \\ 7.3 \\ \hline 10 \end{array}$$
403.72

4+80 cross wire fence

T.P. 12.64 436.42 1.45 423.78

4+28

4+00 cross wire fence

3+80

T.P. 12.53 425.23 1.49 412.70

3+56

3+15

$$\begin{array}{r} 426.4 \\ 10.0 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 426.2 \\ 10.2 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 426.6 \\ 9.8 \\ \hline 10 \\ \hline \end{array}$$

436.42

$$\begin{array}{r} 423.23 \\ 2.0 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 421.9 \\ 3.3 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 422.9 \\ 2.3 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 415.2 \\ 10.0 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 418.7 \\ 6.5 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 420.03 \\ 5.2 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 412.8 \\ 12.4 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 415.4 \\ 7.8 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 419.7 \\ 5.5 \\ \hline 10 \\ \hline \end{array}$$

425.23

$$\begin{array}{r} 410.2 \\ 4.0 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 413.5 \\ 0.7 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 415.8 \\ 4.6 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 409.2 \\ 5.0 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 406.0 \\ 8.2 \\ \hline 10 \\ \hline \end{array}$$

$$\begin{array}{r} 408.5 \\ 5.7 \\ \hline 10 \\ \hline \end{array}$$

414.19

6+75 - 97' Rt. = N.E. Cor. House

6+63

T.P. 6.39 450.50 0.95 444.11

6+50 5' Rt. = ctr. 18" diam. eucalyptus

6+49 cross wire fence.

6+35 - 75' I Rt. = N.E. Cor. House

6+20

T.P. 11.98 445.06 3.34 433.08

5+80

5+52 <sup>71</sup> A 52°-10' Rt. (sec. on split of A)

5+00

75

447.5  
3.0  
97  
2nd Floor

447.7  
2.8  
97  
Floor

26

445.3  
 $\frac{5.2}{10}$

445.1  
5.4

443.8  
 $\frac{6.7}{10}$

~~3.7~~  
~~10~~

~~3.2~~  
~~10~~

450.50

439.1  
 $\frac{6.0}{10}$

438.7  
6.4  
5

438.9  
6.2

441.1  
 $\frac{4.0}{10}$

446.3  
+1.2  
75  
2nd.

446.8  
+1.7  
75  
Floor

437.1  
8.0  
 $\frac{10}{10}$   
W

437.3  
7.8

438.8  
6.3  
 $\frac{10}{10}$

445.96

433.9  
2.5  
 $\frac{12}{12}$

434.3  
2.1

435.8  
0.6  
 $\frac{10}{10}$

433.8  
 $\frac{1.6}{10}$

433.07  
 $\frac{3.35}{10}$

432.5  
3.9  
 $\frac{10}{10}$

429.1  
 $\frac{2.3}{10}$

428.4  
8.0  
 $\frac{2}{2}$

427.8  
8.6  
 $\frac{10}{10}$

428.4  
8.0  
 $\frac{2}{2}$

429.5  
6.9  
 $\frac{10}{10}$

436.42

7+06<sup>12</sup> =

4.65 445.85

Note.

This box can be gone under  
 without trouble because cut  
 will have to be at least 10' deep.  
 Using this line will save 1 M.H.

6+93 = ctr. 2'x2' gas. line box

6+79 start oil pave. on 67<sup>th</sup>
 445.85  
 4.65  
 Hub.

used as BM to  
 extend line  
 southerly on 67<sup>th</sup>  
 see p 39 & 40

 446.16  
 4.34

445.8

4.7

450.50

La Mesa Colony Sewer

Lots 36+37

7-10-50

Sammermyer

Bunch  
Shepard

FB 1762

38

T.P. 29

27

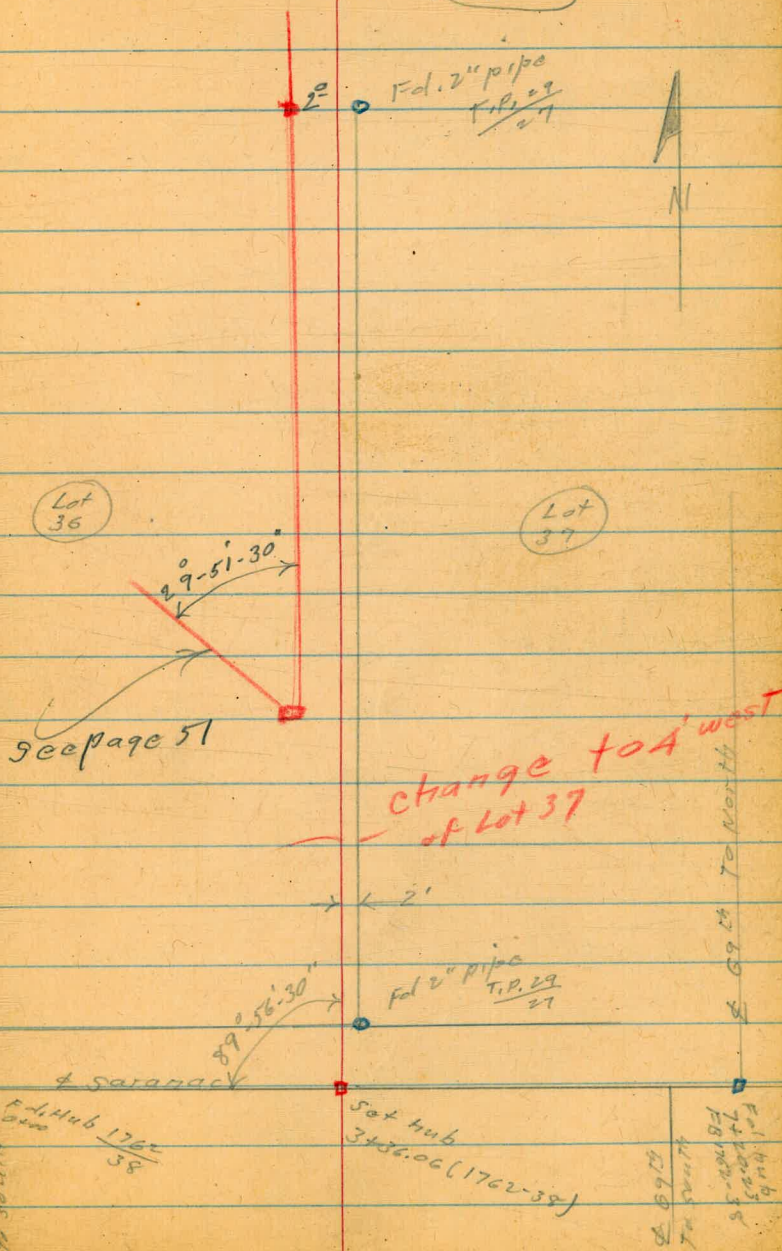
INDEXED

AUG 21 1950

Set hub at 2+18.5 t 9-19-50  
4' west of west line lot #37

sketch  
Cont. - P. 49 & 9/19/50

28



Lots 36 + 37  
La Mesa Colony

4.76 446.17 11.43 441.41

1750

Wire fence 2' rt. of #  
1745: End picket fence + start barb.

1700

H = Ground 15 higher

W = low spot in N.W. qly. - S. Ely. wash

0769 - 2' rt. = start picket fence.

0750

0741 - 18" pepper on #  
2' rt. of 0730  
2' pipe

5.44 447.40 B.M. #1

0730

0700 = # Saranac.

447.67

T.P.

5.87 452.84 0.96 446.95

T.P.

0.86 447.91 6.60 447.05

7.80 453.65 - 445.85

B.M. = # Saranac + 67 1/2

1/2 = 0700 1762  
25

H

10.5

8.8

7.7

7.0

6.1

H

5.17

Hub

452.84

442.3

444.0

445.1

445.8

446.7

447.67

441.6

444.1

8.7  
3.0  
at house  
w

449.8

7.0  
8.5  
at house

11.2  
4.0  
w

29



T.P. 8.10 451.96 2.31 - 443.86

N.W. by S. Ely.

5+00 Here wash runs into a canyon.

4+00

also start woven wire fence

3+78 - 2' RR. = end barb wire fence.

3+50

3+00

2+50

2+30

2+00

444.2 ✓  
22.0  
150  
W

436.8  
7.4  
115

443.2  
3.0 H

432.5  
13.7  
103  
W

437.5  
8.7  
76

442.6  
3.6 H

442  
4.2 H

8.4  
45  
W

441.0  
5.2 H

6.9  
15  
W

440.0  
6.2 H

H

440.0  
6.2 H

H

440.8  
5.4  
5.6  
10  
W

446.17 ✓

10+00

10+20

T.P. 6.22 456.03 2.15 449.81

9+62 2' Rt. = 2' pipe (N.Y. line Lot 36)

Set B.M. Top of pipe 2.15 449.81 B.M. #1

9+00

8+00

7+00

+50

6+07 - 2' Rt. = end woven wire fence.  
also: start barb wire fence.

6+00

449.1

6.9  
456.03

438.3 440.0 448.9 449.8

$\frac{13.7}{200}$   $\frac{8.0}{100}$  3.1  $\frac{2.15}{2}$  H

Top of pipe

436.3 444.2 448.4

$\frac{15.7}{200}$   $\frac{7.8}{100}$  3.6 H

438.2 441.8 447.6

4.4 H

446.2

$\frac{13.8}{150}$   $\frac{12.2}{100}$  5.8 H

445.4

6.6

444.6

7.4 H

451.96

orig B.M. P.29		6.98	445.85	✓
T.P.	9.58	452.83	9.36	443.25 ✓
check over		4.92	447.69	(447.67)
T.P.	3.64	452.61	11.26	448.97 ✓
T.P.	0.74	460.23	1.79	459.49 ✓
T.P.	0.36	461.28	1.88	460.92 (461.00)
T.P.	8.82	462.80	2.05	453.98

= 0+00 page 29

0+00 -  $\frac{1762}{49}$  -  $\frac{1}{2}$  69<sup>th</sup> + Saranac  $\frac{1}{2}$

N.W. Cor. conc. Porch - House s.E. Cor. Mandalay + 69<sup>th</sup>

13+00

12+50

12+00

11+00

442.9  
 13.1  
 200  
 445.6  
 7.9  
 10.4  
 100  
 448.1  
 449.7  
 6.3  
 450.3  
 5.7  
 H

456.03

Lots B x 32 La Mesa Colony

sketch Page 22

7-11-50

33

T.P. 8.96 427.07 0.94 418.11

1+29 7' 4" = ± of 2-10" iron pipes  
side by side for culvert.

428.3  
6.22  
7.2  
I.E. East  
pipe  
413.00  
6.05  
6.4  
I.E. west  
pipe

1+20 start fill on ±

409.7  
7.4  
1.7  
W  
413.9  
5.2  
H  
419.05

T.P. 10.44 419.05 0.97 408.61

404.6  
4.8  
2.5  
W  
407.6  
1.8  
1.2  
H  
409.4  
0.0  
H

0+80

INDEXED  
WPK  
AUG 21 1950

401.5  
7.9  
2.2  
W  
406.9  
2.5  
H

0+50

0+33 cross E. + W. wire fence.

399.4  
10.0  
1.7  
W  
401.2  
8.2  
H

0+25

H = Gnd higher than ±  
W = bottom of wash

0+00

397.1  
12.3  
7  
W  
398.33  
11.05  
409.38

11.05 409.38 — 398.33

B.M. = 2+17.36 (2x2)  
Page 24

3.44

(445.85 P.27)

~~3.46~~ 445.81

11.27 449.25 0.66 437.98

T.P. 11.75 438.64 0.18 426.89

property  
due south to serve additional  
This line can be angled aprox

1+80

H

7.9

7.5

7  
W

419.2

419.6

pipes - laid side by side

1+72

5' RT. = 1/2 of 2

Conc. Culvert

H

9.9

12.38

12.48

44

I.E. East  
Pipe

58

I.E. West  
Pipe

417.2

414.7

414.6

423.1

422.9

422.8

1+57 = leave private road

4.0

4.2

4.3

5

5

1+43 = 1/2 P.O.T.

4.54 422.53

422.7

422.6

422.7

1+41 = start E. &amp; W. Private road

4.4

4.5

4.4

5

5

427.07

Easement to serve  
Portion of Lot "B" La Mesa Colony

35

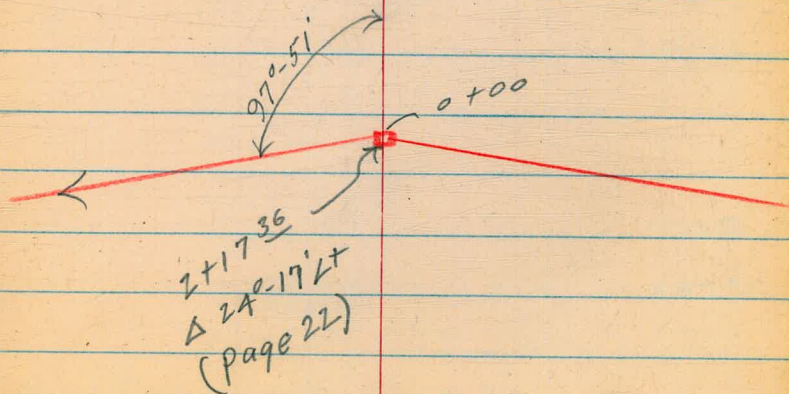
Sommermeier

8-11-50

Boggs

Allen

INDEXED  
MK  
AUG 21 1950



Part Lot "B"  
Levels

T.P. 12.87 428.04 0.13 415.17

428.04

0+55

0.0 415.3

0+30

8.4 406.2

0+22<sup>5</sup> cross fence line

403.4

0+20

11.9

T.P. 11.91 415.30 0.04 403.39

415.30

0+06

4.6 398.3

0+00

5.1 398.3

0+00

403.43

5.10 403.43 - 398.33

B.M. =  $\frac{1}{2}\Delta$  2+17<sup>36</sup> (P22 + 2A)

See p 45 - time change

check 1743 - P.O.T.

Page 34

5.47 422.57 (422.53)

1732 34<sup>1</sup> Lt. = N.W. cor. house

0+92

0+88

427.1	426.2	426.2
0.9	1.8	1.8
342	34	
Floor	Ord	
level		

425.0  
3.0

423.2  
4.8

428.04



Location of 24" water line

by Finder

8/15/50

Begg  
Allan  
Sisson  
Pope

7+21.10 did not find

15 17

14 6+0

13 5+00

14 4+00

15 3+00

69

16 2+00

17 1+00

19 Fd Pipe

0+00

33 Fd Hub

39.91

15

15-2



SARANDOC

6957 to South

Water Co -  
information

La Mesa Colony  
Sewer.

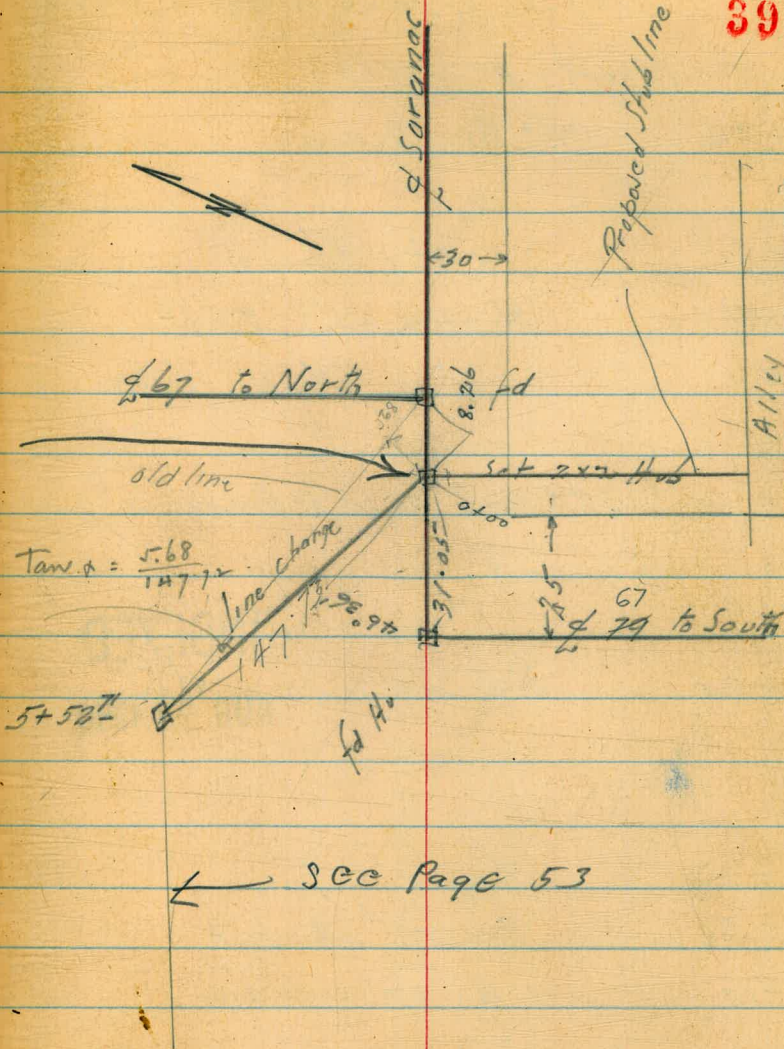
Line change

See p 22

8/17/50

Begg  
Johnson  
Allan  
Hatch

See P 53

$$\begin{array}{r} 153 \phantom{00} \\ 5 \phantom{00} \\ \hline 147 \phantom{00} \\ \phantom{147} 41 \\ \phantom{147} 68 \\ \hline \phantom{147} 73 \end{array}$$


by St. from Saranac to South  
in private property.

to Alley line + or -

40

0 + 84 14° Rt Acacia

0 + 61 14 Rt Acacia

0 + 51 BC conc walk 25 ft

0 + 46 130 ft NW cor House

0 + 40 35 R bush 14 Rt Acacia

0 + 30 Prop Line

INDEXED  
W.K.  
AUG 21 1950

0 + 22 Pepper on g

0 + 20 Hydrant 4' left

0 + 17 1' R 12" corr pipe

0 + 00

H.1  
6.10 451.95

445.85 BM.  
on hub P.27

447.1

4.9

446.5

5.5

67 St South from  
Saratoga

1+24

19 Lt NW cor

449.0  
3.0  
floor elev

41

1+20.5 S edge of drive

447.48  
4.47

1+12.5 N edge of 8' conc driveway

6' end of drive

447.48  
4.47

1+05 8.5 L Pine Tree

1+05 14.0 R Peacora

1+05 9 Bush Tel pole 7.0 R

+95 crosses 2.5 conc walk

447.09  
corn 4.87

0+91 13 Lt S W cor House

67 St South from  
Saranac

42

1+64

SW cor House 135 ft

4479  
H.1

1+50

ococlo 14 ft

1+79

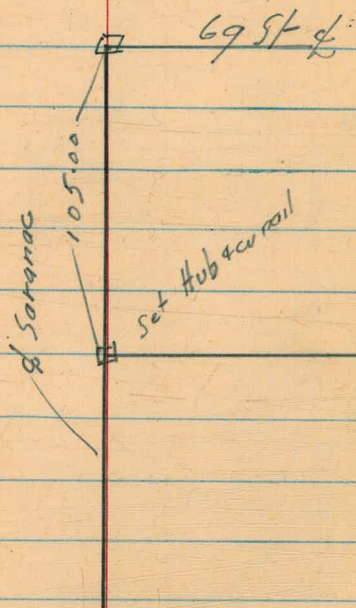
ococlo 14 ft

Sarandac St Stub to  
School House



69 St

counter manded  
8/18/50



Survey for line change

Saranac &c

8/18/50

WO 31644

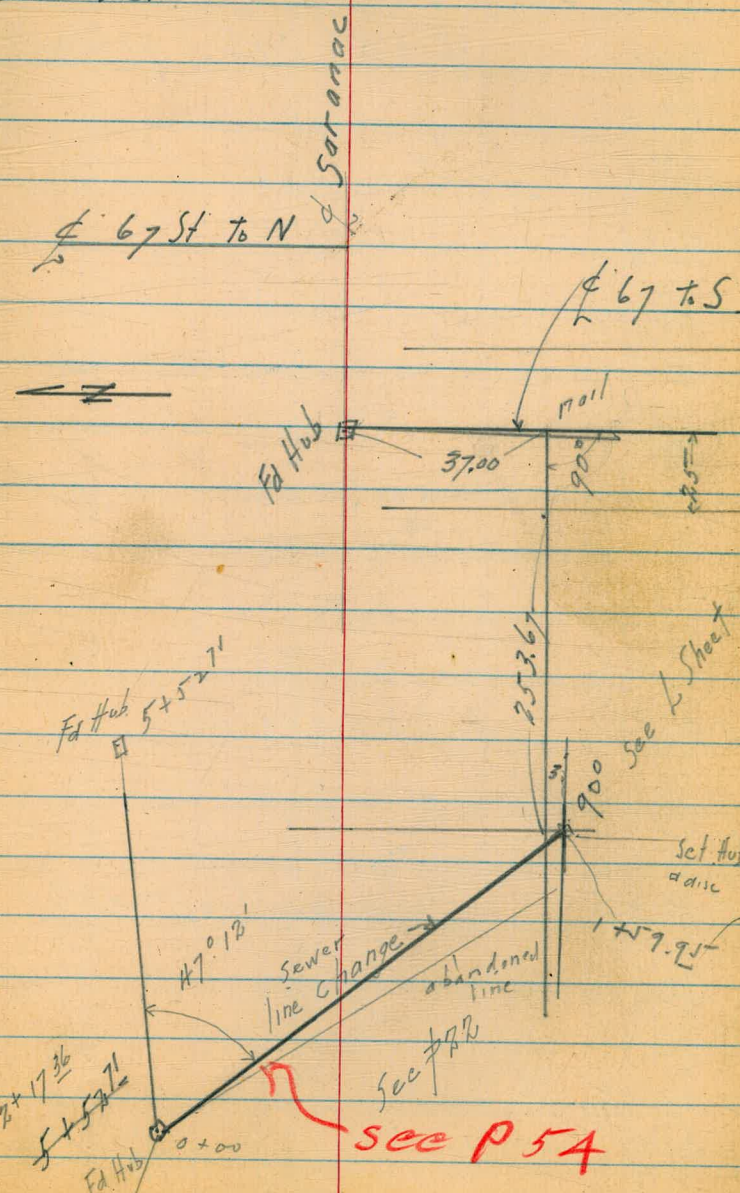
Begg

Johnson

Allan

Hatch

of Sewer



## Levels Sewer line Levels

for line change see p 44 &amp; L sheet

Begg

8/18/50 WD 316 44

Johnson

Allen  
Hatch

0 + 70

3.00

407.8

0 + 50

5.8

405.0

0 + 37

7.9

402.2

7.9

0 + 36

3 strand wire fence

0 + 35

loose boulder wall

9.0

401.8

12.49

410.82 H1

2 + 17<sup>b</sup> = 00

398.33 Hub

page 34

398.33 P 24



1+59.95

1.40

422.54

on old Hub P37  
of abandoned  
survey

424.0  
+0.1

46

1+50

419.2

4.7

1+30

412.6

11.3

412.96  
412.85  
10.98 11.09 11.14  
4.5 FT  
Twin 12" Pipe

1+26

410.0

13.9

1+18

411.9

12.0

T.P.

13.52

423.94

0.40

418.42

423.94

1+00

409.9

0.9

410.82

Gas line location

68<sup>th</sup>

North of Saranac.

□ = Fd 1/2 truck

— = Gas line

summermeyer  
Johnson  
Allen  
7-6-50

FB 1762

2+30

INDEXED

SEP 7 1950

NOK.

1+30

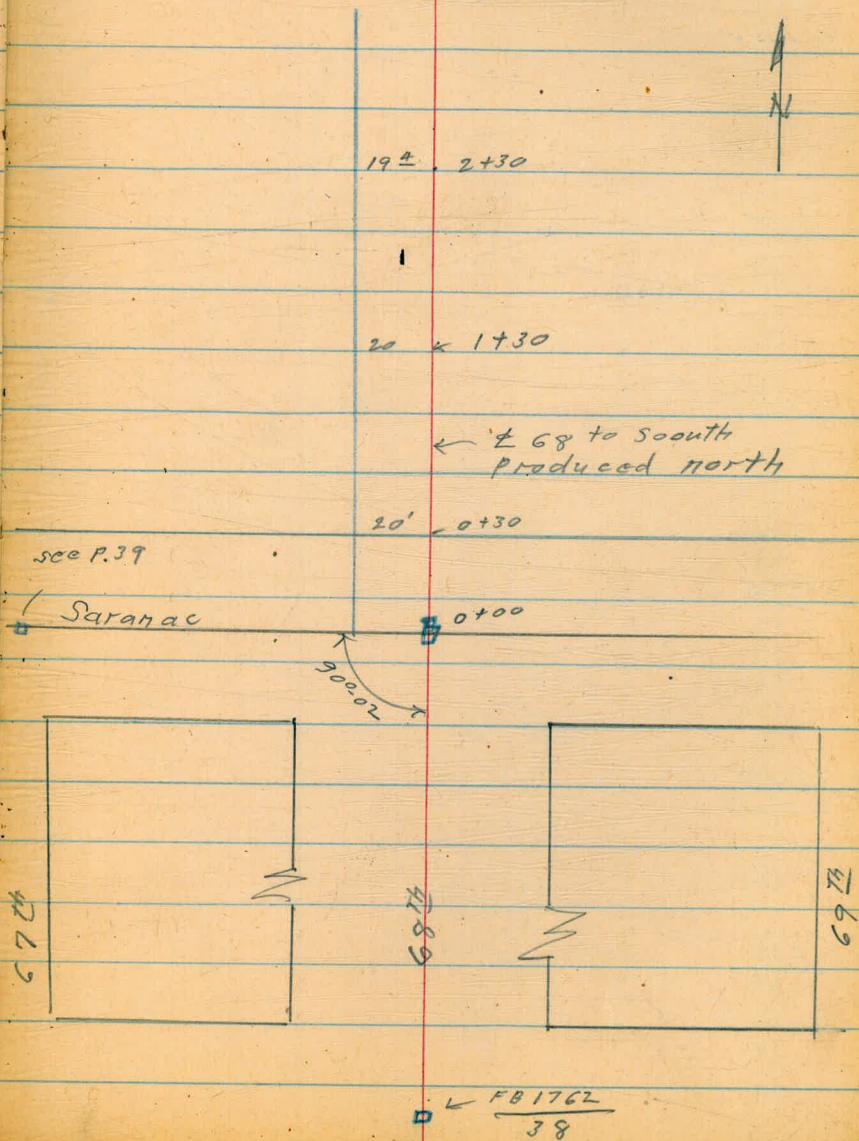
0+30 Nly. line Saranac.

0+000 ± Saranac

Have no. data from which  
to locate 68<sup>th</sup> north of Saranac in  
reference to 68<sup>th</sup> south of Saranac.  
see map of area.

± 68  
Produced from  
south

47



Gas line location - 68<sup>th</sup> St.  
North of Saranac.

± 68<sup>th</sup>  
produced from  
south of Saranac.

48

6+05

140

5+70

17<sup>5</sup>

5+37

17<sup>5</sup>

5+30

18<sup>0</sup>

4+30

18<sup>5</sup>

3+30

19<sup>0</sup>

La Mesa Colony  
North of Lots 36+37

9-19-50

49

Sammermeyer

Johnson  $\pi$

Allen

□ = set hub + disk

▣ = Fd. " " "

○ = fd pipe

See page 28

P.O.T. #1 = 12+35  $\square$  EL. = 448.6

9+62 - Notes from here on by stadia

9+62 - (P. 28)  $\square$

$\rightarrow 2^{\circ} \leftarrow$   
 $+ 2' \leftarrow$

BM #1 P. 31  
EL. = 449.81

uly line  
Lot 37

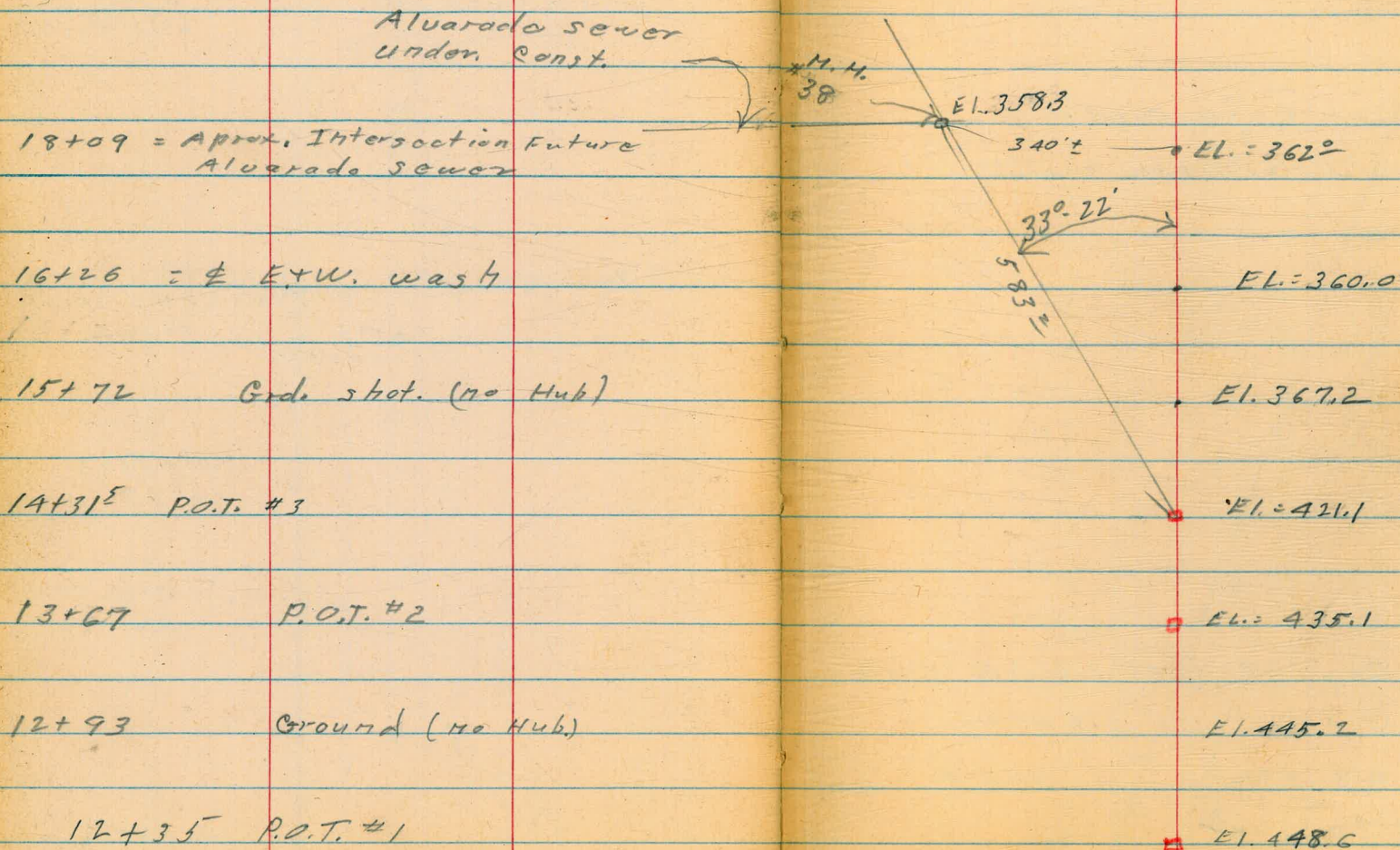
Orig. line  
Page 28

$\swarrow 89^{\circ} 56' 30'' \searrow$

0+30 P. 28

$\square$  Saranac

273'



Thru Lot 36 La Mesa Col.  
To Alvarado Canyon line

51

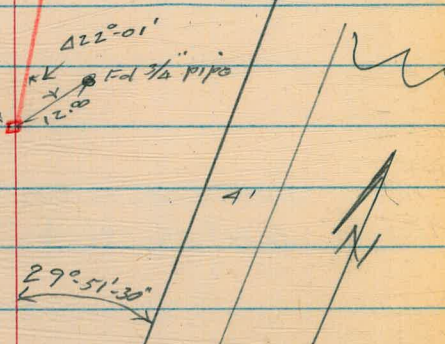
▣ = set hub + disk

□ = Fd. " " "

(G' Lt. =  $\pm$  wash EL. = 429<sup>0</sup>)

2+43 -  $\Delta = 7^{\circ} - 19' - 30''$  Rt.  $\Delta^* 1$

EL. 431.4



Lot 37  
La Mesa Colony

= 0+00

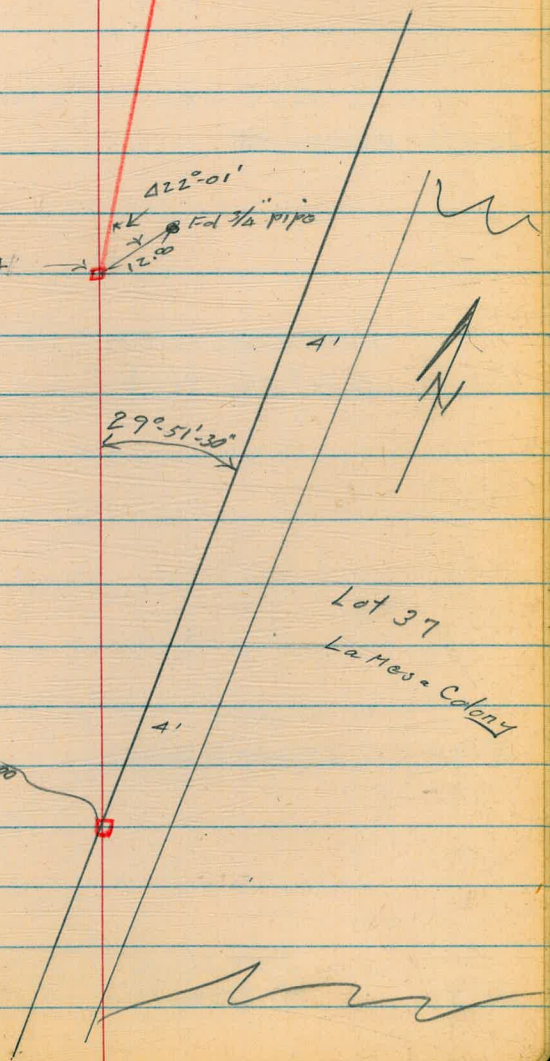
2+18<sup>5</sup>  $\pm$  Page 28 = 0+00 hub EL. = 440.2

0+17 hub at 0+00 5.5 440.2

4.9 445.7 7.0 440.8

EL. 2+00 P. 28 = 440<sup>8</sup>

0+00



2041A = 162166<sup>66</sup> M.H. 37 Alvarado Canyon line

10' RT = E wash - EL. 370<sup>0</sup>

14+32  $\Delta 0^{\circ}-11'$  RT

$\Delta$  #5

13' RT = E Wash - EL. = 381<sup>0</sup>

11+43 -  $\Delta 11^{\circ}-21'-30''$  Lt.

A #4

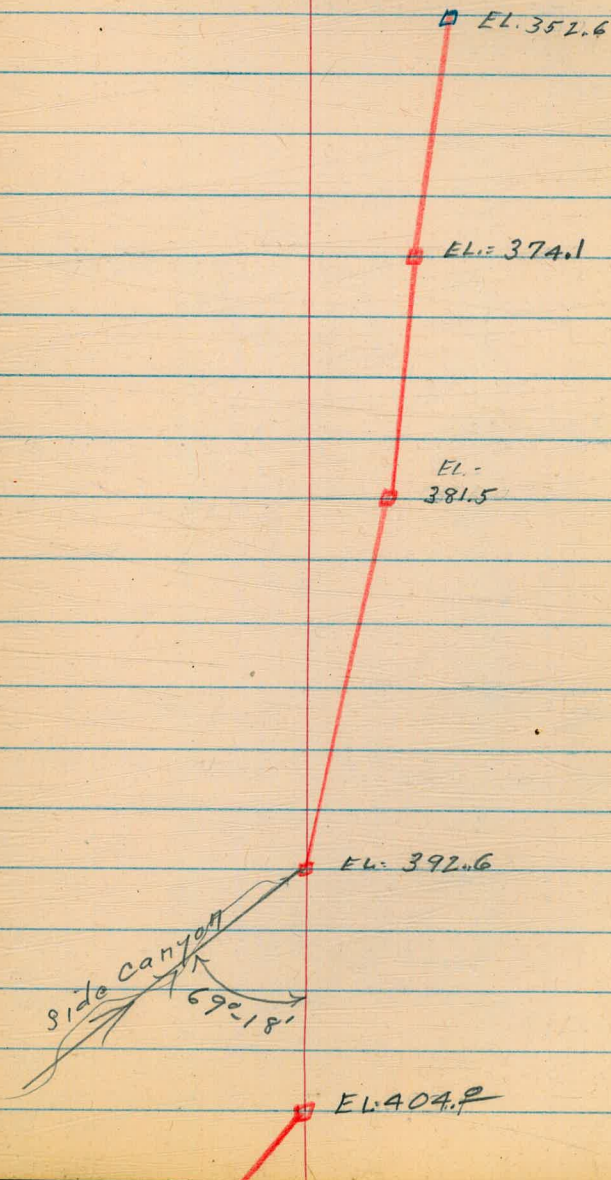
IN wash

8+57  $\Delta 38^{\circ}-28'-30''$  RT.

A #3

$\Delta 27^{\circ}-08'$  Lt.  
6+80. IN wash

A #2



From G7<sup>th</sup> + Saranac

Ally. to Reservoir Dr. Sewer line

Sommerneyer

9-27-50

Allen  
Lockhead

□ = set 1/4" dist

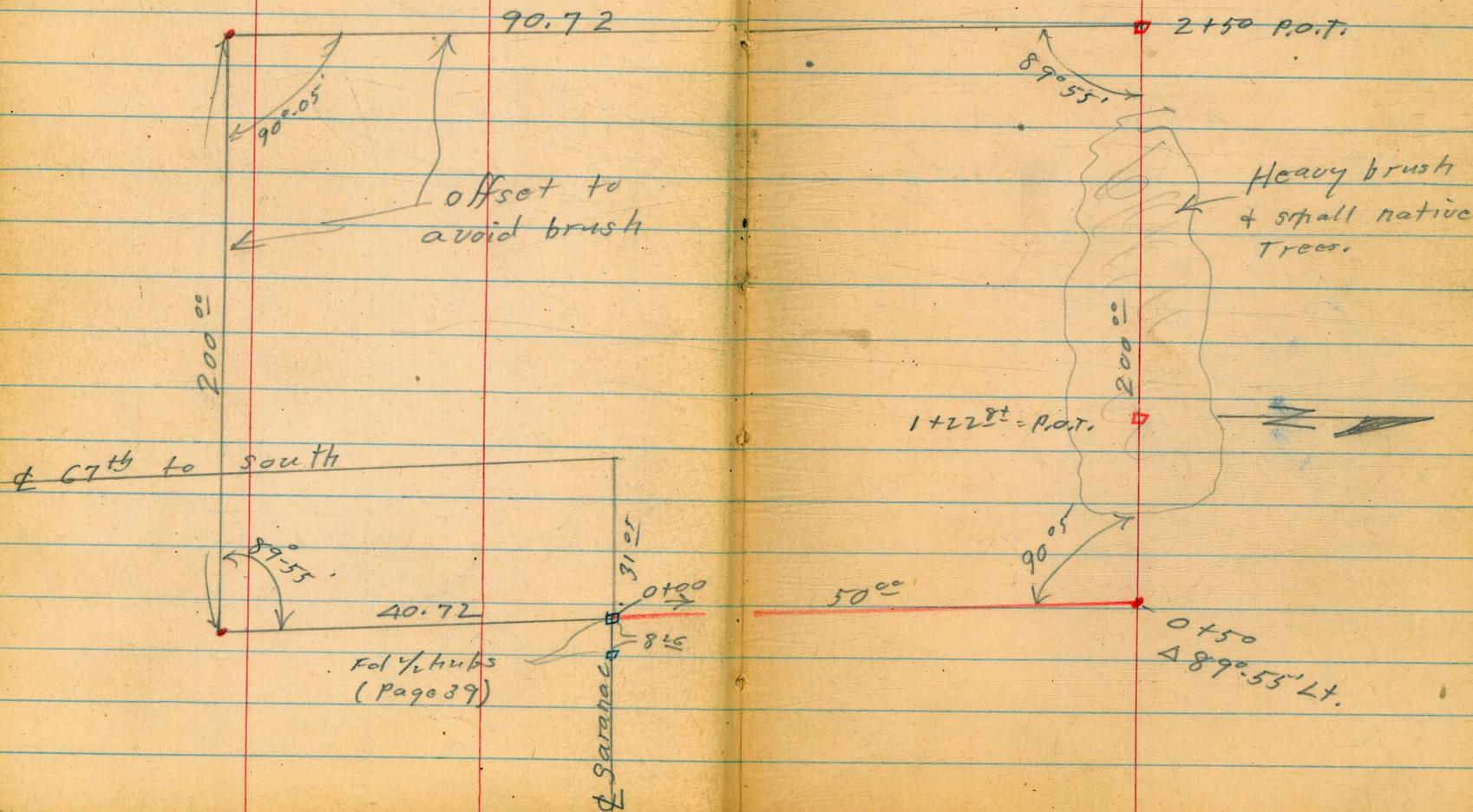
• = Nail

□

INDEXED

53

A+00



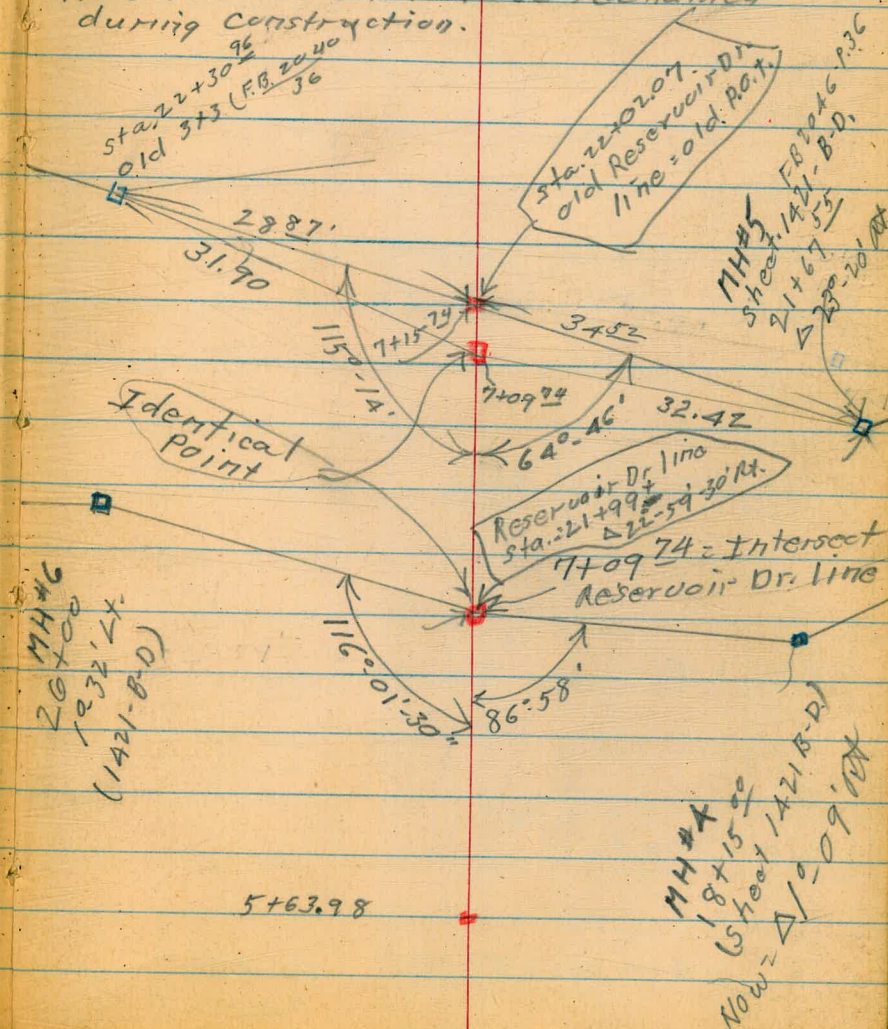
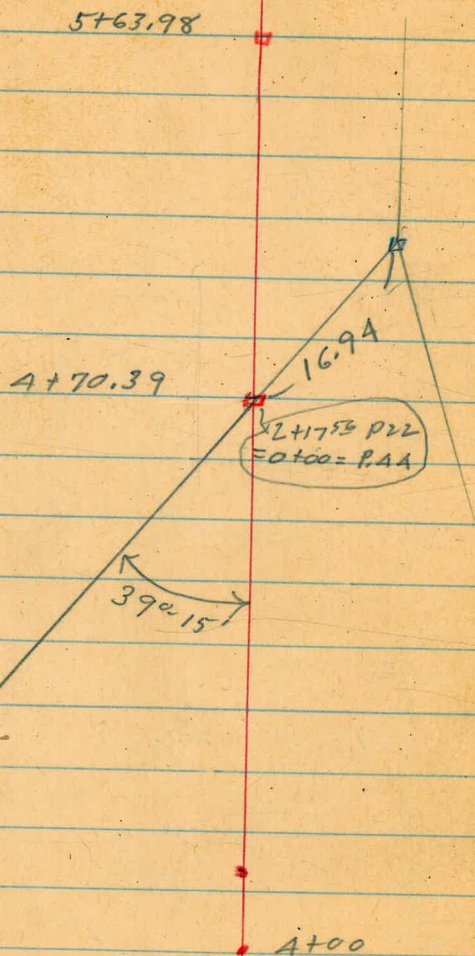


Note

54

This sketch off scale so to better show distances & Δ to orig. line as shown on sheet 1A21-B-D.

Reservoir drive line to be reestablished during construction.



5+63.98

0+90

12.3

4383

0+72

 $\frac{10.0}{10}$ 

4406

11.0

4396

 $\frac{10.7}{10}$ 

4399

103 Lt. = start wire fence  
 0+62 = cross wire fence

5.8

4448

0+52 = end oil pump

4.9

4457

0+50 = Δ

4.8

Nail

4458

0+00 = (0+00 P-39)

4.47

44612

4.74 450.59

445.85

7+06<sup>12</sup> (P-27)450.59

0.81 431.95 12.41 431.14

3405 = Cross wire fence

2+90 11<sup>2</sup> Lt. = line of fence

431.0  
12.6  
10

429.7  
13.9

427.3  
16.3  
10

2+50<sup>00</sup> = 1/2 P.A.T.

2+36<sup>5</sup> cross wire fence

2+36 - 11' Lt. = end board shed (shed is 12' X 33')

11' Lt. = start board shed on post

2+24

10<sup>5</sup> Lt. = line of fence

434.48  
9.07  
446

442.9  
0.7  
11  
Floor  
of shed

440.3  
3.7  
10

438.6  
5.0

436.4  
7.4  
10

712 2.99 443.55 10.03 440.56

443.55

1+80

444.3  
6.3  
10

442.2  
7.7

440.8  
9.8  
10

1+50

444.5  
6.1  
10

443.3  
7.3

441.2  
9.3  
10

1+22<sup>8</sup> pat. 10' Lt. = line of fence.

443.6  
7.0  
10

442.9  
7.7

440.9  
9.7  
10

450.59

715.74  
563.98  
151.76

709.74  
563.98  
145.76

4

57

5+63 98 1/2 P.O.T.

11' Lt. = line of fence  
5+21 11' Lt. = end of rock wall

5+10

12' Lt. = line of fence + rock wall  
4+70 39 1/2 P.O.T. =

11' Lt. = line of fence  
4+30 11' Lt. = start 2' high loose rock wall

T.P. 1.60 408.08 13.10 406.48

3+90 12' Lt. = line of fence

T.P. 0.38 419.58 12.75 419.20

3+35

407A  
0.7  
10

40409  
3.99  
H46  
10

4005  
7.6  
10

404A  
3.7  
10

401A  
6.7  
10

3987  
9.4  
10

4030  
5.1  
10

40015  
7.93  
H46  
10

3989  
9.2  
10

4019  
6.2  
10

4013  
6.7  
10

4019  
6.2  
10

408.08

4121  
7.5  
10

4098  
9.8  
10

4071  
12.5  
10

419.58

4243  
7.7  
10

4233  
8.7  
10

4217  
10.3  
10

431.95

6+97

$$\begin{array}{r} 384.1 \\ 12.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 384.3 \\ 11.9 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 384.1 \\ 12.1 \\ \hline 10 \end{array}$$

6+88 Bottom of N+S. Wash

$$\begin{array}{r} 382.1 \\ 14.1 \\ \hline \end{array}$$

6+76 = Cross wire fence.

$$\begin{array}{r} 385.2 \\ 11.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 384.6 \\ 11.6 \\ \hline \end{array}$$

$$\begin{array}{r} 383.9 \\ 12.8 \\ \hline 10 \end{array}$$

6+65

$$\begin{array}{r} 398.1 \\ 3.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 391.6 \\ 4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 390.1 \\ 6.1 \\ \hline 10 \end{array}$$
T.P. 0.49 396.15 12.42 395.66
$$\begin{array}{r} 396.15 \\ \hline \end{array}$$

6+48: Cross wire fence

6+35

$$\begin{array}{r} 399.1 \\ 8.4 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 398.3 \\ 7.8 \\ \hline \end{array}$$

$$\begin{array}{r} 396.7 \\ 11.4 \\ \hline 10 \end{array}$$

5+91 - 10' Lt. = Δ in fence

$$\begin{array}{r} 406.3 \\ 1.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 405.9 \\ 4.2 \\ \hline \end{array}$$

$$\begin{array}{r} 401.0 \\ 7.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 408.08 \\ \hline \end{array}$$

(0109<sup>38</sup> - Page 23 - EL: 383<sup>0</sup>) 13.05 383.10 ✓

15' Rt = line of wire fence  
 7+15<sup>74</sup> = Intersect Reservoir Dr. line

384.7

$$\frac{11.5}{10}$$

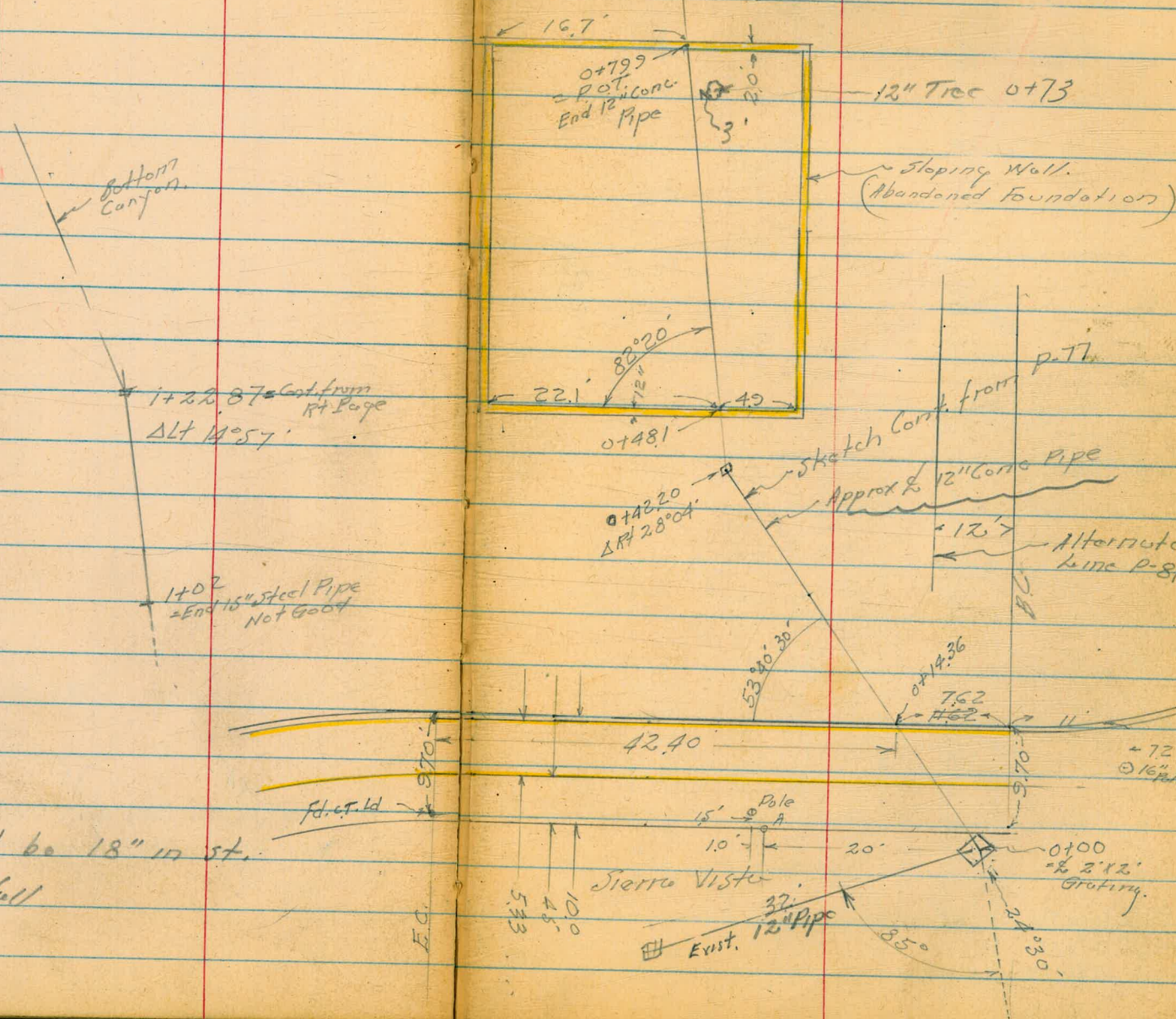
384.17

$$\frac{11.98}{\text{Hub}}$$

383.8

$$\frac{12.4}{10}$$
396.15

Set Hub + Disk  
1+22.87 = See Cont. on Lt. Page  
Δ Lt



Bottom Canyon

0+799  
= Pot. Conc.  
End 12" Pipe

12" Trce 0+73

Sloping Wall.  
(Abandoned Foundation)

1+22.87 Cont. from  
Rt Page  
Δ Lt 14°57'

0+4220  
Δ Rt 28°04'

Sketch Cont. from  
P-71

Approx. 12" Conc. Pipe

Alternate  
Line P-81

1+02  
= End 15" Steel Pipe  
Not Good

42.40

7.62  
#52

+72  
@ 16' ft

Fl. ct. Id

Pole  
A  
15'  
10'

Sierra Vista

0+100  
= 2'12"  
Grating

Est. 12" Pipe

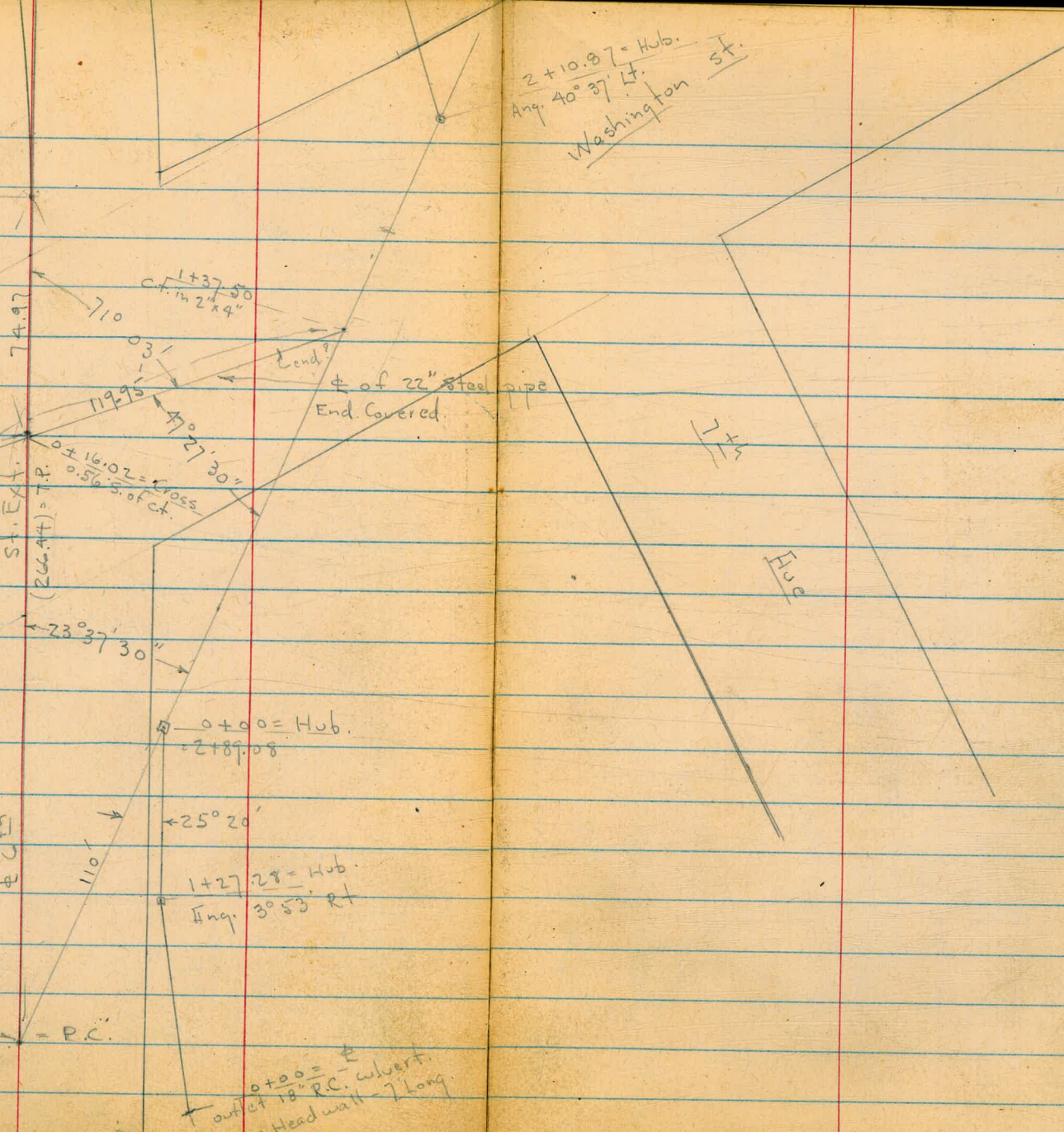
Pipe should be 18" in st.  
And 24" outfall

E.G.

61

2+10.87 = Hub.  
Ang. 40° 37' Lt.  
Washington St.

c.t. = P.C.



B. 1562  
P. - 2 = Id. ct.

I.E. cut in  
pipe = Iron Pipe  
Elev. = 245.10

St. EX. 1  
(266.44) = T.P.

0+16.02 = Cross  
0.56' S. of ct.

End?  
φ of 22" steel pipe  
End Covered.

0+00 = Hub.  
= 2189.08

1+27.28 = Hub.  
Ang. 30° 53' Rt.

0+00 = φ  
outlet 18" RC. culvert.  
+ Head wall - 7' long.

Fd. Ld. + c.t.  
Shown on T.P.  
Sheet. 258

φ c.t.

110'

← 25° 20'

← 23° 37' 30"

← 119° 03'

← 710  
c.t. in 2" x 4"

74.97

Hub

1+14



74  
73

Block 1 - Williams Sub.  
Map 855

± 6 1/2 St. Ext. ↗

5+69.43 = end.  
Hub.

Lot 53  
Lot 54

4+22.04 = Hub.  
Ang. 42° 09' Rt.

3+31.90 = Nail  
Ang. 22° 14' Lt.

2+48.28 = Gal. Nail

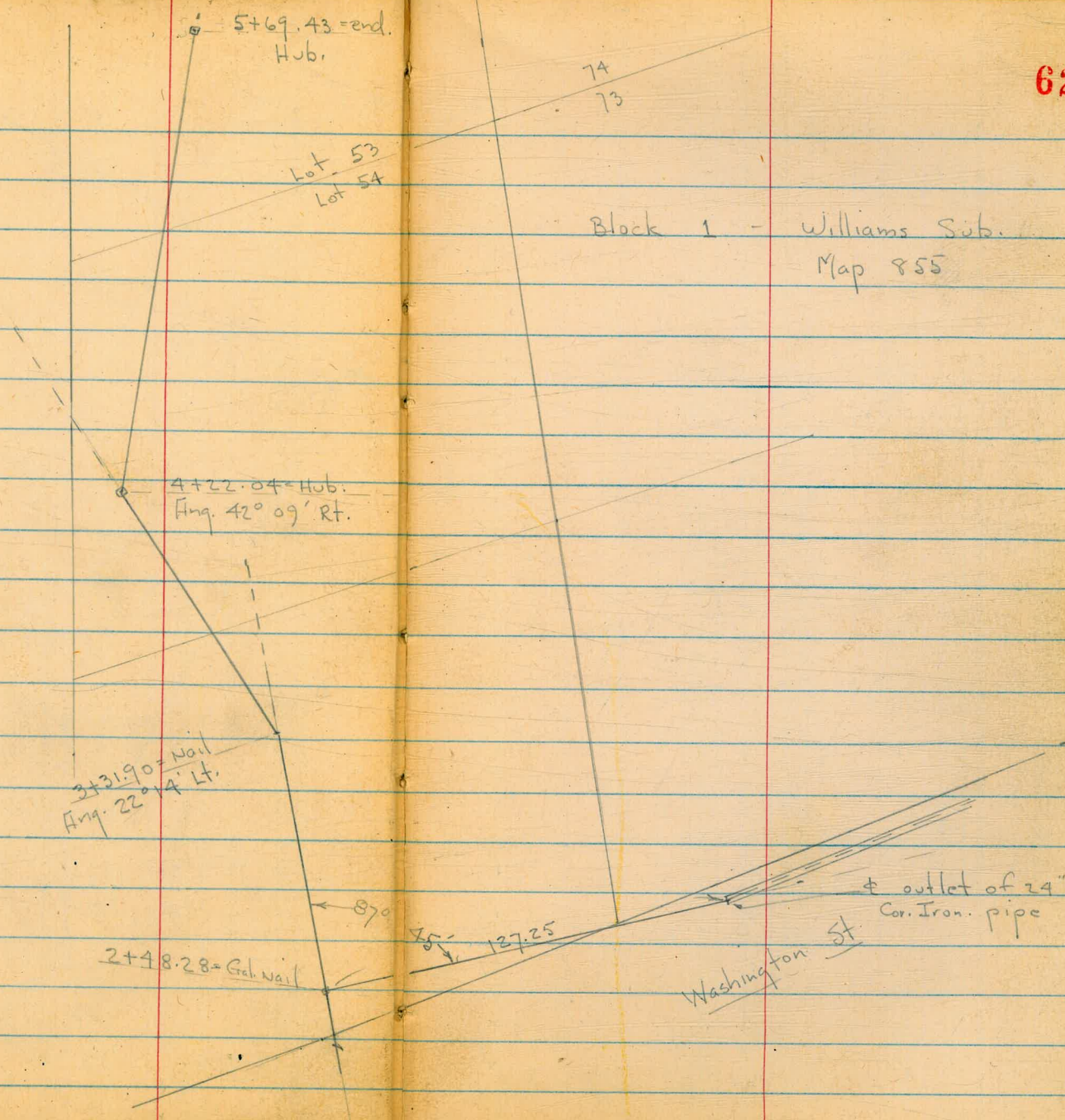
87°

45°

127.25

Washington St.

± outlet of 24"  
Cor. Iron. pipe



Levels along  $\pm$  of Prop. Drain - E. of  
6<sup>th</sup> St. extension - Washington St. - N.

# 4810      11-17-50  
W.O. 20755      7.0.

1+37.50 = Int. with approx. E of 22" steel pipe -  
end. Covered - end = 21' Lt. along line

233.2  
7.0  
12  
222.8  
8.4  
3  
Toe  
226.21  
9.49  
7 wash  
225.2  
11.0  
15  
7 wash  
220.5  
7.7  
30

1+00

231.7  
7.5  
15  
226.3  
9.9  
6  
Toe  
Fill  
225.3  
10.9  
15  
225.7  
10.5  
15  
225.5  
10.4  
30 = Toe

0+96.5 - 14.2 Lt. Near Cor. Conc. Bridge. Gl.

0+50

233.1  
3.1  
20  
227.5  
8.7  
9  
Toe  
222.1  
9.1  
7 wash  
227.7  
8.5  
15  
231.1  
5.1  
25

0+00 = Toe of Fill slope on Lt.

231.20 ✓  
5.00  
= on Hub  
236.20  
7 wash  
220.3  
5.9  
14

0.60 236.20 ✓ 12.71 235.60 ✓

1.11 248.31 ✓ 12.48 247.20 = ct. 7.6<sup>th</sup>  $\pm$  Washington R.O.W. ✓

0.26 259.68 ✓ 13.19 259.42 ✓

0.67 272.61 ✓ 13.02 271.94 ✓

B.M. 1.09 284.96 ✓ 283.87 = M.W. B.P. - 6<sup>th</sup> + Univ.

3+00

2+70

Levels - Later - Sec P. 67

2+48.28 = Tie to 24" Culvert on Rt.

Waste Conc. from old plant - pretty Hard.

2+35 = ± Wash = Beg. Conc. Bottom in Wash

2+27 = 31.8 Lt = ± Sewer M.H. - Top = Top fill

2+21.5 = 13.6 Rt = Near Cor. Conc. Bridge Col.

2+10.87 = Ang. 40° 37' Lt. - Sect. on split

T.P. 70.6 232.81 1045 225.75 = 1045 2+10.87

1+90

1+70

Lt Rt  
 230.1 225.4 222.5 224.0  
 2.0 7.4 10.3 8.8 7.3  
 10 on Hard 6 14 30  
 Conc. wash

1.9 230.9 226.1 224.0 223.6  
 10 6.7 8.8 9.2 5.4  
 Toe ± wash 22

↓  
 225.08  
 7.73  
 on Nail

230.0 224.9 221.2 224.4 222.7  
 2.8 7.9 8.6 8.4 0.1  
 15 7 7 19  
 Toe Toe

230.5 225.6 222.9 222.36 230.9  
 2.2 7.2 8.9 10.45 1.9  
 25 15 5 on Hdb 10  
 Toe ± wash

232.81 ✓

11.6  
 ± wash

232.8 226.6 223.9 224.1 225.0  
 2.4 9.6 12.3 10.1 7.2  
 15 4 15 25  
 236.20 Toe wash

4+91 = 157' Lt. =  $\Phi$  24" Euc.

4+81.88 = Cross 12" Gas Main

4+50

B.M. on Hub. 4+22.04

2.86 204.29 ✓

T.P. 0.53 207.15 ✓

13.14 206.62

4+22.04 = Ang. 42° 09' Rt. - Sect. on split

4+15 = 9' Lt. =  $\Phi$  24" Euc.

Wash Conc. in wash from here on

3+85 = end of Solid Conc. in Wash + fill

3+70

T.P.

0.12

219.76

13.17

219.64

3+31.90 = Ang. 22° 14' Lt. - Sect. on split

Lt.

Rt.

Rt.

65

207.2  
0.0  
20  
204.8  
4.7  
12  
wash  
202.4  
4.8  
3  
203.8  
3.3  
213.4  
+ 6.2  
15

200.55  
6.60 = Top Pipe

207.15 ✓

213.5  
6.3  
20  
fill  
204.6  
15.2  
6  
= Toe  
204.5  
15.3  
wash  
204.6  
15.2  
12  
213.0  
6.8  
25

210.9  
8.9  
22  
Conc. fill  
208.1  
11.7  
4 wash  
208.1  
11.7  
2  
221.3  
+ 1.5  
20

213.4  
6.4  
15  
Conc. fill  
211.7  
8.1  
4 wash  
211.7  
8.1  
4  
221.6  
+ 1.8  
15

219.76 ✓

224.7  
6.1  
20  
on Conc.  
221.7  
11.1  
10  
Conc. Wash  
219.0  
13.8  
2  
222.9  
9.9  
8  
223.0  
9.8  
26  
Bot. Bank  
232.81 ✓

5+69.43 = Hub = End.

5+52.5-12' Lt. =  $\pm 14"$  Euc.

5+43-7' Rt. =  $\pm 10"$  Euc.

5+42.5-13' Lt. =  $\pm 10"$  Euc.

5+41-19' Lt. =  $\pm 18"$  Euc.

5+40

5+36-11' Lt. =  $\pm 5-6"$  Euc.

5+35-12' Rt. =  $\pm 30"$  Euc.

5+35-5' Rt. =  $\pm 2-10"$  Euc.

5+31-10' Lt. =  $\pm 24"$  Euc.

5+28-8' Rt. =  $\pm 30"$  Euc.

5+22-5.5' Lt. =  $\pm 10"$  Euc.

5+11-8' Lt. =  $\pm 8"$  Euc. - Dead.

5+11-4' Lt. =  $\pm 18"$  Euc. - Dead.

T.P. 154 195.63 ✓ 13.06 194.09 ✓

5+00

4+96.8-26.3' Lt. =  $\pm$  Sewer M.H. 3.94

4+92-21' Lt. =  $\pm 24"$  Euc.

189.2  
6.4  
25

187.9  
7.7  
18

187.66  
7.97  
on Hub.

187.8  
7.8  
5

193.8  
1.8  
20

wash

193.9  
1.7  
30

189.6  
6.0  
7

189.7  
5.9  
8

189.7  
5.9  
8

190.5  
5.1  
20

190.9  
+1.3  
30

wash

inside wash

on S. Bank.

200.8  
6.3  
27

193.6  
13.6  
16

195.63 ✓  
13.4  
wash

193.8  
3.6  
20

203.6

207.15 ✓

on Rim

Req. levels along  $\pm$  of Prop. Side Drain  
Sta. 2+48.28 to outlet of 24" Cor. Iron.

T.P. 8.24 256.72 0.56 248.44

0+72

0+70 -  $\pm$  at Top Bank

T.P. 11.61 249.00 2.11 237.39

0+55

0+28.5 =  $\pm$  of 12" Cor. Main 10.06 226.88

0+20

0+00 = Nail = 2+48.28

B.M. = Nail 12.42 237.50 225.08  
2+48.28 - 7.64

L. E Rt.

241.1  
7.9  
15  
238.4  
10.6  
233.6  
15.4  
3  
wash  
231.7  
11.3  
12  
229.5  
7.5  
20

230.5  
18.5

249.00

233.1  
1.4  
15  
232.6  
4.9  
7  
226.2  
11.3  
4  
wash  
226.4  
11.1  
2  
226.4  
16.1  
14  
235.1  
2.4

227.9  
9.6  
17  
224.4  
13.1  
13  
225.1  
12.4  
11  
230.2  
7.3

225.08  
12.42  
on Nail

237.50

Lt.

Rt.

68

1+27.25 = out let 24" C.I. pipe = end.

1+10

201.6

5.1

ground.

206.55

0.17

I.E.  
Pipe

202.6

4.1

10

201.0

5.7

256.72

201.2

9.2

5

\*wash

202.0

4.7

12

Beginning levels along  $\pm$  of Prop  
 Drain Extension from outlet of 18" R.C.  
 Culvert from 6<sup>th</sup> + Univ. to -0+00  
 on P. 61

-1+27.28 = Ang. 3° 53' Rt. - Sect. on split

1+14 = 9.5' Rt. =  $\pm$  6" Euc.  
 1+09 = 21' Lt. =  $\pm$  24" Euc.  
 1+00

0+79 = 9' Rt. =  $\pm$  6" Euc.

0+59 = 5.5' Lt. =  $\pm$  20" Euc.

0+51 = 5.5' Lt. =  $\pm$  12" Euc.

0+50

0+06

seems to seep underground.

Note: Ext. Waterway wanders to E. and

0+00 = Cross on Top of 7' Head wall at  $\pm$  of  
 outlet of 18" R.C. Pipe

4.98

276.92

271.94 = T.P.

-P. 63

266.4  
 10.5  
 15

7.7  
 269.2

8.0  
 268.9  
 20

9.3  
 267.6  
 20

8.0  
 268.9

8.0  
 268.9  
 20

269.14  
 7.78  
 31  
 edge Conc.  
 Pave

6.5  
 270.4

7.1  
 269.8  
 20

8.6  
 268.3  
 50  
 $\pm$  waterway

271.9  
 5.0  
 10

4.3  
 272.6

6.4  
 270.5  
 4

3.9  
 273.0  
 7

269.57

7.35  
 I.E. pipe

4.89  
 272.03

Top Hed wall.

276.92 ✓



~~RT~~

Notes Reduced. 11-27-50

4          4          RT

P. 63  
check Hub. 0+00

9.97      231.20 ✓

2+89.08 = .end = 0+00 ahead.

2+67- 5.5' Lt. = ± 6" Euc.

2+62- 24' Rt = ± 12" Euc.

2+55- 22' Rt = ± 14" Euc.

2+45

2+27- 13' Rt = ± 12" Euc.

2+15- 17' Rt = ± 14" Euc.

2+03- 17.5' Rt = ± 10" Euc.

2+00

T.P.      2.14      241.17 ✓      12.65      239.03

1+91- 12' Rt = ± 24" Euc.

1+90

1+76- 11.5' Rt = ± 18" Euc. (Trees on Rt. are

1+70 = on N. side of old fill

1+69- 6 Lt = ± 16" Euc.

0.07      251.68 ✓      13.14      251.61

T.P.      0.70      264.75 ✓      12.87      264.05

+2.2  
15

9.97  
on Hub.

11.0  
15

8.6  
34

+5.2  
15

6.6  
Toe

8.1  
3

8.3  
14

4.5  
25

+8.0  
15

4.5  
Toe

4.8  
12

0.7  
20

12.8  
238.9

city of large grove)

+ a.] 251.3  
15

4.8  
9

3.7  
Toe

0.0  
20

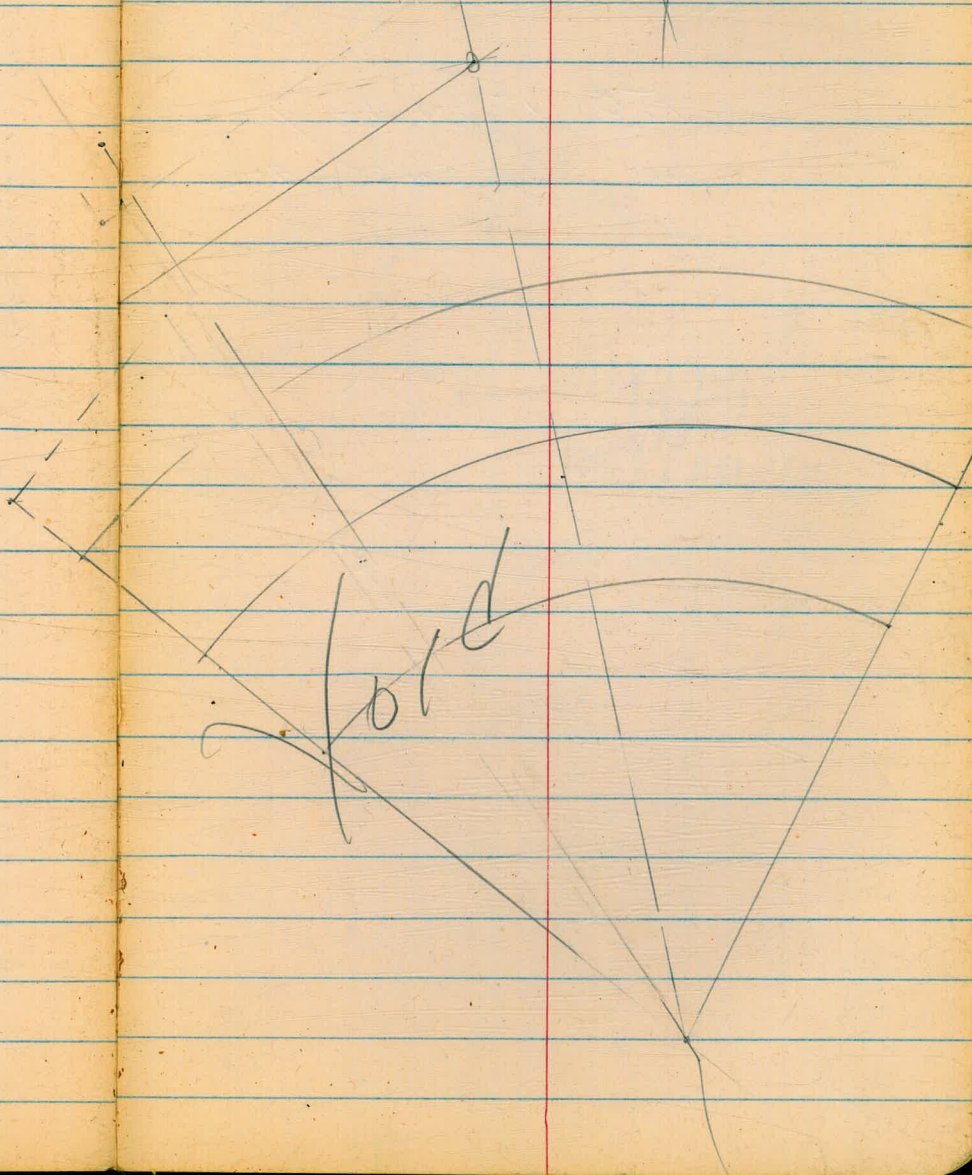
Toe  
D.W.

251.68 ✓

276.92 ✓

Word 71

Word



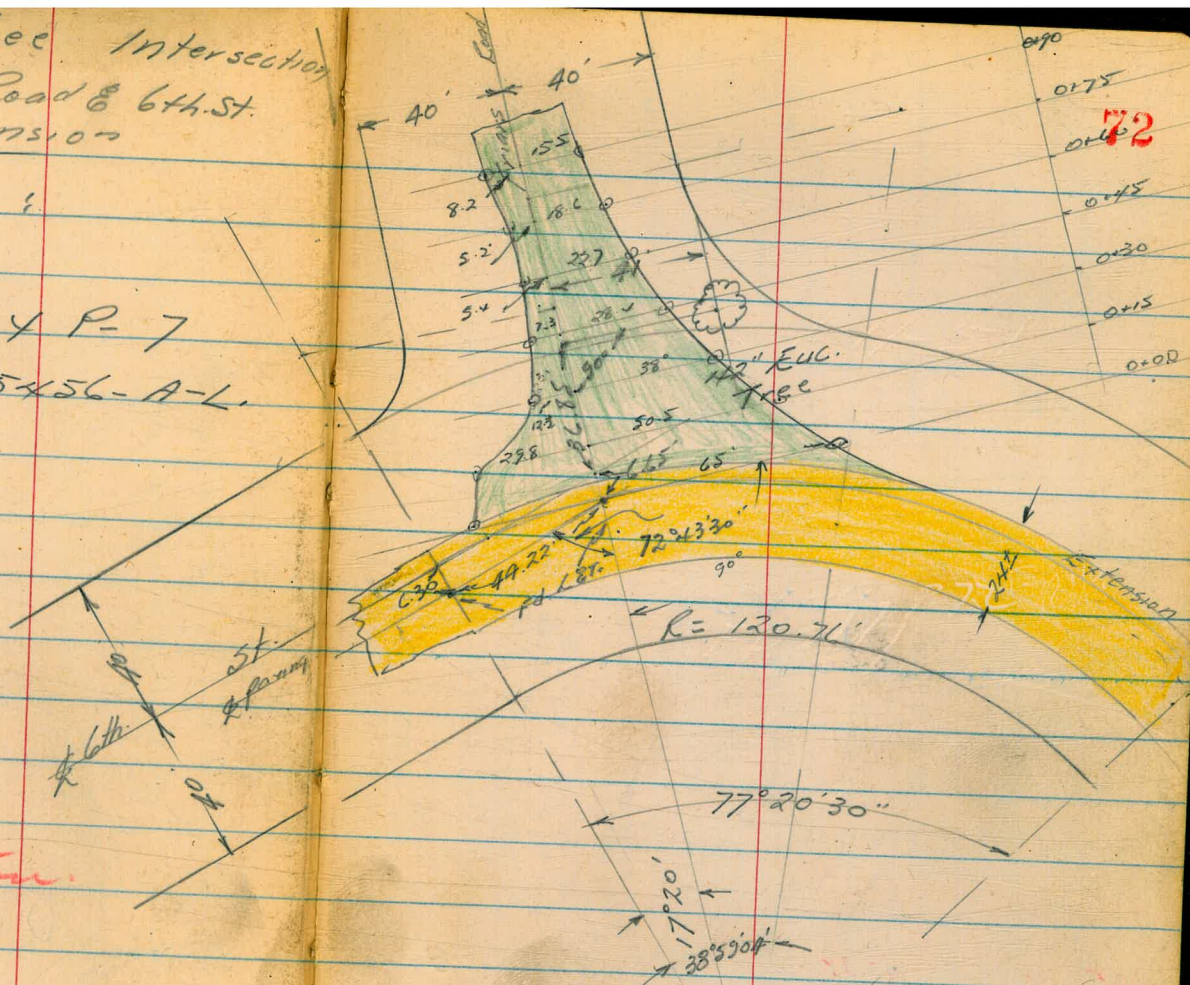
Locate Tree Intersection  
 Hendricks  
 Shepard  
 Crawford  
 Friars Road & 6th St.  
 Extension

Reference:

FB 1534 P-7  
 and Dwg. 5456-A-L

INDEXED  
 JAN 12 1951

Plotted by Remington  
 See 4191-B



Sierra Vista Drain

Cont Rt. Page 80

73

1+63

2227.7	2207	218.0	220.1	222.30
7.0	9.0	11.7	9.6	7.4
10	5	Ditch	5	10
2227.7	226.4	222.4	225.6	228.5
2.0	3.3	27.3	4.2	1.2
10	5	Ditch	5	10
2227.7	228.3	227.4	228.7	227.9
0.0	1.4	2.3	6.0	2.3
10	5		5	10

1+33

1+28

1+228) 81+

TP 2.05 227.70 ✓ 939 227.65 ✓

1+10

1+02 - End 15" Steel Pipe

239.0	234.6	227.6	231.7	231.0
2.4	8.4	9.4	5.3	6.0
10	5	216.4	6	1
238.0	228.6	227.6	233.6	236.20
2.0	3.7	0.80	3.4	0.8
15	7	Invert	0	3
237.0	237.04 ✓	237.04 ✓	237.04 ✓	237.04 ✓
239.0	234.6	227.6	231.7	231.0

TP 0.06 237.04 ✓ 1293 236.98 ✓

0+92

0+80

290.7	294.2	292.7	294.2	294.2
9.2	5.7	6.2	5.7	15.0
10	10	13.2	10	10
294.2	294.2	294.2	294.2	294.2
294.2	294.2	294.2	294.2	294.2

0+799 - End 12" Conic Pipe 249.91

4.25	5.11	5.04	5.7
10	Invert	0	10
Top Fdn.	249.91	Top Fdn.	Top Fdn.

4-3-51  
 Pope  
 Clark  
 Huffman

Profile & Proposed Drain  
 6<sup>th</sup> St. Ext. & Washington  
 (Sta. 0+00 To 3+50  
 As Per Drawing 8604-L)

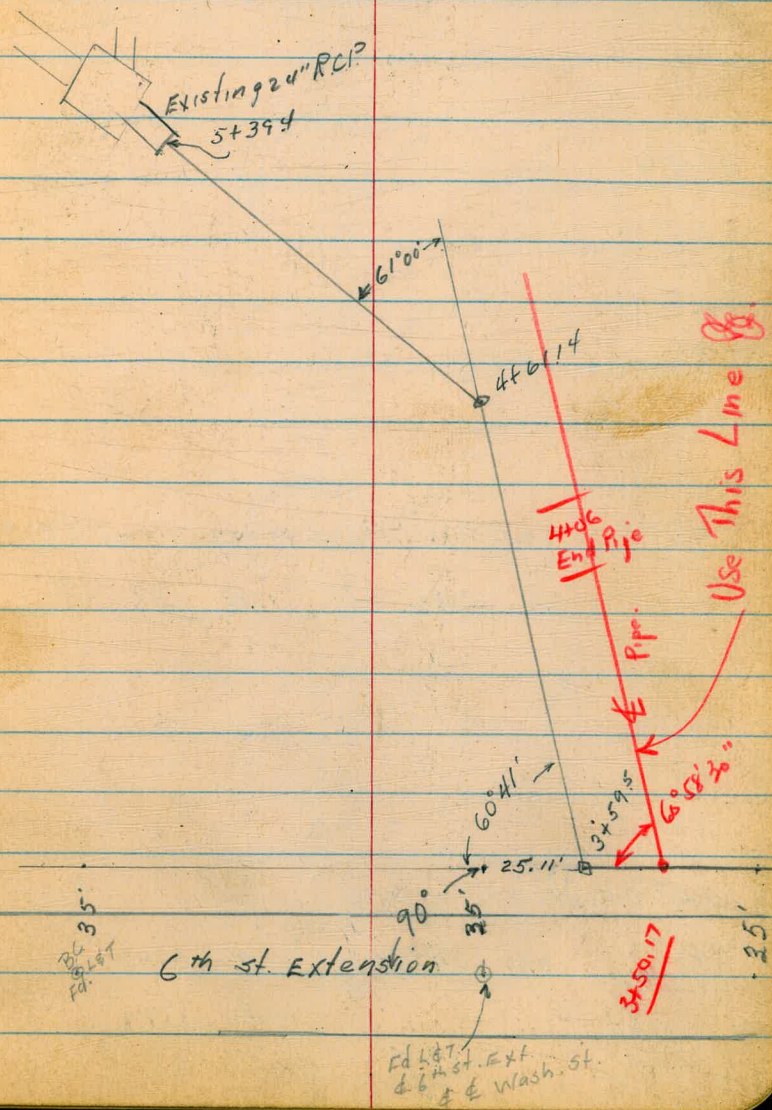
W.O. 20755

3+25		8.7	249.5
2+955		5.6	247.6
2+875		4.4	248.8
2+795		3.1	250.1
TP 170	253.18 ✓	11.47	251.48 ✓
2+575		10.7	252.2
2+275		9.0	254.0
1+975		7.4	255.6
1+675		6.3	256.6
1+50		3.6	259.2
TP	1.05 262.95 ✓	12.36	261.90 ✓
1+25		8.1	266.2
1+00		5.5	268.8
+75		5.3	269.0
+050		3.5	270.8
0+25		2.9	271.2
0+00 Fl.		4.69	269.57 ✓
T.P. Headwall	223 274.26 ✓	12.13	272.03 ✓
BM	029 284.16 ✓		283.87 ✓

INDEXED

AUG 2 1951

74



4+61.14 Angle  
61° Lt.

4+50

4+25

3+78.5 & South Face 4.5' x 4.5' Bridge column & Bottom Fill

T.P. 251 234.19 ✓ 1228 23168

3+74 Edge Fill

3+59.5 ANGLE  
60° 41' Rt.

T.P. 0.90 243.96 ✓ 1012 243.06 ✓

3+50

253.181

1.44 238.8

6.1 228.1  
30

9.1 225.1  
20

9.1 225.1  
10

6.2 228.0

9.0 225.2  
10

8.7 225.5

7.7 226.5  
10

7.2 227.0  
10

8.8 225.4

8.8 225.4  
10

6.0 228.2  
4.5

6.2 228.0

8.1 226.1  
10

234.19 ✓

4.0 240.0  
10

6.2 237.8

8.7 235.3  
10

5.0 239.0  
10

6.4 237.6

7.3 236.7  
10

243.96 ✓

5+49.40  $\phi$  Existing  $\phi$  Type Cleanout

10.80 223.39  
FL

5+39.40 Flowline Existing 24" C.R.P.

10.33 223.86  
FL

5+10

44	24.8	9.2	225.0	9.2	225.0	9.0	225.2	7.3	226.9
15		8				5		10	

4+76

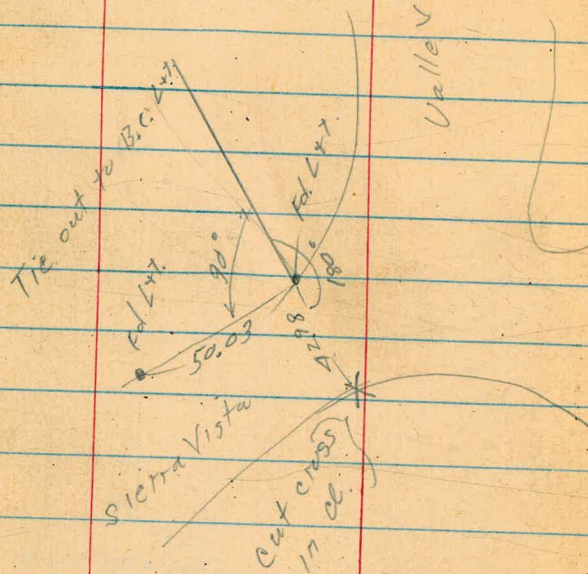
7.8	226.4	9.2	225.0	8.8	225.4
20		10			

234.19

Location And Extension  
Existing Culvert  
on Sierra Vista & Altura Pl.

Walker  
Pope  
Clark  
Huffman  
5-25-51

NO 20823

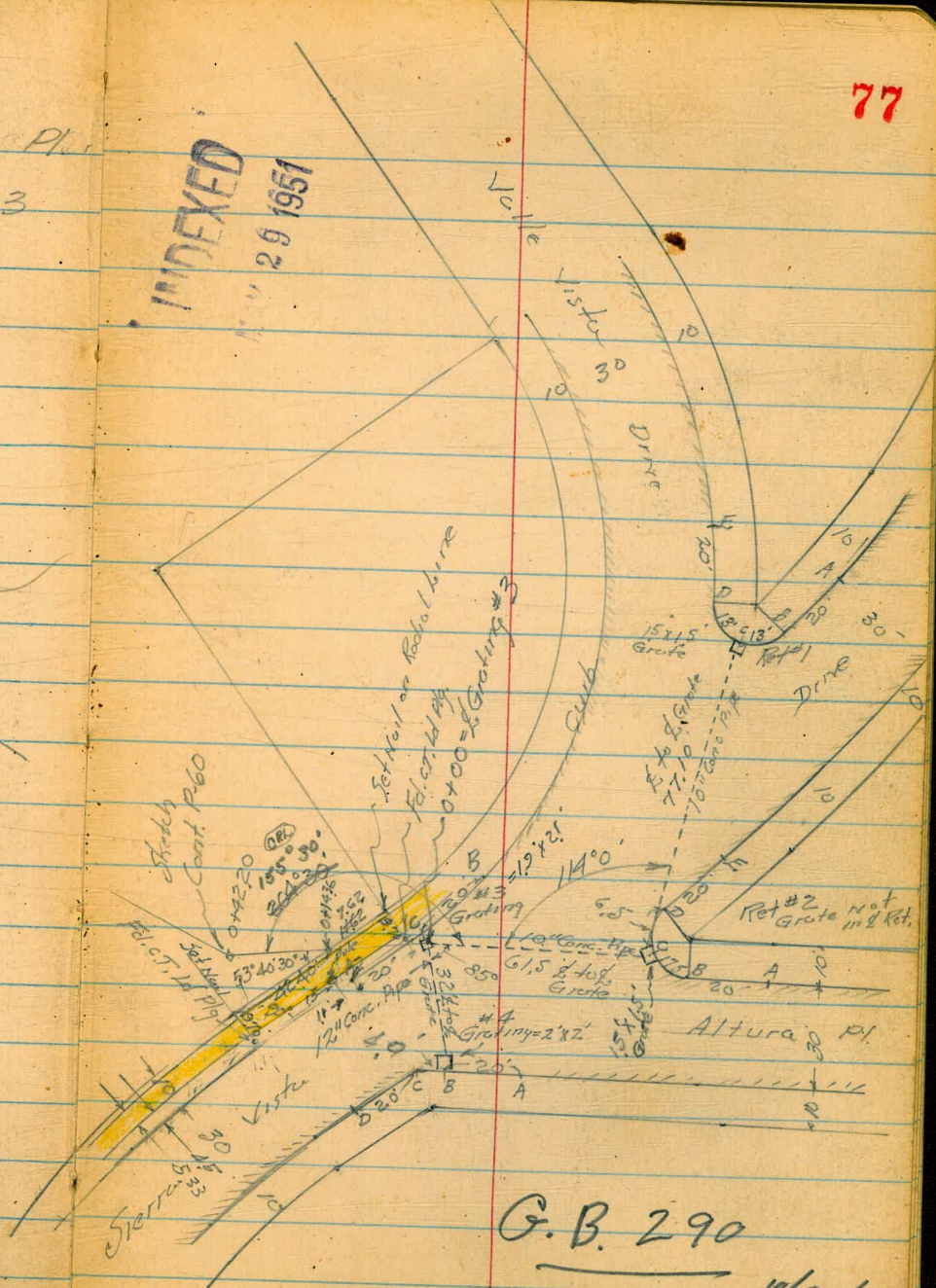


0 + 42.20 = A RT.

0 + 14.36 = P.O.T. = Int. Prop. Line

0 + 00 = L. Grading #3

Set Hub.



77

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NOV 29 1951

G.B. 290  
P 68 10/24/52



Sierra Vista - Drain

78

Ret # 3

261.12	261.84	260.71	261.64	258.13	258.08
654	582	695	602	953	2,58
A	A	C	C	C	C
Gut.	cb	on Grating	cb	invert 12" from #4 Grating	10" invert from #2 Ret.

Return No 4 - SE

262.74	263.31	261.96	262.78	259.26	262.08	262.71	262.70	262.94
492	435	570	488	770	558	495	536	472
A	A	B	B	B	C	C	D	D
Gut	cb	on Grating	cb	on Invert. = Bottom Inlet Box.	Gut.	cb	Gut	cb

Return No 2 Cont.

262.39	262.39	261.74	262.34	528	473	492	432
D	D	E	E	Gut	cb	Gut	cb

Ret # 2

262.94	263.42	262.32	262.77	261.99	262.73	260.68	260.72
472	424	534	489	567	423	628	624
A	A	B	B	C	C	on Flow Inlet Box	C
Gut.	cb.	Gut.	cb.	on Grating	cb	10" Pipe Invert.	cb

Ret # 1 Cont

264.28	264.84	263.35	263.80	262.88	263.51	261.36	263.07	263.67
338	282	431	386	478	418	630	489	399
A	A	B	B	C	C	inlet Box	D	D
Gut	cb	Gut	cb	Gut Grating	cb		Gut	cb

Return No 1

TR	487	267.66	582	262.79
	167	268.61		266.94

B.M. NE. BP. Fort Stockton a Sierra Vista

Sierra Vista Drain

79

0+61.5 = $\frac{1}{2}$ Grade #3	6.95	260.71
0+50.	6.00	261.66
0+25	4.93	262.73
0+20	4.87	262.79
0+05	5.22	262.44
0+77 = 0+00 Ahead = $\frac{1}{2}$ Grating No 2		
0+62	4.90	262.76
0+45	4.44	263.22
0+30	4.25	263.41
0+15.	4.21	263.45
0+00 = $\frac{1}{2}$ Grating No 1	4.78	262.88

Levels from  $\frac{1}{2}$  15x15 Grating Return #1

Ret # 3 Cont.

267.66

257.96	761.08	261.72
9.70	6.58	5.94
c	8	8
on 12" Invert	on	on $\phi$ .
outlet to Canyon	out	

267.66

## Sierra Vista Drain

80

Cont. P-73

TP 044	2499/	1786	249.47
0+49 Ground.		140	253.3
0+48.1 on Wall Fdn		497	262.36
0+42.2 Δ Pt. on Hub		475	262.58
0+14 = West Edge Walk		549	261.85
0+06.86 = Walk		576	261.67
0+01.5 Top cb		570	261.63
0+01.5 Gut		669	260.64
0+00 = Gate #3		661	260.72

267.33

B.P. N.W. Sierra - Valle Vista (No Record in My Book)

TP 3.51	267.33	384	263.82
0+32 = Gate #3		625	260.11
0+24		582	261.84
0+14		515	262.51
0+10		512	262.54
0+00 = Gate #4		526	262.40

267.66

Reduced by backhead  
6-13-51

TP chk starting B.M. P-78

B.M. B.P. N.W. Sierra Vista - Valle Vista

TP 4.71	268.51	413	263.80
TP 12.21	267.93	036	255.02
TP 12.89	255.38	000	242.49
TP 13.04	242.49	025	229.45

229.70

Cont. from P-73

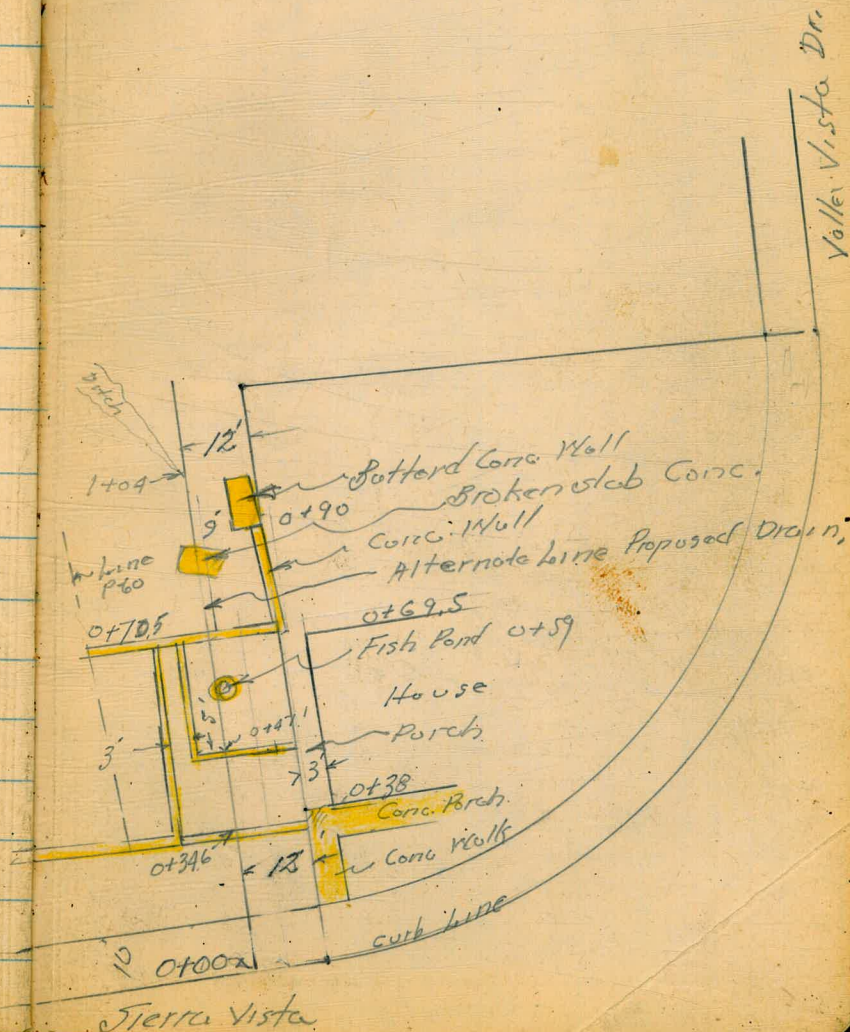
8) Alternote line

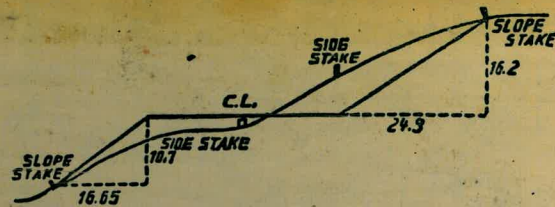
Proposed Drain  
Sierra Vista.

Orig. line P-60

Walker  
Pope  
Clark  
Huffman  
6-15-51

T.P.	1+18 10' # Ditch.	405	225.4
OT	1+18 10' Rt	289	237.5
OT	1+18	339	232.5
OT	(1+02 P-73 chk steel Pipe Invert	303	236.1
OT	16' Rt	225	241.9
OT	1+04 5' Rt	285	237.9
OT	1+04 = Int. Hd of Ditch	335	232.9
OT	0+86 (10' Rt.)	252	241.2
OT	0+86	287	237.7
OT	0+74 Ground at Wall	250	241.4
	0+70.5 = Int 10" Wall	198	246.6
	0+64 Ground	168	249.6
B.P.	6" Conc. 2'R = Hd = 131	253.3	
T.P.	0+59.8 = E 8 1/2" dia. Fish Pond	2' Rt = 9. Pond	
	0+56.8		
0	0+48 Ground	129	253.5
0	0+47.1 = West edge 8" Conc. Wall	102	256.2
	5' Lt 24" Date Palm		
0	0+36 = 8' Rt. 36" Date Palm		
	0+35 Ground	90	257.4
0	0+34.6 = West edge	425	262.10
OT	0+00 on Cb	455	261.80
	West		
	0+00 = Cb. Sierra Vista. Gutter = 5.34	261.01	
	B.M. on Hub 3.77	266.35	262.58
	0+12.2 P-80		





**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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