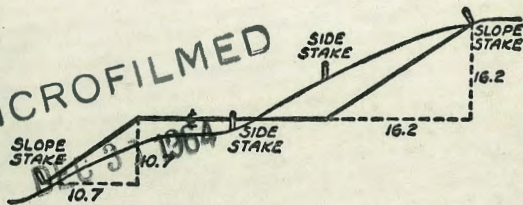


2086

MICROFILMED



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEXED

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except page # 4

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Page

1- X-Sect. Imperial - 40th to 46th

20-35 incl X-Sec Roswell St, Melrose Pl. to Beverly St

36-42 incl X Sec Hilltop Dr Roswell to Winston Dr

44-51 Niagara - Venice to Capistrano

53 - 41st - Newton to National

55 - Ties - n. Li Roswell @ Hilltop

58 X-Sec Roswell St @ 56th X-Sec.

66 Tripoints, B&K-14 - Beverly

X-Sect. Imperial - from Boundary
to 46th for Grade est.

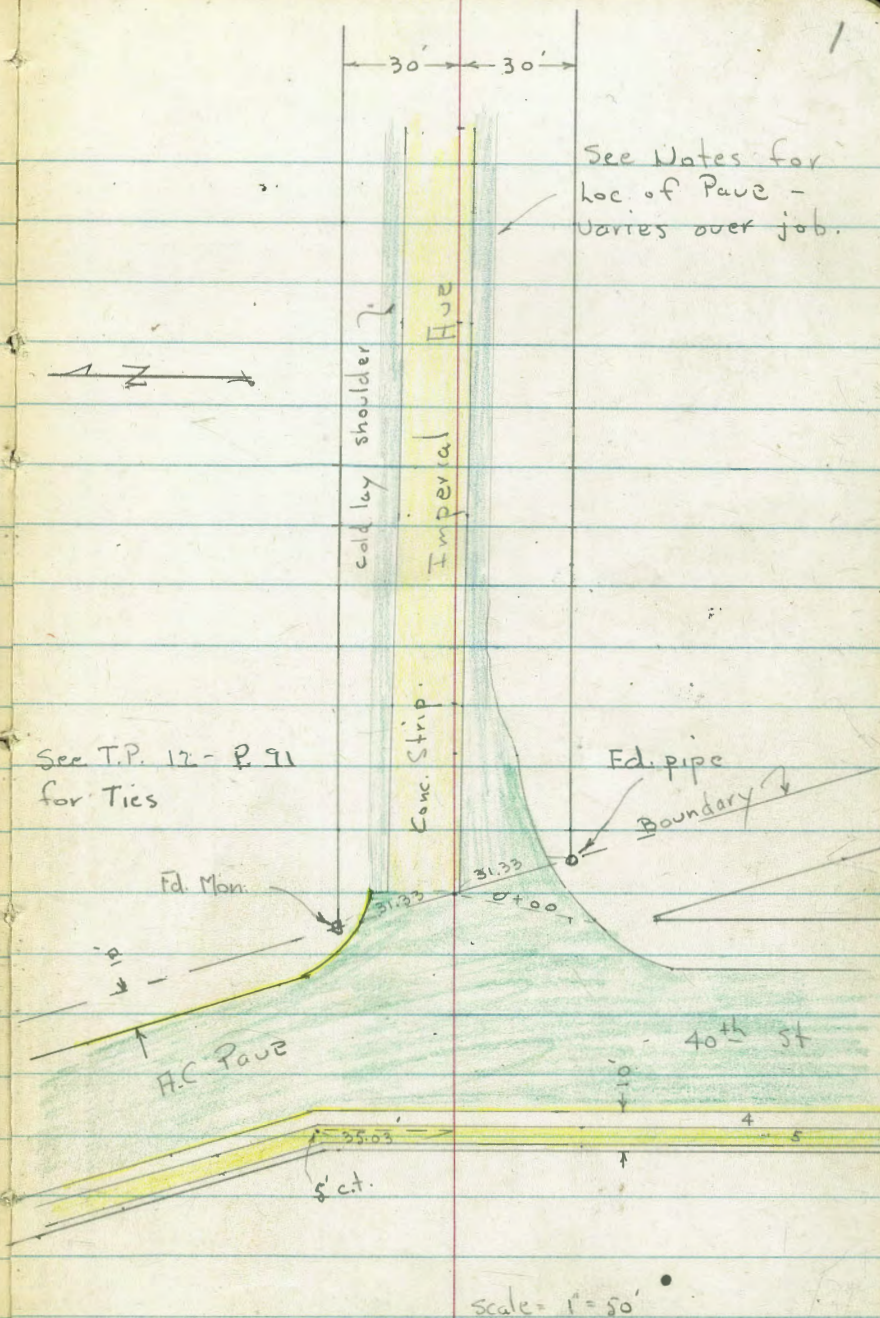
4928

W.O. 25020

4-11-50 = Comp.

Osborne
Hardin
Hatch
Shepard

INDEXED
T.H.K.
APR 12 1950



Lot 45

$7+48.35$
Ang. $0^{\circ}12'20''$ Lt.

$15+33.15 = P.O.T.$
Chisel Cross

Imperial Euc
Line Straight Thru from 0100 to 7+48.35

30' 30'

Fd. ct. - 1.23 South of E

Lot 50

Lot 49
Hortons Purchase



See T.P. 12
P. 91

Terrace

w.L. of Palomar
Map. 2076

50' 30'

$24+13.03$
= Cross

Line Straight Thru to 48.45
Imperial Euc

Fd. ct. 0.61 S. of E

Fd. ct. 0.93 S. of E

$20+80.66 =$ (Pavement)
Ang. $0^{\circ}01'$ Lt

E.L. Panorama Hts.
Map. 1548

30' 30'

✓

46th

15
15

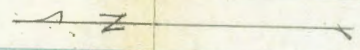
st.

$37 + 54.82 = \text{Cross}$
0.46 S. of c.t.

30' 30'

30' 30'

Sec T.P. 19
P. 27
also 1551-P. 67



E.L. Palamar Terr.

Imperial Ave

Imperial Ave

West st.

$34 + 0.63 = \text{ct.} = .05 \text{ south}$

30'
45th
30'

$30 + 11.75 = \text{ct.}$
Ang. $0^{\circ} 01' \text{ Rt.}$

50' 30'

st

4

REDUCED 4-17-50
P.V.S.

Lt. = N.

Rt. = S.

Req. X-Sections of Imperial for
Grade est.

0+50

110.5	110.5	108.42	108.72	108.86	108.85	108.8	108.4	108.4
6.1	6.1	8.20	7.90	7.76	7.77	7.8	8.2	8.2
40	30	21.5	16.5	2	2	16	30	40
		C.L.	5			C.L.		on C.L. Drive
111.6	109.61	109.80	110.03	110.07	109.86	109.49	109.23	109.23
5.0	7.01	6.82	6.59	6.55	6.76	7.13	7.39	7.39
30	21	16.2	17	17	15	30	33	33
along Cemetery	edge of Cold Lay = C.L.	edge Conc = S	edge Conc = S	edge Conc = S	edge Conc = S	edge Conc = S	edge A.C.	edge A.C.

0+10 = will use letter 'S' to represent edge of
Conc. Strip. - C.L. = edge of Cold Lay.

0+01.4 = opp. end of cb. on Lt.

110.30	109.85
6.32	6.77
21.4	9.4 = 21.4
Top	

0+00 = ± at Boundary - Sect. on Bound. Line

111.1	110.58	110.04	110.24	110.33	110.33	110.06	109.42	109.22	108.9
4.9	6.04	6.58	6.34	6.29	6.29	6.56	7.20	7.40	7.7
31.33	25.1	25.1	16.8	1.8	1.8	15	31.33	34	50
Cor.	Top	gut	edge Conc Strip	edge Conc.	edge Conc.	edge Conc.	Cor.	edge A.C. Pave Drive	c.L. Drive

0-22 = opp. P.C. of Cb. on Lt.

111.57	111.07	110.88	110.95	111.05	110.99	110.79	110.57
5.05	5.55	5.74	5.67	5.57	5.63	5.83	6.05
38.2	38.2	30	15	15	15	30	50
Top P.C.	gut						

0-30 = Sect. 90° to ±

- See P. ? = end.

Please check before reducing

113.21	112.57	111.39	111.27	111.29	111.26	111.10	110.91	110.58
3.41	4.05	5.23	5.35	5.33	5.36	5.52	5.71	6.04
65.7	65.7	30	15	15	15	30	50	100
Top	gut			116.62				

B.M. 4.04 116.62
Using 118.40 at S.E. B.P. 39th + Imp.

112.58
112.51 - should be

S.E. Top. Hyd 40th + Imperial
→ B. 1722 - P. 28

Imperial

3+50

	Lt.				Rt.			
	106.4	103.3	103.58	103.63	103.28	103.1	102.9	100.1
	3.5	6.6	6.32	6.27	6.62	6.8	7.0	9.8
	30	19	12	5	6.2	10	25	30
	S.	C.L.	S.	S.	S.	C.L.	S.	S.

3+00

	106.3	103.1	103.82	103.88	103.76	103.1	102.4	101.3
	3.4	6.2	6.08	6.02	6.14	6.2	5.5	8.6
	40	30	19	13.2	4.7	15	30	32
	S.	C.L.	S.	S.	S.	C.L.	S.	S.

2+50 = end Cold Lay on Rt.

2+21 - 30.3' Rt. = + of 2 Gas pumps

104.06	104.40
5.84	5.50
30.3	33.8
Ret. pumps	floor
	House

T.P. 5.03 109.90 117.5 104.87

2+00 = Beg. Ser Sta. Cold Lay on Rt.

109.90							
107.1	106.8	104.3	104.48	104.52	104.44	104.2	104.1
9.5	9.8	12.3	12.14	12.10	12.18	12.4	12.2
40	30	19.5	13.8	4	10	19	30
S.	C.L.	S.	S.	S.	S.	C.L.	S.

1+50

107.3	105.5	105.66	105.76	105.70	105.6	106.0	105.9
9.3	11.1	10.96	10.86	10.92	11.0	10.6	10.7
30	20	14.5	5	3.5	12	17.5	30
C.L.	S.	S.	S.	S.	C.L.	C.L.	S.

1+00

108.7	108.2	107.0	107.23	107.26	107.20	107.4	107.2	107.87
7.9	7.9	9.6	9.39	9.36	9.42	9.2	9.4	8.75
40	30	20	15	5	3	17	29.8	29.8
S.	C.L.	S.	S.	S.	S.	C.L.	along Bldg.	floor.

116.62

Imperial

6+50

1009 Lt.	1043	104.42	109.50	109.30 Rt.	104.6
1.0	5.6	5.48	5.40	5.60	5.3
30	15	8.6		9.4	30
	C.L.	S		S	C.L.

6+00

109.1	108.8	105.0	105.10	105.18	105.02	104.8	105.1	105.2
0.8	1.1	4.9	4.80	4.72	4.88	5.1	4.8	4.7
40	30	16	9.2		8.9	14	30	40
		C.L.	S		S	C.L.		

5+50

108.6	104.9	105.13	105.17	105.02	104.8	104.4	104.3
1.3	5.0	4.77	4.73	4.88	5.1	5.4	5.6
30	16	9.8		8.3	13	30	40
	C.L.	S		S	C.L.		

5+00

108.3	108.0	104.5	104.72	104.79	104.56	104.9	103.9	100.3	104.1
1.6	1.9	5.4	5.18	5.11	5.34	5.5	6.0	9.6	10.8
40	30	16.5	10.3		7.8	11.0	30	36	45
		C.L.	S		S	C.L.		Toe	

4+50

107.5	104.2	104.43	104.54	104.41	104.2	104.1	103.9
2.4	5.7	5.47	5.36	5.49	5.7	5.8	6.0
30	17	10.9		7.1	11	30	40
	C.L.	S		S	C.L.		

4+00

107.1	106.7	103.6	103.98	104.02	103.07	103.5	103.1	99.3	99.43
2.8	3.1	6.3	5.92	5.88	6.03	6.4	6.8	10.6	16.2
40	30	18	11.5		6.5	10	23	30	39
		C.L.	S		S	C.L.			Toe

for loc. + E lev.

3+76 = Φ 12" Cor. Iron Culvert - see B 1772-P. 25

3+53 - 19.5' Rt = Φ of Inlet to $\frac{1}{2}$ 12" Cor. Iron open drain - outlet over end of outlet to next drain

109.90

104.49
7.41
19.5
I.E. Drain

Imperial

9+76 - 22.6' Rt. = ± of 10' opening cb. Inlet.

(standard) - 18" Cor. Iron - culvert

Lake on Lt.

9+50

9+00 - Beg. Lake on Lt.

T.P. 5.51 103.41 12.00 97.90

8+50

8+00 - Beg. C.L. roll on edge on Rt.

7+50

7+00

Lt	±	Rt	8
91.8 11.6 45 water level	93.5 9.9 41 High water Mark	96.1 6.5 30 C.L.	96.1 6.7 11 C.L.
	97.3 6.1 30 C.L.	98.5 6.9 11 C.L.	98.28 7.13 5 S
	96.33 7.08 15 grate	95.90 7.51 22.6 Top of cb.	95.36 8.05 22.6 I.E. of Box
	96.26 7.15 13 S	95.90 7.51 22 C.L.	95.6 7.8 30
	94.9 8.5 40	98.9 4.5 30	96.8 6.6 12 C.L.
	96.66 6.75 5.3 S	96.72 6.69 12.7 S	96.37 7.04 22 C.L.
	96.12 6.69 12.7 S	96.1 7.3 22 C.L.	96.2 7.2 30 Toe
	97.1 7.1 60 Toe	97.3 7.2 30 Toe	97.3 7.2 30 Toe
	101.8 8.1 30 C.L.	97.1 12.2 12 C.L.	97.74 12.16 6.1 S
	99.5 10.4 13 C.L.	99.54 10.36 6.8 S	99.67 10.23 11.3 S
	101.4 2.5 30 C.L.	101.3 8.6 14 C.L.	101.50 8.40 7.4 S
	101.59 8.31 10.6 S	101.45 8.45 10.6 S	101.3 8.6 10.7 C.L.
	103.34 6.56 10.1 S	103.21 6.69 14 C.L.	103.1 6.8 14 C.L.
	103.25 6.65 8.0 S	103.2 6.69 14 C.L.	103.1 6.2 30
	109.90 6.56 10.1 S	103.21 6.69 14 C.L.	103.1 6.2 30
	111.9 10.2 40	109.0 0.9 30	103.1 6.8 14 C.L.
	103.1 6.8 14 C.L.	103.25 6.65 8.0 S	103.2 6.2 30
	107.4 2.5 30 C.L.	107.3 8.6 14 C.L.	107.4 2.5 40
	107.3 2.6 40	109.9 0.9 30	100.6 9.3 30
	100.9 9.0 40	100.9 9.0 40	100.9 9.0 40

Imperial

Lt.

±

Rt.

9

12+50

110.8
1.9
30
107.8
4.9
13
c.L.
108.02
4.66
5.6
5
108.15
4.53
12.6
5
108.08
4.9
17
c.L.
108.1
4.6
30

12+00

108.0
4.7
40
107.4
5.3
30
105.0
7.7
11
c.L.
105.12
7.56
5.3
5
105.23
7.45
12.8
5
105.07
7.61
17
c.L.
104.6
8.1
17
c.L.
103.0
9.7
30
102.9
9.8
40

11+50

105.6
7.1
30
102.3
10.4
11
c.L.
102.18
10.50
5
5
102.23
10.45
13.1
5
102.10
10.58
17.5
c.L.
101.9
10.8
17.5
c.L.
101.1
11.6
30

T.P. 10.94 112.68 167 101.24

112.68

11+00

102.4
1.0
40
102.2
1.2
30
99.7
3.7
10
c.L.
99.67
3.74
4.8
5
99.71
3.70
13.3
5
99.57
3.84
17.5
c.L.
99.4
4.0
17.5
c.L.
99.5
3.9
30
102.9
1.0
50

10+60 - end lake on Lt.

10+50

91.0
11.6
45
99.2
4.2
30
98.1
5.3
11
c.L.
97.96
5.45
4.6
5
98.01
5.40
13.5
5
97.81
5.60
17
c.L.
97.6
5.8
17
c.L.
98.1
5.3
30
94.8
9.6
42
Toe

10+00 = end of roll cb. on Rt.

91.8
11.6
45
98.0
5.4
30
96.9
6.5
11
c.L.
96.77
6.64
4.4
5
96.76
6.45
13.6
5
96.38
7.03
23
c.L.
95.9
7.5
23
c.L.
96.3
7.1
30
80.9
22.5
53
Toe

B.M. = top-back of cb.

7.07 96.34

E. end of Inlet.

103.41

Imperial

Set B.M. on Ct. - 123 S.

1045 115.00

17 + 48.35 = Cross = Ang. 0° 12' 30" Lt.

Lt.				Rt.			
121 ⁹	120 ³	115 ¹	114 ²	114.85	114.99	114.90	114 ⁸
3.6	4.7	10.4	10.9	10.60	10.46	10.55	10.7
40	30	22	12	7.7		10.2	14
				S	on Cross	S	C.L.

17+00

121 ⁴	121 ³	116 ⁷	116 ²	116.81	116.90	116.77	116 ⁶
4.1	4.2	8.8	8.8	8.64	8.55	8.68	8.9
40	30	22	13	7.6		10.5	14
			C.L.	S		S	C.L.

16+75

122 ¹	122 ¹	117 ⁶	117 ⁶	117.73	117.80	117.67	117 ⁵
2.8	3.4	7.9	7.9	7.72	7.65	7.74	8.0
40	30	22	13	7.4		10.6	14
			C.L.	S		S	C.L.

16+50

126 ⁶	125 ³	118 ⁸	118 ⁴	118.40	118.51	118.39	118 ⁰
+1.1	0.2	6.7	7.1	7.05	6.94	7.06	7.5
40	30	22	13	7.3		10.6	14
			C.L.	S		S	C.L.

16+00

130 ²	128 ⁴	120 ⁰	119 ³	119.42	119.50	119.40	119 ²
+4.7	+2.9	5.5	6.2	6.03	5.95	6.05	6.3
40	30	22	13	7		10.9	15
			C.L.	S		S	C.L.

15+75

130 ³	128 ¹	120 ³	119 ⁶	119.72	119.84	119.77	119 ⁵
+4.8	+3.2	5.2	5.9	5.73	5.61	5.64	6.0
40	30	22	12	7		11	15
			C.L.	S		S	C.L.

15+50

129 ⁶	127 ⁹	120 ¹	119 ²	119.9	119.89	119.78	119 ⁵
+4.1	+2.4	5.4	5.8	5.64	5.56	5.67	6.0
40	30	22	12	6.8		11.1	15
			C.L.	S	125.45	S	C.L.

Imperial

20+50 - Pond on Lt. - No Culvert Thru

19.0
50

87-1
19.7
44

95-1
10.3
30

102-1
3.4
20

101.8
4.0
11

101.99
3.77
8.2

5
C.L.

\$

102.22
3.54

101.91
3.85

101-5
4.3

9.8
5

Rt

102-3
3.5

100-2
5.6

84-9
20.9

27
30

55
Toe

12

T.P. 2.41 105.76 12.76 103.35

Water Level

105.76

20+00

87-5
28.6
50
Toe

91-5
18.6
30

104-4
11.7
18

103-9
12.2
11

104.14
11.97
8.2

5
C.L.

104.38
12.12
9.8
5

103.99
12.2
14
C.L.

103-9
13.0
30

103-1
19.5
40

19+50

91-9
18.7
37
Toe

101-4
14.7
30

106-3
9.4
20

106-2
9.9
11

106.25
9.86
8.2

5
C.L.

106.53
9.85
9.8
5

106.26
9.8
14
C.L.

106-3
9.2
30

106-9
8.8
40

19+00

102-6
13.6
40

105.77
10.34

103-3
12.3
30

108-9
7.2
17

108-3
7.8
11

108.42
7.69
8

5
C.L.

108.57
7.70
10.14
5

108.41
7.9
14
C.L.

108-3
6.6
30

109-5
6.4
40

18+79 - 16.1' Lt. = Outlet of Culvert

18+74 - 21.4' Rt. = Inlet of 12" Cor. Iron Culvert

16.1
I.E. Pipe

106.96
9.15
21.4 = I.E. Pipe

18+50

113-3
2.8
40

112-5
3.6
30

110-6
5.5
25

110-6
5.5
13

110.57
5.54
7.8

5
C.L.

110.69
5.58
10.1
5

110.53
5.7
14
C.L.

110-4
5.5
25

110-6
2.7
30

113-3
1.9
40

18+00

119-2
+2.1
40

118-2
+2.1
30

112-8
3.7
25

112-6
3.5
12

112.68
3.43
7.9

5
C.L.

112.77
3.46
10.1
5

112.65
3.8
14
C.L.

112-3
3.7
25

112-4
1.1
30

115-0
0.0
40

B.M. 111 116.11 115.00

Imperial

13

24+00

Lt.					Rt.					
100.8	99.6	84.9	84.2	84.36	84.48	84.37	84.2	85.3	84.2	89.0
+6.5	+5.3	9.4	10.1	9.92	9.80	9.91	10.0	9.0	5.1	5.3
40	30	20	12	8.4	9.6	14	20	30	40	
Top					C.L.					S

23+50

102.9	103.1	101.3	87.8	87.2	87.25	81.34	81.22	87.2	87.8	94.1	95.1
+10.6	+8.8	+7.0	6.5	7.1	7.03	6.94	7.06	7.1	6.5	0.2	+0.8
40	33	30	20	13	8.3	9.6	14	20	30	40	
Top					C.L.					S	

23+00

112.2	112.1	90	90	90.01	90.17	90.01	89.9	90	95	91	
+18.6	+17.8	3.6	4.3	4.21	4.11	4.21	4.4	3.8	+1.3	+2.7	
40	30	20	12	8.3	9.7	14	20	30	40		
Top					C.L.					S	

T.P.

Sd BM. 0.94 94.28 1242 93.34

#P76142 94.28

Nail in Pole -23+03
on Rt.

22+50

113.8	112.8	93	92	92.85	92.94	92.91	92.8	95.1	95.5	
+8.0	+7.0	12.8	13.2	12.91	12.82	12.85	13.0	10.7	7.3	
40	30	22	12	8.3	9.8	14	30	40		
Top					C.L.					S

22+00

104.7	103.8	96.1	95.1	95.58	95.64	95.56	95.1	96.0	97.8	
1.1	2.0	9.7	10.1	10.18	10.12	10.20	10.1	9.0	8.0	
40	30	18	12	8.2	9.8	14	30	40		
bank					C.L.					S

21+50

95.7	96.6	97.9	97.96	98.11	97.91	97.8	97.7	91.5	
10.1	9.2	7.9	7.90	7.65	7.85	8.0	8.1	14.3	
40	30	12	8.2	9.8	14	30	40		
C.L.					Toe				

21+00

99.8	95.7	100.3	99.8	99.96	100.16	99.71	99.6	100.2	98.4
16.0	10.1	5.5	6.0	5.80	5.60	6.05	6.2	5.8	7.4
40	30	20	11	8.2	9.8	14	27	30	
Toe					C.L.				

Imperial

Sect. on Diag = end of Bridge

26+60.7 = 10.4 Lt. = wly. of Bridge curb

26+58.5 = 9.4 Rt. = wly. of Bridge curb.

T.P. 2.51 72.60 12.63 70.09

26+30

with conc. Headwall

26+12 = 18.5 Lt. = Inlet of 12" C.I.

26+00

11.84 5
18.5 9.1
I.F. 5.2
Pipe 40

25+50

85 5
+2.8
40

25+00

91 5
+14.5
40

T.P. 1.40 82.72 12.96 81.32

24+50

103.0 5
+9.0
40

	Lt.					Rt.				
	23.19	20.76	20.03	20.16	69.99	20.73	75.15			
	to. 59	18.4	25.7	2.44	2.61	18.7	+0.55			
	Top.	10.4	10.4		9.4	9.4				
	Rail	Top	cut.		cut.	Top	Top			
		cb.				cb.	Rail			
	= Ely. of 10' conc. spillway.					72.60				
	13	15	17	17.31	71.51	71.34	71	71	71	71
	9.4	9.7	11.0	11.35	11.21	11.38	11.4	11.5	8.5	
	40	30	12	9		9.4	12	30	40	
			C.L.	S		S	C.L.			
	10	10	12	12	72.89	73.00	72.91	72.8	72	72
	6.3	6.5	10.1	10.1	9.83	9.72	9.81	9.9	10.0	9.8
	30	25	20	13	8.7		9.3	13	30	40
			C.L.	S			S	C.L.		
	85	76	75	75.74	75.81	75.72	75	76	80	80
	+2.8	+3.1	6.5	7.0	6.98	6.91	7.00	7.1	6.6	21
	40	30	20	12	8.6		9.4	13	20	25
			Top	C.L.	S		S	C.L.		
	91	78	78	78.65	78.76	78.69	78	79	81	81
	+14.5	+14.8	4.0	4.3	4.07	3.96	4.03	4.3	3.7	0.9
	40	30	20	13	8.6		9.4	13	20	25
			Top	C.L.	S		S	C.L.		
	103.0	82.1	81	81.56	81.66	81.56	81	81	82	82
	+9.0	+8.7	12.1	12.9	12.72	12.62	12.72	12.8	12.0	11.8
	40	33	20	13	9.5		9.5	13	30	40
			Top	C.L.	S		S	C.L.		
					94.28					

Imperial

Lt. Rt. W

29+00

55.3	56.2	62.9	62.8	62.84	63.10	62.94	5	5	9	4
17.3	16.6	9.7	9.8	9.76	9.50	9.66	9.1	14.1	14.7	15.2
40	30	20	12	9.1	5	9	15	25	30	40
	Toe		c.l.	5		5		Toe		

Note end of wall is buried - about 28+75

28+50 = Last shot on wall

51.9	53.72	51.0	63.1	64.0	64.04	64.35	64.29	65.3	51.0	56.9
21.2	18.88	15.6	8.9	8.6	8.56	8.25	8.31	7.3	15.6	15.7
Bot. wall	34.6	30	20	12	9	9.1	15	30	40	
	Top wall		c.l.	5		5				

28+00

49.3	53.58	51.1	65.3	65.35	65.74	65.73	61.0	51.4	56.1
23.4	19.02	15.5	7.3	7.25	6.86	6.87	5.6	15.2	16.5
Bot. wall	35.1	30	20	10	9	9	18	30	40
	Top wall			Covered		Covered			

27+50 = P.C. Ret. wall on Lt.

Ret. wall on Lt. curves out from abutment and
 Conc. spillway Drain.

Runs Parallel

47.0	53.64	51.0	66.9	67.07	67.08	67.08	61.6	51.1	54.8
25.6	18.96	15.6	5.7	5.53	5.52	5.52	5.0	15.9	17.8
Bot. wall	35.9	30	15	9.2		8.6	15	30	40
	Top wall			Conc. Ret. wall	Covered	Covered			

27+37.4 = 10.3 Lt = Ely. Bridge cb = wly. of 8.3

27+36.1 = 9.8 Rt = Ely. Bridge cb = wly. of
 10' Conc. spillway Drain

10.62	68.73	67.56	67.60	67.47	68.07	10.53
1.98	4.47	5.04	5.00	5.13	4.53	2.07
Top rail	10.3	10.3		9.8	9.8	Top Rail
	cb.	Top gut.		+Drain	Top cb.	

27+00 = on Bridge

for add Inf on Bridge Sec B. 1722-P. 23

47.0	69.34	68.65	68.75	68.66	69.37
25.6	3.26	3.95	3.85	3.94	3.23
= Creek Bed.	10.4	10.4		9.6	9.6
	Top cb.	gut.		gut.	Top cb.

72.60

Imperial

Lt

±

Rt

16

31+50

⁶ 56	⁴ 57	⁹ 59	³ 60	60.31	60.48	60.30	² 60	⁶ 60
8.5	7.7	5.2	4.8	4.80	4.63	4.81	4.9	4.5
35	30	25	13	8.9		9.1	13	30
			CL	5		5	C.L.	

31+07.75 = E.L. 45th

³ 56	¹ 57	⁹ 59	⁶ 59	⁶ 59.68	59.88	59.71	⁵ 59	¹ 59	³ 59
8.8	8.0	5.2	5.5	5.43	5.23	5.40	5.55	5.6	5.4
50	35	30	12	9		9	16.5	22	30
			C.L.	5			edge	C.L.	
							conc.		

See B. 1722-P. 23

check B.M. = c.f. - ± 45th + Imp.

5.50 59.61 59.81

30+77.75 = ± 45th

¹ 56	⁰ 57	⁹ 58	⁶ 59	³ 59.63	59.73	59.65	³ 59	¹ 59	³¹ 58	¹ 57
8.4	8.1	6.2	5.5	5.48	5.38	5.46	5.73	6.04	6.80	7.50
100	75	30	12	9		9	30	50	100	150
			C.L.						± Conc. strip	

30+47.75 = W.L. 45th

² 56	⁸ 57	³ 60	¹ 59	⁹ 59.69	59.91	59.78	⁵ 59	⁶ 59	⁵ 58
8.9	7.3	4.9	5.4	5.42	5.20	5.33	5.46	5.5	5.6
40	30	20	11	9		9	16.5	20	30
			C.L.	5		Imp.	edge	C.L.	
							conc.		

30+00

⁵ 55	⁶ 55	² 61	⁴ 60	60.37	60.67	60.56	³ 60	¹ 59	⁰ 58
9.6	9.5	3.9	4.7	4.74	4.44	4.55	4.8	6.0	7.1
40	30	20	11	9		9	13	30	40
			C.L.	5		5	C.L.		

T.P.

4.51

65.11

12.00

60.60

65.11

29+50

⁴ 55	³ 55	³ 61	³ 61	61.50	61.87	61.75	⁵ 61	¹ 60	⁹ 58	⁸ 57
11.2	11.3	11.1	11.3	11.10	10.73	10.85	10.8	10.1	12.5	13.7
40	30	20	12	9	10	9	11	15	20	30
		Toe	C.L.	5		5	C.L.			

72.60

Imperial

Lt.

±

Rt.

17

33+88.63 = w.l. West. st.

69 ¹ 4.3 40	69 ⁶ 7.8 30	69 ⁶ 7.8 15 C.L.	69.62 7.78 9.1 S	69.75 7.65	69.63 7.77 8.9 S	69 ³ 8.1 16	70 ⁰ 7.4 30	70 ⁶ 6.8 50
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33+50

67 ⁹ 9.5 30	67 ⁸ 9.6 15 C.L.	67.90 9.50 9 S	68.02 9.38	67.95 9.45 9 S	67 ⁴ 10.0 16 C.L.	68 ⁰ 9.4 30
------------------------------	--------------------------------------	-------------------------	---------------	-------------------------	---------------------------------------	------------------------------

33+33 - 30' Rt = ± 10' Conc Dr.

67.04 10.36 37 walk	66.97 10.43 29.6 = walk	67.38 10.02 30 Dr.	68.57 8.83 38.7 Dr.
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33+33 = 29.6' Lt = ± 4' Conc. walk

33+00

65 ² 12.2 40	65 ⁴ 12.0 30	65 ⁶ 11.8 15 C.L.	65.69 11.71 9 S	65.75 11.65	65.69 11.71 9 S	65 ⁴ 12.0 15 C.L.	65 ¹ 11.7 30	67 ⁴ 10.0 40
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T.P. 12.42 77.40 0.13 64.98 77.40

32+50

62 ⁹ 2.2 30	63 ³ 1.8 15 C.L.	63.42 1.69 8.9 S	63.51 1.60	63.40 1.71 9 S	63 ³ 1.8 16 C.L.	63 ⁶ 1.5 30
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32+00

58 ⁴ 6.7 40	58 ³ 6.8 30	61 ⁴ 3.7 25	61 ⁶ 3.5 13 C.L.	61.71 3.40 8.8 S	61.85 3.26	61.71 3.40 9.2 S	61 ⁴ 3.7 16 C.L.	61 ⁸ 3.3 30	61 ⁶ 3.5 40
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65.11

Imperial

36+50

Lt. Rt. 18

85.2	84.2	84.69	85.00	84.79	84.5	85.81
14	19	17.1	16.0	18.1	2.1	0.8
30	15	9.3		8.7	14	30
	C.L.	S		S	C.L.	

36+00

10 ^A	18 ^B	8 ^A	81.69	81.90	81.82	1	5	1
8.2	7.8	5.2	4.91	4.7	4.78	4.9	5.1	5.5
40	30	15	9.3		8.7	14	30	40
		C.L.	S		S	C.L.		

35+50

15 ¹	18 ³	18.73	18.91	18.75	18 ⁶	17 ⁵
11.5	8.3	7.87	6.9	7.85	8.0	9.1
30	15	9.3		8.7	13	30
	C.L.	S		S	C.L.	

35+00

12 ²	13 ⁴	15 ⁰	15 ⁵	15.79	15.89	15.75	15 ⁵	15 ⁰	15 ^A
12.7	13.2	11.6	11.1	10.81	10.7	10.85	11.1	11.6	11.2
40	30	20	15	9.3		8.7	13	30	40
			C.L.	S		S	C.L.		

34+65

12 ¹	13 ³	13 ⁶	13.77	13.84	13.70	13 ³	13 ⁶
14.5	13.3	13.0	12.83	12.76	12.90	13.3	13.0
30	20	15	9.2		8.8	14	30
		C.L.	S		S	C.L.	

H. - 35+14
Nail in Pole

I.P. #306156-H 10.37 86.60 117 76.23 86.60

34+28.63 = E.L

10 ⁶	10 ⁹	11 ⁵	11.71	11.79	11.61	11 ⁵	12 ⁰	12 ⁹
6.8	6.5	5.9	5.69	5.61	5.79	5.9	5.4	4.5
50	30	15	9.2		8.8	16	30	50
		C.L.	S		S	C.L.		

34+08.63 = West

10 ⁴	10 ¹	10 ⁵	10.63	10.73	11.31	10 ⁵	10 ⁶	11 ²	13 ⁴	16 ⁶
7.0	7.3	6.9	6.77	6.67	6.79	6.9	6.8	6.2	4.0	0.8
50	30	15	9.1		8.8	16	30	50	100	150
		C.L.	S	77.40	S	C.L.		± Dirt rd.		

check B.M. = ct. - 46th

4.29 90.95 91.16 = B. 1722 - P. 22

See B-1818 for Sections - 46th to 47th

37+54.82 = ct. 46th

89 ²	91 ⁰	90 ⁸	90 ¹	90 ⁸	90 ⁹⁵	90 ⁸⁰	90 ⁹	91 ¹	91 ³	91 ⁹
5.3	4.2	4.4	4.5	4.41	4.29	4.44	4.3	4.1	3.9	3.3
100	50	30	15	9.5	4.29	8.5	14	30	50	100
			C.L.	S		S	C.L.			

37+39.82 = w.L. 46th

89 ³	90 ⁴	90 ³	89 ⁹	90 ⁰²	90 ¹³	90 ⁰¹	90 ⁰	91 ⁰	91 ⁵	91 ⁹
5.9	4.8	4.9	5.3	5.22	5.11	5.23	5.2	4.0	3.7	3.3
100	50	30	15	9.5	5.11	8.5	14	30	50	100
			C.L.	S		S	C.L.			

37+00

88 ⁸	89 ⁶⁸	87 ⁹	87 ¹	87 ¹⁷	87 ⁸⁵	87 ⁷⁰	87 ⁶	88 ⁸	89 ⁴	88 ⁶
6.4	5.56	7.3	7.5	7.47	7.39	7.54	7.6	6.4	5.9	6.6
40	28.6	28.6	15	9.4	7.39	8.5	14	20	30	40
	Top		C.L.	S		S	C.L.			
	8" conc. wall									

36+95 = 28.6' Lt. = 4 Conc Steps thru wall

T.P. 8.76 95.24 0.12 86.48

88 ⁸⁶	88 ⁷²	88 ¹⁸
6.38	6.52	7.06
40	29.6	28.6
	Top =	Top of
	walk	bot. step
		95.24
		86.60

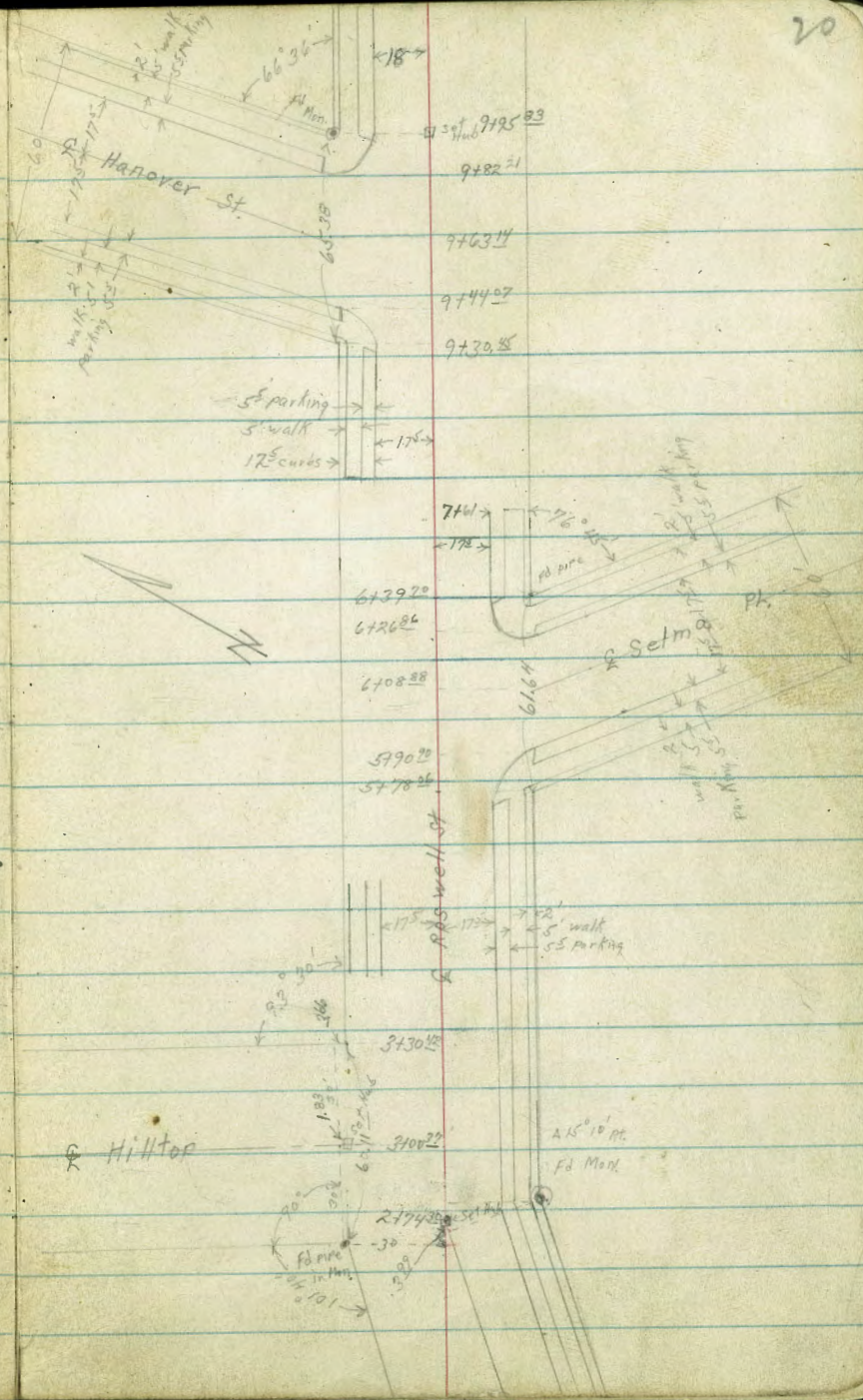
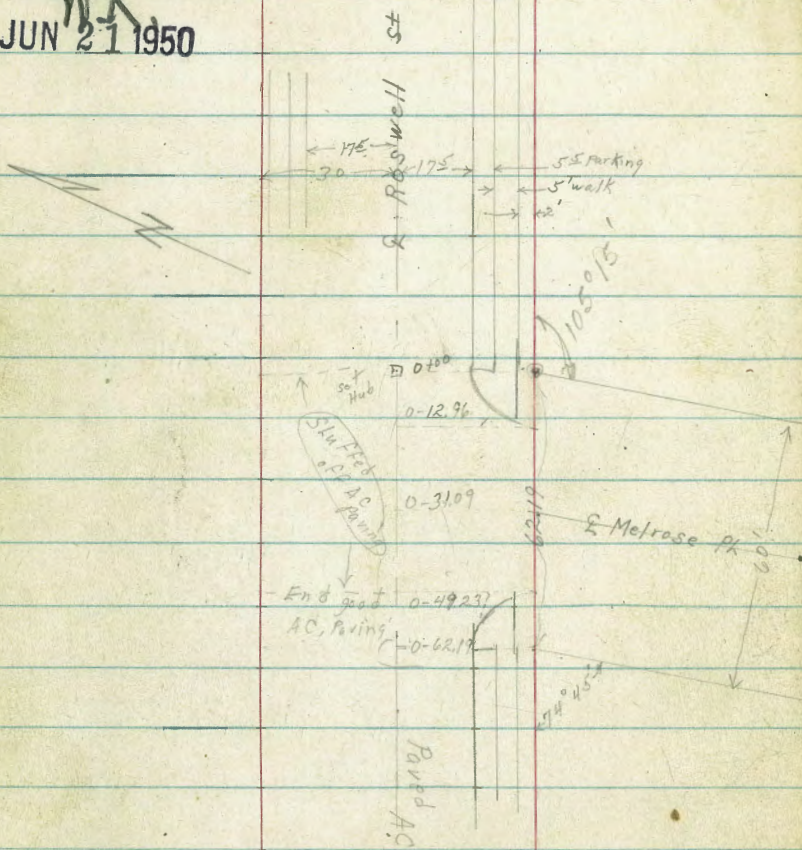
D. Smith.
E. Gregory
E. Sherman
G. Cota

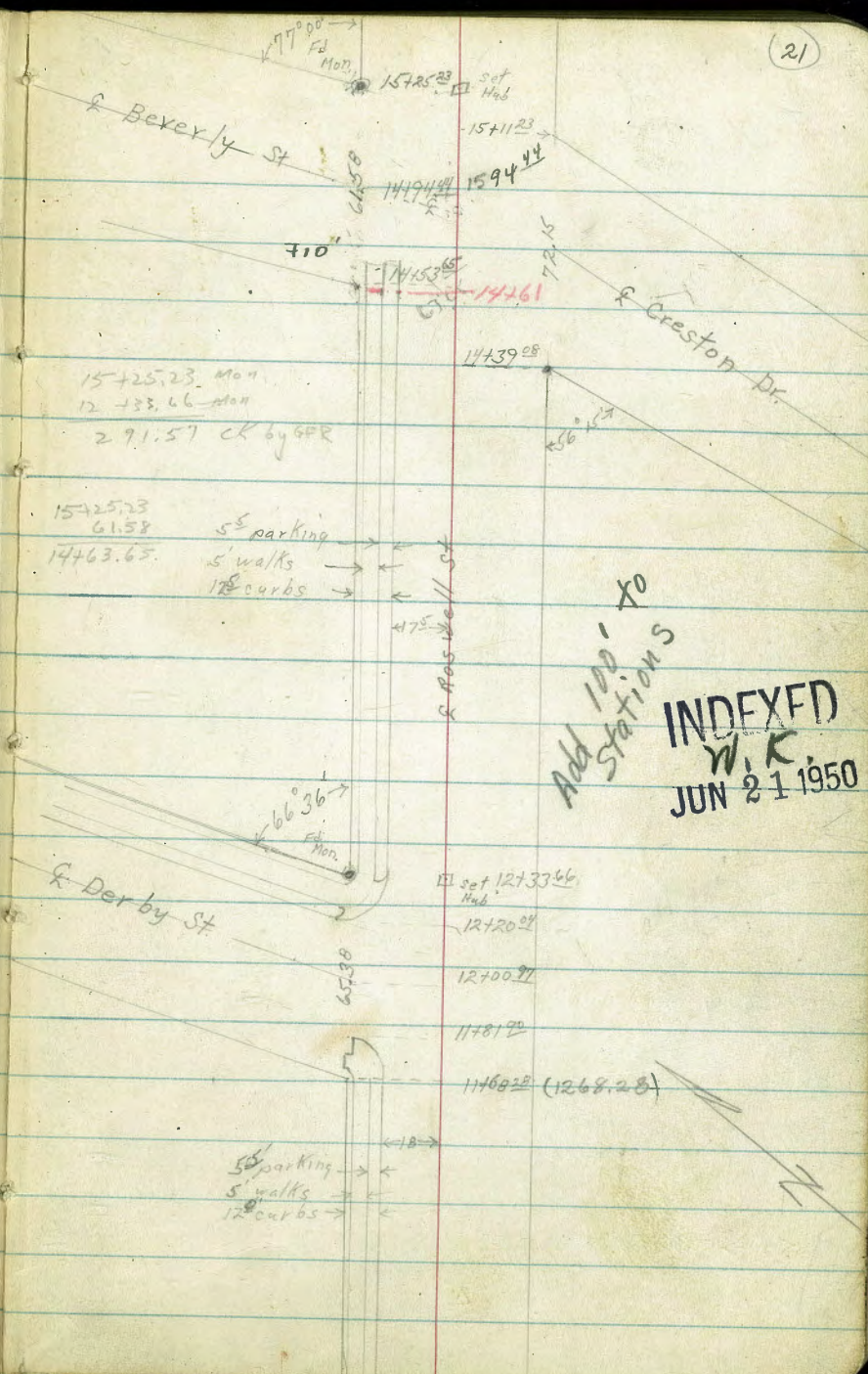
W.O. # 31502
6/2/50

Cross-Section Roswell St. Melrose Pl. to Beverly St.

INDEXED

JUN 21 1950





Add 100' to
 Stations 5
INDEXED
 W.K.
JUN 21 1950

D. Smith
E. Gregory
F. Sherman
G. Ota

X Sec Roswell St
Melrose H. to Beverly

6/2/50
wo# 31502

22

INDEXED
N.K.
JUN 21 1950

0+19 E 27⁵ E 2' con walk

0+04 19° Lt E 2" tree

0+00 East Prop Melrose End of Sluffed off AC paving

0-10 19° Lt E 3" tree

0-12.96 East Cb Line Melrose

0-18 19° Lt E 3" tree

0-31.09 E Melrose

Reduced
7-5-50
gmt.

0-49.23 West Cb Line Melrose End good AC paving

0-52 19° Lt E guy pole

0-62.19 West Prop Melrose

←→ Note: All grade breaks in Cbs are L breaks NO

B.M. 338 246 25 243 37 Roswell + Melrose
FB 1611-24

vertical curves!

North Lt

South Lt

242.23
452 450
30 275

242.21 242.25 241.5 241.8 242.2 243.21 243.37 243.4
44 47 53 50 45 34 32 34
30 18 15 175 175 23 30
347 746 walk

242.2 242.5 241.8 242.1 242.5 243.17 243.37 243.7
44 43 50 47 43 35 35 31
30 23 15 175 28 28 30
746 347
End

242.2 242.0 241.7 242.0 242.0 243.1
44 48 51 48 44 32
30 18 15 175 30

241.8 241.6 240.55 241.01 241.66 242.04 243.6 243.6
50 52 62 54 50 47 32 32
30 23 17 175 28 28 30
Edge AC Top of End

240.8 239.40 240.04 240.79 241.86 242.09 242.27 242.5
60 735 67 526 489 466 448 43
30 18 175 175 23 28 30
Edge AC 347 746 walk walk

246 25

1791 Lt End Cb + walk

240.3 No. 02 (7)
 34 334 338 365 38 35 32 319 33
 30 28 23 175 175 175 23 30
 walk walk cb gut gut walk

1782 Rt Begin broken out Cb

TP 13⁰⁵ 243³⁰ 647

NW Mon Prop Hilltop & Roswell

1750

240.31 240.19 240.00 239.7 243.36
 65 656 625 71 69 70 627 617 63
 30 23 175 175 175 175 23 30
 walk cb gut gut cb walk

1708 Rt & 12' con drive

240.65 240.77 240.02 240.3
 60 598 623 65 65 570 560 58
 30 23 175 175 175 23 30
 walk drive gut cb walk

1700 Lt & 10' con drive

240.9 241.01 241.02 240.77 240.1 240.4 240.4 241.28 241.31 241.2
 59 524 523 598 62 64 64 547 544 56
 30 28 23 175 175 175 175 23 30
 walk walk cb gut gut cb walk

0790 175 Lt Begin cb + walk

0751 192 Lt & 3" tree

0750

0746 192 Lt & 3" Oleander

0739 190 Lt & 2" tree

0731 192 Lt & 2" tree

241.1 241.2 240.8 241.0 241.1 242.08 242.29 242.3
 51 51 60 58 52 467 442 45
 30 18 15 175 175 23 30
 walk cb walk

246.75

3730⁴² East Prop Hilltop Dr Took Soil Sample

3727 RT. begin badly broken walk

3700³⁹ E Hilltop also End broken cb on Rt

2792 18^l Rt Northwly edge 18" Power Pole #976550

2791 RT begin broken out cb

-398 on line ahead to catch West Prop Hilltop
@ RT 10

2774³⁸ taken on split off

2730

1798 RT End of broken out cb

1795 20^l Lt & 5" tree

North 24

2389	2392	2372	2378	2378	2382	2376
45	51	52	56	62	53	58
30	19	17		175	175	30
				947	cb	

2388	2387	2385	2379	2394	2391	2388
45	42	42	55	45	43	46
30	175		175	175	23	30
			947	cb	walk	

2407	2397	2392	2392	2389	239.67	239.83
22	32	42	41	45	369	353
30	15	12		192	192	242
				947	cb	walk

2406	2391	2392	2388	239.67	239.80	2392
28	43	43	46	369	356	42
30	12		175	175	232	
			947	cb	walk	Prop

2399	2392	2395	2398	2394	239.81	240.06	2404
35	35	32	36	40	305	328	30
30	17	15		175	175	23	30
				947	cb	walk	

243 36

4782 RT & 15" Corrigated Storm Drain pipe in Cb

4775 21° Lt & 8" tree

4765 20° Lt & 5" tree

4750 Lt end Cb + walk

4743 RT End broken cb

4732 RT Begin broken out Cb.

4700 RT end broken up walk

3796 Lt & 10' con drive

3790 Lt Begin cb + walk

3750

North Lt

236.1	236.6	236.24	236.7	234.76	236.74	236.29	236.7	232.21
7°	6°	7°	6°	8°	7°	7°	7°	11°
30	19	17		17	17	23	30	11
				Fl.	cb	walk		Fl end Pipe

236.7	236.64	236.47	236.38	236.2	236.6	235.8	236.43	236.42	235.7
6.2	6.2	6.9	6.9	7.2	6.8	7.4	6.2	6.2	7.2
30	28	23	17	17	17	17	23	30	
	walk	walk	cb	sat		sat	cb	walk	
end	end	end							

237.2	237.00	236.96	236.5	236.9	236.1	236.79	236.82	236.93	236.5
6.2	6.30	6.40	6.2	6.5	7.2	6.57	6.57	6.43	6.2
30	23	17	17	17	17	17	23	28	30
	walk	cb	sat		sat	cb	walk	walk	

237.16	236.40
6.20	6.26
23	17

237.4	237.31	237.23	237.05	236.9	236.3	236.88	236.5
6.0	6.05	6.13	6.31	6.5	7.1	6.48	6.2
30	28	23	17	17	17	17	30
	walk	walk	cb	sat	sat	cb	
end	end	end					

238.9	238.3	237.9	237.3	237.4	236.9	237.66	237.1
15	5	5	6	6	6	5	6
30	27	19	17		17	17	30
					sat	cb	

24336

North Lt

South Rt

5 + 78⁰⁶ W Prop line Selma Pl.

2392	2387	2379	2383	2380	238.55	238.65	2382
82	84	92	88	94	85	84	84
30	19	15		175	175	23	30
				gat	cb	walk	

5 + 69 18⁵ Lt E guy pole #rove

5 + 37 Rt End Broken Cb.

236 ⁵¹	2371	2368	2372	2369	23753	23754	2371
102	102	103	99	102	953	952	100
30	20	17		175	175	23	30
				gat	cb	walk	

5 + 35

5 + 22 Rt Begin broken cb

234.25	235.58
128	1148
323	183
Front let	FL inlet

5 + 10 18³ Lt E 12" Corrugated Pipe Drain

5 + 08 21⁰ Lt E 7" tree

TP 547 247⁰⁶ 172 241⁵⁹

Pipe SE Prop cor Selma & Roswell

5400

247 ⁰⁶	247 ⁰⁶						
2265	2367	2364	2368	2361	236.65	236.73	23651
69	62	70	66	73	62	63	62
30	18	16		172	175	23	30
				gat	cb	walk	

4198 21⁰ Lt E 9" tree

243³⁶

North Lt

South Rt

TP 11⁰³ 255⁷⁷ 2³² 244⁷⁴

7+00

2422 2435 2425 2430 2428 2437 24385 2490 2442

44 36 45 42 43 335 321 306 24

30 19 15 175 175 23 28 30

9at cb walk walk

6+70

2418 2420 2414 2412 2415 24227 24241 2429

53 51 52 54 56 478 465 42

30 20 17 175 175 23 30

9at - cb walk

6+39²⁰ East Prop Selma

2402 2409 2403 2405 2403 24098 24117 2414

64 62 62 66 68 608 582 52

30 20 16 175 175 23 30

9at cb walk

6+26⁸⁶ East Cbline Selma

2402 2403 2396 2401 2399 2398 24083

62 68 75 70 72 73 623

30 19 15 175 30 30

9at cb

6+08⁸⁸ S Selma

2393 2396 2390 2393 2394 2392

78 75 81 78 72 74

30 19 16 175 30

5+90⁹⁰ W Cbline Selma

2388 2389 2385 2387 2383 2382 23865

83 82 86 84 88 88 84

30 19 17 175 30 30

9at cb

24706

9+00

8+90 Lt & 1/4th con drive

8+72 Lt Begin C6 + walk

8+35

8+60

7+61 Rt End C6 + walk

7+30

North	Lt					South	Rt
254.0	253.59	253.45	252.5	252.1	252.1	252.2	253.5
18	28	23	32	32	32	22	23
30	23	17	17	15	17	30	
	walk	cb	set				

252.98	252.22
27	35
23	17

252.6	252.15	252.12	251.93	251.0	250.9	250.6	251.6	251.9	252.7
32	36	35	38	48	42	53	42	32	35
30	28	23	17	17	14	17	28	30	
	walk	walk	cb	set					
	End	End	End						

250.3	250.0	249.0	249.3	249.1	249.2	250.4	251.3
55	58	62	65	62	59	54	45
30	19	16		17	18	28	30

248.5	248.2	247.1	247.5	247.5	248.4	248.3	249.8
73	75	82	83	83	74	75	60
30	20	15		17	19	27	30

245.9	246.2	245.3	245.5	245.6	246.77	247.02	247.04	247.5
92	96	105	103	103	90	87	87	83
30	18	15		17	17	23	28	30
					cb	walk	walk	
					End	End	End	

243.0	244.5	244.9	244.0	244.2	244.1	245.14	245.37	245.8
128	113	102	118	116	111	104	104	100
30	26	18	16		17	17	23	30
					set	cb	walk	

255.27

10+35

9+35 27° Rt & 2° con walk

(ORIGINAL STATIONS 100' SHORT)

9+95⁸³ East Prop line Hanover

9+82⁸¹ East C6 line Hanover

9+63¹⁴ & Hanover

TP 10° 265⁷⁴ 0° 254⁸²

9+44⁰⁷ West C6 line Hanover

9+41 20° Rt & power Pole # p 44561

9+30⁴⁵ West Prop Hanover Top soil sample &

North Lt

South Lt

29

258⁵ 258.46 258.35 257.9 258.1 259.50 259.52 259.58

72 72 73 80 78 76 62 62 66

30 23 18 18 14 27 30 40

walk cb sat onwalk onwalk onwalk

257.1 256.76 256.67 255.9 256.2 256.3 256.8 257.3

86 82 92 93 95 94 82 84

30 23 18 18 15 17 30

walk cb sat

256.42 255.5 255.4 255.7 255.5 256.4 256.0

93 10 10 10 10 9 9

30 30 17 14 18 30

cb sat

255.0 255.0 255.0 254.9 255.6 255.9

10 10 10 10 10 9

30 17 15 20 30

265⁷⁴

254.95 254.1 254.0 254.2 254.0 254.7 255.2

0 12 12 16 12 11 0

30 30 17 16 17 30

cb sat

255.0 254.9A 254.75 253.5 253.1 253.4 254.2 254.7

0 0 1 2 2 2 1 1

30 23 17 15 17 30

walk sat

255.27

1 12
X700

11
X094 292 RT E 8' con drive

11
X486 195 RT E Power Pole # P171127

TP 10 48 275 92 030 265 44

11
X760

11
X015 Lt End Broken Cb

10
X784 Lt Begin Broken Cb

10
X770

10
X768 Lt End Broken out Cb for dirt drive

10
X768 200 RT E Power Pole # JP 276334

10
X751 Lt Begin Broken out Cb for dirt drive

North Lt

266⁰
92 100 100 100 100
30 235 18 18
walk Cb 54

264¹ 264.12 264.02 263² 263⁴ 263² 263⁹ 263⁹
10 102 172 25 23 25 18 18
30 235 18 18
walk Cb 24

262¹ 262.12 262.04 261³ 261⁴ 261³ 262⁰ 262³
36 362 320 44 43 44 32 35
30 235 18 18
walk Cb 54

260⁰ 260.07 260.02 259⁴ 259⁵ 259⁷ 260⁴ 260²
52 567 522 63.6 60 53 55
30 235 18 18
walk Cb 94

265 74

30

South RT

265¹ 265³ 265⁹ 266²
100 100 100 92
12 18 30
266.23 266.29
962 963
292 40
drive drive
54

13
X+03 19^{RT} & Power Pole # JP 276335

13
X+00 27 & Derby St

12
X+87 27^{RT} & 3' con walk

12
X+81 20 Lt West Cbline Derby

12
X+68 3^{RT} Lt West Prop Derby St

12
X+56 30^{RT} & 8' con drive

12
X+40

12
X+24 26^{RT} & 3' con walk

12
X+24 Lt End broken Cb

12
X+09 Lt Begin broken Cb

2695
64
30
2692
62
175
2690
60
12
2689
70
15
2693
66
30
2693
66

269.01
62
269.01
62
26906
62
275
walk
end
30
40
walk
walk

2688
72
30
2688A
70
28
Cb
end
2686
73
28
94
2684
75
18
2684
75
13
2683
76
16
2689
70
30
2689
70

2690
62
30
2688
70
23
walk
2687
71
18
2687
81
18
94
2678
80
12
2679
81
14
2683
76
30
2685
74

2679
80
30
2677
82
23
walk
2676
82
18
Cb
2667
93
18
94
2669
90
14
2678
82
19
2672
82
30
2676
83

268.30
762
30
2
drive
end
268.32
760
40
drive
267.42
850
26
walk
end
267.43
849
30
walk
267.46
846
40
walk

14
13+60

14
13+31 Lt C6 grade break also walk

14
13+25 20° RT & Power Pole # P 171128
22° RT Begin 5' wire fence

14
13+09 18° RT & 8° con drive

14
13+00

13
13+70

13
13+33 66 Lt East Prop line Derby St.

13
13+20 04 Lt East C6 line Derby St.

32

North Lt				South RT			
2699	270.01	269.95	2688	2688	2682	2689	2694
60	52	62	74	74	72	70	65
30	23	173	173		12	14	22
	walk	cb	gut				30

2716	271.84	271.77	271.66	270.31	270.4	270.0	271.1	271.2
43	40	45	42	56	55	52	48	46
30	28	23	173	173		12	22	30
	walk	walk	cb	gut				

271.13
271.66
271.65

2718	271.59	271.52	270.8	271.0	271.0	271.1
44	43	40	54	42	42	42
30	23	173	173		13	30
	walk	cb	gut			

183 drive end
30 drive
40 drive

2715	271.27	271.6	270.6	270.6	270.6	271.2	271.4
44	45	42	53	53	53	42	45
30	23	173	173		12	16	30
	walk	cb	gut				

2709	270.77	270.71	270.0	2699	2698	270.4	270.2
52	51	52	52	60	64	55	53
30	23	173	173		12	17	30
	walk	cb	gut				

270.64	2698	2692	2695	2694	270.1	270.4
52	64	62	64	65	53	55
30	30	173		12	17	30
cb	gut					

275.92

529 270 65 NETrop 110 Derby & Roswell 270 FB 16/2-11

16
X5725²³ Lt East Prop Beverly

16
X5711²³ Rt East Prop Creston

5
X494⁴⁴ E Beverly

15763.65 P.L. cKed from Sta X2133.66

15
X461 175 Lt End C6 + walk ← This is OK.

15
X453⁶⁵ Lt West Prop Beverly

1563⁶⁵
Part line
N.G.

15
X4739⁶⁸ 28 RT End 5' wire fence Took soil sample

15
X4739⁶⁸ Rt West Prop Creston Dr

T.P. 6⁶⁰ 271⁶⁰ 10⁹⁸ 265⁰⁰

15
X4700

742 263.72
263.72
263.72
263.72

North 14
264.6 263.6 263.2 262.7 262.4 262.6 261.3
70 80 84 87 92 90 103
30 17 15 11 25 30

264.4 263.7 263.4 262.9 262.5 262.2 262.4
72 72 82 87 91 82 92
30 17 15 11 14 30

264.4 263.8 263.1 262.6 263.1 262.4
74 78 85 90 85 92
30 17 11 14 30

264.57 264.40 264.30 264.0
73 72 73 76
30 23 17 17
walk 2nd 2nd 94

265.3 264.90 264.75 264.2 263.9 263.5 263.8 263.4
63 62 68 74 72 82 78 83
30 23 17 17
walk 2nd 2nd 94

266.0 265.48 265.31 264.4 264.3 263.9 264.3 263.9
59 61 62 72 73 71 73 72
30 23 17 17 11 17 30
walk 2nd 94

267.6 267.57 267.38 271.00 266.1 266.1 265.4 266.1 266.5
83 83 84 98 98 105 98 94
30 23 17 17 12 13 30
walk 2nd 94

275.92

End cb not prop

268.6
72
268.4
74
268.2
76
268.0
78
268.0
94
269.8
60
270.1
52
270.0
58
270.0
94

268.84
70
268.84
70
268.79
70
268.75
70
270.65
512
270.67
512
270.69
512
270.72
512

BC Roswell

10' Rad

18° Length 3 parts 6° ea

NW Return Roswell + Derby

EC, Derby

2/3

1/3

BC Roswell

10' Rad

20 length 3 parts 6° ea

NE Return Roswell + Derby

BM

5.19

275.84

270.65

NE Prop Mon
Derby + Roswell
page 32

EC, Hanover

2/3

1/3

BC Roswell

10' Rad

15° Length 3 parts 5° ea

NW Return Roswell + Hanover

EC, Hanover

2/3

1/3

BC, Roswell

10' Rad

17 1/2 Length 3 parts 5 1/2 ea

NE Return Roswell + Hanover

BM

5.64

262.31

NE Prop Mon
Hanover + Roswell
page 29

253.9
84
253.9
84
253.2
86
253.4
82
255.5
60
255.5
60
255.7
66
255.8
65

254.82
74
254.80
75
254.76
75
254.72
75
256.40
59
256.42
59
256.39
59
256.45
58

EC, Selma

238.31

62

6⁴⁰

238.58

End Cb Melrose not prop

243.1

32

4²⁸

242.04

2/3

238.21

68

6⁴¹

238.57

2/3

242.3

42

4²⁴

242.08

1/3

238.1

62

6⁴³

238.55

1/3

242.1

42

4²⁵

242.07

BC Roswell

238.0

70

6⁴⁴

238.54

BC Roswell

241.04

5²⁸

5⁰³

241.99

10' Rad 19⁴ length 3 parts 6⁴ ea

10' Rad 17⁰ length 3 parts 5¹ ea

SW Return Roswell + Selma Pl

SW Return Roswell + Melrose

EC, Selma

239.9

51

4¹⁹

240.79

End Cb Melrose not prop.

243.1

32

3²⁶

243.16

2/3

239.9

51

4²¹

240.77

2/3

242.2

42

3²¹

243.21

1/3

240.1

42

4²⁰

240.78

1/3

242.3

42

3²¹

243.21

BC, Roswell

240.2

48

4¹²

240.81

BC, Roswell

242.1

42

3²⁰

243.22

10' Rad 15² length 3 parts 5³ ea

10' Rad 19⁰ length 3 parts 6³ ea

SE Return Roswell + Selma Pl

SE Return Roswell + Melrose

BM

339

244.98

241.59

SE Proppine Roswell + Selma page 24

BM

365

247.02

243.37

SE Proppine Roswell + Melrose page 22

D. Smith
E. Sherman
G. Cota

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JUN 21 1950

Cross Sec. Hilltop Dr. Roswell to Winston Dr

1725 17⁶ Lt & Power Pole #P76551

1700 302 Rt Begin 3' Picket fence

0+80

0+40

0+0183 Lt - N.W. Prop Cor Roswell

0+00

0-D/83 Rt = NE Prop Cor Roswell

BM

511

245⁹⁹

240²⁸

NW Prop Mo
Hilltop
Roswell
page 23

245³⁹

West Lt

Wo# 31502

37

6-20-50

East Rt.

240 ⁰	240 ¹	239 ²	239 ¹	240 ⁵
54	53	55	52	48
30	12		15	30

240 ⁵	240 ²	240 ⁰	239 ⁸	240 ²
42	52	54	56	52
30	12		15	30

240 ⁹	240 ¹	239 ⁸	239 ¹	240 ³
45	53	56	63	54
30	12		15	30

240 ⁶	239 ¹	238 ⁷	238 ²	239 ²
48	63	62	72	62
30	18		18	30

240 ⁵	239 ⁰	238 ⁶	238 ¹	239 ⁹
42	62	62	73	65
30	18		18	30

2760 24⁵ Lt Begin con brick wall

2730

2700

1798 32² Rt Begin 6' wire fence

1785 27² Lt Northernly double garage con floor + apron

1765 27² Lt Southernly double garage con floor + apron

1750

174

1747 36⁰ Lt E 2⁵ con walk

1735 30⁰ Rt End Picket fence

West
 232.8 232.3 233.74 234.4 235.2 235.7 235.9 237.7 239.2
 12⁸ 13² 11⁶⁵ 11⁰ 10³ 10³ 10⁰ 8² 7²
 30 24⁵ 24⁵ 24⁵ 15 18 30 30

232.2 234.9 236.2 236.6 237.0 236.9 238.5
 13² 10⁵ 9³ 8² 8⁴ 8⁵ 6²
 50 30 27 15 18 30

233.9 236.9 237.5 237.6 238.1 239.1 239.8
 11⁵ 8⁵ 7² 7³ 7³ 7³ 5⁶
 50 50 27 15 15 30

237.48 237.97
 7² 7⁴²

45¹ 27²
 Floor apron
 237.59 237.99
 7⁸⁰ 7⁴¹

45¹ 27²
 Floor apron
 237.57 238.34 238.3 239.2 239.3 239.1 240.4
 7⁸⁷ 7⁰⁵ 7¹ 6³ 6¹ 6³ 5⁰
 40 30 15 15 30
 end walk

245³⁹

West Lt East Rt

TP 0³⁷ 224¹⁶ 11⁵⁴ 223⁷⁹

3+75

224 2229 2240 2238 2238 2243 2243 2234
 13° 125 114 116 116 114 114 120
 50 30 19 5 15 30 50

3+60

2241 2262 2273 2273 2274 2276 2283 2279 2273
 113 92 72 81 80 78 71 75 81
 50 30 21 5 13 23 30 50

3+25

2234 2280 2298 2307 2307 2307 2307 2323 2324
 120 74 56 42 54 52 42 34 30
 50 30 23 12 5 15 30 30

3+18 124 Lt & dead man gay wire

2272 2310 2316 23914 2314 2326 2327 2337 2340 2347
 82 44 38 132 40 28 7 12 14 13
 50 30 27 242 242 12 18 30 50
 Top Footing
 All over

3+00 Took Soil Sample &

2+97⁵⁵ EC 245 Lt & 2' x 2' con pillar

2+94 143 Lt & Power Pole # P 76552

23914 2317 23420
 +394 37 123
 242 242 245
 Footing Footing Topwall
 2167

2+82 24⁶ Lt & 2' x 2' con Pillar also End con + brick wall

2+73 32³ Rt End 6' wire fence

TP 1⁸⁸ 235⁴³ 11⁸⁴ 233⁵⁵

235⁴³

18420 W. 1/2 Sec 10
S. 1/4 167-39

West Lt

East RL

40

TP 0¹⁹ 212¹⁹ 12¹⁶ 212⁰⁰

4765 24° Lt Begin concrete block wall in bldg process

4765 10° Lt Begin floral planting

4758 Lt & single garage concrete floor + apron

4757⁰² EC 22° Lt & Power Pole # 173923

4725

4720 20° Lt & dead man wire guy

4700

2119
 Now 123
 242
 Footings only
 215.44 215.29 215.1 213.2 212.7
 822 888 92 102 115
 465 32 28 18 11
 floor edge apron cold lay
 215.5 214.5 213.0 213.3 213.2 213.3 212.7 210.4
 82 92 112 102 110 102 115 138
 50 30 11 6 10 30 50
 218.1 217.3 217.2 215.2 216.1 216.5 215.9 214.9
 62 62 70 85 82 72 83 93
 50 30 24 10 10 30 50
 2190 2199 2203 2195 2198 2203 2199 2195
 52 42 32 42 44 32 43 42
 50 30 18 5 14 30 50
 221.16
 223.77

6+08³⁸ E Winston to East

SE
6+00⁴⁸ (SW) Prop Cor Winston

NE
5+75⁰¹ (SE) Prop Cor Winston

5+50

TP 0²⁹ 20/08 11⁴⁰ 200²²

5+25

5+05 24⁵ at end con block wall in bldg process now

5+00 10' at End floral planting

West Lt & East Pt 41

1885 1885 1892 1892 1898
12⁶ 12⁶ 11⁴ 11⁴ 12³
30 15 15 30

1908 1898 1893 1903 1902 1996
10³ 11³ 11⁸ 10⁸ 10² 11⁵
30 25 15 15 30

1944 1941 1941 1929 1927 1902 1918
6² 7⁰ 7⁰ 8³ 8⁴ 10² 10¹
50 30 15 15 24 30

1999 1985 1971 1965 1963 1969 1973 1964
1² 2⁶ 4⁰ 4⁶ 4⁸ 4³ 3⁸ 4²
50 30 14 14 17 30 50

2017
45
24⁵
Footings
2044 2032 2028 2006 2008 2015 2012 2000
7⁸ 9⁰ 10² 11⁶ 11⁴ 10² 11⁰ 12²
50 30 12 12 14 30 50

2106 2097 2090 2055 2054 2055 2061 2058 2037
16 25 32 62 6⁸ 6² 6¹ 6⁴ 8⁵
50 30 20 5 10 12 30 50

21212

11²² 235⁰³ 00⁸ 223⁸¹
 TP 11⁸³ 223⁸⁵ 03⁵ 212⁰²
 TP 11⁵⁶ 212³⁷ 05² 200⁸¹
 TP 11⁸⁴ 201³⁸ 2⁴⁹ 189⁵⁴

BM 9³⁵ 182⁶⁵ NW Prop. Map.
 Winston + Hilltop
 (184²⁵) FB 11/17-22
 NE

BM

TP

West Lt East Rt 42

3⁶³ 240³¹ Start BM
(240²⁵)

146 233⁵⁷

6764²⁵ 2² Lt & Power Pole

6764²⁵ N.W. Prop Cor Winston

6756 5' Rt & anchor dead man

6753²⁵

6741²⁶ NE Prop Cor Winston

6737 Guard Rail 3' Lt 13' Rt

6732⁶² & Winston to West

TP 2⁴⁹ 192⁰³ 11⁵⁴ 189⁵⁴

182⁸ 182² 181⁸ 181² 181⁴
 9² 9⁸ 10² 10² 10⁶
 30 12 15 30

184⁶
74

185³ 186² 186⁹ 187³ 187² 184¹
 6² 5⁸ 5¹ 4² 4⁸ 7⁸
 30 25 15 16 30

185⁸ 187⁴ 188¹ 188² 188⁰ 187¹
 6² 4⁶ 3² 3² 4⁰ 4²
 30 23 15 22 30

192⁰³

Locations Existing Curb/Inlets
at 5356 Wilshire Drive

NO 20766

Location House Lot I & J

Sub Map # 1879

Walker
Pope
R. Sisson
1-18-51

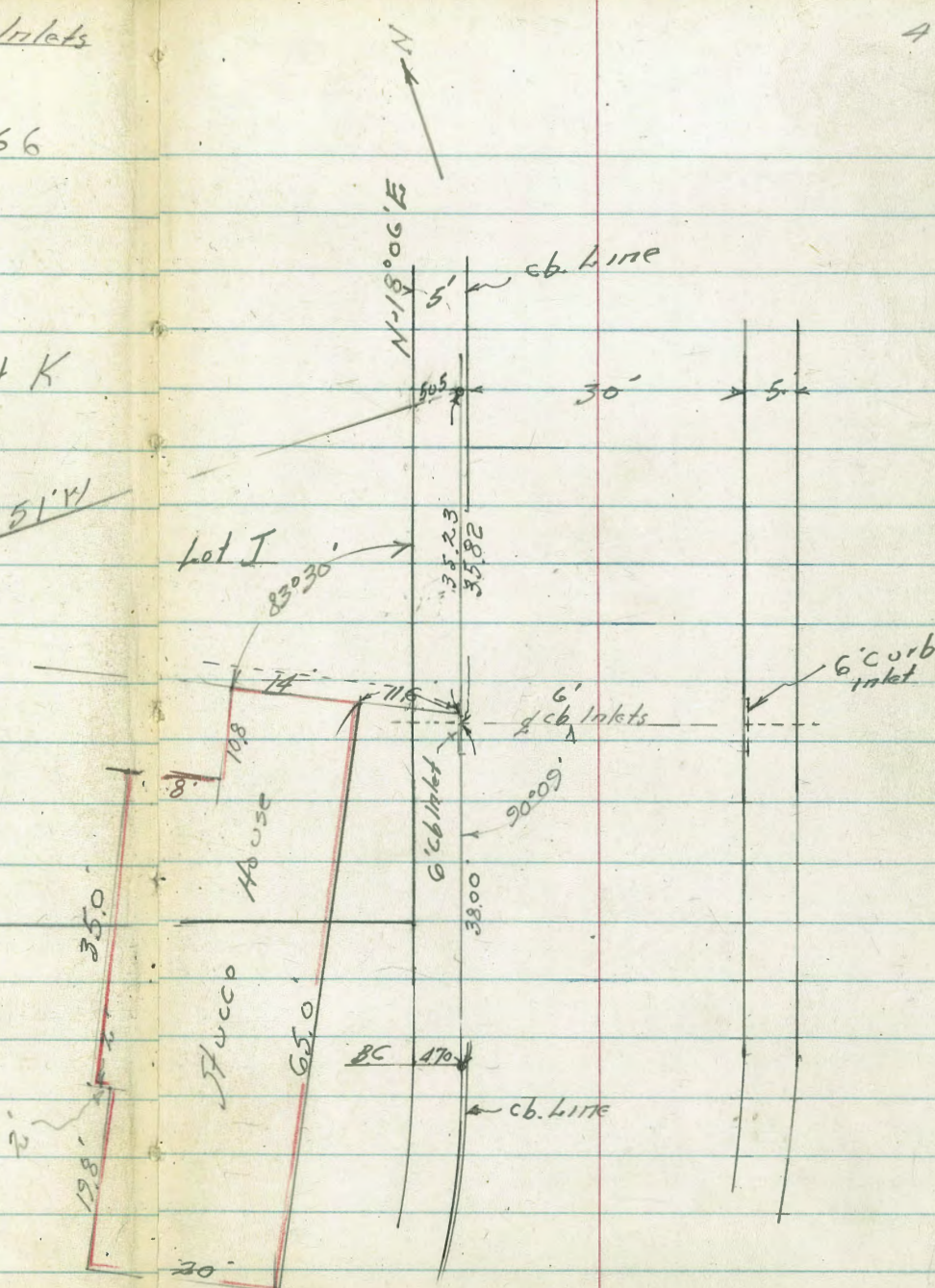
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JAN 19 1951

Note: Grades for Drain
Grade Book 27K
56

Lot K

Lot J

Lot I



Alaqa St.
Venice to Catalina
X-sec. for Imp.

Sommermeyer
Begg
Bunch
Bruner

○ = Fd. Lt.

● = Fd. Pipe

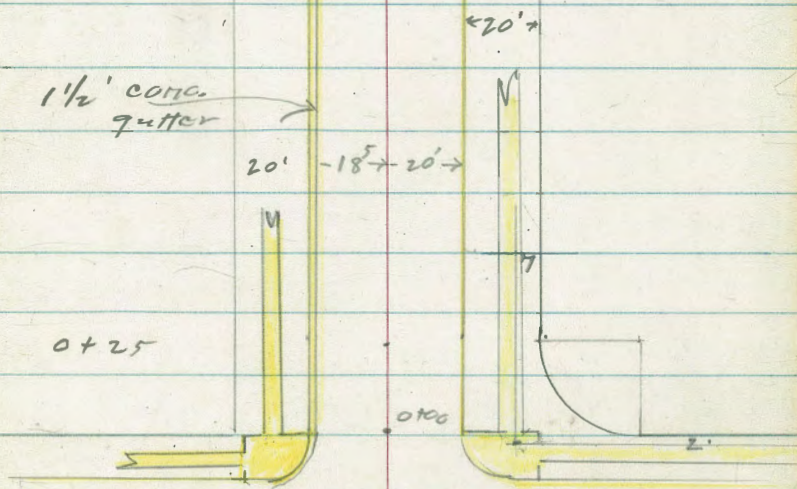
Soil sample taken.

Reduced by
C.R. Washhead
2-26-51

2-21-51
W.O. 31872

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MAY 28 1951

44

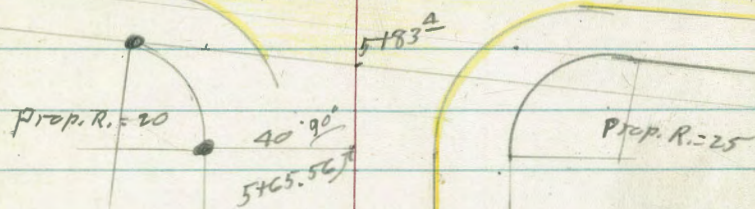


Venice St.
Unimproved St.

Niagara St.

45

Catalina - Conc. Pave.



4+42.5

15' Alley

Niagara

1+00	214.78	214.10	214.7	214.14	215.1	214.9	214.9	214.7	214.66
	6.81	7.44	6.8	7.40	6.4	6.6	6.6	6.8	6.88
	20	20	20	185	10	10	20	20	20
	cl.	G	Gnd	E.G.					cl.
0+75	215.53	214.91	215.6	214.92	216.0	215.9	215.6	215.3	215.30
	6.01	6.63	5.9	6.62	5.5	5.6	5.9	6.24	6.24
	20	20	20	185	3		10	20	20
	cl.	G	Gnd	EG					cl.
0+50	216.37	216.4	215.74	215.73	216.4	216.4	216.3	215.8	215.91
	5.17	5.1	5.80	5.81	5.1	5.1	5.2	5.7	5.63
	20	20	20	185	10		10	20	20
	cl.	Gnd.	G	EG.					cl.
0+25 = Prop. B.C. on south.	217.19	217.1	216.55	216.60	217.3	216.9	216.7	216.3	216.57
ch. = top of curb	4.35	4.4	4.99	4.94	4.2	4.6	4.8	5.2	4.97
G. = gutter at curb.	20	20	20	182	10		10	20	20
E.G. = outside edge 15' wide Conc. gutter	cl.	Gnd.	G	EG.					cl.
0+00 = Ely in Venice to North	218.18	217.8	217.53	217.55	217.7	217.5	217.0	216.7	217.24
for intersection & ch. Ret.	3.36	3.7	4.01	3.99	3.8	4.0	4.5	4.8	4.30
	20	20	20	185	10		13	20	20
	cl.	Gnd.	G	EG.					cl.

See Venice St. Proposed Imp. plans

221.54 ✓

3.82

221.54 ✓

217.72

S.W.B.P. Niagara + Venice

Niagara

T.P. 0.57 199.99 ✓ 13.09 199.42 ✓

2+20

1+90

1+70

1+65 21' Lt = dead man

(street side)

1+50^s - 20^a Lt = Face of pole # 4262

1.79 212.51 ✓ 10.82 210.72 ✓

32^s Lt = end back of walk.

27^a Lt = end conc walk

1+50 } 20' Lt = end conc. curb.

1+20

211.5	208.7	201.2	200.8	200.5	200.4	200.5	201.27
1.0	3.8	11.3	11.7	12.0	12.1	12.0	11.24
30	40	30	10	10	10	20	cc.
211.2	208.2	207.0	206.7	206.5	206.7	206.7	207.01
1.3	4.3	5.5	5.8	6.2	5.8	5.8	5.99
40	34	10	10	10	20	20	20
cc.							cc.
214.5	213.5	210.8	210.4	209.7	209.4	209.9	210.07
+2.0	+1.0	1.7	2.1	2.8	3.1	2.6	2.44
30	40	35	20	7	20	20	20
cc.							cc.
				212.51 ✓			
				215.6			
5.9	9.18	9.25					
40	32 ^s	27 ^a					
	walk	walk					
	+ 8						
211.94	211.35	211.40	211.8	212.4	212.0	211.8	212.58
7.60	10.19	10.14	9.7	9.1	9.5	9.7	9.16
20	20	18 ^s	18 ^s	12	10	20	20
cc.	G	E.G.					cc.
214.07	213.43	213.45	213.4	214.3	214.2	213.6	214.11
7.47	8.11	8.09	8.1	7.2	7.3	7.9	7.43
20	20	18 ^s	18 ^s	10	10	20	20
cc.	G	E.G.	Ord				cc.
				221.54 ✓			

Niagara

3+80

176.4	174.1	173.1	172.1	172.2	172.2	172.0	172.58
$\frac{5.0}{40}$	$\frac{7.3}{34}$	$\frac{8.3}{20}$	$\frac{9.3}{7}$	9.2	9.2	9.4	$\frac{8.83}{20}$
							cc

3+70

172.77	172.57
$\frac{7.64}{20}$	
cc	

3+50

180.6	177.4	176.5	175.9	176.2	176.1	175.8	176.57
$\frac{0.8}{40}$	$\frac{4.0}{32}$	$\frac{4.9}{10}$	$\frac{5.5}{7}$	5.2	$\frac{5.3}{10}$	$\frac{5.6}{20}$	$\frac{4.82}{20}$
							cc

3+49

176.74	176.57
$\frac{4.67}{20}$	
cc	

3+30

182.7	180.8	179.7	179.3	179.4	179.4	179.4	180.04
$\frac{+1.3}{40}$	$\frac{0.6}{32}$	$\frac{1.7}{15}$	2.1	2.0	2.0	2.0	$\frac{1.37}{20}$
							cc

T.P. on dist
33' RT of
3+43

3.81

181.41

9.92

177.60

181.41

3+00

190.3	185.1	184.9	184.7	184.7	185.2	185.71
$\frac{+2.8}{40}$	$\frac{2.9}{33}$	$\frac{2.6}{10}$	2.8	$\frac{2.8}{10}$	$\frac{2.3}{20}$	$\frac{1.75}{20}$
						cc

0.42

187.52

12.89

187.10

187.52

2+52 - 20' RT = crack thru curb

199.4	199.1	194.9	195.0	194.6	194.7	194.8	195.44
$\frac{0.6}{50}$	$\frac{0.9}{40}$	$\frac{5.1}{30}$	$\frac{5.0}{10}$	5.4	$\frac{5.3}{10}$	$\frac{5.2}{20}$	$\frac{4.55}{20}$
							cc

2+50 20' RT = crack thru curb

199.99

Niagara

A+70

165.0	164.7	163.8	162.3	162.1	162.2	162.7	163.5
3.8	4.1	5.0	6.5	6.7	6.6	6.1	5.32
40	20	13	11		10	20	20
							80

A+53 - 20' Rt. = E.C. 3' Rad. ^{110'} cl. Ret

169.6	169.2	168.8	164.9	164.5	164.7	165.0	165.9	165.8	166.7
0.2	10.4	0.0	3.9	4.3	4.1	3.8	2.88	3.0	2.06
40	30	24	8		10	20	23	40	40
							80	80	80

40' Rt. = curb end - alley cl.
 A+50 - 23' Rt. = B.C. 3' Rad. alley cl. Ret.

40' Rt. = end cl.
 A+35 - 23' Rt. = E.C. alley cl. Ret.

170.6	169.4	168.4	166.3	166.3	166.7	167.28	166.4	167.23
11.8	10.6	2.4	2.5	2.5	2.1	1.55	2.2	1.60
40	19	8		10	20	23	40	40
						80	80	80

A+32 20' Rt. = B.C. 3' Rad. Alley cl. Ret.

1.34
20
cl. B.C.

T.P. 0.66 168.83 13.24 168.17

168.83

A+00

172.5	171.7	169.9	170.0	170.1	169.9	170.56
8.9	9.7	11.5	11.4	11.3	11.5	10.85
40	20	8		10	20	20
						80

181.41

Niagara

5+83⁴ = start Pave

197.1	147.9	147.0	147.28
$\frac{5.0}{40}$	$\frac{4.2}{30}$	$\frac{5.1}{20}$	4.79

5+79² 32^s Rt = start Pave.

147.5	148.2	148.1	147.7	148.2	148.3	148.29	149.22
$\frac{4.6}{40}$	$\frac{3.9}{30}$	$\frac{4.0}{13}$	4.4	$\frac{3.9}{10}$	$\frac{3.8}{20}$	$\frac{3.78}{32^s}$	$\frac{2.85}{32^s}$
			152.07 ✓				
				pave			
				cc			

T.P. 3.19 152.07 8.70 148.88 ✓

5+65⁸⁶ 20' Lt = Prop. B.C. Lt.

148.9	150.8	149.6	150.0	150.0	151.06
$\frac{8.7}{40}$	$\frac{6.8}{15}$	8.0	$\frac{7.6}{10}$	$\frac{7.6}{23}$	$\frac{6.52}{23}$
Top. ch.					

5+50 - 20' Rt = B.C. Ch. Ret.

152.93
4.65
20
cc. B.C.

5+48⁸⁶ - 40' Rt = Prop. B.C. Rt.

149.9	152.3	152.1	152.1	152.3	153.03
$\frac{7.7}{40}$	$\frac{5.3}{8}$	5.5	$\frac{5.5}{10}$	$\frac{5.3}{20}$	$\frac{4.52}{20}$
cc					

T.P. 1.00 157.58 12.25 156.58 ✓

157.58

5+00

157.4	158.2	157.7	158.3	158.5	158.9	159.57
$\frac{11.4}{40}$	$\frac{10.6}{14}$	$\frac{11.1}{10}$	10.5	$\frac{10.3}{10}$	$\frac{9.9}{20}$	$\frac{9.26}{20}$
						cc
						168.83 ✓

0.26 $\frac{+ 0.02}{157.50}$ (157.52)

N.E.B.P. Narragansett & Catalina

T.P. 7.58 157.76 1.89 150.18

€ Catalina

139.23	141.12	143.06	144.53	145.72	146.97	148.39
12.84	10.95	9.01	7.54	6.35	5.10	3.68
150	90	40		40	90	140

55' Lt. = E.C. 35' Rad. cl. Ret.
 65' Rt. = E.C. cl. Ret. Aprox. 35' cl. Rad

141.59	141.02	143.51	147.42	148.12	148.72
10.49	11.05	8.56	4.65	3.95	3.35
105	105	55	65	115	115
cl.	G	E.C. cl. Ret.	E.C. cl. Ret.	G	cl.

A.C. Pavement

section Along cl. Liria - Catalina
on € Niagara5797² = Wly. cl. Liria Catalina

142.95	143.85	144.71	145.40	146.17	146.61	146.86
7.12	8.22	7.36	6.67	5.90	5.46	5.21
55	40	20		20	40	65
G						G

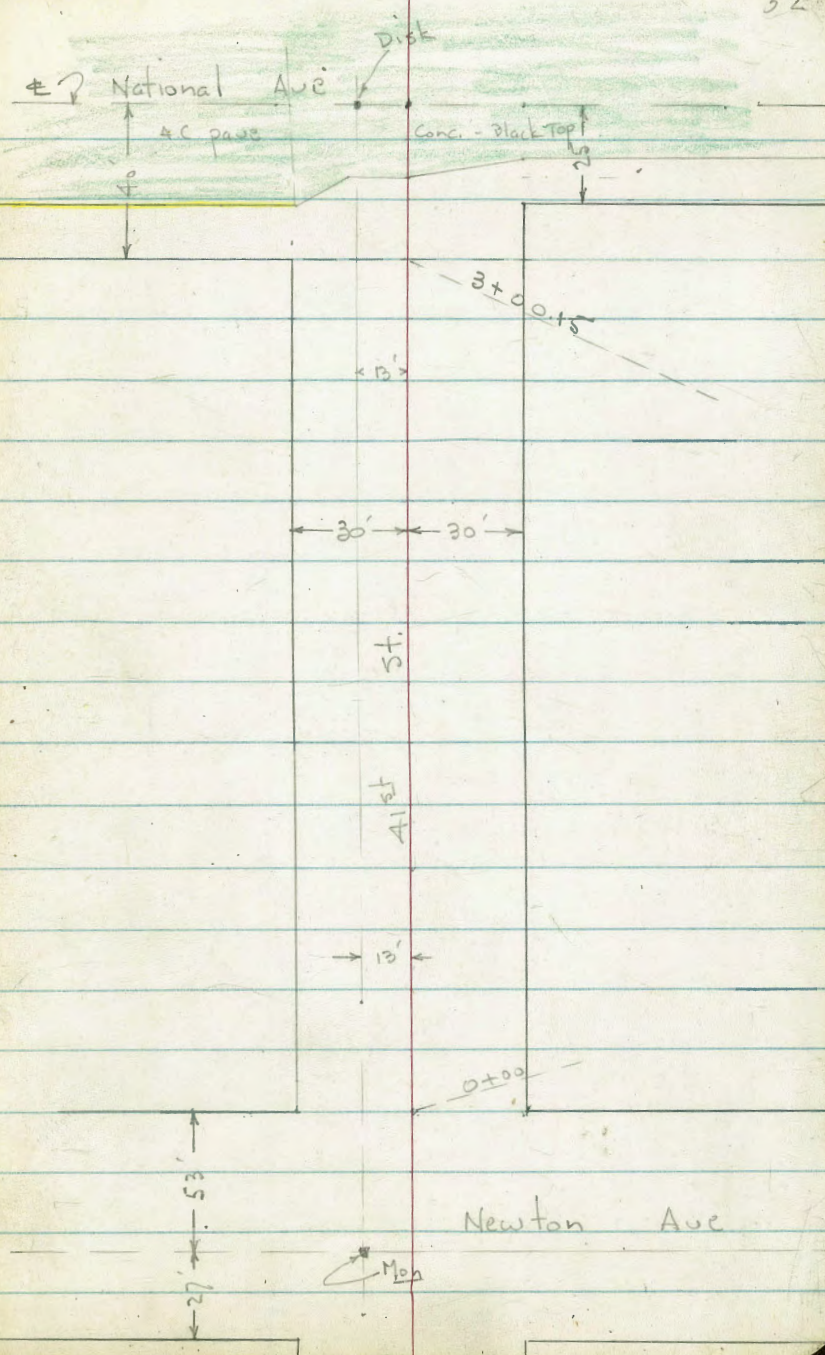
5786¹ - 37' Lt. = Nly cor walk.

146.6	146.85
5.5	5.22
40	37
Encl	walk + Encl

5786 26¹ Lt. = start. cl. + Pave

146.81	146.27	146.8
5.26	5.80	5.3
26 ¹	26 ¹	26 ¹
cl.	Pave	Encl

152.07



87.2
40
127.2

No adjusting of miles necessary.
self-reading Rod

INDEXED

MAY 31 1951

53

X-Section 41st St. from Newton to

Lt

#

Rt

National - for Grade Est. - 60' st. - Not graded

5325 5-31-51 7.0.

W.O. 25020 - See Book 2126-P. 6 - National to E.

2+00

26.2 26.4 26.1 25.9 26.1
40 30 30 40

1+50 - 0.5' Lt. = Sewer M.H.

25.9 26.35 25.7
30 on Rim
MH 30

1+41.4 = fence - 2.2' Rt. + 34' Lt. = Corners

1+27.2 - 33.9' Lt. = Cor. Bldg.

1+00

25.8 26.0 26.0 25.7 25.8
33.9 30 30 40
at Bldg.

33.9' Lt. = end at Cor. of gal. Iron Bldg.

0+87.2 = 6 Board fence - 22' Rt. = Cor.

26.41
33.9
conc. floor

0+50 25.7 25.9 25.7
30 30

0+00 = N.L. Newton

25.5 25.4 25.7 25.2 25.1
40 30 30 40

See X-Section of Newton

0+40 = Newton - Dirt Rough Graded

25.9 25.6 25.5 25.3 25.7 25.9 26.3
90 30 20 20 30 90

Note: Used Elev. Rod. Actual Elev. shown.

B.M.

35.75 = N.W. B.P. National + 41st

Lt.

±

Rt.

3+40.15 = ± Both ways

36.81
8034.55
30

33.40

32.27
30

2+21 = Edge A.C. Pavc at ±

34.12
5033.25
3032.79
15.5
diag. edge

32.37

31.4
3030.6
50
Dirt. 4's. of edge

3+14.15 = S. cb. to W. - 1/2 S. of S.L. to E.

35.08

35.45
8032.72
3033.11
30

32.67

33.09
28.4 =

32.2

31.6
3030.9
50

got

Top

got

Top

got

end cb. Top

3+00.15 = S.L. of National to west.

28.1
4028.7
30

28.5

27.6
3027.6
40

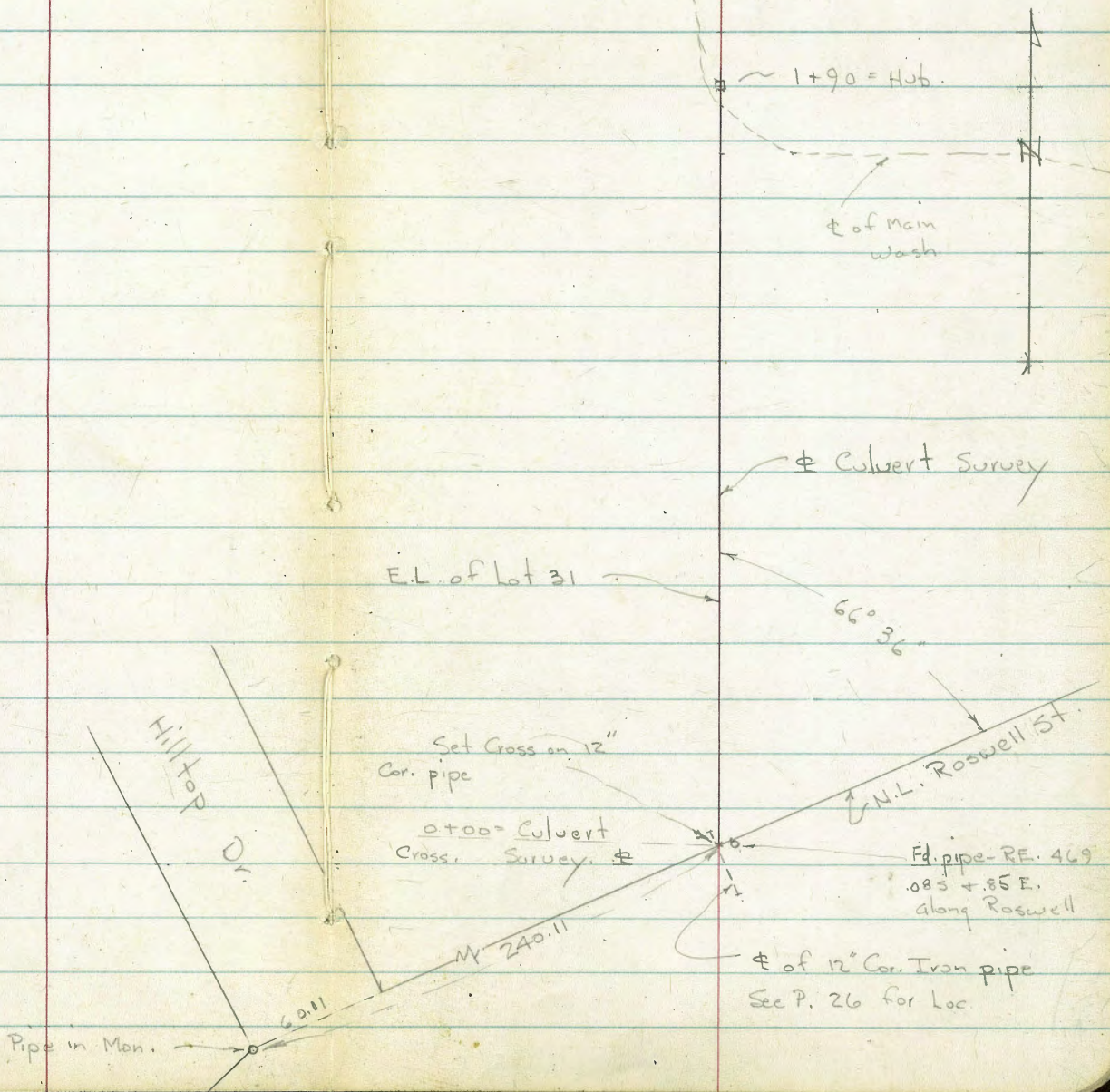
2+50

27.0
30

26.9

26.5
30

INDEXED
law
OCT 22 1951



Indexed

Levels along \pm of Prop. Culvert along
Lot Line Bet lots 31+32 - Blk. 12

Beverly - Map 1129

5638 10-1-51 - 7.0

w.o. 20861 - sketch - P. 55

0+65

T.P. 0.33 229.43 12.74 229.10

0+38- 8.4 Lt. = \pm 4" Quava

0+35

0+26- 7 Lt. = \pm 4" Quava

0+15- 4.4 Lt. = \pm 4" Quava Tree

0+05 = \pm Exist Water way - noted as ditch

0+02- 0.7 Lt. = outlet \pm 12" C.I. pipe

0+00 = Cross on Top of 12" C.I. pipe on N.L.
Roswell

B.M. 0.25 241.84 241.59 = S.E. Pipe - Schmat Roswell 241.84

P. 20

50

Lt. \pm Rt.

226.7

2.7
10

226.1

3.3
10

224.5

4.9
10

226.2

3.2
20

229.43

Ditch

231.0

10.8
10

231.8

10.6
6

231.0

10.8
6

230.6

11.2
15

\pm Ditch

233.8

8.0

234.25

7.59 = I.E. pipe

235.54

0.30

on Cross

Lt.

±

Rt.

See Lath
B.M. = Nail in Post.

1321 204.89

1+90 = Hub.

8.64 197.56 on Hub.

1+85 = ± of Main Wash - See sketch

200.9
5.9
10
197.8
8.4
199.7
6.5
10

1+70

T.P. 1.12 206.20 11.97 205.08

203.6
2.6
10
200.7
5.5
206.20
199.5
6.9
5
199.6
6.6
19
± Ditch
199.5
6.7
20
± wash
to E.

1+45 - Brush - Both Sides

209.3
7.7
10
207.6
9.4
214.4
12.6
5
± Ditch
1206.5
10.5
15

T.P. 0.07 217.05 12.45 216.98

217.05

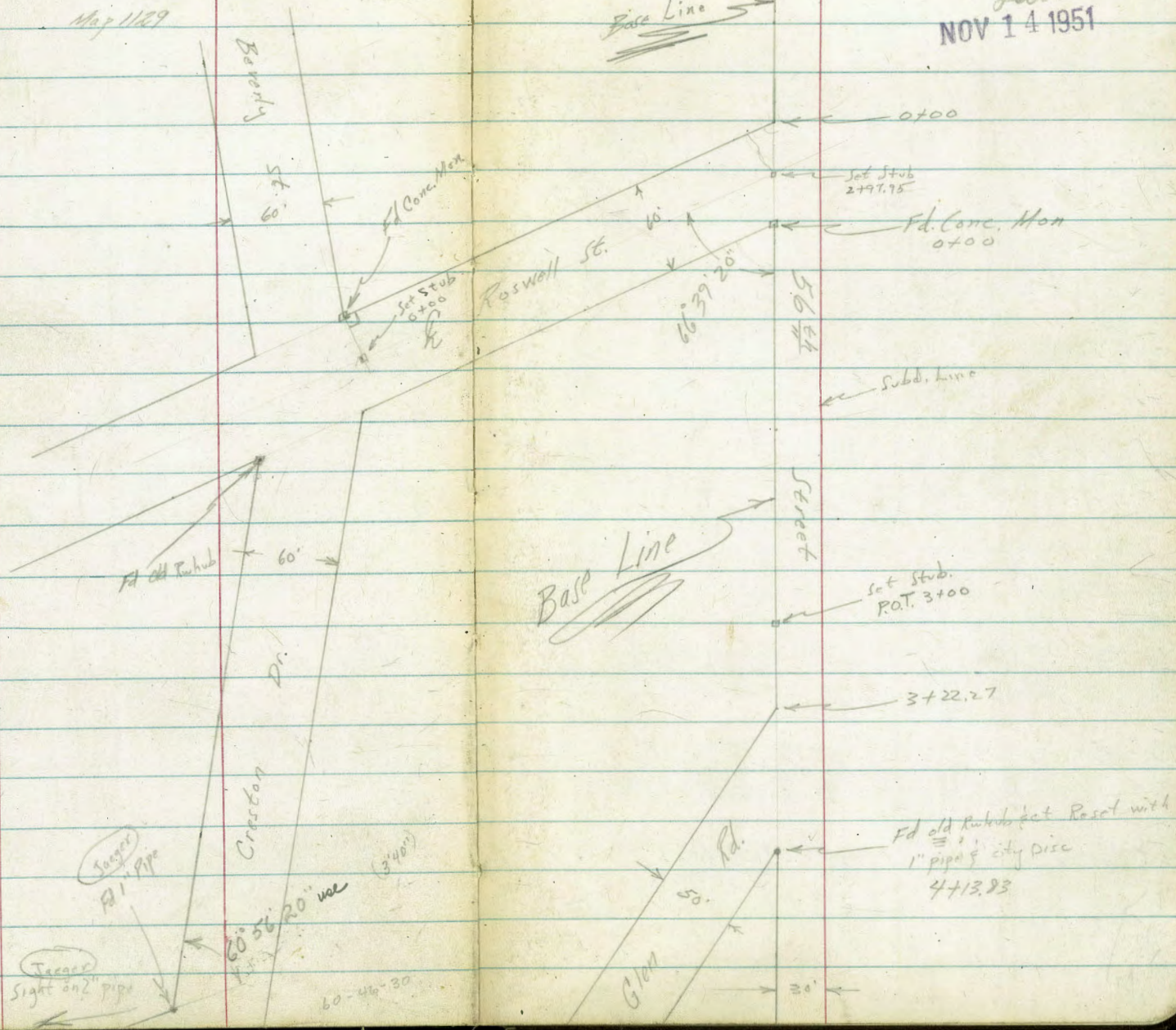
1+00

219.4
16.0
10
216.3
11.1
229.43
215.9
13.5
11
± Ditch
218.7
10.7
20

Roberts
Allen
Moore
Fellon
11-13-51
NO. 31502

X-Section Roswell Street
Beverly to 56th
X-section 56th St. 100' either side of
Roswell
Map 1129

INDEXED
Law
NOV 14 1951



Contd From Page 58

X- Sect Roswell
Beverly to 56[±]

Lt

E

Rt

59

1+38

20[±] Rt to center P.Pole # JP173532

1+00

264.6	264.0	262.9	262.4	262.5	262.2	262.5	262.3	262.1
4.0	4.6	5.7	6.2	6.1	6.4	6.1	6.3	6.5
50	30	17	16		15	16	30	50

0+50

265.7	264.0	263.0	262.5	262.7	262.4	262.7	262.2	261.7	260.7	259.8
2.7	4.6	3.6	6.1	5.9	6.2	5.9	6.4	6.9	7.9	9.8
50	30	19	18		15	16	27	30	35	75

0+00

Line thru NE Prop Coc. Beverly & Roswell 70° to R

266.1	264.1	263.5	263.0	263.1	262.8	263.2	262.7	258.7	256.4
2.5	4.5	5.1	5.6	5.5	5.8	5.4	5.9	9.9	12.2
50	30	16	15		15	16	30	43	75

0-30

264.8	264.1	263.2	262.7	262.6
3.8	4.5	5.4	5.9	6.0
50	30		30	50

0-01

20[±] Rt to center Fire Hydrant

0-04[±]

20' Rt to center P. Pole # P171129

BM

4.7726866 X

263.89 NE. PL.

Mon. Beverly & Roswell See FB/612 page B

268.66 X

32.7' Lt. End Fence & conc wall
 Section & location of Fence on this line
 2+97.95 West Line of 56th

263.9	262.5	263.6	263.2	262.2	261.8	261.5	261.7	261.0	259.4
7.7	6.1	5.0	5.4	6.4	6.8	7.1	6.9	7.6	9.2
32.7	32.7	32.7	29	25		14	15	32.2	48
Top	Foot	GRD							Top Wash

2+88 20.5' Rt to Center Pole # P171130

2+79 29' Lt & 4' Conc Walk

263.69
 197
 29.2
 conc

2+57 30' Lt Begin Picket Fence on small conc wall

263.3	262.2	262.5	261.8	261.7	261.7	261.4	261.6	261.1	258.7	257.4
5.3	6.4	6.1	6.8	6.9	6.9	7.2	7.0	7.5	9.7	10.2
30	30	30	19	17		14	15	30	35	56
Top	Foot	GRD								Top Wash

2+25

262.0	262.0	261.8	261.8	261.5	261.9	261.5	261.1	259.3	244.4
6.6	6.6	6.8	6.8	7.1	6.7	7.1	7.5	9.3	24.2
30	17	16		13	14	27	30	37	56
									Top Return Wash

2+00

261.6	262.3	262.2	261.9	261.9	261.6	261.9	261.6	258.8
7.0	6.3	6.4	6.7	6.7	7.0	6.7	7.0	9.8
50	30	17	16		15	16	30	54
								Top Wash

1+50

262.7	262.7	262.7	262.0	262.3	261.9	262.2	262.1	263.0	261.9	259.6
5.9	5.9	5.9	6.6	6.3	6.7	6.4	6.5	5.6	6.7	9.0
50	30	17	16		15	16	28	30	50	75

268.667

268.667

Cont'd From Page 60

X-Set 56th
Roswell to Glen Rd.

1400

0750 7³/₄ Lt to Deadman

0741

Top wash

0731 7' Lt to Guy Pole

0731

Bottom wash

0717

Top wash

0700

Wash Ends at 20 Lt.
SW Prop. Corner 56th & Roswell

T.R.

170

261.54 π

8.82

259.84

Mon

SW Cor (Prop.) Roswell & 56th

268.66 π

Lt

264.8

+33
60

263.1

+16
30

261.1

0.4
12

East Line

258.4

3.1

254.8

6.7

17
Top
wash

241.7

19.8

32
Bottom
wash

264.5

+30
60

261.0

0.5
30

260.2

1.3
12

258.4

3.1

257.4

4.1

10
Top
wash

251.4

10.1

15
Bottom
wash

257.0

4.5

26
7' Lt
wash

258.5
3.0

253.8

7.7

259.3

2.2

263.3

+18
60

261.54

0
30

260.7

0.8
15

261.1

0.4

261.54 π

61

Rt

Base Line
at Page 1.

4+00

228.5	232.4	235.7	239.6
21.0	17.1	13.8	9.9
60	30		30

3+50

242.8	242.8	244.1	248.8
6.7	6.7	5.4	0.7
60	30		30

T.P. 0.56 249.57 π 12.53 249.01

249.57 π

3+00

251.0	252.8	254.0	252.6	249.4
10.5	8.7	7.5	8.9	12.1
60	30		15	30

2+50

259.7	259.2	257.6	257.2	255.4	250.0
1.8	2.3	3.7	4.3	6.1	11.5
60	30	24	8		30

2+00

263.3	262.5	260.7	259.5	258.0	251.9
+1.8	+1.0	0.8	2.0	3.5	9.6
60	30	22	5		30

1+50

265.5	264.7	262.5	261.7	259.9	253.3	249.2
+4.0	+3.2	+1.0	+0.2	1.6	8.2	12.3
60	30	23	6		30	50

T.O.P
wash

261.54 π

261.54 π

Cont'd From Page 62

X-Section 5616
Roswell N.H.

Base Line
West P.L.

1700

264.7	264.7	263.8	263.4	263.8	265.0
3.5	3.5	4.4	4.8	4.4	3.2
5		3	30	32	60

0+97.5 Old End Picket Fence

0+50

263.9	263.4	263.3	262.8	263.6	263.2	265.1
4.3	4.8	4.9	5.4	4.6	5.0	3.1
20		3	27	30	45	60

0+24 02' 14" End conc. wall

263.8	263.0	263.5
4.4	5.2	4.7
0.2	0.2	0.2
Top	Foot	GRD

0+00 } South Bayin Fence
N.H. Line Roswell

263.6	262.3	262.3	263.1
4.6	5.9	5.9	5.1
7	30	60	

Q Roswell

R.L. to Base Line

261.8	262.1	263.5
6.4	6.1	4.7
	30	60

T.P. 8.40 268.24 π 1.84 259.84

268.24 π

T.P. 12.67 261.18 0.56 249.01

249.57 π

3700

259.8 263.9 263.7 266.8
 8.4 4.3 4.5 1.4
 30 30 60

2750

257.1 262.5 263.9 263.7 264.3 266.2
 11.1 5.7 4.3 4.5 3.9 2.0
 30 5 30 42 60

2709 75' Rt to Center P.P. 1/6 # 7

2700

255.4 258.2 263.9 263.7 264.7 265.5
 12.8 10.0 4.3 4.5 3.5 2.7
 30 10 10 30 50 60

1750

261.4 260.4 263.6 263.8 264.6
 6.8 7.8 4.6 4.4 3.6
 30 8 30 60

1740

264.1 262.6 264.2 263.8 264.2 264.4
 4.1 5.6 4.0 4.4 4.0 3.8
 30 17 30 32 60

1713 0.1' Lt & 11' Conc Agreen

265.53 264.87
 2.71 3.37
 6 0.1
 Floor Conc

268.247

268.247

Floor Line
w.p.l.

Cont'd From Page 64

65

Bar Line
(W.P.L.)

Check 361 263.89 = 263.89 Starting BM

T.P. 5.71 267.50 6.45 261.79

4400

264.6	265.7	262.5	262.1	265.3
36	2.5	5.7	6.1	2.9
30		8	30	60

3750

262.1	265.4	265.4	263.4	263.1	266.5
6.1	2.8	2.8	4.8	5.1	1.7
30		2	8	30	60

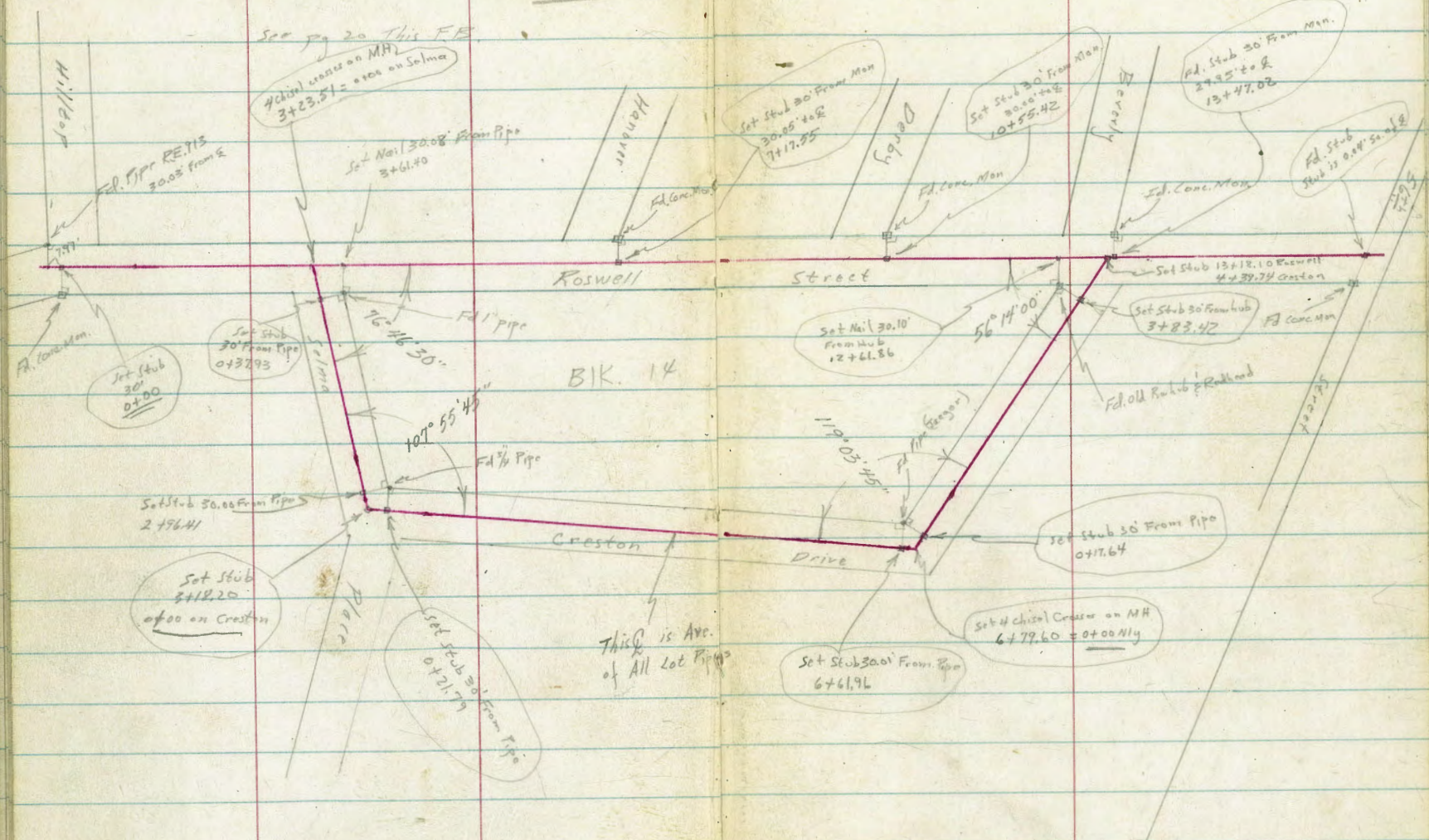
268.24X

268.24X

Robert
Moore
Pellen
11-27-51
W.O. 31502

CK. Block 14, Beverly

Ties



See pg 20 This FR

Set chisel cross on MH
3+23.51 = 0+00 on Salma

Set Stub 30' From MH
30.85 to R
7+17.25

Set Stub 30' From MH
30.00 to R
10+55.42

Set Stub 30' From MH
2+95 to R
13+47.02

Set Stub
Stub is 0.44' to R

Set Nail 30.10'
From Hub
12+61.86

Set Stub 13+12.10 Roswell
4+39.74 Creston

Set Stub 30' From Hub
3+83.42

Set Stub 30' From Pipe
0+17.64

Set chisel cross on MH
6+77.60 = 0+00 Nly

Set Stub 30.00' From Pipe
6+61.96

Set Stub
2+18.20
on Creston

Set Stub 30.00' From Pipe
2+96.41

Set Stub
30' From Pipe
0+37.93

Set Stub
30'
0+00

BIK. 14

This is Ave.
of All Lot Pipes

INDEXED
LOW
JUL 1 1952

lt. ♀ Rt.

x-Sept. for Prop. Drain on South side
 of Roswell - at sta 4+82 - P. 25
 Present Culvert empties into Head of wash
 Water has washed large gully. - ♀ at
 90° to S.L. of Roswell - 0+00 = S.L.
 W.O. 20861 - 2-28-52 - 7.0.

0+40 = Top of Bank - ♀ of Wash angles to
 Right

0+30

				232.0	
				6.2	
	235.2	233.7	225.0		
	2.0	4.5	13.2	216.3	211.9
	20	13	8	71.9	26.3
			to		33 = face of Bank on Bottom

0+14.2 = end of 15" Cor. Iron pipe

	233.0	233.8	227.8	223.5	232.17	227.1	235.4	233.5
	5.2	4.4	10.4	14.7	6.04	11.1	4.8	4.9
	15	7	6	9	end	IE of Pipe	12	15

0+09 = edge of bank

	234.6	234.02	234.1
	3.6	4.19	4.1
	10	Top pipe	10

0+00

236.3
1.9

B.M. 267 - 738.21

235.54 - Cross of pipe - 0+00 - P. 56

238.21

0+00 - South Line of Roswell - sta. 4+82
 P. 25

265
1096
275 26
519
270 67

190 15
938
180 77

~~473~~
473
511
984
492

12 30 Lt.

37+54.82
15
+39.82

01 Rt.

1722 - P. 23 = Bridge

3754.82
3077.75

677.07

26+59
24+13.03

2.46

24+13.03
20+80.66

332.37

3077.75
2413.03

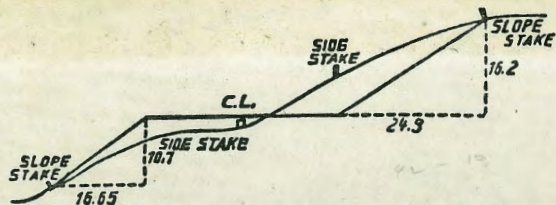
664.72

3077.75
4185

2659.2

41.84
556

36.28



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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