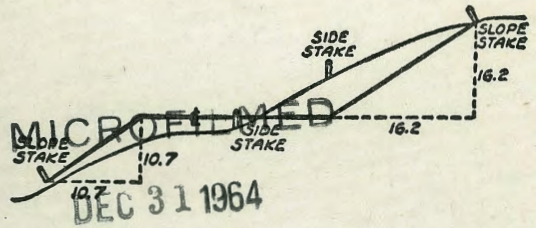
2087



MICROFILMED
DEC 31 1964

Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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Table XIII—Corrections for Tangents and Externals

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

For Tangents Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

For Externals Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Cross Sec. Wabash Blvd. Sec. #" 97+85.0' to 219+75.12 1-61

" " Area East of Wabash Blvd N of Federal 62-65

" " Wightman St & 40th St 66-67

" " 40th St. Wightman to Universal 68-78

Cross Section Wabash Boulevard
Section "H" 97+65.01 to 219+75.12

Note:- Rt.&Lt. + Above ℄ - Below ℄

INDEXED
WJC.
JUN 7 1950

March 31.50
AS.5507
D. Smith
Rorer
Chavez
Cota

Station	Lt. = West			℄	Rt. = East	
+50.8°	48.1 -2.2 76.8=F5.2 4:1	48.3 -2.0 50	49.1 -1.2 25'	50.3 5.5	50.5 +0.2 28'	50.4 +0.4 49=℄S.F.L.
99+0		45.0 -1.6 56.6=F9.4 1½:1	46.0 -0.6 25	46.6 9.2	47.4 +1.1 32'	48.8 +2.2 51.4=F4.9 1½:1
+50		44.8 -0.5 56.2=F8.1	45.1 -0.2 30	45.3 10.5	45.7 +0.4 28'	48.3 +3.0 53.3=F6.2
98+0		44.5 -0.9 56.3=F8.1	44.8 -0.6 30'	45.4 10.4	46.2 +0.8 25	46.8 +1.4 56.3=F8.2
97+65.01 F.C.		44.9 -0.9 55.4=F7.6 1½:1	45.6 -0.2 30'	45.8 10.0	45.3 -0.5 27	45.3 -0.5 59.5=F10.3 1½:1

For Head Bank See #2071 Page 2

BM 1.72 55.82 54.10 Mon. [illegible] So. Broadway 55.82

Sta.					Lt.	℄	Rt.
+50					65.1 / 0.0 / 64.0 · 66.1 / +1.0 / 32 · 66.4 / +1.3 / 14	65.1 / 9.9	60.4 / −4.7 / 41 · 56.4 / −8.7 / 67.0 = 0.0
TP	4.88	75.02	1.32	63.14		75.02	
+36					64.5 / +3.1 / 67.0 · 65.7 / +4.3 / 58.0 · 65.4 / +4.0 / 24	61.4 / 3.1	58.6 / −2.8 / 22 · 58.1 / −3.3 / 44 · 47.7 / −10.7 / 67.3
101+0					64.0 / +4.7 / 65.3 = 68.3 / 11 · 65.2 / +5.9 / 35	59.3 / 5.2	57.1 / −2.2 / 5 · 56.3 / −3.0 / 31 · 48.1 / −11.2 / 41 · 49.2 / −10.1 / 81.6 = 56.4 / 9.1
+65					57.8 / +3.3 / 64.0 · 55.6 / +1.1 / 25	54.5 / 10.0	51.3 / −3.2 / 32 · 49.4 / −5.1 / 80
+25					54.6 / +0.7 / 60 · 54.1 / +0.2 / 30	53.9 / 10.6	53.8 / −0.1 / 52.0 · 53.5 / −0.4 / 75
TP	11.05	64.46	2.41	53.41		64.46	
100+0					55.0 / +2.0 / 57.0 = 0.0 · 52.5 / −0.5 / 34.0	53.0 / 2.8	53.0 / 0.0 / 34.0 = ℄ Loop
	55.82					55.82	

April 1-50
start 102+50

Station						Lt.			℄	Rt.			
104+00						77.5 −9.4 / 75	84.3 −2.6 / 51	85.8 −1.1 / 28'	86.9 5.4	87.1 +0.2 / 33	87.4 +0.8 / 60	87.8 +0.9 / 82.2 = c26.2 1:1	87.8 +0.9 / 100'
+81.72							78.2 −8.2 / 74.7 = c17.7 1:1	85.0 −1.4 / 41.0	86.4 5.9	87.2 +0.8 / 42'	87.6 +1.2 / 82.6 = c26.4 1:1		87.8 +1.4 / 100
+50						78.5 −7.5 / 75.1 = c18.1 1:1	73.1 −2.9 / 50	74.5 −1.5 / 32'	86.0 6.3	86.8 +0.8 / 38'	87.0 +1.0 / 82.9 = c26.4 1:1		87.1 +1.1 / 100
103+00						73.6 −11.6 / 71.0 = c14.0 1:1	78.9 −6.3 / 46	83.8 −1.4 / 20'	85.2 7.1	85.0 −0.3 / 43'	82.0 −3.2 / 79.5 = c22.5 1:1		81.3 −3.9 / 100
TP	8.17	92.34	0.09	84.17					92.34				
+50							68.4 −11.4 / 67.9	73.3 −6.5 / 38	79.8 4.5	81.8 +2.0 / 24	76.6 −3.2 / 59	76.3 −3.5 / 66.7 :5	74.9 −4.9 / 85.0
TP	12.52	84.26	3.28	71.74	on ℄ Hub				84.26				
102+00							66.8 −4.7 / 65.0	68.3 −3.2 / 37	71.5 3.5	72.4 +0.9 / 25'	70.7 −0.8 / 54	68.5 −3.0 / 66.0	
		75.02							75.02				

Cross Section Wabash Blvd.
Section "A"

Note! Rhodes Arc Used
From Sta. 106+0 - 113+50

Rhodes Arc Used

+75						69.4 / -26.1 / 45=0.0	71.0 / -18.5 / 44	81.4 / -8.1 / 26	95.5 / 6.5	100.6 / +5.1 / 30	105.5 / +10.0 / 73.8=C38.5 3/4:1	105.7 / +10.2 / 122		
+50						64.8 / -29.2 / 84	78.0 / -16.0 / 54.1=C9.1 1:1	83.3 / -10.7 / 45	87.1 / -6.9 / 30	94.0 / 7.8	98.1 / +4.1 / 30	102.3 / +8.3 / 72.9=C35.9 3/4:1	102.6 / +8.6 / 100	101.2 / +7.2 / 140
106+0						72.2 / -16.9 / 99	79.1 / -10.0 / 83.0	80.3 / -8.8 / 57.5=C12.5 1:1	85.8 / -3.3 / 26	89 / 12.7	92.2 / +3.1 / 32	94.1 / +5.0 / 79.2=C39.2 1:1	95.3 / +6.2 / 100	95.3 / +6.2 / 172
IP	12.24	101.77	2.81	89.53	07 Z Hob 105+49.75				101.77					
+49.75	B.C.Rt.					76.5 / -13.0 / 75	79.9 / -9.6 / 58.7=C13.7 1:1	86.2 / -3.3 / 22	89.5 / 2.81 07 Hub	90.9 / +1.4 / 46	91.8 / +2.3 / 80.6=C27.6 1:1	92.3 / +2.8 / 100		
105+0						71.7 / -17.5 / 76	76.4 / -12.8 / 56.8=C11.8 1:1	85.8 / -3.4 / 30	89.2 / 0.1	90.7 / +1.5 / 42	90.7 / +1.5 / 82.4=C27.4 1:1	90.8 / +1.6 / 100		
104+50						73.8 / -14.4 / 75	82.9 / -5.3 / 42	87.3 / -0.9 / 17	88.2 / 41	88.9 / +0.7 / 40	89.0 / +0.8 / 81.9=C26.4 1:1	89.2 / +1.0 / 100		

92.34

92.34

Lt ℄ Rt

108+05
65.8 / −13.5 / 53.0 — 64.1 / −15.2 / 36.0 — 65.1 / −14.2 / 11.0 — 70.2 / −9.1 / 3.0 — 79.3 / 1.4 — 97.3 / +18.0 / 41.0 — 114.4 / +35.1 / 78.0 — 122.3 / +43.0 / 100.0 — 125.1 / +46.8 / 133.0 — 127.6 / +18.3 / 176.0

108+93
65.2 / −5.2 / 53.0 — 64.0 / −6.4 / 26.0 — 64.5 / −5.9 / 9.0 — 70.4 / 10.3 — 73.1 / +5.0 / 5.0 — 82.2 / +11.8 / 6.0 — 96.4 / +26.0 / 37.0 — 107.4 / +37.0 / 60.0 — 121.6 / +50.2 / 100.0
121.9 / +51.5 / 130.0 — 123.4 / +53.0 / 156.0 — 124.2 / +53.8 / 190.0

+50
64.3 / −1.7 / 54.2 = F 68 / 1½:1 — 62.8 / −3.2 / 7.0 — 66.0 / 14.7 — 69.8 / +3.8 / 6′ — 72.9 / +6.9 / 13.0 — 97.5 / +31.5 / 18.0 — 102.5 / +36.5 / 41.0 — 112.1 / +46.1 / 68.0
116.8 / +50.8 / 100.0 — 117.0 / +51.0 / 125.0 — 118.3 / +52.3 / 150.0

Rhodes Arc

+15
62.7 / −9.1 / 54.0 — 63.8 / −8.0 / 12′ — 71.8 / 8.9 — 73.6 / +1.8 / 4.0 — 96.8 / +35.0 / 8.0 — 104.8 / +33.0 / 38.0 — 110.2 / +38.4 / 65.0
111.3 / +39.5 / 100.0 — 111.3 / +39.5 / 125.0 — 110.4 / +38.6 / 144.0

TP 5	2.48	80.69	12.75	78.21
TP	2.13	90.96	12.94	88.82

80.69

107+0
62.4 / −33.3 / 55.6 = F 77 / 1½:1 — 62.4 / −33.3 / 20.0 — 68.7 / −27.0 / 11.0 — 94.1 / −1.6 / 5 — 95.7 / 6.1 — 102.8 / +7.1 / 3.0 — 108.2 / +12.5 / 64.9 = C 40.7 / 2:1 — 109.0 / +10.3 / 100 — 108.1 / +13.0 / 118

101.77

101.77

TP	4.70	79.19	13.60	74.49
+94.17				
+50				
110+0				
TP	6.89	87.09	0.49	80.20
+50				
109+0				
108+50				
		80.69		

Rhodes Ave

68.6 / −12.0 / 61 — 68.0 / −13.6 / 47 — 69.6 / −11.0 / 22 — 77.0 / −3.6 / 5.0 — 80.6 / 6.5 — 106.1 / +25.5 / 32.5 — 127.4 / +46.8 / 72.0 — 140.7 / +60.1 / 123.0 = F4H 2.0

67.5 / −18.8 / 60.0 — 67.4 / −18.9 / 33.0 — 70.3 / −16.0 / 25.0 — 76.1 / −10.2 / 18.0 — 86.3 / 0.8 — 115.5 / +29.2 / 49.0 — 131.0 / +44.7 / 84.0 — 141.0 / +54.7 / 126

67.4 / −16.2 / 67.0 — 66.4 / −17.2 / 46.0 — 68.1 / −15.5 / 32.0 — 75.0 / −8.6 / 18.0 — 83.6 / 3.5 — 113.6 / +30.0 / 53.0 — 126.6 / +43.0 / 80.0 — 133.6 / +50.0 / 100.0 — 141.5 / +57.9 / 133.0

87.09

66.2 / −14.0 / 57.8 = F9.3 1½:1 — 66.4 / −13.8 / 42.0 — 67.6 / −12.6 / 26.0 — 74.0 / −6.2 / 13.0 — 80.2 / 0.5 — 113.1 / +32.9 / 57.0 — 123.0 / +42.8 / 78.0 — 132.0 / +51.8 / 100.0 — 139.7 / +59.5 / 140.0

66.5 / −10.2 / 55.7 = F7.8 1½:1 — 65.7 / −11.0 / 28.0 — 70.1 / −6.6 / 13.0 — 72.9 / −3.8 / 5.0 — 76.7 / 4.0 — 104.8 / +28.1 / 50.0 — 116.8 / +40.1 / 77.0 — 127.1 / +50.4 / 100.0 — 136.6 / +59.9 / 151.0

64.7 / −12.2 / 57.2 = F8.8 1½:1 — 65.8 / −11.1 / 35.0 — 65.4 / −11.5 / 17.0 — 71.9 / −5.0 / 11.0 — 76.9 / 3.8 — 96.5 / +19.6 / 45.0 — 120.5 / +43.6 / 90 — 125.3 / +48.4 / 105 — 128.9 / +52.0 / 136 — 131.1 / +54.2 / 165.0

80.69

April 20-50 113+50 Start

F.S. 5502
D Smith
Rorer
Chavez
Cota

Rboder Are Used

Station	Lt.			℄	Rt.			
114+0	73.0 −0.5 / 75.0	74.4 +0.9 / 57.0'	73.7 +0.2 / 25	73.5 5.7	72.9 −0.6 / 21.0	74.7 +1.2 / 50	80.2 +6.7 / 60.5 =0.0	82.4 +8.9 / 65.5
+50				72.8 6.4	73.3 +0.5 / 39.0	79.8 +7.0 / 57.4 =0.0	82.0 +9.2 / 58.0	
113+0	71.5 +0.6 / 51.0	71.9 +1.0 / 25.0		70.9 8.3	71.6 +0.7 / 26.0	80.7 +9.8 / 49.0	96.8 +25.9 / 71.6 =C17.8 1:1	
+50	70.6 −1.1 / 50.0	71.7 0.0 / 23.0		71.7 7.5	71.3 −0.4 / 25	79.9 +8.2 / 43.0	90.2 +18.5 / 58.0	113.4 +41.7 / 90.3 =C35.3 1:1
112+0	69.8 −0.2 / 52.0	69.4 −0.6 / 26.0		70.0 9.2	70.8 +0.8 / 15'	79.0 +9.0 / 28.0	102.0 +32.0 / 61.0	126.2 +56.2 / 92.0 =C49 3/4:1
111+50	68.9 −2.9 / 54.0	69.0 −2.8 / 24.0'	70.1 −1.7 / 3.0'	71.8 7.4	78.1 +6.3 / 11.0	99.9 +28.1 / 40.0	127.8 +56.0 / 81.6	136.2 +64.4 / 99.4 =C58.2 3/4 Change Framin

Cross Section Wabash Blvd.
Section "A"

Sta.	BS	HI	FS	Elev.	Note	Lt	Lt	Lt	Lt	℄	Rt	Rt	Rt	Rt
BM			4.80	79.26	× on MH Rim 100' Lt ℄ 116+0 79.26									
+50						78.5 +0.1/77'	78.7 +0.3/57.1 =F8.7	78.4 0.0/36	78.4 0.0/15	78.4 5.7	78.3 −0.1/26	78.4 0.0/52.3 Stake out	78.3 −0.1/65.0	
TP	6.00	84.06	1.13	78.06						84.06				
116+0						78.1 0.0/83'	78.2 +0.1/57.3 Slope stake out	77.4 −0.4/44'	77.5 −0.6/20'	78.1 1.1	78.0 −1.0/32.6	78.3 +0.2/52.3 =F5.5	77.5 −0.6/65'	
+50						77.2 +1.6/83'	77.4 +2.1/60.3 =F8.3	77.4 +1.8/43'	76.1 +0.5/16'	75.6 3.6	75.1 −0.1/26	76.9 +1.3/53.3 =F6.2	77.8 +2.2/69	
115+0						76.0 +0.3/82	76.4 +0.7/66.3 =F9.1 1½:1	76.4 +0.7/42'	76.0 +0.3/17	75.7 2.5	75.5 −0.2/20	76.0 +0.3/40	76.3 +0.6/52.7 =F5.8 1½:1	78.7 +3.0/63.0
+50						74.4 −0.2/81.0	74.6 0.0/71.1 =F10.3 1½:1	75.1 +0.5/50'	74.7 +0.1/25	74.6 4.6	74.4 −0.2/12'	74.4 −0.2/34'	75.1 +0.5/55'	80.5 +5.9/68.0 =0.0
114+13.54	℄ Curve						73.4 −0.7/74.0	73.7 +0.1/43.0	73.9 +0.3/25'	73.6 5.6	74.6 +1.0/10	72.9 −0.7/27'	75.3 +1.7/54'	80.9 +7.3/65.0
		79.19								79.19				

Sta.				Lt.				℄	Rt.				
TP		-0.33	83.73	on ℄ Stake 119+50									
+50				82.3 / -1.5 / 67	82.3 / -1.5 / 58.1 =F9.4 1½:1	82.3 / -1.5 / 40'	83.1 / -0.7 / 20	83.8 / 0.3	84.5 / +0.7 / 21	84.4 / +0.6 / 50.6 =F4.4 1½:1	84.7 / +0.9 / 62		
119+0				80.2 / -1.1 / 70	80.4 / -0.9 / 59.8 =F10.5	81.0 / -0.3 / 42	80.9 / -0.4 / 20	81.3 / 2.8	81.6 / +0.3 / 16'	81.9 / +0.6 / 35	83.9 / +2.6 / 46.0	81.9 / 0.6 / 53.2 =F6.1	83 / +1.7 / 62
+50				19.9 / -0.9 / 70'	19.8 / -1.0 / 59.6 =F10.4	19.3 / -1.5 / 36	80.4 / -0.4 / 16'	80.8 / 3.3	80.5 / -0.3 / 25'	80.8 / 0.0 / 55.4 stake out	81.5 / +1.0 / 67.0'		
118+0				19.4 / -0.4 / 70.0'	19.7 / -0.4 / 58.6 =F9.7	19.8 / -0.3 / 38	19.7 / -0.4 / 15'	80.1 / 4.0	19.8 / -0.3 / 25'	80.1 / 0.0 / 48'	18.0 / -2.1 / 36.8 =F8.5	18.3 / -1.8 / 68'	
+50				19.7 / -0.2 / 67	80.1 / +0.2 / 56.9 =F8.6	19.4 / -0.5 / 38'	19.7 / -0.2 / 16'	79.9 / 4.2	19.3 / -0.6 / 21.0	19.4 / -0.5 / 41	18.5 / -1.4 / 55.1 =F7.4	18.7 / -1.2 / 65	
117+0				18.9 / +0.1 / 69.0	19.2 / +0.4 / 57.5 =F9.0 1½:1	19.0 / +0.2 / 41.0	19.1 / +0.3 / 17'	78.8 / 5.3	18.9 / +0.1 / 20	19.0 / +0.2 / 42	19.1 / +0.3 / 54.2 =F6.8 1½:1	18.3 / -0.5 / 65.0	
	84.06							84.06					

122+0					91.2 / -9.7 / 63; 93.8 / -7.1 / 49.6 =F1.4 4:1; 96.4 / -4.5 / 38; 98.4 / -2.5 / 12.0; 100.9 / 7.0; 103.8 / +2.9 / 8'; 107.5 / +6.6 / 28; 109.6 / +8.7 / 62.0 =C17.8 1:1; 110.1 / +9.2 / 72.0
+50					87.4 / -8.8 / 70; 87.8 / -8.4 / 54.2 =F8.8 1½:1; 92.8 / -3.4 / 21; 96.2 / 11.7; 99.8 / +3.6 / 14; 103.9 / +7.7 / 34; 107.5 / +11.3 / 60.6 =C15.6; 107.2 / +11.0 / 71
TP	6.05	107.88	0.23	101.83	107.88
121+0					86.1 / -7.2 / 66; 86.4 / -6.9 / 55.4 =F7.6; 89.3 / -4.0 / 29.0; 93.3 / 8.8; 95.9 / +2.6 / 20; 97.5 / +4.2 / 38; 98.2 / +4.9 / 52.0 =C7.0; 99.3 / +6.0 / 64.0
+50					85.2 / -4.6 / 70; 85.4 / -4.4 / 55.7 =F7.8 1½:1; 87.5 / -2.3 / 27; 89.8 / 12.3; 92.0 / +2.2 / 20; 93.6 / +3.8 / 37; 93.4 / +3.6 / 48.0 =C3.0 1:1; 92.2 / +2.4 / 58.0
TP	12.37	102.06	1.51	89.69	102.06
+13					84.0 / -3.5 / 69; 84.2 / -3.3 / 57.1 F8.4; 86.3 / -1.2 / 24; 87.5 / 3.7; 89.1 / +1.6 / 18'; 89.7 / +2.2 / 45 =0.0; 89.5 / +2.0 / 55.0
120+0					83.1 / -3.8 / 68; 83.3 / -3.6 / 57.7 =F9.1 1½:1; 83.4 / -3.5 / 42; 84.9 / -2.0 / 20; 86.9 / 4.3; 87.6 / +0.7 / 23; 88.3 / +1.4 / 45.8 =F1.2 1½:1; 88.2 / +1.3 / 60.0
BM	11.94	91.20		79.26	X on MH Rim 100 Lt. 116+0; 91.20

					Lt.		Rt.
124+0					107.0 114.6 113.7	115.4 116.7 116.6	
					-7.5 -6.7 -1.1 11.1	+1.7 +3.0 +2.9 +3.4	
					51.0 25.7=C 10.7 24.0	24 45.0 85.4=C 20.4 76	
					4.1	1.1.1	
TP	10.62	124.82	2.17	114.19	124.82		
+50					101.1 101.8 101.4 112.2	113.6 114.3	
					-12.4 -11.1 -10.4 -1.5 3.3	+1.4 +2.1 -2.9	
					78.0 66.0=C 1.5 60.0 25.0	27 38.8=C 1.88 75.0	
					4.1	1.1.1	
123+0					99.1 103.6 108.1 110.2	111.3 112.7 113.2 113.2	
					-13.5 -10.5 -6.6 -2.1 5.3	+1.1 +2.5 +3.0 +3.0	
					75.0 61.5=C 3.4 50.0 24.0	18.0 43 63.7=C 1.97 75	
					4.1	1.1.1	
BM			2.17	114.19	02 100 BP. Rt. 123+77.33 114.20		
+77.33 EC					95.5 96.0 97.5 105.7 3.80	110.3 111.9 112.7 112.9	
					-12.8 -12.3 -10.8 -2.6 7.11	+2.0 +3.6 +3.9 +4.6	
					80 70 0.0 58 25 6.2+0.5	20 46.0 63.1=C 1.81 75.0	
						1.1.1	
TP	9.73	115.36	0.25	107.63	115.36		
+50					95.3 95.9 98.2 102.5 105.9	109.9 110.9 112.0 112.7	
					-10.6 -10.0 -7.7 -3.4 3.0	+4.0 +5.0 +6.1 +6.8	
					70 60=0.0 39.0 20.0	24.0 45.0 63.5=C 1.85 75.0	
						1.1.1	
122+18			5.1		94.2 95.5 98.5 102.8 5.1	104.2 108.2 110.7	
					-8.6 -7.3 -4.3	+1.4 +5.4 +7.9	
					55 45.5=0.0 22.0	6.0 37.0 63.0	
		107.88			107.88		

Wabash Blvd Section "A" April 28-50

A. Sisson
D. Smith
Rarer
Chayek
Cota

Sta.						Lt.			℄	Rt.			
+75						90.3 / −20.5 / 57.0 Slope Line	90.5 / −20.3 / 49.0	90.8 / −20.0 / 36.0	110.8 / 12.3	115.8 / +5.0 / 8.0	120.4 / +9.6 / 32.0	123.9 / +13.1 / 70 Slope Line	125.1 / +14.3 / 80
126+0						90.4 / −22.6 / 56.8 F8.5	91.4 / −21.6 / 39.0	101.6 / −11.9 / 26.0	113.0 / 10.1	119.2 / +6.3 / 17	123.0 / +10 / 69.1 C24.1	124.3 / +11.3 / 79.0	
±70						90.9 / −24.6 / 58.0	90.6 / −24.9 / 49.0	101.8 / −13.7 / 27	115.5 / 7.6	119.1 / +3.6 / 8	119.9 / +4.4 / 30	121.0 / +5.5 / 50.0	122.5 / +7.0 / 71.0
TP	8.47	123.05 ✓	10.24	114.58	Stub 75' Rt. 126+75				123.05				
+50						93.5 / −20.0 / 55.0	98.2 / −15.3 / 45.0 = 0.0	111.0 / −2.5 / 10.0	113.5 / 11.3	118.3 / +4.8 / 22	121.3 / +7.8 / 55	121.8 / +8.3 / 68.5 = C23.5 1:1	13 / +9.3 / 79.0
125+0						11 / −4.9 / 68.0	112.8 / −3.9 / 60.2 = C15.2 1:1	115.9 / −0.8 / 23	116.7 / 8.1	118.3 / +1.6 / 27.0	122.3 / +5.6 / 69.6 C24.6 1:1	130.0 / +6.0 / 80	
124+50						−4.7 / 7.0	111.7 / −4.6 / 59.7 C14.7 1:1	114.1 / −1.6 / 27.0	116.7 / 9.1	117.0 / +1.3 / 19.0	119.1 / +3.4 / 48	120.2 / +4.5 / 68.3 C23.3 1:1	+5.5 / 78.0
		124.82 ✓							124.82				

+50

128+0

+50

127+0

+65

TP	0.52	99.25	12.53	98.73
TP	0.95	111.26	12.74	110.31

126+40

123.05

96.5 96.3 97.0 95.0 93.5 94.2 96.7 102.6

+1.5 +1.3 +2.0 4.3 -1.5 -0.8 +1.7 +7.6

95.7 95.5 94.3 92.5 92.0 94.2 93.3 95.4 101.8

+2.9 +2.7 +1.6 -0.3 6.5 +1.4 +0.5 +2.6 +9.0

94.5 93.5 91.6 92.0 92.8 93.5 101.0

+2.5 +1.5 -0.4 7.3 +0.8 +1.5 +9.0

92.6 93.6 91.3 92.2 95.4 100.4 105.4

+1.3 +2.3 8.0 +0.9 +4.1 +9.1 +14.1

92.6 93.0 91.3 91.5 89.9 98.1 109.7

+1.1 +1.5 -0.2 7.8 -1.6 +6.6 +18.7

99.25

92.6 92.6 90.1 89.9 96.6 104.8 110.2 120.9

+1.2 +1.2 +1.7 +1.5 34.7 +10.2 +16.4 +20.8 +25.5

123.05

				Lt.			Rt.		
				98.2	98.2	98.2	98.2	97.6	106.4
				0.0	0.0	10.0	0.0	+1.4	+8.2
				56.3=58.2	33.0		28.0	62.0	74.0 0.0
1210+0									
				97.6	97.2	97.3	97.4	98.0	102.0	105.6
				+0.3	-0.1	10.9	+0.1	+0.7	+4.7	+8.3
+50				56.0 =58.0	26.0		23.0	58.0	64.0	73.4 0.0
				97.7	97.1	96.3	95.2	96.3	96.3	101.4	104.6
				+2.5	+1.9	+1.1	12.0	+1.1	+1.1	+6.2	+9.4
1230+0				54.7=57.2	38.0	18.0		28.0	52.0	63	70.0 =0.0
								108.17			
TP	11.87	108.17	2.95	96.30							
				97.8	97.5	96.9	95.6	95.0	95.4	104.0
				+2.2	+1.9	+1.3	5.6	-0.6	-0.2	+8.4
+50				53.5=56.3	35.0	8.0		22.0	30.0	38.4 =0.0
				97.5	96.9	96.6	96.4	95.2	96.4	103.4
				+1.1	+0.5	+0.2	2.9	-1.2	0.0	+7.0
1290+0				52.9=55.7	33.0	15.0		19.0	45.0	53.5 0.0
				96.3	96.3	96.1	95.7	93.9	94.1	96.0	103.0
				+0.6	+0.6	+1.0	3.6	-1.8	-1.6	+0.2	+7.2
1280+57				54.0	28.0	11.0		16.0	39.0	46.0	55.0 =0.0
		99.25						99.25			

Station	Rod	H.I.	Remarks	Elevations	Cross-section readings
+50				103.7, 104.0, 103.7, 102.7, 102.3, 100.0, 101.1, 107.0	+1.0/53.5 F6.3, +1.3/36.0, +1.0/15.0, 5.5, −0.4/14.0, −2.7/27.0, −1.6/62.0, +4.3/77.3 0.0
+13				103.9, 102.9, 102.2, 101.4, 99.9, 100.6, 107.6	+2.5/54.0, +1.5/38.0, +0.8/8.0, 6.8, −1.5/13.0, −0.8/43.0, +6.5/58.0
133+0				103.3, 102.0, 100.7, 99.7, 100.8, 109.4	+2.6/53.0 F6.0, +1.3/15.0, 7.5, −1.0/22.0, +0.1/44.0, +8.7/57.0 0.0
BM	3.75	104.42	x on M H Rim 60' Lt 132+50		
132+50				100.8, 100.5, 98.7, 98.9, 100.4, 101.0, 108.6	+1.9/55.9 F7.9, +1.6/22.0, −0.2/14.0, 9.3, +1.5/20.0, +2.1/38.0, +9.7/59.5 0.0
132+0				99.8, 98.9, 99.1, 99.9, 104.4, 107.8	+0.7/56.9 F8.0, −0.2/29.0, 9.1, +0.8/31.0, +5.3/61.0, +8.7/72.9 0.0
131+50				99.1, 98.9, 99.2, 99.2, 100.3, 102.7, 107.1	−0.1/56.9 F8.0 11.1, −0.3/28.0, 9.0, 0.0/29.0, +1.3/55.0, +3.5/64.0, +7.9/73.0 0.0

10 8.17

Wabash Blvd. Section "A"

Saturday April 29-50 16

				Lt.	℄	Rt.
136+13				106.9 +1.2 55.0 Slope Line	106.1 +0.5 30.0	105.6 105.5 105.2 105.3 106.6 111.1 11.6 -0.1 -0.4 -0.3 +1.0 +5.5 16.0 42.0 71.0 86.0 95.0
+95				107.1 107.4 107.8 106.6 +1.3 +1.5 +1.7 +0.7 52.0 25.0 15.0 10.0		105.9 105.4 104.7 104.9 105.3 107.9 11.3 -0.5 -1.2 -1.0 -0.6 +2.0 13.0 45.0 67.0 80.0 95.0
+50				105.8 -1.1 55.0 Slope Line	106.2 -0.7 30.0	106.9 106.3 106.6 103.4 104.6 104.2 105.3 10.3 -0.6 -0.3 -3.5 -2.3 -2.7 +1.4 21.0 42.0 64.0 89.0 106.0 116.8 -0.0
135+0				104.6 -1.2 53.4 Slope Line	106.0 +0.2 27.0	105.8 106.1 105.7 103.6 103.7 105.2 106.0 11.4 +0.3 -0.1 -2.2 -2.1 -0.6 +2.2 25.0 49.0 66.0 95.0 127.0 131.5 -0.0
+50				104.3 -0.6 54.8 Slope Line	105.9 +1.0 47.0	106.0 105.6 104.9 104.8 104.7 102.9 102.6 103.6 12.3 -0.1 -0.2 -2.0 -2.4 -1.3 -2.8 17.0 45.0 58.0 88.0 102.1 116.0 126.5 -0.0
TP	12.92	117.23	3.86	104.31		
134+06				104.7 +0.4 52.0	105.4 +1.1 35.0	105.1 104.3 103.5 100.1 102.0 103.0 106.2 10.9 -0.8 -4.2 -2.3 -1.3 +3.9 30.0 45.0 78 102 114.0
		108.17				

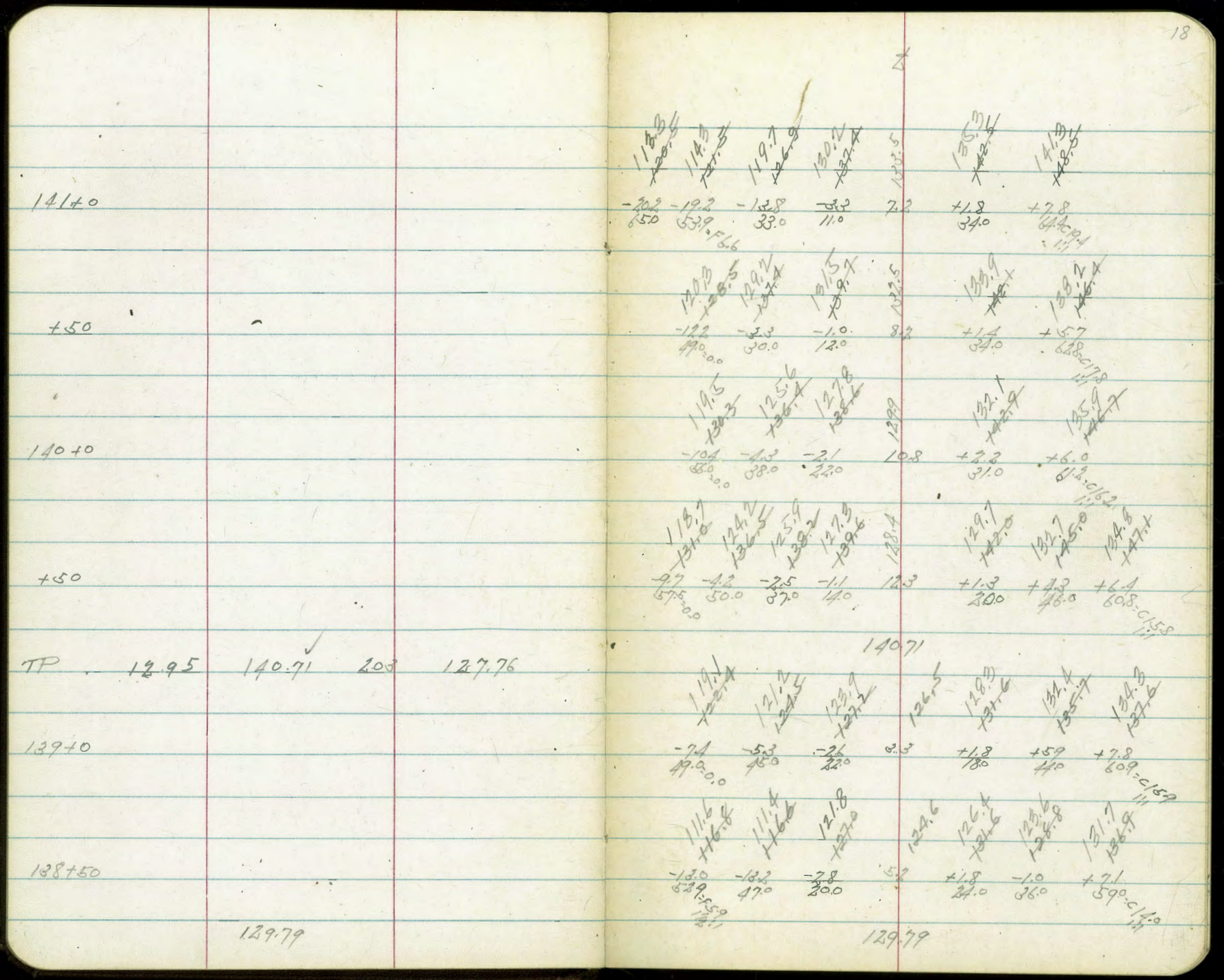
0.7 ℄ Hub 134+06

117.23

108.17

+24				
TP	12.57	129.79 ✓	0.01	117.22
138+0				
137+85				
+50				
137+0				
136+50				
		117.22		

Lt.			℄			Rt
109.6 / 119.2	110.4 / 120.6	119.7 / 129.3	120.2	120.9 / 130.5	127.8 / 137.4	132.5 / 142.1
-10.6 / 55.0	-9.8 / 28.0	-0.5 / 10.0	9.6	+0.7 / 26	+7.6 / 46.0	+12.3 / 66.0
			129.79			
109.1 / 111.2	109.3 / 111.4	112.7 / 114.8	115.1	118.7 / 120.8	123.3 / 127.4	129.5 / 131.6
-6.0 / 55.3 = F7.5 1½:1	-5.8 / 37.0	-2.4 / 19.0	2.1	+3.6 / 13.0	+10.2 / 38.0	+14.4 / 57.8 = C14.8 1½:1
108.4 / 118.8	110.3 / 114.7		112.8	113.4 / 117.8	121.4 / 125.8	125.2 / 129.6
-4.4 / 55.0	-2.5 / 27.0		4.4	+0.6 / 9.0	+8.6 / 23.0	+12.4 / 40.0
						129.1 / 133.5 ; +16.3 / 60.0
108.0 / 115.6	108.2 / 115.8	109.8 / 117.4	109.6	109.8 / 117.4	111.6 / 119.2	116.1 / 123.7
-1.6 / 57.0	-1.4 / 31.0	+0.2 / 10.0	7.6	+0.2 / 13.0	+2.0 / 34.0	+6.5 / 44.0 = 0.0 Berm
106.3 / 116.5	106.5 / 116.7	107.6 / 117.8	107.0	118.0 / 107.8	118.2 / 108.0	119.4 / 109.2
-0.7 / 57.4 = F8.8	-0.5 / 24.0	+0.6 / 17.0	10.2	+0.8 / 16.0	+1.0 / 40.0	+2.2 / 53.0 = 0.0 F6.0
107.4 / 118.5	106.6 / 117.7		106.1	105.8 / 116.9	106.8 / 117.9	107.7 / 118.8 ; ?109.0 / 120.1
+1.3 / 54.7 = F7.1 1½:1	+0.5 / 30.0		11.1	-0.3 / 18.0	+0.7 / 44.0	+1.6 / 66.0 ; +2.9 / 81.0 = 0.0 Graded Area
			117.22			


141+0
+50
140+0
+50
TP 12.95 140.71 203 127.76
139+0
138+50
129.79
140.71
129.79

TP 5.96 134.17 12.20 128.51

143+0

+47.59 BC.1

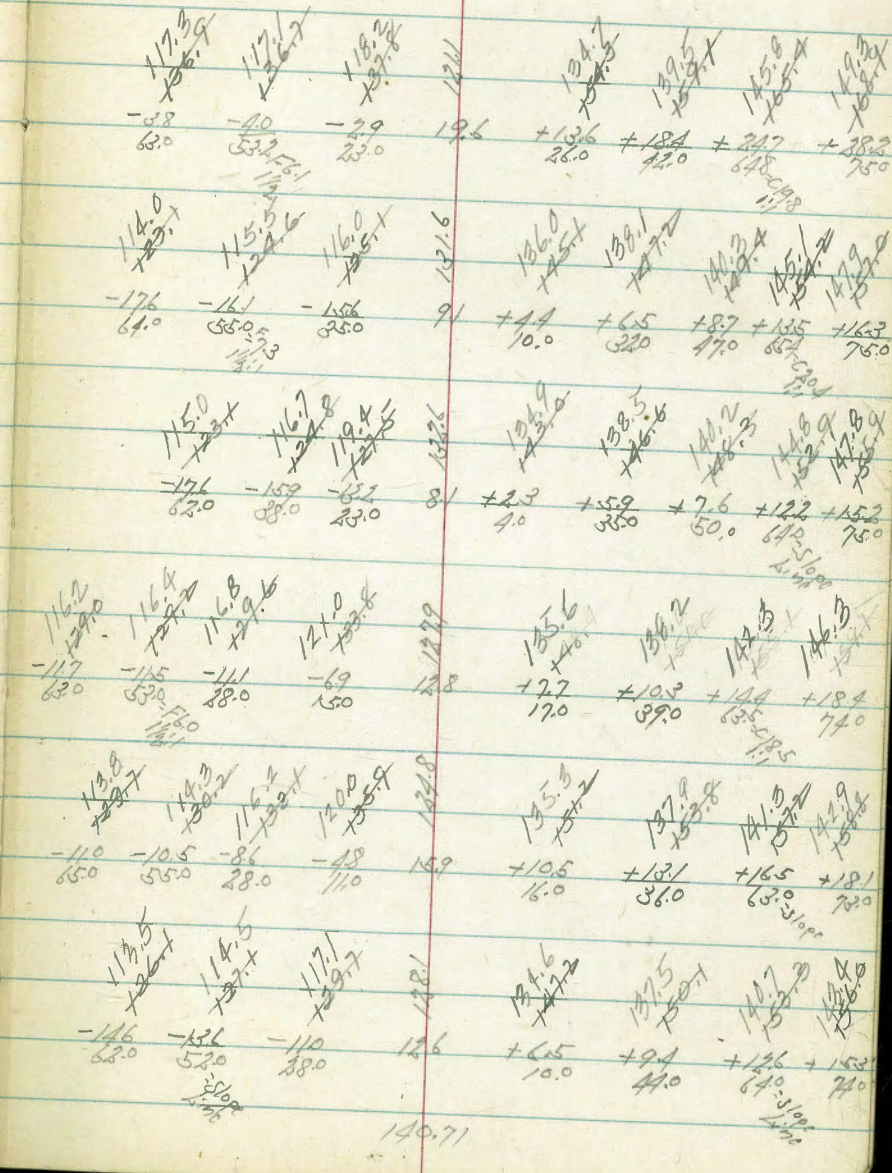
+30

142+0

+65

141+31

140.71



Wabash Blvd. Section "H"

					Lt.	℄	Rt.
TP	13.21	145.53 ✓	2.15	132.32	0 ? ℄ Stub 145+60		
+65 = Bottom Drain on Rt					120.9 −13.2/18.0 · 120.3 −12.8/68 (Slope Line) · 124.0 −9.1/54.0 · 130.1 −3.0/27.0 · 132.3 −0.8/9.0	133.1 1.4	134.9 +1.8/20.0 · 134.3 +1.2/34.0 · 137.1 +4.0/60.0
+25					122.1 −8.2/64 · 122.6 −7.7/58.0 · 124.5 −5.8/44.0 · 127.2 −3.1/24.0	130.3 4.2	132.4 +2.1/12.0 · 142.8 +12.5/40.0 · 149.3 +19.0/57.0 · 151.4 +21.1/67.1 = C 22.1 1:1
145+0					121.9 −5.2/70.0 · 122.4 −4.7/59.2 = F 3.8 4:1 · 123.9 −3.2/44.0 · 124.0 −3.1/22.0	127.1 7.4	131.8 +4.7/16.0 · 141.9 +14.8/40.0 · 150.9 +23.8/60.0 · 154.2 +27.1/70.0 = C 25.0 1:1
+50					121.1 −2.1/72.0 · 120.9 −2.3/62.0 = F 4.5 4:1 · 120.2 −3.0/40.0 · 121.1 −2.1/19.0	123.2 11.3	124.5 +1.3/8.0 · 131.8 +8.6/37.0 · 141.9 +18.7/58.6 = C 13.6 1:1 · 145.3 +22.1/70
144+0					119.3 +0.2/62.0 · 119.4 +0.3/52.0 = F 5.3 1:2:1 · 119.3 +0.2/32.0 · 118.2 −0.9/5.0	119.1 15.4	124.6 +5.5/17.0 · 129.1 +10.0/33.0 · 140.3 +21.2/57.7 = C 12.7 1:1 · 144.6 +25.5/68.0
143+50					117.9 −0.7/63.0 · 117.9 −0.7/53.3 = F 6.2 4:1 · 118.6 0.0/29.0	118.6 15.9	126.3 +7.7/20.0 · 134.0 +15.4/34.0 · 144.6 +26.0/57.0 · 146.9 +28.3/65.0 = C 30.0 1:1 · 149.7 +31.1/75.0
		134.47 ✓				134.47	

For check   6.85   138.68   ✓ 0+25 Stab 148+0 138.7 Ahead

+50

+25

147+0

+75

+50

146+0

145.53

Con't Page 21

−16.7/80.0	−17.6/71.2	−17.9/51.0	−10.6/30.0	−4.2/9.0	5.0	+8.2/30.0	+16.5/40.0	+24.4/60.8	+26.9/68.0
	F6.8 4:1							C23.5 2:1	
−16.9/80.0	−18.1/57.0	−15.9/39.0	−10.5/30.0	−6.0/12.0	5.1	+8.7/20.0	+16.0/37.0	+23.1/54.0	+26.0/64.0
−14.9/80.0	−14.8/70.4	−13.0/42.0	−7.9/34.0	−4.5/15.0	8.2	+14.0/35.0	+19.8/48.0	+23.0/58.7	+26.3/69.0
	F6.6 4:1							C28.4 2:1	
−17.8/70.0	−15.5/46.0	−13.6/44.0	−7.3/20.0	5.7	+11.2/28.0	+18.9/50.0	+26.0/74.0	+28.0/86.0	
−20.6/78.0	−20.0/67.6	−20.0/51.0	−15.3/40.0	−9.2/20.0	3.0	+9.2/20.0	+16.2/33.0	+20.0/53.0	+22.0/70.0
	F5.9 4:1								+24.2/80.0 C35.5 1:1
−17.2/80.0	−17.9/70.4	−15.9/47.0	−10.8/34.0	−4.9/13.0	6.7	+7.7/16.0	+14.6/36.0	+14.0/50.0	+13.4/66.7
	F6.6 4:1								+18.1/74 C21.7 1:1

145.53

Cross Section Wabash Blvd.
Section "H"

Station					
150+0					
+75					
+50					
TP	12.71	156.01	0.00	143.30	
149+0					
+50					
148+0					
TP	12.84	143.30	0.56	130.46	
BM	10.92	131.02		130.10	x on MH Rim 300' Lt 144+0

April 21-50
H Sisson
D Smith
Porer
Chavez
Coto

Lt				℄	Rt				
129.1 / 135.8	133.9 / 139.9	139.3 / 145.4	143.3 / 149.4	149.9	153.3 / 159.6	158.9 / 165.0	164.4 / 170.6	172.9 / 179.0	175.9 / 182.0
-20.2 / 60.0	-16.1 / 50.0 = 0.0	-10.6 / 35.0	-6.6 / 23.0	6.1	+3.6 / 5.0	+9.0 / 23.0	+14.5 / 40.0	+22.0 / 62.8 = C31.5 1/2:1	+21.0 / 72.0
132.1 / 137.5	133.1 / 140.3	141.8 / 139.1		148.7	153.4 / 160.1	159.58 / 166.8	168.4 / 175.7	171.1 / 174.0	
-16.5 / 54.0	-15.5 / 44.0 = 0.0	-6.9 / 11.0		7.3	+4.7 / 17.0	+10.8 / 34.0	+19.7 / 60.8 = 32.6	+23.0 / 72.0	
125.4 / 137.2	126.0 / 137.8	132.8 / 144.6	138.6 / 140.4	144.2	151.4 / 163.2	156.8 / 168.0	159.4 / 171.2	162.3 / 171.4	
-18.8 / 73.2 = F7.3 4:1	-18.2 / 62.0	-11.4 / 41.0 = 0.0	-5.6 / 19.0	11.8	+17.2 / 24.0	+12.0 / 40.0	+15.2 / 56.7 = C24.4	+18.1 / 68.0	
				156.01					
128.6 / 130.4	132.2 / 134.0	135.9 / 137.7		141.5	148.2 / 150.0	154.9 / 155.9	163.6 / 165.4	168.3 / 170.3	
-12.9 / 54.0	-9.3 / 44.0 = 0.0	-5.6 / 22.0		1.8	+6.7 / 19.0	+12.6 / 34.0	+22.1 / 59.1 = C27.1 1/2:1	+27.0 / 72.0	
126.4 / 131.0	126.4 / 131.0	132.0 / 136.6	136.4 / 141.0	138.7	142.2 / 146.8	152.6 / 157.2	162.7 / 167.3	167.8 / 172.4	
-12.3 / 74.0	-12.3 / 64.0 = F5.0 4:1	-6.7 / 33	-2.3 / 10	4.6	+3.5 / 9	+13.9 / 34.0	+24.0 / 59.0 = C28.9 1/2:1	+29.1 / 71.0	
122.6 / 137.2	123.1 / 137.7	126.0 / 130.6	132.9 / 137.5	138.7	147.8 / 152.4	153.5 / 158.1	162.9 / 167.5	168.3 / 173.3	
-16.1 / 84	-15.6 / 74.4 = F7.6 4:1	-12.7 / 52.0	-5.8 / 20	4.6	+9.1 / 25	+14.8 / 59.0	+24.2 / 59.4 = C29.0 1/2:1	+30.0 / 73.0	
				143.30					

For Sta. 47+50 Page 21

2

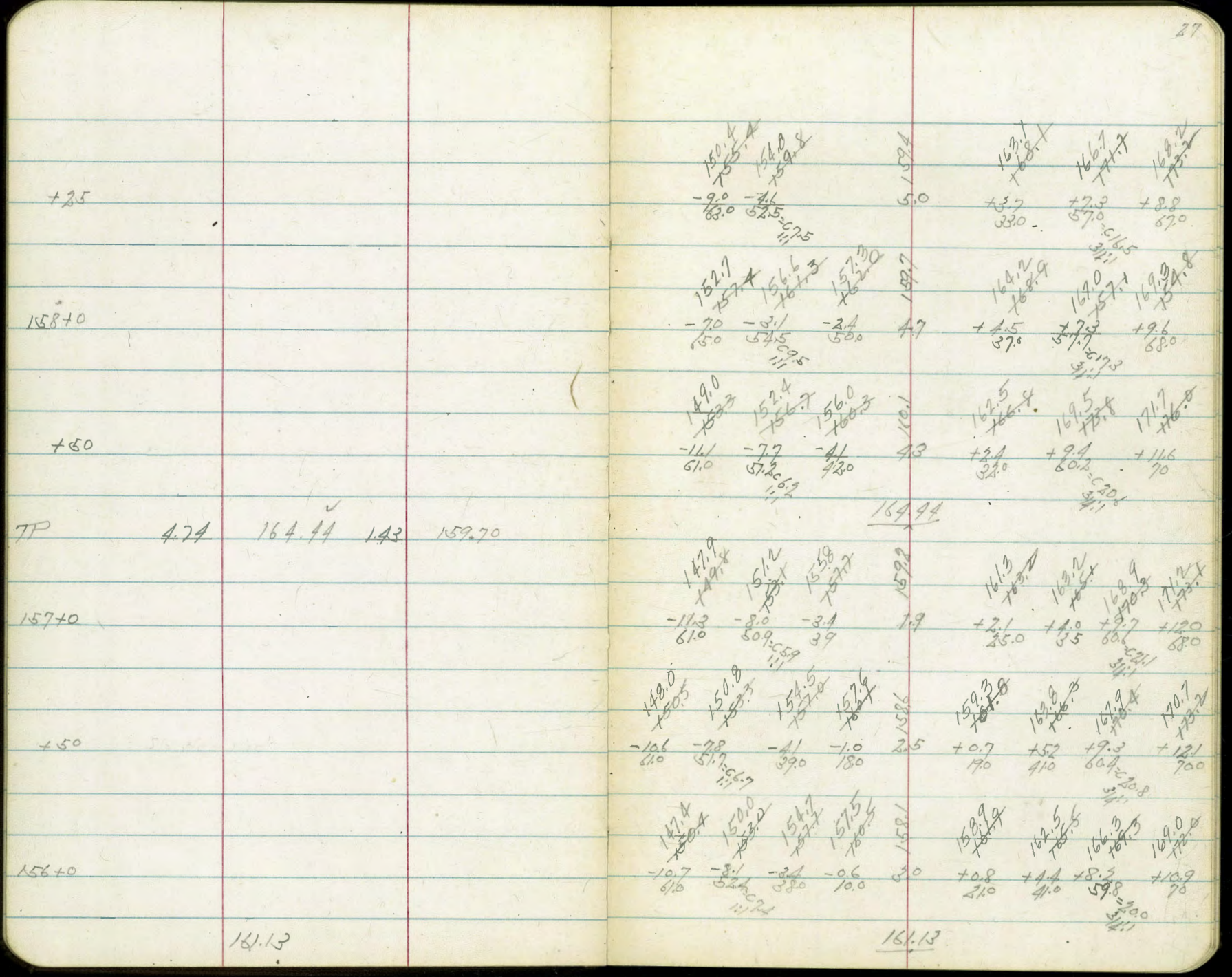
Station								
+50	145.3 / 151.4 -9.7 / 62.0	146.6 / 152.7 -8.4 / 51.5 : C9.0 3/4:1	152.2 / 158.3 -2.8 / 21.0	155.0 6.1	157.5 / 163.6 +2.5 / 19.0	160.2 / 166.3 +5.2 / 37.0	163.0 / 169.1 +8.0 / 55.8 : C22.5 3/4:1	166.5 / 172.6 +11.5 / 66
152+00	144.0 / 151.2 -9.9 / 58.0	144.5 / 151.7 -9.4 / 50.5 : C7.6 3/4:1	147.9 / 155.1 -6.0 / 29.0	150.6 / 157.8 -3.3 / 14.0	153.9 7.2	157.1 / 164.3 +3.2 / 19.0	161.3 / 168.5 +7.4 / 35.0	167.5 / 174.7 +13.6 / 58.5 : C28.0 3/4:1	169.9 / 177.1 +16.0 / 68.0
+50	142.2 / 149.8 -11.3 / 60.0	143.3 / 150.9 -16.2 / 50.2 : C7.3 3/4:1	146.5 / 154.1 -7.0 / 27.0	149.4 / 157.0 -4.1 / 16.0	153.5 7.6	159.5 / 167.1 +6.0 / 17.0	165.2 / 172.8 +11.7 / 41	168.5 / 176.1 +15.0 / 59.4 : C29.8 3/4:1	170.5 / 178.1 +17.0 / 69.0
151+00	140.8 -15.1 / 60.0	142.4 -13.5 / 50.1 : C7.1 3/4:1 Slab out	149.9 -6.0 / 18.0	155.9 5.2	160.9 +5.0 / 20.0	165.4 +9.5 / 41.0	171.4 +15.3 / 61.1 : C33.1 3/4:1	173.5 +17.6 / 71.0
+70	140.1 / 143.9 -17.2 / 60.0	142.7 / 146.5 -14.6 / 48	152.0 / 155.8 -5.3 / 21.0	157.3 3.8	161.6 / 165.4 +4.3 / 21.0	165.7 / 169.5 +8.4 / 40	171.9 / 175.7 +14.6 / 64.0	173.9 / 177.7 +16.6 / 70
150+40	136.1 / 139.9 -21.2 / 39.0	143.6 / 147.4 -13.7 / 42.0	151.0 / 154.8 -6.3 / 19.0	157.3 3.8	162.1 / 165.9 +4.8 / 22.0	166.7 / 170.6 +9.4 / 43.0	172.5 / 176.3 +15.2 / 62.0	174.1 / 177.9 +16.8 / 67

TP	6.26	161.13	1.14	154.87	161.13
			156.01		

+50	151.0 −6.3 / 66.0	153.7 −3.6 / 55.8 =C10.8 1:1	155.0 −2.3 / 45.0	156.6 −0.7 / 24.0	157.3 3.8	159.0 +1.7 / 23.0	163.5 +6.2 / 43.0	165.9 +8.6 / 60.1 =C20.5 3/1:1	166.9 +9.6 / 64.0
155+0	153.0 −5.4 / 60.0	155.0 −3.4 / 54.5 =C13.0 3/1:1	156.1 −2.3 / 43.0	156.5 −1.9 / 28.0	158.4 2.7	159.5 +1.1 / 22.0	162.0 +3.6 / 41.0	163.7 +5.3 / 54.1 =C19.2	165.3 +6.9 / 65.0
+50	155.0 −1.1 / 59.0	154.7 −1.4 / 53.9 =C13.5 3/1:1	155.4 −0.7 / 28.0		156.1 5.0	158.3 +2.2 / 21	160.5 +4.4 / 36.0	163.7 +7.6 / 54.5 =C19.9 3/1:1	166.8 +10.7 / 64.0
154+0	153.8 −2.1 / 65.0	154.3 −1.6 / 55.3 =C14.0 3/1:1	155.0 −0.9 / 21.0		155.9 5.2	157.8 +1.9 / 20.0	160.2 +4.3 / 36.0	165.1 +9.2 / 55.6 =C22.2 1/2:1	167.2 +11.3 / 65.0
+50	153.2 −1.5 / 65.0	153.2 −1.5 / 55.0 =C13.7 3/1:1	153.1 −1.6 / 45.0	153.4 −1.3 / 13.0	154.7 6.4	157.4 +2.7 / 17.0	162.0 +7.3 / 37.0	165.9 +11.2 / 55.4 =C23.8 1/2:1	167.4 +12.7 / 62.0
153+0	150.2 −5.5 / 64.0	151.3 −4.4 / 54.2 =C12.6 3/1:1	153.6 −2.1 / 22.0		155.7 5.4	158.1 +2.4 / 20.0	160.9 +5.2 / 37.0	166.3 +10.6 / 57.0 =C25.0 1/2:1	168.1 +12.4 / 67.0

161.13

161.13


+25
158+0
+50
TP 4.24 164.44 1.43 159.70
157+0
+50
156+0
164.94
164.13
164.13

Wabash Blvd. Section "A"

April 22-50
Saturday

A. Sisson
D. Smith
Rorer
Chavez
Coto

Sta.					Lt.	℄	Rt.
160+0					141.7 / 151.4, −1.2 / 67.0; 141.7 / 151.4, −1.2 / 57.1 =F8.7 1½:1; 142.3 / 152.0, −0.6 / 35.0; 140.9 / 150.6, −2.0 / 15.0	142.9, 9.7	146.3 / 156.0, +3.4 / 30; 151.9 / 161.6, +9.0 / 48.8 =F1.2 4:1; 154.9 / 164.6, +12.0 / 59.0
+65					141.8 / 151.4, −1.2 / 65; 141.2 / 150.8, −1.8 / 56.9 =F8.6; 140.8 / 150.4, −2.2 / 20	143.0, 9.6	148.2 / 157.8, +5.2 / 31; 152.5 / 162.1, 9.5 / 45.0 0.0; 156.5 / 166.1, +13.5 / 55.0
+50					141.7 / 150.7, +.9 / 66.0; 141.5 / 150.4, −2.1 / 56.0 =F8.0; 141.5 / 150.4, −2.1 / 20	143.6, 9.0	153.7 / 162.7, +10.1 / 45.7 =C1.5 4:1; 158.0 / 167.0, +14.4 / 56
159+0					140.5 / 143.8, −8.8 / 66.0; 140.5 / 143.8, −8.8 / 56.3 =F8.2 1½:1; 140.8 / [illegible], −8.5 / 25	143.3, 3.3	159.2 / 162.5, +9.9 / 31.0; 165.0 / 168.3, +15.7 / 55.0 =C13.6 ¾:1; 167.0 / 170.3, +17.7 / 65.0
TP	0.24	152.59	12.09	152.35		152.59	
+75					139.8 / 149.2, −15.2 / 67.0; 139.9 / 149.1, −15.3 / 56.9 =F8.6 1½:1; 145.1 / 154.5, −9.9 / 27.0	155.0, 9.4	160.4 / 169.8, +5.4 / 15.0; 163.3 / 172.7, +8.3 / 36.0; 166.3 / 175.7, +11.3 / 56.2 =C15.3 ¾:1; 167.5 / 176.9, +12.5 / 65.0
158+45					143.4 / 150.9, −12.5 / 60.0; 149.6 / 155.1, −9.3 / 45.0 stake out	158.9, 5.5	163.0 / 168.5, +4.1 / 32.0; 166.1 / 171.6, +7.2 / 56.2 =C15.6 ¾:1; 168.0 / 173.5, +9.1 / 67.0
		164.41				164.44	

+58

TP 7.58 159.81 0.30 152.29

+50

162+0

+50

161+0

160+50

152.59

159.81

152.59

Sta.					Lt.				℄				Rt.
+50					151.1 / 160.0 -2.3 / 67.0	151.3 / 160.2 -2.1 / 56.8 = F9.5 / 3:1	151.8 / 160.2 -1.6 / 35.0	153.2 / 162.1 -0.2 / 15.0	153.4 8.9	153.6 / 162.5 +0.2 / 26.0	154.3 / 163.2 +0.9 / 56.6 = F8.4 / 3:1		154.7 / 163.6 +1.3 / 67.0
165+0					Old Sewer under Const.	152.6 / 160.4 -1.9 / 53.3 = F6.3 / 2:1	152.9 / 160.7 -1.6 / 32.0	154.6 / 162.2 +0.1 / 10.0	154.5 7.8	155.6 / 163.4 +1.1 / 16.0	163.3 / 155.5 +1.0 / 32.0	156.3 / 164.4 +1.8 / 52.1 = F5.4 / 3:1	157.3 / 164.8 +2.5 / 62.0
+50					153.1 / 158.6 -4.1 / 72.0	153.3 / 158.4 -3.9 / 62.0 = F4.5 / 4:1	153.6 / 158.1 -3.6 / 38.0	156.0 / 161.1 -1.2 / 15.0	157.2 5.1	157.4 / 162.5 +0.2 / 26.0	158.8 / 163.8 +1.6 / 52.0 = F3.0 / 4:1		159.2 / 164.3 +2.0 / 62.0
164+0					152.7 / 158.2 -4.1 / 69.0	153.2 / 158.7 -3.6 / 59.2 = F3.5 / 4:1	154.0 / 159.5 -2.8 / 38.0	155.3 / 160.8 -1.5 / 17.0	156.8 5.5	156.6 / 162.1 -0.2 / 25.0	158.4 / 163.9 +1.6 / 50.0 = F1.5 / 4:1		159.8 / 165.3 +3.0 / 55.0
+50					153.8 / 160.0 -2.3 / 62.0	154.0 / 160.2 -2.1 / 52.4 = F2.1 / 4:1	155.2 / 161.4 -0.9 / 33.0	156.05 / 162.7 +0.4 / 16.0	156.1 6.2	156.4 / 162.6 +0.3 / 29.0	156.8 / 163.0 +0.7 / 53.2 = F2.3 / 4:1		155.4 / 161.6 -0.7 / 63.0
B.M.	8.42	162.25	5.98	153.83	L+T M.H 70' Lt. 164+65 153.85				162.25				
163+0					151.3 / 157.8 -2.0 / 69.0	151.3 / 157.8 -2.0 / 59.6 = F3.9 / 2:1	152.5 / 159.0 -0.8 / 40.0	153.8 / 160.3 +0.5 / 18.0	153.3 6.5	152.1 / 158.6 -1.2 / 20.0	151.2 / 157.7 -2.1 / 39.0	150.1 / 156.6 -3.2 / 56.0 = F8.0 / 3:1	151.2 / 157.7 -2.1 / 66.0
		159.81							159.81				

167+0

+75

TP 1267 174.57 0.35 161.90

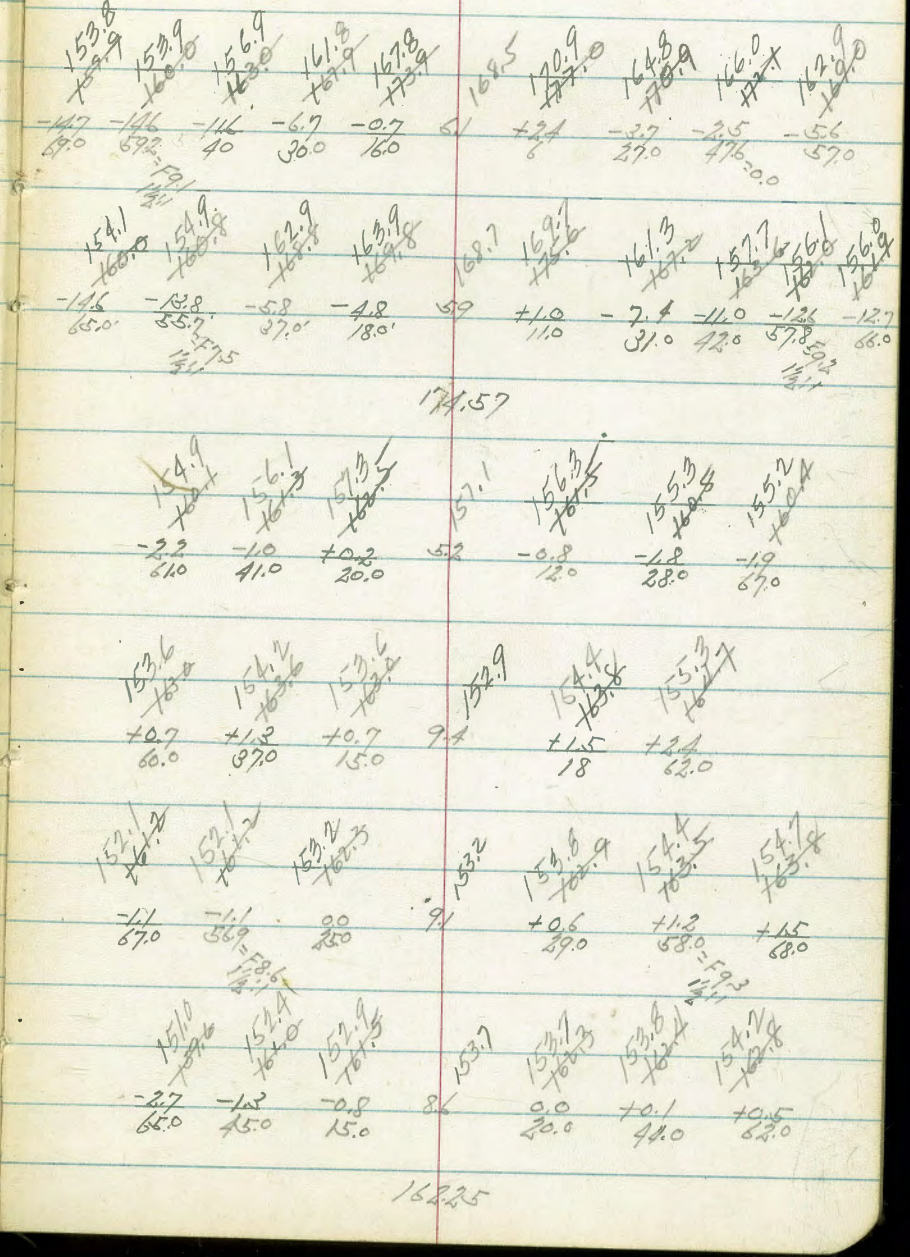
+30

+20

166+0

165+76

162.25



Wabash Blvd. Section "A"

TP	11.72	194.16	2.92	182.44
169+0				
+50				
+31.66 = opp 0-893.48				
168+0				
+50				
TP	11.16	185.36	0.87	174.20
167+25				
	174.57			

Lt — ℄ — Rt

169+0: 155.4, 154.4, 154.7, 156.0, 171.6 | 176.6 | 181.0, 184.8, 186.6
-21.2, -22.2/76.1, -21.9/62.0, -20.6/41.0, -5.0/20.0 | 8.8 | +4.4/25.0, +8.2/53.0, +10.0/71.0 = Slope Line
F 13.4, 13.1

+50: 153.5, 153.4, 154.0, 155.8, 170.5 | 173.8 | 177.8, 183.9, 183.8
-20.5/85.0, -20.4/75.5, -19.8/55.0, -18.0/47.0, -3.3/18.0 | 11.6 | +4.0/24.0, +8.6/49.0, +10.0/76.0
F 13.0

+31.66: 153.8, 153.1, 153.3, 156.7, 170.2 | 174.1 | 176.6, 181.3, 182.4, 182.1
-20.3/85.0, -21.0/74.8, -20.8/60.0, -17.4/47.0, -3.9/20.0 | 11.3 | +2.5/19, +7.7/45, +8.3/68.6 = C 12.6, +8.0/78.0
F 12.8

168+0: 152.9, 152.9, 152.8, 157.9, 170.6 | 172.6 | 178.6, 180.4, 179.9, 170.1
-19.7/83.0, -19.7/72.8, -19.8/60.0, -14.7/45.0, -2.0/20.0 | 12.8 | +6.0/29.0, +7.8/51.0, +7.3/63.0, -2.5/76.0 = 0.0
F 12.2

+50: 153.7, 154.6, 156.8, 167.9 | 173.0 | 175.4, 176.7, 178.0, 168.2
-19.3/74.0, -18.4/64.1, -16.2/50.0, -5.1/22.0 | 12.4 | +2.4/14.0, +3.7/32.0, +5.0/56.0, -4.8/68.0 = 0.0
F 9.4

185.36

167+25: 153.6, 154.1, 156.2, 165.0 | 172.1 | 173.5, 175.5, 172.1, 168.0
-18.5/71.0, -18.0/61.5, -15.9/45.0, -7.0/23.0 | 2.5 | +1.4/17.0, +3.4/44.0, 0.0/59.0, -4.1/70.0 = 0.0
F 9.4, 12.4

174.57

Station					
TP	12.87	166.96	16.28	154.09	on 108 RP 168+31.66 2071-37 154.08
171+0					
TP	0.80	170.37	12.47	169.57	
+50					
TP	1.00	182.04	12.12	181.04	
170+0					
+62					
169+50					

19416

171+0:
160.1 159.4 159.5 160.0 161.3 166.9 177.2 190.5 193.6 195.5
-6.6 -7.3 -7.2 -6.7 -5.4 3.7 +11.1 +23.8 +26.9 +28.8
81.0 5.0 33.0 26 15.0 | 35.0 52.0 75.0 91.0 = Slope Line
Slope Line

170.37

+50:
157.9 157.8 157.9 160.8 169.9 179.5 185.3 188.6 191.3 192.6
-12.0 -12.1 -12.0 -9.1 12.1 +9.6 +15.4 +18.7 +21.1 +22.7
90.0 79.0 21.0 24.0 | 2.0 35.0 45.0 65.0 85.0
Slope Line

182.04

170+0:
157.1 157.0 156.0 163.5 177.1 185.4 188.4 191.0
-20.0 -20.1 -21.1 -13.6 17.1 +8.3 +11.3 +13.9
85.0 77.0 55.0 37.0 | 25.0 52.0 80.0

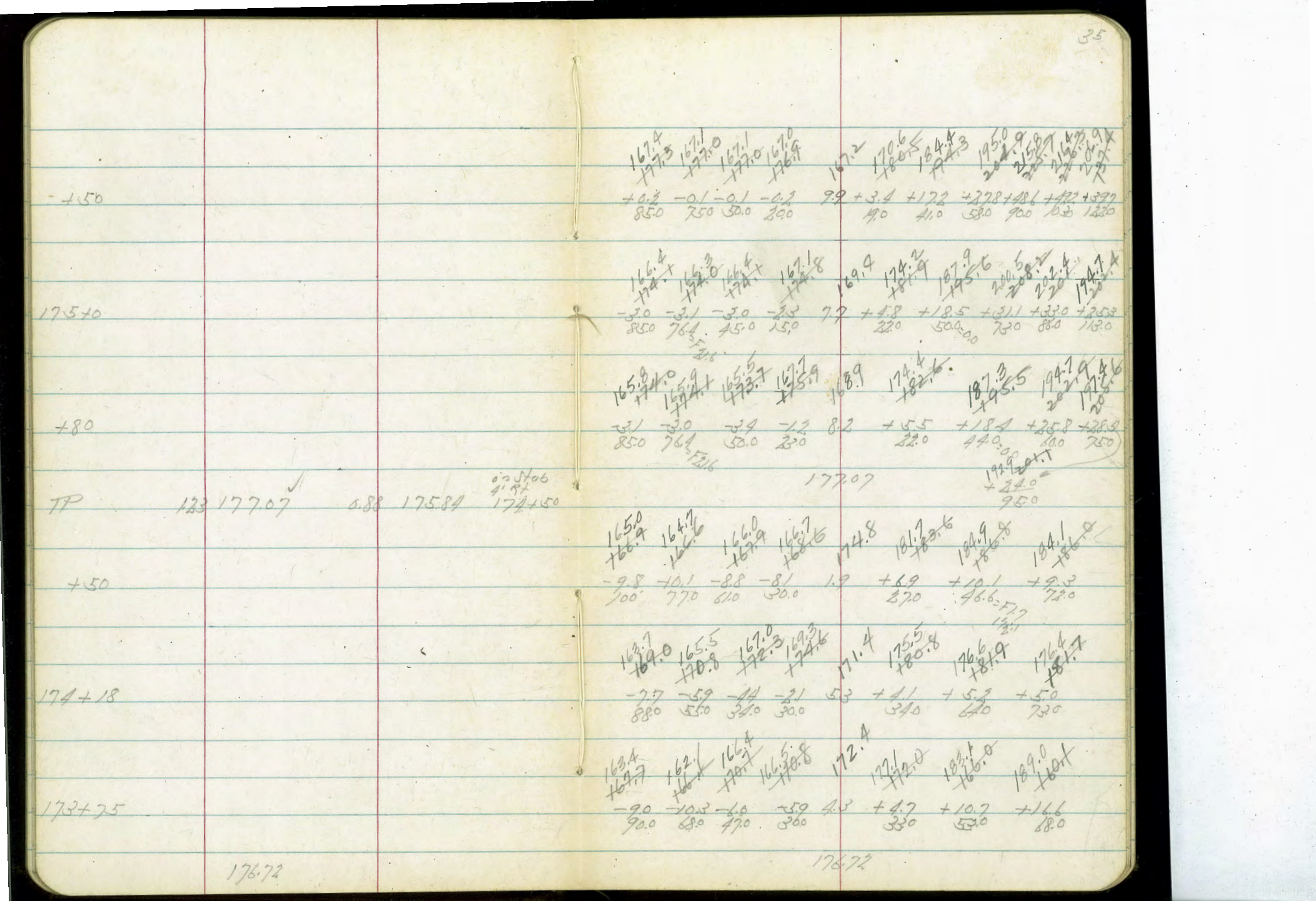
+62:
136.4 155.9 156.5 162.6 169.4 184.0 185.2 188.3 189.8
-27.6 -28.1 -27.5 -21.4 -14.6 10.2 +1.2 +4.2 + 5.8
87.0 77.0 = Slope Line 58.0 48.0 30.0 | 32.0 61 76.0 = Slope Line

169+50:
136.3 155.5 155.9 161.7 169.7 183.1 185.9 185.5 188.3
-26.8 -27.6 -27.2 -21.4 -13.4 11.1 +2.8 +2.4 + 5.7
87.0 76.8 56.0 46.0 30 | 29.0 42.0 76.0 = Slope Line
F 13.7
2.1

19416

+50				
TP	10.75	17672	0.99	16597
173+0				
+50				
172+0				
+75				
+50				
171+89.2° E.C.				
		166.96		

166.96


-150
175+70
+80
TP 123 177.07 0.88 175.84 174+50
+50
174+18
173+75
176.72
177.07
176.72

Wabash Blvd. Section "A"

+18				
177+0				
TP	10.72	197.67 ✓	1.23	186.95
+75				
TP	11.16	188.18 ✓	6.05	177.02
+50 End				
+35				
176+0				
	177.07			

Lt. ℄ Rt.

169.0 ~~172.2~~ 170.2 ~~173.4~~ 186.0 ~~189.2~~ 194.5 219.5 ~~222.7~~ 235.3 ~~238.5~~ 238.2 ~~241.4~~

−25.5 −24.3 −8.5 0.2 +25.0 +40.8 +43.7
78.0 52.0 21.0 45.0 87.0 112.0

170.5 ~~173.9~~ 168.9 ~~172.3~~ 171.6 ~~180.0~~ 189.3 207.6 ~~216.0~~ 232.1 ~~240.5~~ 235.1 ~~243.5~~ 238.5 ~~246.9~~

−18.8 −20.4 −17.7 8.4 +18.3 +42.8 +45.8 +49.3
89.0 79.0 42.0 31 68.0 87.5 109
C42.5

197.67

169.0 ~~174.1~~ 168.8 ~~173.9~~ 169.7 ~~174.4~~ 183.1 198.6 ~~172.7~~ 215.1 ~~220.2~~ 231.2 ~~236.3~~ 235.2 ~~240.3~~

−14.1 −14.3 −13.4 5.1 +15.5 +32.0 +48.1 +52.1
82.0 58.0 26.0 29.0 56.0 77.0 108.0

188.18

168.6 ~~166.8~~ 168.3 ~~168.5~~ 168.2 ~~168.4~~ 169.8 ~~170.0~~ 170.0 ~~170.2~~ 176.9 191.9 ~~178.6~~ 209.2 ~~209.4~~ 226.1 ~~226.9~~ 232.5 ~~232.7~~ 234.2 ~~234.4~~

−8.3 −8.6 −8.7 −7.1 −6.9 0.2 +15.0 +32.3 +49.8 +55.6 +57.3
90.0 78.7 65.0 45.0 17.0 22.0 58 80.1 91.0 121.0
F23.1 C35.1

168.4 ~~174.5~~ 168.4 ~~174.3~~ 169.7 ~~175.6~~ 168.8 ~~174.7~~ 171.2 173.0 ~~175.3~~ 183.4 ~~189.3~~ 192.5 ~~198.4~~ 214.2 ~~220.1~~ 225.0 ~~230.9~~ 231.8 ~~237.7~~ 233.9 ~~239.8~~

−2.8 −2.8 −1.5 −2.4 5.9 +1.8 +12.2 +21.3 +43.0 +53.8 +60.6 +62.7
85 75 45 15 8 17.0 40.0 65.0 84.0 96.0 117.0

168.0 ~~175.7~~ 168.2 ~~175.9~~ 168.9 ~~176.6~~ 168.0 ~~175.7~~ 169.4 174.9 ~~182.6~~ 191.4 ~~199.1~~ 209.4 ~~217.1~~ 226.3 ~~234.0~~ 226.8 ~~234.5~~ 224.0 ~~231.7~~

−1.4 −1.2 −0.5 −1.4 7.7 +5.5 +22.0 +40.0 +56.9 +57.4 +54.6
85.0 75.0 47.0 25.0 15.0 45.0 76.0 104.0 125.0 150.0

177.07

Rhodes Arc
Used on Rt.

+50

173.7 ~~182.0~~	173.7 ~~182.6~~	175.3 ~~183.6~~	184.0 ~~192.3~~	189.4	198.1 ~~206.4~~	210.5 ~~218.8~~	215.1 ~~223.4~~
-15.7	-15.7	-14.1	-5.4	8.3	+8.7	+21.1	+25.7
98.0	86.5 = F21.5 81.7	50.0	19.0		25.0	59.8 = C15.1 60.1 1:1	85.0

179+0

172.9 ~~181.6~~	172.2 ~~180.9~~	173.7 ~~182.4~~	184.0 ~~192.7~~	189.0	200.5 ~~209.2~~	210.2 ~~218.9~~	215.9 ~~224.6~~
-16.1	-16.8	-15.3	-5.0	8.7	+11.5	+21.2	+26.9
98.0	83.3 = F22.4 80.6	62.0	25.0		36.0	60.8 = C15.3 60.3 1:1	72.0

+50

171.9 ~~179.7~~	172.6 ~~180.4~~	178.8 ~~186.6~~	180.9 ~~188.7~~	189.9	198.8 ~~206.6~~	217.0 ~~224.8~~	220.0 ~~227.8~~	236.0 ~~243.8~~
-18.0	-17.3	-11.1	-9.0	7.8	+8.9	+27.1	+30.1	+46.1
98.0	79.7 = F22.0 78.2	48.0	39.0		23.0	42.0	70.3 = C25.4 1:1	85.0

178+0

169.7 ~~175.7~~	170.4 ~~176.4~~	172.5 ~~178.5~~	179.6 ~~185.6~~	186.3 ~~192.3~~	191.7	203.7 ~~209.7~~	214.4 ~~220.4~~	228.0 ~~234.0~~	233.7 ~~240.0~~
-22.0	-21.3	-19.2	-12.1	-5.4	6.0	+12.0	+22.7	+36.3	+42.0
94.0	83.0	75.8 = F31.0 Lt Lane	51.0	19.0		30.0	52.0	79.0 = C34.2 1:1 79.2	91.0

+50

170.1 ~~171.5~~	169.7 ~~171.1~~	170.2 ~~171.6~~	182.1 ~~183.5~~	188.8 ~~190.2~~	196.3	212.3 ~~213.9~~	221.0 ~~223.4~~	235.9 ~~237.3~~
-21.2	-21.6	-21.1	-14.2	-7.5	1.4	+16.0	+25.7	+39.6
93.0	79.5 = F23.4	66.0	36.0	14.0		33.0	56.0	91.6 on R.P.

177+39.46

170.0 ~~170.6~~	170.1 ~~170.7~~	184.6 ~~185.2~~	197.1	211.8 ~~213.4~~	221.6 ~~222.2~~	235.1 ~~236.7~~
-27.1	-27.0	-12.5	8.6	+14.7	+24.5	+58.0
82.0	65.0	28.0		30.0	53.0	87.0

197.67

197.67

Wabash Blvd Sec. "A" Right Lane

Sta.					
182+0					
+80.03 B.C. Rt. Lane					
TP	.581	212.17	1.57	206.36	on Hub C℄
+50					
181+0					
+50					
TP	10.98	207.93	0.72	196.95	
180+0					
		197.67			

Lt. ℄ Rt.

178.0 / 179.6, 182.4 / 184.0, 188.6 / 190.2, 199.9 / 201.5, 210.6, 217.7 / 219.3, 230.7 / 232.3, 240.2 / 241.9, 233.6 / 235.2

−22.6 / 115 = Slope Line, −28.2 / 96.0, −22.0 / 61.0, −10.7 / 28.0, 1.6, +7.1 / 22.0, +20.1 / 58.0, +29.6 / 88.4 = C44.3 1:1, +23.0 / 94.0 in RR Cut

178.4 / 181.8, 181.5 / 184.9, 187.8 / 191.2, 196.6 / 200.0, 204.9 / 208.3, 208.8, 222.0 / 225.4, 230.8 / 234.2, 240.6 / 244.0

−30.4 / 116.0, −27.3 / 96.0, −21.0 / 57.0, −12.2 / 33.0, −3.9 / 14.0, 3.4, +13.2 / 32.0, +22.0 / 57.0, +31.8 / 84.7

212.17

178.2 / 180.9, 178.3 / 181.0, 184.0 / 186.7, 188.7 / 191.4, 198.2 / 200.9, 205.7, 215.2 / 217.9, 227.7 / 230.4, 238.2 / 240.9, 233.3 / 236.0

−27.0 / 107, −26.9 / 100, −21.2 / 79.0, −16.5 / 48.0, −7.0 / 21.0, 2.7, +10.0 / 25.0, +22.5 / 53.0, +33.0 / 87.2 = C42.2 1:1, +28.1 / 92.2

177.0 / 184.3, 177.3 / 184.6, 181.6 / 188.9, 185.3 / 192.6, 190.6 / 197.9, 200.6, 216.7 / 224.0, 226.1 / 233.4, 233.8 / 241.1, 238.4 / 245.7

−23.6 / 110.0, −23.3 / 96.0, −19.0 / 87.0, −15.3 / 63.0, −10.0 / 30.0, 7.3, +16.1 / 37.0, +25.5 / 65.0, +33.2 / 83.1 C37.8 1:1, +37.8 / 83.0

176.3 / 186.3, 176.4 / 186.4, 179.5 / 189.5, 188.1 / 198.1, 197.9, 207.0 / 217.0, 220.9 / 230.9, 235.1 / 245.1, 235.4 / 245.4

−21.6 / 98.0, −21.5 / 85.0, −18.4 / 59.0, −9.8 / 27.0, 10.0, +9.1 / 21.0, +23.0 / 50.0, +37.2 / 84.1 C39.2 1:1, +37.5 / 91.0

207.93

175.0 / 178.7, 175.4 / 179.1, 175.9 / 179.6, 185.1 / 188.8, 187.9 / 191.6, 194.0, 202.3 / 206.0, 211.1 / 214.8, 222.0 / 225.7, 231.7 / 235.4

−19.0 / 98.0, −18.6 / 87.0 Slope Line, −18.1 / 56.0, −8.9 / 29.0, −6.1 / 17.0, 3.7, +8.3 / 29.0, +17.1 / 50.0, +28.0 / 71.0 = C26.1 1:1, +37.7 / 95.0

197.67

Right Lane

+50

+40

+14

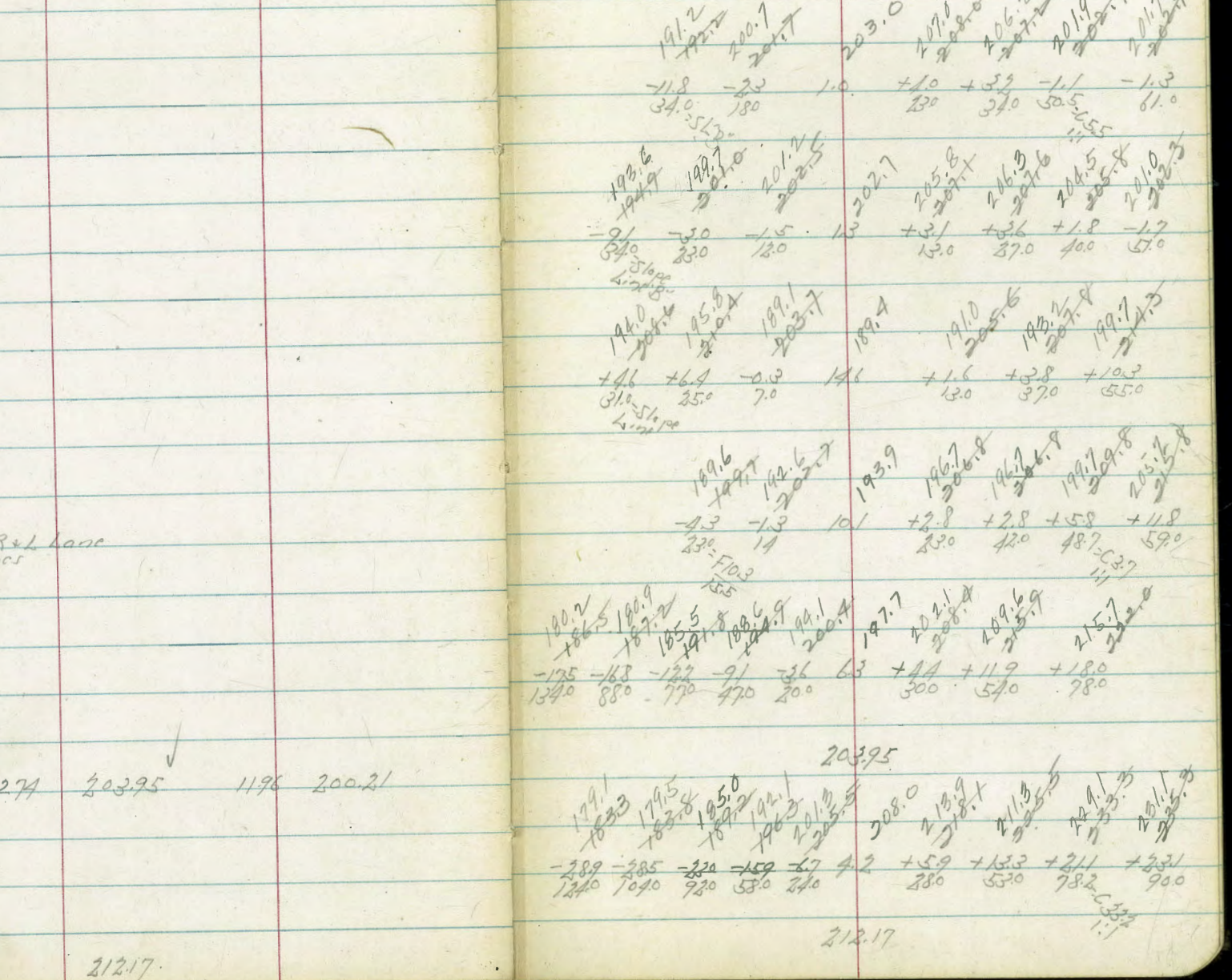
183+0 = Jct. R+L Lane slopes

+82

TP 2.74 203.95 11.96 200.21

182+50

212.17



Wabash Blvd. Section "H"
Right Lane

Rhodes
Aic
Used on Rt

May 30 - 50
Saturday
T. Sisson
O. Smith
Rorer
Chavez
Coto

186+0 — 186.7 / 194.4, 186.7 / 194.4, 186.5 / 194.2, 190.1, 207.3 / 215.0, 224.1 / 232.4, 226.0 / 233.9, 227.7 / 235.4
-3.4 / 53.0, -3.4 / 26.0, -3.6 / 6.0, 7.7, +17.2 / 25.0, +34.6 / 52.0, +35.9 / 72.8, +37.6 / 87.0

+50 — 185.5 / 188.0, 185.5 / 188.0, 184.4 / 186.9, 186.4 / 188.9, 195.3, 205.8 / 208.3, 215.3 / 217.8, 226.4 / 228.9, 226.9 / 229.4
-9.8 / 50.0 (Slope Lim), -9.8 / 39.0, -10.9 / 24.0, -8.9 / 15.0, 2.5, +10.5 / 18.0, +20.0 / 38.0, +31.1 / 51.0, +31.6 / 74.2

164 | 196 [16] ℄ stub 185+00

197 [80]

BM | 8 [81] | 197 [80] | 188 [99] | 187 2 top 185+90 (Let on MH) — 228.1 / 236.5, 226.2 / 234.0; +32.5 / 76.5, +30.0 / 87.0

185+0 — 184.4 / 192.2, 184.4 / 192.2, 196.2, 207.4 / 215.2, 214.2 / 222.0, 218.5 / 226.3, 228.5 / 236.3
-11.8 / 53.0, -11.8 / 25.0, 7.8, +11.2 / 19.0, +18.0 / 34.0, +22.3 / 45.0, +32.3 / 66.0

+50 — 184.1 / 190.3, 185.2 / 191.4, 197.8, 204.5 / 210.7, 212.8 / 219.0, 225.4 / 231.6, 227.0 / 233.2
-13.7 / 43.0 SL, -12.6 / 22.0, 6.2, +6.7 / 13.0, +15.0 / 38.0, +27.6 / 72.8, +29.2 / 83.0

184+0 — 188.7 / 189.7, 191.9 / 192.9, 199.8 / 200.8, 203.0, 208.0 / 209.0, 210.0 / 211.0, 212.9 / 213.9, 215.0 / 216.0
-14.3 / 37.0 SL, -11.1 / 33.0, -3.2 / 21.0, 1.0, +5.0 / 24.0, +7.0 / 42.0, +9.9 / 61.2, +12.0 / 74.0

203.95 | 203.95

Right Loop

189+0

+60

+30

TP 12.46 210.23 0.03 197.77

188+0

+50

187+0

186+50

197 80

210 23

197 80

Right Lane

+75

222.3 227.3 · 224.3 229.1 · 229.1 · 242.7 247.5 · 254.9 259.7 · 267.9 272.7 · 271.9 276.7

-1.6 · -4.8 · 4.8 · +13.6 · +25.8 · +38.8 · +42.8
36.0 · 13.5 · 31.0 · 58.0 · 91.7 · 102.0
C 6.5 1:1 · C 54.5 3:1

+50

212.3 220.5 · 217.6 225.7 · 221.8 230.0 · 222.8 231.0 · 225.7 · 236.1 244.9 · 249.2 257.4 · 259.1 267.9 · 266.4 274.6 · 271.7 279.9

-13.4 · -8.2 · -3.9 · -2.9 · 8.2 · +11.0 · +23.5 · +34.0 · +40.7 · +46.0
50.0 · 38.4 · 24.0 · 9.0 · 27.0 · 49.0 · 68.0 · 91.0 · 101.0
C 9.6 1:1 · C 41.6 3:1

+38.93 P.O.C. Mid Point

22.87
10.99
on Hub

190+0

203.7 215.0 · 207.5 218.8 · 221.6 231.9 · 222.6 · 223.7 235.0 · 240.4 251.7 · 252.7 264.0 · 260.0 271.3 · 265.7 277.0

-18.9 · -15.1 · -1.0 · 11.3 · +1.1 · +17.8 · +30.1 · +37.4 · +43.1
51.0 · 37.6 · 8.0 · 19.0 · 52.0 · 70.0 · 86.8 · 97.0
0.0 · C 55.1 3:1

TP 12.35 233.86 ✓ 0.81 221.51 P.O.C. Hub 189+75

233.86

+75 P.O.C.

202.5 203.3 · 206.4 207.2 · 221.3 · 224.4 225.2 · 237.2 238.0 · 241.5 242.3 · 259.3 260.1

-19.0 · -15.1 · 0.81 · +2.9 · +15.7 · +20.0 · +37.8
46.0 · 36.0 · on Hub · 23.0 · 49.0 · 68.0 · 87.0

189+50

202.1 209.8 · 204.9 212.0 · 208.0 215.1 · 215.2 · 224.1 231.2 · 227.8 234.9 · 237.2 244.3 · 257.0 264.1 · 259.0 266.1

-12.5 · -10.3 · -7.2 · 7.1 · +8.9 · +12.6 · +22.0 · +41.8 · +42.8
36.0 · 22.0 · 16.0 · 15.0 · 34.0 · 51.0 · 85.3 · 90.0
0.0 · C 54.0 3:1

TP 12.61 222.32 ✓ 0.52 209.71

222.32

Right Lane

+50				
192+0				
+75 P.C.				
TP	9.81	267.66	0.38	257.85
+50				
TP	12.72	258.23	0.15	245.51
TP	11.96	245.66	0.16	233.70
191+0				
		233.86		

235.8 / 246.3 241.3 / 251.8 257.2 268.0 / 278.5 275.2 / 285.7 279.9 / 290.4 282.5 / 293.0 283.7 / 294.2

−21.4 / 39.0 −15.9 / 27.2 = C 30.2 / 1:1 10.5 +10.8 / 18.0 +18.0 / 35.0 +22.7 / 60.0 +25.3 / 81.2 = C 73.4 / 3:1 +26.5 / 92.0

239.5 / 243.6 244.7 / 249.0 254.4 / 258.7 263.4 268.4 / 272.7 273.3 / 277.6 278.7 / 282.8 280.0 / 284.3

−24.1 / 41.0 −18.7 / 31.4 = C 34.4 / 1:1 −9.0 / 18.0 4.3 +5.0 / 19.0 +9.9 / 49.0 +14.8 / 79.2 = C 70.3 / 3:1 +16.6 / 90.0

233.8 / 238.7 241.4 / 246.3 245.7 / 250.6 254.8 / 259.7 262.8 267.1 / 272.0 270.9 / 275.8 275.8 / 280.7

−29.0 / 42.0 −21.4 / 31.0 −12.1 / 24.0 −8.0 / 19.0 4.9 +4.3 / 21.0 +8.1 / 49.0 +13.0 / 78.0

267.66

237.7 / 239.6 243.3 / 245.2 250.5 / 252.4 256.3 258.3 / 260.2 262.3 / 264.2 267.8 / 269.7 270.3 / 272.2

−18.6 / 41.0 −13.0 / 31.0 = C 34.0 / 1:1 −5.8 / 16.0 1.9 +2.0 / 17.0 +6.0 / 40.0 +11.5 / 75.0 = C 61.0 / 3:1 +14.0 / 86.0

258.23

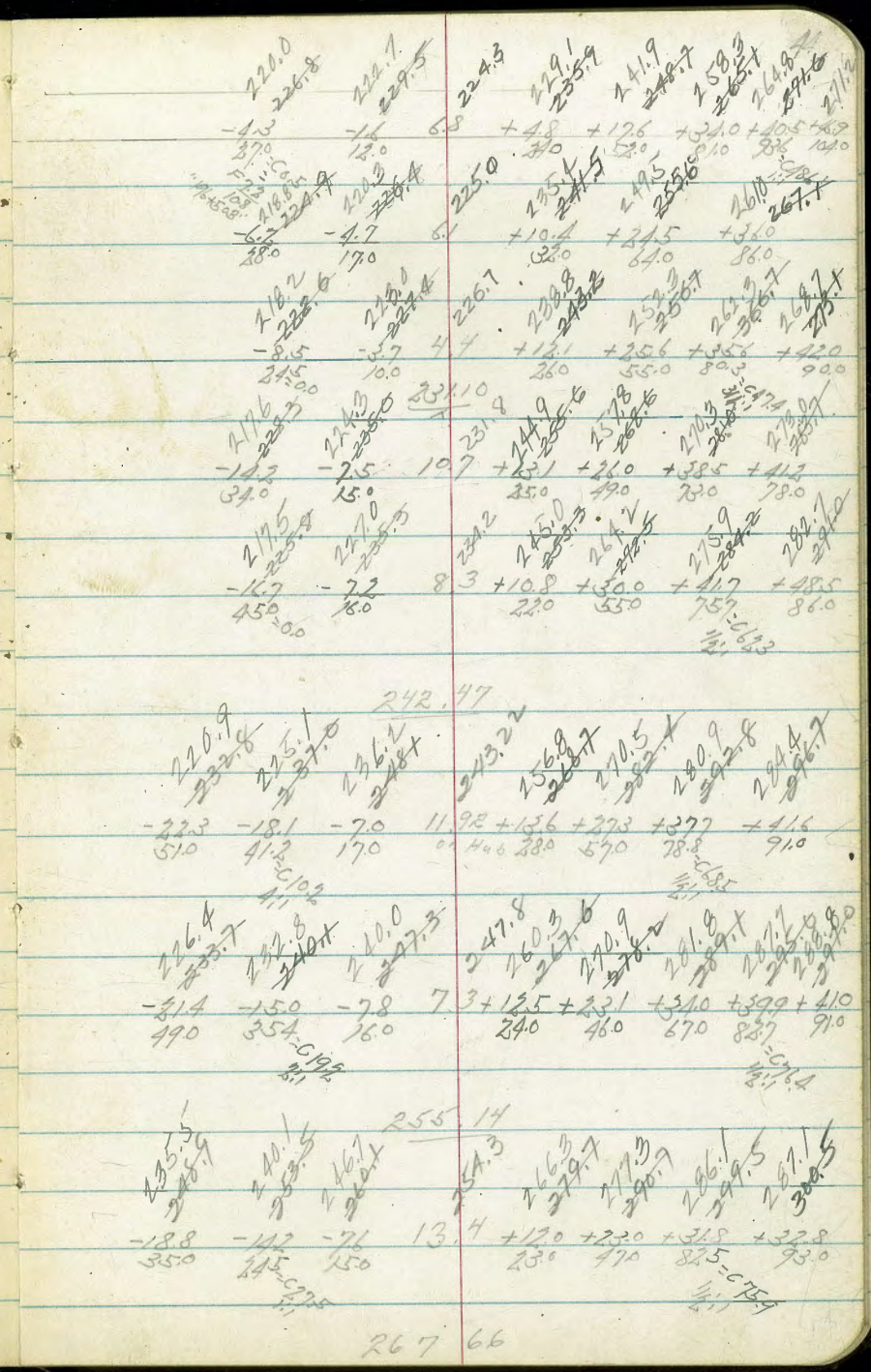
226.4 / 228.9 231.7 / 233.4 231.7 235.7 / 237.4 241.7 / 243.9 257.9 / 260.1 260.3 / 262.5 264.5 / 266.7

−5.0 / 35.0 −0.5 / 20.0 = C 23.0 / 1:1 2.2 +4.0 / 31.0 +10.0 / 50.0 +21.2 / 72.0 +28.6 / 85.6 = C 54.5 / 3:1 +32.8 / 96.0

233.86

Right Lane

1+50				
1+25				
1+00				
TP	1.84	231.10	13.21	229.26
0+75				
0+50				
TP	0.16	242.47	12.83	242.31
0+00	P.O.C.			
0+50				
TP	0.86	255.14	13.37	254.29
-0+25				
		267.66		



Right Lane

+50

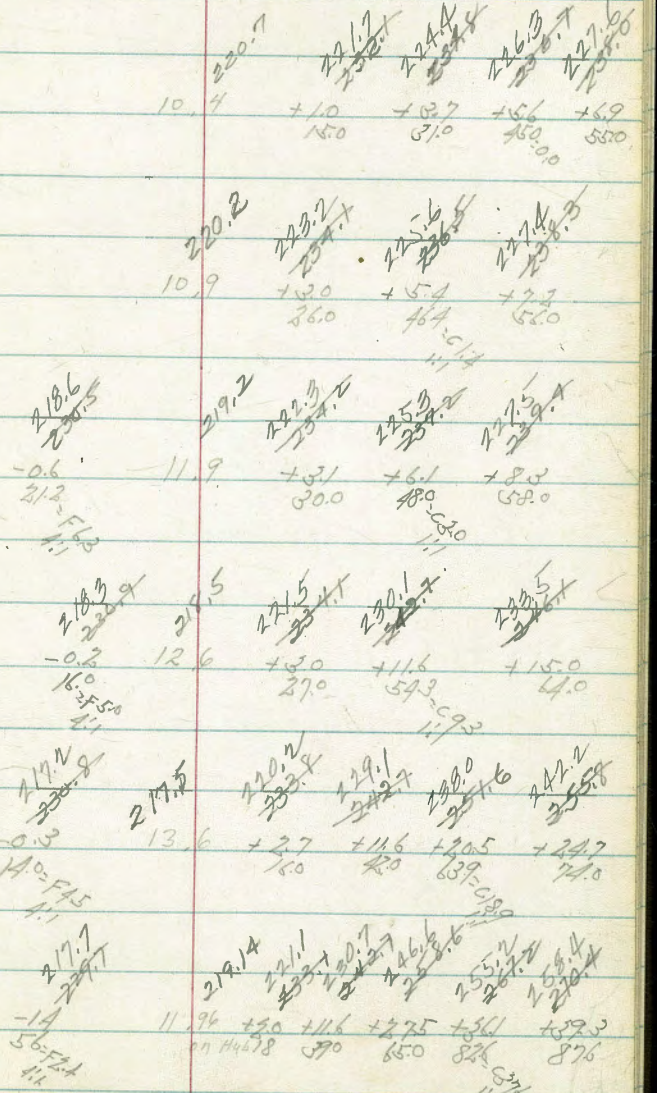
198+0

+50

197+0

+50

196+0 P.O.C.



231.10

231.10

TP			2.32	231.53	rim MH. 25' Lt 201+53 Rt slope stak
TP	8.28	233.85	5.53	225.57	198+00

199+13 [26]
=s
198+97 83 E.C. "A" Line

FB 2071-66
231.48

224.3 ~~234.5~~ 224.1 ~~234.3~~ 223.3 ~~233.5~~ 220.92 222.8 ~~233.0~~ 226.1 ~~236.9~~ 228.5 ~~238.7~~ 230.3 ~~240.5~~

+3.4 64.0 | +3.2 53.8 | +7.4 22.0 | 10.18 on Hub | +1.9 24.0 | +5.8 35.0 | +7.6 47.0 | +9.4 57.0

= F 6.5 [illegible]

0.0

231.10

231.10

Cross Section Wabash Blvd & Wabash Ave.
Left Lane "B" Line

May 22 '50
A. Sisson
O. Smith
Rorer
Chavez
Coto

Lt ℄ Rt

185+0
185.4 197.6 186.0 197.9 186.1 198.0 185.2 197.1 185.2 197.1 184.4 184.1 196.0 184.5 196.4
+1.3 +1.6 +1.7 +0.8 +0.8 11.9 -0.3 +0.1
120.0 110.0 96.0 62.0 31.0 14.0 25.4 = F19.6
SL 29.4

+50
185.2 198.7 185.4 198.9 185.5 199.0 183.8 197.3 183.2 196.7 182.8 183.9 197.4 184.7 198.2
+2.4 +2.6 +2.7 +1.0 +0.4 13.5 +1.1 +1.9
116.0 106.0 95.0 57.0 25.0 13.0 23.3 = F18.1
SL 27.3

184+0
183.5 197.8 183.0 197.3 182.3 196.6 182.5 196.8 181.4 195.7 182.0 182.9 197.2 188.5 202.8
+1.5 +1.0 +0.3 +0.5 -0.6 14.3 +0.9 +6.5
114.0 104.0 75.0 45.0 20.0 7.0 15.0 = F13.5
19.8

+50
188.8 191.6 187.7 190.5 186.7 189.5 188.0 190.8 193.5 197.7 200.5
-4.7 -5.8 -6.8 -5.5 2.8 +4.2
110 100.0 46.0 14.0 9.5 = F9.0
SL

+25
180.8 183.6 180.1 182.9 180.0 182.8 181.0 183.8 187.2 190.0 187.4 190.2 192.3 195.1 193.5 194.3 197.1
-12.7 -13.4 -12.5 -12.5 -6.3 -6.1 -1.5 2.8 +0.8
112.0 102.0 72.0 42.0 26.0 16.0 9.0 49 = F5.9
SL 13.1

183+0
180.6 188.8 179.5 187.1 180.5 188.1 184.5 192.1 187.2 194.8 188.7 187.4 195.0 189.6 197.8
-8.1 -9.2 -8.2 -4.2 -1.5 7.6 -1.3 +0.9
107 99.0 57.0 37.0 15.0 6.0 11.5
Top

BM 7.33 196.32 188.99 L+T M.H. 167.68 Lt. 185+95 "B" 196.32

Left Lane "B" Line

Station				Cross-section readings
188+0				190.4/196.7 0.0/100 · 192.4/198.7 +2.0/84.2 · 191.7/198.0 +1.3/56.0 · 191.8/198.1 +1.4/50.0 · 190.4/196.7 0.0/16.0 · 190.4 6.3 · 191.0/197.3 +0.6/11.0 · 190.8/199.1 +0.4/32.6 = F24.4, 1½:1 · 191.7/198.0 +1.3/5.0
+50				192.8/199.4 +2.7/100.0 · 190.9/197.5 +0.8/83.3 F26.3, 1½:1 · 189.7/196.3 -0.4/41.0 · 189.7/196.3 -0.4/22.0 · 190.1 6.6 · 190.4/197.0 +0.3/17.0 · 190.0/196.6 -0.1/30.8 F23.2, 34.8 · 189.9/196.2 -0.3/95.0
187+0			190.5/197.8 +1.1/95.0	190.7/198.0 +1.3/80.6 = F24.4 · 189.8/197.1 +0.4/60.0 · 188.2/195.5 -1.3/32.0 · 188.7/196.0 -0.7/12.0 · 189.4 7.3 · 189.1/196.4 -0.3/18.0 · 189.1/196.4 -0.3/29.0 = F23.0
+50				188.8/199.9 +1.3/90.0 · 188.1/197.2 +0.5/75.3 = F24.2 · 187.6/196.7 0.0/43.0 · 187.3/196.3 -0.3/19.0 · 187.6 9.1 · 187.9/197.0 +0.3/17.0 · 187.6/196.7 0.0/28.0 = F21.3, 32.0
186+0				189.1/199.8 +2.1/90.0 · 188.1/198.8 +2.1/70.7 = F21.8, 1½:1 · 187.6/198.3 +1.6/47 · 186.7/197.4 +0.7/21.0 · 186.0 10.7 · 187.1/197.8 +1.1/11.0 · 186.6/197.3 +0.6/26.8 = F20.5, 30.8, 1½
TP	7.67	196.66	7.33 188.99	L+TMH Lt 185+85 · 196.66
185+50				185.7/196.8 +0.5/81.0 · 185.9/197.0 +0.7/71.0 = F22.0, 1½:1 · 186.1/197.2 +0.9/45.0 · 186.2/197.3 +1.0/17.0 · 185.2 11.1 · 185.4/196.5 +0.3/26.2 = F20.1, 30.2, 1½:1

19632 · 19632

Left Lane "B" Line

Station	B.S.	H.I.	F.S.	Elev.	Lt	℄	Rt
TP	13.25	212.78 ✓	1.02	200.53			
190+81.60						198.1 / 3.5	197.3 ~~200.8~~ −0.8 / 20.0; 198.0 ~~201.5~~ −0.1 / 34.3 = F25.5 38.3
+90.37							
+50					~~200.8~~ 193.4 −0.8 / 100; 195.4 ~~202.8~~ +1.2 / 87.2 = F28.8; 196.2 ~~203.6~~ +2.0 / 65.0; 194.4 ~~201.8~~ +0.2 / 60.0; 194.4 ~~201.8~~ +0.2 / 20	194.2 / 7.4	194.7 ~~202.1~~ +0.5 / 21; 195.1 ~~202.5~~ +0.9 / 34.0 = Slope Line; 195.3 ~~202.7~~ +1.1 / 50.0
TP	7.22	201.55 ✓	2.43	194.23		201.55	
189+0					192.0 ~~195.4~~ −1.0 / 100.0; 194.6 ~~198.3~~ +1.6 / 86.2 = F28.1; 194.8 ~~198.5~~ +1.8 / 72.0; 194.6 ~~198.3~~ +1.6 / 55.0; 192.8 ~~196.5~~ −0.2 / 22.0	193.0 / 3.7	192.2 ~~196.9~~ +0.2 / 17; 193.6 ~~197.3~~ +0.6 / 33.7 = F25.1; 195.5 ~~199.2~~ +0.5 / 50.0
188+50					190.9 ~~195.5~~ −1.2 / 100.0; 192.5 ~~197.1~~ +0.4 / 86.8 = F28.5 1½:1; 193.6 ~~198.2~~ +1.5 / 65.0; 193.4 ~~198.0~~ +1.3 / 45.0; ~~196.6~~ 192.0 −0.1 / 20	192.1 / 4.6	191.8 ~~196.4~~ −0.3 / 18.0; 192.2 ~~196.8~~ +0.1 / 33.2 = F24.8 1½:1; 192.4 ~~197.0~~ +0.3 / 52.0

196.66

196.66

Left Lane "B" Line

Station		Lt				℄	Rt		
+50		206.8 ~~214.4~~ +0.6 / 95.0	206.0 ~~213.6~~ −0.2 / 81.1 = F24.9 1:2.1	205.8 ~~213.4~~ −0.4 / 67.0	205.9 ~~213.5~~ −0.3 / 25.0	206.2 7.6	211.3 ~~218.9~~ +5.1 / 19.2 = F15.4	215.8 ~~223.4~~ +9.6 / 29.0	
193+0	205.6 ~~213.x~~ −0.4 / 100.0	204.1 ~~211.4~~ −1.9 / 83.3 = F26.2	204.9 ~~212.7~~ −1.1 / 67.0	204.3 ~~212.1~~ −1.7 / 41.0	203.4 ~~211.2~~ −2.6 / 10.0	206.0 7.8	212.6 ~~220.3~~ +6.5 / 16.9 = F13.9	215.8 ~~223.6~~ +9.8 / 27.0	
+50	204.1 ~~213.6~~ −0.2 / 95.0	202.8 ~~212.3~~ −1.5 / 84.8 = F27.2	203.0 ~~212.5~~ −1.3 / 60.0	203.1 ~~212.6~~ −1.2 / 34.0	202.2 ~~211.4~~ −2.1 / 8.0	204.3 9.5	207.8 ~~217.3~~ +3.5 / 11.0	210.4 ~~219.9~~ +6.1 / 19.6 = F15.7	214.8 ~~224.3~~ +10.5 / 30.0
192+0		202.8 ~~215.2~~ +1.4 / 100	202.6 ~~215.0~~ +1.2 / 84.2 = F28.8	201.5 ~~213.9~~ +0.1 / 55.0	201.0 ~~213.4~~ −0.4 / 25.0	201.4 12.4	203.4 ~~215.8~~ +2.0 / 15.0	206.3 ~~218.7~~ +4.9 / 24.8 = F19.9 28.8	210.4 ~~222.8~~ +9.0 / 27.0
191+50		200.8 ~~215.3~~ +1.5 / 100.0	199.9 ~~214.4~~ +0.6 / 87.2 = F28.8	199.5 ~~214.0~~ +0.2 / 54.0	199.6 ~~214.1~~ +0.3 / 25.0	199.3 14.5	200.2 ~~214.7~~ +0.9 / 17.0	202.1 ~~216.6~~ +2.8 / 29.9 = F22.6 1:2.1	204.8 ~~219.3~~ +5.5 / 45.0
191+15.44		196.1 ~~211.4~~ −2.4 / 100.0 = Bottom Holes	198.1 ~~213.4~~ −0.4 / 89.0 = F30.0 1:2.1	198.4 ~~213.7~~ −0.1 / 64.0	198.9 ~~214.2~~ +0.4 / 35.0	198.5 15.3	199.8 ~~215.1~~ +1.3 / 36.0	203.5 ~~218.8~~ +5.0 / 65.0	

213.78

213.78

Left Lane B Line

Lt. Reduced P. Rt.

196+0

+50

195+0

+66.49 E.C.

+50

TP. 12.53 227.89 3.42 210.36

194+0

213.78

210.36

227.89

213.78

Left Lane 3rd Line

Lt. | ℄ | Rt.

199+0

+50

198+0

+50

TP 7.38 229.50 0.77 222.12

197+0

196+50

222.89

229.50

222.89

Wabash Blvd Section "A"

Sta.				
201+0				
+50				
TP	11.95	239.46	7.99	227.51
200+0				
+50				
199+13.76 Ahead				
200+01.16 B' Back				
198+97.83 ECH Back				
199+50				
	229.50			

Lt			℄	Rt			
229.7 ~~242.9~~ +3.4 70.0	228.8 ~~242.0~~ +2.5 56.8 =F8.5 1½:1	227.6 ~~240.8~~ +1.3 25.0	226.3 15.2	~~241.8~~ 228.6 +2.3 14.0	~~243.8~~ 230.6 +4.3 43.0	~~244.1~~ 230.9 +4.6 53.6 =F6.4 1½:1	231.9 ~~245.1~~ +5.6 64.0
227.9 ~~242.0~~ +2.5 75.0	227.2 ~~241.3~~ +1.8 56.0 =F8.0	226.9 ~~240.0~~ +1.5 29.0	225.4 14.1	226.4 ~~240.5~~ +1.0 14.0	227.7 ~~241.8~~ +2.3 35.0	229.4 ~~243.5~~ +4.0 52.4 =F5.6	230.1 ~~244.2~~ +4.7 63.0
			229.46				
229.0 ~~234.00~~ +4.5 65.0	227.9 ~~232.9~~ +3.4 52.0 =F5.3	226.6 ~~231.6~~ +2.1 33.0	229.5 5.0	224.7 ~~229.7~~ +0.2 14.0	224.5 ~~229.5~~ 0.0 21.0	228.5 ~~233.5~~ +4.0 50.0 =F4.0	230.0 ~~235.00~~ +5.5 59.0
227.8 ~~233.60~~ +4.1 76.0	225.5 ~~231.30~~ +1.8 53.0 =F6.0	224.9 ~~230.7~~ +1.2 26.0	223.7 5.8	222.1 ~~228.5~~ −1.0 2.0	221.2 ~~233.0~~ +3.5 34.0	229.8 ~~235.6~~ +6.1 50.0 =0.0	231.7 ~~237.5~~ +8.0 60.0

See Page 46

Lt			℄
221.3 ~~231.10~~ +1.6 80.0	220.9 ~~229.7~~ +0.2 56.3 =F8.2 [illegible]	221.7 ~~230.5~~ +1.0 26.0	220.7 8.8

229.50

Station	BS	HI	FS	Elev.		Lt.				℄		Rt.		
204+0						239.3 ~~255.2~~ +3.4 76.0	237.1 ~~253.0~~ +1.2 66.2= 14.8 1½:1	237.2 ~~253.1~~ +1.3 50.0	237.1 ~~253.0~~ +1.2 25.0	235.9 15.9	235.9 ~~251.8~~ 0.0 21.0	236.6 ~~252.5~~ +0.7 43.0	~~235.3~~ 239.4 +3.5 62.8=F12.5 1½:1	244.1 ~~260.03~~ +8.2 73.0
+50							237.8 ~~255.5~~ +3.7 74.0	236.5 ~~254.2~~ +2.4 63.4=F12.9	235.2 ~~252.9~~ +1.1 35.0	234.1 17.7	235.0 ~~252.7~~ +0.9 19.0	236.5 ~~254.2~~ +2.4 42.0	238.4 ~~256.13~~ +4.3 59.0=F10.0	242.3 ~~260.0~~ +8.2 70.0
TP	13.07	251.83 ✓	0.70	238.76						251.83				
203+0							236.7 ~~243.0~~ +3.5 71.0	235.7 ~~242.0~~ +2.5 61.1=F11.4	~~239.6~~ 233.3 +0.1 31.0	233.2 6.3	234.3 ~~240.6~~ +1.1 29.0	235.5 ~~241.76~~ +2.3 61.4=F11.6	237.7 ~~243.96~~ +4.5 72.0	
+50							236.2 ~~243.6~~ +4.1 70.0	234.5 ~~241.9~~ +2.4 59.0=F10.0	232.6 ~~240.0~~ +0.5 30.0	232.1 7.4	232.0 ~~239.4~~ −0.1 29.0	232.7 ~~240.1~~ +0.6 61.7=F11.8	233.2 ~~240.6~~ +1.1 72.0	
202+0							236.5 ~~244.5~~ +5.0 70.0	232.8 ~~240.76~~ +1.3 58.9=F9.3	230.9 ~~238.9~~ −0.6 31.0	231.5 8.0	230.2 ~~238.2~~ −1.3 23.0	231.4 ~~239.4~~ −0.1 47.0	232.3 ~~240.3~~ +0.8 58.6=F9.7	232.1 ~~240.1~~ +0.6 70.0
BM		✓	7.96	231.50	on M.H. 24' Lt 201+52									
201+50						231.5 ~~247.5~~ +3.0 63.0	231.2 ~~247.2~~ +2.7 56.6=F8.4 1½:1	229.7 ~~240.7~~ +1.2 44.0	227.8 ~~238.8~~ −0.7 26.0	228.5 11.0	229.3 ~~240.3~~ +0.8 20.0	231.5 ~~244.5~~ +3.0 56.3=F8.2 1½:1	232.0 ~~245.0~~ +3.5 66.0	
		239.46								239.46				

		✓		
TP	12.42	275.34	0.65	262.92
206+50				
		✓		
TP	12.16	263.57	0.42	251.41
206+0				
BM			7.31	244.56 (x on MH 125' Lt 205+80 244.52)
+80				
+50				
205+0				
204+50				
		251.83		

Lt.				℄	Rt.			
244.1 ~~246.6~~ −17.0 90.0	243.3 ~~245.8~~ −17.8 75.5 =F21.0 1½:1	246.9 ~~249.9~~ −14.2 45.0	253.2 ~~257.7~~ −5.9 18.0	261.1 2.5	267.6 ~~270.1~~ +6.5 23.0	279.2 ~~281.7~~ +18.1 49.0	286.1 ~~288.6~~ +25.0 66.6 =C21.6 1:1	292.4 ~~295.4~~ +21.8 79.0
				263.57				
242.1 ~~246.2~~ −5.6 9.0	242.1 ~~246.2~~ −5.6 24.2 =F20.1	243.1 ~~246.6~~ −5.2 38.0	244.8 ~~248.3~~ −3.5 9.0	248.3 3.5	256.1 ~~259.6~~ +7.8 22.0	263.9 ~~267.4~~ +15.6 40.0	270.2 ~~273.7~~ +21.9 53.1 =C8.1 1:1	276.3 ~~279.83~~ +28.0 62.0
241.5 ~~250.13~~ −1.7 94.0	241.3 ~~249.9~~ −1.9 56.0	241.8 ~~250.43~~ −1.4 27.0		243.2 8.6	249.6 ~~258.2~~ +6.4 17.0	255.9 ~~264.5~~ +12.7 32.0	261.1 ~~269.7~~ +17.9 45.0	265.9 ~~274.5~~ +22.7 54.0
240.8 ~~251.1~~ −0.7 83.0	240.5 ~~250.83~~ −1.0 72.1 =F18.9	240.3 ~~250.6~~ −1.2 50.0	240.6 ~~250.9~~ −0.9 25	241.5 10.3	242.2 ~~252.5~~ +0.7 13.0	245.3 ~~255.63~~ +3.8 30.0	255.3 ~~265.6~~ +13.8 50.9 =F4.6 1½:1	261.7 ~~272.0~~ +20.2 60.0
243.3 ~~255.6~~ +3.8 80.0	240.6 ~~252.9~~ +1.1 68.5 =F16.3	238.5 ~~250.8~~ −1.0 51.0	239.5 ~~251.8~~ 0.0 23.0	239.5 12.3	240.1 ~~252.4~~ +0.6 20.0	239.6 ~~251.9~~ +0.1 50.0	244.7 ~~257.0~~ +5.2 62.3 =F12.2	261.1 248.8 +9.3 70.0
240.6 ~~254.9~~ +3.1 76.0	240.1 ~~253.5~~ +2.7 65.5 =F14.3 1½:1	238.4 ~~252.8~~ +1.0 52.0	238.1 ~~252.5~~ +0.7 28.0	237.4 14.4	237.5 ~~251.9~~ +0.1 22.0	237.8 ~~252.2~~ +0.4 45.0	240.7 ~~255.1~~ +3.3 64.7 =F13.8 1½:1	~~258.5~~ 244.1 +6.7 75
				251.83				

Wabash Blvd. Section 4

20970				
TP	12.42	310.75	0.51	298.33
+50				
20870				
+75				
TP	12.87	298.84	0.48	285.97
+50				
TP	11.48	286.45	0.37	274.97
20770				
		275.34		

56

264.8 / 276.6	273.8 / 284.6	284.9 / 295.7	300.0	313.0 / 323.8	313.1 / 322.9	320.3 / 331.1	320.9 / 331.7			
-35.2 / 68.0	-26.2 / 49.0	-15.1 / 27.0	10.8	+12.0 / 35.0	+12.1 / 65.0	+20.3 / 88.2	+20.9 / 100.0			
	-F33 / 11.41					-C42 / 1.1				
			310.75							
292.0 / 303.8	295.5 / 306.3	267.0 / 274.8	284.2 / 295.0	291.0	302.1 / 316.0	309.1 / 316.9	316.0 / 323.8	316.3 / 324.1	317.9 / 325.7	
-39.0 / 90.0	-32.5 / 68.0	-24.0 / 44.0	-11.8 / 19.0	7.8	+11.1 / 33.0	+18.1 / 45.0	+25.0 / 75.0	+25.8 / 86.6	+26.9 / 97.0	
	-F16.0							-C41.6 / 1.1		
248.1 / 257.6	248.3 / 257.8	262.5 / 272.0	275.2 / 284.7	289.3	300.3 / 309.8	308.0 / 317.5	312.4 / 321.9	313.3 / 322.8		
-41.2 / 91.0	-41.0 / 79.7	-26.8 / 60.0	-14.1 / 25.0	9.5	+11.0 / 33.0	+18.7 / 68.0	+22.1 / 85.1	+24.0 / 96.0		
	-F23.9						-C40.1 / 1.1			
248.0 / 257.8	248.7 / 258.5	264.7 / 274.5	277.8 / 287.6	291.0	299.0 / 306.8	304.8 / 312.6	305.7 / 313.5	314.3 / 322.1	314.0 / 321.8	
-42.0 / 90.0	-42.8 / 76.0	-26.2 / 45.0	-13.2 / 23.0	7.9	+8.0 / 26.0	+16.8 / 63.0	+14.7 / 72.0	+21.3 / 76.0	+23.0 / 90.0	
			298.84							
247.0 / 256.2	247.8 / 256.0	257.1 / 266.3	269.6 / 278.8	282.3	291.9 / 299.1	298.6 / 306.8	304.3 / 312.5	305.8 / 313.0	306.6 / 313.8	
-24.3 / 93.0	-34.5 / 77.1	-25.7 / 56.0	-12.7 / 26.0	4.2	+9.6 / 16.0	+16.2 / 40.0	+20.0 / 57.0	+23.5 / 68.0	+24.9 / 82.0	
	-F22.1								-C37.0 / 1.1	
								306.9		
								+24.6 / 92.0		
			286.45							
246.0 / 249.7	246.0 / 249.7	249.0 / 252.3	264.1 / 267.8	271.6	278.5 / 282.2	290.8 / 294.3	297.7 / 301.4	300.6 / 304.3	304.4 / 308.1	
-25.6 / 91.0	-25.6 / 76.1	-22.0 / 53.0	-7.5 / 19.0	3.7	+6.9 / 18.0	+19.2 / 35.0	+26.1 / 58.0	+29.0 / 78.6	+30.8 / 90.0	
	-F20.7 / 1.21							-C32.2 / 1.1		
			275.34							

212+0				
T.P.	2.44	325.61 ✓	0.22	323.17
+50				
211+0				
+50				
210+0				
T.P.	12.85	323.39 ✓	0.21	310.54
209+50				

310.75

308.1 ~~310.0~~ -15.6 / 93.0	310.4 ~~312.3~~ -12.9 / 82.6 C18.3 2:1	306.4 ~~318.3~~ -7.3 / 50.0	320.7 ~~322.6~~ -3.0 / 27.0	323.7 1.9	325.5 ~~327.4~~ +1.8 / 31.0	326.6 ~~328.5~~ +2.9 / 55.0	326.9 ~~328.8~~ +3.2 / 78.3 C33.2 1:1	327.0 ~~328.9~~ +3.3 / 89.0	

325.61

300.6 -22.6 / 88.0	303.9 -17.3 / 78.0 C16.0 2:1	312.2 -11.0 / 59.0	318.7 -4.5 / 38.0	323.2 0.2	325.0 +1.8 / 26.0	325.8 +2.6 / 50.0	326.5 +3.3 / 80.8 C35.8 1:1	327.1 +3.9 / 91.0
294.8 ~~296.7~~ -27.2 / 81.0	299.4 ~~300.8~~ -22.6 / 69.6 C11.8 2:1	311.7 ~~313.1~~ -10.3 / 44.0	318.0 ~~319.4~~ -4.0 / 28.0	322.0 1.4	323.8 ~~325.2~~ +1.8 / 4.0	324.3 ~~325.7~~ +2.3 / 31.0	325.3 ~~326.7~~ +3.3 / 52.0	326.6 ~~328.0~~ +4.6 / 88.7 C38.7 1:1 ; 326.5 ~~327.9~~ +4.5 / 95.0
292.1 ~~297.7~~ -25.7 / 66.0	298.1 ~~303.1~~ -20.3 / 57.6 C12.6 1:1	308.4 ~~313.4~~ -10.0 / 27.0	318.2 ~~323.2~~ -0.2 / 11.0	318.9 5.0	320.3 ~~325.3~~ +1.9 / 4.0	322.1 ~~327.69~~ +4.3 / 35.0	324.1 ~~329.1~~ +5.7 / 50.0	325.3 ~~330.3~~ +6.9 / 88.1 C40.1 1:1 ; 325.2 ~~330.2~~ +6.8 / 95.0
283.8 ~~292.4~~ -31.0 / 66.0	290.4 ~~299.0~~ -24.4 / 52.8 C7.8 1:1	302.6 ~~311.2~~ -12.2 / 31.0	314.8 8.6	319.8 ~~328.4~~ +5.0 / 17.0	321.9 ~~330.5~~ +7.1 / 38.0	323.3 ~~331.9~~ +8.5 / 57.0	324.1 ~~332.7~~ +9.3 / 86.8 C41.8	324.2 ~~332.8~~ +9.4 / 97.0

323.39

274.6 ~~276.5~~ -34.3 / 78.0	279.8 ~~281.7~~ -29.1 / 54.5 C0.0	290.8 ~~292.7~~ -18.1 / 37.0	298.9 ~~300.8~~ -10.0 / 21.0	308.9 1.9	316.5 ~~318.4~~ +7.6 / 27.0	320.9 ~~322.8~~ +12.0 / 51.0	321.1 ~~323.0~~ +12.2 / 67.0	322.6 ~~324.5~~ +13.7 / 87.9 C32.9 1:1	323.3 ~~325.2~~ +14.4 / 100.0

310.75

TP	6.49	313.24	12.86	312.75
+35				
214+0				
213+81.27 BC Lt.				
+50				
213+0				
212+50				
		325.61		

	299.4	302.3	309.2		318.2	322.2	324.9	325.6
	~~310.9~~	~~312.8~~	~~320.7~~	314.1	~~329.7~~	~~333.7~~	~~336.4~~	~~337.0~~
	-14.7	-11.8	-4.9	11.5	+4.1	+8.1	+10.8	+11.4
	48.0	38.0 (0.0)	17.0		11.0	24.0	54.0	65.0
	304.0	307.0	313.6	319.3	322.3	323.6	325.0	326.0
	~~310.9~~	~~337.9~~	~~331.3~~		~~328.6~~	~~329.9~~	~~331.3~~	~~332.3~~
	-15.3	-12.3	-5.7	6.3	+5.0	+4.2	+5.7	+6.7
	61.0	57.0 C6.0 2:1	25.0		21.0	41.0	57.4 C19.4 1:1	68.0
304.1	307.9	310.4	316.8		323.6	327.9	327.7	327.9
~~309.3~~	~~313.7~~	~~315.6~~	~~322.0~~	320.4	~~328.8~~	~~333.1~~	~~332.9~~	~~333.1~~
-16.3	-12.5	-10.0	-3.6	5.23 on Hub	+3.2	+7.5	+7.3	+7.5
64.0	54.3 C7.6 2:1	45.0	19.0		36.0	54.0	61.3 C22.2 1:1	71.0
	304.1	308.5	316.4		323.6	324.9	327.3	327.9
	~~308.3~~	~~312.7~~	~~320.6~~	321.4	~~321.8~~	~~329.1~~	~~331.6~~	~~332.1~~
	-17.3	-12.9	-5.0	4.2	+2.2	+3.5	+5.9	+6.5
	68.0	58.4 C9.5 2:1	30.0		25.0	44.0	62.9 C21.5	73.0
305.6	309.5	317.1	319.9		325.1	326.3	326.8	327.5
~~308.0~~	~~311.9~~	~~319.5~~	~~322.3~~	323.2	~~327.6~~	~~328.7~~	~~329.2~~	~~329.9~~
-17.6	-13.7	-6.1	-3.3	2.4	+1.9	+3.1	+2.6	+4.3
77.0	66.9 C12.7 2:1	46.0	29.0		22.0	44.0	67.6 C27.2 1:1	78.0
310.3	312.8	316.5	321.2		325.4	326.7	327.1	327.2
~~311.8~~	~~314.3~~	~~318.0~~	~~322.7~~	324.1	~~326.9~~	~~328.2~~	~~328.6~~	~~328.7~~
-12.8	-11.3	-7.6	-2.9	1.5	+1.3	+2.6	+3.0	+3.1
92.0	80.6 C18.3 2:1	59.0	27.0		22.0	52.0	73.3 C30.3 1:1	83.0

325.61

Wabash Blvd. Section "I"

Station	B.S.	H.I.	F.S.	Elev.
+50				
216+0				
T.P.	1.52	290.64	12.68	289.12
+50				
215+20				
215+0				
T.P.	1.00	301.80 ✓	12.44	300.80
214+50				
		313.24		

June 2-50
H. Sisson
W. Garber
Chavez

289.5 ~~289.7~~ 285.2 ~~286.1~~ 280.1 ~~290.0~~ 278.2 ~~288.1~~ 288.7 | 290.8 ~~290.7~~ 286.7 ~~296.4~~ 296.2 ~~306.1~~ 307.7 ~~317.6~~
+8.8 +1.5 −0.6 −2.5 9.9 | +0.1 +6.0 +15.5 +27.0
88.0 78.3 52.0 17.0 | 30.0 48.0 72.8 87.0
F27.5 1½:1 2:1 | F22.2 1½:1 2:1

279.9 −5.8 97.0 | 286.7 ~~286.6~~ 275.4 ~~288.6~~ 281.6 ~~281.6~~ 277.2 ~~287.1~~ 279.4 ~~289.3~~ 285.1 | 290.4 ~~295.3~~ 294.7 ~~299.6~~ 305.1 ~~310.0~~ 303.1 ~~313.6~~
−9.0 −10.0 −9.5 −8.5 −6.3 4.9 | +4.7 +9.0 +19.4 +22.0
86.7 80.0 50.0 33.0 15.0 | 9.0 29.0 55.0 64.0
F33.1 | F12.0 1½:1

290.64

275.2 ~~285.6~~ 274.0 ~~286.1~~ 275.1 ~~289.4~~ 279.0 ~~292.8~~ 287.4 ~~297.4~~ | ~~313.8~~ 302.4 309.9 ~~320.5~~ 314.4 ~~329.8~~
−16.3 −17.4 −15.7 −12.4 −9.0 10.4 | +11.0 +18.5 +23.0
97.0 87.2 68.0 44.0 20.0 | 25.0 43.9 66.0
F38.5 | F1.6 1½:1

273.5 ~~379.9~~ 277.7 ~~384.1~~ 281.6 ~~286.0~~ 287.4 ~~293.8~~ 295.4 | ~~311.8~~ 305.4 ~~319.2~~ 312.8 319.4 ~~325.8~~
−21.9 −17.7 −13.8 −8.0 6.4 | +10.0 +17.4 +24.0
90.0 67.0 38.0 19.0 | 23.0 37.0 48.0
0.0

273.8 ~~277.8~~ 273.8 ~~277.3~~ 280.3 ~~285.8~~ 288.2 ~~291.1~~ 298.3 | 306.3 ~~309.8~~ 313.3 ~~316.8~~ 323.4 ~~326.9~~ 326.4 ~~329.9~~
−24.5 −24.5 −18.0 −10.1 3.5 | +8.0 +15.0 +25.1 +28.1
95.0 83.3 51.0 21.0 | 20.0 33.0 49.8 59.0
F31.2 | C1.8 1:1.8

301.80

288.0 ~~289.7~~ 292.6 ~~294.2~~ 294.7 ~~296.4~~ 303.0 ~~304.4~~ 311.5 | 315.9 ~~317.6~~ 320.0 ~~321.7~~ 323.5 ~~325.2~~ 325.3 ~~327.0~~ 325.8 ~~327.5~~
−23.5 −19.0 −16.8 −8.5 1.7 | +1.4 +8.5 +12.0 +13.8 +14.3
63.0 52.6 46.0 21.0 | 12.0 25.7 38.0 54.7 64.0
F10.4 1½:1 | C9.4 1½:1

313.24

+50					
218+0					
B.M. Corrected	4.03	334.36 ✓	4.56	330.33	BM NW
				330.38	Landis + 404
					330.33
T.P.	7.42	334.94 ✓	0.27	327.52	
+80		✓			
2 T.P.	12.79	327.79	0.36	315.00	
+50		✓			
T.P.	12.83	315.36	0.39	302.53	
T.P.	12.92	302.92	0.64	290.00	
217+0					
		290.64			

~~335.0~~ 329.8   ~~334.9~~ 329.7   ~~335.1~~ 329.9   329.2   ~~332.6~~ 327.4   ~~328.2~~ 323.0   ~~325.4~~ 320.2   ~~326.9~~ 321.7   ~~324.8~~ 319.6

+0.6 / 53.0   +0.5 / 42.3 = 65.3 1:1   +0.7 / 23.0   5.2   -1.8 / 20   -6.2 / 30.0   -9.0 / 40.0   -7.5 / 48.8 = F6.5 1:1   -9.6 / 60.0

324.1 / ~~341.3~~   323.1 / ~~340.3~~   321.5 / ~~338.7~~   320.2 / ~~337.9~~   317.2   308.0 / ~~325.2~~   296.2 / ~~313.4~~   291.2 / ~~308.4~~   287.3 / ~~304.5~~   287.2 / ~~304.4~~

+6.9 / 50.0   +5.9 / 38.6 = C16 1:1   +4.3 / 27.0   +3.0 / 5.0   -9.2 / 18.0   -21.0 / 40.0   -26.0 / 74.0   -29.9 / 97.4 = F38.9   -30.0 / 107.0

334.36

321.3 / ~~335.8~~   320.2 / ~~334.7~~   319.0 / ~~333.5~~   316.5 / ~~331.0~~   313.3   310.0 / ~~324.5~~   300.3 / ~~314.8~~   293.3 / ~~307.8~~   288.3 / ~~302.8~~   285.3 / ~~299.8~~

+8.0 / 50.0   +6.9 / 37.0 = 0.0   +5.7 / 30.0   +3.2 / 12.0   1.6   -3.3 / 4.0   -13.0 / 25.0   -20.0 / 46.0   -25.0 / 78.0   -28.0 / 96.0

327.79

318.0 / ~~329.0~~   316.2 / ~~327.2~~   313.9 / ~~324.9~~   304.4   296.4 / ~~307.4~~   287.0 / ~~298.0~~   284.2 / ~~295.2~~   286.1 / ~~297.1~~   292.1 / ~~303.1~~

+13.6 / 50.0   +11.8 / 40.5 = F2.3   +9.5 / 30.0   11.0   -8.0 / 20.0   -17.4 / 50.0   -20.2 / 78.0   -18.3 / 95.7 = F31.8   -12.0 / 106.0

315.36   -8.0 / 20.0

303.5 / ~~304.1~~   301.1 / ~~301.7~~   297.0 / ~~297.6~~   294.1 / ~~294.7~~   290.0   283.6 / ~~284.2~~   282.7 / ~~283.3~~   283.4 / ~~284.0~~   289.3 / ~~289.9~~   300.0 / ~~300.6~~

+13.5 / 68.0   +11.1 / 58.3 = F14.8 1/2:1   +7.0 / 40.0   +4.1 / 18.0   0.6   -6.4 / 20.0   -7.3 / 44.0   -6.6 / 74.0   -0.7 / 86.8 = F3.2 1/2:1   +10.0 / 100.0

290.64

+75 1/2 FC

+50

219+0

218+65

Lt. ℄ Rt

Reduced A.T. Lamore

331.6 / ~~335.2~~ | 331.9 / ~~334.5~~ | 331.6 / ~~334.2~~ | 331.0 / ~~333.6~~ | 331.8 | 331.0 / ~~333.6~~ | 331.8 / ~~334.4~~ | 331.8 / ~~334.4~~
+0.8 | +0.1 | -0.2 | -0.8 | 2.6 | -0.8 | 0.0 | 0.0
40.0=C2.4 Gut. | 39.0 | 26.0=CS | 26.0=Gut. | | 25.7=Gutter 1.7 Orr | 33.0 | 40.0=Col. Gutter

331.8 / ~~335.2~~ | 331.3 / ~~334.7~~ | 330.9 / ~~334.3~~ | 330.2 / ~~333.6~~ | 331.0 | 330.2 / ~~333.6~~ | 330.8 / ~~334.2~~ | 331.2 / ~~334.6~~
+0.8 | +0.3 | -0.1 | -0.8 | 3.4 | -0.8 | -0.5 | +0.2
39.8=C2.9 Gutter | 38 | 25.5=CS | 25.5=Gut | | 26.4=Gut | 26.4=CS | 40.2=Col. Gutter

329.8 / ~~334.3~~ | 329.7 / ~~334.3~~ | 329.4 / ~~334.0~~ | 329.8 | 329.4 / ~~334.0~~ | 329.3 / ~~333.9~~ | 329.4 / ~~334.0~~
0.0 | -0.1 | -0.4 | 4.6 | -0.4 | -0.5 | -0.4
50.0 | 37.4=C2.4 | 24.0 | | 26.0 | 40.2=F0.8 1 1/2" | 50.0

329.2 / ~~333.7~~ | 329.3 / ~~333.8~~ | 329.9 / ~~334.4~~ | 329.9 | 329.6 / ~~334.3~~ | 328.9 / ~~333.4~~ | 329.1 / ~~333.6~~
-0.7 | -0.6 | 0.0 | 4.5 | -0.1 | -1.0 | -0.8
51.0 | 41.0=C4.0 1.1 | 28.0 | | 23 | 40.0=0.0 | 50.0

334.36

Cross Section Area East of Wabash Blvd.
North of Federal Blvd. Bridge
102+75 to 107+0

Nov. 22-50
Rorer
Pullen
F.S.: 550 = Garber
Rt: East

Station						
+50	79.1 4.4 72: Top Cut	79.0 4.5 100'	78.1 5.4 126	78.4 5.1 171: E/I Cut	72.5 11.0 179	
104+0	78.1 5.4 73: Top Cut	77.7 5.8 100	77.1 6.4 128	77.2 6.3 160: E/I Cut	72.8 10.7 166'	
+81.72	77.4 6.1 72: Top Cut	77.1 6.4 100	76.7 6.9 128	76.2 6.6 158: E/I Cut	72.5 11.0 165'	
+50	77.0 6.5 73: Top Cut	76.8 6.7 100	76.5 7.0 124	76.5 7.0 157: E/I Cut	73.4 10.1 161	
103+0	76.2 7.3 72: Top Cut	76.1 7.4 100	76.0 7.5 124	75.8 7.7 143: E/I Cut	72.0 11.5 146	
102+75	73.3 10.2 70'	75.7 7.8 81	75.8 7.7 100	75.5 8.0 122	75.0 8.5 138	71.1 12.4 146'

B.M. 7.85 83.51 75.66 B.P. H Inlet Rt 81+0 Federal

83.51

Nov. 27-50
A. Sisson
Gorber
Rorer
Pullen

℄ | Rt. = East.

TP	12.29	97.46	0.70	85.17		
BM	9.89	85.87	5.38	75.98	N.E. Chisel [illegible] Federal + Wabash Br.	
BM	7.70	81.36		73.66	B.P. H Inlet Rt 31+0 Federal	
107+0						86.6 5.3/35' · 85.2 6.7/54 · 86.8 5.1/79 · 86.7 5.2/100' · 86.1 5.8/127 · 87.0 4.9/143 · 86.4 5.5/168 · 4.4/191 = Bot. 17 N.E.O.C.
+50						84.0 7.9/50' · 83.7 8.2/75 · 83.5 8.4/100 · 83.4 8.5/128 · 82.3 9.6/164 · 82.7 9.2/198 = 17 N.E.O.C. · 10.2/218 = Bot.
106+0						83.3 8.6/68' = Top Cut · 82.2 9.7/75' · 81.7 10.2/100' · 81.2 10.7/126' · 81.9 10.0/163 · 80.3 11.6/196' = 17 N.E.O.C. · 12.3/246 = Bot. Cut
TP	9.81	91.93	1.39	82.12		91.93
+49.75 = BC Rt.						82.0 1.5/71.0 = Top Cut · 80.8 2.7/87' · 80.7 2.8/100' · 80.6 2.9/139 · 79.8 3.7/185 · 79.5 4.0/211
105+0						80.2 3.3/71.0 = Top Cut · 80.0 3.5/100' · 79.3 4.2/136 · 78.7 4.8/183 = E Heat. · 73.2 10.3/191

83.51

109+10				
TP	10.63	120.60	0.49	109.97
+50				
108+05				
+93				
TP	13.23	110.46	0.23	97.23
+50				
107+15				
	97.46			

℄ Rt: East

108.1 113.0 110.9 109.5
12.5/56 7.6/65: top Cut 9.7/100' 11.1/124.0'

120.60

104.2 107.9 107.2 108.4 107.9 107.1
6.3/57' 3.6/63 3.3/84 2.1/100 3.6/120' 5.4/139: Bot. Cut.

93.5 97.4 104.3 104.3 103.2
17.0/35' 13.1/65 6.2/100' 6.2/125' 7.3/154: Bot Cut

93.0 95.2 101.2 103.0 102.8 101.8
16.6/33' 15.3/55' 9.3/86' 7.5/100' 7.7/131 8.7/158: Bot Cut

110.46

87.2 89.6 91.6 94.0 96.3 93.7
10.3/15' 7.9/42' 5.9/65 3.5/100' 1.2/128' 3.8/166: Bot. Cut.

88.1 86.7 88.1 88.7 89.3 88.8
9.4/28: top Cut 10.8/51' 9.4/95' 8.8/130 8.3/157' 8.7/184: Bottom Cut Exc.

97.46

Note 1 = North only Pioneer Road

Station		℄		Rt = East	
112+0			110.3 / 10.3 / 62' Pioneer Road	109.6 / 11.0 / 78'	
111+50			118.4 / 2.2 / 63'	117.6 / 3.0 / 70'	117.0 / 3.6 / 85' = Box Cut
+94.17 = 0+00 N.E.O.C.			112.8 / 7.8 / 40'	119.0 / 1.6 / 51' = W/L Cut	117.5 / 3.1 / 75	117.9 / 2.7 / 99' = Box Cut
+50			112.9 / 7.7 / 43	118.5 / 2.1 / 52'	116.8 / 3.8 / 75	117.1 / 3.5 / 102 = Box Cut
110+0			111.8 / 8.8 / 48'	117.0 / 3.6 / 57 = W/L Cut	115.8 / 4.8 / 80	115.4 / 5.2 / 107 = Box Cut
109+50			110.2 / 10.4 / 51'	114.6 / 6.0 / 60 = W/L Cut	113.6 / 7.0 / 80'	113.6 / 7.0 / 115 = Bottom Cut

120.60

120.60

Cross Section Wightman St.
At 40th St.

Jan. 18-51 66
A. Sisson
Garber
Rt. Roper

Lt. = West
Rt. = East

+61
342.45 342.12 342.52 ℄ 342.52 342.14 341.58 342.04
5.03 5.40 5.00 5.00 5.38 5.94 5.48
40: W/y Pav. 26 13 13 26 40: E/y Pav.

+48
342.07 341.62 342.12 341.82 342.31 342.02 342.42
5.45 5.9 5.40 5.7 5.21 5.5 5.10
53: Cb. E.C. 90: Gr. 90: Cb. 135: Gr. 135: Cb. 179 179: Cb. N.H. Walk

+48 = South Curb Line Wightman
342.39 341.52 341.96 342.11 342.25 342.48 342.53 342.06 341.65 341.62 341.54 341.42
5.13 6.0 5.56 5.41 5.27 5.04 4.99 5.46 5.87 5.90 5.98 6.1
53: Cb. E.C. 53: Ground 40 33 26 17 17 26 33 40: E/y Pav. 53: Ground

+38 = N/y Center Island
342.81 342.76 342.08 342.44 342.57 343.08 342.06 341.68 342.27 342.37 342.27
4.71 4.76 5.44 5.08 4.95 4.44 5.46 5.84 5.25 5.20 5.25
40: 07 Conc. Walk 35.5: Cb. 35.5: Gut. 17 0.0: Gut. 0.0: Cb. 17 35: Gut. 35: Cb. 40: 07 Conc. Walk 53: 07 Conc. Walk

225+28 = Curb B.C. Rt. + Lt. 20' Curb Rad.
342.80 342.10 342.44 342.54 343.05 342.99 342.51 342.19 341.61 342.25
4.72 5.42 5.08 4.98 4.47 4.53 5.01 5.33 5.91 5.27
33: Cb. 33: Gut. 17 2.0: Gut. 1.5: Cb. 1.5: Cb. 2.0: Gut. 17 33: Gut. 33: Cb.

347.52

used →	4.43	347.52		343.09 N.W. B.P. Wightman + 40th St.
B.M.	4.43	347.26	0.68	342.83 Rec. 343.09
B.M.	11.36	343.51		332.15 N.E. B.P. Landis + 40th St.

Lt = West ℄ Rt = East

226+14 = North Line of Wightman St.

343.42 343.08 342.56 342.82 342.85 342.54 342.05 342.54 342.82

4.1 / 40 | 4.44 / 26 Cb | 4.96 / 26 Gut | 4.70 / 13' | 4.67 | 4.98 / 13' | 5.47 / 26 Gut | 4.98 / 26 Cb | 4.7 / 40

226+0

342.63 342.12 342.81 342.52 342.96

4.89 / 90 Cb | 5.4 / 135 Gut Gr. | 4.71 / 135 Cb | 5.0 / 179 Gut | 4.56 / 179 Cb N. Alley

226+0 = North Curb Line

343.00 342.45 342.40 342.67 342.73 342.40 341.88 342.05 342.54 342.02

4.52 / 40 Cb | 5.07 / 40 Gut N/AC | 5.12 / 26 | 4.85 / 13 | 4.79 | 5.12 / 13 | 5.64 / 26 | 5.47 / 40 Gut | 4.98 / 40 Cb | 5.5 / 90 Ground

+87

342.61 342.28 342.55 342.60 342.32 341.78 342.22

4.91 / 40 | 5.24 / 26 | 4.97 / 13 | 4.92 | 5.20 / 13 | 5.74 / 26 | 5.30 / 40

225+71 = ℄ Wightman

342.73 342.28 342.64 342.63 342.32 341.69 342.28

4.79 / 40 N/AC | 5.28 / 26 | 4.88 / 13' | 4.89 | 5.30 / 13 | 5.83 / 26 | 5.24 / 40 FL/AC

347.52

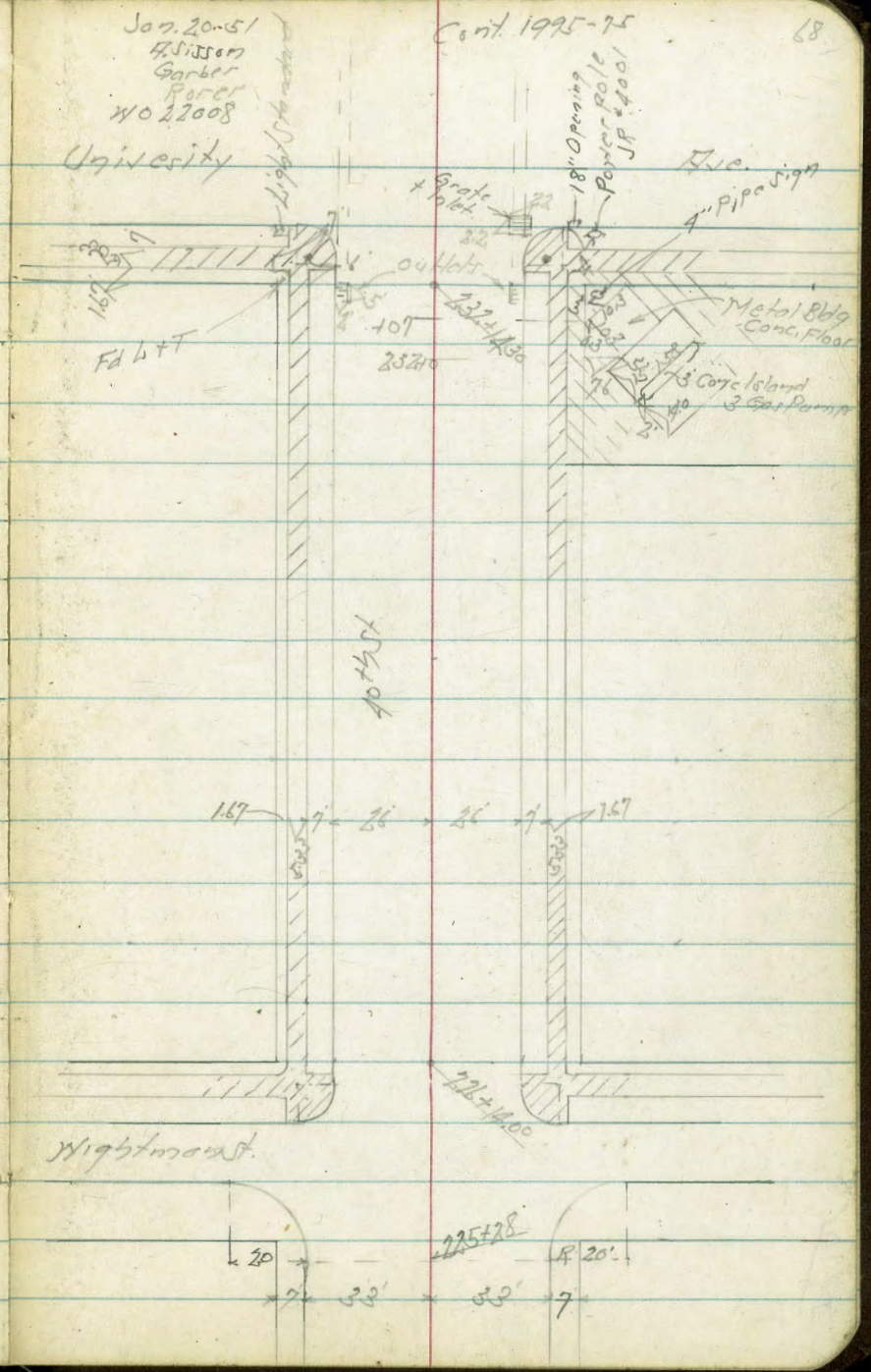
347.52

Cross Section 40th St.
Wightman St. to University Ave.
Levels next Page
Topog Page 77-78

Jan. 20-51
H. Sisson
Garber
Rorer
WO 22008

Cont. 1995-75

68



+50.7	= ℄ 4' Conc Walk on Lt.		
+28	= ℄ 4' Conc Walk on Rt.		
227+03.1	= ℄ 2.7' Conc Walk on Lt.		
+95.5	= ℄ 4' Conc Walk on Rt.		
+50	= ℄ 3.5 Conc Walk on Rt.		
226+38.7	= ℄ 2.7' Conc Walk on Lt.		
B.M. 4.92	348.01	343.09	N.W. B.P. Wigstrom #40th

Lt. = W ℄ Rt. = East

344.60 3.41 48' on Walk
344.55 3.46 41 on Walk
344.83 3.18 38.3
344.53 3.48 26 Cb
344.00 4.01 26 Gut
344.37 3.64 13
344.53 3.48
344.28 3.73 13
343.71 4.30 26 Gut
344.38 3.63 26 Cb
344.73 3.28 38.3 E Conc W
344.71 3.3 40

343.49 4.52 26
344.03 3.98 26 Cb
344.27 3.74 38.3 E Conc Walk
344.47 3.54 48 on Walk

344.32 3.69 48 on Walk
344.25 3.76 38.3 E Conc Walk
344.07 3.94 26 Cb
343.46 4.55 26

344.21 3.8 40
344.10 3.91 38.3 W Conc Walk
344.00 4.01 26 Cb
343.39 4.62 26 Gut
343.69 4.32 13
343.84 4.17
343.60 4.41 13
343.05 4.96 26
343.69 4.32 26
343.97 4.04 38.3 E Conc Walk
344.16 3.85 48 on Walk

343.91 4.1 40
343.59 4.42 38.3 W Conc Walk
343.36 4.65 26 Cb
342.84 5.17 26 Gut
343.19 4.82 13
343.27 4.74
342.94 5.07 13
342.38 5.63 26 Gut
342.96 5.05 26 Cb
343.22 4.79 38.3 E Conc Walk
343.46 4.55 48 on Walk

343.77 4.24 48 on Walk
343.53 4.48 38.3 W Conc Walk
343.27 4.74 26 Cb
342.73 5.28 26 Gut

348.01

+27.3	= ℄ 4.7' Conc Walk on Lt			
+06	= ℄ 3' Conc Walk on Lt			
228+0				
TP	6.44	351.35	3.10	344.91
+83	= ℄ 2' Conc Walk on Rt			
+71.8	= ℄ 3' Conc Walk on Lt			
227+57	= ℄ 4.7 Conc Walk on Rt			

348.01

Lt ℄ Rt

346.14 345.73 345.54 344.90
5.21 5.62 5.83 6.45
48 on Walk 38.3 W/Conc Walk 26-Cb 26-Gut

345.55 345.50 345.26 344.65
5.80 5.85 6.10 6.70
48 38.3 26-Cb 26-Gut

345.55 345.44 345.14 344.58 345.03 345.18 344.88 344.47 345.05 345.36 345.25
5.8 5.91 6.21 6.77 6.32 6.17 6.47 6.88 6.30 5.99 6.1
40 38.3 26 26 13 13 26 26 38.3 40

351.35

344.21 344.79 345.09 345.21
3.80 3.22 2.92 2.80
26-Gut 26-Cb 38.3 48 on Walk

345.05 345.11 344.83 344.22
2.96 2.90 3.18 3.79
48 on Walk Conc 38.3 26 26

343.81 344.48 344.86 344.79
4.20 3.53 3.15 3.22
26-Gut 26-Cb 38.3 48' E/Conc Walk

348.01

+111.3 = ℄ Drive + Walk on Lt

229+08.2 = Sly Conc Drive on Rt

+92 = ℄ 5' Conc Walk on Lt

+88.8

+64.3 = ℄ 3.6' Conc Walk on Lt.

+51 = ℄ 38 Conc Walk on Rt

228+40.8 = ℄ 5' Conc Walk on Lt

346.95 4.50 48 on Drive
346.95 4.40 38.3 Wly Conc Walk
346.83 4.52 33 Ely Conc Walk
345.97 5.38 26 Gut. in Drive

346.01 5.34 26
346.67 4.68 26 Cb
346.91 4.44 38.3 Ely Conc Walk
347.23 4.12 41 on Drive
348.07 3.28 52 on Conc Drive

346.59 4.76 48 on Walk
346.59 4.76 38.3
346.30 5.05 26
345.69 5.66 26
346.17 5.18 13
346.35 5.00
346.15 5.20 13
345.79 5.56 26
346.47 4.88 26
346.68 4.67 38.3
346.95 4.4 40

345.76 5.59 26
346.44 4.91 26 Cb
346.64 4.71 38.3
346.88 4.47 40 Bottom Slope
347.39 3.96 40 Top Slope

346.30 5.05 48 on Walk
346.20 5.15 38.3
345.97 5.38 26 Cb
345.30 6.05 26

346.15 5.2 40
346.07 5.28 38.3
345.77 5.58 26
345.16 6.19 26
345.61 5.74 13
345.80 5.55
345.61 5.74 13
345.12 6.23 26
345.76 5.59 26
346.17 5.18 38.3 Ely Conc Walk
346.44 4.91 41 on Walk
346.59 4.76 48 on Walk

345.92 5.43 48 on Walk
345.85 5.50 38.3 Wly Conc Walk
345.64 5.71 26 Cb
345.07 6.28 26 Gut

230+01.5 = ℄ Conc Walk + Steps on Rt.

+95 = ℄ 8' Conc Walk on Lt.

+73 = ℄ 3.6' Conc Steps + Walk on Rt.

TP	8.00	355.18	4.17	347.18

+63.3 = ℄ 2' Conc Walk on Rt.

+45.7 = ℄ 4.3 Conc Walk on Lt

229+23 = N/Y Conc Drive on Rt.

351.35

Lt. ℄ Rt.

347.04 347.70 348.04 348.08 350.04

8.14/26 Gut 7.48/26 Cb 7.14/38.3 7.10/40.4 Bot Steps 5.14/44 Top Steps

348.22 348.17 347.76 347.69 347.44 346.76 347.25 347.48 347.38 347.01 347.68 347.93 348.28

6.86/48 7.01/40 Top Step 7.42/40 Bot Step 7.49/38.3 Wk 7.74/26 Cb 8.42/26 Gut 7.93/13 7.70 7.80/13 8.17/26 7.50/26 7.25/38.3 6.9/40

346.86 347.45 347.71 347.80 349.72

8.32/26 7.73/26 Cb 7.47/38.3 7.38/40.8 Bot Step 5.46/44.5 Top Steps

355.18

347.55 347.31 347.13 346.50 347.06 347.25 347.03 346.76 347.33 347.59 347.86 349.07

3.8/40 4.04/38.3 4.22/26 4.85/26 4.29/13 4.10 4.32/13 4.59/26 Gut 4.62/26 Cb 3.76/38.3 3.49/40 on Walk 2.28/46 on Walk

347.76 347.72 347.21 346.94 346.27

3.59/48 on Walk 3.63/42.5 on Walk 4.14/38.3 W/ Conc Walk 4.41/26 Cb 5.08/26

347.45 347.15 346.67 346.05 346.53 346.73 346.60 346.28 346.87 347.10 347.60 348.21

3.9/40 4.20/38.3 W/ Conc Walk 4.68/26 Cb 5.30/26 Gut 4.82/13 4.62 4.75/13 5.07/26 Gut 4.48/26 Cb 4.35/38.3 E/ Conc Walk 3.35/44 on Dr. 3.14/52 on Dr.

351.35

+83 = 5½ Conc Drive on Lt

+78.1 = 5½ Ramp on Lt.

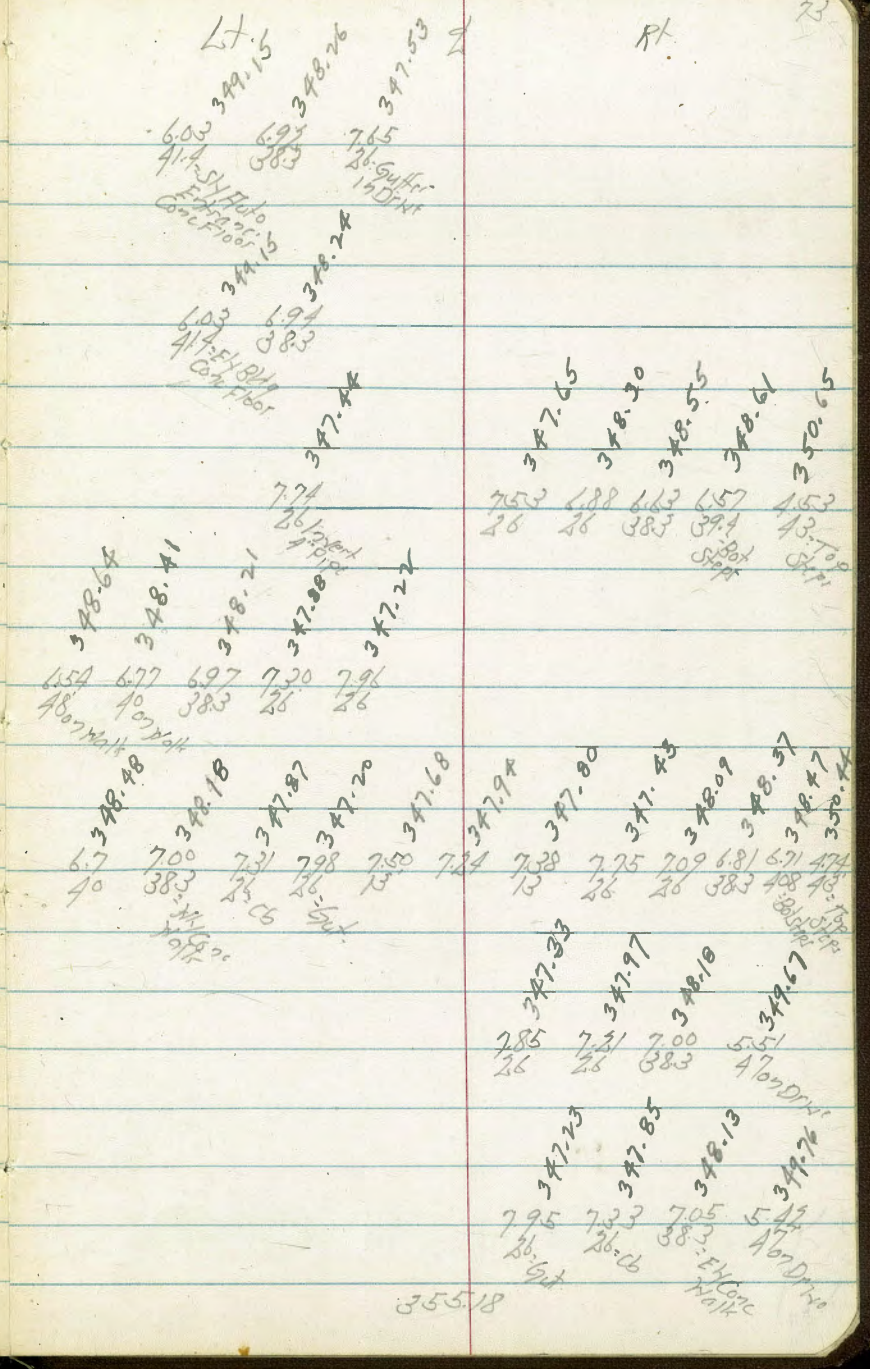
+65.3 = 2½ 2' Conc Walk & Steps on Rt

+50.7 = 2½ 4' Conc Walk on Lt

+40.7 = 2½ Conc Walk & Steps on Rt

+25.3 = 11½ Conc Drive on Rt

230+17.3 = 5½ Conc Drive on Rt



355.18

355.18

+6.9 = Sly Conc Drive on Rt

+47.6 = Nly Drive on Lt

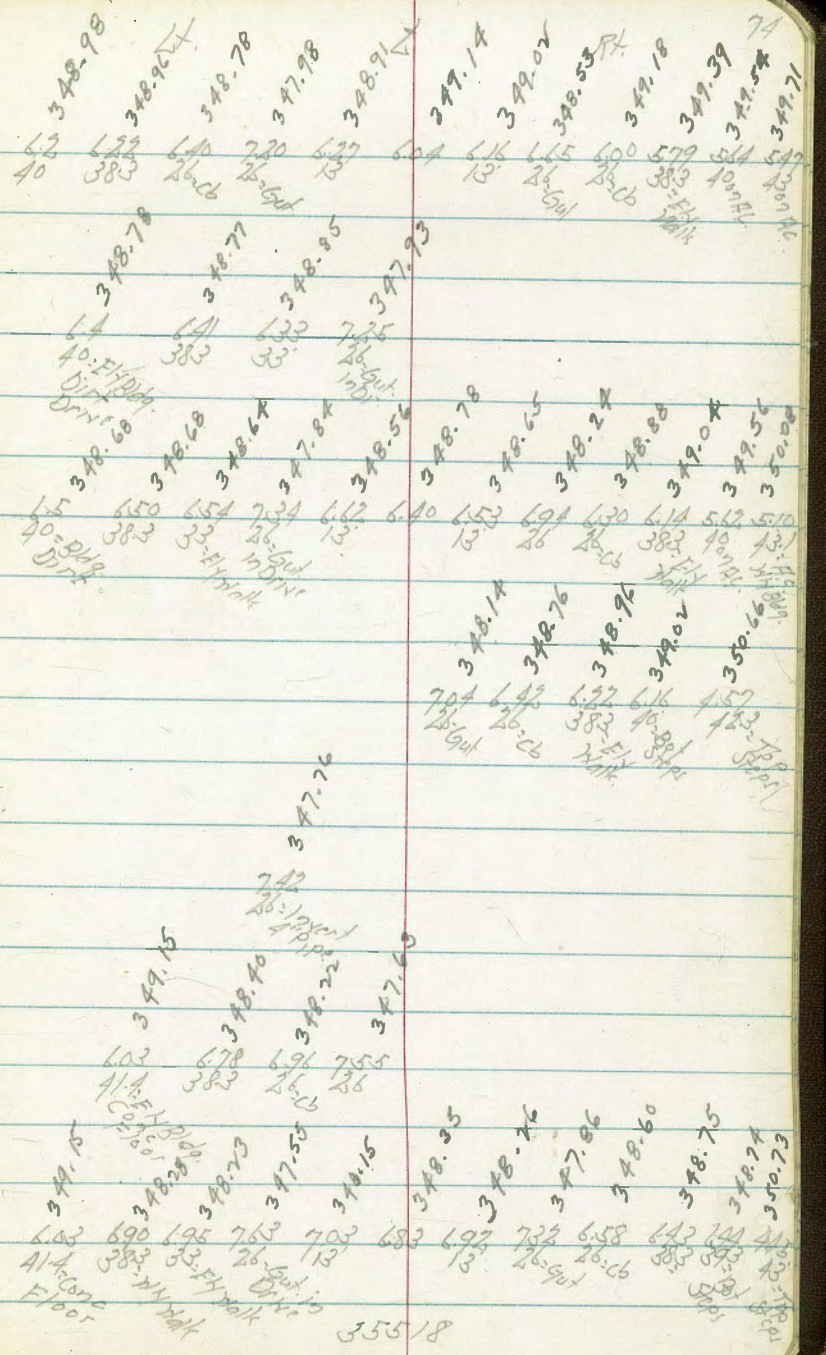
+36.7 = Sly Conc Drive on Lt

+16 = Σ 3' Conc. Walk x Stepron Rt

+12.3

231+00.8 = Nly Ramp end

230+90.5 = Σ 3' Conc. Walk x Stepron Rt



Lt. | Rt

+28.3

+28.3 = South Curb Line

+1430 = South Line University Ave

232+08.3 = S/L out let's Rt + Lt

+926 = Conc Drive on Rt

TP 5.18 354.58 5.78 349.40

232+80.9 = Conc Dr on Lt

355.18

354.58

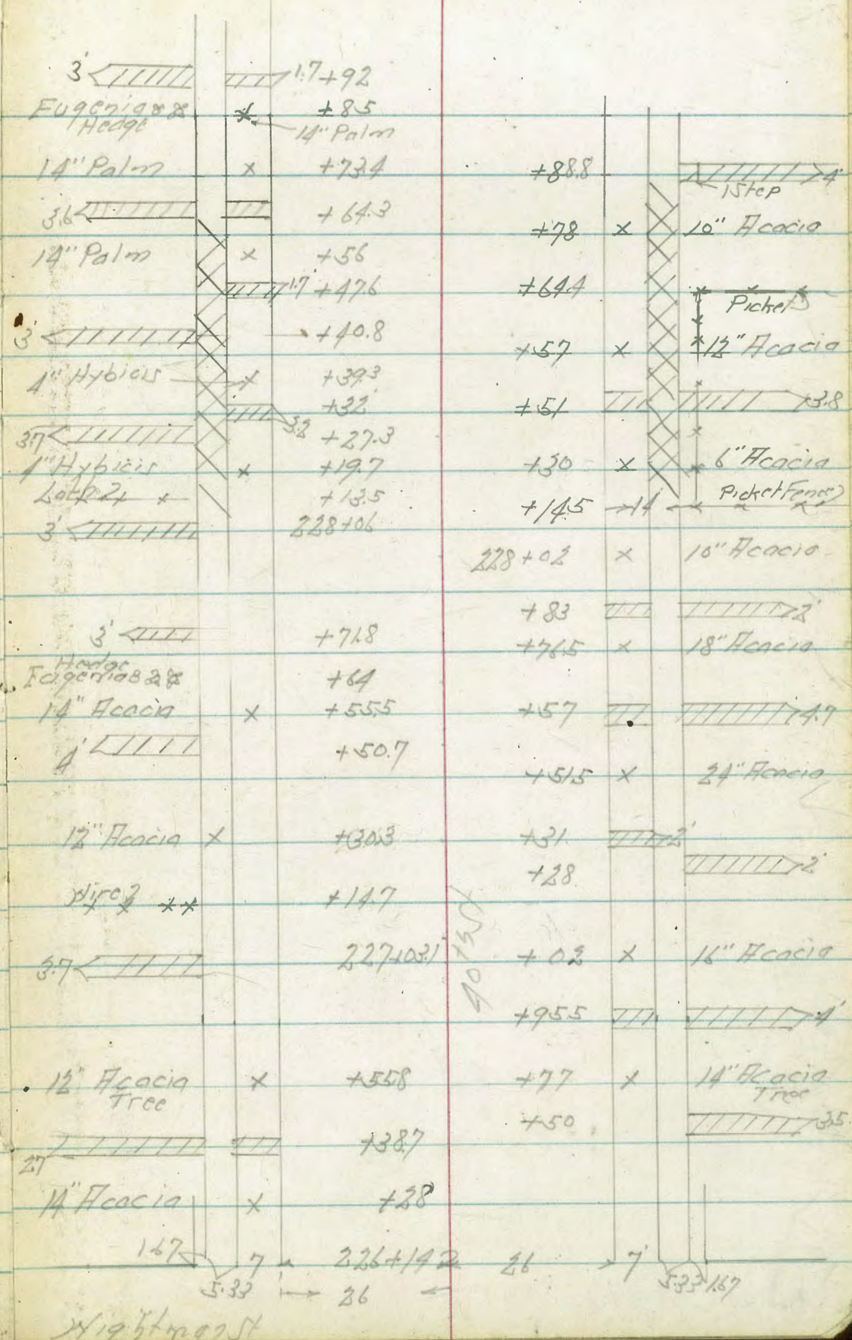
355.18

Lt.=West. ℄ Rt.=East

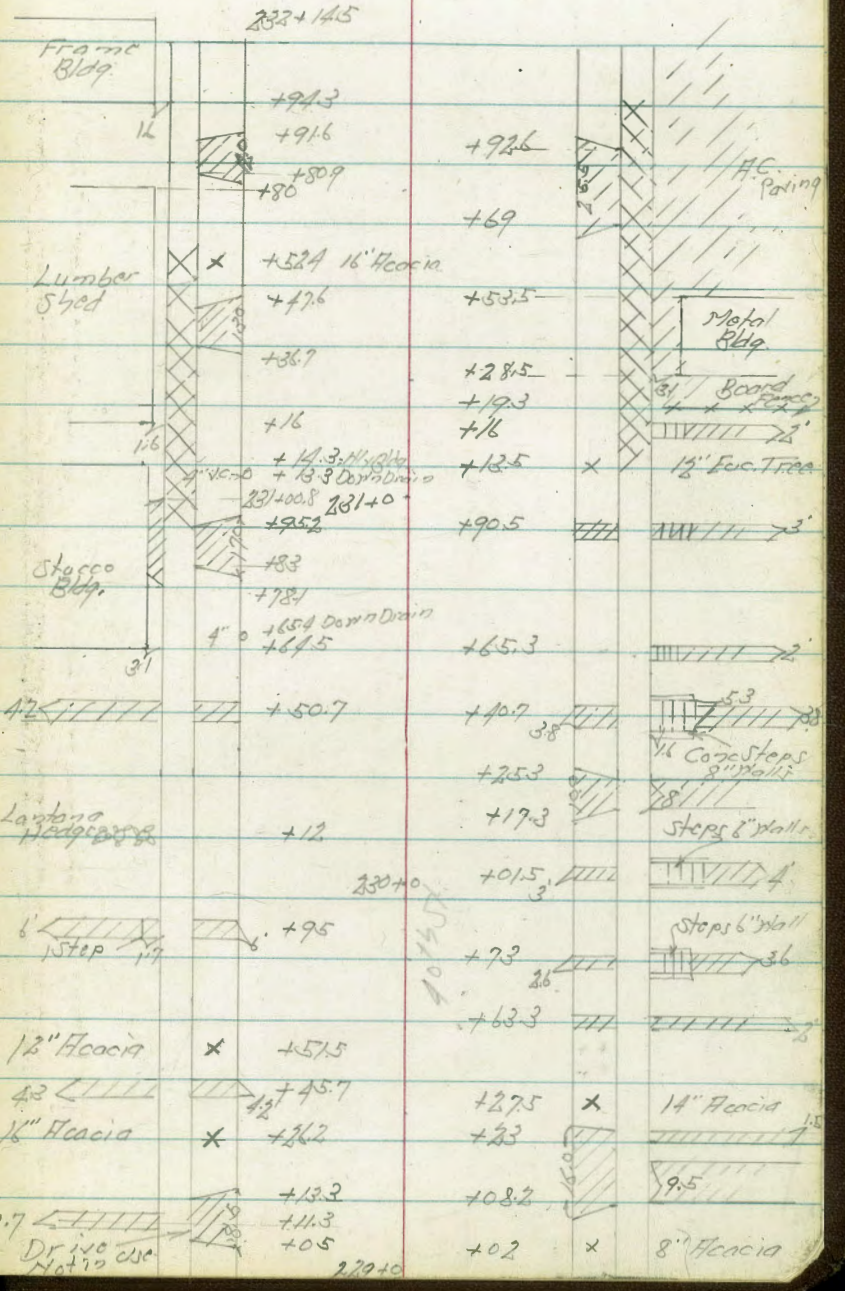
BM			1.68	343.05	N.W. BP Wigwam +4.04 343.09
TP	6.30	344.73	10.67	338.43	
BM	1.82	349.10		347.28	N.W. BP Univ +3.96 347.24
BM			5.09	347.28	N.W. BP Univ +3.96 347.24
TP	3.53	352.37	5.74	348.84	
+54.3 = ℄ University Ave					
232+41.3 = 5th University Ave					
		354.58			

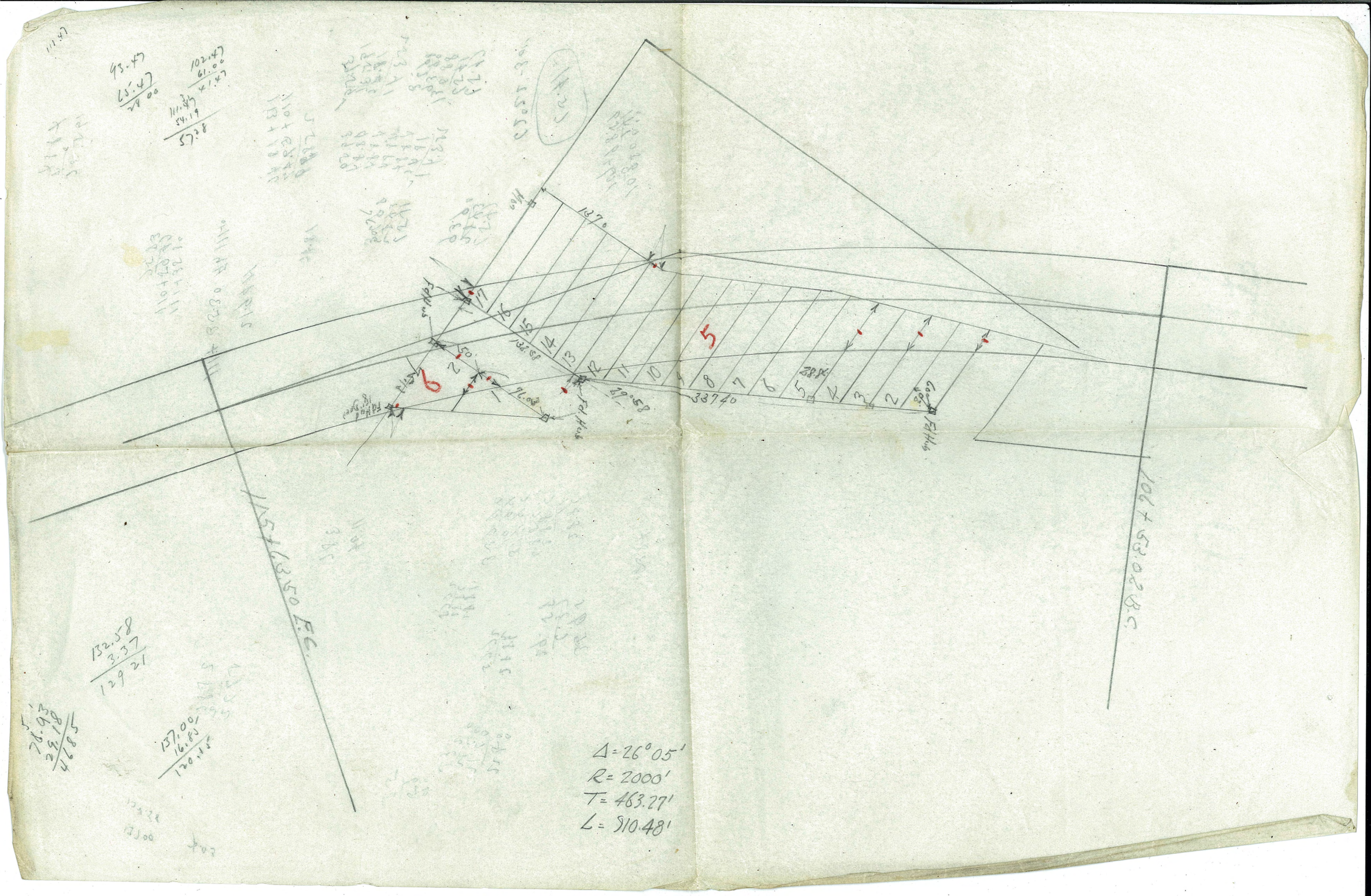
349.57	349.94	350.00	350.15	350.38	350.36	350.55	
5.01 90	4.64 40	4.58 28	4.43	4.29 26	4.33 40	4.03 78	
349.24	349.64	349.77	350.00	350.10	350.14	350.20	
5.36 90	4.96 40	4.81 28	4.58	4.48 26	4.44 40	4.38 78	

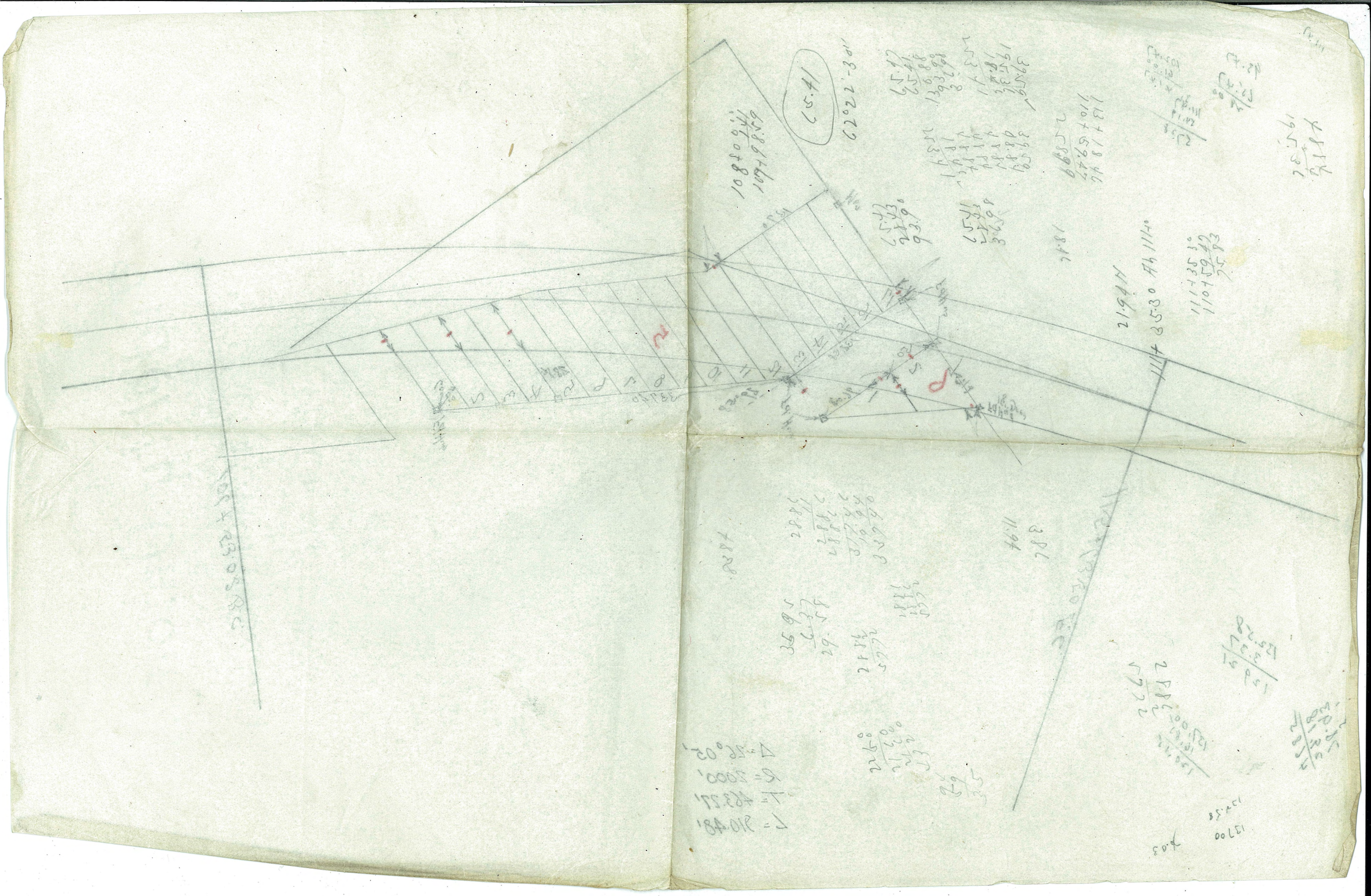
354.58


3'
1.7+92
Eugenia Hedge
+85
14" Palm
14" Palm
+73.4
3.6
+64.3
14" Palm
+56
1.7 +47.6
3'
+40.8
4" Hybicis
+39.3
+32
3.2
3.7
+27.3
4" Hybicis
+19.7
Lot 24
+13.5
3'
228+06
3'
+71.8
Hedge Eugenias
+64
14" Acacia
+55.5
4'
+50.7
12" Acacia
+30.3
Wire 2
+14.7
3.7
227+03.1
12" Acacia Tree
+55.8
2.7
+38.7
14" Acacia
+28
1.67
7
226+14.2
5.33
26
Wightman St
+88.8
Step
4'
+78
10" Acacia
+64.4
Picket
+57
12" Acacia
+51
3.8
+30
6" Acacia
+14.5
Picket Fence
228+02
10" Acacia
+83
2'
+76.5
18" Acacia
+57
4.7
+51.5
24" Acacia
+31
2'
+28
2'
+0.2
16" Acacia
+95.5
4'
+77
14" Acacia Tree
+50
3.5
26
7'
5.33
1.67

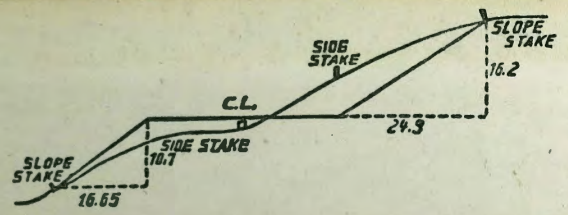
University Ave.




Δ = 26° 05'
R = 2000'
T = 463.27'
L = 910.48'



4 in
6' N of S.C 6
40+75 to 38+75



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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