

2081

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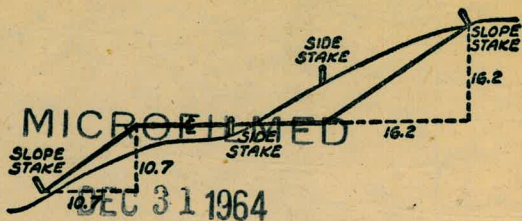
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TRANSIT BOOK

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DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

|    | 0     | .1    | .2    | .3    | .4    | .5    | .6    | .7    | .8    | .9    |    |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0  | 0.00  | 0.10  | 0.20  | 0.30  | 0.40  | 0.50  | 0.60  | 0.70  | 0.80  | 0.90  | 0  |
| 1  | 1.00  | 1.10  | 1.20  | 1.30  | 1.40  | 1.50  | 1.60  | 1.70  | 1.80  | 1.90  | 1  |
| 2  | 2.00  | 2.10  | 2.20  | 2.30  | 2.40  | 2.50  | 2.60  | 2.70  | 2.80  | 2.90  | 2  |
| 3  | 3.00  | 3.10  | 3.20  | 3.30  | 3.40  | 3.50  | 3.60  | 3.70  | 3.80  | 3.90  | 3  |
| 4  | 4.00  | 4.10  | 4.20  | 4.30  | 4.40  | 4.50  | 4.60  | 4.70  | 4.80  | 4.90  | 4  |
| 5  | 5.00  | 5.10  | 5.20  | 5.30  | 5.40  | 5.50  | 5.60  | 5.70  | 5.80  | 5.90  | 5  |
| 6  | 6.00  | 6.10  | 6.20  | 6.30  | 6.40  | 6.50  | 6.60  | 6.70  | 6.80  | 6.90  | 6  |
| 7  | 7.00  | 7.10  | 7.20  | 7.30  | 7.40  | 7.50  | 7.60  | 7.70  | 7.80  | 7.90  | 7  |
| 8  | 8.00  | 8.10  | 8.20  | 8.30  | 8.40  | 8.50  | 8.60  | 8.70  | 8.80  | 8.90  | 8  |
| 9  | 9.00  | 9.10  | 9.20  | 9.30  | 9.40  | 9.50  | 9.60  | 9.70  | 9.80  | 9.90  | 9  |
| 10 | 10.00 | 10.10 | 10.20 | 10.30 | 10.40 | 10.50 | 10.60 | 10.70 | 10.80 | 10.90 | 10 |
| 11 | 11.00 | 11.10 | 11.20 | 11.30 | 11.40 | 11.50 | 11.60 | 11.70 | 11.80 | 11.90 | 11 |
| 12 | 12.00 | 12.10 | 12.20 | 12.30 | 12.40 | 12.50 | 12.60 | 12.70 | 12.80 | 12.90 | 12 |
| 13 | 13.00 | 13.10 | 13.20 | 13.30 | 13.40 | 13.50 | 13.60 | 13.70 | 13.80 | 13.90 | 13 |
| 14 | 14.00 | 14.10 | 14.20 | 14.30 | 14.40 | 14.50 | 14.60 | 14.70 | 14.80 | 14.90 | 14 |
| 15 | 15.00 | 15.10 | 15.20 | 15.30 | 15.40 | 15.50 | 15.60 | 15.70 | 15.80 | 15.90 | 15 |
| 16 | 16.00 | 16.10 | 16.20 | 16.30 | 16.40 | 16.50 | 16.60 | 16.70 | 16.80 | 16.90 | 16 |
| 17 | 17.00 | 17.10 | 17.20 | 17.30 | 17.40 | 17.50 | 17.60 | 17.70 | 17.80 | 17.90 | 17 |
| 18 | 18.00 | 18.10 | 18.20 | 18.30 | 18.40 | 18.50 | 18.60 | 18.70 | 18.80 | 18.90 | 18 |
| 19 | 19.00 | 19.10 | 19.20 | 19.30 | 19.40 | 19.50 | 19.60 | 19.70 | 19.80 | 19.90 | 19 |
| 20 | 20.00 | 20.10 | 20.20 | 20.30 | 20.40 | 20.50 | 20.60 | 20.70 | 20.80 | 20.90 | 20 |
| 21 | 21.00 | 21.10 | 21.20 | 21.30 | 21.40 | 21.50 | 21.60 | 21.70 | 21.80 | 21.90 | 21 |
| 22 | 22.00 | 22.10 | 22.20 | 22.30 | 22.40 | 22.50 | 22.60 | 22.70 | 22.80 | 22.90 | 22 |
| 23 | 23.00 | 23.10 | 23.20 | 23.30 | 23.40 | 23.50 | 23.60 | 23.70 | 23.80 | 23.90 | 23 |
| 24 | 24.00 | 24.10 | 24.20 | 24.30 | 24.40 | 24.50 | 24.60 | 24.70 | 24.80 | 24.90 | 24 |
| 25 | 25.00 | 25.10 | 25.20 | 25.30 | 25.40 | 25.50 | 25.60 | 25.70 | 25.80 | 25.90 | 25 |
| 26 | 26.00 | 26.10 | 26.20 | 26.30 | 26.40 | 26.50 | 26.60 | 26.70 | 26.80 | 26.90 | 26 |
| 27 | 27.00 | 27.10 | 27.20 | 27.30 | 27.40 | 27.50 | 27.60 | 27.70 | 27.80 | 27.90 | 27 |
| 28 | 28.00 | 28.10 | 28.20 | 28.30 | 28.40 | 28.50 | 28.60 | 28.70 | 28.80 | 28.90 | 28 |
| 29 | 29.00 | 29.10 | 29.20 | 29.30 | 29.40 | 29.50 | 29.60 | 29.70 | 29.80 | 29.90 | 29 |
| 30 | 30.00 | 30.10 | 30.20 | 30.30 | 30.40 | 30.50 | 30.60 | 30.70 | 30.80 | 30.90 | 30 |
| 31 | 31.00 | 31.10 | 31.20 | 31.30 | 31.40 | 31.50 | 31.60 | 31.70 | 31.80 | 31.90 | 31 |
| 32 | 32.00 | 32.10 | 32.20 | 32.30 | 32.40 | 32.50 | 32.60 | 32.70 | 32.80 | 32.90 | 32 |
| 33 | 33.00 | 33.10 | 33.20 | 33.30 | 33.40 | 33.50 | 33.60 | 33.70 | 33.80 | 33.90 | 33 |
| 34 | 34.00 | 34.10 | 34.20 | 34.30 | 34.40 | 34.50 | 34.60 | 34.70 | 34.80 | 34.90 | 34 |
| 35 | 35.00 | 35.10 | 35.20 | 35.30 | 35.40 | 35.50 | 35.60 | 35.70 | 35.80 | 35.90 | 35 |
| 36 | 36.00 | 36.10 | 36.20 | 36.30 | 36.40 | 36.50 | 36.60 | 36.70 | 36.80 | 36.90 | 36 |
| 37 | 37.00 | 37.10 | 37.20 | 37.30 | 37.40 | 37.50 | 37.60 | 37.70 | 37.80 | 37.90 | 37 |
| 38 | 38.00 | 38.10 | 38.20 | 38.30 | 38.40 | 38.50 | 38.60 | 38.70 | 38.80 | 38.90 | 38 |
| 39 | 39.00 | 39.10 | 39.20 | 39.30 | 39.40 | 39.50 | 39.60 | 39.70 | 39.80 | 39.90 | 39 |
| 40 | 40.00 | 40.10 | 40.20 | 40.30 | 40.40 | 40.50 | 40.60 | 40.70 | 40.80 | 40.90 | 40 |
| 41 | 41.00 | 41.10 | 41.20 | 41.30 | 41.40 | 41.50 | 41.60 | 41.70 | 41.80 | 41.90 | 41 |
| 42 | 42.00 | 42.10 | 42.20 | 42.30 | 42.40 | 42.50 | 42.60 | 42.70 | 42.80 | 42.90 | 42 |
| 43 | 43.00 | 43.10 | 43.20 | 43.30 | 43.40 | 43.50 | 43.60 | 43.70 | 43.80 | 43.90 | 43 |
| 44 | 44.00 | 44.10 | 44.20 | 44.30 | 44.40 | 44.50 | 44.60 | 44.70 | 44.80 | 44.90 | 44 |
| 45 | 45.00 | 45.10 | 45.20 | 45.30 | 45.40 | 45.50 | 45.60 | 45.70 | 45.80 | 45.90 | 45 |
| 46 | 46.00 | 46.10 | 46.20 | 46.30 | 46.40 | 46.50 | 46.60 | 46.70 | 46.80 | 46.90 | 46 |
| 47 | 47.00 | 47.10 | 47.20 | 47.30 | 47.40 | 47.50 | 47.60 | 47.70 | 47.80 | 47.90 | 47 |
| 48 | 48.00 | 48.10 | 48.20 | 48.30 | 48.40 | 48.50 | 48.60 | 48.70 | 48.80 | 48.90 | 48 |
| 49 | 49.00 | 49.10 | 49.20 | 49.30 | 49.40 | 49.50 | 49.60 | 49.70 | 49.80 | 49.90 | 49 |
| 50 | 50.00 | 50.10 | 50.20 | 50.30 | 50.40 | 50.50 | 50.60 | 50.70 | 50.80 | 50.90 | 50 |

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

| Central Angle | DEGREE OF CURVE |      |      |      |      |      |      |      |      |      |      |      |      |      |
|---------------|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
|               | 5°              | 10°  | 15°  | 20°  | 25°  | 30°  | 35°  | 40°  | 45°  | 50°  | 55°  | 60°  | 65°  | 70°  |
| 10°           | .03             | .06  | .09  | .13  | .16  | .19  | .22  | .25  | .28  | .31  | .34  | .38  | .42  | .46  |
| 15°           | .04             | .10  | .14  | .19  | .24  | .29  | .34  | .39  | .45  | .51  | .53  | .58  | .63  | .68  |
| 20°           | .06             | .13  | .19  | .26  | .32  | .39  | .45  | .51  | .58  | .65  | .72  | .79  | .84  | .90  |
| 25°           | .08             | .16  | .24  | .33  | .40  | .49  | .58  | .67  | .75  | .83  | .90  | .99  | 1.06 | 1.14 |
| 30°           | .10             | .19  | .29  | .39  | .49  | .59  | .69  | .79  | .89  | .99  | 1.09 | 1.20 | 1.29 | 1.39 |
| 35°           | .11             | .22  | .34  | .47  | .58  | .69  | .79  | .81  | .92  | 1.04 | 1.29 | 1.42 | 1.54 | 1.68 |
| 40°           | .13             | .26  | .40  | .53  | .67  | .80  | .93  | 1.06 | 1.20 | 1.34 | 1.49 | 1.64 | 1.79 | 1.94 |
| 45°           | .15             | .30  | .44  | .60  | .76  | .91  | 1.06 | 1.21 | 1.37 | 1.52 | 1.70 | 1.87 | 2.04 | 2.21 |
| 50°           | .17             | .34  | .51  | .68  | .85  | 1.02 | 1.19 | 1.36 | 1.54 | 1.72 | 1.91 | 2.10 | 2.29 | 2.48 |
| 55°           | .19             | .38  | .57  | .76  | .95  | 1.14 | 1.32 | 1.52 | 1.72 | 1.92 | 2.14 | 2.35 | 2.56 | 2.77 |
| 60°           | .21             | .42  | .63  | .84  | 1.05 | 1.27 | 1.49 | 1.71 | 1.94 | 2.17 | 2.38 | 2.60 | 2.83 | 3.07 |
| 65°           | .23             | .46  | .69  | .93  | 1.16 | 1.40 | 1.64 | 1.88 | 2.13 | 2.38 | 2.63 | 2.88 | 3.13 | 3.39 |
| 70°           | .25             | .51  | .76  | 1.02 | 1.28 | 1.54 | 1.80 | 2.06 | 2.33 | 2.60 | 2.88 | 3.16 | 3.44 | 3.72 |
| 75°           | .27             | .56  | .83  | 1.12 | 1.40 | 1.69 | 1.98 | 2.27 | 2.57 | 2.87 | 3.16 | 3.47 | 3.78 | 4.09 |
| 80°           | .30             | .61  | 1.01 | 1.22 | 1.53 | 1.84 | 2.15 | 2.46 | 2.78 | 3.10 | 3.44 | 3.78 | 4.12 | 4.46 |
| 85°           | .33             | .66  | 1.00 | 1.33 | 1.68 | 2.02 | 2.36 | 2.70 | 3.05 | 3.40 | 3.77 | 4.14 | 4.55 | 4.89 |
| 90°           | .36             | .72  | 1.09 | 1.45 | 1.83 | 2.20 | 2.57 | 2.94 | 3.32 | 3.70 | 4.10 | 4.50 | 4.91 | 5.32 |
| 95°           | .39             | .79  | 1.19 | 1.55 | 2.00 | 2.40 | 2.80 | 3.20 | 3.61 | 4.02 | 4.40 | 4.98 | 5.38 | 5.83 |
| 100°          | .43             | .86  | 1.30 | 1.74 | 2.18 | 2.62 | 3.06 | 3.50 | 3.95 | 4.40 | 4.88 | 5.37 | 5.85 | 6.34 |
| 110°          | .51             | 1.03 | 1.56 | 2.08 | 2.61 | 3.14 | 3.67 | 4.21 | 4.76 | 5.31 | 5.86 | 6.43 | 7.01 | 7.60 |
| 120°          | .62             | 1.25 | 1.93 | 2.52 | 3.16 | 3.81 | 4.45 | 5.11 | 5.77 | 6.44 | 7.12 | 7.80 | 8.50 | 9.22 |

FOR EXTERNALS ADD

| Central Angle | DEGREE OF CURVE |      |      |      |      |      |      |      |      |      |      |      |      |      |
|---------------|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
|               | 5°              | 10°  | 15°  | 20°  | 25°  | 30°  | 35°  | 40°  | 45°  | 50°  | 55°  | 60°  | 65°  | 70°  |
| 10°           | .001            | .003 | .004 | .006 | .007 | .008 | .009 | .011 | .012 | .014 | .015 | .017 | .018 | .020 |
| 15°           | .003            | .007 | .010 | .014 | .018 | .023 | .027 | .029 | .032 | .035 | .039 | .043 | .047 | .051 |
| 20°           | .006            | .011 | .017 | .022 | .028 | .034 | .038 | .045 | .051 | .057 | .063 | .070 | .076 | .083 |
| 25°           | .009            | .018 | .027 | .036 | .046 | .056 | .065 | .074 | .083 | .093 | .106 | .120 | .127 | .135 |
| 30°           | .013            | .025 | .038 | .051 | .065 | .078 | .090 | .103 | .116 | .129 | .149 | .170 | .179 | .188 |
| 35°           | .018            | .035 | .054 | .072 | .086 | .109 | .131 | .153 | .175 | .197 | .213 | .230 | .247 | .264 |
| 40°           | .023            | .046 | .070 | .093 | .117 | .141 | .172 | .203 | .234 | .265 | .277 | .290 | .315 | .341 |
| 45°           | .030            | .060 | .093 | .119 | .153 | .184 | .216 | .254 | .289 | .325 | .351 | .378 | .411 | .445 |
| 50°           | .037            | .075 | .116 | .151 | .189 | .227 | .266 | .305 | .345 | .384 | .425 | .467 | .508 | .550 |
| 55°           | .046            | .093 | .142 | .188 | .236 | .283 | .332 | .381 | .420 | .479 | .530 | .582 | .641 | .700 |
| 60°           | .056            | .112 | .168 | .225 | .283 | .340 | .398 | .457 | .516 | .575 | .636 | .697 | .774 | .851 |
| 65°           | .067            | .135 | .204 | .273 | .343 | .412 | .483 | .554 | .625 | .697 | .771 | .845 | .922 | 1.01 |
| 70°           | .080            | .159 | .240 | .321 | .403 | .485 | .568 | .652 | .735 | .819 | .906 | .994 | 1.08 | 1.17 |
| 75°           | .095            | .182 | .286 | .383 | .480 | .578 | .678 | .777 | .877 | .977 | 1.07 | 1.18 | 1.29 | 1.39 |
| 80°           | .110            | .220 | .332 | .445 | .558 | .671 | .787 | .903 | 1.02 | 1.13 | 1.25 | 1.38 | 1.50 | 1.62 |
| 85°           | .128            | .259 | .391 | .524 | .657 | .790 | .926 | 1.06 | 1.20 | 1.34 | 1.47 | 1.62 | 1.76 | 1.91 |
| 90°           | .149            | .299 | .450 | .603 | .756 | .910 | 1.07 | 1.22 | 1.38 | 1.54 | 1.70 | 1.87 | 2.03 | 2.20 |
| 95°           | .174            | .350 | .522 | .706 | .885 | 1.06 | 1.25 | 1.43 | 1.62 | 1.80 | 1.99 | 2.18 | 2.38 | 2.58 |
| 100°          | .200            | .401 | .604 | .809 | 1.01 | 1.22 | 1.43 | 1.64 | 1.85 | 2.06 | 2.28 | 2.50 | 2.73 | 2.96 |
| 110°          | .268            | .536 | .806 | 1.08 | 1.35 | 1.63 | 1.91 | 2.20 | 2.48 | 2.76 | 3.05 | 3.35 | 3.66 | 3.96 |
| 120°          | .360            | .721 | 1.08 | 1.45 | 1.82 | 2.19 | 2.57 | 2.95 | 3.33 | 3.72 | 4.11 | 4.50 | 4.91 | 5.32 |

Page

- 2-11- X-Sect. Fortuna + Roosevelt - Kendall to Lamont
- x 150 49 + 49
- 43-47 66. Elev. Orchard. Catalina Ely
- 55 X-Sec. Gladiola - Pendleton to Quincy
- 12 X-Sec. Alley BIK 27 O.B
- 29 X-Sec. Quincy - Chalcedony to Wilbur
- 48 Orchard Avenue - Levels on new curbs  
from N.W'ly line Loma Hands Park
- 38 X-Sec. Loring - Lamont to E'ly  
Termination
- 22 X-Wilbur Ave. establishing Grade
- 29 X-Sec. Quincy, Chalcedony to Wilbur,  
Establishing grade
- 35 X-Sec. Gladiola, Pendleton to Quincy,  
Establishing Grade
- 38 X-Sec. Loring St. - Lamont to  
E'ly termination
- 43 Orchard - Catalina E'ly,  
curb elevations
- 48 Orchard, Levels on new curbs  
from N.W'ly line Loma hands Park
- 50 X-Sec. Alley BIK. 195,  
City Heights
- 62. X-Sec Alley <sup>Blk 2</sup> Ocean Beach
- 74 - X Sec. A St - 17 to 18th  
survey lots 37 + 38 BIK 38
- 79. Ocean Beach



X-Sect. Fortuna - Kendall to Lamont.  
75' st. Graded - No cbs. or walks

# 49 03

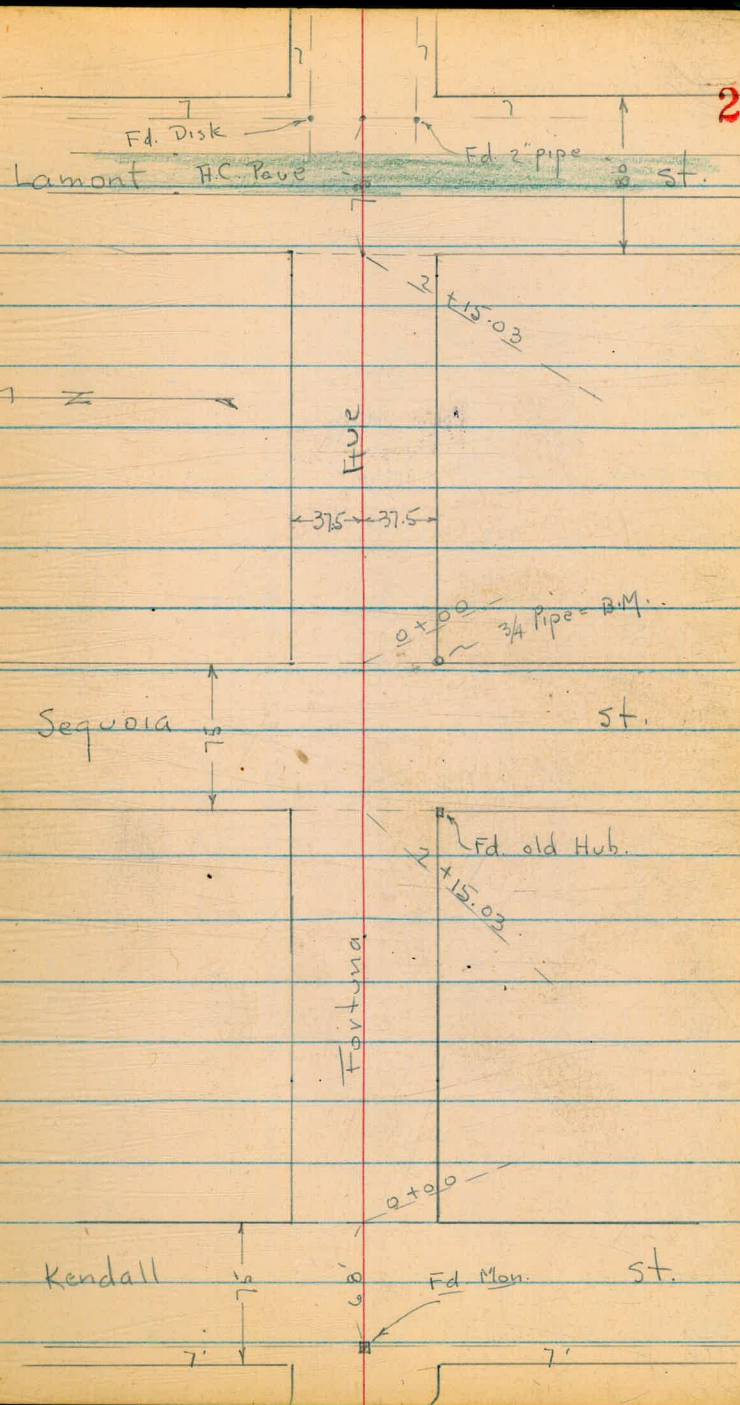
W.O. 31582

INDEXED  
W.K.  
MAR 14 1950

2-21-50

Osborne  
Hardin  
Hatch  
Shepard

Reduced by  
Lacey  
3-16-50













2+15.03 = W.L. Lamont.

2+13- 28.8 Rt. = ± Tel. pole # 500268 H

2+02- 22.4 Lt. = ± 4.5' Palm

1+90- 22.5 Rt. = ± Guy Pole

1+93- 37.3 Lt. = ± 3' Conc. walk

1+87- 22.4 Lt. = ± 4.5' Palm

1+80

1+73- 22.3 Lt. = ± 47" Palm

1+58- 22.3 Lt. = ± 4' Palm

1+43- 22.5 Lt. = ± 5' Palm

1+40

1+29- 22.8 Lt. = ± 8" Cypress

1+21- 37.9 Lt. = ± Sing. Gar. - Conc. floor

1+07- 02 Lt. = ± Sewer M.H. <sup>23.76</sup> 5.65 on Rim ?

1+01- 36.7 Rt. = ± Tel. pole # 1875

1+00

0+83- 37.5 Lt. = ± <sup>Conc.</sup> 7.5' Apron to Sing. Gar.

0+76- 28.4 Rt. = ± Tel. pole # 500269 H

0+50- 37.3 Lt. = wly. of 3' Conc. walk

|            |              |        |        |        |        |            |
|------------|--------------|--------|--------|--------|--------|------------|
| 6.5        | 7.1          | 7.3    | 8.1    | 8.2    | 8.2    | 8.0        |
| 45         | 37.5         | 20     |        | 20     | 37.5   | 50         |
| 5.77       | 6.04         |        |        |        |        |            |
| 50         | 37.3         |        |        |        |        |            |
| 5.23.5     | 6.23.0       | 6.22.8 | 7.22.4 | 6.22.6 | 7.22.2 | 7.22.3     |
| 45         | 37.5         | 20     | 0      | 20     | 37.5   | 41         |
|            |              |        |        |        |        | along Gar. |
| 5.24.4     | 5.24.1       | 5.23.9 | 6.23.0 | 6.23.0 | 6.22.9 | 6.23.1     |
| 45         | 37.5         | 20     | 4      | 20     | 37.5   | 45         |
| 4.24.50    |              |        |        |        |        |            |
| 4.91       |              |        |        |        |        |            |
|            | 37.9 = floor |        |        |        |        |            |
| 4.25.3     | 4.25.3       | 4.25.0 | 5.23.9 | 5.23.7 | 5.24.0 | 6.23.4     |
| 45         | 37.5         | 20     | 5      | 20     | 37.5   | 45         |
| 26.34      | 26.32        |        |        |        |        |            |
| 42.5       | 37.5 = apron |        |        |        |        |            |
| 42.5 floor |              |        |        |        |        |            |
| 3.07       | 3.18         | 3.24   | 4.1    | 4.0    | 4.1    | 3.6        |
| 48.7       | 37.3         | 20     | 4.1    | 20     | 37.5   | 45         |
| steps      | walk         |        | 29.41  |        |        |            |







X-Sept. Roosevelt - from Kendall to  
Lamont. - 75' st. Graded - No cbs. or walks

# 49 03

**INDEXED** 2-23-50

W.O. 31582

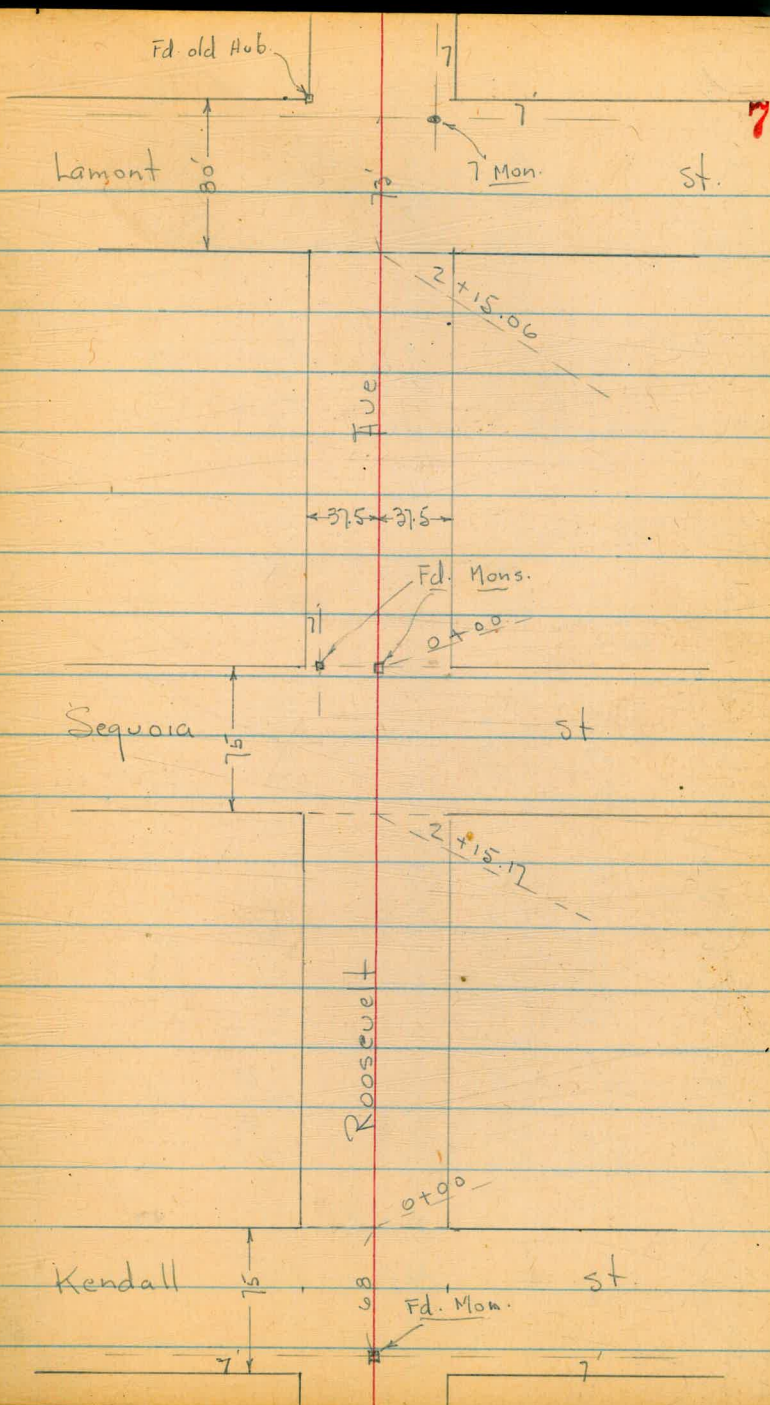
W.K.  
MAR 14 1950

7.0

Levels - P. 8

See P. 2 for Fortuna

Reduced by  
Jimmy  
3-16-50





X-Sect Roosevelt - sketch - P-7.

0+50 = on 14' Conc. Dr. on Lt.

0+00 = F.L. of Kendal

0-20

0-37.5 =  $\Phi$

0-55

0-75 = w.L. Kendall

B.M. 132 28.04 3.46 24.58  
26.72

|       | It.   | It.  | It.   | It.  | It.  | 8    |
|-------|-------|------|-------|------|------|------|
| 28.18 | 26.93 | 25.7 | 25.4  | 25.4 | 26.1 | 28.2 |
| 2.50  | 3.75  | 5.0  | 5     | 5.3  | 4.6  | 2.5  |
| 54    | 37.4  | 20   | 3     | 20   | 37.5 | 45   |
| floor | Dr.   |      |       |      |      |      |
| Gar.  |       |      |       |      |      |      |
| 270   | 272   | 26.4 | 25.8  | 26.0 | 27.2 | 273  |
| 37    | 35    | 4.3  | 4.9   | 4.7  | 3.5  | 3.4  |
| 80    | 37.5  | 20   | 20    | 20   | 37.5 | 80   |
| 26.1  | 26.2  | 26.3 | 26.1  | 26.2 | 26.2 | 25.9 |
| 4.6   | 4.5   | 4.4  | 4.6   | 4.5  | 4.5  | 4.8  |
| 80    | 37.5  | 20   | 20    | 20   | 37.5 | 80   |
| 26.2  | 26.1  | 26.2 | 26.3  | 26.4 | 26.4 | 26.1 |
| 4.5   | 4.6   | 4.5  | 4.4   | 4.3  | 4.3  | 4.6  |
| 80    | 37.5  | 20   | 20    | 20   | 37.5 | 80   |
| 26.4  | 26.3  | 26.1 | 26.3  | 26.1 | 26.1 | 26.1 |
| 4.3   | 4.4   | 4.6  | 4.4   | 4.6  | 4.6  | 4.6  |
| 80    | 37.5  | 20   | 20    | 20   | 37.5 | 80   |
| 272   | 272   | 26.8 | 26.4  | 27.0 | 27.5 | 27.9 |
| 3.5   | 3.5   | 3.9  | 4.3   | 3.7  | 3.2  | 2.5  |
| 80    | 37.5  | 20   | 20    | 20   | 37.5 | 80   |
|       |       |      | 30.68 |      |      |      |

N.E. 7 Mon. Sequoia + Roosevelt.  
Pipe S.E. Sequoia + Fortuna  
See P. 3







20' E. of w.L.

2+15.06 = w.L. Lamont

2+12- 27.7' Rt. = P. pole # 1899

1+80

1+60 - 37.4' Lt. = Conc. apron to Sing. Gear

1+40

1+08 - 0.6' Lt. = Sewer MH

T.P. 2.04 26.63 7.09 23.59

1+00 = w.L. Alley.

0+98 - 27.5' Rt. = P. pole # 1875

0+70 - 36.5' Lt. = 3.5' Conc. walk

0+50

|     |      |     |     |     |      |     |
|-----|------|-----|-----|-----|------|-----|
| 4.2 | 4.1  | 5.1 | 5.1 | 5.3 | 4.7  | 5.0 |
| 50  | 37.5 | 17  | 19  | 20  | 37.5 | 50  |

|     |      |     |     |     |     |      |     |
|-----|------|-----|-----|-----|-----|------|-----|
| 3.7 | 3.8  | 4.3 | 4.7 | 4.8 | 3.8 | 4.1  | 4.0 |
| 45  | 37.5 | 20  | .12 | 20  | 25  | 37.5 | 45  |

|     |      |     |     |     |     |      |     |
|-----|------|-----|-----|-----|-----|------|-----|
| 3.5 | 3.6  | 3.5 | 4.6 | 4.2 | 3.6 | 3.7  | 3.9 |
| 45  | 37.5 | 16  | 11  | 20  | 25  | 37.5 | 45  |

|     |      |     |     |     |     |     |      |
|-----|------|-----|-----|-----|-----|-----|------|
| 2.9 | 2.9  | 3.1 | 4.0 | 3.9 | 3.5 | 2.9 | 3.0  |
| 45  | 37.5 | 25  | 12  | 30  | 20  | 25  | 37.5 |

|     |      |     |     |     |     |      |     |
|-----|------|-----|-----|-----|-----|------|-----|
| 2.7 | 2.7  | 2.1 | 2.6 | 2.5 | 2.3 | 2.3  | 2.6 |
| 45  | 37.5 | 25  | 12  | 20  | 25  | 37.5 | 45  |

|     |      |     |     |     |      |     |
|-----|------|-----|-----|-----|------|-----|
| 5.7 | 6.5  | 6.4 | 7.3 | 5.9 | 6.3  | 6.4 |
| 75  | 37.5 | 25  | 12  | 20  | 37.5 | 75  |

|     |      |     |     |     |     |      |     |
|-----|------|-----|-----|-----|-----|------|-----|
| 5.7 | 5.6  | 5.7 | 5.7 | 6.6 | 5.7 | 5.6  | 5.7 |
| 45  | 37.5 | 18  | 10  | 30  | 20  | 37.5 | 45  |

10



Soil Sample at E.L. Sequoia

vail in Pole  
check B.M. - P-6 4.22 2241 2240

80' E. = E.L. of Lamont = end

68' E - 27.9' Rt. =  $\Phi$  Guy Pole # 461134 H  
 $\Phi$  of 20' Return on N.E. Cor. - No walks

60' E. = Line of curb in to N.

50' E. = Fly. of Pav

40' E. =  $\Phi$

30' E. = Wly. of AC Pav Strip

|        |       |        |       |       |       |        |       |      |
|--------|-------|--------|-------|-------|-------|--------|-------|------|
| 4.9    | 5.1   | 5.4    | 5.7   | 5.2   | 5.6   | 5.3    | 5.4   | 5.5  |
| 50     | 37.5  | 20     | 20    | 14    | 20    | 20     | 37.5  | 50   |
| 21.7   | 21.5  | 21.29  | 20.9  | 21.4  | 21.0  | 21.3   | 21.2  | 21.1 |
| 5.70   | 6.205 | 5.4    | 5.0   | 5.7   | 5.214 | 5.4    | 5.2   | 5.7  |
| 80     | 9.4   | 40     | 40    | 20    | 20    | 20     | 37.5  | 80   |
| Top    | 9.4   | Top=PC | 9.4   | 20    | 20    | 20     | 37.5  | 80   |
| 5.2093 | 6.205 | 21.19  | 20.6  | 20.9  | 21.4  | 21.2   | 21.4  | 20.9 |
| 80     | 9.4   | 40     | 40    | 20    | 20    | 20     | 37.5  | 80   |
| Top    | 9.4   | Top=PC | 9.4   | 20    | 20    | 20     | 37.5  | 80   |
| 5.2101 | 5.50  | 21.13  | 21.35 | 21.44 | 21.34 | 21.17  | 21.63 |      |
| 80     | 37.5  | 20     | 20    | 20    | 20    | 37.5   | 80    |      |
| 5.2135 | 21.19 | 21.64  | 21.69 | 21.60 | 21.45 | 20.87  |       |      |
| 80     | 37.5  | 20     | 20    | 20    | 37.5  | 80     |       |      |
| 5.2111 | 5.44  | 21.30  | 21.29 | 21.23 | 21.03 | 20.53  |       |      |
| 80     | 37.5  | 20     | 20    | 20    | 37.5  | 80     |       |      |
| 5.228  | 5.14  | 4.99   | 4.94  | 5.03  | 5.18  | 5.76   |       |      |
| 80     | 37.5  | 20     | 20    | 20    | 37.5  | 80     |       |      |
| 5.2111 | 5.44  | 5.33   | 5.34  | 5.70  | 5.60  | 6.2053 |       |      |
| 80     | 37.5  | 20     | 20    | 20    | 37.5  | 80     |       |      |



KiSec. for grade Est.  
Alley BIK. 27 Ocean Beach

Sommermeier  
Bc99  
A1107  
Sherman

W.O. 25020  
5-22-50

INDEXED  
WR  
MAY 24 1950

- = Fd. L&T.
- = set nail in pave
- = Nail

Base = base of footing for walls

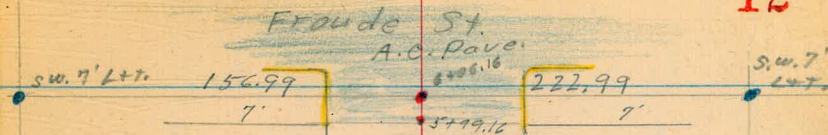
NOTE!

ALLEY CHECKED FOR NEW IMPROVEMENTS

6-28-51 NEW IMPROVEMENTS

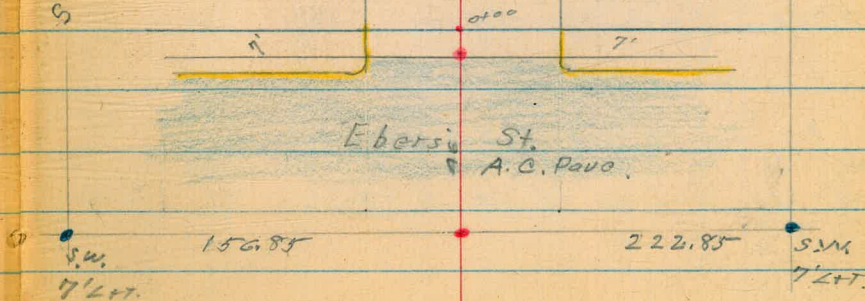
UNDER LINED IN GREEN

12



5'4" 7' line Cape May

5'4" 7' line Saratoga





0+50

42.6  
9.1  
30

43.6  
8.1  
10

43.9  
7.8

45.0  
6.7  
10

45.4  
6.3  
20

0+44 10' RT = end stucco house

44.8  
6.9  
10'  
Ord. at house

T.P. 8.02 51.72 0.71 43.70

51.72

10' RT = start stucco house.

0+14 9' RT = end conc. wall.

42.5  
1.8  
99  
Ord

42.0  
2.4  
99  
Base

43.3  
1.1  
99  
Top

42.6  
1.9  
10  
Ord at house

0+00 9' RT = start 7" wide conc. wall.

41.0  
3.4  
99  
Ord

40.9  
3.5  
99  
Base

42.0  
2.4  
99  
Top

10' LT  
9.9 RT = End alley cbs.

0+00 = End A.C. Pave.

40.86  
3.55  
10  
Cb.

40.79  
3.62  
10  
G

40.44  
3.97  
Pave

40.90  
3.51  
99  
G

41.36  
3.05  
99  
Cb

0-12 = Ely. Cb. line Ebers

39.87  
4.54  
60

39.20  
5.21  
60

40.81  
3.60  
12  
Cb.

40.13  
4.28  
12  
G

40.17  
4.24  
10

40.28  
4.13

40.53  
3.88  
10

40.66  
3.75  
12  
G

41.30  
3.11  
12  
Cb.

41.59  
2.82  
60  
G

42.25  
2.16  
60  
Cb

S.W.B.P.  
CapoMay 7.99 44.41 — 36.42  
Ebers

44.41



Alley BIK 2708

±

1+23 - 10<sup>2</sup> Rt. = end Bldg. on Conc. slab.

|                 |                 |    |
|-----------------|-----------------|----|
| 46.9            | 46.7            | 14 |
| 4.8             | 5.0             |    |
| 10 <sup>2</sup> | 10 <sup>2</sup> |    |
| End.            | Base            |    |

1+14 - 10<sup>5</sup> Rt. = Approx ± Bldg. & step up in conc. slab.

|                 |                 |                 |
|-----------------|-----------------|-----------------|
| 46.4            | 46.0            | 46.6            |
| 5.3             | 5.7             | 5.1             |
| 10 <sup>5</sup> | 10 <sup>5</sup> | 10 <sup>5</sup> |
|                 | Base to west    | Base to east    |

1+02 - 10<sup>8</sup> Rt. = start board & batt Bldg. on Conc. slab.

|                 |                 |
|-----------------|-----------------|
| 46.2            | 46.0            |
| 5.5             | 5.7             |
| 10 <sup>8</sup> | 10 <sup>8</sup> |
| End             | Base of slab.   |

1+00 - 8<sup>8</sup> RT CENTER POWER POLE# JPA 4680

|      |      |      |      |      |
|------|------|------|------|------|
| 44.8 | 45.9 | 45.5 | 46.2 | 46.7 |
| 6.9  | 5.8  | 6.2  | 5.5  | 5.0  |
| 30   | 10   |      | 10   | 30   |

0+96 12<sup>0</sup> Rt. = End apron to A Car. Gar.

|       |            |
|-------|------------|
| 46.24 | 46.26      |
| 5.48  | 5.40       |
| 12    | 15         |
| Apron | Car floor. |

0+80 ± Car. Bldgs.

|       |           |
|-------|-----------|
| 45.96 | 46.22     |
| 5.76  | 5.50      |
| 112   | 149       |
| Apron | Car Floor |

0+61 112 Rt. = start Conc. Apron to A Car. Gar.

|       |            |
|-------|------------|
| 45.71 | 46.22      |
| 6.01  | 5.50       |
| 112   | 149        |
| Apron | Car floor. |

51.72



1+76 - 10' Lt. = start shed on Conc. blocks

49.0

2.710'  
end,1+75 8.5 RT. & POLE # JPA 2660

48.86

2.8610'  
walk

1+74 - 10' Lt. = ± 3' Conc. walk

49.82

1.9015'  
Gar. floor

1+67 15' RT. = ± Sing Gar. Conc. floor.

48.4

3.310'  
end

1+64 10' Lt. = end frame Bldg. on Conc. Blocks

~~49.9~~~~1.90~~~~15'  
floor~~~~1+67 15' RT. = ± Sing Gar. Conc. floor~~

47.8

3.910'  
end

1+52 10' Lt. start Frame Bldg. on Conc. blocks.

47.1

4.6  
30

47.6

4.1  
10

47.6

4.1

48.4

3.3  
10

48.7

3.0  
30

1+50

51.72



2+31 - 12<sup>2</sup> Rt. = end Conc. apron to 3 car. Gar.

|                 |                 |
|-----------------|-----------------|
| 52.33           | 52.73           |
| <u>9.22</u>     | <u>8.82</u>     |
| 12 <sup>2</sup> | 20 <sup>2</sup> |
| Apron           | Gar. floor      |

2+03 = 12<sup>1</sup> Rt. = start Conc. apron to 3 car. <sup>Gar.</sup>

|                 |                 |
|-----------------|-----------------|
| 51.47           | 52.69           |
| <u>10.08</u>    | <u>8.86</u>     |
| 12 <sup>1</sup> | 20 <sup>1</sup> |
| Apron           | Gar. floor      |

2+00

|             |             |              |             |             |             |
|-------------|-------------|--------------|-------------|-------------|-------------|
| 49.9        | 50.2        | 50.3         | 50.7        | 50.1        | 51.0        |
| <u>11.7</u> | <u>11.4</u> | <u>11.3</u>  | <u>10.9</u> | <u>10.9</u> | <u>10.6</u> |
| 30          | 10          |              | 10          | 20          | 30          |
|             |             | <u>61.55</u> |             |             |             |

T.P. 10.08 61.55 0.25 51.47

1+9A - 13<sup>4</sup> Rt. = Apron to Sing. Gar.

|                 |                 |
|-----------------|-----------------|
| 50.42           | 50.46           |
| <u>1.30</u>     | <u>1.26</u>     |
| 13 <sup>4</sup> | 15 <sup>8</sup> |
| Conc. Apron     | Gar. Floor      |

1+93 - 15<sup>2</sup> Lt. = Sing. Gar. Conc. floor

|             |
|-------------|
| 49.67       |
| <u>2.05</u> |
| 15          |
| Gar. Floor  |

15<sup>8</sup> Rt. = Sing. Gar. Conc. Floor.

1+8A 10<sup>1</sup> Lt. = end shed

|            |                 |
|------------|-----------------|
| 49.4       | 50.38           |
| <u>2.3</u> | <u>1.34</u>     |
| 10         | 15 <sup>8</sup> |
| Gar.       | Gar. Floor      |

51.72



3+46 23 Lt = End Conc. Apron to sing Gar.

|                   |       |
|-------------------|-------|
| 61.5 <sup>3</sup> | 61.45 |
| 12.13             | 12.21 |
| 242               | 23    |
| Gar Floor         | Apron |

3+34 - 23 Lt = start Conc. Apron to Sing. Gar.

|           |       |       |
|-----------|-------|-------|
| 61.47     | 61.31 |       |
| 12.19     | 12.35 |       |
| 242       | 23    |       |
| Gar Floor | Apron | 73.66 |

T.P. 12.35 73.66 0.24 61.31

3+00 £ = ori Man hole

|      |      |             |      |      |
|------|------|-------------|------|------|
| 56.8 | 56.8 | 56.79       | 57.6 | 58.6 |
| 4.8  | 4.8  | 4.76        | 4.0  | 3.0  |
| 30   | 10   | ori<br>M.H. | 10   | 50   |

2+88 - 10<sup>2</sup> Lt. = end Conc. apron to double Gar.

|            |       |
|------------|-------|
| 55.13      | 55.60 |
| 582        | 5.95  |
| 182        | 102   |
| Gar. Floor | Apron |

2+75 8.9 PT. & POLE # JPA 4648

2+7A- 10<sup>3</sup> Lt. = start Conc. apron to double <sup>Gar.</sup>

|            |       |
|------------|-------|
| 55.69      | 55.29 |
| 586        | 626   |
| 182        | 102   |
| Gar. floor | Apron |

2+50

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 52.3 | 53.1 | 53.2 | 53.9 | 53.7 | 54.2 |
| 7.3  | 8.5  | 8.4  | 7.7  | 7.9  | 7.4  |
| 30   | 10   |      | 10   | 30   | 50   |

61.55



4+28 17<sup>2</sup> FT. CORNER DOUBLE GARAGE UNDER CONSTRUCTION, NO FLOOR YET. APPROX ELEV. FLOOR- 71.8

4+00  
 $\begin{array}{r} 66.4 \\ 7.3 \\ \hline 30 \end{array}$       $\begin{array}{r} 66.9 \\ 6.8 \\ \hline 10 \end{array}$       $\begin{array}{r} 66.5 \\ 7.2 \\ \hline 10 \end{array}$       $\begin{array}{r} 66.9 \\ 6.8 \\ \hline 10 \end{array}$       $\begin{array}{r} 68.0 \\ 5.7 \\ \hline 30 \end{array}$

3+75 8.5 FT. & POLE # JPAK36

3+74<sup>3</sup> 9<sup>2</sup> Ft. = ± 6" N.+S. Conc. wall.

$\begin{array}{r} 63.3 \\ 10.4 \\ 9 \\ \hline \text{End base} \end{array}$       $\begin{array}{r} 62.9 \\ 12.8 \\ 9.2 \\ \hline \text{base} \end{array}$       $\begin{array}{r} 64.9 \\ 14.8 \\ 9.2 \\ \hline \text{Top} \end{array}$

3+74 - 10<sup>5</sup> Ft. = end Conc. apron to double Gar.

$\begin{array}{r} 63.10 \\ 10.56 \\ 10.5 \\ \hline \text{Apron} \end{array}$       $\begin{array}{r} 63.14 \\ 10.52 \\ 18 \\ \hline \text{Gar. Floor} \end{array}$

3+54 - 10<sup>4</sup> Ft. = start. Conc. apron to double Gar.

$\begin{array}{r} 62.03 \\ 11.63 \\ 10.4 \\ \hline \text{Apron} \end{array}$       $\begin{array}{r} 63.14 \\ 10.52 \\ 18 \\ \hline \text{Gar. Floor} \end{array}$

3+52 - 10<sup>4</sup> Ft. = ± 3' wide. Conc. walk

$\begin{array}{r} 61.94 \\ 11.72 \\ 10.4 \\ \hline \end{array}$       $\begin{array}{r} 63.16 \\ 10.50 \\ 17 \\ \hline \end{array}$

3+50 - 10<sup>4</sup> Ft. = ± N.+S. Conc. wall. (8" wide)

$\begin{array}{r} 61.5 \\ 12.2 \\ 30 \end{array}$       $\begin{array}{r} 61.6 \\ 12.1 \\ 10 \end{array}$       $\begin{array}{r} 61.1 \\ 12.6 \\ 10 \end{array}$       $\begin{array}{r} 61.9 \\ 11.8 \\ 10 \end{array}$       $\begin{array}{r} 60.6 \\ 13.1 \\ 10.4 \\ \hline \text{Base} \end{array}$       $\begin{array}{r} 64.1 \\ 9.7 \\ 10.4 \\ \hline \text{top} \end{array}$

73.66



5+00

|                  |                  |                 |                  |                  |
|------------------|------------------|-----------------|------------------|------------------|
| 78 <sup>0</sup>  | 78 <sup>5</sup>  | 79 <sup>1</sup> | 77 <sup>9</sup>  | 79 <sup>4</sup>  |
| $\frac{8.3}{30}$ | $\frac{7.8}{10}$ | 6.6             | $\frac{8.4}{10}$ | $\frac{7.9}{30}$ |

4+99 - 10<sup>5</sup> Rt. = End frame shed.

77<sup>6</sup>  
 $\frac{8.7}{105}$   
 End

4+89 - 10<sup>5</sup> Rt. = start frame shed on <sup>blocks</sup> conc.

77<sup>0</sup>  
 $\frac{9.3}{105}$   
 End

4+74 8.5 RT. @ POLE # JPA 4622

86.27

T.P. 12.66 86.27 0.05 73.61

4+50

|                  |                  |                 |                  |                  |
|------------------|------------------|-----------------|------------------|------------------|
| 71 <sup>5</sup>  | 72 <sup>3</sup>  | 72 <sup>1</sup> | 72 <sup>5</sup>  | 72 <sup>6</sup>  |
| $\frac{2.2}{17}$ | $\frac{1.4}{10}$ | 1.6             | $\frac{1.2}{10}$ | $\frac{1.1}{30}$ |

4+47 17<sup>2</sup> RT CORNER DOUBLE GARAGE UNDER CONSTRUCTION NO FLOOR YET APPROX ELEV FLOOR = 71.8

4+45 - 17<sup>2</sup> Lt. =  $\frac{1}{2}$  Sing. Gar dirt floor

71<sup>2</sup>  
 $\frac{2.5}{17}$   
 Floor

4+34 - 17<sup>2</sup> Lt. =  $\frac{1}{2}$  Sing Gar. Conc. floor

70<sup>9</sup> 70<sup>9</sup>  
 $\frac{2.75}{17}$   $\frac{2.8}{17}$   
 Gar. Floor End.

73.66



Alley BIK 27- O.B.

20

5+99.7 10.7 Lt. end Conc. slab.

5+99.2 13.9 PT CORNER STUCCO HOUSE

10.7 Lt. = line of conc. slab.

92 Rt. } start alley elev.  
99 Lt. }

5+99.6 = Wly. line Froude = start A.C. Pavc. →

5+95 11.3 PT CORNER 2.5 WIDE WALK PARALLEL TO LINE  
→ ELEV. = 86.41

T.P. 5.62 90.04 1.85 84.42

5+70 13.9 PT. COR. STUCCO HOUSE

5+75 →

5+65.5 11.3 PT. CORNER 2.5 WIDE WALK PARALLEL  
TO LINE → 85.99 = ELEV. WALK

5+58 - 10.7 Lt. = start Conc. slab.

5+50

5+22 25' Lt. = 1/2 Sing Gar. Conc. floor.

84.52  
95.00  
5.52 5.04  
25 10.7  
on slab

85.00 84.58 84.29 84.22 84.65 85.15 ✓  
5.04 5.16 5.75 5.82 5.39 4.89  
10.2 9.9 9.2 Pavc 9.2 9.2  
Slab. 0.6 0 90.04 0 Cl.

84.8 85.1 85.6 85.6 86.0 86.2  
1.5 1.2 0.7 0.7 0.3 0.1  
10.2 10 9 10 30  
Slab.

84.1 84.31  
2.2 1.96  
20 10.7  
on slab

82.8 83.8 83.2 83.8 84.0  
3.5 2.5 2.6 2.5 2.3  
30 10 10 30

80.16  
6.11  
25  
Gar. floor

86.27



Alley BIK, 27 - O.B.

21

Orig B.M. S.W.B.P.  
Ebers + Cape May 10.57 <sup>0.07</sup> 36.44 (36.42)

T.P. 0.16 47.01 11.42 46.85

T.P. 0.52 58.27 12.88 57.75

T.P. 1.27 70.63 12.28 69.36

S.W.B.P. Cape May  
Froude SS 5.62 76.02 (75.98)

T.P. 3.57 81.64 11.97 78.07

Cont

6+11.16 ↘

5+11<sup>16</sup> = Wly. cl. line Froude

83.15  
6.89 7.48  
60 60  
cl G

82.56  
4.35 3.73  
60 60  
G cl

85.69  
86.31

84.44  
5.60 6.18 6.15 5.90 5.63 5.59 4.76  
12 12 10 10 12 12  
cl.E.C. G cl.E.C.

83.86  
83.89  
84.14  
84.41  
84.45  
85.08

90.04



Robert  
Moore  
Clark  
7-3-50  
No. 25020

X- Sect Wilbur Ave.  
for Establishing Grade  
(Pendleton to Randall)

May 16 35

For TBM see FB 2103  
Pg. 1

1450

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 219.7 | 218.8 | 217.9 | 215.8 | 215.0 | 213.3 |
| 5.7   | 6.8   | 7.7   | 8.8   | 10.6  | 12.3  |
| 45    | 25    | 10    | 8     | 25    | 45    |

140

INDEXED  
MK  
JUL 20 1950

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 218.4 | 216.5 | 215.9 | 213.3 | 213.1 | 213.0 | 211.7 |
| 7.2   | 9.1   | 8.7   | 12.3  | 12.5  | 12.6  | 13.9  |
| 45    | 25    | 12    | 9     | 25    | 25    | 45    |

0465

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 213.9 | 213.2 | 211.3 | 210.3 | 209.0 |
| 11.7  | 12.4  | 14.3  | 13.3  | 16.6  |
| 45    | 25    | 25    | 25    | 45    |

0430

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 206.1 | 210.1 | 209.5 | 208.1 | 204.9 |
| 19.5  | 15.5  | 16.1  | 17.5  | 20.7  |
| 45    | 25    | 25    | 25    | 45    |

040 East Line Pendleton

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 198.3 | 198.2 | 198.1 | 196.5 | 196.0 |
| 27.3  | 27.4  | 27.5  | 29.1  | 29.6  |
| 45    | 25    | 25    | 25    | 45    |

Sit TBM

206 ✓  
216.53

hub EC Pipe on North Side Entry at Wilbur

T.P

7.27 ✓  
225.58 X

1.02 ✓  
218.31

225.58 X

TBM

1137 ✓  
219.33

209.96



4+50

225.0  
0  
45

224.2  
0.8  
25

221.8  
3.2

218.9  
6.1  
25

215.6  
9.4  
45

T.P.

2.44

225.00  $\pi$

3.06

222.52

225.00  $\pi$

4+0

227.6  
+2.0  
45

225.6  
0  
25

222.5  
3.1

219.6  
6.0  
25

217.0  
8.6  
45

3+50

226.9  
+1.3  
45

224.4  
1.2  
25

222.6  
3.0

219.9  
5.7  
25

217.7  
7.7  
45

3+0

226.4  
+0.8  
45

225.1  
0.5  
25

222.7  
2.9

221.1  
4.5  
25

219.4  
6.2  
45

2+50

224.9  
0.7  
45

224.0  
1.6  
25

223.2  
2.4  
10

222.0  
3.6  
8

221.6  
4.0

219.3  
6.3  
25

217.0  
8.6  
45

2+0

223.2  
2.4  
45

221.6  
4.0  
25

221.0  
4.6  
10

219.1  
6.5  
8

218.7  
6.9

217.1  
8.5  
25

216.2  
9.4  
45

225.58  $\pi$

225.58  $\pi$



T.P. 0.12 200.29<sup>✓</sup> 12.59 200.17<sup>✓</sup>

7+00

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 201.9 | 200.9 | 200.5 | 197.1 | 194.5 |
| 10.7  | 11.9  | 11.3  | 15.7  | 12.3  |
| 45    | 25    |       | 25    | 45    |

T.P. 0.75 212.76<sup>✓</sup> 12.99 212.01<sup>✓</sup>

212.76<sup>✓</sup>

6+50

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 212.3 | 211.4 | 209.7 | 209.6 | 208.0 |
| 12.7  | 13.6  | 15.3  | 15.4  | 17.0  |
| 45    | 25    |       | 25    | 45    |

6+0

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 216.2 | 217.6 | 217.5 | 217.0 | 214.5 |
| 8.8   | 7.4   | 7.5   | 8.0   | 10.5  |
| 45    | 25    |       | 25    | 45    |

5+50

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 219.0 | 219.5 | 219.3 | 218.1 | 215.2 |
| 6.0   | 5.5   | 5.7   | 6.9   | 9.8   |
| 45    | 25    |       | 25    | 45    |

5+0

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 221.4 | 221.1 | 220.2 | 217.9 | 215.8 |
| 3.6   | 3.9   | 4.1   | 7.1   | 9.2   |
| 45    | 25    |       | 25    | 45    |

225.00<sup>✓</sup>

225.00<sup>✓</sup>



Wilber Cont'd

24

Q

R

25

8+30

|           |           |       |           |           |
|-----------|-----------|-------|-----------|-----------|
| 149.8     | 146.8     | 143.6 | 141.2     | 140.2     |
| 13.6      | 16.6      | 19.1  | 22.2      | 23.2      |
| <u>45</u> | <u>25</u> |       | <u>25</u> | <u>45</u> |

T.P. 12.10 163.35  $\checkmark$  12.70 151.25  $\checkmark$

163.35  $\checkmark$

8+0

|           |           |       |           |           |
|-----------|-----------|-------|-----------|-----------|
| 156.2     | 157.8     | 158.9 | 156.4     | 155.2     |
| 7.7       | 6.1       | 5.7   | 7.5       | 8.8       |
| <u>45</u> | <u>25</u> |       | <u>25</u> | <u>45</u> |

Bottom Ravine

T.P. 0.46 163.95  $\checkmark$  12.89 163.49  $\checkmark$

163.95  $\checkmark$

T.P. 0.97 176.38  $\checkmark$  13.12 175.41  $\checkmark$

7+65

|           |           |       |           |           |
|-----------|-----------|-------|-----------|-----------|
| 167.8     | 175.1     | 175.8 | 172.9     | 171.8     |
| 20.7      | 13.4      | 12.7  | 15.6      | 16.7      |
| <u>45</u> | <u>25</u> |       | <u>25</u> | <u>45</u> |

← Ravine

T.P. 1.07 188.53  $\checkmark$  12.83 187.46  $\checkmark$

188.53  $\checkmark$

7+25

|           |           |       |           |           |
|-----------|-----------|-------|-----------|-----------|
| 188.6     | 191.7     | 192.3 | 191.5     | 190.3     |
| 11.7      | 9.6       | 8.0   | 8.8       | 10.0      |
| <u>45</u> | <u>25</u> |       | <u>25</u> | <u>45</u> |

← Ravine

200.29  $\checkmark$

200.29  $\checkmark$



Wilbur Cont'd

14

2

Rt 26

9+57 Where Wilbur hits Lot 15 BK 5

|                 |                 |       |                  |                   |
|-----------------|-----------------|-------|------------------|-------------------|
| 198.4           | 195.4           | 195.8 | 192.9            | 191.2             |
| $\frac{35}{45}$ | $\frac{65}{25}$ | 6.1   | $\frac{9.0}{25}$ | $\frac{14.7}{45}$ |

9+47

|                  |                  |       |                   |                   |
|------------------|------------------|-------|-------------------|-------------------|
| 194.2            | 192.5            | 192.3 | 188.5             | 185.7             |
| $\frac{7.7}{45}$ | $\frac{9.4}{25}$ | 9.6   | $\frac{13.4}{25}$ | $\frac{16.2}{45}$ |

T.P. 13.19 201.93X 0.11 188.74

201.93X

T.P. 12.68 188.95 0.12 176.17

9+0

|                   |                  |       |                  |                  |
|-------------------|------------------|-------|------------------|------------------|
| 166.1             | 168.0            | 169.0 | 170.8            | 168.7            |
| $\frac{10.2}{45}$ | $\frac{8.3}{25}$ | 7.3   | $\frac{5.5}{25}$ | $\frac{7.6}{45}$ |

T.P. 12.18 176.29X 0.24 163.11

Rock in  
Aster

176.29X

8+65

|                   |                   |       |                   |                   |
|-------------------|-------------------|-------|-------------------|-------------------|
| 141.2             | 140.2             | 139.0 | 138.0             | 136.8             |
| $\frac{22.2}{45}$ | $\frac{23.1}{25}$ | 24.4  | $\frac{25.3}{25}$ | $\frac{26.5}{45}$ |

8+55

|                   |                   |       |                   |                   |
|-------------------|-------------------|-------|-------------------|-------------------|
| 145.2             | 143.8             | 142.0 | 140.8             | 140.0             |
| $\frac{18.2}{45}$ | $\frac{19.6}{25}$ | 21.4  | $\frac{22.6}{25}$ | $\frac{23.4}{45}$ |

163.35X

163.35X



Wilbur Cont'd

24

Q

27

27

12+0

11+20 PCC

check

11+50

11+0

T.P.

10+50

10+0

9+57 = BC Wilbur on Rt 40' ROW

201.93X

0.68 ✓  
207.93 = 207.96

2.01 ✓  
208.61X

0.35 ✓  
201.64

208.61X

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 206.0 | 202.7 | 198.0 | 193.5 | 188.8 |
| 2.6   | 5.9   | 10.6  | 15.1  | 19.8  |
| 40    | 20    |       | 20    | 40    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 210.9 | 207.9 | 203.1 | 199.9 | 195.5 |
| + 2.3 | 0.7   | 5.0   | 8.7   | 13.1  |
| 40    | 20    |       | 20    | 40    |

|       |       |       |       |        |
|-------|-------|-------|-------|--------|
| 208.7 | 204.7 | 200.4 | 196.2 | 192.01 |
| 10.1  | 3.9   | 8.2   | 12.4  | 16.6   |
| 40    | 20    |       | 20    | 40     |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 203.3 | 200.3 | 196.7 | 192.3 | 187.9 |
| 7.4   | 1.6   | 5.2   | 9.6   | 14.0  |
| 40    | 20    |       | 20    | 40    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 198.5 | 193.7 | 188.1 | 179.4 | 175.9 |
| 3.4   | 8.2   | 13.8  | 22.5  | 26.0  |
| 40    | 20    |       | 20    | 40    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 196.2 | 191.9 | 184.0 | 177.9 | 170.4 |
| 5.7   | 10.0  | 17.9  | 24.0  | 31.5  |
| 40    | 20    |       | 20    | 35    |

201.93X



Wilbur Centid

Lt

Q

R

28

check Been hit 7.10 170.58 = 170.12 ✓

T.P. 1.76 177.18 12.48 175.42 ✓

14455 IN Roadall

184.3 181.0 176.5 173.3 171.0  
3.6 6.9 11.4 14.6 16.9  
40 20 20 20 40

1440

189.4 185.1 180.9 178.2 174.5  
4.5 2.8 7.0 9.7 13.4  
40 20 20 20 40

T.P. 1.78 187.90X 12.79 186.12 ✓

181.90X

13450

194.1 189.8 185.4 181.5 178.6  
4.8 3.1 13.5 17.4 20.3  
40 20 20 20 40

13400

197.8 192.9 188.7 185.2 181.3  
4.1 6.0 10.2 13.7 17.6  
40 20 20 20 40

12450

201.0 197.0 191.5 187.6 184.1  
7.1 1.9 7.4 11.3 14.4  
40 20 20 20 40

T.P. 3.02 198.89X 12.77 195.87 ✓

198.89X

208.61X



Roberts  
7-14-50

X-Section Quincy  
Chalcedony to Wilder  
For Establishing Grade

T.P. 12.85 101.68 0.25 81.83

1+85

INDEXED  
ms  
JUL 20 1950

1+45

(60' ROW)

1+0

T.P. 2.82 89.087 12.42 86.26

0+50

0+0 L Quincy North Line Chalcedony (80' ROW)

BM 12.75 98.687 85.93

Lt.

L

Rt.

29

72.1 72.8 73.1 69.4 71.4

170 16.3 16.0 19.7 17.7  
50 30 30 30 50

78.2 76.2 75.0 74.1 70.5 67.8 70.3

10.7 12.9 14.1 15.0 18.6 21.3 18.8  
60 40 20 40 50 60

82.8 80.8 76.1 70.6 67.6 70.1

6.3 8.3 13.0 18.7 21.7 19.0  
60 40 40 50 60

89.1

89.087

95.7 92.5 86.4 77.2 74.4

3.0 6.2 12.3 21.5 21.5  
60 40 40 60

106.7 105.7 97.3 91.2 86.0

11.0 17.0 14 7.5 12.7  
60 40 40 40 60

98.687

cont. from SN 7 Chalcedony + Randall



Quincy Cont'd

3+65

(40' ROW)

3+25.72

South Line Beryl ✓ (Station O.K.)

T.P.

13.07 127.61X 0.04 114.54

3+0

2+70

T.P.

13.00 114.58X 0.10 101.58

2+30

101.64X

87.7 91.6 96.7 96.9 91.8 89.5 92.3  
14.0 10.1 5.0 4.8 9.9 12.2 7.4  
50 30 15 30 40 50

# OFFICIAL BALLOT MUNICIPAL PRIMARY ELECTION

**INSTRUCTIONS**  
To vote for a candidate of your selection, stamp a cross in the voting square in the same office are to be elected, stamp a cross after the names of all the candidates who are to be elected. To vote on any measure, stamp a cross in the square provided. All distinguishing marks or erasures are forbidden and make the ballot void. All distinguishing marks or erasures are forbidden and make the ballot void.

## FOR MAYOR

(Vote for One)

HARLEY E. KNOX  
(Incumbent)

EDGAR F. HASTINGS

JOSEPH G. SHEA

## PROPOSITION NO. 1. Amendment to the Charter of the City of Quincy

This amendment abolishes the Department of Public Utility and Division of Accountancy and places the same under the supervision of a Director of Public Utility. It provides for the creation of a Department of Public Utility; provides for the creation of a Department of Public Utility, and for the creation of an advisory Commission on Public Utility to water development.

## PROPOSITION NO. 2. Amendment to the Charter of the City of Quincy



Quincy Cont'd

R

30

sta 0+00 N.L. Chalcedony 0+00  
 Average Station S.L. Bergl 3+23.72  
 " " N.L. Bergl 3+84.94  
 " " S.L. Poinsetta 4+94.46  
 Station Opp B.C. Rt 4+95.00  
 Station on Curve N.L. Poinsetta 5+40.50  
 Point of Reverse Curve & Quincy 6+89.98  
 End of Curve & Quincy 8+60.33  
 Station & Quincy S.L. Wilbur 13+50.56

|           |           |       |            |            |
|-----------|-----------|-------|------------|------------|
| 120.7     | 119.7     | 118.3 | 116.9      | 116.0      |
| 6.9<br>40 | 7.9<br>20 | 9.3   | 10.7<br>20 | 11.6<br>40 |
| 119.3     | 119.6     | 117.0 | 119.0      | 112.6      |
| 8.3<br>50 | 8.0<br>30 | 10.6  | 13.6<br>30 | 15.0<br>50 |
| 127.6     |           |       |            |            |
| 127.617   |           |       |            |            |

|           |           |            |       |           |           |
|-----------|-----------|------------|-------|-----------|-----------|
| 111.2     | 113.6     | 116.1      | 114.9 | 110.1     | 109.8     |
| 3.4<br>50 | 1.0<br>30 | 10.5<br>10 | 0.2   | 4.5<br>30 | 4.8<br>50 |

|            |           |       |           |            |           |
|------------|-----------|-------|-----------|------------|-----------|
| 98.9       | 104.9     | 108.5 | 106.0     | 99.6       | 107.6     |
| 15.7<br>50 | 9.7<br>30 | 6.1   | 8.6<br>30 | 15.0<br>50 | 7.0<br>70 |
| 119.6      |           |       |           |            |           |
| 114.587    |           |       |           |            |           |

|            |            |      |           |           |            |           |
|------------|------------|------|-----------|-----------|------------|-----------|
| 87.7       | 91.6       | 96.7 | 96.9      | 91.8      | 89.5       | 92.3      |
| 14.0<br>50 | 12.1<br>30 | 5.0  | 4.8<br>15 | 9.9<br>30 | 12.9<br>40 | 7.4<br>50 |
| 101.7      |            |      |           |           |            |           |
| 101.687    |            |      |           |           |            |           |

DISTRICT NO

T.P.

2+30

101.687

101.687



Quincy Cont'd

6+50

J.P. 12.94 153.37A 0.09 140.43

6+0

5+50

J.P. 12.91 140.52A 0.0 127.61

5+05 BC Pt

(4195<sup>True</sup> station)

4+50

4+0

127.61A

Lt

Q

Rt

152.6 150.6 149.1 198.3 146.1 145.8 **31**

0.8 2.8 4.3 5.1 7.3 7.6  
40 20 20 25 40

153.37A

139.5 140.1 140.4 140.0 137.5 137.7

1.0 0.4 0.1 0.5 3.0 2.8  
40 20 15 20 40

132.9 132.9 131.8 131.1 131.1

7.6 7.6 8.7 9.4 7.4  
40 20 20 40

140.52A

127.7 128.0 126.9 127.0 127.3

7.0 7.0 0.7 0.6 0.3  
40 20 20 40

124.3 124.2 123.3 123.2 123.2

3.3 3.4 4.3 4.4 4.4  
40 20 20 40

121.9 121.0 120.9 120.2 119.6

5.7 6.6 7.2 7.4 8.0  
40 20 20 40

127.61A



Quincy Cont'd

9+0

8+63 EC

TP

13.17

192.61X 0.05 179.44

8+0

TP

13.12

179.49X 0.10 166.37

7+50

6+93 PRC

TP

13.34

166.47X 0.14 153.23

153.37X

Lt

Q

Rt

32

180.9 183.6 185.1 185.6 190.8 190.9 193.9

17  
40 90  
20 75 7.0  
10 18 1.7  
15 20 7.13  
40

176.7 179.6 180.6 181.3 188.1 188.5 191.5

15.9  
40 13.0  
20 12.0 11.3  
10 4.5  
15 4.1  
20 1.1  
40

172.61X

171.9 171.9 172.8 173.7 177.3 173.5

7.6  
40 8.1  
20 6.7 5.8  
15 2.2  
20 6.0  
40

172.49X

169.9 169.3 167.3 169.9 165.3 166.0 163.2

13.4  
40 12.8  
26 10.8  
20 1.6  
18 1.2  
9.5  
20 3.3  
40

162.2 158.3 153.9 155.1 154.6 151.9

4.3  
40 8.2  
20 11.1  
15 11.4  
11.9  
20 14.6  
40

166.47X



Quincy Cont'd

44

Q

re

33

11+50

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 203.3 | 206.4 | 207.9 | 208.1 | 208.2 | 211.3 | 219.2 |
| 15.4  | 12.3  | 10.8  | 10.6  | 10.5  | 7.4   | 4.5   |
| 40    | 20    | 13    |       | 15    | 20    | 20    |

T.P.

13.28

218.72X 0.10 205.44

218.72X

11+9

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 197.6 | 201.5 | 209.0 | 209.1 | 209.3 | 207.5 | 210.8 |
| 7.9   | 4.0   | 1.5   | 1.4   | 1.2   | +2.0  | +5.3  |
| 40    | 20    | 13    |       | 14    | 20    | 40    |

10+50

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 191.6 | 194.9 | 192.0 | 199.2 | 199.6 | 202.9 | 205.5 |
| 13.9  | 10.6  | 6.5   | 6.3   | 5.9   | 2.6   | 0     |
| 40    | 20    | 13    |       | 13    | 20    | 40    |

10+0

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 187.8 | 190.2 | 193.6 | 194.2 | 194.7 | 198.5 | 202.6 |
| 17.7  | 15.5  | 11.9  | 11.3  | 10.8  | 7.0   | 3.5   |
| 40    | 20    | 13    |       | 12    | 20    | 40    |

T.P.

13.02

205.54X 0.09 192.52

205.54X

9+50

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 183.8 | 185.8 | 189.4 | 189.9 | 172.6 | 194.5 | 198.6 |
| 8.8   | 6.8   | 3.2   | 2.7   | ?     | 4.9   | 4.0   |
| 40    | 20    | 13    |       | 12    | 20    | 40    |

192.61X

192.61X



Quincy Cont'd

Lt

£

R

34

check

2.15 216.57 = 216.53

Reduced  
J. T. Lamore

13+50

Wilbur

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 210.5 | 213.0 | 215.0 | 215.7 | 217.1 |
| 8.2   | 5.7   | 3.7   | 3.0   | 16    |
| 40    | 20    | 13    |       | 20    |

13+0

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 209.9 | 213.0 | 215.7 | 216.2 | 217.7 | 219.9 |
| 8.8   | 5.7   | 3.0   | 2.5   | 10    | +12   |
| 40    | 20    | 13    |       | 20    | 40    |

12+50

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 208.4 | 211.5 | 214.3 | 214.7 | 216.0 | 220.4 |
| 10.3  | 7.2   | 4.4   | 4.0   | 2.7   | +1.7  |
| 40    | 20    | 13    |       | 20    | 40    |

12+0

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 206.9 | 209.0 | 211.4 | 211.2 | 211.5 | 214.0 | 216.7 |
| 11.8  | 9.7   | 7.3   | 7.5   | 7.2   | 4.7   | 2.0   |
| 40    | 20    | 13    |       | 16    | 20    | 40    |

218.72 X

218.72



Roberts  
7-19-50

X-Section Gladola  
(Pendleton to Quincy)  
For Establishing Grade

Lt

Q

Rt

35

2+0

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 201.1 | 197.1 | 194.1 | 193.1 | 191.1 | 188.1 |
| 5.0   | 9.0   | 12.0  | 15.0  | 15.0  | 18.0  |
| 40    | 20    | 12    |       | 20    | 40    |

1+50

INDEXED  
MK  
JUL 20 1950

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 202.7 | 198.7 | 196.9 | 191.4 | 186.6 | 193.8 | 190.8 |
| 3.4   | 6.4   | 7.2   | 8.7   | 9.5   | 12.3  | 15.3  |
| 40    | 20    | 15    | 12    |       | 20    | 40    |

1+0

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 205.0 | 202.8 | 202.4 | 199.9 | 199.1 | 197.9 | 194.9 |
| 1.1   | 5.3   | 3.7   | 6.2   | 7.0   | 8.2   | 11.2  |
| 40    | 20    | 17    | 12    |       | 20    | 40    |

0+75

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 205.7 | 203.0 | 200.3 | 199.2 | 197.6 | 193.9 |
| 0.4   | 3.1   | 5.8   | 6.9   | 8.5   | 12.2  |
| 40    | 20    | 12    |       | 20    | 40    |

0+35

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 201.0 | 196.8 | 197.2 | 189.4 | 185.1 |
| 4.2   | 9.3   | 8.9   | 16.7  | 21.0  |
| 40    | 20    |       | 20    | 40    |

0+0

Rt Lt to NE Cor Pendleton & Gladola

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 195.1 | 190.1 | 186.1 | 183.1 | 180.1 |
| 11.0  | 16.0  | 20.0  | 23.0  | 26.0  |
| 40    | 20    |       | 20    | 40    |

T.P.

0.94 206.087 12.75 205.14

206.087

T.M.

1.36 217.89

216.53 <sup>old</sup> 466 NE Cor. Wilbur & Quincy



Gladiola Cont'd

kt

Q

R

36

T.P. 0.15 169.20X 12.79 169.05

4+50

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 178.3 | 179.0 | 177.1 | 170.3 | 169.6 | 166.8 | 162.5 |
| 3.5   | 7.8   | 10.7  | 11.5  | 12.2  | 15.0  | 19.3  |
| 40    | 20    | 12    |       | 14    | 20    | 40    |

4+0

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 182.2 | 179.0 | 176.2 | 175.5 | 174.8 | 172.4 | 169.0 |
| 4.4   | 2.8   | 5.6   | 6.3   | 7.0   | 9.4   | 12.8  |
| 40    | 20    | 12    |       | 13    | 20    | 40    |

T.P. 0.09 181.84X 12.21 181.35

181.84X

3+50

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 189.4 | 189.7 | 181.2 | 189.3 | 179.2 | 176.7 | 174.4 |
| 4.6   | 9.3   | 12.8  | 13.7  | 14.8  | 17.3  | 19.6  |
| 40    | 20    | 12    |       | 12    | 20    | 40    |

3+0

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 192.7 | 188.9 | 185.9 | 185.0 | 182.0 | 178.4 |
| 1.3   | 5.1   | 8.1   | 9.0   | 12.0  | 15.6  |
| 40    | 20    | 13    |       | 20    | 40    |

2+50

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 197.0 | 193.5 | 189.2 | 189.4 | 185.3 | 181.9 |
| 13.0  | 0.5   | 3.8   | 4.6   | 8.7   | 12.1  |
| 40    | 20    | 12    |       | 20    | 40    |

T.P. 0.86 193.96X 12.98 193.10

193.96X

206.08X



Gladiola Cont'd

LL

R

R

37

check 12.14 119.52 = 119.56

TP 0.45 131.66 12.95 131.21

TP 0.27 144.16 12.75 143.89

Reduced  
N.T. Lawrence

6+75 In Quincy

156.6 153.1 150.9 147.4

0 35 57 92  
20 14 20

6+35

163.6 157.6 154.8 153.2 151.9 149.4 145.2  
+7.0 +1.0 1.8 3.4 4.7 7.2 11.4  
40 20 12 14 20 40

TP 0.50 156.64X 13.06 156.14

156.64X

6+0

165.1 160.2 156.7 155.6 154.6 150.2 147.0  
4.1 9.0 12.5 13.6 14.6 19.0 22.0  
40 20 12 13 20 40

5+50

169.2 164.8 160.6 159.6 158.6 154.7 151.7  
0 4.6 8.6 9.6 10.6 14.5 17.5  
40 20 12 13 20 40

5+0

172.5 168.6 165.0 163.9 163.1 159.3 156.2  
+3.3 0.6 4.2 5.3 6.1 7.9 13.0  
40 20 14 13 20 40

169.20X

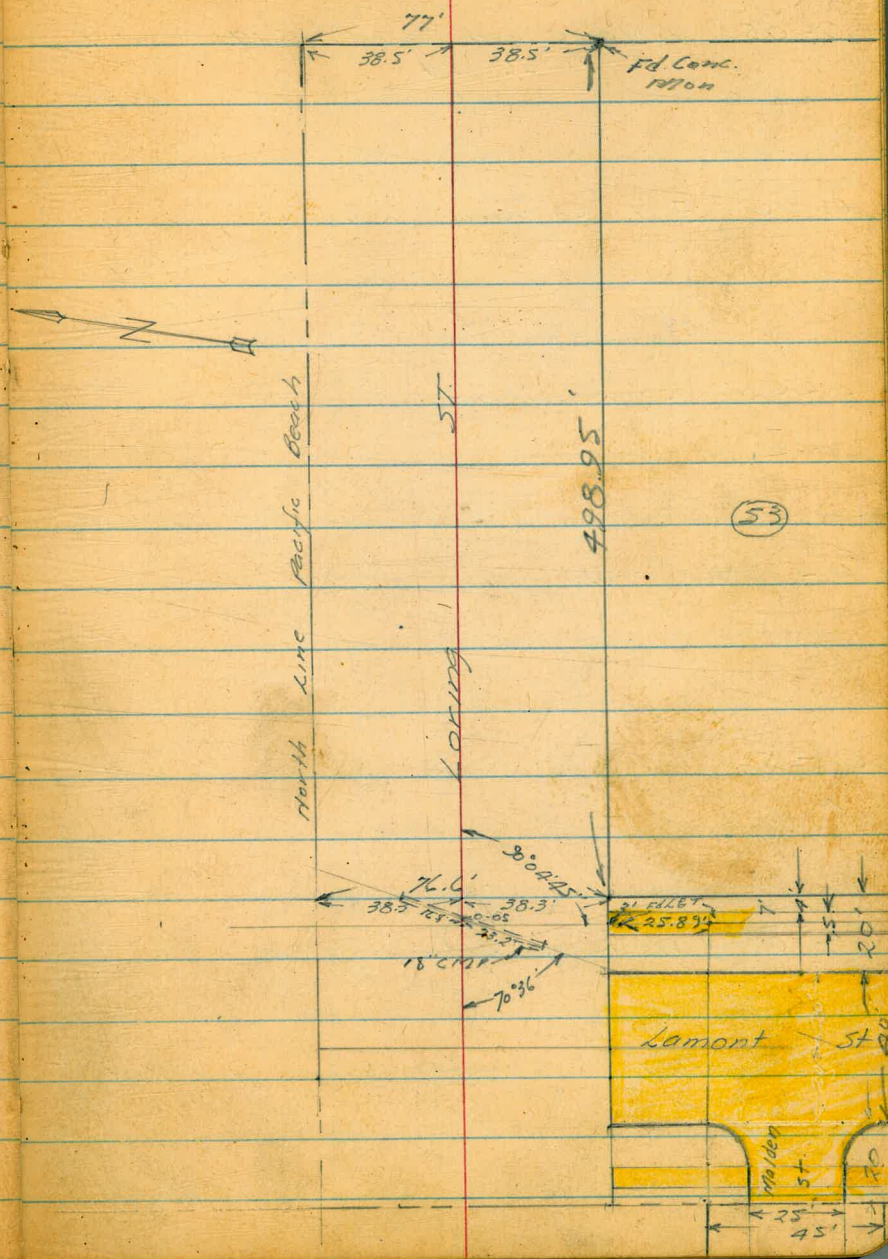
169.20X



731-50 X Sect. Loring St.  
 Hendrick Lamont to Ely, Termination  
 Johnson  
 Greer  
 Crawford  
 WO # 3182C

INDEXED

JUL 31 1950





Levels Loring St.

0-05 Intersection of 18" CMP at E  
70°36' Lt

0-20 East Ch line Lamont

0-40 E Lamont

0-48

0-52

0-60 West Ch line Lamont

BM 9.29 216.14

206.85

39

|        |        |        |        |        |
|--------|--------|--------|--------|--------|
| 209.74 |        |        |        | 207.08 |
| 140    |        |        |        | 905    |
| 168    |        |        |        | 23.2   |
| Fl     |        |        |        | Fl     |
| Diag   |        |        |        | Diag   |
| 214.61 | 213.34 | 209.9  | 206.22 | 206.22 |
| 15     | 28     | 63     | 985    | 925    |
| 50     | 38     |        | 38.3   | 38.3   |
|        |        |        | G      | cb.    |
|        |        |        |        | 69     |
|        |        |        |        | 69     |
|        |        |        |        | cb     |
| 214.4  | 213.1  | 209.54 | 206.67 | 204.62 |
| 12     | 30     | 66     | 947    | 1152   |
| 50     | 38     |        | 380    | 66     |
|        |        |        | Pav    |        |
| 214.4  | 213.0  | 209.4  | 206.6  |        |
| 12     | 31     | 67     | 958    |        |
| 50     | 38     |        | 380    |        |
|        |        |        | Pav    |        |
| 215.1  | 213.9  | 211.4  | 209.4  | 206.95 |
| 10     | 23     | 42     | 52     | 969    |
| 50     | 38     | 20     |        | 1162   |
|        |        |        |        | 384    |
|        |        |        |        | Pav    |
|        |        |        |        | 66.3   |
|        |        |        |        | Pav    |
| 214.9  | 213.7  | 209.8  | 206.75 | 206.78 |
| 13     | 24     | 63     | 981    | 936    |
| 50     | 38     |        | 386    | 385    |
|        |        |        | G      | cb     |
|        |        |        |        | 66.3   |
|        |        |        |        | 66.3   |
|        |        |        |        | cb     |
|        |        |        |        | cb     |

L&T East 7' line Lamont  
3' south of So. line Loring

BC. 1511 cor.  
174100 P.47



Loring St. Cont'd

T.P. 10.81 22(87) 0.08 216.06  
 1+16 Conc Drive on Rt

1+00 End Wall on Rt

0+75

0+44 wall steps up on Rt

0+00 East Line Lamont

0-04 Beg Conc Wall 38.4' Rt

216.14  
 T

222.3 219.2 216.2 216.0 215.2 214.9 219.2 214.5 213.5 217.4 211.69  
 16 13 10 0 0 1 1 1 2 3 4 5  
 50 35 31 20 18 16 18 33 38.1 50

219.0 216.9 215.1 215.1 214.3 213.8 213.1 213.5 212.0 211.20 210.3 201.1  
 12 10 10 10 18 2 3 3 2 4 4 8 9  
 50 35 32 20 18 16 18 35 38.2 39 50  
 Wall

216.1 214.8 213.9 213.8 212.9 212.4 211.79 212.2 211.2 211.28 207.5 207.3  
 0 1 2 2 3 3 4 3 4 4 8 8  
 45 36 33 20 18 16 18 38.2 38.2 39 50  
 Gr Wall Gr

215.8 214.4 212.9 212.9 212.0 211.2 210.4 210.8 209.4 209.44 211.25 207.4  
 0 1 3 3 4 4 5 5 6 6 8 8  
 50 42 32 20 19 16 20 38.2 38.2 39 50  
 Gr Wall Gr

214.5 212.8 211.6 211.2 211.0 210.74 209.2 209.1 208.2 209.2 207.2 206.6  
 1 3 4 4 5 8 6 7 7 6 8 8  
 50 38 20 19 12 18 22 38.4 38.4 39 50  
 Gr Wall

207.4  
 8.2 209.08  
 7.06  
 38.4 38.4  
 Gr Wall

216.14  
 T



4+00

|    |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 235.3 | 233.6 | 223.9 | 223.7 | 222.9 | 222.4 | 222.3 | 223.2 | 223.3 | 220.3 | 219.0 |
| 18 | 16    | 30    | 32    | 40    | 45    | 46    | 37    | 36    | 65    | 72    |       |
| 45 | 35    | 27    | 19    | 18    |       | 18    | 19    | 34    | 39    | 50    |       |

3+50

|    |       |       |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 233.7 | 231.7 | 232.1 | 223.8 | 223.4 | 222.8 | 222.5 | 222.5 | 223.0 | 223.3 | 223.1 | 221.2 | 221.0 |
| 16 | 14    | 15    | 31    | 35    | 41    | 44    | 44    | 39    | 36    | 38    | 57    | 59    |       |
| 60 | 44    | 35    | 27    | 19    | 18    |       | 18    | 19    | 23    | 34    | 39    | 50    |       |

3+00

|    |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 234.9 | 232.7 | 223.3 | 223.0 | 222.3 | 222.1 | 222.3 | 223.0 | 222.6 | 222.7 | 222.9 |
| 18 | 15    | 35    | 37    | 46    | 48    | 46    | 39    | 36    | 32    | 40    |       |
| 48 | 35    | 27    | 19    | 18    |       | 17    | 19    | 36    | 39    | 50    |       |

2+50

|    |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 236.4 | 224.3 | 222.5 | 222.3 | 221.4 | 221.4 | 221.3 | 222.0 | 221.9 | 221.1 | 220.4 |
| 19 | 17    | 44    | 46    | 55    | 55    | 55    | 49    | 50    | 22    | 25    |       |
| 44 | 35    | 26    | 19    | 18    |       | 16    | 20    | 36    | 38    | 50    |       |

2+00

|    |       |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 233.9 | 220.9 | 220.9 | 220.8 | 220.0 | 219.7 | 219.8 | 220.6 | 220.1 | 221.3 | 220.9 | 220.3 |
| 17 | 16    | 60    | 61    | 62    | 72    | 72    | 71    | 63    | 68    | 55    | 60    | 66    |
| 47 | 34    | 28    | 20    | 18    |       | 16    | 18    | 34    | 36    | 44    | 50    |       |

1+50

|    |       |       |       |       |       |       |       |       |       |       |       |       |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 226.9 | 224.9 | 218.2 | 218.2 | 217.4 | 217.3 | 216.6 | 217.1 | 217.1 | 217.4 | 215.5 | 215.4 |
| 0  | 20    | 87    | 87    | 95    | 96    | 10    | 98    | 98    | 98    | 85    | 85    | 85    |
| 50 | 35    | 28    | 21    | 19    |       | 16    | 18    | 32    | 38    | 39    | 50    |       |

226.87  
/

226.87  
/



Loring St. Contd.

42

Reduced  
H.T. January

590 22097 22099

4 Sidewalk 8.5 RT 545.4+98.87  
(FB 1553 P. 50)

5+00

|       |       |       |       |
|-------|-------|-------|-------|
| 229.4 | 227.9 | 229.9 | 222.4 |
| 12 5  | 11 1  | 20    | 4 5   |
| 40    | 21    | 17    | 31    |
|       |       |       | 220.8 |
|       |       |       | 219.6 |
|       |       |       | 7 3   |
|       |       |       | 39    |

4+96

|       |       |       |       |
|-------|-------|-------|-------|
| 229.4 | 227.9 | 229.9 | 222.4 |
| 12 5  | 11 0  | 2 1   | 4 5   |
| 40    | 21    | 17    | 39    |
|       |       |       | 219.9 |
|       |       |       | 7 0   |
|       |       |       | 39    |

4+90

|       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 235.2 | 231.7 | 229.3 | 229.1 | 229.9 | 223.3 | 223.3 | 223.2 | 221.3 | 219.8 |
| 18 3  | 14 8  | 12 1  | 22    | 2 5   | 3 5   | 3 5   | 37    | 5 5   | 7 1   |
| 52    | 46    | 35    | 27    | 19    |       | 17    | 27    | 30    | 40    |

4+50

|       |        |       |       |       |       |       |       |       |       |       |
|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 235.3 | 233.67 | 223.3 | 223.4 | 222.8 | 222.6 | 222.3 | 222.7 | 222.5 | 219.7 | 219.3 |
| 18 1  | 16 5   | 3 5   | 2 5   | 1 1   | 1 3   | 4 5   | 4 3   | 1 1   | 7 3   | 7 6   |
| 48    | 35     | 28    | 20    | 18    |       | 17    | 18    | 34    | 39    | 50    |

226.87

7

226.87

7



Curb elevations  
Orchard-Catalina-Ely.

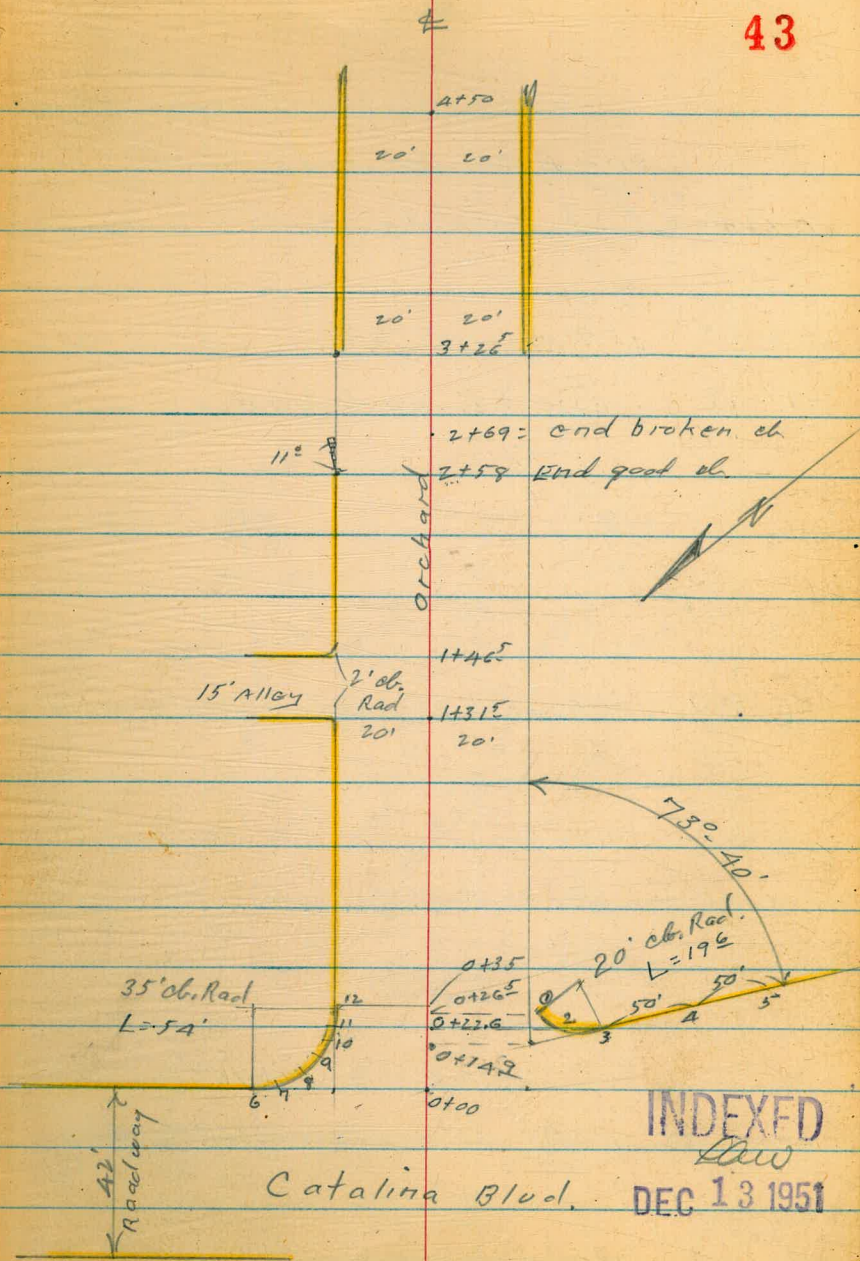
Sommormeyer  
Be99  
Allen

10/14/50  
U.O. 25020

Ely cb. line Catalina = 0+00

Also See P. 48

43



INDEXED  
DEC 13 1951



Orchard

See p. 45 for rods

0+26<sup>5</sup> <sup>26<sup>2</sup>RT</sup> End existing curb.

0+22<sup>5</sup> 45<sup>4</sup> RT. = Ch. B.C.

0+14<sup>9</sup> 20' RT. = P.I. curb lines

Ely Return. Rods by number (See sketch)

0+00 - 55' Lt. = B.C. 35' Rad. Ch. Ret.

3.52 200.02 - 196.50

~~0+00 55' Lt. = B.C. 35' Rad. Ch. Ret.~~

~~155  
G~~

~~3.25 199.75 - 196.50~~

±

44

|  |        |             |        |        |        |          |        |
|--|--------|-------------|--------|--------|--------|----------|--------|
|  | 195.08 |             | 194.49 |        | 195.14 |          | 195.19 |
|  | 4.94   | 5.53        |        |        | 4.88   | 4.83     |        |
|  | 10     | .10         |        |        | 11     | 12       |        |
|  | cc     | G           |        |        | cc     | Ch. E.C. |        |
|  |        | = end pave. |        |        |        |          |        |
|  | 194.49 | 194.02      | 194.64 | 194.12 | 194.75 | 194.34   | 194.97 |
|  | 5.53   | 6.00        | 5.38   | 5.90   | 5.24   | 5.68     | 5.05   |
|  | G      | G           | 7      | 7      | 8      | 8        | 9      |
|  | cc     | G           | cc     | G      | cc     | G        | cc     |
|  | B.C.   |             |        |        |        |          | G      |
|  | 192.70 | 192.21      | 193.57 | 193.12 | 194.49 | 194.02   |        |
|  | 7.32   | 7.81        | 6.45   | 6.90   | 5.53   | 6.00     |        |
|  | 155    | 155         | 105    | 105    | 55     | 55       |        |
|  | cc     | G           | cc     | G      | cc     | G        |        |
|  |        |             |        |        | B.C.   |          |        |

200.02

S.W. BP Catalina & Orchard

|  |      |      |      |      |
|--|------|------|------|------|
|  | 6.63 | 6.20 | 5.70 | 5.26 |
|  | 155  | 105  | 105  | 55   |
|  | cc   | G    | cc   | G    |
|  |      |      |      | B.C. |

199.75

S.W. B.P. Catalina & Orchard



Orchard

T.P. 6.01 201.27 4.76 195.26

1+29<sup>E</sup> 20' Lt. = B.C. 2' Rad. Alley cl. Ret

195.26  
4.76  
20  
cl. B.C.

1+00

195.25  
4.77  
20  
cl.

0+50

195.20  
4.82  
20  
cl.

0+35 - 2d Lt. = E.C. 35' Rad. cl. Ret

195.19  
4.83  
35  
cl. E.C.

0+28 - 25<sup>E</sup> Rx. = end exist pavement

195.12  
4.30  
25<sup>E</sup>

see sketch

Sly curb return rods by number

|        |          |        |        |        |          |        |        |        |        |
|--------|----------|--------|--------|--------|----------|--------|--------|--------|--------|
| 195.17 | 196.45   | 195.91 | 196.50 | 195.91 | 196.53   | 196.34 | 196.92 | 196.17 | 197.37 |
| 4.25   | 3.57     | 4.11   | 3.52   | 4.11   | 3.49     | 3.68   | 3.10   | 3.25   | 2.65   |
| T      | T        | Z      | Z      | Z      | 3        | 4      | 4      | 5      | 5      |
| G      | cl. curb | G      | cl.    | G      | cl. B.C. | G      | cl.    | G      | cl.    |

Mid Curve

200.02



orchard

2+58 - 20' Lt. = end good Exist. cl.

195.31

£

5.96  
20  
cl.

2+50

195.23

6.04  
20  
cl.

2+00

195.32

5.95  
20  
cl.

1+50

195.34

5.73  
20  
cl.

1+48<sup>E</sup> 20' Lt. = E.C. 2' Rad. Alley cl. Ret.

195.32

5.95  
20  
cl. E.C.

1+46<sup>E</sup> 40' Lt. = end alley curb  
20' Lt. = B.C. 2' Rad Alley cl. Ret.

195.52

5.75  
40  
end cl.

195.36

5.91  
22  
cl. B.C.

1+31<sup>E</sup> 40' Lt. = end of alley cl.  
22' Lt. = end 2' Rad alley Ret.

195.48

5.79  
40  
end cl.

195.25

6.02  
22  
cl. E.C.



check. orig. B.M. - P 44 4.77 196.50 OK

4+50

199.43  
1.84 2.45 2.38  
20 20 18E  
cb G E.G.

198.92  
2.35 2.48 1.81  
18E 20 20  
E.G. G cc

4+25<sup>A</sup>

198.34  
2.93 3.52 3.48  
20 20 18E  
cc G E.G.

197.96  
3.31 3.45 2.80  
18E 20 20  
E.G. G cc

4+00

197.53  
3.74 4.35 4.26  
20 20 18E  
cb G E.G.

197.09  
4.18 4.31 3.62  
18E 20 20  
E.G. G cc

3+50

196.22  
5.05 5.68 5.56  
20 20 18E  
cb G E.G.

195.68  
5.59 5.72 5.05  
18E 20 20  
E.G. G cc

G=gutter at curb

E.G.= edge of gutter

20<sup>1</sup> RT }  
20<sup>1</sup> LT } = Face of cb. at top of cb.

3+26<sup>E</sup>

18E RT }  
18E LT } start conc. comb. set gutter

195.80  
5.47 6.10 5.98  
20 20 18E  
cb G E.G.

195.27  
6.00 6.15 5.53  
18E 20 20  
E.G. G cc

201.27



Orchard Ave.

Levels on new curbs  
From N.Wly line Loma Lands Park  
N.Ely 175'

0+00 = N.Wly line Loma Lands Park.

Also see P. 43

Sommermeier  
Begg  
R. Sisson  
Fleming

19-Apr. 1951  
W.O. 31783

0+75

|        |        |        |        |
|--------|--------|--------|--------|
| 197.57 | 196.95 | 196.99 | 197.67 |
| 5.26   | 5.87   | 5.31   | 5.83   |
| cl     | G      |        | cc     |

0+50

|        |        |        |        |
|--------|--------|--------|--------|
| 196.84 | 196.22 | 196.55 | 197.15 |
| 5.98   | 6.60   | 6.00   | 6.27   |
| cl     | G      |        | cl     |

0+25

|        |        |        |        |
|--------|--------|--------|--------|
| 196.25 | 195.57 | 196.27 | 196.85 |
| 6.57   | 7.25   | 6.41   | 6.56   |
| cl     | G      |        | cl     |

std. cl. - 1 1/2' gutters.

40' Roadway, A.C. Pavc.

0+00 N.Wly. line Loma Lands Park.

|               |        |        |        |        |
|---------------|--------|--------|--------|--------|
| 195.78        | 195.19 | 196.05 | 196.22 | 196.85 |
| 7.04          | 7.63   | 6.77   | 6.60   | 5.97   |
| cl            | G      |        | G      | cl     |
| <u>202.82</u> |        |        |        |        |

T.P. 5.97 202.82 3.73 196.85

4.08 200.58 - 196.50

S.W.B.P. Catalina + Orchard

INDEVEN

APR 19 1951

£

48



orchard

#

43

6.32 196.50 0119 B.H.

1+75

0.90 1.49 1.03 1.52 0.92  
cl G G cl

1+50

2.10 2.72 2.31 2.84 2.75  
cl G G cl  
17 drive

1+25

3.33 3.95 3.45 3.98 3.35  
cl G G cl

1+00

4.37 4.97 4.40 5.01 4.36  
cl G on M.H. cl  
Cover

201.82



Alley BIK, 195 City Hqts

Sommormeyer  
Begg  
R. Sisson  
oltman

16-May, 1957  
W.O. 31107

INDEXED

MAY 23 1957

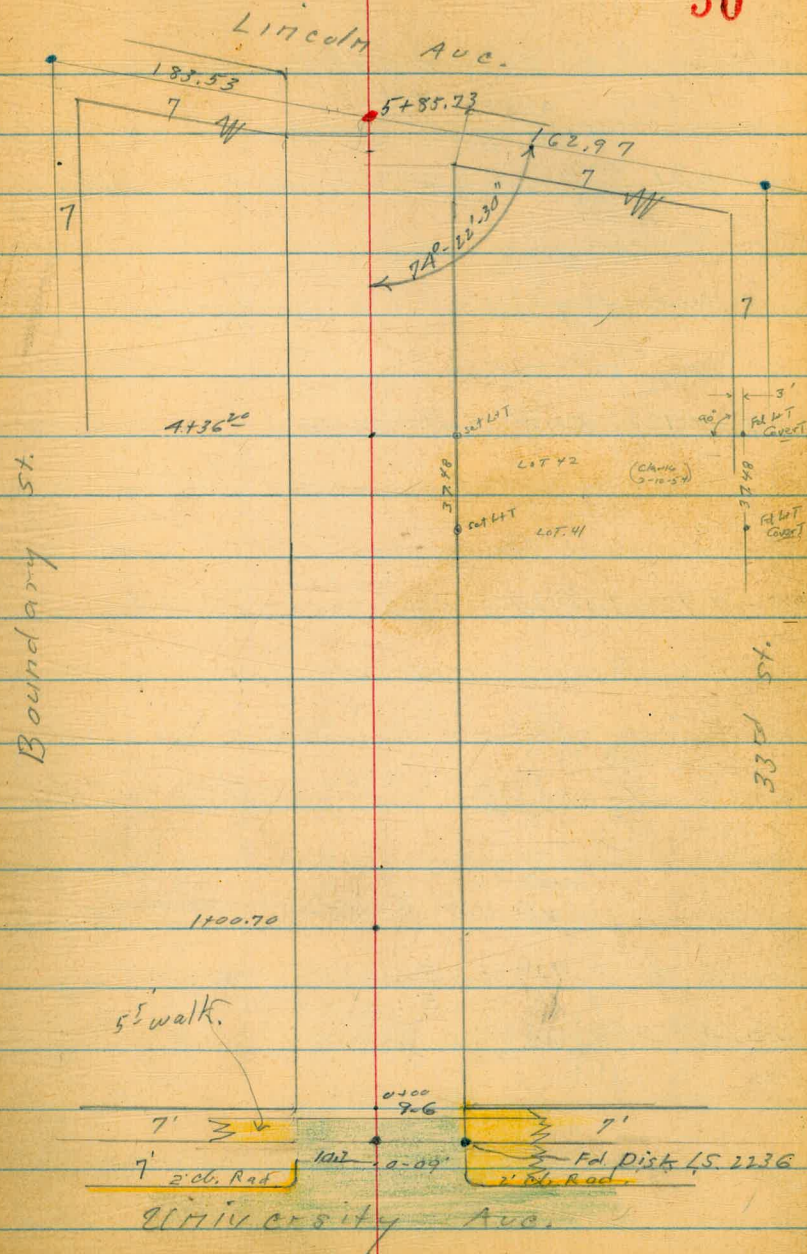
FB 1365  
46

- = Fd. L+T
- = Fd Nail
- = set nail
- = set 1/2

(W) = ctr. water meter box

Pole outs taken to outside (or back)  
of pole

50





Alley BIK 195 - City Hqts.

0+12 - 9' Lt. = Deadman

8' Rt. = (W)

95 Rt. = end cl.

0+01 10<sup>2</sup> Rt = start stucco Bldg.

8' Rt. = (W)

0+00 = Nly line Univ.

0-01<sup>5</sup> end A.C. Pave

0-09. 10<sup>2</sup> Lt. = end good curb

0-12  $\left. \begin{matrix} 10^2 \text{ Lt.} \\ 95 \text{ Rt.} \end{matrix} \right\} = \text{E.C. 2' Rad alley Cb. Ret.}$

$\left. \begin{matrix} 10^2 \text{ Lt.} \\ 95 \text{ Rt.} \end{matrix} \right\} = \text{B.C. 2' Rad. Alley Ret.}$

0-1A = Nly  $\left\{ \begin{matrix} 12^2 \text{ Lt.} = \text{B.C. 2' Rad. Alley Ret.} \\ 115 \text{ Rt.} = \text{E.C. 2' Rad. Alley Ret.} \\ \text{Cb. University} \end{matrix} \right.$

5.74 332.98 8.93 327.24

2.73 336.17 - 333.44

REDUCED  $\pm$

Ryan  
5-23-51

51

328.0

5.3  
10

327.64

5.34  
10<sup>2</sup>  
pave

327.73

5.25  
10<sup>2</sup>  
end cl

327.64

5.34  
10<sup>2</sup>  
cl. E.C.

327.14

5.84  
10<sup>2</sup>  
G

526.56

6.42  
95  
G

526.98

6.00  
95  
cl. E.C.

|        |        |                 |                 |        |        |          |        |        |
|--------|--------|-----------------|-----------------|--------|--------|----------|--------|--------|
| 329.20 | 328.53 | 327.66          | 327.07          | 326.70 | 326.32 | 326.79   | 324.84 | 325.32 |
| 3.78   | 4.45   | 5.32            | 5.91            | 6.28   | 6.66   | 6.09     | 8.14   | 7.66   |
| 60     | 60     | 12 <sup>2</sup> | 12 <sup>2</sup> | 332.98 | 115    | 115      | 60     | 60     |
| cl.    | G      | cl. B.C.        | G               | G      | G      | cl. B.C. | G      | cl.    |

Disk - LS. 22.36 - 10' Rt. of 0-07

N.W.B.P. - Boundary + University



Alley BIK 195  
City Hqts

1+00 8<sup>5</sup> Rt. = end lath fence

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 337.0 | 336.5 | 337.0 | 336.4 | 336.3 |
| 4.9   | 5.6   | 4.9   | 5.5   | 5.6   |
| 10    |       | 8     | 10    | 20    |

0+96

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 337.3 | 337.4 | 336.5 | 336.3 | 337.3 | 330.6 | 327.6 |
| 4.6   | 4.5   | 5.4   | 5.6   | 4.6   | 11.3  | 14.3  |
| 15    | 10    | 8     |       | 16    | 13    | 20    |

0+80 7<sup>5</sup> Rt. = start lath fence

0+70

|       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 337.3 | 337.3 | 336.5 | 334.7 | 334.8 | 335.1 | 336.9 | 337.7 | 327.8 |
| 4.6   | 4.6   | 5.4   | 7.2   | 7.1   | 6.7   | 5.0   | 4.7   | 14.1  |
| 15    | 12    | 10    | 7     |       | 5     | 7     | 10    | 11    |
|       |       |       |       |       |       |       |       | 20    |

0+67 9<sup>8</sup> Rt. = end stucco Bldg.

|       |       |       |       |       |       |        |
|-------|-------|-------|-------|-------|-------|--------|
| 337.2 | 336.0 | 334.4 | 334.7 | 335.0 | 335.8 | 330.4  |
| 4.4   | 4.7   | 5.9   | 7.5   | 7.2   | 6.9   | 6.1    |
| 20    | 14    | 10    | 8     |       | 6     | 8      |
|       |       |       |       |       |       | 98     |
|       |       |       |       |       |       | A+Bldg |

0+50

|       |       |       |       |       |       |         |
|-------|-------|-------|-------|-------|-------|---------|
| 337.4 | 335.9 | 333.0 | 333.3 | 333.5 | 333.9 | 333.7   |
| 4.5   | 6.0   | 8.9   | 8.6   | 8.4   | 8.0   | 8.2     |
| 15    | 10    | 7     |       | 5     | 7     | 99      |
|       |       |       |       |       |       | A+Bldg. |

0+40 9<sup>5</sup> Lt. = Pole # P.A. 3903 into grounds with conduit

341.90

T.P. 7.92 341.90 1.00 331.98

0+15

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 336.5 | 335.5 | 332.2 | 329.5 | 329.2 | 328.9 |
| +3.5  | +2.5  | 0.8   | 3.5   | 3.8   | 4.1   |
| 15    | 12    | 10    | 6     |       | 10    |

332.98



Alloy BIK. 195

City Hqts

53

T.P. 3.16 338.64 6.42 335.48  
2+11 16<sup>3</sup> Rt. =  $\phi$  2' wide Conc. walk

|       |       |       |       |       |                 |       |
|-------|-------|-------|-------|-------|-----------------|-------|
| 336.2 | 335.7 | 335.3 | 334.9 | 334.0 | 332.4           | 332.1 |
| 5.7   | 6.2   | 6.6   | 7.0   | 7.9   | 9.50            | 9.8   |
| 10    | 8     |       | 7     | 10    | 16 <sup>3</sup> | 20    |
|       |       |       |       |       | walk            |       |
|       |       |       |       |       | end             |       |
|       |       |       |       |       | 333.7           |       |
|       |       |       |       |       | 8.2             |       |
|       |       |       |       |       | 15 <sup>2</sup> |       |
|       |       |       |       |       | end.            |       |

2+05 - 15<sup>2</sup> Rt = end porch

2+00 - 11<sup>2</sup> Lt. = start board fence, Posts  
Set in Conc. base - 15' diam  
15<sup>2</sup> Rt. = start Cobble Conc. Porch  
1+97 - 14<sup>3</sup> Rt. = end house

|       |       |       |       |       |                 |  |
|-------|-------|-------|-------|-------|-----------------|--|
| 337.1 | 336.9 | 336.1 | 335.7 | 335.1 | 334.8           |  |
| 4.8   | 5.0   | 5.8   | 6.2   | 6.8   | 7.1             |  |
| 15    | 10    | 8     |       | 10    | 14 <sup>3</sup> |  |
|       |       |       |       |       | at house        |  |

1+86 - 8' Rt. = (W)

1+82 11<sup>A</sup> Lt. = end frame Bldg.

10<sup>2</sup> Lt. = Pole # PA.3919  
1+76 15<sup>2</sup> Rt. = start frame house

1+73 - 9' Lt. = (W)

1+60 10<sup>5</sup> Lt. =  $\phi$  door. (1 car wide)

337.2  
4.7  
10<sup>5</sup>  
dirt floor

(vertical boards - mud sills)  
1+54 10<sup>5</sup> Lt. = start frame Bldg.

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 337.3 | 336.8 | 336.7 | 336.5 | 336.5 |
| 4.6   | 5.1   | 5.2   | 5.4   | 5.4   |
| 10    | 8     |       | 8     | 10    |

1+50

341.90



Alley BIK. 195  
City Hqts.

54

11<sup>6</sup> Lt. = end board fence  
2+50 10<sup>5</sup> Rt. = start conc. apron to Bldg.  
(4 Car Gar. + dwelling rooms)

335.3  
4.0  
10

334.8  
4.5  
7

334.4  
4.9

333.75  
5.55  
102  
Apron  
+ Ord.

333.69  
5.61  
115

333.85  
5.45  
125  
at Bldg.

2+49<sup>5</sup> 10' Rt. =  $\pm$  1" wide E. + W. open Conc. drain

333.2  
6.10  
10  
on drain

331.2  
8.1  
27

329.5  
9.8  
35  
Enters  
down  
spout.

T.P. Nail  
Pole # PA 3934 4.74 339.30 4.28 334.56

339.30

2+48- 11<sup>7</sup> Lt. =  $\pm$  4' wide Conc. walk.

335.64  
3.00  
117  
walk

2+45 11<sup>6</sup> Lt. = end shed start board fence

2+44 - 11<sup>5</sup> Rt. =  $\pm$  Sing. Gar. dirt floor

333.5  
5.1  
115  
Floor

9' Lt. = (W)

2+34 11<sup>5</sup> Rt. =  $\pm$  Sing. Gar. dirt floor

333.5  
5.1  
115  
Floor

2+28 11<sup>2</sup> Lt. = start board shed  
= end board fence

336.4  
2.2  
112

336.4  
2.2  
10

335.2  
3.4  
8

334.7  
3.9

333.5  
5.1  
10

333.5  
5.1  
15

2+27 8' Rt. = (W)

338.64



2+99 10' Lt. = Pole # P.A. 3935

2+97- 11' Lt. = end conc. apron to double

|           |        |
|-----------|--------|
| 334.57    | 334.50 |
| 4.73      | 4.80   |
| 13        | 11'    |
| Gar Floor | Apron  |

2+82- 10<sup>E</sup> Lt. = start conc. Apron to double

|                 |                 |
|-----------------|-----------------|
| 334.56          | 334.50          |
| 4.74            | 4.80            |
| 12 <sup>E</sup> | 10 <sup>E</sup> |
| Gar. floor      | Apron           |

2+80 9' Lt. = £ 3' Conc. walk.

|                 |         |        |       |       |       |                 |
|-----------------|---------|--------|-------|-------|-------|-----------------|
| 335.05          | 335.00  | 335.00 | 334.5 | 334.2 | 333.8 | 333.84          |
| 4.25            | 4.30    | 4.30   | 4.8   | 5.1   | 5.5   | 5.46            |
| 11 <sup>2</sup> | 10      | 9      | 7     |       | 10    | 10 <sup>E</sup> |
| at. step.       | on walk |        |       |       |       | Edge apron      |

2+77 = £ 3<sup>rd</sup> Gar.

|                 |                 |                    |
|-----------------|-----------------|--------------------|
| 333.83          | 333.79          | 333.9 <sup>5</sup> |
| 5.47            | 5.51            | 5.35               |
| 10 <sup>E</sup> | 11 <sup>E</sup> | 1A                 |
| on apron        |                 | Gar Floor          |

2+72- 8' Lt. = (W)

2+66 £ 2<sup>nd</sup> Gar.

|                 |                 |           |
|-----------------|-----------------|-----------|
| 333.83          | 333.78          | 333.92    |
| 5.47            | 5.52            | 5.38      |
| 10 <sup>E</sup> | 11 <sup>E</sup> | 13        |
| on apron        |                 | Gar Floor |

£ 1<sup>st</sup> Gar.2+56 10<sup>E</sup> Rt. = edge apron

|                 |                 |            |
|-----------------|-----------------|------------|
| 333.75          | 333.70          | 333.90     |
| 5.55            | 5.60            | 5.40       |
| 10 <sup>E</sup> | 11 <sup>E</sup> | 13         |
| Apron           |                 | Gar. floor |

339.30



Alley Bk. 195  
City Hqts

±

56

T.P. 3.48 336.52 6126 333.04  
3+31- 13<sup>E</sup> RT. = start. stucco Bldg, on  
Con. foundation wall,

330.3  
9.0  
14<sup>E</sup> Floor E160

3+30 14<sup>E</sup> RT. = Ely face 8" Conc. wall (3' long)

333.3 333.3 333.2 333.4 333.6 330.0 329A  
6.0 6.0 6.1 5.9 5.7 9.3 9.9  
15 10 10 14<sup>E</sup> 15 20  
Ground

3+28 - 9' Lt. = (W)

3+25<sup>E</sup> 11' RT. = Top landing to Conc. steps.

334.00 334.01 327.57  
5.30 5.29 11.73  
11<sup>E</sup> 13<sup>E</sup> 22<sup>E</sup>  
on walk  
bottom of  
steps

3+2A 13<sup>E</sup> RT. = end Bldg.  
11' RT. = end conc. apron

334.01 334.11  
5.29 5.19  
11<sup>E</sup> 13<sup>E</sup>  
on apron

3+22 - 8' Lt. = (W)

3+09 - 10<sup>E</sup> RT. = edge Apron  
= ± 4<sup>th</sup> Gar.

333.95 334.06 334.17  
5.35 5.24 5.13  
10<sup>E</sup> 13 13<sup>E</sup>  
Apron Gar  
Floor

3+06 - 13<sup>E</sup> Lt. = ± Sing. Gar. dirt floor

334.11  
5.2  
13<sup>E</sup>

3+04 - 9' RT. = (W)

3+00 10<sup>E</sup> RT. = ± 6' wide entrance way,

334.2 333.9 333.8 333.9 333.89 334.07 334.07  
5.1 5.4 5.5 5.4 5.21 5.23 5.23  
10 7 10 10<sup>E</sup> 13A 19  
on Apron Conc.

339.30



Alley Bk 195  
City Hqts

57

3+71 9' Lt. = (W)

3+66 - 62' Rt. = 7' high fig tree

see survey storm drain  
Bk. 195

3+64 67<sup>E</sup> Rt. = top N. & S. wall.

77' Rt. = L drain opening - see note

53' Rt. = 8' high eugenia

32' Rt. = 5' high peach tree 1" boards - 4x4 posts.

3+63 7' Rt. = start board retaining fence  
9' Rt.

3+62<sup>E</sup> = 1/2 8" wide E+W. Ret. wall

3+62 9' Rt. = (W)

3+60 - 13<sup>E</sup> Rt. = end stucco Bldg.

3+44

3+37 10' Lt. = 1/2 sing. car dirt floor

|                 |       |       |
|-----------------|-------|-------|
| 327.6           | 325.7 | 325.3 |
| 8.9             | 10.8  | 11.2  |
| 67 <sup>E</sup> | 68    | 77'   |
| top             |       |       |
| wall            |       |       |

|       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 332.2 | 332.3 | 332.0 | 332.2 | 332.9 | 332.9 | 329.5 | 328.1 |
| 3.3   | 4.2   | 4.5   | 4.3   | 3.6   | 3.6   | 7.0   | 8.4   |
| 10    | 9     | 4     | 5     | 9     | 10    | 20    |       |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 332.2 | 332.3 | 333.0 | 334.6 | 327.9 |
| 3.3   | 4.2   | 3.5   | 1.9   | 8.6   |
| 10    | 9     | 9     | 9     | 9     |
|       |       | End   | Top   | Base  |

|       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 333.4 | 333.4 | 332.5 | 332.4 | 332.2 | 333.0 | 333.6 | 332.8 |
| 3.1   | 3.1   | 4.0   | 4.4   | 4.3   | 3.5   | 3.5   | 3.7   |
| 15    | 10    | 9     |       | 4     | 6     | 10    | 13    |

|       |       |       |
|-------|-------|-------|
| 333.4 | 333.0 | 333.4 |
| 3.7   | 3.5   | 3.1   |
| 10    |       | 10    |

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 332.5 | 332.5 | 332.9 | 333.1 | 333.3 |
| 4.0   | 4.0   | 3.6   | 3.4   | 3.2   |
| 10    | 8     | 6     |       | 10    |

336.52



Alley B/K 195  
City Hqts.

58

12<sup>3</sup> Rt. = 12" trunk accacia  
 4+46 9' Lt. = (W)  
 4+45- 15<sup>3</sup> Lt. = end Conc. Apron to double Gar.  
 4+35 12' Rt. = 8" trunk Accacia  
 4+28- 15<sup>6</sup> Lt. = start Conc. Apron to double Gar.

530.20 330.18  
 6.32 6.34  
 162 153  
 Gar. Floor Apron  
 330.22 330.20  
 6.30 6.32  
 164 156  
 Gar. Floor Apron

4+27 - 12<sup>5</sup> Rt. = Ctr. 10" trunk Accacia  
 Also = Nly Face 6" wide E+W. Conc. wall.  
 9<sup>3</sup> Rt. = end 9" wide Conc. wall  
 4+22 8' Rt. = pole # JPA 3952

330.2 329.8 329.6 329.1 329.20 328.1  
 6.3 6.7 6.9 7.4 7.32 8.4  
 10 4 9 9.3 11-End  
 wall by wall

4+15- 8' Rt. = (W)

10<sup>8</sup> Lt. = Face 9' Conc. wall.  
 4+00 9<sup>9</sup> Lt. = end board garage

331.3 330.7 330.7 329.5 329.7 327.5  
 5.2 5.8 5.8 7.0 6.8 9.0  
 10 9 10 10.8 12  
 Top of End wall

3+98- 8' Rt. = (W)

3+95 9<sup>8</sup> Lt. = ± door to Gar. dirt floor.

331.4  
 5.1  
 9.8

3+87- 9<sup>8</sup> Lt. = start board garage.

3+85- 11 Rt. = start 9" Conc. Ret. wall.

333.4 333.3 331.6 331.1 330.9 329.5 329.5 329.1 327.8  
 3.1 3.2 4.9 5.4 5.6 7.0 7.0 8.4 8.7  
 15 10 9 8 10 11 12 15  
 Top wall

336.52



5+07 Top of new fill.

4+98 = Ctr. M.H. - (This has just been raised.)

T.P. 9.89 339.98 0.62 330.09

4+98 ~~±~~ M.H.

4+97- 11<sup>2</sup> Lt. = Water meter. No box up in air

4+95 15<sup>2</sup> Lt. = end conc. wall

4+90 = Toe of New loose fill.

(see drain survey)

4+60 { 38<sup>5</sup> Ft. = E. Nly end. drain Ret. wall.  
10<sup>2</sup> = west end - east face E+W.

4+55 11<sup>5</sup> Ft. = 12" trunk accacia

Nail in pole P.A. 3957

T.P. 0.62 330.71 6.43 330.09

4+50 9' Lt. = Pole # P.A. 3957

4+49- 15<sup>4</sup> Lt. = start conc Ret. wall.

335.5 335.4 335.4 332.0  
4.5 4.6 4.6 8.0  
10 10 20

332.32  
7.66  
Rim

339.98

331.3 329.7  
+0.6 1.0  
152 152  
top of end  
wall

327.8 327.8 325.9 324.9 323.3 323.1 325.2  
2.9 2.9 4.8 5.8 7.4 7.6 5.5  
152 10 8 10 16 25  
at wall

328.7 331.7 328.7 327.3 326.8 328.0 325.4 320.9 327.4  
2.0 7.0 2.0 3.4 3.9 2.7 5.3 9.8 3.3  
152 152 10 10 102 17 385 385  
End. Top of I.E. Top  
wall drain wall

330.71

331.52 331.52 329.7 329.7 329.1 328.9 328.0  
5.0 5.8 6.8 6.8 7.4 7.6 8.5  
10 154 154 10 4 10  
top of end  
wall

336.52



Alley B/K 195

60

5+94<sup>5</sup> 10' Lt. = B.C. 2' Rad curb. Ret.

|          |        |
|----------|--------|
| 335.87   | 335.22 |
| 4.11     | 4.76   |
| 10       | 10     |
| cc. B.C. | G      |

5+87<sup>4</sup> 13<sup>2</sup> Rt. = B.C. 2' Rad alley Ret.

|                 |                 |
|-----------------|-----------------|
| 335.87          | 336.46          |
| 4.11            | 3.52            |
| 13 <sup>2</sup> | 13 <sup>2</sup> |
| G               | cc. B.C.        |

5+85<sup>3</sup> = intersect sly 7' line Lincoln

|                 |                 |
|-----------------|-----------------|
| 335.86          | 335.71          |
| 4.12            | 4.27            |
| 10 <sup>1</sup> | 10 <sup>1</sup> |
| cc              | G               |

5+81<sup>2</sup> - 10' Lt. = start alley cl. + pave

5+80 - 10<sup>2</sup> Lt. = Telephone pole. No. #

|       |       |
|-------|-------|
| 336.3 | 335.8 |
| 3.7   | 4.2   |
| 10    |       |

5+78<sup>2</sup> start A.C. Pave.

5+75<sup>66</sup> 9<sup>8</sup> Rt. = start alley cl. + pave

|       |       |                |                |
|-------|-------|----------------|----------------|
| 336.5 | 335.8 | 336.12         | 336.44         |
| 3.5   | 4.2   | 3.86           | 3.54           |
| 10    |       | 9 <sup>8</sup> | 9 <sup>8</sup> |
|       |       | G              | cc             |

5+50 Approx. Emd. new fill

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 337.5 | 337.5 | 337.1 | 337.3 | 337.2 |
| 2.5   | 2.5   | 2.9   | 2.7   | 2.8   |
| 20    | 10    |       | 10    | 20    |

339.98



Alley Blk 195  
City Hqts.

61

|           |      |        |             |
|-----------|------|--------|-------------|
| orig B.M. | 4.88 | 333.43 | (333.44)    |
| T.P.      | 4.15 | 338.31 | 7.19 334.16 |
| T.P.      | 2.72 | 341.35 | 7.12 338.63 |
|           |      | 4.73   | 341.02      |

N.W.B.P. Boundary & Union

Set. B.M. S.E. Nail in cl. Boundary & Lincoln

|      |      |        |      |        |
|------|------|--------|------|--------|
| T.P. | 9.01 | 345.75 | 3.24 | 336.74 |
|------|------|--------|------|--------|

5+93<sup>2</sup> Cont. 12<sup>3</sup> Lt. = start curb inlet

|                 |                 |
|-----------------|-----------------|
| 336.38          | 335.40          |
| 3.60            | 4.58            |
| 12 <sup>2</sup> | 12 <sup>3</sup> |
| Top. N.         | Start Inlet     |

Section Along sly. cl. Lincoln.

5+93<sup>3</sup> intersect sly. cl. line Lincoln  
Back to

|                 |                 |        |                 |                 |        |        |
|-----------------|-----------------|--------|-----------------|-----------------|--------|--------|
| 335.96          | 335.43          | 335.66 | 335.95          | 336.27          | 335.97 | 336.47 |
| 4.02            | 4.55            | 4.32   | 4.03            | 3.61            | 4.01   | 3.49   |
| 12 <sup>2</sup> | G               |        | 16 <sup>2</sup> | 16 <sup>2</sup> | 50     | 50     |
| cl.             | 12 <sup>2</sup> |        | G               | cl. EIC.        | G      | cl.    |
| EIC.            |                 |        |                 |                 |        |        |



X-SEC. FOR PAVING ALLEY BLK 2

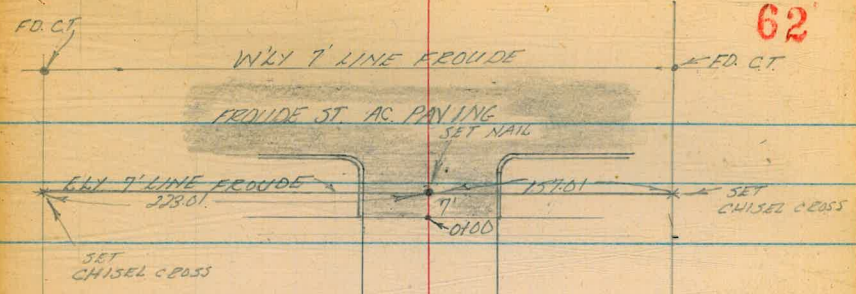
OCEAN BEACH  
CONT. PG. 65

COTA  
PULLEN  
BRUNER

W.O.# 31821  
6-28-51

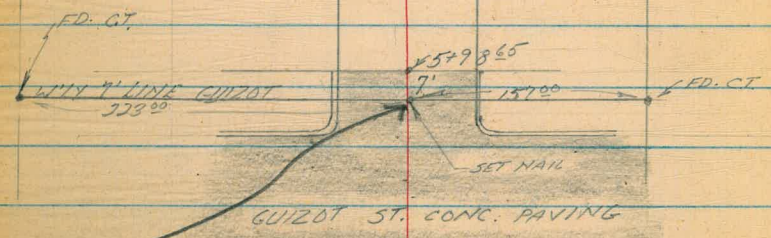
IMPROVED  
Law  
JUN 29 1951

62



WLY 7' LINE FROUDE

WLY 7' LINE FROUDE



This point 1' to North of Alley.  
removed it & cut cross in  
pave on Alley. A-7457  
in true position. JH



63







N-SEC. ALLEY BLK 2 O.B  
 CONT. FROM PG 62

65

LT                      \$                      RT

0+00 102 FT BROWN WOODS WIRE FENCE

TP                      12.70 98.81A                      2.76                      86.11

98.81A

0+00 EAST PROP LINE FROUDE, END AC, 10° PT & UT TO END OF CBS.

|       |       |              |       |       |
|-------|-------|--------------|-------|-------|
| 85.53 | 85.32 | 85.26        | 85.91 | 86.17 |
| 354   | 375   | 3.71         | 3.16  | 290   |
| 100   | 100   | EDGE<br>A.C. | 100   | 100   |
| CB    | GUT   |              | GUT   | CB    |

(0-10)  
 0-02 EC 3° RAD. CB RETURNS 9° PT, 9° UT

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 85.44 | 85.09 | 85.18 | 85.69 | 86.07 |
| 363   | 398   | 3.89  | 3.38  | 300   |
| 99    | 99    |       | 99    | 99    |
| CB    | GUT   |       | GUT   | CB    |

(0-12)  
 0-05 EAST CB LINE FROUDE

|       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 84.49 | 83.86 | 84.86 | 85.30 | 85.16 | 86.07 | 85.46 | 86.33 | 86.96 |
| 4.58  | 5.21  | 4.21  | 3.77  | 3.91  | 3.00  | 3.11  | 3.74  | 2.11  |
| 50    | 50    | 13    | 13    |       | 13    | 13    | 50    | 50    |
| CB    | GUT   | GUT   | CB    |       | CB    | GUT   | GUT   | CB    |

1309 89.07A

75.98 SW. BR. FROUDE  
 & CAPE MAY

89.07A



X-SEC. ALLEY BLK 2. O.B.  
CONT. FROM PG. 65

LT.

2

RT.

66

1440 13.2 FT. CENTER DOUBLE GARAGE DIRT FLOOR

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 100.4 | 100.9 | 101.3 | 101.6 | 102.7 | 102.4 |
| 10.7  | 10.2  | 9.8   | 9.5   | 8.7   | 8.7   |
| 20    | 10    |       | 6     | 10    | 13.2  |
|       |       |       |       |       | CRD.  |

TP 13.02 111.17A 0.66 98.15

111.17A

1461 88 RT. & POLE # PA. 4584

1400 END FENCE 10° LT.

|      |      |      |      |      |
|------|------|------|------|------|
| 98.8 | 98.8 | 98.5 | 98.7 | 98.7 |
| 0.0  | 0.0  | 0.3  | 0.1  | 0.1  |
| 20   | 10   |      | 10   | 20   |

0482 10° LT & POLE NO NUMBER

0450

|      |      |      |      |      |
|------|------|------|------|------|
| 92.1 | 91.8 | 91.2 | 91.7 | 92.4 |
| 6.7  | 7.0  | 7.6  | 7.1  | 6.4  |
| 20   | 10   |      | 10   | 20   |

98.81A



V-SEC ALLEY BLK 2 O.B.  
CONT. FROM PG 66

LT.                      \$                      RT.                      67

2450 16" LT END CONC WALL, BEGIN 5" HIGH WOOD FENCE

|              |       |       |       |       |       |
|--------------|-------|-------|-------|-------|-------|
| 102.9        | 104.2 | 104.1 | 104.1 | 104.8 | 105.3 |
| 82           | 69    | 70    | 70    | 63    | 58    |
| 10           | 10    |       | 6     | 10    | 20    |
| FOOTING WALL |       |       |       |       |       |

2400 END CB, BEGIN CONC WALL 3" HIGH 16" LT

|                |        |       |       |       |       |       |
|----------------|--------|-------|-------|-------|-------|-------|
| 102.0          |        |       |       |       |       |       |
| 9.1            |        |       |       |       |       |       |
| 10             |        |       |       |       |       |       |
| FOOTING WALL   |        |       |       |       |       |       |
| 101.89         | 103.16 | 102.9 | 102.9 | 103.0 | 104.1 | 105.1 |
| 9.28           | 8.01   | 8.2   | 8.2   | 8.1   | 7.0   | 6.0   |
| 10             | 10     | 10    |       | 6     | 10    | 20    |
| FOOTING TOP CB |        |       |       |       |       |       |
| CB.            |        |       |       |       |       |       |

1499 8.6 RT POLE # DA 4568

1456 \$ SINGLE CAR-CONC FLOOR 17.5 RT

|       |         |       |       |       |       |             |
|-------|---------|-------|-------|-------|-------|-------------|
| 101.1 | 102.20  | 101.8 | 102.1 | 102.2 | 103.3 | 104.72      |
| 10.0  | 8.97    | 7.3   | 7.0   | 8.9   | 7.8   | 6.75        |
| 20    | 10      | 10    |       | 6     | 10    | 17.5        |
|       | TOP CB. |       |       |       |       | CONC. FLOOR |

1450 10" LT BEGIN CONC CB & 4" HIGH WOOD FENCE

|         |         |
|---------|---------|
| 102.09  | 101.43  |
| 9.08    | 9.74    |
| 10.0    | 10.0    |
| TOP CB. | FOOTING |

111.17X



X-SEC ALLEY BLK 2 O.B.  
CONT. FROM PG. 67

LT.

\$

BT.

68

3450 12.2 BT CORNER SHED

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 109.4 | 109.6 | 109.2 | 108.9 | 109.2 | 109.7 |
| 1.7   | 1.5   | 1.9   | 2.2   | 1.9   | 1.4   |
| 20    | 10    | 6     |       | 10    | 12    |

3421 11<sup>2</sup> BT CORNER SHED, BEGIN 5' HIGH WOOD FENCE

3401 11<sup>2</sup> BT CORNER SHED

3400 END 5' HIGH WOOD FENCE 10<sup>2</sup> LT.

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 106.0 | 106.4 | 106.0 | 106.0 | 107.2 | 107.2 |
| 5.1   | 4.7   | 5.1   | 5.1   | 3.9   | 3.9   |
| 20    | 10    |       | 5     | 10    | 20    |

2499 93 BT @ POLE #PA 4552

2460 10<sup>3</sup> LT 25 NIDE WALK

|        |        |
|--------|--------|
| 104.15 | 104.15 |
| 7.02   | 7.02   |
| 15     | 10.3   |
| WALK   | WALK   |

111.17A



N-SEC. ALLEY BLK 2 O.B.  
CONT. FROM PG 68

69

LT

¢

RT

A490 16 1/2 RT CENTER DOUBLE GARAGE - CONC. FLOOR

|                    |             |
|--------------------|-------------|
| 118.17             | 118.37      |
| 3.76               | 3.76        |
| 14.4               | 16.2        |
| APRON<br>(80 WIDE) | CONC. FLOOR |

A400 108 RT CORNER 4° HIGH WOOD FENCE

|       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|
| 113.8 | 113.4 | 113.7 | 114.0 | 114.7 | 114.7 |
| 8.3   | 8.7   | 8.4   | 8.1   | 7.4   | 7.4   |
| 10    | 5     |       | 7     | 10    | 20    |

3499 95 RT. & POLE # PA 45.36, 10<sup>3</sup> RT. COR. 4° HIGH WOOD FENCE

3469 94 RT BEGIN 6° HIGH WOOD FENCE

T.P. 11.78 122.13 X 0.97 110.20

122.13 X

3458 { 12.2 RT. COR. SHED  
17' 11" CENTER SINGLE GARAGE - CONC FLOOR

110.60  
0.57  
17.1  
CONC. FLOOR

111.17 X



X-SEC ALLEY BLK 2 O.B.  
CONT. FROM PG. 69

70

KP 12.3A 134.26A 0.21 121.92

A477 35.5 LT. CENTER GARAGE - DIRT FLOOR

111.2  
0.9  
35.5  
GROUND

A466 35.5 LT. CENTER GARAGE DIRT FLOOR

120.5  
1.6  
35.5  
GROUND

A454 13.6 FT. 30" TREE

A450

|       |       |       |       |       |
|-------|-------|-------|-------|-------|
| 119.1 | 118.5 | 118.6 | 118.5 | 118.4 |
| 3.0   | 3.6   | 3.5   | 3.6   | 3.7   |
| 20    | 10    |       | 10    | 20    |

A449 9' LT. END 6' HIGH WOOD FENCE

122.13A



X-SEC ALLEY BLK 2 O.B.  
CONT. FROM PG. 70

71

5432 17° RT. SINGLE GARAGE CONC FLOOR

129.40  
1.86  
17  
CONC FLOOR

5429 9° LT. END 5° HIGH FENCE

5403 98 FT GA. GOING NORTH. BEGIN 5° HIGH WOOD FENCE

125.54 124.32  
8.72 9.94  
9.8 9.8  
TOP OF FOOTING

5400 8.5 RT. POLE# PA # 4520

|       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|
| 123.6 | 124.0 | 123.6 | 123.7 | 123.8 | 124.6 | 124.8 |
| 10.6  | 10.2  | 10.6  | 10.5  | 10.4  | 9.6   | 9.4   |
| 20    | 10    | 7     |       | 5     | 10    | 20    |

4497 COR. DOUBLE GARAGE 28° RT. TO APRON 30° RT. TO CONC FLOOR

123.71 123.93  
10.55 10.33  
28° 30°  
APRON CONC FLOOR

4478 COR. DOUBLE GARAGE 28°<sup>RT</sup> TO APRON, 30° RT. TO CONC FLOOR

123.69 123.86  
10.57 10.40  
28° 30°  
APRON CONC FLOOR

134.267



X-SEC. ALLEY BLK 2 O.B.  
CONT. FROM PG. 71

5460 9<sup>6</sup> LT. END 5<sup>0</sup> HIGH WOOD FENCE

5450

129.6      129.7      130.6  
4.6      4.5      3.6  
9.5           10

5445 9<sup>6</sup> LT. BEGIN 5<sup>0</sup> HIGH WOOD FENCE

129.11      128.34  
5.15      5.92  
17<sup>0</sup>      9<sup>0</sup>  
FLOOR      APRON

5436 CENTER SINGLE GARAGE 9<sup>2</sup> LT. TO APRON 8<sup>0</sup> WIDE 17<sup>0</sup> LT TO CONC FLOOR

5436 11<sup>4</sup> RT BEGIN CONC BLK WALL

129.2  
50  
11<sup>1</sup>  
FOOTING

134.26 T



X-SEC ALLEY BLK 2 O.B.  
CONT. FROM PG. 72

73

BM CHECK

8.90 12470 = 12495 S.W. BR.  
CAPE MAY 5  
GUITZOT

T.P.

101 13380X

1.49 132.79

6+10.65 WEST CB LINE GUITZOT

|        |        |        |         |        |
|--------|--------|--------|---------|--------|
| 131.91 | 132.44 | 132.45 | 133.55  | 132.95 |
| 2.35   | 1.82   | 1.81   | 0.71    | 1.31   |
| 12     | 12     |        | 12      | 12     |
| GUT.   | TOP CB |        | TOP CB. | GUT.   |

5+78.65 WEST PL. GUITZOT 9' LEFT RT. TO END OF CBS  
105' RT. END CONC. BLK WALL.

|                    |              |        |        |                 |
|--------------------|--------------|--------|--------|-----------------|
| 132.79             | 132.75       | 133.18 | 133.52 | 132.77          |
| 1.47               | 1.51         | 1.08   | 0.74   | 1.49            |
| 9.9                | EDGE<br>RAVE | 9.9    | 9.9    | 10.6            |
| TOP CB<br>& GUTTER |              | GUT    | CB.    | FOOTING<br>WALL |

134.26 X



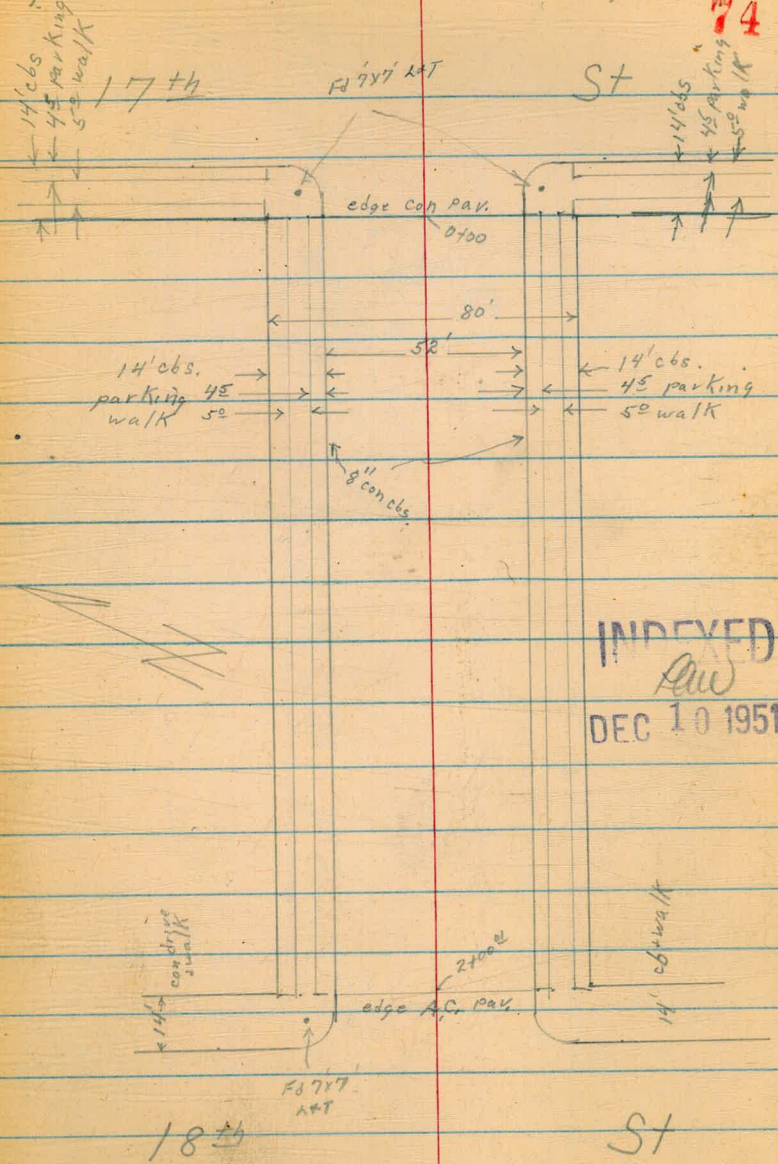
D. Smith  
G. Roberts  
W. Moore  
Basil Pullen

X Sec "A" St

17<sup>th</sup> to 18<sup>th</sup>

WO # 31540  
12-7-51

74





D. Smith  
G. Roberts  
W. Moore  
Pallen

Cross Sec "A" St 17th to 18th

W04 31540  
12-7-51

75

E Prop 17th

105.88  
8-37

105.48  
8-27

2/3

105.86  
8-39

105.43  
8-22

1/3

105.83  
8-42

105.43  
8-22

S Prop A

105.73  
8-52

105.34  
8-21

SE Return 10' Rad 24 length Prop to Prop  
3 parts 8' eq

E Prop 17th

106.21  
5-34

109.92  
6-33

2/3

109.24  
5-01

106.43  
5-22

1/3

109.57  
4-68

108.83  
5-42

North Prop A

109.86  
4-39

109.17  
5-08

NE Return 10' Rad 24 length Prop to Prop  
3 parts 8' eq

B.M. 316 11425

11109 NW BP  
17th St

11425

INDEXED  
Law  
MAY 4 1953



1700

|       |       |      |      |      |      |       |
|-------|-------|------|------|------|------|-------|
| North |       |      |      |      |      | South |
| LT    |       |      |      |      |      | RT    |
|       | 97.10 | 96.1 | 96.5 | 96.7 | 96.1 | 94.8  |
|       | 44    | 52   | 50   | 48   | 54   | 62    |
|       | 26    | 26   | 13   |      | 13   | 26    |
|       | cb    | gut  |      |      | gut  | cb    |

76

TP, 64 101<sup>54</sup> 13<sup>12</sup> 101<sup>13</sup>

101<sup>54</sup>

0469 End Broken cb

0468 RT End Broken cb

0450

|  |        |       |       |       |       |      |           |
|--|--------|-------|-------|-------|-------|------|-----------|
|  | 103.28 | 102.1 | 102.2 | 102.0 | 101.3 | 99.9 | 100.6     |
|  | 117    | 123   | 121   | 123   | 130   | 144  | 132       |
|  | 26     | 26    | 13    |       | 13    | 26   | 26        |
|  | cb     | gut   |       |       |       | gut  | cb broken |

0448 RT Begin Broken cb

0444 LT Begin Broken cb

0419<sup>5</sup> LT 17' con drive

|  |        |        |
|--|--------|--------|
|  | 106.45 | 105.94 |
|  | 760    | 831    |
|  | 305    | 26     |
|  | walk   | 41     |

0408 LT End Broken cb

0402 LT Begin Broken cb

|  |        |        |        |        |        |        |        |
|--|--------|--------|--------|--------|--------|--------|--------|
|  | 108.91 | 107.92 | 107.54 | 106.94 | 106.34 | 105.28 | 105.88 |
|  | 534    | 633    | 621    | 731    | 791    | 897    | 837    |
|  | 26     | 26     | 13     |        | 13     | 26     | 26     |
|  | cb     | gut    |        |        |        | gut    | cb     |

0400 E Prop 17<sup>th</sup> St edge con paving

0-14 E cb line 17<sup>th</sup> St

|  |        |        |        |        |        |        |        |        |        |        |        |        |        |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|  | 112.74 | 112.09 | 109.86 | 109.17 | 108.54 | 108.24 | 107.78 | 107.07 | 105.95 | 105.34 | 105.73 | 102.38 | 102.76 |
|  | 151    | 216    | 439    | 509    | 571    | 601    | 647    | 718    | 836    | 891    | 852    | 1187   | 1111   |
|  | 65     | 65     | 40     | 40     | 26     | 13     |        | 13     | 26     | 40     | 40     | 65     | 65     |
|  | cb     | gut    | cb     | gut    |        |        |        |        |        | gut    | cb     | gut    | cb     |

T 11425



2114 W cb Line 18<sup>th</sup>

2400 W Prop 18<sup>th</sup> St edge AC

1491 Lt Break in grade on cb

TP2 250 9/15 12<sup>89</sup> 88<sup>65</sup>

1436

1445 Lt & can drive

North  
Lt

86.85 86.49 86.29 85.98 85.62 85.48 85.28 85.13 84.96 84.83 85.52 85.44

4<sup>30</sup> 4<sup>22</sup> 4<sup>06</sup> 5<sup>27</sup> 5<sup>53</sup> 5<sup>67</sup> 5<sup>87</sup> 6<sup>02</sup> 6<sup>19</sup> 6<sup>32</sup> 5<sup>63</sup> 7<sup>21</sup>

65 65 40 40 26 13 13 26 40 40 65

cb 94t cb 94t 94t drive

86.21 85.72 85.85 85.74 85.44 85.05 85.03

4<sup>24</sup> 5<sup>43</sup> 5<sup>30</sup> 5<sup>41</sup> 5<sup>21</sup> 6<sup>10</sup> 5<sup>62</sup>

26 26 13 13 26 26

cb 94t 94t cb

86.55 86.3 86.3 86.4 86.1 85.8 86.26

4<sup>60</sup> 4<sup>9</sup> 4<sup>9</sup> 4<sup>8</sup> 5<sup>1</sup> 5<sup>4</sup> 4<sup>89</sup>

26 26 13 13 26 26

cb 94t 94t cb

91.23 90.2 90.7 91.0 90.6 89.6 90.66

10<sup>31</sup> 11<sup>3</sup> 10<sup>8</sup> 10<sup>5</sup> 10<sup>9</sup> 11<sup>2</sup> 10<sup>88</sup>

26 26 13 13 26 26

cb 94t 94t cb

91.97 91.13

9<sup>57</sup> 10<sup>41</sup>

305 26

walk Lin

10/54

77



|  |                         |                         |
|--|-------------------------|-------------------------|
| W Prop 18 <sup>th</sup>                  | <sup>85.53</sup><br>562 | <sup>85.03</sup><br>610 |
| $\frac{2}{3}$                            | <sup>85.52</sup><br>563 | <sup>84.99</sup><br>616 |
| $\frac{1}{3}$                            | <sup>85.46</sup><br>569 | <sup>84.95</sup><br>620 |
| South Prop AST                           | <sup>85.52</sup><br>563 | <sup>84.83</sup><br>632 |
| SW Return 10' Rad 24' length Propto Prop |                         |                         |

|                         |                         |                         |
|-------------------------|-------------------------|-------------------------|
| W Prop 18 <sup>th</sup> | <sup>86.21</sup><br>494 | <sup>85.72</sup><br>543 |
|-------------------------|-------------------------|-------------------------|

|               |                         |                         |
|---------------|-------------------------|-------------------------|
| $\frac{2}{3}$ | <sup>86.24</sup><br>491 | <sup>85.67</sup><br>548 |
|---------------|-------------------------|-------------------------|

|               |                         |                         |
|---------------|-------------------------|-------------------------|
| $\frac{1}{3}$ | <sup>86.28</sup><br>487 | <sup>85.68</sup><br>547 |
|---------------|-------------------------|-------------------------|

|  |                         |                         |
|--|-------------------------|-------------------------|
| N Prop AST                               | <sup>86.29</sup><br>486 | <sup>85.78</sup><br>537 |
| NW Return 10' Rad 24' length Propto Prop |                         |                         |

BM

1193 68<sup>10</sup> ✓  
NEBP 18<sup>th</sup> 2B ✓

T 91<sup>15</sup>TP<sub>3</sub>125 80<sup>03</sup>

1237

78 <sup>78</sup>



Stake Lots 37-38 BIK 38

Ocean Beach W020006  
4-7-53

79

C.H.S.  
Begg  
altman  
Schelin

Ref. Sheet 7656-L

" TIP.# 778

No map

BIK. is Regular

X denotes cut cross on edge  
of pavement

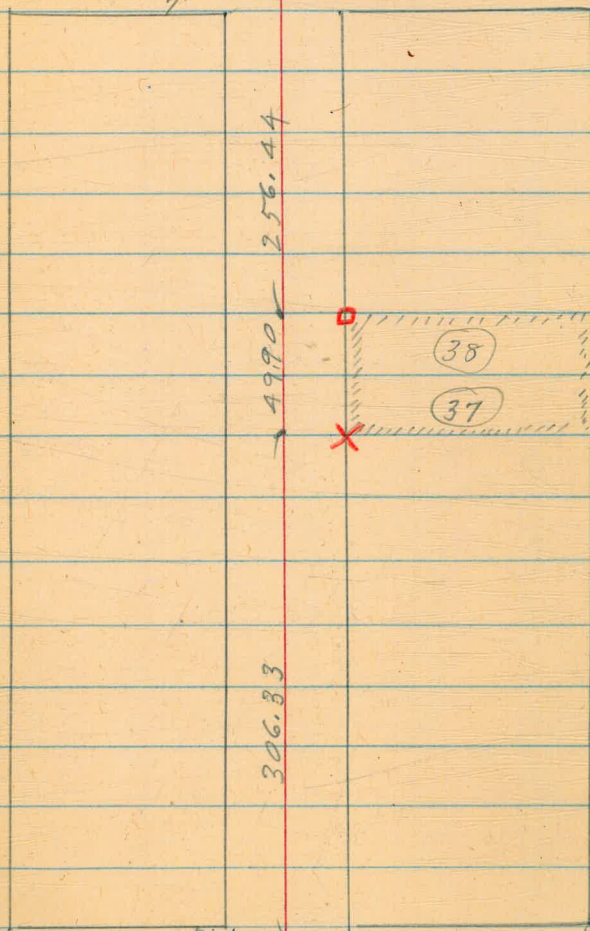
□ denotes set hub + copper nail

Sunset Cliffs Blvd.

Fol Nail

Del Mar. Ave

Coronado Ave



Ebers

Fol nail

St.

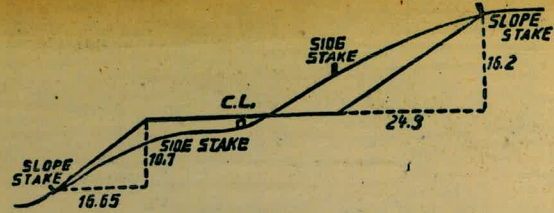


80



1749-69

4498.90



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

|    | 0     | .1    | .2    | .3    | .4    | .5    | .6    | .7    | .8    | .9    |    |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0  | 0.00  | 0.15  | 0.30  | 0.45  | 0.60  | 0.75  | 0.90  | 1.05  | 1.20  | 1.35  | 0  |
| 1  | 1.50  | 1.65  | 1.80  | 1.95  | 2.10  | 2.25  | 2.40  | 2.55  | 2.70  | 2.85  | 1  |
| 2  | 3.00  | 3.15  | 3.30  | 3.45  | 3.60  | 3.75  | 3.90  | 4.05  | 4.20  | 4.35  | 2  |
| 3  | 4.50  | 4.65  | 4.80  | 4.95  | 5.10  | 5.25  | 5.40  | 5.55  | 5.70  | 5.85  | 3  |
| 4  | 6.00  | 6.15  | 6.30  | 6.45  | 6.60  | 6.75  | 6.90  | 7.05  | 7.20  | 7.35  | 4  |
| 5  | 7.50  | 7.65  | 7.80  | 7.95  | 8.10  | 8.25  | 8.40  | 8.55  | 8.70  | 8.85  | 5  |
| 6  | 9.00  | 9.15  | 9.30  | 9.45  | 9.60  | 9.75  | 9.90  | 10.05 | 10.20 | 10.35 | 6  |
| 7  | 10.50 | 10.65 | 10.80 | 10.95 | 11.10 | 11.25 | 11.40 | 11.55 | 11.70 | 11.85 | 7  |
| 8  | 12.00 | 12.15 | 12.30 | 12.45 | 12.60 | 12.75 | 12.90 | 13.05 | 13.20 | 13.35 | 8  |
| 9  | 13.50 | 13.65 | 13.80 | 13.95 | 14.10 | 14.25 | 14.40 | 14.55 | 14.70 | 14.85 | 9  |
| 10 | 15.00 | 15.15 | 15.30 | 15.45 | 15.60 | 15.75 | 15.90 | 16.05 | 16.20 | 16.35 | 10 |
| 11 | 16.50 | 16.65 | 16.80 | 16.95 | 17.10 | 17.25 | 17.40 | 17.55 | 17.70 | 17.85 | 11 |
| 12 | 18.00 | 18.15 | 18.30 | 18.45 | 18.60 | 18.75 | 18.90 | 19.05 | 19.20 | 19.35 | 12 |
| 13 | 19.50 | 19.65 | 19.80 | 19.95 | 20.10 | 20.25 | 20.40 | 20.55 | 20.70 | 20.85 | 13 |
| 14 | 21.00 | 21.15 | 21.30 | 21.45 | 21.60 | 21.75 | 21.90 | 22.05 | 22.20 | 22.35 | 14 |
| 15 | 22.50 | 22.65 | 22.80 | 22.95 | 23.10 | 23.25 | 23.40 | 23.55 | 23.70 | 23.85 | 15 |
| 16 | 24.00 | 24.15 | 24.30 | 24.45 | 24.60 | 24.75 | 24.90 | 25.05 | 25.20 | 25.35 | 16 |
| 17 | 25.50 | 25.65 | 25.80 | 25.95 | 26.10 | 26.25 | 26.40 | 26.55 | 26.70 | 26.85 | 17 |
| 18 | 27.00 | 27.15 | 27.30 | 27.45 | 27.60 | 27.75 | 27.90 | 28.05 | 28.20 | 28.35 | 18 |
| 19 | 28.50 | 28.65 | 28.80 | 28.95 | 29.10 | 29.25 | 29.40 | 29.55 | 29.70 | 29.85 | 19 |
| 20 | 30.00 | 30.15 | 30.30 | 30.45 | 30.60 | 30.75 | 30.90 | 31.05 | 31.20 | 31.35 | 20 |
| 21 | 31.50 | 31.65 | 31.80 | 31.95 | 32.10 | 32.25 | 32.40 | 32.55 | 32.70 | 32.85 | 21 |
| 22 | 33.00 | 33.15 | 33.30 | 33.45 | 33.60 | 33.75 | 33.90 | 34.05 | 34.20 | 34.35 | 22 |
| 23 | 34.50 | 34.65 | 34.80 | 34.95 | 35.10 | 35.25 | 35.40 | 35.55 | 35.70 | 35.85 | 23 |
| 24 | 36.00 | 36.15 | 36.30 | 36.45 | 36.60 | 36.75 | 36.90 | 37.05 | 37.20 | 37.35 | 24 |
| 25 | 37.50 | 37.65 | 37.80 | 37.95 | 38.10 | 38.25 | 38.40 | 38.55 | 38.70 | 38.85 | 25 |
| 26 | 39.00 | 39.15 | 39.30 | 39.45 | 39.60 | 39.75 | 39.90 | 40.05 | 40.20 | 40.35 | 26 |
| 27 | 40.50 | 40.65 | 40.80 | 40.95 | 41.10 | 41.25 | 41.40 | 41.55 | 41.70 | 41.85 | 27 |
| 28 | 42.00 | 42.15 | 42.30 | 42.45 | 42.60 | 42.75 | 42.90 | 43.05 | 43.20 | 43.35 | 28 |
| 29 | 43.50 | 43.65 | 43.80 | 43.95 | 44.10 | 44.25 | 44.40 | 44.55 | 44.70 | 44.85 | 29 |
| 30 | 45.00 | 45.15 | 45.30 | 45.45 | 45.60 | 45.75 | 45.90 | 46.05 | 46.20 | 46.35 | 30 |
| 31 | 46.50 | 46.65 | 46.80 | 46.95 | 47.10 | 47.25 | 47.40 | 47.55 | 47.70 | 47.85 | 31 |
| 32 | 48.00 | 48.15 | 48.30 | 48.45 | 48.60 | 48.75 | 48.90 | 49.05 | 49.20 | 49.35 | 32 |
| 33 | 49.50 | 49.65 | 49.80 | 49.95 | 50.10 | 50.25 | 50.40 | 50.55 | 50.70 | 50.85 | 33 |
| 34 | 51.00 | 51.15 | 51.30 | 51.45 | 51.60 | 51.75 | 51.90 | 52.05 | 52.20 | 52.35 | 34 |
| 35 | 52.50 | 52.65 | 52.80 | 52.95 | 53.10 | 53.25 | 53.40 | 53.55 | 53.70 | 53.85 | 35 |
| 36 | 54.00 | 54.15 | 54.30 | 54.45 | 54.60 | 54.75 | 54.90 | 55.05 | 55.20 | 55.35 | 36 |
| 37 | 55.50 | 55.65 | 55.80 | 55.95 | 56.10 | 56.25 | 56.40 | 56.55 | 56.70 | 56.85 | 37 |
| 38 | 57.00 | 57.15 | 57.30 | 57.45 | 57.60 | 57.75 | 57.90 | 58.05 | 58.20 | 58.35 | 38 |
| 39 | 58.50 | 58.65 | 58.80 | 58.95 | 59.10 | 59.25 | 59.40 | 59.55 | 59.70 | 59.85 | 39 |
| 40 | 60.00 | 60.15 | 60.30 | 60.45 | 60.60 | 60.75 | 60.90 | 61.05 | 61.20 | 61.35 | 40 |
| 41 | 61.50 | 61.65 | 61.80 | 61.95 | 62.10 | 62.25 | 62.40 | 62.55 | 62.70 | 62.85 | 41 |
| 42 | 63.00 | 63.15 | 63.30 | 63.45 | 63.60 | 63.75 | 63.90 | 64.05 | 64.20 | 64.35 | 42 |
| 43 | 64.50 | 64.65 | 64.80 | 64.95 | 65.10 | 65.25 | 65.40 | 65.55 | 65.70 | 65.85 | 43 |
| 44 | 66.00 | 66.15 | 66.30 | 66.45 | 66.60 | 66.75 | 66.90 | 67.05 | 67.20 | 67.35 | 44 |
| 45 | 67.50 | 67.65 | 67.80 | 67.95 | 68.10 | 68.25 | 68.40 | 68.55 | 68.70 | 68.85 | 45 |
| 46 | 69.00 | 69.15 | 69.30 | 69.45 | 69.60 | 69.75 | 69.90 | 70.05 | 70.20 | 70.35 | 46 |
| 47 | 70.50 | 70.65 | 70.80 | 70.95 | 71.10 | 71.25 | 71.40 | 71.55 | 71.70 | 71.85 | 47 |
| 48 | 72.00 | 72.15 | 72.30 | 72.45 | 72.60 | 72.75 | 72.90 | 73.05 | 73.20 | 73.35 | 48 |
| 49 | 73.50 | 73.65 | 73.80 | 73.95 | 74.10 | 74.25 | 74.40 | 74.55 | 74.70 | 74.85 | 49 |
| 50 | 75.00 | 75.15 | 75.30 | 75.45 | 75.60 | 75.75 | 75.90 | 76.05 | 76.20 | 76.35 | 50 |

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