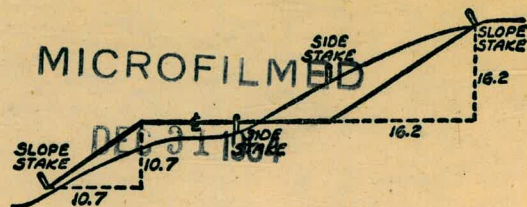


2082

TRUST BOOK





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

42 74  
6 64  
36 72

42 38  
6 64  
36 34

INDEXED  
to page # 579  
except page # 30



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.895	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

X SECTION TOOLEY-W.L. PARADISE c.w.s. to E.L. PARA. ON NORTH <sup>1-3</sup>  
 X - Section - Paradise-Tooley to Mallard #.  
 " " Alley Blk 39, Fairmount Add. 2078  
 Paradise Hills - Survey Storm Drain 29-41  
 Bro Sewer, Paradise Hills, Blk 14 - 42-51  
 X Sec Pump house - Patomac St. 52  
 Winchester - X Sec. 59  
 Ext. Drain - 32d. S. of Thorn 67



3-6-50

Moore  
Beag  
Shoemaker  
Crawford

Sketch, FB, 1859-67

< & P<sub>7</sub>

2

W. O. 25020

X-Section TOOLEY - Paradise to South  
To Paradise to North.

INDEXED

W.K.  
MAR 7 1950

REDUCED 3-7-50  
P.V.S.

1+00

359 <sup>1</sup>		358 <sup>0</sup>	358 <sup>1</sup>	357 <sup>9</sup>
4.9		6.0	5.9	6.1
30			10	30

0+50

300 <sup>3</sup>		300 <sup>2</sup>	A 360	360 <sup>0</sup>
3.7		3.8	3.6	4.0
30			10	30

0+00 = E. Line PARADISE To South

362 <sup>2</sup>	362 <sup>1</sup>	361 <sup>7</sup>	361 <sup>6</sup>	361 <sup>6</sup>	361 <sup>9</sup>
1.8	1.9	2.3	2.4	2.4	2.1
50	30		10	30	50

BM 2" pipe 1.95. 464.01  
Δ Pt. N.E. Tooley  
at Paradise  
1859-51

462.06

464.01



x Sect TOOLEY From E.L. PARADISE  
 TO SOUTH TO W.L. PARADISE TO NORTH

2+45

<del>425</del> <sup>1</sup>	<del>433</del> <sup>1</sup>	<del>433</del> <sup>2</sup>	<del>432</del> <sup>8</sup>	<del>432</del> <sup>9</sup>
28.9	30.3	30.8	31.2	31.8
<u>30</u>		<u>10</u>	<u>30</u>	<u>40</u>

2+25

E.L. Paradise to North

<del>439</del> <sup>3</sup>	<del>439</del> <sup>4</sup>	<del>438</del> <sup>1</sup>	<del>437</del> <sup>4</sup>	<del>436</del> <sup>7</sup>	<del>435</del> <sup>8</sup>
24.7	24.6	25.9	26.6	27.3	28.2
<u>30</u>	<u>20</u>		<u>10</u>	<u>30</u>	<u>40</u>

1+95 = ~~4~~ PARADISE TO NORTH

<del>446</del> <sup>6</sup>	<del>443</del> <sup>8</sup>	<del>443</del> <sup>3</sup>	<del>441</del> <sup>7</sup>	<del>440</del> <sup>4</sup>
17.4	20.2	20.7	22.3	23.6
<u>30</u>		<u>10</u>	<u>30</u>	<u>40</u>

1+65 = W. Line Paradise to North

<del>453</del> <sup>3</sup>	<del>452</del> <sup>8</sup>	<del>451</del> <sup>1</sup>	<del>450</del> <sup>3</sup>	<del>448</del> <sup>6</sup>	<del>447</del> <sup>9</sup>
10.7	11.2	12.9	13.7	15.4	16.1
<u>30</u>	<u>6</u>		<u>10</u>	<u>30</u>	<u>50</u>

1+45

<del>455</del> <sup>6</sup>	<del>454</del> <sup>5</sup>	<del>454</del> <sup>7</sup>	<del>453</del> <sup>6</sup>	<del>451</del> <sup>1</sup>	<del>451</del> <sup>2</sup>
8.4	9.5	9.3	10.4	12.1	12.8
<u>30</u>		<u>4</u>	<u>10</u>	<u>30</u>	<u>50</u>

464.01

464.01



SKETCH-1859-62

xsect Paradise-Tooley To MALLARD

1+00

INDEXED

MAR 7 1950

0+65

REDUCED 3-7-50  
P.V.S.

0+40

0+00 = N.L. TOOLEY

TP

8.07

460.23

11.85

452.16

460.23

TP

464.01

464.01

LT

R

RT

4561	4661	4555	4551	4540	4525	4491	4476	4428
3.5	3.5	4.7	4.8	6.2	7.7	10.8	12.6	17.4
30	28	21	12		10	24	30	45

4550	4540	4522	4523	4490	4428	4400
4.4	6.2	6.2	7.9	11.2	17.4	20.2
30	20	10		10	30	45

4522	4521	4520	4481	4460	4414	4386
6.0	7.5	7.6	11.5	14.2	18.8	21.6
30	20	12		10	30	45

4531	4520	4472	4465	4463	4381	4359
7.0	8.2	12.5	13.7	15.9	21.5	24.3
30	13	5		10	30	45



2+60

2+20

1+80

1+65

1+45

460.23

LT

~~E~~

RT

5

$\begin{array}{r} 457^3 \\ 2.9 \\ \hline 30 \end{array}$	$\begin{array}{r} 456^4 \\ 3.8 \\ \hline 30 \end{array}$	$\begin{array}{r} 456^3 \\ 3.9 \\ \hline 5 \end{array}$	$\begin{array}{r} 457^0 \\ 3.2 \\ \hline 10 \end{array}$	$\begin{array}{r} 458^2 \\ 2.0 \\ \hline 21 \end{array}$	$\begin{array}{r} 457^1 \\ 3.1 \\ \hline 30 \end{array}$
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$\begin{array}{r} 457^1 \\ 2.5 \\ \hline 30 \end{array}$	$\begin{array}{r} 456^9 \\ 3.3 \\ \hline 10 \end{array}$	$\begin{array}{r} 457^0 \\ 3.0 \\ \hline 30 \end{array}$	$\begin{array}{r} 457^1 \\ 3.1 \\ \hline 10 \end{array}$	$\begin{array}{r} 457^1 \\ 3.1 \\ \hline 20 \end{array}$	$\begin{array}{r} 455^1 \\ 4.5 \\ \hline 30 \end{array}$
--	--	--	--	--	--

$\begin{array}{r} 458^0 \\ 2.2 \\ \hline 30 \end{array}$	$\begin{array}{r} 457^3 \\ 2.9 \\ \hline 23 \end{array}$	$\begin{array}{r} 457^4 \\ 2.8 \\ \hline 12 \end{array}$	$\begin{array}{r} 456^8 \\ 3.4 \\ \hline 30 \end{array}$	$\begin{array}{r} 455^6 \\ 4.6 \\ \hline 10 \end{array}$	$\begin{array}{r} 453^4 \\ 6.8 \\ \hline 30 \end{array}$	$\begin{array}{r} 451^5 \\ 8.7 \\ \hline 40 \end{array}$
--	--	--	--	--	--	--

$\begin{array}{r} 457^9 \\ 2.3 \\ \hline 30 \end{array}$	$\begin{array}{r} 457^0 \\ 3.2 \\ \hline 23 \end{array}$	$\begin{array}{r} 457^1 \\ 3.1 \\ \hline 11 \end{array}$	$\begin{array}{r} 457^1 \\ 2.4 \\ \hline 30 \end{array}$	$\begin{array}{r} 456^6 \\ 3.6 \\ \hline 10 \end{array}$	$\begin{array}{r} 452^1 \\ 7.1 \\ \hline 30 \end{array}$	$\begin{array}{r} 449^3 \\ 10.9 \\ \hline 45 \end{array}$
--	--	--	--	--	--	---

$\begin{array}{r} 458^0 \\ 2.2 \\ \hline 30 \end{array}$	$\begin{array}{r} 456^1 \\ 3.5 \\ \hline 23 \end{array}$	$\begin{array}{r} 456^8 \\ 3.4 \\ \hline 12 \end{array}$	$\begin{array}{r} 456^0 \\ 4.2 \\ \hline 30 \end{array}$	$\begin{array}{r} 453^5 \\ 4.7 \\ \hline 10 \end{array}$	$\begin{array}{r} 452^1 \\ 7.5 \\ \hline 30 \end{array}$	$\begin{array}{r} 449^2 \\ 11.0 \\ \hline 45 \end{array}$
--	--	--	--	--	--	---

460.23



4+50

4+20

4+20

TP

0.20

450.94  
mm

9.49

450.74

3+90

3+50

3+00

460.23  
mm

LT

432<sup>8</sup>  
18.1  
40

435<sup>2</sup>  
15.7  
30

443<sup>1</sup>  
7.8

ET  
447<sup>2</sup>  
3.7  
10

447<sup>5</sup>  
3.4  
22

448<sup>9</sup>  
2.0  
24

6

450<sup>1</sup>  
0.8  
30

439<sup>7</sup>  
11.2  
40

443<sup>2</sup>  
7.7  
30

450<sup>9</sup>  
0.0

450<sup>7</sup>  
0.2  
10

450<sup>5</sup>  
0.4  
21

452<sup>1</sup>  
+1.2  
23

452<sup>6</sup>  
+1.7  
30

450.94  
mm

449<sup>0</sup>  
11.2  
30

451<sup>6</sup>  
8.6  
20

452<sup>4</sup>  
7.8

453<sup>1</sup>  
7.1  
10

453<sup>0</sup>  
7.2  
21

454<sup>3</sup>  
5.9  
23

454<sup>1</sup>  
6.1  
30

453<sup>5</sup>  
6.7  
30

454<sup>8</sup>  
5.4

454<sup>9</sup>  
5.3  
10

455<sup>3</sup>  
4.9  
23

455<sup>6</sup>  
4.7  
30

456<sup>1</sup>  
4.1  
30

456<sup>3</sup>  
4.0

456<sup>2</sup>  
4.0  
10

456<sup>2</sup>  
4.0  
30

460.23  
mm



6+05

LT				RT
405 <sup>01</sup>	x10 <sup>0</sup>	415 <sup>1</sup>	418 <sup>5</sup>	424 <sup>0</sup>
19.9	15.7	10.0	7.2	1.7
<u>50</u>	<u>30</u>		<u>10</u>	<u>30</u>

5+80

412 <sup>4</sup>	419 <sup>1</sup>	421 <sup>5</sup>	423 <sup>1</sup>	426 <sup>1</sup>
13.3	6.6	4.2	2.6	10.4
<u>50</u>	<u>30</u>		<u>10</u>	<u>30</u>

T.P.      0.05      425.66      12.90      425.61

425.66

5+50

417 <sup>4</sup>	420 <sup>3</sup>	426 <sup>3</sup>	429 <sup>6</sup>	433 <sup>8</sup>
21.1	18.2	12.0	8.7	4.7
<u>50</u>	<u>30</u>		<u>10</u>	<u>30</u>

T.P.      0.18      438.51      12.61      438.33

438.51

5+00

425 <sup>3</sup>	427 <sup>2</sup>	434 <sup>1</sup>	436 <sup>6</sup>	443 <sup>5</sup>	443 <sup>5</sup>
25.6	23.7	16.8	14.3	7.4	7.4
<u>45</u>	<u>30</u>		<u>10</u>	<u>23</u>	<u>30</u>

450.94

450.94



T.P. 0.94 390.77 12.79 389.83

7+20

T.P. 0.42 402.62 12.45 402.20

6+90

6+50

T.P. 2.00 414.65 13.01 412.65

425.66

LT

E

RT

8

390.77

380.2

22.4  
50

383.1

18.9  
30

391.1

10.9  
10

399.8

7.8  
10

399.5

3.1  
30

402.62

384.5  
30.2  
50

388.6  
26.1  
30

398.5  
16.2  
10

402.9  
11.8  
10

406.1  
8.2  
30

395.0

19.7  
50

400.2

14.5  
30

406.2

8.5  
10

410.0

4.7  
10

413.8

1.9  
30

414.65

425.66



9+00

$\frac{356^9}{21.7}$	$\frac{359^3}{19.3}$	$\frac{364^3}{14.3}$	$\frac{365^9}{12.7}$	$\frac{369^4}{9.2}$
	$\frac{\quad}{30}$		$\frac{\quad}{10}$	$\frac{\quad}{30}$

8+50

$\frac{360^7}{17.9}$	$\frac{364^0}{14.6}$	$\frac{369^3}{9.3}$	$\frac{372^4}{6.2}$	$\frac{376^4}{2.2}$
$\frac{\quad}{50}$	$\frac{\quad}{30}$		$\frac{\quad}{10}$	$\frac{\quad}{30}$

TP 0.59 378.57 12.79 377.98

378.57

8+00

$\frac{366^7}{24.1}$	$\frac{369^7}{21.1}$	$\frac{377^1}{13.7}$	$\frac{379^1}{11.7}$	$\frac{384^2}{5.9}$
$\frac{\quad}{50}$	$\frac{\quad}{30}$		$\frac{\quad}{10}$	$\frac{\quad}{30}$

7+50

$\frac{379^5}{16.3}$	$\frac{377^5}{13.3}$	$\frac{384^5}{6.3}$	$\frac{387^5}{3.3}$	$\frac{393^2}{+3.1}$
$\frac{\quad}{50}$	$\frac{\quad}{30}$		$\frac{\quad}{10}$	$\frac{\quad}{30}$

390.77

390.77



LT

+

RT.

10

10+50

$$\begin{array}{r} 345.4 \\ 8.9 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 346.4 \\ 7.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 349.9 \\ 4.9 \end{array}$$

$$\begin{array}{r} 351.1 \\ 3.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 352.9 \\ 1.4 \\ \hline 30 \end{array}$$

T.P.

0.60

354.31

12.75

353.71

354.31

10+00

$$\begin{array}{r} 350.4 \\ 16.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 350.9 \\ 15.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 354.0 \\ 12.5 \end{array}$$

$$\begin{array}{r} 355.1 \\ 11.4 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 357.9 \\ 8.6 \\ \hline 30 \end{array}$$

9+50

$$\begin{array}{r} 353.1 \\ 13.2 \\ \hline 45 \end{array}$$

$$\begin{array}{r} 355.1 \\ 11.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 359.9 \\ 6.6 \end{array}$$

$$\begin{array}{r} 360.9 \\ 5.6 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 363.3 \\ 3.2 \\ \hline 30 \end{array}$$

TP

0.70

366.46

12.81

365.76

366.46378.57

378.57



12+40

12+10

11+71 80 = Intersection W.L. Swanif  
E.L. Paradise

T.P. 3.77 345.50 12.58 341.73

11+50

11+00

354.31

LT	340 <sup>B</sup>	342 <sup>3</sup>	342 <sup>2</sup>	342 <sup>1</sup>	11
	4.7	3.2	3.1	2.8	
	<u>30</u>		<u>10</u>	<u>30</u>	

340 <sup>2</sup>	341 <sup>3</sup>	341 <sup>9</sup>	342 <sup>1</sup>
4.8	4.2	3.6	2.8
<u>30</u>		<u>10</u>	<u>30</u>

340 <sup>1</sup>	342 <sup>1</sup>	342 <sup>1</sup>	344 <sup>0</sup>
5.2	3.4	2.8	1.5
<u>30</u>		<u>10</u>	<u>30</u>

340 <sup>6</sup>	341 <sup>5</sup>	344 <sup>1</sup>	349 <sup>8</sup>	345 <sup>3</sup>
13.7	12.8	10.2	9.5	9.0
<u>40</u>	<u>30</u>		<u>10</u>	<u>30</u>

342 <sup>3</sup>	343 <sup>0</sup>	345 <sup>6</sup>	347 <sup>0</sup>	348 <sup>5</sup>
12.0	11.3	8.7	7.3	5.8
<u>40</u>	<u>30</u>		<u>10</u>	<u>30</u>

354.31



LT

E

R.

Check to B.M. P.L.  
Mon. P.O.T. 80'± W.  
OF PARADISE ON  
MALLARD - 1859.60

7.15  $\frac{338.35}{0.02}$

Note. Swan St. bladed since X Section.

13+12.52 This section parallel with  
Mallard.

$\frac{340}{5.0}$	$\frac{342}{2.8}$	$\frac{341}{4.3}$	$\frac{341}{3.9}$	$\frac{341}{3.7}$	$\frac{342}{3.3}$	$\frac{343}{2.3}$	$\frac{343}{2.3}$
22.10	7.1	7		10	30	32	40.06

12+86.20

$\frac{340}{4.7}$	$\frac{341}{3.8}$	$\frac{341}{3.9}$	$\frac{343}{2.1}$
30		10	30

345.50

345.50



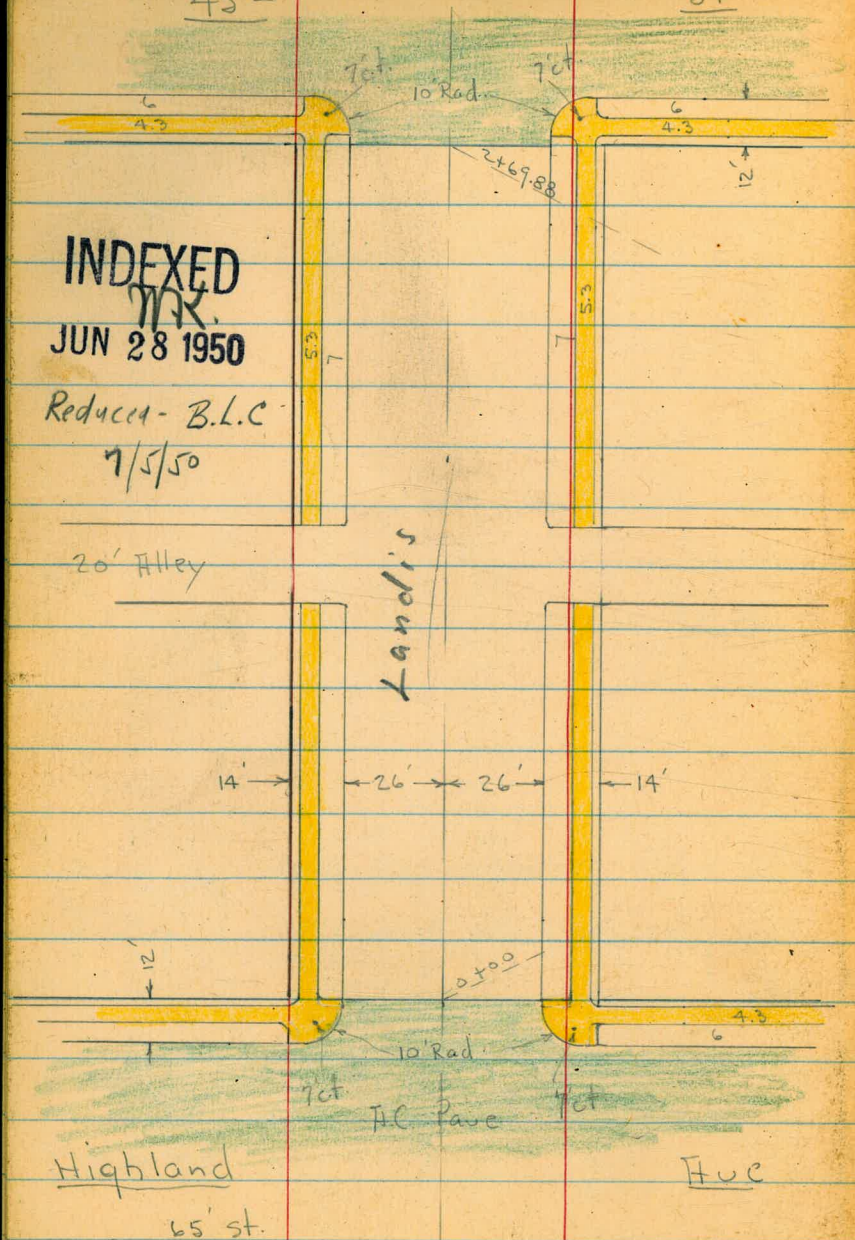
45<sup>th</sup>

St

13

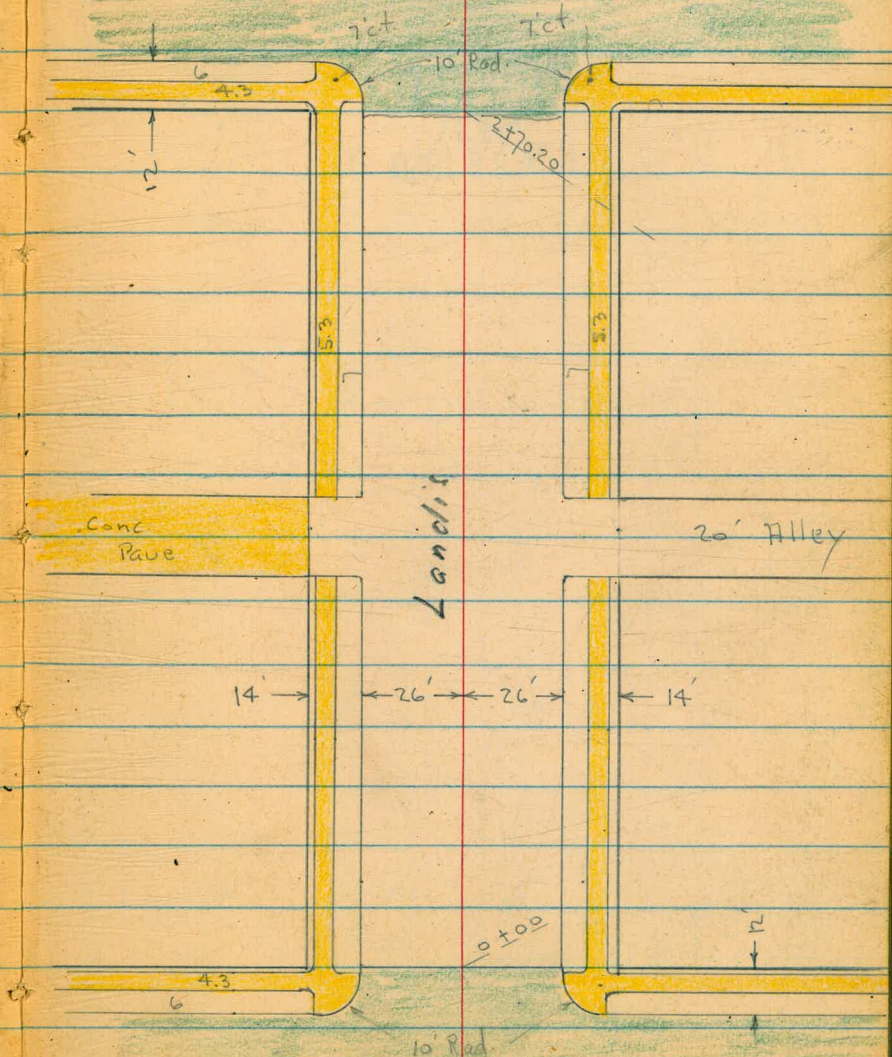
INDEXED  
MK.  
JUN 28 1950

Reduced - B.L.C.  
7/5/50



Chamoune - 60' st. Ave

AC Pave



45<sup>th</sup> - 60' st. A.C. Pave St



X- Sect. Landis - Highland to Chamoune

# 4577  
w.o. 31426

6-27-50  
Osborne  
Hardin  
Hatch  
Shepard.

Lt. = N.  $\neq$

Rt. = S.  
**14**

Soil Sample taken - 75' E. of EL. 45<sup>th</sup>

0+20

**INDEXED**  
JUN 28 1950

Reduced  
B.L.C.  
7/5/50

0+00 = Edge of A.C. Pavc = EL Highland

# of Returns (from Prop. to Prop.)

0-12 = E. cb.

0-22

0-32.5 =  $\neq$  Highland

B.M. 3.19 356.78

353.59 - N.W. 7' ct. Highland + Landis

352.34 4.44 Top	351.16 5.2 25.8 9.4	352.1 4.7 13	352.2 4.6	352.0 4.8 13	351.5 5.3 25.9 9.4	352.20 4.58 Top
353.01 3.77 Top	352.42 4.36 25.9 9.4	352.81 3.97 13	352.89 3.89	352.72 4.06 13	352.33 4.45 25.8 9.4	352.50 3.98 Top
352.70 4.08 9.4	353.16 3.62 Top	352.53 4.25 9.4	352.95 3.80 Top			
353.52 3.26 9.4 9.4	353.19 3.89 4.0 Top	352.64 4.14 4.0 9.4	352.78 4.00 2.6 13	353.04 3.74 13	353.13 3.65	352.97 3.81 13
353.05 3.73 9.0	353.14 3.64 4.0	353.17 3.61 2.6	353.32 3.75	353.23 3.55 2.6	353.06 3.72 4.0	352.12 4.09 9.0
353.42 3.36 9.0	353.56 3.22 4.0	353.52 3.26 2.6	353.45 3.33	353.38 3.40 2.6	353.38 3.40 4.0	353.16 3.62 9.0

356.78



Landis

Lt

D

Rt

15

1+85

584	6.6	6.2	6.0	6.1	6.6	589
Top	gut	13	13	13	25.8	Top
346.14	345.5	345.8	346.0	345.9	345.5	346.09

1+80 = 9' Conc. Dr. on Lt.

583	6.02
32.9	25.8
walk	gut in Dr.
346.45	345.96

1+48 = E.L. Alley

402	431	5.0	4.6	4.6	4.4	4.8	4.44	4.09
39.9	26	26	13	13	26	26	Top	4.0
Top end Ret. + Dirt	Top 2 Rad	gut	13	13	gut	gut	Top 2 Rad	Top end Ret. + Dirt
347.96	347.67	347.0	347.4	347.5	347.6	347.2	347.54	347.59

T.P. 4.11 381.98 8.91 347.87 ✓

1+25 = w.L. 20' Alley

8.05	8.19	8.9	8.6	8.4	8.5	8.7	8.36	8.04
40	Top	26	13	13	13	26	Top	39.8
Top end Ret. + Dirt	2 Rad.	gut	13	13	13	gut	2 Rad.	end Ret.
348.73	348.59	347.9	348.2	348.4	348.3	348.1	348.42	348.74

0+90 = on 10' Conc. Dr. on Lt.

6.83	7.34	7.5	7.5	7.4	7.6	7.8	7.17
32.9	25.8	25.8	13	13	13	25.8	Top
walk	Dr	gut	13	13	13	gut	Top
349.95	349.44	349.3	349.3	349.4	349.2	349.0	349.61

0+50 = on 10' Conc. Dr. on Lt.

5.34	5.96	6.0	5.8	6.0	6.5	5.63
32.9	25.7	13	13	13	25.7	Top
walk	gut	13	13	13	gut	Top
351.43	350.82	350.5	351.0	350.8	350.3	351.15

356.78



± of Returns

NE. Ret.	5.31	4.56	SE. Ret.	5.31	4.70
342.73	342.19	342.57	342.16	342.19	342.19
4.42	4.96	4.58	5.18	5.16	4.78
90	90	40	40	26	13
Top	gut.	Top	gut.	Top	Top

48' E. = E. cb.

342.27	342.73	342.36	342.64	342.79	342.58	342.35	342.69	342.37
3.88	4.42	4.79	4.51	4.36	4.57	4.80	4.46	3.78
90	40	26	13	13	13	26	40	90
						cross		
						gut.		

30' E = ±

342.25	342.13	342.85	342.45	342.42	342.75	342.96	342.75	342.42	342.45	342.92	342.77	342.30
2.90	4.52	4.20	4.67	4.73	4.40	4.19	4.40	4.73	4.70	4.23	4.38	3.80
90	90	40	40	26	13	19	13	26	40	40	90	90
Top	gut.	Top	gut.						gut.	Top	gut.	Top

12' E. = w. cb.

± of Returns

NW. Ret.	4.65	4.14	SW. Ret.	4.72	4.21
342.50	342.01	342.18	342.94		
gut.	Top	gut.	Top		

T.P. 4.19 347.15 9.02 342.96 = N.W. B.P. - 45<sup>th</sup>

2+69.88 = w.l. 45<sup>th</sup> + edge of A.C. pave.

342.89	342.52	342.90	342.15	343.02	342.55	342.89
9.09	9.46	9.08	8.80	8.96	9.43	9.09
Top	25.9	13	13	13	25.9	Top
	gut.				gut.	

2+25 = 3' E of ± of 8' Conc Dr. on Rt.

344.62	343.35	344.2	344.4	344.3	344.23	344.69
7.36	8.2	7.8	7.6	7.7	7.95	7.29
Top	26	13	13	13	25.7	32.8
	gut.				gut.	walk

351.98 on Dr.







Landis

± of Returns

Rough - about 1' W. of w.L.

2+70.20 = w.L. Chamoune = edge of pave is

2+50

2+15

T.P.

4.32 345.54 5.93 341.22 ✓

1+80

1+45 = E.L.

1+35 = ± Alley

N.W. Ret. 5.26 4.67 5.26 4.67 5.84 5.22  
got Top got Top got Top  
340.28 Lt. 340.57 340.28 340.21 340.19 340.05 339.81 340.39  
340.57 340.28 340.21 340.19 340.05 339.81 340.39

18

4.67 5.26 5.33 5.35 5.46 5.73 5.15  
26 26 13 13 13 25.9 15  
Top got got got got Top  
340.96 340.0 340.5 340.5 340.3 339.8 340.53  
4.58 5.5 5.0 4.9 5.2 5.7 5.01  
Top got 13 13 13 25.8 1  
341.19 340.3 340.5 340.0 340.7 340.0 340.84  
4.35 5.2 4.7 4.5 4.8 5.5 4.70  
Top got 13 13 13 25.8 1  
got got got got got got

341.38 340.6 341.1 341.4 341.0 340.4 341.06  
5.77 6.6 6.1 5.8 6.2 6.8 6.09  
Top 26 13 13 13 25.9 1  
got got got got got got  
341.68 341.54 341.53 340.8 341.3 341.6 341.2 340.8 341.25 341.4 341.52  
5.7 5.61 5.62 6.4 5.9 5.6 6.0 6.4 5.92 5.8 5.63 8.1  
40 40 26 26 13 13 26 26 Top 40.1 40.1 60  
Top got 2 Rad. got 2 Rad. got 2 Rad. got 2 Rad. Top Top  
341.41 341.37 340.9 341.5 341.6 341.3 340.8 341.1 340.5 339.0  
5.54 5.78 6.3 5.9 5.6 5.9 6.4 6.1 6.4 8.7  
60 40 26 13 341.15 13 26 33 40 60  
edge Pave.







Alley Blk. 39 - Fairmount Add,  
X-Sec. for grade Establishment.

Sommerneyer  
Johnson  
Allen

9-7-50  
W.O. 25020

□ = Fd. 1/2 hub + ct. T.P. book # 23

● = set disk in conc.

◻ = set 1/2 hub + tack

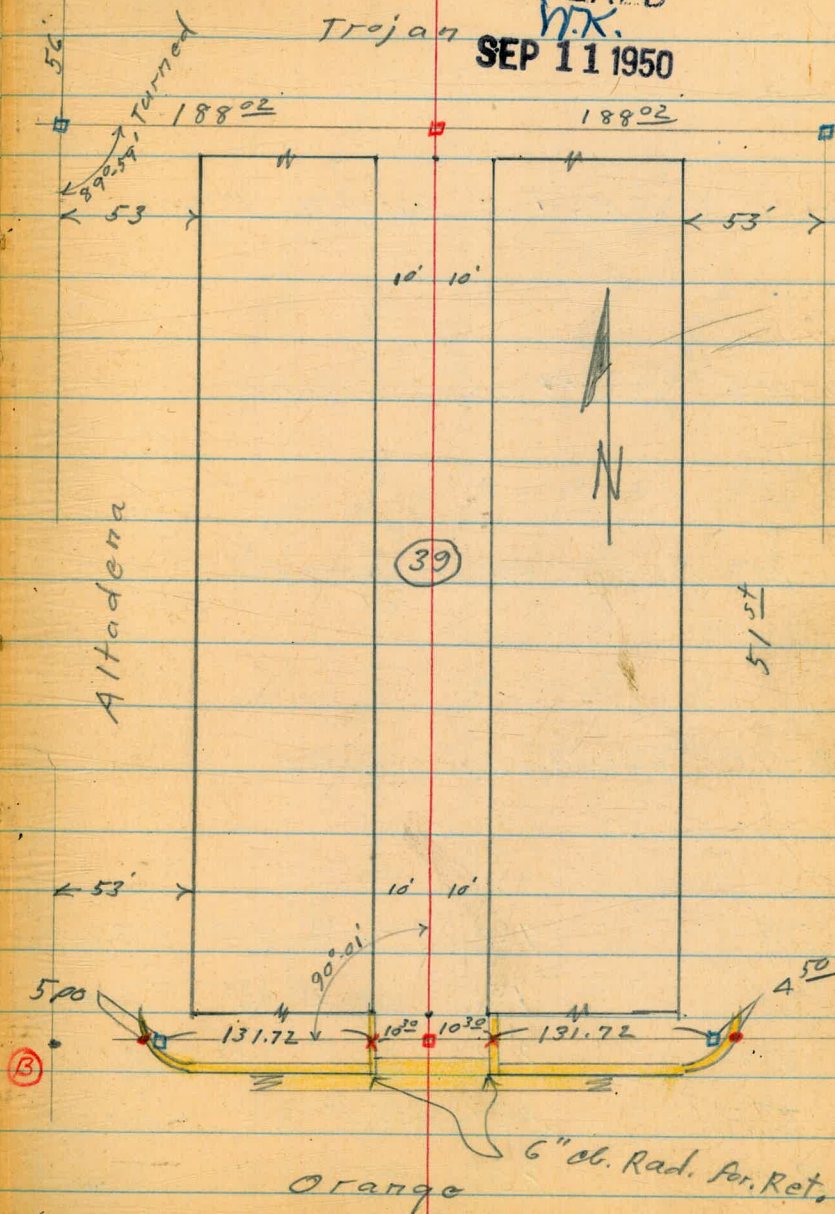
• = Nail

ⓑ = set brass plug in curb for B.M.  
N.W. Orange + Altadena

No soil sample taken.

Reduced by P. Hon  
9-29-50

7  
2' ← set disk in walk.





Alley 81K 39  
Fairmount Add.

L+

Q

R+

21

0+00.8 = End of Existing Curbs

313.36 312.8 312.5 313.5 313.95  
428 40 51 41 369  
Cb dirt dirt Cb  
10 10

0-12.5 = North edge Gutter

313.27 312.55 312.72 313.05 313.95  
437 509 492 459 369  
Cb G G Cb  
10 10

0-15 = North Curb on Orange

312.18 313.07 312.42 313.31 312.58 312.90 314.37 314.62 315.46  
526 457 522 433 526 474 372 302 218  
G Cb G Cb G Cb G Cb  
35 10 10 35

0-18.5 = South Edge Gutter

312.42 312.71 312.89 313.22 314.84  
522 423 425 422 280  
35 10 10 35

317.64  
T ✓

T.P. 423 317.64 364 312.71 N.W. B.P. Altadena & Orange

T.P. 150 322.35 888 320.85 S.E. B.P. 50th & Orange

T.P. 229 329.73 779 327.44

T.P. 161 335.23 161 333.62 Ck-S.W. B.P. 49th & Orange

B.M. 228 335.23 332.75 S.W. B.P. 49th & Orange



Alley BIK 39  
Fairmount Add

1+12 = Cor. House 12<sup>3</sup> Rt

T.P. 898 321<sup>33</sup> 529 312<sup>35</sup>

1+00

0+65

0+50

0+38 = ♀ M.H. 1<sup>9</sup> Right

0+20

Note: Probably best location for  
Catch basin in Alley.

See Drainage Plans this  
Area for further data.

Lf.

♀

Rt. 22

312.51  
88<sup>2</sup>  
12<sup>3</sup>  
Floor of House

321<sup>33</sup> ✓

314.7	314.3	310.6	310.1	310.3	310.6
29	33	70	75	73	71
45	22	10		10	30

315.3	315.7	309.3	309.0	309.0
23	19	83	86	86
40	22	9		10

308.7	308.6	308.2
80	90	97
10		10

309.39  
82.5  
Rim. of  
M.H.

306.4	307.0	307.6	307.9	307.5
11.2	10.6	10.0	9.7	10.1
25	10		10	25

317.64



Alley Bk. 39  
Fairmount Add.

1788<sup>5</sup> £ of 11' conc. drive 9<sup>7</sup> left

1783 = End Block wall - 9<sup>7</sup> left

1770 = Cor. House 13<sup>3</sup> Lt

1768 = 9<sup>9</sup> Lt 5<sup>5</sup> Wall

1757 = Cor House 13<sup>3</sup> Lt

1750

1744 = Cor House 12<sup>2</sup> Rt

1740 = Cor House 8<sup>8</sup> Rt,

1724 = Cor House 8<sup>7</sup> Rt.

Lt.

317.69 317.33 316.92 £  
364 400 441  
224 20 97  
Floor Ramp  
527 48 316.5  
Footing dirt  
97

318.09  
324

315.51 133  
Floor  
582 52 316.1  
Footing dirt  
99 318.09

324  
133

Floor

63

10

314.2  
71

75

10

Rt.

23

318.56  
727  
122  
Floor  
725 313.38  
88  
Floor

88

87

766 313.67

87

~~32/33~~ Floor House



3+50

3+09 = 1/2 Single Garage 18' Lt dirt Floor

3+00

T.P. 13" 334<sup>32</sup> 0<sup>12</sup> 321<sup>21</sup>

2+50

2+39 = Cor House 12' Lt

2+19 = Cor House 12' Lt

2+00 = End 5' BIK wall 9' Lt

1+93 = 5' BIK wall 9' Lt

Lt. 332.5 £ 332.0 331.2 Rt.  
10 2 3 3-  
10

326.4  
72  
182  
325.3 324.9 324.6 324.6 324.6  
90 91 97 97 97  
30 10 10 50

334<sup>32</sup> ✓  
318.9  
24 24 25  
10 10  
320.15

118  
Floor  
124  
319.89  
144  
Floor  
124  
317.3 316.66 317.2 316.43 316.1 315.3  
40 467 41 42 52 60  
20 footing 99 dirt 10 35

316.55 316.9  
428 44  
footing 97 dirt  
32/33



4+55 = 9<sup>LT</sup> & 4' walk

4+50

341.16  
 5 55<sup>LT</sup> 6 3  
 walk dirt  
 9<sup>LT</sup> 340.4 340.0  
 6 3 6 2 6 8 7 8 5  
 35 10 10 35

4+28 = 11<sup>RT</sup> End shed

4+00

338.0 337.6 337.3 338.3  
 8 2 9 1 9 4 9 2 8 4  
 30 10 9 2 11 0 336.8  
 9 7 9 7

3+85 = 9<sup>RT</sup> shed dirt floor

336.0  
 10 2  
 9 4

3+83 = 14<sup>LT</sup> & Jangle Garage dirt floor

336.2  
 10 5  
 14 5

T.P. 17 20 346 71 0 31 334 01

346 71  
 334 32



5726 = Start Garage 17' Rt

345.36 Rt.  
 135  
 165 Apron  
 175 Floor  
 345.61

5705 = 4' Walk 13' Lt

343.28  
 343  
 13' Walk  
 343.85  
 342.56  
 343.1  
 28c Floor  
 95 Footing  
 36 dirt  
 11.3

5703 = End Garage & Wash shed - 11' Lt

5700

343.1  
 342.7  
 342.8  
 340.0  
 36 40 32 67  
 10 10 35

4776 = Start of Combination Garage & Wash Shed - 11' Lt

342.13  
 341.06  
 341.5  
 45c Floor  
 50c Footing  
 52 dirt  
 17.4

4771 = Single Garage 12' Lt dirt floor

341.1  
 56  
 120  
 56 341.10

4761 = Single Garage 12' Lt Conc. Floor

120  
 Floor 346.31



6+07<sup>27</sup> = South 7' line Trojan & Alley on Hub

6+00

352.11

60	62	72	74	92	101
25	10		10	20	40

5+83 = 10<sup>4</sup> Lt. End Apron of Double Garage

350.99

724	860
291	104
Floor	Apron

5+66 = 10<sup>3</sup> Lt Apron of Double Garage

350.99

779	925
291	103
Floor	Apron

T.P.

17<sup>63</sup>    358<sup>73</sup>    061    346<sup>10</sup>  
           ↑

5+50

358<sup>73</sup> ✓

346.69	346.69	346.66
03	04	05
10		10

5+99 = End Double Garage 17<sup>2</sup> Rt

345.69

346 <sup>21</sup>	177
↑	Floor



Lt.

E

Rt.

0.06

376.14

Check B.M.

279 376.22

N.W.B.P. Trojan 50<sup>th</sup>

T.P

8.26 379.01 0.46 378.75

West  
on disk 7 line Aladeng

T.P.

12.69 371.21 0.21 358.52

3' tie back of N.P.L. Trojan

6+30

357.6

355.7

354.2

1.1

3.0

4.5

30

40

6+15

358.7

355.2

354.1

353.5

353.2

353.9

0.2

3.5

4.6

5.2

5.5

4.8

30

20

10

10

40

358.73

T



D. Smith  
G. Pope  
R. Sission

1/2" 6 grate  
Note: No pipe to East  
1/2" 6 grate  
11" 8" corr. pipe  
to end pipe  
18" corr. pipe  
4' Ditch  
open

# Survey Proposed

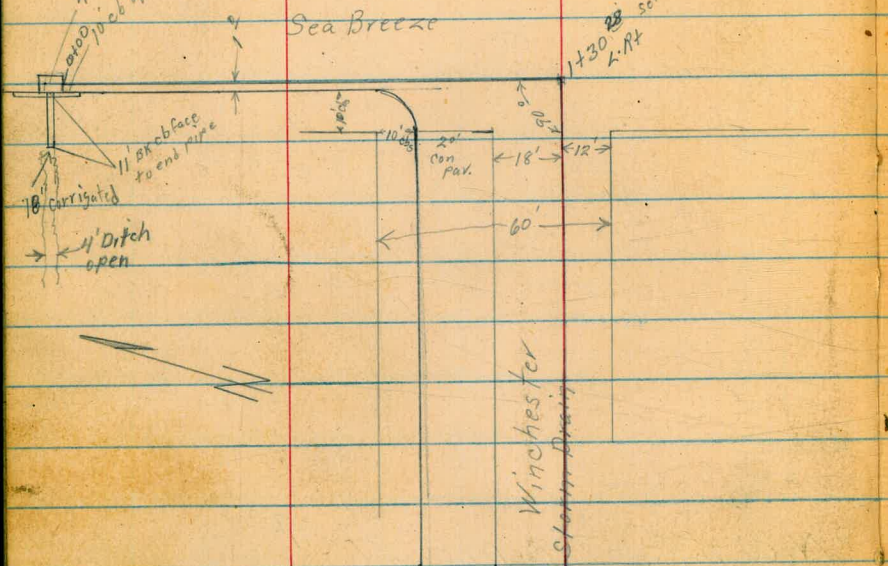
Sea Breeze and Winchester

# Storm Drain Paradise Hills

1-11-50  
W<sup>#</sup> 20530

29

BIK 26 + 20



Levels P-31-41

set Hub  
5785 40  
L. RT 70° 15'

For Pipe 3"  
RE 5794 8110

For Pipe 3"  
RE 5794 121 75 = 517 Line Cumberland

RECORD  
70:11:20

5785 40  
L. RT set Hub

base line cont.  
For sections in low ground  
Sta cont. both ways westward  
North

Sta cont.  
7734 15  
Edge Pav. Rec.

East

set Hub  
15466 30  
End

14 BIK 20  
Lot Line Approximately  
15 BIK 20



30



Levels: Proposed Storm Drain

Paradise Hills

Blks. 26-20

Location on P-29

1730<sup>28</sup> L. RT

0791<sup>E</sup> Ncb line Winchester on west.

0781<sup>E</sup> BC cb on west

0750

67  
117  
4/23

0725

0700 South inside edge inlet Box.

BM

Weekend Plug  
Sea Breeze  
Winchester  
(Not in Record)

Lt. East

Q

RT = West

31

245<sup>3</sup>  
14

245<sup>8</sup>  
2

246<sup>68</sup>  
Stab

245<sup>6</sup>  
60

244<sup>2</sup>  
39

244<sup>3</sup>  
14

243<sup>2</sup>

243<sup>2</sup>  
11

244<sup>19</sup>  
11  
947 06

244<sup>0</sup>  
60

244<sup>3</sup>  
39

243<sup>5</sup>  
14

242<sup>3</sup>

242<sup>2</sup>  
11

243<sup>51</sup>  
11  
947 06

242<sup>3</sup>  
39

241<sup>2</sup>  
14

240<sup>5</sup>

240<sup>5</sup>  
11

241<sup>53</sup>  
11  
947 06

242<sup>0</sup>  
39

240<sup>1</sup>  
14

239<sup>6</sup>

239<sup>6</sup>  
11

239<sup>29</sup>  
11  
947 06

241<sup>8</sup>  
39

240<sup>0</sup>  
14

239<sup>63</sup>  
cb

238<sup>20</sup>  
gate

236<sup>72</sup>  
FL

239<sup>8</sup>  
11

236<sup>34</sup>  
11

ground  
FL  
outlet



Paradise Hills - Storm Drain

Lt = South

RT = North

32

2775

235<sup>2</sup><sub>12</sub> 235<sup>1</sup> 233<sup>5</sup><sub>15</sub> 232<sup>20</sup><sub>18 pav</sub>

2750

236<sup>4</sup><sub>12</sub> 236<sup>7</sup> 236<sup>5</sup><sub>15</sub> 235<sup>32</sup><sub>18 pav</sub>

TP

238<sup>56</sup>

2725

241<sup>4</sup><sub>12</sub> 239<sup>9</sup> 239<sup>4</sup><sub>16</sub> 238<sup>25</sup><sub>18 pav</sub>

2700

243<sup>17</sup><sub>12 drive end</sub> 243<sup>4</sup> 241<sup>5</sup><sub>16</sub> 240<sup>84</sup><sub>18 pav</sub>

1775

245<sup>3</sup><sub>12</sub> 244<sup>4</sup> 243<sup>5</sup><sub>15</sub> 242<sup>69</sup><sub>18 pav</sub>

1741<sup>28</sup> 18° RT Begin south edge con paving

247<sup>3</sup><sub>12</sub> 246<sup>6</sup> 245<sup>9</sup><sub>5</sub> 245<sup>4</sup><sub>16</sub> 244<sup>33</sup><sub>18 pav</sub>



Paradise Hills Storm Drain

Lt = South

Rt = North

33

4750

224<sup>2</sup> 225<sup>0</sup>

225<sup>31</sup>  
18  
pav.

4743 4.5 Lt =  $\frac{1}{2}$  Elec. Pole # 88637

224<sup>1</sup> 225<sup>0</sup>  
12

225<sup>5</sup> 225<sup>89</sup>  
10 18  
pav.

4725

224<sup>6</sup> 225<sup>0</sup> 225<sup>7</sup> 226<sup>15</sup>  
12 10 18  
pav.

4700

225<sup>5</sup> 225<sup>9</sup> 226<sup>49</sup>  
12 18  
pav.

3775

225<sup>6</sup> 226<sup>4</sup> 226<sup>2</sup> 227<sup>13</sup>  
12 5 18  
pav.

3750

228<sup>0</sup> 228<sup>1</sup> 228<sup>46</sup>  
12 18  
pav.

3725

TP<sub>2</sub>

229<sup>20</sup>

231<sup>6</sup> 230<sup>2</sup> 231<sup>1</sup> 230<sup>55</sup>  
12 15 18  
pav.

3700



Paradise Hills - Storm Drain

Lt. E Ad.

6700 to West

2150 2151 2155 21568  
25 12 18  
Pov.

5792 to West

2156 2159 2160 21618  
25 12 18

5785A - POT. for Sec. to West

2188 2175A 2171 21644  
12 Hub 10 18  
Pov.

5785 5.5' Lt. = 2' Elec Pole J.P. 89527

5780

2194 2187 2178 21683  
12 11 18  
Pov.

5750

2206 2204 2195 21886  
12 13 18  
LOW 17 Pov.

5700

22067 22189 22266 2229 2227 22220  
22 15 7 13 18  
DRIVE DRIVE Top Conc. DRIVE Core Pov.

4765 4' Lt. = 2' Pole Anchor

Tg

22466

4753 6' Lt E 2 1/2" gas valve box 2" pipe cross-shin. 90'

22300 22466  
Top 2" Top box  
gas pipe 6  
6



Paradise Hills - Storm Drains

35

Sections from 5+85.40 to North Cont. P-36

→ Last sec. to west.

Sec. Parallel to Rea Dr.

7+34.15 = East edge Rea Pav.

21481	21493	21526	21543	21589	21610	21637
50	25	12		18	385	50
Pav.	Pav.	Pav.	Pav.	Pav.	Pav.	Pav.

7+00 to West

2141	2138	2140	21409
25	12		Pav.

6+75 to West

2140	2138	2139	21389
25	12		18
Lawn			Pav.

6+40 = ~~1/2~~ Conc. Drive

21424	21384	2140	21416
17	11		18
Drive	Toe Drive		Pav.

6+25

2140	2140	2144	21463
25	12		18
			Pav.

T.P. on L. Hub 5+85.40

21784



Paradise Hills - Storm Drains

Lt.

L

Rt.

36

7+52

2144 2147 2152 2150 2161  
20 4 7 20

7+40

8+07 = End 5' Chain Wire Fence 3.3 Lt.

7+47 = Beg. 5' Chain Wire Fence 3 Lt.

7+47 = End 3.5' Picket Fence 3 Rt.

6+90 = Beg. 3.5' Picket Fence 4 Rt.

2140 2146 2165 2168 2177  
20 6 7 20  
Yard Lawn

7+00

6+88 = Pole # 88405 1.0 Lt.  
Elec.

2145 2146 2163 2173 2180  
15 5 5 20

6+65 .99 Lt. Pole Anchor.

6+45 Sec RA to Line

2151 2156 2180 2184 2188  
20 6 10 25

6+25.7 Cont.

21515 21574 21442 21502 21848 21909  
125 125 100 100 50 50  
cut ch. cut ch. cut ch.

Sec. Parallel to Winchester.

6+25.7 = N. Cut Winchester

21408 21470 21414 21479 21460 21522 21552 21612 21729 21790  
75 75 50 50 25 25 50 50 32 32  
cut ch. cut ch. cut ch. cut ch. cut ch. cut ch.

6+04.6 = Sec. Parallel to Winchester  
on S.W. edge Conc. Pav.

21457 21394 21394 21413 21498 21616 21853 21935  
125 100 75 50 25 38 50



Paradise Hills Storm Drain

Lt.

R

Rt.

37

9+87 = End 2.5' Picket Fence 45' Lt. 52' Rt.

9+87 = End 4' Chain Wire Fence 6' Lt.

21227	2103	2102	2102	21274
6	6		5	5.2
Top Wall	Ground		Ground	Top Wall

9+28

9+27.5 0.7' Lt. = 1/2 Elec. Pole # 88403

9+28 = Beg. 2.5' Picket Fence 45' Lt. set 8" Conc. Wall

9+27 = Beg. 4' Chain Wire Fence 6' Lt. set in Conc. <sup>Wall</sup> Base

TP

21220

21226	2122	2122	21304
6'		4	4.5
on Wall			Wall

9+27 = End 4' Chain Wire Fence on 70' Lt.

9+00

2140	2129	2129	2128	2130
20	5		5	20

8+67 = End 4' Chicken Wire Fence on 36' Lt.

8+50

2139	2141	2141	2140	2145
20	4		5	20

8+09 0.7' Lt. = 1/2 Elec. Pole # 88404

8+07 = Beg. 4' Chicken Wire Fence on 33' Lt.

8+07 = Beg. 4' Chain Wire Fence on 33' Lt.

8+00

2141	2146	2147	2147	2150
20	4		7	20



Paradise Hills - Storm Drain

Lt

Rt

Rt. 38

12

12+00

Elec.

11+50 = Pole 07' Lt # 88401

TP

206.01  
= Beg. 10" Conc. Base For Fence on Rt. = 0.5' Rt.

11+50 = End 4' Wire Fence on Lt.

2053 2052 2054 2065 2070  
20 6 9 15

2055<sup>2</sup> 2054 2056 2058 2061 2074  
0.5 20 6 5 15  
Wall

95'

11+10

2062 2065 2063 2063 2077  
20 6 5 20

5.9' Lt.

11+07 = Beg. 4' Wire Fence Posts set in conc.

11+00

2090 2093 2069 2065 2069  
20 6 5 20

10+47 = End Fences Rt & Lt 58' Lt 54' Rt

10+47 = E Elec Pole # 88402 0.5' Lt

21042 2090 2084 2083 2080  
58 5 5 15  
Top wall

= Beg 4' Wire Fence 5.2' Rt Posts set in conc.

9+87.2 = Beg 10" Conc. Tile wall with 4' chain wire fence

21042  
6  
Top wall



Paradise Hills - Farm Drain

Lt.

♀

Rt.

39

13+85

2017  
20

2029

2036  
20

13+50

2029  
20

2040

2050  
20

13+27.6 = N Guts

20334  
25  
cb.

20378  
25  
Gut

20414  
Gut

20476  
0  
cb.

20543  
25  
Gut

20602  
25  
cb.

13+06.5 = ♀ Pvc

20358  
25  
Pvc

20501  
Pvc

20628  
25  
Pvc

12+85.5 = South cb line Cumberland Roadway

20348  
25  
Gut

20408  
25  
cb.

20539  
cb.

20479  
0  
Gut.

20657  
25  
cb.

20597  
25  
Gut

12+82 = ♀ Elec. Pole 87996 3.5 ft

All sections in this st. Parallel to some.

12+75 = Sky Line Cumberland

2048  
20

2053  
10

2059

2061  
10

2066  
20

12+29 = End 10" Line Base For Fence on Rt.

2051

2054  
6

2055

20542  
05  
Wall

2061  
5.6  
5.16 Cor H.



Paradise Hills Storm Drain

Lt.

R

Rt. 40

15+57

1959 1960 1944 1946 1961 1970  
20 12 10 2 3 10  
Ditch Ditch

15+50

1970 1976 1970 1960 1967 1970  
20 10 2 2 6 10  
L Ditch

= Beg. 3' Picket Fence 6.5' Rt

15+06 = End chain wire fence 6.5' Rt

15+00

1988 1992 1971 1971 1976 1976  
20 2 4 6.4 15  
Ditch Ditch

T.P.

20137

14+46.5 = Beg. 4' <sup>wire</sup> chain fence 6.4' Rt

14+40

2006 2014 2001 1976 1976 1988 1990  
20 3 4 6 8 20  
Ditch

14+25

2009 2016 1996 1976 1985  
20 13 17 25  
Ditch

14+32.5 2.2' Rt = E. Telec. Pole J.P. 88589

13+93

2016 2025 2021 2003 2004  
20 2 7 20



Paradise Hills - Storm Drain  
Levels  
Locatist P-29

Lt.

L.

Rt.

41

FB. 2026-28 → 194.89 ✓  
0/0° diff.  
Chk. SW. B.P. Cumberland & Rco 194.99 sur

15+66.3 = End of line

1939	1945	1957	1962	1974
15	ditch	on Hub	6	14

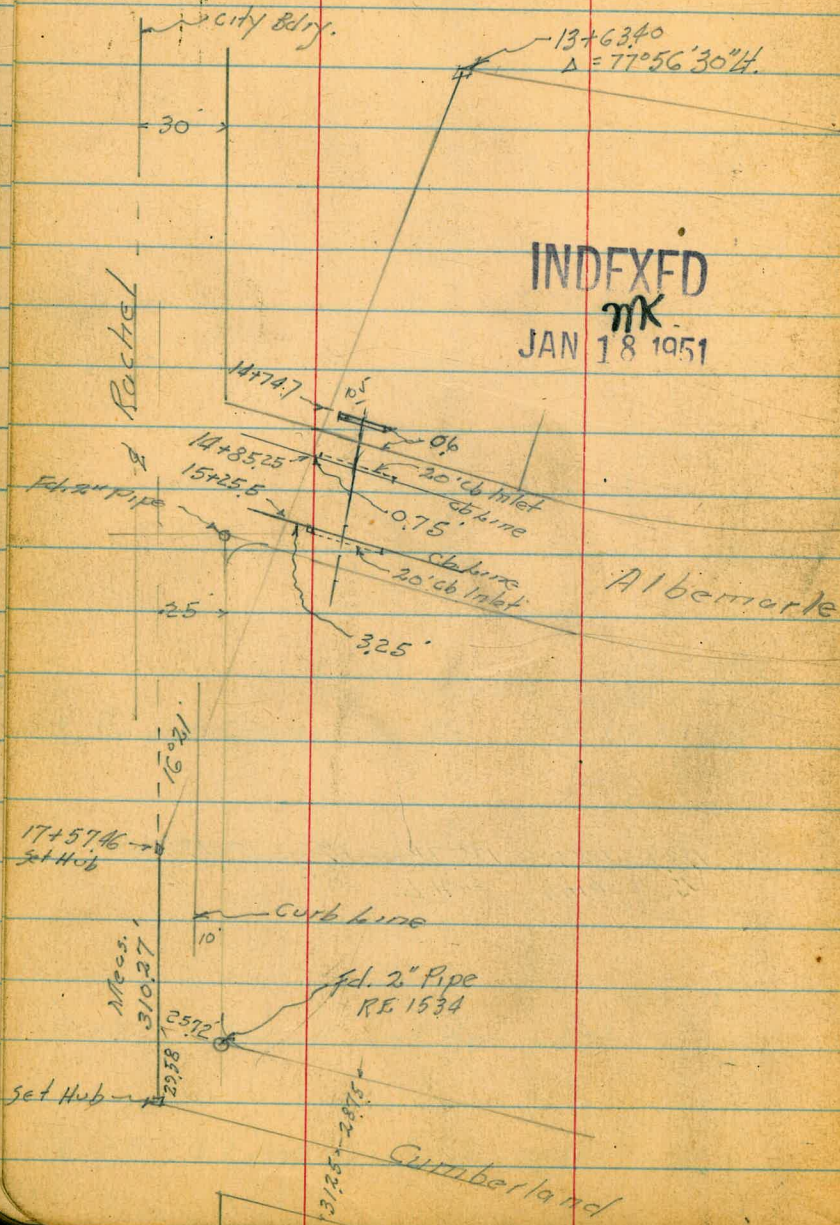
15+66 - End of Picket Fence 66' H

15+65 2.1' RT Elec. Pole 477670-H



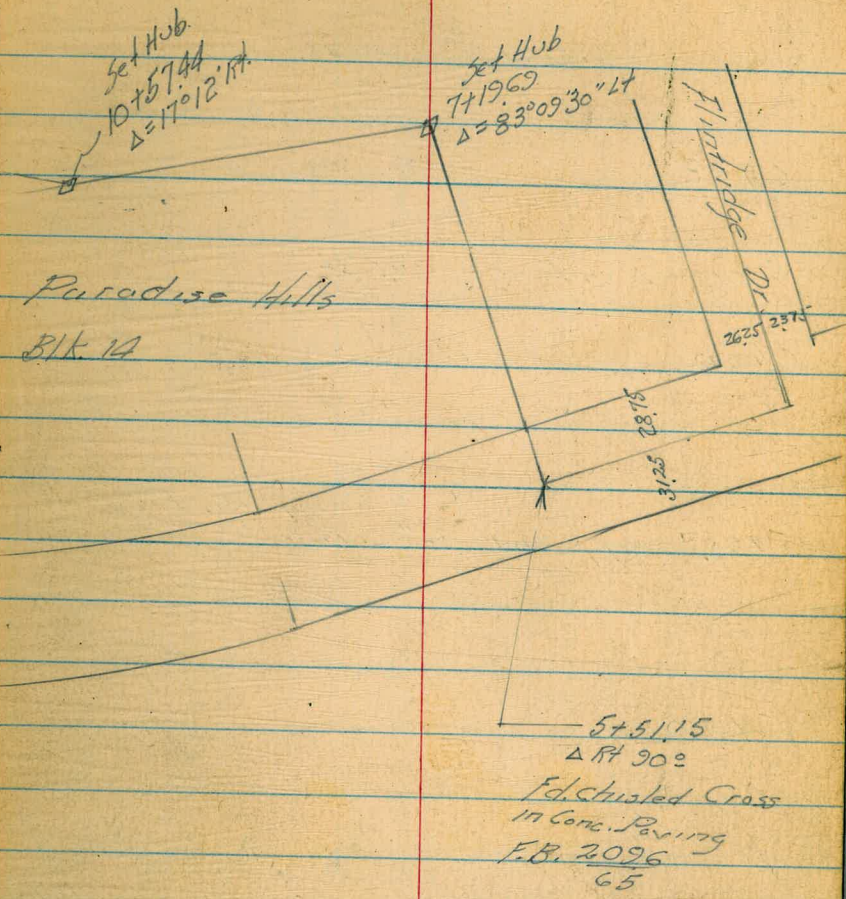
Location Proposed Sewer

Walker Blk-14 - Paradise Hills M.D. 31667  
 Pope  
 R. Sisson  
 1-15-51



INDEXED  
 MK  
 JAN 18 1951

Albemarle



Paradise Hills  
 Blk 14

5+51.15  
 Δ RT 90°  
 fd. chisled Cross  
 in Conc. Paving  
 F.B. 2096  
 65



Prelim. Sewer S/K-14  
Paradise Hills

Location P-42

6+25

172.5	172.0	162.8	165.5	162.7	162.3
42	47	112	112	140	144
50	40	22	9	5	2
Yard at Leaky Fence				Ditch	Ditch

6+15 = Δ in Fence 28.5 ft

6+00

172.0	171.5	164.0	163.7	165.0
47	52	127	180	117
42	28.5	16	8	
at House	of Fence	Ditch Wedge	Ditch E edge	

5+96.7 = opp end 36" Corrug. Iron Pipe  
Corrug. Iron Pipe

172.0	171.5	163.57	166.8
47	52	130.9	9.9
42	28.5	17	
E side House	of Fence	Invert 36" Pipe	

5+80

172.3	171.8	171.7	172.1
44	49	5.0	4.6
42.3	25.5	18.8	
Yard Lawn	at Fence		

5+69.9 North Gut

172.38	171.68	172.04	171.23	171.95	170.82	169.92
42.8	49.8	46.2	54.3	48.1	58.0	12.78
32	30	40	40	28.8	28.8	18.3
cb	Gut	cb	Gut	cb	Gut	Flour Invert cb inlet

171.62	170.80	171.70	170.92	172.36	171.52
48.4	58.6	47.6	5.77	4.30	5.14
188	188	8.8	8.8	cb	Gut
cb	Gut	cb	Gut	cb	Gut
at Inlet Grating			East end cb Inlet		

5+51.15 Δ Rt 90°

172.29	171.93	171.94	171.76	172.19	172.53
43.7	47.3	47.2	4.20	4.47	4.13
38	40	30	20	8.8	

41.3

176.66 ✓

172.53

176.66 ✓

B.M. on Shaded Cross in Conc. Puy  
5+51.15 F.B. 2096-75



7+41

7+33

7+19.69° Δ LA 83°09'30"

7+00

6+90

6+73

6+50

T.P. 5.90

169.51 ✓ 130.5

163.61 ✓

176.66 ✓

141.5  
80  
25

160.8  
87  
10

158.6  
10.9

44

157.7  
9.8

144.81  
4.70  
07 Hub

162.4  
71  
50

141.3  
82  
16

159.6  
99  
13

158.9  
106  
7  
Wedge  
DITCH

157.6  
99  
N. edge  
DITCH

163.5  
60  
50

141.4  
81  
8  
Bank

159.1  
10.4  
Ditch

162.3  
32  
50

144.1  
54  
46

163.0  
65  
38

141.9  
76

172.4  
+2.9  
50

144.1  
54  
34

163.1  
69

169.51 ✓

~~176.66~~



TP 465 162.18 ✓ 1198 157.53 ✓

9+00

168.4  
1.1  
50144.2  
52  
17160.3  
92  
27159.9  
96  
27154.8  
147  
65

8+65

173.7  
+42  
50168.3  
12  
15165.1  
44  
16160.4  
21  
24159.1  
10.1  
24152.7  
12.8  
65  
& ditch

8+15

174.2  
+47  
50167.8  
17  
32165.4  
41  
16162.1  
74

7+90

168.3  
12  
50165.4  
41  
35161.7  
7.8  
14160.6  
8.9

7+50

162.2  
7.3  
35160.8  
8.7  
7159.9  
96

7+48

169.51 ✓

158.8  
107  
& ditch.  
169.51 ✓



10+15

151.2  
110  
Ditch  
Edge

10+00

157.6  
4.6  
50

155.0  
72  
45

154.0  
82  
14

151.1  
111  
13  
Ditch

151.6  
10.6  
7  
Ditch

154.2  
80  
5

154.9  
73

9+94

155.5  
67

9+92

151.6  
10.6

9+82

151.6  
10.6  
2 Ditch

9+77

155.0  
72

9+50

158.2  
4.0  
50

156.7  
5.5  
35

155.7  
6.5  
15

155.6  
6.6  
35

156.0  
6.2  
35

153.1  
9.1  
40

162.18

162.18 ✓

2 Ditch



Blk. 14 - Paradise Hills

47

11+00

152.8  
94  
50

152.0 151.0 149.8 149.9 153.2  
102 112 124 123 89  
25 23 20 13  
S edge Ditch  
Ditch N edge

10+88

151.9  
103

10+72

150.1  
121  
2  
Ditch

10+57.44 A 17°12' Rt

151.39  
1079  
on H

10+50

155.8 152.8 151.7 150.4  
6.7 24 9.5 11.8  
50 8 15  
E Ditch

10+30

152.3  
9.9

10+25

162.18

150.8  
11.4  
W. edge  
Ditch  
162.18



13+00

12+50

12+43

12+35

TP 477

12+00

11+50

153.91 ✓

130.4

149.14 ✓

162.18 ✓

150.3

11.9

50

149.4  
4.5  
50

148.1  
5.8  
15

147.0  
6.9  
15

146.3  
7.6

146.0  
7.9  
6  
2 Ditch

147.3  
6.6  
20

148.2  
5.7  
50

148.4  
5.5  
45  
Bank

147.0  
6.9  
32  
Ditch

146.9  
7.0  
10  
Ditch

146.8  
7.1  
Ditch

148.4  
5.5  
7  
Bank

146.6  
7.3  
Ditch

149.0  
4.9

153.91 ✓

148.7  
13.5  
50

147.4  
14.8  
49  
2 Ditch

149.2  
13.0  
39

151.6  
10.6

150.2  
12.0  
42

148.6  
13.6  
39  
Ditch

148.6  
13.6  
36  
Ditch

151.6  
10.6  
32

153.3  
8.9

162.18 ✓



14+85.25 - N curb Albemarle section on curb

148.21	147.24	148.01	147.01	141.56	147.03	147.94	147.81	148.53	148.90	149.52
570	667	690	690	1235	688	597	610	538	581	439
207	207	107	Groing	107	0	0	14	14	30	30
cb	Gut.	cb	107	Invert	cut.	cb	Gut.	cb	Gut.	cb

Hd. Wall and Section Parallel  
14+74.7 opp N. end Hd. Wall - To Curb here

149.8	147.7	146.40	141.84	146.40	147.2	150.7
41	62	751	1207	751	6.7	3.2
50	35	165	10.5	4.5		6
		Top Hd. Wall	Invert	Top		
			26" corr. Iron curbst.	W. end Hd. Wall		

14+50

151.6	144.7	142.6	146.9	148.3	151.9	157.9
2.4	9.2	11.3	7.0	5.6	2.0	2.0
50	33	24	4		8	15
		& Ditch	Top Slope			

14+00

143.7	146.0	147.7	149.9	151.7
10.2	7.9	6.2	4.0	3.2
25	8		6	10
& Ditch	Top Slope		Slope Side	Slope Side

13+63.40  $\Delta$  14 77° 56' 30"

145.91	147.3	150.2
8.00	6.6	3.7
on curb	5	10
	Top Slope	Side of Slope

13+50

143.6	144.5	145.5	145.7
10.3	9.4	8.4	8.3
Ditch	2.8	& Ditch	2.0
	Ditch		& Ditch

13+20

148.5	146.9	146.7
5.4	7.0	7.3
50	30	
		15391 ✓



15+75

141.7  
93

15+53

144.0  
7.0

0.55 151.03 ✓

150.48 = 8M

151.03 ✓

FB 1626-80

0.01  
150.48

344

150.47 ✓

CHK SE BP Rachel & Albemarle

at RT Δ to our 61178

15+42 opp end of 36" Corrug. Iron Pipe

140.65  
142.7  
1326.  
7.2  
14.4  
Invert

Sec.

15+30 Parallel to curb

148.6  
147.7  
148.1  
149.2  
5.8  
6.0  
5.8  
4.7  
30  
13  
25

15+25.5 sec on S. curb

148.22  
147.18  
5.62  
673.  
2325  
2325.  
Cb. Gut. Eend Inlet

148.05  
140.78  
147.03  
5.86  
1313  
6.88  
1325  
1325  
Cb. Invert. Groding

147.95  
147.10  
5.96  
6.81  
325  
325  
Cb. Gut. Inlet W. end

147.31  
148.20  
5.71  
5.16  
30  
30  
Cb. Gut. Cb

148.75  
149.38  
4.53  
30  
Cb

15+05.4 sec Along E. Paring.  
153.91 ✓

148.44  
147.96  
148.01  
5.47  
30  
5.25  
17  
5.90  
153.91 ✓  
Pav. Pav. Pav.

149.37  
4.54  
25  
Pav.



17+57.46

Sec on E curb

17+03.50 = E curb Ratchet

128.96	139.95	135.32	139.92	138.59	138.99	129.98	139.24	140.07
1207	1108	1570	1111	1214	1204	1125	1177	1096
345	345	245	245	245	145	145	0	0
Gut. cb inlet	cb	Inlet	cb	Gut. cb	Gut. cb	Gut. cb	Gut. cb	cb
36" corr. Pipe				New inlet				

17+00

16+75

16+58

16+25

16+00

1157  
139.46  
140.4  
106  
140.9  
101  
141.3  
141.0  
140.7  
10.3  
151.03 ✓

REMOVED - 1-25-51. AEC.



Cross Sections for Proposed Pump House

Mulkey  
Pope  
1-17-51

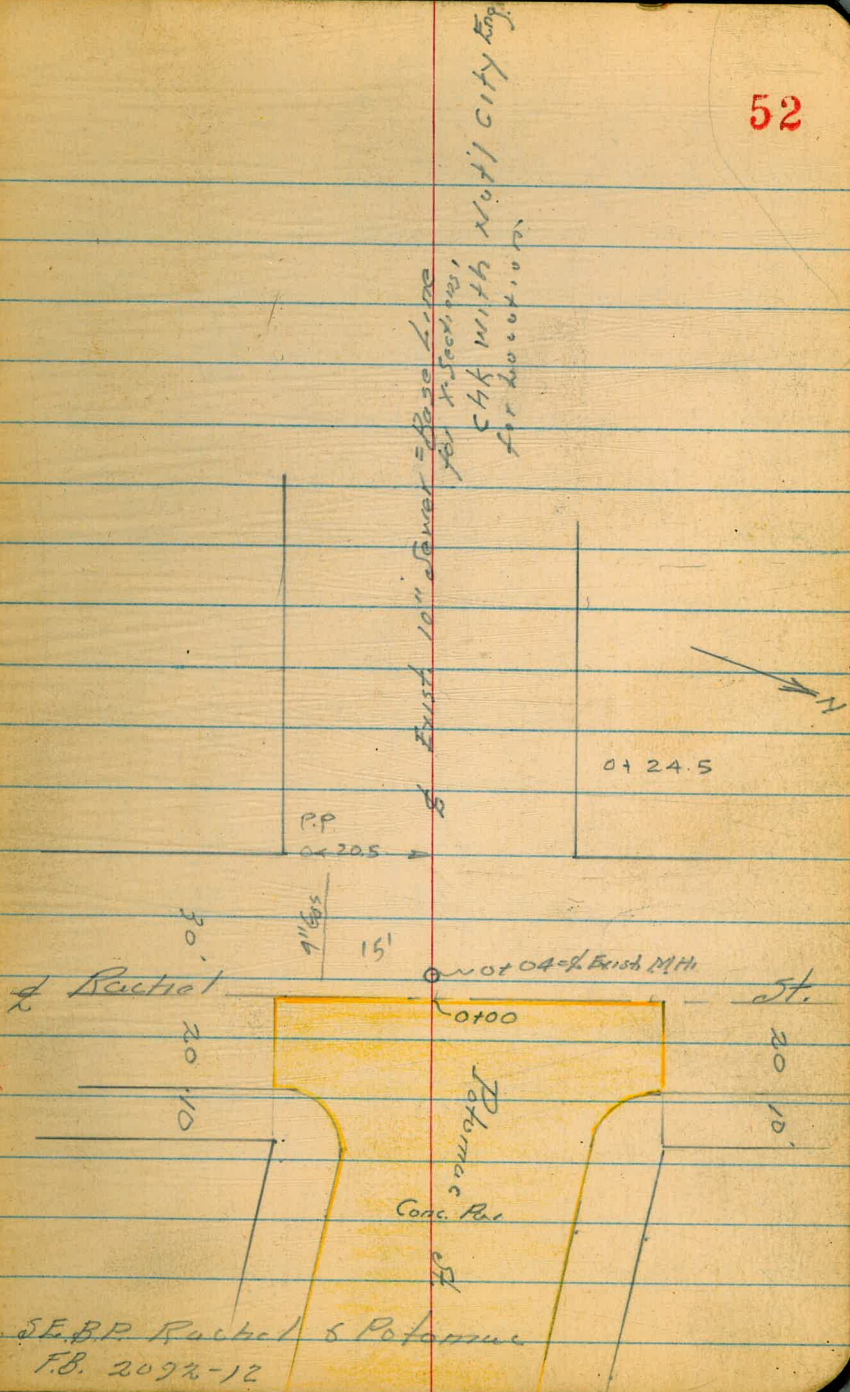
West end Potomac Street  
177 Paradise Hills NO 31667

INDEXED  
MK  
JAN 18 1951

370 165.34 ✓  
3

161.64

52



SE. B.P. Rachel & Potomac  
F.B. 2092-12

10' of concrete = 10' of steel  
for 10' of concrete  
check with North City Eng.



Potomac Cont.

0+75

Lt. Lt. Lt. Lt. Lt. Lt. Lt. Lt. Lt.  
 160.8 153.5 153.31 153.44 153.26 153.3 148.0 150.3  
 4.5 118 1203 1190 1208 120 170 151  
 30 18 14 4 10 20 30

0+50

156.2 154.8 156.27 156.50 156.52 156.5 151.7  
 70.3 55 207 884 882 88 13.6  
 30 22 15 15 4 17 30  
 Edge Pav. Edge Pav. Edge Pav. Edge Pav.

0+30

164.2 158.92 159.18 157.26 157.0 160.1 157.3  
 1.1 642 616 508 6.3 52 80  
 30 15 15 5 16 25 30  
 Pav. Edge Pav. Edge Pav. Edge Pav. Edge Pav.

0+20

162.2 160.44 160.01 160.33 160.39 160.4  
 3.0 490 533 514 495 49  
 30 15 15 7 30  
 Pav. Pav. Pav. Edge Pav.

0+10

161.48 161.21 161.05 161.05 160.88 159.9  
 386 413 429 429 446 54  
 30 25 15 15 11 30  
 Pav. Pav. Pav. Pav. Pav.

0+04 -& Exist. MH

161.22  
 4.12  
 Rim

0+00

162.01 161.66 161.31 161.20 159.91  
 333 368 403 414 543  
 30 30 15 8 30  
 Pav. Pav. Pav. Pav. Pav.  
 165.34 ✓  
 Pav. End Conc. Pav.

✓  
 165.34 Pav 52



Lt.

Σ

Rt.

54

Potomac Cont. from p-53

1700

156.1	151.5	151.57	151.41	151.21	150.8	146.8	147.1
92	138	1377	1393	1413	145	135	137
30	19	14		4	11	20	30
		Edge Post		Edge Post			
			16534 ✓				



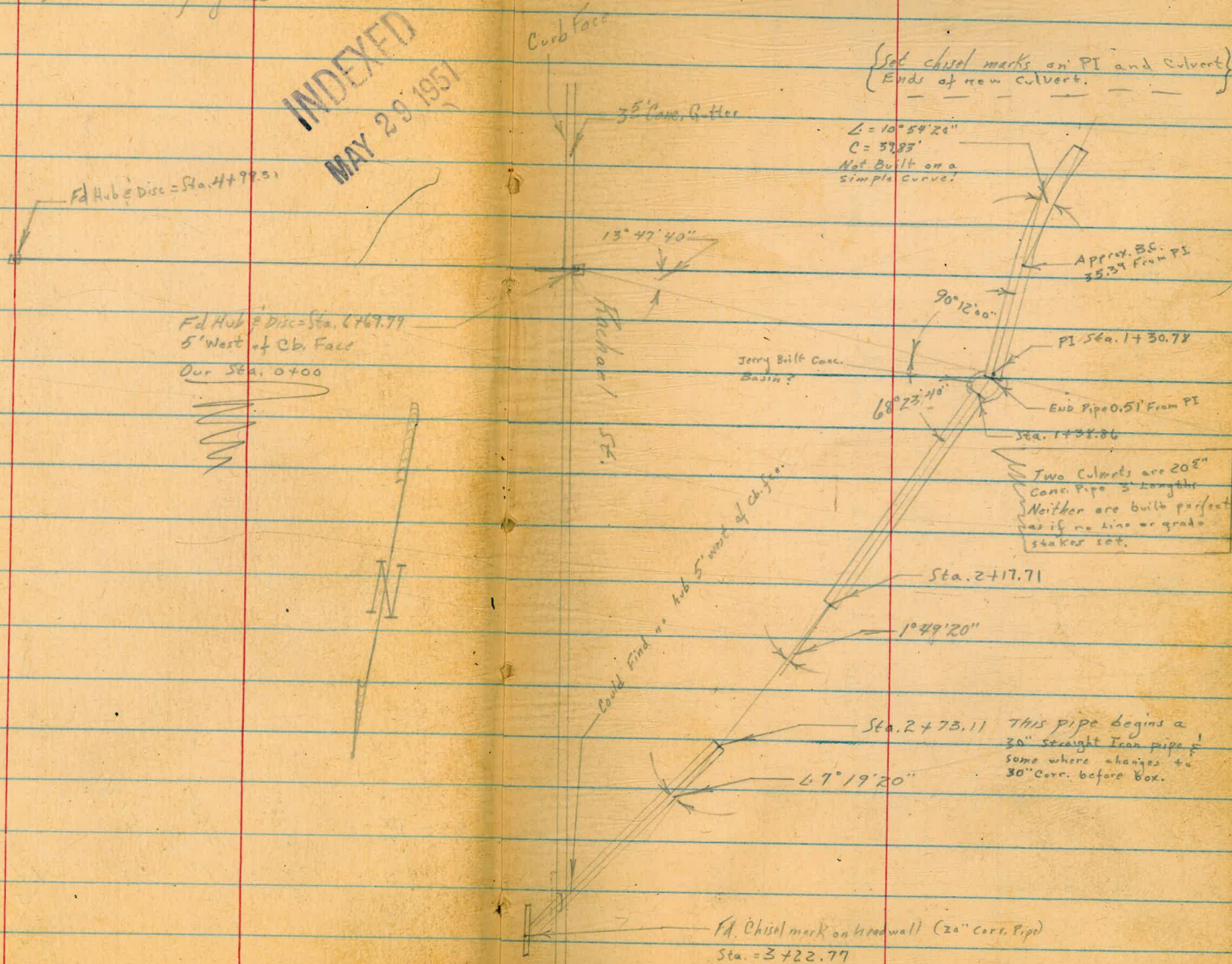
Roberts  
Cota  
Moore  
Piller  
5-17-51  
W.O. 20530

Location of Culverts in National City  
West of Rachaol, 2' North of Cumberland

55

See FB 1796 page 62

INDEXED  
MAY 28 1951





0+82

1392  
5.4

0+52

1392  
5.3

0+50

1420  
5.6

0+49 Railroad tie barbed wire fence TP to Rachael

1435

0+24

1.1

0+22

1404  
1.5

0+00 Fd. Hub of city Disc

1435  
1.1

BM

1.06 144.59 X

143.53 Hub & Disc Sta. 6+69.79 FB17967969 or Sta. 0+00

144.59 X



1451 Dirt Cover

144.4  
3.2  
25  
140.2  
81  
8.9  
14  
Top

1438.86 Begin Culvert

141.0  
2.8  
25  
140.0  
3.8  
12  
137.2  
7.4  
3  
135.20  
9.39  
INVERT  
8.6  
2  
135.4  
9.0  
25

END OF CULVERT (South End) (75.22 From PJ)

135.0  
9.6  
Pipe  
134.4  
10.0  
Invert  
134.4  
11.21  
INVERT  
133.2  
7.9  
Pipe  
135.2  
9.4  
Pipe

END OF CULVERT 0.51' North of PJ (North End)

135.2  
9.40  
INVERT

1430.78 Dirt Cover Top

137.45  
6.94

1423 Edge of Dirt Cover over Culvert

135.5  
9.1

0+89

135.2  
8.9

144.59X

144.59X



Contd From Page 57

Lt E Rt

58

check

106 143.53 = 143.53

2+73.11 Begin Culvert

1392	1386	1342	1392	1398
47	60	9.95	49	49
20	2	INVERT	7	25

2+44

1393	1380	1365	1380	1385
5.3	6.6	8.1	6.6	5.0
15	3		15	20

2+17.71 END CULVERT

1393	1378	13548	1389	1392	1392
5.3	6.8	9.11	6.2	4.9	4.7
20	2	INVERT 2	8		25

2+11 Dirt Cover

1400	1400	1392	1392
4.6	4.6	4.7	4.8
16	5		25

14459X

14459X



Roberts  
Moore  
Fillon  
5-28-51  
W.O.

X-Section Winchester  
Rancho Dr. to Roo Dr.

INDEXED  
JUL 6 1951

0+50

0+11 opposite EC curb Ret.

0+00 West Line Rancho (Levels on Line TP & Rancho)

Q Curb Return

West Curb Line Rancho

{ set Hub & Disc NW Cor. Rancho & Winchester replaced N.E. Cor.  
Hub no tank (Hub had been disturbed) with Hub & Disc FROM  
Hub & CT NW Corner Sea Breeze & Winchester AND Hub &  
C.F. N.E. Corner Roo & Winchester

Q Rancho Drive

BM

8.64 226.60 X

217.96 NW 8P

Winchester & Roo

226.60 X

Lb.

Q

R

59

220.7	222.3	223.0	223.29	221.75	221.37	222.1	221.2
59	43	3.6	4.31	1.85	4.23	4.5	5.4
40	30	22		20 got	20 cb	30	30

222.7	223.8	224.6	225.32	224.60	225.23	225.1	224.1
3.7	2.8	2.0	1.28	2.00	1.37	1.5	2.5
50	131.5	23	Edge Pav.	22 got	22 cb	131.5	50

224.32	224.96
2.28	1.64
20 got	20 cb

223.2	223.8	224.9	225.62	225.06	224.65	225.30	222.69	223.28
3.4	2.8	1.7	0.98	1.54	1.95	1.30	3.91	3.32
48	31.5	23	Edge Pav.	221	35.5 EC got	33.5 cb	100 got	100 cb

223.5	224.3	225.88	225.39	225.28	224.80	223.45
3.1	2.3	0.72	1.21	1.32	1.80	3.15
48	131.5	Edge Pav.	221 cb Lini	131.5 P.L.	50	100



Cont'd. From Page 59

2±40= BC. Set Hub & Disc North Line

2+00

1+89<sup>±</sup>

Lt E Single Garage

1+45

1+36<sup>±</sup> 23<sup>±</sup> Lt to Center P. Pole # JP 89537

1+35

1+00

0+53<sup>±</sup>

Q 6<sup>2</sup> Conc. Drive

226.60X

Lt

213.8	213.8	213.86	214.17	214.79	214.3	2140	60
12.8	12.8	12.74	12.43	11.81	12.3	12.6	
50	30	50	20 got	30 cb	30	50	

214.2	214.1	214.00	214.10	214.70	214.5	214.4
12.4	12.5	12.60	12.50	11.90	12.1	12.2
50	30	50	20 got	30 cb	30	50

214.38	213.87					
12.22	12.73					
341 Floor	292 Apex					

215.3	215.8	216.08	215.71	216.32	217.6	218.3	218.6
11.3	10.8	10.52	10.89	10.28	9.0	8.3	8.0
50	30	50	20 got	20 cb	30	35 0	30

215.6	218.3	219.0	216.61	216.22	216.82	217.9	218.7
11.0	8.3	7.6	9.99	10.38	9.78	8.7	7.9
63	30	27	50	20 got	20 cb	30	50

220.4	220.5	220.5	218.87	218.50	219.11	219.3	219.4
6.2	6.1	6.1	7.73	7.10	7.49	7.3	7.2
50	30	20	50	20 got	20 cb	30	50

220.81	220.64	221.82	222.61			
6.9	5.6	4.78	3.99			
49 Floor	41 BKK	34 BKK	283 Edge			

226.60X



Cont'd From Page 60

Lt

Q

Rt

61

East Curb Line Res (No curb to South)

214.30  
12.30  
70

215.18  
11.42  
131.5

215.76  
10.84  
Pav  
Edge

216.04  
10.56  
208

216.18  
10.42  
261  
Gut

216.75  
9.85  
261  
Cb

218.09  
8.51  
100  
Gut

218.72  
7.88  
100  
Cb

2+86<sup>2</sup> E. Line Res Drive

214.7  
11.9  
50

215.3  
11.3  
131.2

215.91  
11.7  
Pav  
Edge

215.84  
10.76  
208  
Gut

216.46  
10.44  
208  
Cb

216.9  
9.7  
131.5

226.60X

226.60<sup>v</sup>X



Storm Drain Survey Paradise Hills  
Winchester, Roanoke Co. & Roanoke

See Page 29

1+63.5 W. Edge Pav.

1+48.5 E. Edge Pav.

1+43.57 49.08' to N.E. Cor. Hub  
Set Hub E. Line Ro. L.H. = N° 57' 30"

1+00

0+50

0+00 = 5185.40' Fd. Hub & CT  
Also Fd. Sub Sta. 1+30.28

226.60  $\pi$  ✓ From Page 61

INDEXED

JUL 6 1951

215.91

10.73

215.35

11.25

215.11

11.49

213.8

12.8

217.0

12.6

217.5

9.1

INDEXED 62

JUL 6 1951



Cont'd From Page 62

4+00

3+50

3+00

2+50

2+00

TP

0.25

216.93  $\pi$

992

216.68  $\pi$

1+91.12 } Set Hub @ Rio 2' East of East Edge of West Pav Strip

L. Lt = ~~89° 55' 60"~~

90° 55' 00" CPL

226.60  $\pi$

Lt

E

Rt

63

2099

7.0

211.6

5.3

212.9

7.0

214.5

2.4

216.5

0.4

216.93  $\pi$

216.7

99

226.60  $\pi$

2099

7.02

211.62

5.31

212.23

3.70

214.92

2.01

216.61

0.32

216.93  $\pi$

216.7

99

226.60  $\pi$

2 Pav. Edge

2 Pav. Edge

2 Pav. Edge

2 Pav. Edge

2 Pav. Edge



Cont'd From Page 63

5445

5425

5400

4797.1 W. Edge of W. Strip

4782.1 E. Edge of W. Strip

$\angle R_1 = 90^\circ 00' 00''$   
 4780<sup>13</sup> Set Hub & Disc On North Line Roanoke produced from  
 Hub & CT N.W. Cor. Seabreeze & Roanoke thru Hub & CT N.E. Cor.  
 Reo of Roanoke. 51.25' to Hub N.E. Cor. Roanoke & Reo  
 $109^\circ 52' 00'' = \angle$  From N. Line Roanoke to our line.

4750

216.93A

Lt

Rt

64

2028  
14.1

206.0  
10.9  
10

206.0

10.9

203.1

13.8  
10

207.3

9.6

207.18

9.75

207.40

9.53

207.4

9.5

208.3

86

208.35

858

2  
Par.  
Edge

216.93A



Cont'd From Page 64

26

27

27

65

7.700

195.3

9.5

191.8  
130  
6

6.780

193.0

11.8

6.750

199.3

5.5  
10

195.9

8.9

198.5  
6.3  
10

6.730

201.0

3.8  
10

200.3

4.5

200.3  
4.5  
10

6.720<sup>96</sup> Set H.S. & Disc L.H. = 73°00'00" into Ravine

200.8

4.0

6.700

201.2

3.6  
10

201.1

3.7

198.7  
6.1  
10

T.P.

0.61

204.80<sup>✓</sup> 12.81 204.12<sup>✓</sup>

204.80<sup>✓</sup>

216.93<sup>✓</sup>



Cont'd From Page 65

28

E.

RT

66

check

$$125 \cdot 217.99 \checkmark = 217.96 \checkmark$$

T.P.

$$14.45 \cdot 21224 \checkmark \cdot 0.01 = 204.79 \checkmark$$

7+62.05 Sat Stud  $\frac{1}{2}$  mil Ravine L. Rt Approx 32°

1947

10.6  
10

1892

15.6

1920

12.8  
10

1894

15.4

7+40

$$204.80 \checkmark$$

$$204.80 \checkmark$$



Roberts  
Moore  
Fuller  
11-29-51  
W.O. 20937

Survey to Extend Storm Drain  
Block 5, Frary Hts  
See FB 1692 Page 36

INDEXED  
DEC 4 1951  
67

0+75	7.3 10	2743	11.3 10	270.3	271.6 10
0+50	10.7 10	2709	9.6 5	272.00	271.0 5 272.0 5
0+25	8.0 10	2736	9.6 10	2720	273.0 10

0+00 End Existing 48" Conc. Pipe

9.26  
INVERT

T.P.	0.59	281.60	12.76	281.01	281.60
T.P.	0.49	293.77	12.98	293.28	
T.P.	0.11	306.26	9.85	306.15	
(Just Produced Line of Existing 48" Storm Drain See page 36 FB 1692)					
T.P.	1.23	316.00	11.61	314.77	
BM	7.40	326.38		318.98 NW 1/4	31 <sup>st</sup> & Thera



Contd. From Page 67

Lt

Rt

68

check 3.18 318.97 = 318.98

Starting BM

T.P. 11.45 322.15<sup>✓</sup> 0.05 310.70<sup>✓</sup>

T.P. 13.02 310.75<sup>✓</sup> 0.66 297.73<sup>✓</sup>

T.P. 12.81 298.39<sup>✓</sup> 0.52 285.51<sup>✓</sup>

T.P. 12.62 286.03<sup>✓</sup> 0.29 273.41<sup>✓</sup>

13.77 259.93<sup>✓</sup> INVERT

Sly End Culvert under Redwood

T.P. 11.12 273.70<sup>✓</sup> 11.26 272.58<sup>✓</sup>

T.P. 1.73 283.84<sup>✓</sup> 12.66 282.11<sup>✓</sup>

T.P. 2.16 294.77<sup>✓</sup> 0.18 286.61<sup>✓</sup>

T.P. 12.24 286.79<sup>✓</sup> 1.31 274.55<sup>✓</sup>

12.54 263.32<sup>✓</sup> INVERT

Nly End Culvert under Redwood See Next Page

TP 3.94 275.86<sup>✓</sup> 9.85 271.92<sup>✓</sup>

T.P. 0.76 281.77<sup>✓</sup> 0.59 281.01<sup>✓</sup>

1400

Eucalyptus Tree on G

281.60 X

274.9

271.4

270.0

270.9

6.7  
10

102

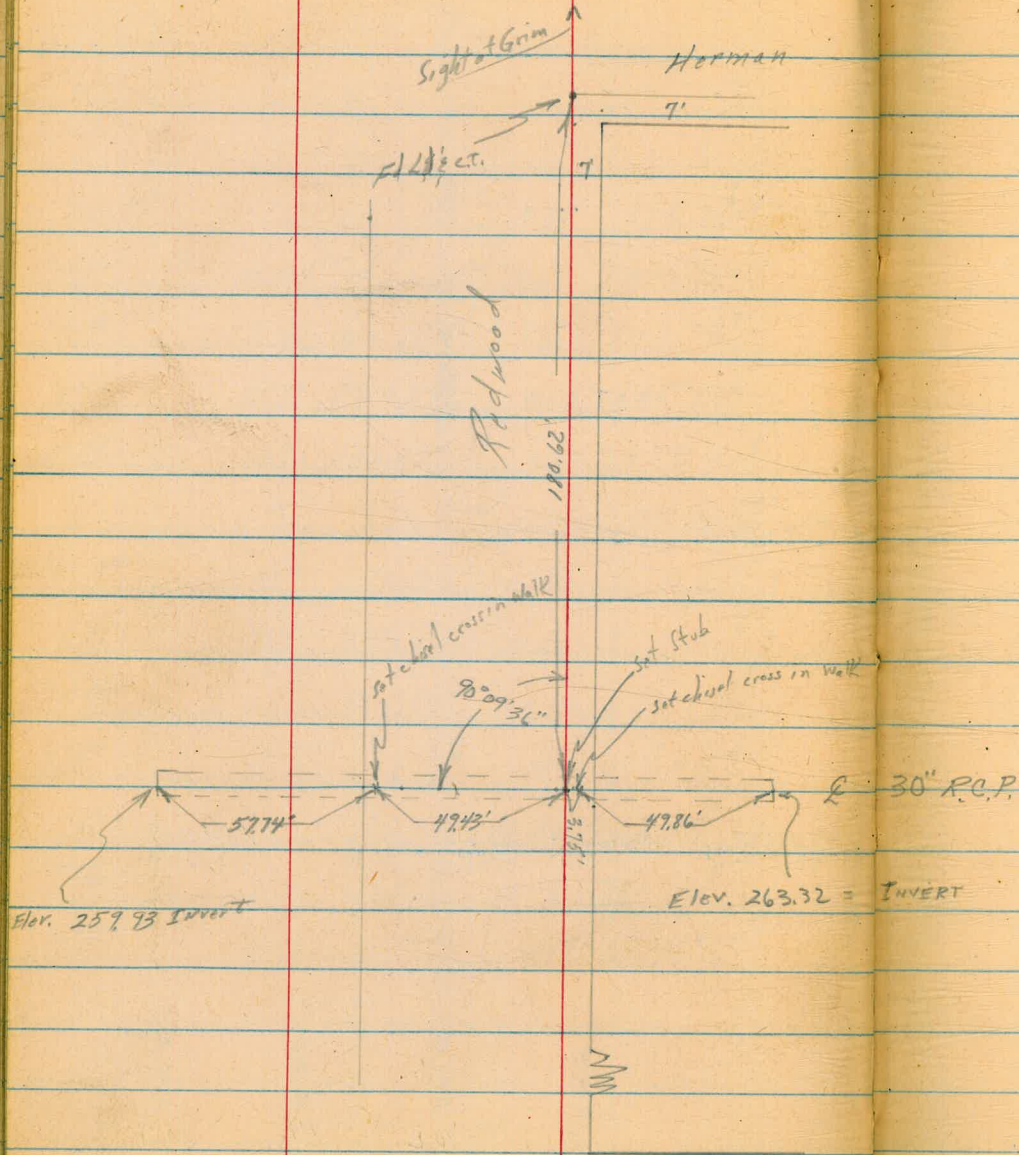
116  
10

10.7  
20

281.60 X

Reduced by ORL 12-19-57





37'nd  
32''







71



72



73



74

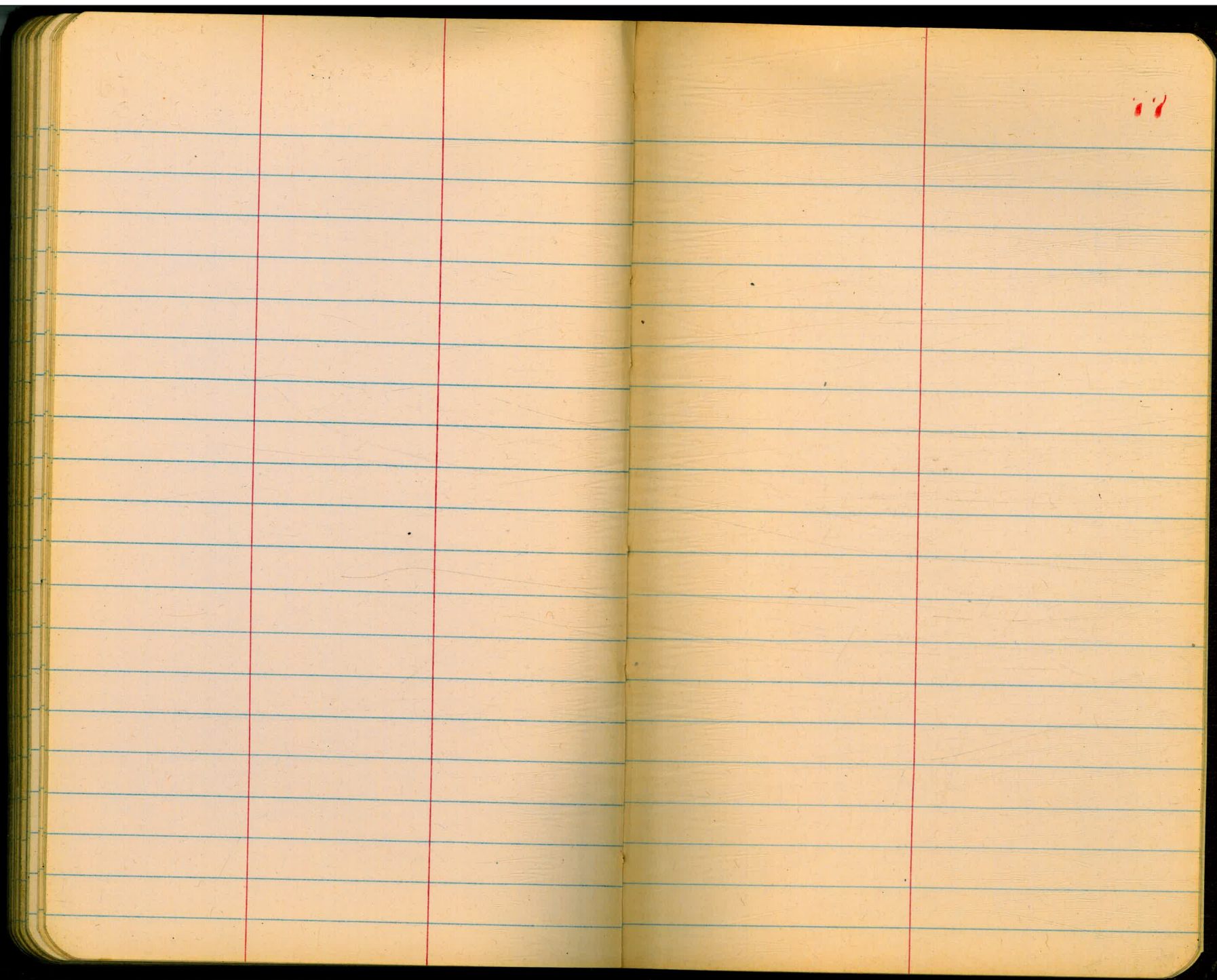


75



76

















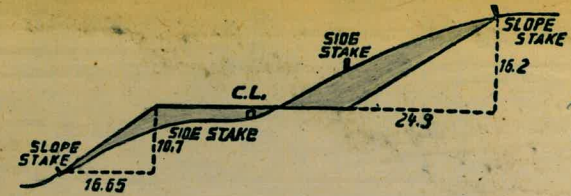


2  
 5785 40  
 1730 28  
 455 12  
 85 00

188  
 67  
 79

1190  
 287  
 1377

N 38-45-30 W  
 70-11-30  
 108-57-00  
 179-60  
 S 76-03 W



1077  
 356  
 13

**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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