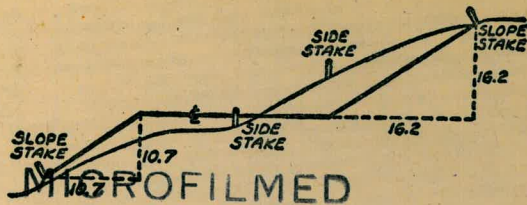


2091

TRANSIT BOOK



DEC 31 1964
 DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

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Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3432	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60' cos	60' cot	50' cos	50' cot	40' cos	40' cot	30' cos	30' cot	20' cos	20' cot	10' cos	10' cot	deg.

TABLE VII Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50	$\frac{1}{2}$ sub chord = \sin of $\frac{1}{2}$ def. angle				Length of arc for 100 ft.
		sin. $\frac{1}{2}$ def. ang.	12.5 Ft.	15 Ft.	20 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

$$T = R \tan \frac{1}{2} I$$

$$T = 50 \tan \frac{1}{2} I$$

$$\sin \frac{1}{2} D = \frac{50}{R}$$

$$\sin \frac{1}{2} D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{\sin. \frac{1}{2} D}{50}$$

$$E = R \text{ ex. sec } \frac{1}{2} I$$

$$E = T \tan \frac{1}{2} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft. see Table II.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance. Multiply the angle by .01745, and the product by the distance.

GENERAL DATA

RIGHT ANGLE TRIANGLES. Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. $10.10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. $25.25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875 = \text{Base}$. Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

LEVELING. The correction for curvature and refraction, in feet and decimals of feet is equal to $0.574 d^2$, where d is the distance in miles. The correction for curvature alone is closely $\frac{1}{2} d^2$. The combined correction is negative.

PROBABLE ERROR. If d_1, d_2, d_3 , etc. are the discrepancies of various results from the mean, and if $\sum d^2$ = the sum of the squares of these differences and n = the number of observations, then the probable error of the mean = $\pm 0.6745 \sqrt{\frac{\sum d^2}{n(n-1)}}$

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.12	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.053	.057	.061
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Walash Freeway & Bridge 2
 X-Sec Chollas Creek Bridge 6
 X-Sec Zoo Road from PK Blvd 10
 Drain Survey- Wightman - mile 22
 X-Sec Alley Blk L- Plumosa PK 25
 X-Sec Hancock Clayton-Sutherland 37

Index See also Previous Pg

37 X-sec Hancock Clayton
to Sutherland

44-47 X-sec Clayton Hancock to Moors

57 Corner Stakes - Lot 65 Blvd Gardens

WABASH FREEWAY

WABASH AVE. - BRIDGE

0+65

Bent No 2

Cross Sections - Bents

0+55 = End Footing

0+27.5

INDEXED
MJK
MAY 24 1950

0+00 Beg. Footing

0-10

Bent No 17

0+50.2

0+40.2 = End Footing

0+00 = Beg. Footing

0-10

20044
BM = Disc. MH.

Walker
F. Gregory
G. Pope
R. Sission
4-13-50

Lt.

C

Rt.

2

195.8 196.2 196.7
10 10

195.7 196.2 196.8
10 10

195.5 196.1 196.3
10 10

195.4 195.7 195.9
10 10

195.1 195.1 195.7
10 10

195.0 195.0 195.4
10 10

194.7 194.8 195.1
10 10

194.3 194.1 194.5
10 10

194.0 194.2 194.3
10 10

Wabash Bridge - Cross Sections
Cont. from p. 2

Bent # 47

0+42.13

Lt. 198.5 198.8 Rt. 199.0
10 10

0+39.13 = End Footing

198.5 198.7 199.0
10 10

0+00 = Beg. Footing

198.0 198.1 198.1
10

0-10

197.9 197.9 198.1
10 10

Bent # 37

0+65

197.7 198.1 198.2
10 10

0+55 = End Footing

197.7 197.9 198.1
10 10

0+27.5

197.1 197.4 197.8
10 10

0+00 = Beg. Footing

196.9 197.2 197.4
10 10

0-10

196.8 197.1 197.3
10 10

This Page Void

176 + 2172

55

52

49

176 + 0093

56

50

47

175 + 74.60

74

65

58

175 + 48.81

Col "A"

179.73

59

59

58

Wabash Freeway
Nile Street Bridge

Walker
Gregory
Pope
Sisson
3/1/50

5

	Col. "D"	7.9
	Col. "C"	8.2
	Col. "B"	6.4
Bent #4	Col. "A"	4.4
	Col. "D"	9.4
	Col. "C"	10.4
	Col. "B"	9.4
Bent #3	Col. "A"	4.3
	Col. "D"	9.4
	Col. "C"	10.4
	Col. "B"	10.2
Bent #2	Col. "A"	5.7
	Col. "D"	9.0
	Col. "C"	9.6
	Col. "B"	7.7
Bent #1	Col. "A"	5.1

9.25 178.93
2

169.68

~~98~~ ~~86~~ ~~79~~
B.M. on M.H. 100' Lt. Sta. 176+00

Cross Sections
Las Chollas Creek Bridge

Mulker
F. Gregory
G. Pope
R. Sisson

6

East Bulkhead

Cont. P-7

1+64.10 = Δ RT 42°45'

Sec RT Δ
TO Bulk Tern

TP

55.62

551
5 540 545
5

549

1+15

534
5 539 542
5

544
10

0+92

532
5 536 553
2

558
7

0+72

533
5 534 536
3

535
8 537
11 612
15 614
20

0+57

530
5 530 535
5

612
12 617
17

0+27

526
5 527 531
5

617
13 613
18

0+12.5 = Δ LT 20°01'52"

525
5 527 530
2

612
10 612
15

0+00 = Beg. SE Wing Wall

525
5 526 528
4

611
11 611
16

63.12

BM. 1st Fly. S. Pav.

Los Chollas Creek

East Blvd. Cont. from P-6

2104.6

579	587	578	578	585
10	5		8	10

1489

56.0	55.5	554	564	562
10	5		5	10

Los Chollus Creek Bridge

4

8

Cross Sections

West Blvd. & Wing Walls

1+87.17 = end NW Wing Wall

54.3 54.5 53.6 53.9
10 5 5

1+48.67

55.0 53.7 53.6 53.5
10 5 5

1+04.39 = NW ^{opp}

52.7 52.6 52.3 52.2
10 5 5

0+39.5 = A

53.2 52.6 52.5 52.1
10 5 5

0+26 = Δ Lt 14°02'10"

53.2 52.8 52.0 52.9
10 5 5

0+00 = Beg. SW Wing Wall

53.0 52.5 52.5 52.6
10 5 5

Las Chollas Creek Bridge
Cross Sections

Bent # 1

Col A	536
" B	535
" C	534
" D	534
" E	533
" F	532
" G	531
" H	530
" I	530

Bent # 2

Col A	550
" B	546
" C	540
" D	537
" E	535
" F	531
" G	531
" H	530
" I	527

Bent # 3

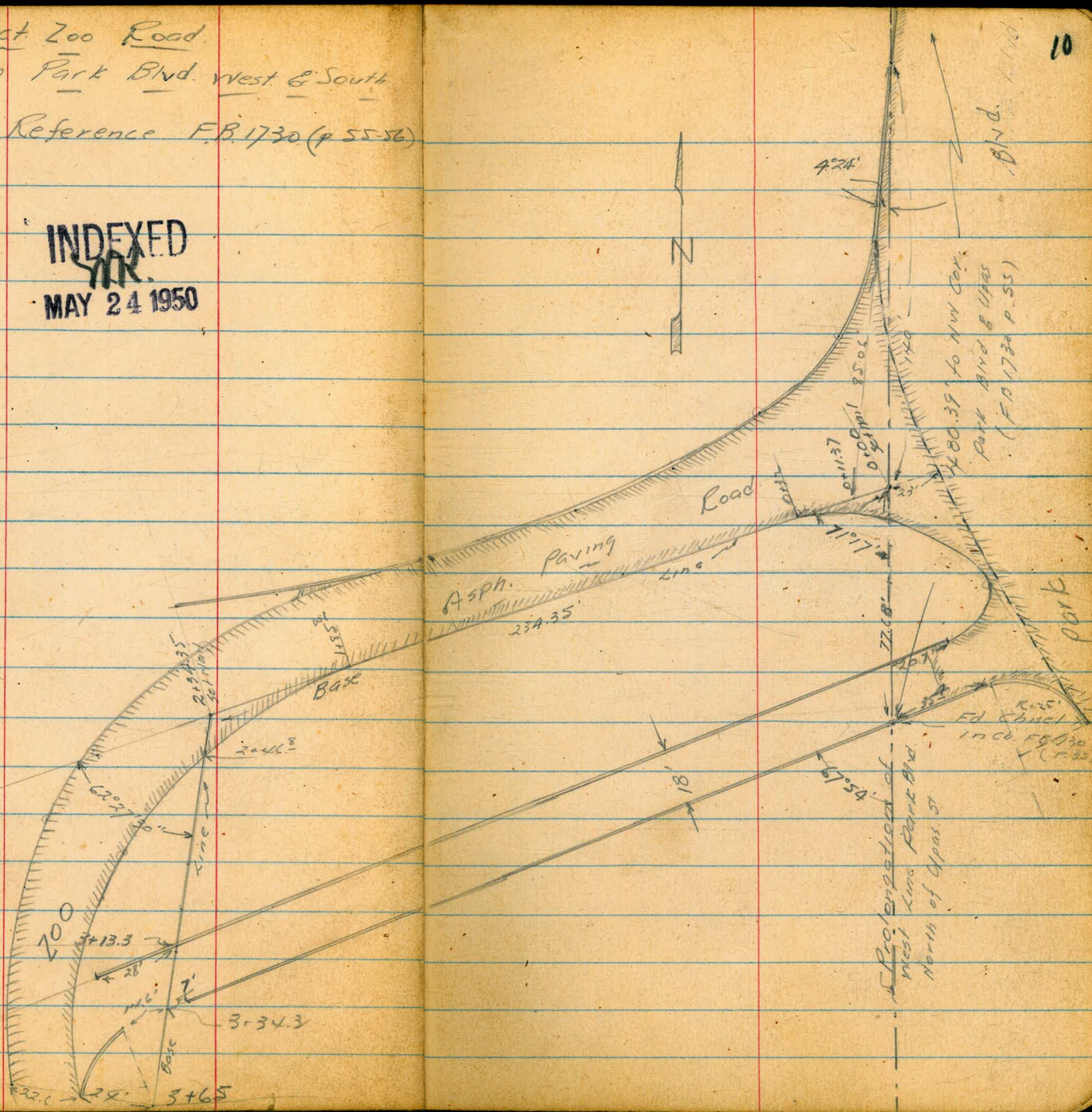
Col A	537
" B	536
" C	535
" D	534
" E	532
" F	531
" G	532
" H	529
" I	530

5-22-50
Hendricks
McCoy
Greer
Crawford
no# 25020

X Sect Zoo Road
From Park Blvd. West & South

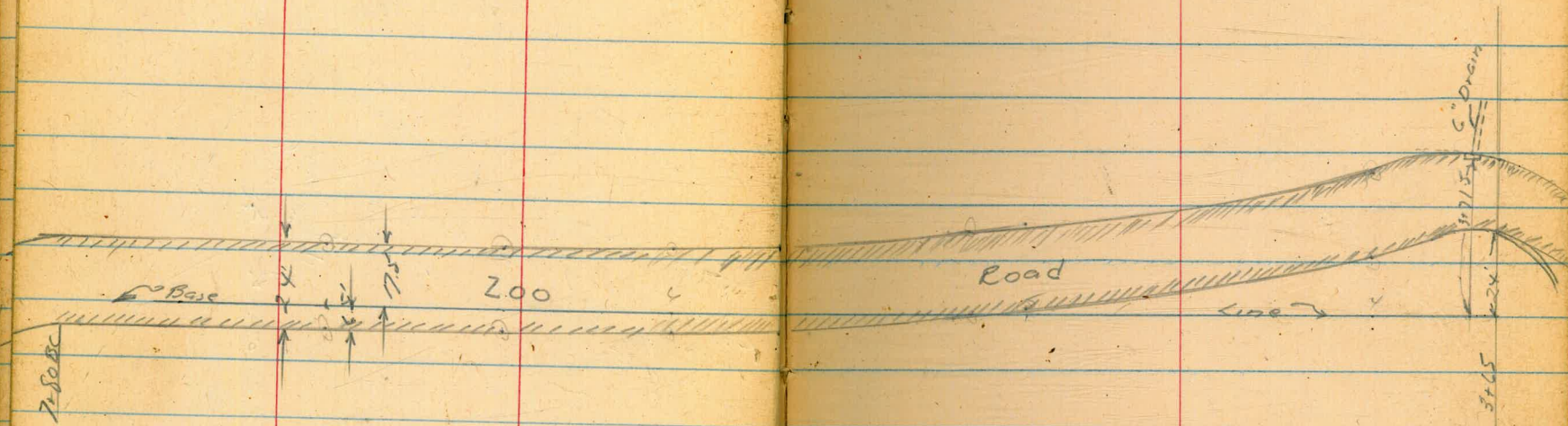
Reference F.B. 1730 (p 55-56)

INDEXED
M.R.
MAY 24 1950



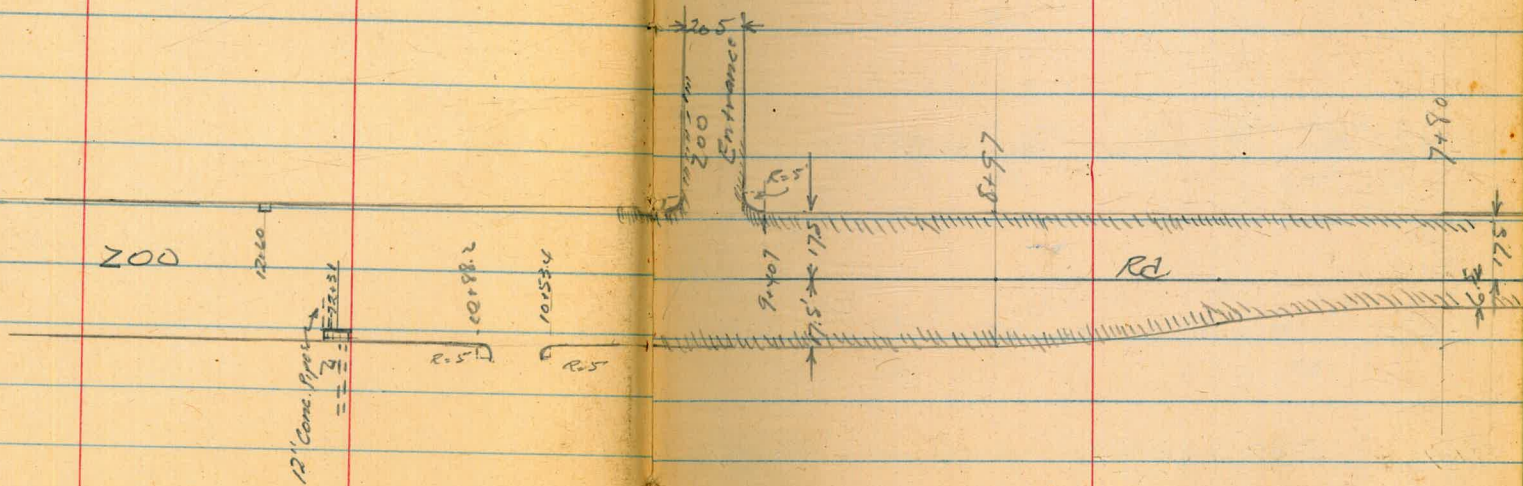
Zoo Rd Cont'd.

11



Zoo Rd. Cont'd

12



Levels Zoo Rd.

Base Line

0+32 Rt. L

294 ⁴⁶	294 ⁴⁷	294 ⁴⁸	294 ⁵⁰	294 ⁴³	294 ⁴⁵	294 ⁴⁷	294 ⁴⁹
73.5	73.5	55.5	55.5	(Pav.)	14	36.5	36.5
Cb.	G	G	Cb.			G	Cb.

0+11.37 Intersection of West Cb Line Park Blvd
(Section Parallel to Cb) 64 Rt)

294 ⁴⁸	294 ⁴⁹	294 ⁵¹	294 ⁵²	294 ⁵³	294 ⁵⁴	294 ⁵⁵	294 ⁵⁶	294 ⁵⁷	294 ⁵⁸
15	42	50	85	85	150	150			
			G	Cb.	G	Cb.			

0+00 Rt. L

294 ⁶⁰	294 ⁶¹	294 ⁶²	294 ⁶⁴	294 ⁶⁵	294 ⁶⁷	294 ⁶⁸	294 ⁶⁹
72	72	54	54	118	16	52.2	52.2
G	G	Cb.	Cb.	Pav.		G	Cb.

0-23 Intersection
(Edge Main Paving Park Blvd)

294 ⁷⁰	294 ⁷¹	294 ⁷²	294 ⁷³	294 ⁷⁴	294 ⁷⁵	294 ⁷⁶
75	75	50		41	77.5	77.5
Cb.	G				G	Cb.

0-53 Section at Rt. L

294 ⁸⁰	294 ⁸²	294 ⁸⁴	294 ⁸⁵
75	50	50	75

BM 5.07 299.54

294.47

Chisel x in Cb. CP #1 FB1730 P.56

2+3435 L. 14 (section Rt. G. to back tan)

293² 294⁰-293⁴ 293⁸ 293¹³ 293³⁸ 293⁰ 293⁴⁹
 50 26 12 85 18 37.2 37.2
 Pav. Pav. G Cb

2+00

294¹ 294⁴ 293⁸ 293²⁵ 293²⁵ 293⁴⁸ 293⁴⁰ 293⁵ 293⁵⁸
 50 20 5 1 14 24 30.5 30.5
 (Pav.) Pav. G Cb

T.P. 4.14 29786 582 29372

1+86

293¹⁷ 294⁴ 293⁴ 293⁷² 294¹ 293⁴² 293³⁴ 293⁶⁷
 829 829 648 648 16 (Pav.) 29. 28
 G G Cb G Cb

1+50

293⁸⁴ 293⁸ 293⁵ 293⁹⁴ 294⁵ 293⁶⁷ 293⁸¹ 293⁴¹ 293⁷⁵
 81 81 63 63 15 Pav. 11 25 25
 Cb G G Cb G Cb

1+00

294²⁰ 293² 293⁵ 294⁵ 294⁵ 293⁹³ 294⁰³ 293⁶¹ 293⁸⁹
 78 60 60 28 Pav. 10 24.8 24.8
 Cb. G G Cb G Cb

0+65

294²¹ 294⁴ 293⁹ 294³⁰ 294⁹ 294¹³ 293⁶¹ 294⁰¹
 76 76 575 575 25 (Pav.) 28.6 28.6
 Cb G G Cb G Cb

29954
 A

3+65 Beg. Cb on Rt.

Baseline

294 ³	292 ⁶	292 ⁸⁸	292 ⁶⁴	292 ⁶⁵	292 ⁹⁴
50		24	24	46.6	46.6
		Cb	G	G	Cb

3+34.3 Mt.

292 ⁹	293 ⁴⁴	292 ²	292 ²⁴	292 ⁸	292 ⁹¹	292 ⁶
50	50	7	7		14.6	14.6
G	Cb	G	Cb		Cb	G

3+13.3 Int. Ho. Cd. Line (Section along Cb.)

293 ⁰	293 ⁴¹	293 ²⁷	293 ¹⁹	293 ⁰
40	40	Cb	28	28
G	Cb	292 ⁸	Cb	G
		G		

3+00

292 ⁸	293 ³⁶	293 ⁶	293 ⁴	292 ⁶⁸	293 ⁰⁴	292 ⁶
21.5	21.5		20	26	52.5	70
G	Cb			Pav.	Pav.	

2+72

294 ⁰	293 ⁹	292 ⁸⁵	293 ¹⁴	293 ¹
50		16.5	44.2	50
		Pav.	Pav.	

2+46.8 Edge Pav.

294 ⁴	293 ³	292 ⁹⁰	293 ²⁵	292 ⁷
25	4	Pav.	31	50
			Pav.	

297.86
X

Zoo Rd. Cont'd.

Base Line

11

5+16.5 Int. Ch line on Lt.

295°	293 ³¹	293 ²⁸	293 ⁰⁰	292 ²⁸
50	293 ⁰⁰	14	24	24
	G		G	cb.

T.P. 5.34 298.42 4.78 293.08

5+00

295°	293 ²⁷	293 ³⁰	292 ⁹⁷	292 ²⁴	292 ²²
50		18	18	26.1	20.1
		cb	G	G	cb

4+50

294 ⁹	293 ⁶	293 ¹⁴	292 ⁸⁴	292 ¹⁵	292 ¹⁵
50		8	8	21	32.2
		cb	G	G	cb

4+33 Fire Hydr. 19.2 ft.

4+00

294 ²	293 ⁶	293 ⁰⁰	292 ⁶⁸	292 ⁹⁵	292 ⁶⁹	292 ⁹⁷
50		16.4	16.4	30	40.8	40.8
		cb	G		G	cb

3+71.5 1.2' x 2' Grate on Rt.

292 ³⁵	288 ⁶⁴	292 ⁹⁵
46.9	46.9	46.9
Grate	Fl	cb

297.86

Base Line

7+80 B.C. (cont. cb)

295 ⁶	292 ⁸¹	292 ⁴⁶	292 ⁶⁵	292 ²¹	292 ⁴⁹	292 ⁸⁰
42	6.5	6.5		6	17.5	17.5
	cb	G			G	cb

7+50

294 ⁸	293 ¹³	292 ⁸¹	292 ⁹⁸	293 ⁰⁴	292 ⁷⁶	293 ⁰⁹
50	6.5	6.5		7	17.5	17.5
	cb	G			G	cb

7+34 Fire Hydr. 19.1' Lt.

7+213 (Power Pole 32.8' Lt.)

7+00

295 ⁰	293 ⁵⁰	293 ¹⁸	293 ³⁵	293 ⁴¹	293 ¹⁵	293 ⁴⁶
50	6.5	6.5		6	17.5	17.5
	cb	G			G	

6+50 Approx. E.C.

295 ⁰	293 ⁶⁵	293 ²⁴	293 ⁴⁹	293 ³³	293 ⁶²
50	6.5	6.5		17.5	17.5
	cb	G		G	cb

6+00

295 ⁰	293 ⁵³	293 ²⁴	293 ⁴⁵	293 ⁵⁴	293 ²³	293 ⁵⁴
50	5.5	5.5		6	18.5	18.5
	cb	G			G	cb

5+50

294 ⁹	293 ⁴¹	293 ¹⁰	293 ²⁰	293 ³⁸	293 ⁰	293 ⁴²
50	2.8	2.8		9	21.2	21.2
	cb	G			G	cb

298.42
7

9+45.7 No. Line Entrance

290^{8.5} 291⁴ 291¹
 17.5 22.5 33.5
 Cb. &
 Drive

T.P. 508 295.30 8.20 290.22

290²⁵ 287⁰⁶ 291³⁸
 17.5 17.5 17.5
 Grade FL Cb.

9+23.4 E 1.2' x 2' Drain on Rt.

9+40.7 B.C. Cb Ret. (Zoo Entrance on Rt.)

293⁴ 291¹⁰ 290¹⁷ 291¹¹ 290⁸⁰ 291²³
 50 17.5 17.5 17.5 17.5
 Cb G G Cb

8+97 EC

293¹ 291⁵⁰ 291¹⁸ 291⁵⁰ 291²⁴ 291⁵⁴
 50 17.5 17.5 17.5 17.5
 Cb G G Cb

8+73 #E53
 (Power Pole 32.8 Lt)

8+47

294² 292¹¹ 291¹⁹ 292⁰⁵ 292⁰⁹ 291⁸⁵ 292¹⁷
 50 14.2 14.2 7 17.5 17.5
 Cb G G Cb

8+13

295¹ 292⁴⁰ 292¹⁰ 292⁴⁰ 292³⁹ 292¹³ 292⁴⁷
 50 8.6 8.6 6 17.5 17.5
 Cb G G Cb

298.42

T

Base Line

Zoo Rd. Cont'd.

10+83.2 So side opening

289⁷⁵ 289⁴³
22.5 17.5
Cb G

Baseline

10+58.4 No. side opening

289⁹⁶ 289⁶⁸
22.5 17.5
Cb G

10+53.4 BC Cb Ret on Lt.

291[±] 290⁰² 289⁷¹ 290⁰¹ 289⁷⁸ 290¹¹
50 17.5 17.5 17.5 17.5
Cb G G Cb

10+22 Power Pole # 32.4' Lt

10+00

292[±] 290⁴⁹ 290¹⁶ 290⁵¹ 290³³ 290⁶²
50 17.5 17.5 17.5 17.5
Cb G G Cb

9+71.2 EC. Cb Ret Zoo Entrance on Rt.

290⁹ 290⁷⁹ 290⁴⁵ 290⁸¹ 290⁶⁶ 290⁹²
40 17.5 17.5 17.5 17.5
Cb G G Cb

9+66.2 So line Zoo Entrance

290⁷² 290⁹⁴ 290⁹¹
17.5 22.5 33.5
G Cb & Dr.

29530
/

12+05 18" Euc. Tree

Base Line

12+00

289 ³	288 ⁴⁰	288 ²⁵	288 ⁵⁸	288 ²⁵	288 ⁵⁹
50	175	175		175	175
	Cb	G		G	Cb.

11+72 Power Pole 32.5' Lt.

11+60 30" Euc Tree 26' Lt.

11+50

290 ³	289 ¹⁰	288 ²¹	289 ⁰⁵	288 ⁸²	289 ¹⁵
50	175	175		175	175
	Cb	G		G	Cb

11+15 Power Pole 32.3 Lt.

11+04 Fire Hydr. 19' Lt.

11+00

291 ³	289 ²⁷	289 ²⁴	289 ²⁵	289 ³²	289 ⁶⁶
50	175	175		175	175
	Cb	G		G	Cb.

10+88.2 EC. Cb Ret. on Lt.

289 ⁶⁸	289 ³⁵
175	175
Cb	G

295.30
A

Zoo Rd. Contd

21

4.25 297.92 297.92

On Hub CP#3
(FB1730 R36)

Base Line

T.P. 13.01 302.17 3.00 289.16

14+00

287⁶ 286¹⁷ 286³⁰ 288⁵⁹ 286³⁰ 286⁶⁰
50 17.5 17.5 17.5 17.5
Cb G G Cb

13+50

288¹ 287¹² 286¹⁹ 287⁰⁹ 286²⁷ 287⁰⁹
50 17.5 17.5 17.5 17.5
Cb G G Cb

13+21 Power Pole 32.9' Lt

13+00

288⁵ 287⁶³ 287²⁸ 287⁵³ 287¹⁷ 287⁵⁰
50 17.5 17.5 17.5 17.5
Cb G G Cb

12+60 R 1.2 x 2' Drop inlet on Rt.

287³⁵ 283⁵⁸ 287⁹⁶
17.5 17.5 17.5
Grate FL Cb

12+50

288⁷ 288⁰⁹ 287²³ 288⁰⁰ 287⁶⁴ 288⁰²
50 17.5 17.5 17.5 17.5
Cb G G Cb

12+31 R 2.2 x 3.6' Drop Inlet on Lt

288²⁹ 283⁴² 287⁸²
17.5 17.5 17.5
Cb FL Grate

T.P. 4.34 292.16 7.48 287.82

(Top & Grate 17.5' Lt. 12+34)

295.30
11

Survey for Drain - S.W. Cor.
Wightman & Nile

7.0.

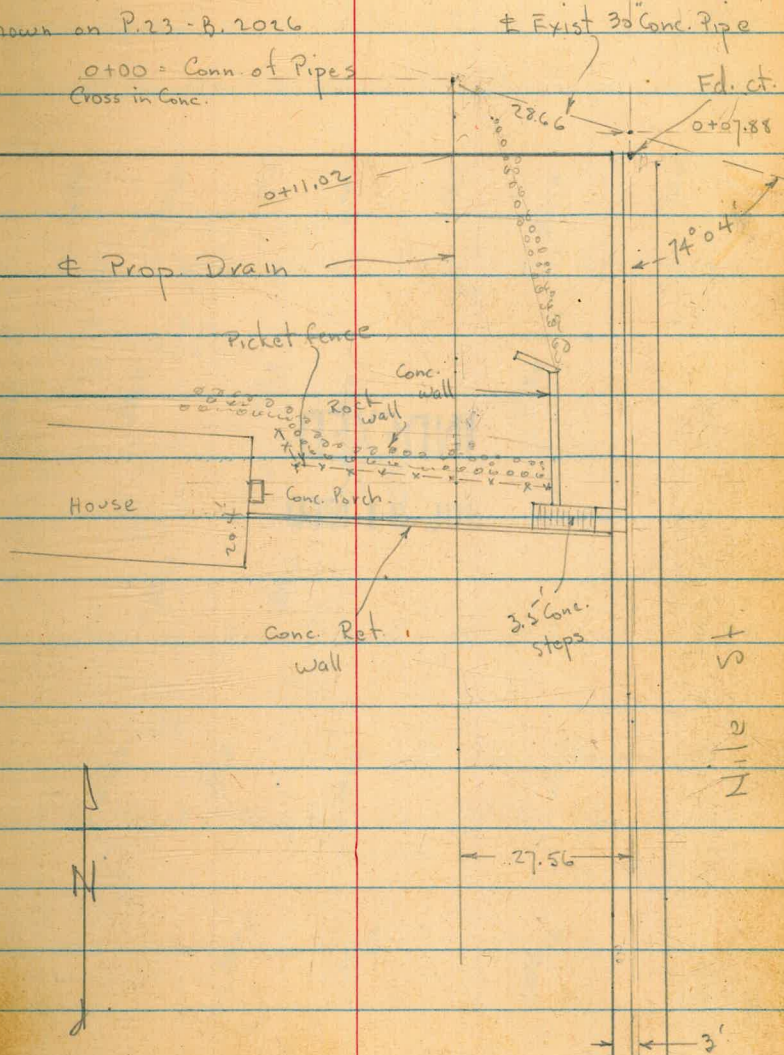
w.o. 20441

7-29-50

INDEXED
MK.
JUL 31 1950

Wightman - St.

Shown on P. 23 - B. 2026
0+00 = Conn. of Pipes
Cross in Conc.



Levels for Prop. Drain in Lots in
 NE. Cor. Blk. 187 ^{City 47s} - Conn. to Exist. Pipe
 Shown on P. 23-B. 2026 + Plan 7988-L

0+44 - 9.1 Lt. = End Rock wall + Beg. 11" Conc
 Wing wall

313.24	308.0	307.31	299.5	299.3	299.7	300.7	303.4
2.31	7.6	13.24	16.1	16.3	15.9	14.9	12.2
26.4	17	9.1	9.1		18	3.5	5.0
edge walk	Top Rock wall	Top Cond wall				Toe fill	on fill

0+20

INDEXED
 JUL 31 1950

312.8	306.0	299.3	298.1	299.0
2.60	9.6	16.3	17.5	16.6
26.4	12	8		10
edge walk	Top wall	Base wall		Toe fill

0+06 = 6 Lt. = Beg. Boulder wall - no mortar

306.9	301.1
9.7	14.5
17	6
Top wall	Base

Covered with Conc. Slab

0+00 = loc of End of old pipe + Conn. of New

312.22	312.1	297.95	301.1
2.83	2.8	17.60	14.5
26.4	23		10
edge Ret.		Top Conc.	on Fill

0-10

307.9	302.6	303.6
7.7	12.0	12.0
10		10

B.M. 0.53 315.55 ✓

315.02 = N.W. ct. Nile + Wrightman
 (No RECORD - AEC)

315.55 ✓

Lt. ♀

Rt. 24

Not Normal to st. - See sketch

0+69.35 - ♀ at N. face of 6" Top. Conc Ret wall

313.24	306.8	313.92	308.0	315.67
2.31	8.8	1.63	7.6	+0.12
24.1	ground	Top wall	32.9	32.9
end. wall			along House	Top wall

0+65.5 - 14.8' Lt = end Conc wall at Conc. steps

313.72	313.71	309.24	307.3	307.48
1.83	1.84	6.31	8.3	8.07
26.4	22.1	14.8	14.8	12.1
at walk	Top Step	Top wall	ground	Bottom Step

0+62 = Top Rock wall at ♀

313.58	309.11	306.85	306.3	307.6	308.70
1.97	6.44	8.70	9.3	8.0	6.85
26.4	14.8	14.8		29	29
walk	Top Conc. wall	Top Rock wall		Top Cor. Conc porch	

0+59 = Base of Rock wall - No mortar

313.51	313.3	304.01	304.8	304.8	301.7	307.3	307.6	308.92
2.04	2.3	6.54	10.8	14.8	13.9	8.3	8.0	6.63
26.4	25	14.4	14.4		15	25	31.8	floor along Elev.
edge walk		Top wall				Top wall	Conc found To House	2.9 from N. Cor.

0+46 - 10' Lt = ± 12" Plum Tree

0+457 - 14.5' Lt = Reg. 11" High Conc wall

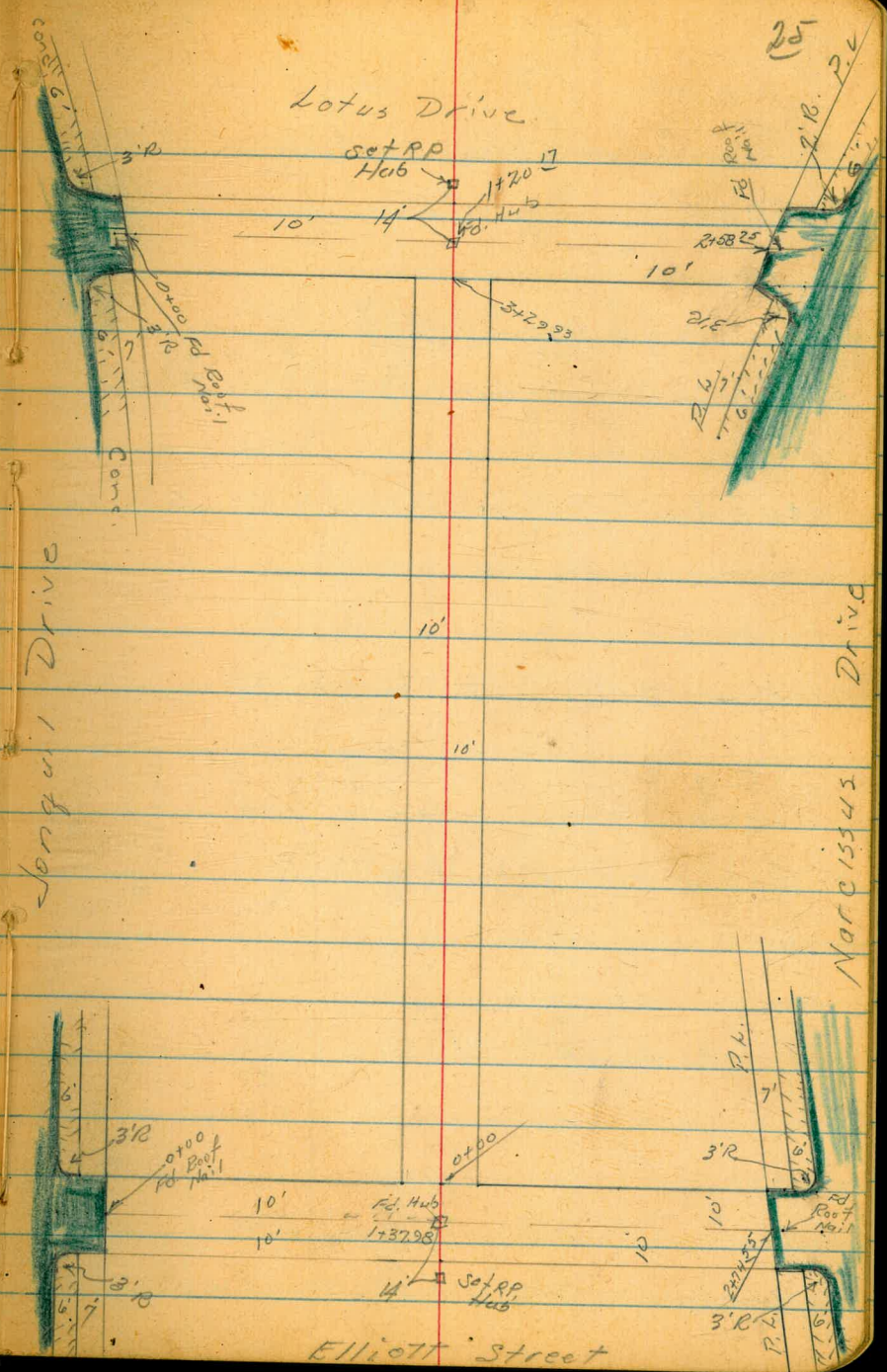
303.59	300.1
6.96	15.5
14.5	14.5
Top wall	

315.55 ✓

Johnson
Cota
Greer
Crawford
7-4-50
W.O. 31698
F.B. 1624-19

X-sect Alleys in BIK L
Plumosa Park

INDEXED
AUG 7 1950



X-sect. Alleys BIK "L"

Plumosa Park

South - East & West Alley

0+50

Lt.	\$	Rt.
0	162.6	161.9
9.9	0	10
	15/162.3	20

T.P. 0.94 162.91 7.14 161.97
 = 3" tree 9.3' RT 8" wide
 0+47 = Start 5' Conc. BIK Wall 9.9' Lt

161.86	162.4	162.91
7.25	6.7	
Rd	Grd	
9.9		
		163.7
		5.4
		5.70
		9.8
		Fd

0+20 = Start 4' Conc. wall 9.8' RT 6" wide

0+00 = East Prop. line Jenguil St

144.08	163.62	163.20
5.03	5.49	5.91
Cb		
10.1		
		5.72
		163.39
		162.66
		9.8
		Cb

0-13 = East Curb line Jenguil St.

164.28	163.72	162.80	162.24	162.22	162.07	162.94	162.85	162.37	162.17	162.71
4.83	5.39	5.21	5.27	5.29	6.04	6.17	6.26	5.74	6.24	6.40
Cb	G	Cb	G	10	6	10	G	26	G	Cb
4.5		13					13		37	

0-30 = E Jenguil St.

164.60	162.86	162.25
9.21	5.25	6.86
5.0		5.0

9.23 169.4 6.81 159.88

169.11

B.M.

9.55

166.69

157.14

S.W.B.P. Elliott & Narcissus

Xsect Cont.

0+91 = Start of 8" conc. fd 9^s Lt

0+82^s = Start 4' Conc. wall 10^s Rt

0+77 = 3' walk 9^s Lt

0+75^s = End 5' Conc. Blk wall 9^s Lt

0+69^s = 2 car garage 10^s Rt Apron 22^s wide

0+60 = End 4' Conc. wall 10' Rt.

0+59 = Power Pole - 8^s Rt PA 3678

158.16 Lt.
93^s Bottom
160.91
2⁰⁰ TOP
9^s

239.5992
161.7
10^s Fd. Grd.

162.09
08^s walk
161.5
14^s Grd
9^s

160.89
2⁰² Fd
161.4
10^s Grd
9^s

161.77
10^s Apron
0.88
14.2 Floor

10.1619
10 Grd
14.16147
14.16147 Fd

162.91

X-sect Cont.

1+58 = 2 car garage 9⁹ to Apron Lt. 15' wide

	156.53	160.31	♀		Rt.
	5.35	5.62			
	158	99			
Floor		Apron			

1+47⁹⁸ = East line North-South Alley
Power Pole 92 P.A. 3668

	156.9	157.1		157.3	157.9
	5.10	4.8		4.6	4.0
	10			5	10
					3.8
					20

1+27⁹⁸ = West line North-South Alley

	157.1	158.2		159.0	159.0
	4.1	3.7		2.9	2.9
	10			10	15

1+14⁵ = End 6' conc. wall 10' Rt

	160.2	159.16
	1.2	2.77
dirt		Found.
	10'	

1+11⁵ = End Conc. found. - 9⁹ Lt

	158.11	160.87	160.1
	3.82	1.06	1.8
Bottom		Top	dirt
	99		

T.P. 1.04 161.93 2.02 160.89

	158.16	160.87	160.2	161.93	160.3	160.8
	9.75	2.04	2.7	2.7	2.5	2.1
	98	98	5		6	10
				162.91		

1400

A-sect -
 South-East & West Alley.

Lt.

\$

Rt

30

Cont next Page

T.P.

3⁰⁸

159⁷⁶

5²⁵

156⁶⁸

3+05³⁵ ± = \$ Narcissus

49.59

12³⁶

43

10⁹⁵

161.93

150.98

152.04

9⁸⁹

31

X-sect Alleys BIK "L"

Plumosa Park

North-South Alley

1+65 = Power Pole - 9' Rt PA2678

1+48 = \$ 2 car garage 9' to Apron Rt ^{16' wide}

1+00

0+64 = \$ 2 car garage 9' Lt to Apron ^{16' wide}

0+55 = Power Pole 9' Rt PA2648

0+50

0+00 = North Line East-west Alley

Station 1+37.28 - 10' Lt

lt.	\$	Rt.
155.4	154.1	154.00
44	57	576
20	10	134
155.4	154.8	154.7
44	50	57
20	10	10
156.89	154.8	154.7
287	389	389
148	92	92
Floor	Apron	Floor
156.5	155.4	155.5
33	49	43
20	10	6
157.8	157.4	157.1
20	24	27
10	10	10
159.76 (see P. 30)		

X-sect.

North-South Alley

3400

2+75^s = Start 4' Conc. Wall 9^s Lt

2+65 = 2 car garage 11^s to Apron ^{ret} 20^s wide

2+60 = 2 Apron 10^s Lt 20' wide

2+50

T.P.

2+00

2 ³⁵	157 ⁸³	4 ²⁸	155 ⁴⁸
	1		

2+1 ²	4 ^{153.2}	8 ^{2.51}	5 ^{152.5}	5 ^{152.7}	5 ^{152.5}
20	4	8	5	5	5
10	5	10	7	10	20

50 ^s	4 ⁸⁸
11	172
Apron	Floor

2 ¹⁴⁷	4 ^{151.21}
26	10 ^s
Apron	Apron

4 ²	4 ⁶	4 ⁷	4 ⁹
10	10	10	20

4 ²	5 ^{154.3}	5 ²	6 ^{152.7}	6 ^{152.7}	6 ^{153.0}
20	10	5	6	10	20
		159 ⁷⁴			
		157 ⁸³			

Xsect - BIK "L"
PLUMOSA Park
North-South Alley

LT. £ RT

Cont. P. 34

T.P. 1332 165⁴⁷ 568 152¹⁵ = Hub on £ North-South & East-west Alleys.

3+79 23 = South Line East-West Alley

4/153.7	4/153.1	5/152.7	5/152.2
4!	4!	5!	5!
10	7		10
		15783	

X-sect - Alleys BIK "L"

PLUMOSA PARK

34

North-East & West Alley

0+34.5 = Power Pole 8th Lt A3675

0+15

LT.		RT.
5/160.5	5/160.0	5/160.5
5.0	5.5	5.0
15	10	7
		10
		20

0+012° = End Curb & Pav. 10' RT

Start 5' Hedge 11' RT

0+00 = East Prop Line Jonguil St.

161.09	161.29
4.38	4.08
G	CB
	10
160.57	
4.90	

0-018 = End Curb & Pav. 10° Lt

160.85	161.04
4.62	4.43
G	CB
	10

0-13 = East Curb Line Jonguil St

5/159.92	5/160.47	5/160.37	4/160.86	5/160.40	4/160.57	4/160.77	4/160.76	4/161.26	4/161.14	3/161.66
G	CB	G	CB	G	G	4.20	4.21	4.21	4.33	3.00
50		12.5	10	10	12.2	15.3	15.3	50	50	

0-30 = E Jonguil St.

4/160.82	4/161.37	3/161.98
4.5	4.10	3.59
50		50

165.47 (see P-35)

Xsect Cont,

North-East & West Alley

0+69 = £ Single garage 9' Rt to Apron
0+63 = End of 5' hedge 9.3 Rt

0+575 = £ double car garage 15' Lt to Apron

0+445 = £ single car garage 15' Lt to Apron

0+40

0+38

T.P.

0+36 = £ 4' walk 9.2 Rt

29	156.8	30	156.1	31	155.8 Lt	32	155.3	33	155.5	34	155.69	35	155.82 Rt
16		13		10		8		94		169			
												Apron	Floor

168 159.43 772 157.55

159.43
7.1 4.21
6 9.2 13
165.27

160.56
4.85

160.62

X-sect. Cont.

North-East & West Alley

1765

1740 = double garage 165 wide
10³ Rt to Apron

1735 = Power Pole 8.7⁴ PA 3661

1730¹⁷ = East Line North-South Alley

1710¹⁷ = West Line North South Alley

1700

0776 = start of 4' Cone wall 9² Rt

	152.1	152.0 ^{Lt}	151.0	150.9 ^{Rt}	151.1	151.3 ^{Rt}
	7 ³	7 ⁴	8 ⁴	8 ⁵	8 ³	8 ¹
	20	10	7		10	20
					7 ¹ _{1/52.28}	6 ¹⁰ _{1/52.53}
					10 ³	14 ²
					Apron	Floor

	6 ⁵	6 ⁴	7 ³	7 ²	7 ¹	
	20	10	6		10	
	6 ¹⁰	6 ¹⁰	6 ¹⁰	6 ¹⁰	6 ¹⁰	6 ¹⁰
	20	10	00	6	10	10
						Wall
	5 ⁴	5 ¹⁰	5 ¹⁰	5 ⁹	5 ⁷	5 ¹⁵
	15	10	8		6	10
						Wall

15943
↑

X-sect - Cont.

North - East & West Alley

2+62.25 = End of Curb & Pave 9' Lt

2+58.25 = West Prop. Line Narcissus

2+55 = End of Curb & Pave 10' Rt

2+35 = Power Pole - 9' Lt. A3651

T.P.

120 151.71
 ^
962 14981

2+00

1+79 = 1/2 Single Garage 8' Lt to Apron 9' wide

Lt. E Rt.

147.91
380
Cb
98.6
101
147.64
147.76
428

148.5
32
20
148.2
34
10
147.9
38
7
147.6
41
18.6
390
G
102
148.15
396
Cb

150.2
92
20
152.80
763
122
Floor
150.4
90
10
148.9
95
6
150.78
816
85
Apron
151.21
148.9
95
8
149.7
97
8
149.9
95
10
150.0
93
15

X-sect Cont BTK "L"
Plumosa Park
North-East & West Alley

Lt. \$ Rt.

0.02

Check Starting B.M. 0.75 157¹² 157¹⁴ J.W.B.P. Elliott & Narcissus
T.P. 8⁹⁹ 157⁸⁷ 2⁵³ 149¹⁰

2791²⁵ = \$ Narcissus (around Curve)

2773²⁵ = West Curbline Narcissus (around Curve)

			489	458	423				
	147.42		146.82	146.98	147.17		50		
			147.66	147.91	147.11				
			146.90	147.28	147.91				
			147.00	148.01	147.28				
	429	422	420	421	423	454	460	380	493
	Cb	G	Cb	G	99	North	G	Cb	G
		47		113		M.H.		182	50

157¹⁷¹
/

X Sec Hancock St

37

from Clayton to Sutherland

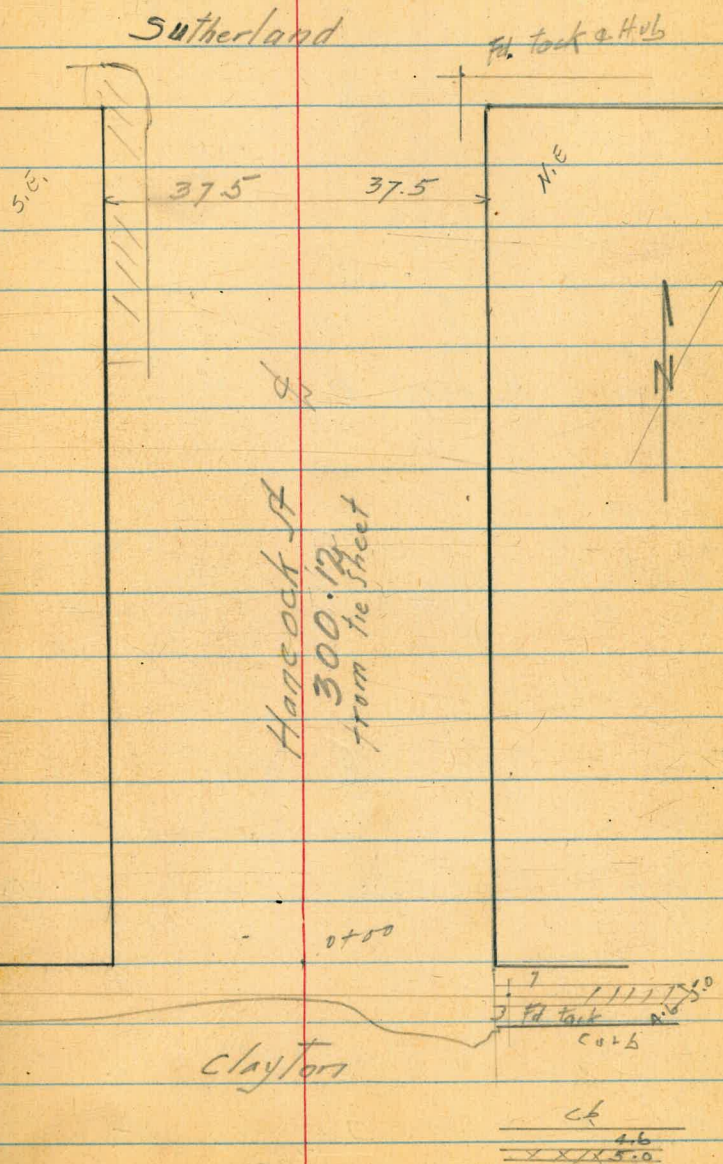
8/18/50

Begg
Johnson
Allan
Hatch

W.O. 31721

INDEXED
WJK
AUG 21 1950

Please verify tack -
Have assumed 7ft + 3' back
from property
not on tie sheet



Hancock St.

38

- 03

285 R. 2 WM

28.8	28.8	28.4	28.8	29.1	30.0	30.10	33.24	44.04
6.4	6.4	6.8	6.4	6.1	5.7	5.14	20	120
37.5	30	21	37.5	19	9	37	96	66

- 14

28.2	28.6	29.7	29.02	29.4	30.2	30.10	33.24	44.04
6.9	6.6	6.5	6.21	5.8	5.0	1.33	20	120
37.5	23	12	37.5	19	37.5	87.50	96	66

end of curb SW

- 40

28.7	29.4	28.6	29.14	29.27	29.6	30.10	33.24	44.04
6.5	5.8	6.6	6.10	5.97	5.6	25.14	15	063
40	26	22	40	12	23	37	87.5	66

- 66

J curb line

28.8	29.4	28.8	29.15	29.32	29.49	29.6	30.10	33.24
6.4	5.6	6.4	6.09	5.92	5.75	5.6	45	41
40	27	22	40	14	12	19	26	40

- 80

31.5 L 1797 P. Pole
S Line Clayton
P Pole 27.3 R 500206H

T.P. 7.44 35.24 435 27.80
BM 3.51 28.64
BM 6.55 32.15 25.60

35.24
BP N.W. Hancock & Sutherland
at SW cor Hancock & Noel P 17 28 / 41

BM This has gone 3.36

BM NE cor chis. □ in curb Ret.
Noel & Pacific 1728/41

Hancock St

0 + 57

10' drive

21.01
3.17
37.4 R

39
31.35
1.80
42.3

4.54 33.18 6.60 28.64

W

33.18
W

0 + 50

P.P. 31.6 L 1811
end of wall 37.5 R

28.5 28.6 28.0 28.5 28.9 20.4 21.1 20.8
6.7 6.6 7.2 6.7 6.3 4.8 4.1 4.4
37.5 26 21 17 28 37.5
Wall fat

0 + 45

g

9' wide drive 37.7 R

30.91
4.37
37.5

0 + 40

end of wall

+ 35

Pole 27.4 R 500208H

0 + 25

dead tree 29 R

0 + 03

dead tree 29 Rt.

0 + 00

N line Clayton

35.24

28.6 28.9 28.2 28.8 29.0 30.1 20.9 20.57
6.6 6.3 7.0 6.4 6.2 5.1 4.3 4.7
37.5 26 21 19 25 37.5
Wall fat

35.24
W

Hancock St

1 + 39 end platform 37.2 Lt

1 + 34

1 + 22

1 + 20 $\frac{1}{2}$ 2 wall 38.2 R

1 + 11 $\frac{1}{2}$ wooden step 38.8 Lt

1 + 00 end ret wall R. 39.9

0 + 89 beg Platform 37.0 Lt

0 + 62 beg ret. wall 37.3 conc

33.18

30.3
2.9
37.6
of conc steps
20.4
2.9
37.8
21.13
2.05 on step
2.13
37.8
3 wide steps

30.4
2.8
38.2
20.76
2.42
walk
38.2

28.8	28.8	27.7	28.3	28.5	29.2	30.7	31.54
4.4	4.4	5.5	4.9	4.7	3.9	2.5	1.64
37	26	21	15	15	29	37.5	37.9
							wall
				1.3	1.55		
				37.3			

33.18

2+00

36.6 Wall

27.0	27.9	27.9	27.2	27.8	28.2	29.1	29.7
6.2	5.3	5.3	6.0	5.4	5.0	4.1	3.5
37.5	36	26	25		23	29	36.4

1+98 of 3 conc steps

1+96 end of conc ret wall

1+74

31.5 ft 1829 Ppk
 36.8 ft 500209 ft

29.7
 3.5
 36.4
 30.02
 3.15
 56.6

1+69

of gar Rt 36.5 dirt floor

x

1+53

beg conc ret wall

29.5
 3.7
 36.5
 20.1
 3.1
 36
 32.82
 0.36
 21 Top
 2.45

1+52

of Ramp

2.97
 36.8 46

1+50

28.4	28.4	27.4	28.0	28.1	conc ramp	
4.8	4.8	5.8	5.3	5.1	4.1	3.2
37.5	27	22		15	26	36.8
						Wall

33.18

33.18

25+93 10" acacia 27.5 R

21+73 8" acacia 27.5 R

23+68 36 R. of con. steps 4 wide

29.1
29.46
4.5 4.14
36 R. steps

TP 594 33.60 5.52 27.66

33.60

28+53 24" 28 R 6" acacia

28+50 beg curb as walk

↖
drive way 30' wide
↘

	27.93	27.41	25.7	27.6	27.7	27.8	28.9	29.2	29.2
	5.25	5.77	6.5	5.6	5.5	5.4	4.7	4.0	4.1
	37.5		30.0		15	83	26	35	37

back edge of walk
& beg. buildg

24.89	27.40	27.55	27.15
8.29	57.8	5.63	6.03
50	39	345	30

28+20 33.18 30' bt beg driveway

33.18

33.18

7.98 25.62
 3 + 40' Sutherland

438 25.60
 225.7
 7.9 7.3 6.9 6.6 6.0 5.4 4.5 + 1.4
 37.5 30 15 14.4 15 25 37.5 81.5
 27.54
 27.6
 28.2
 29.1
 35.0

26.22
 3 + 14" curb line
 7.28
 ori curb
 50

25.1
 26.2
 27.6
 27.4
 6.2 6.0 5.6 4.4
 17 24 37.5
 29.2

3 + 00" contd.

29.8
 38
 37.5

3 + 00" S. Line Sutherland

27.38
 26.5
 27.0
 27.5
 27.6
 27.7
 28.5
 28.8
 6.2 7.1 6.6 6.1 6.0 5.9 5.1 4.8
 cb 31.0 15 13 20 26 27 36
 9
 File
 500210 H

2 + 94 30 ft E of curb
 33.60

27.78
 5.82
 37.5
 back of walk
 27.52
 6.08
 30
 26.4
 7.2
 30
 33.60

X-sec. Clayton - Hancock to Moore

Semmermeyer

Begg

Allen

• = Fd. L+T

INDEXED
Y.P.K.
OCT 5 1950

Oct.
W.O. 31721

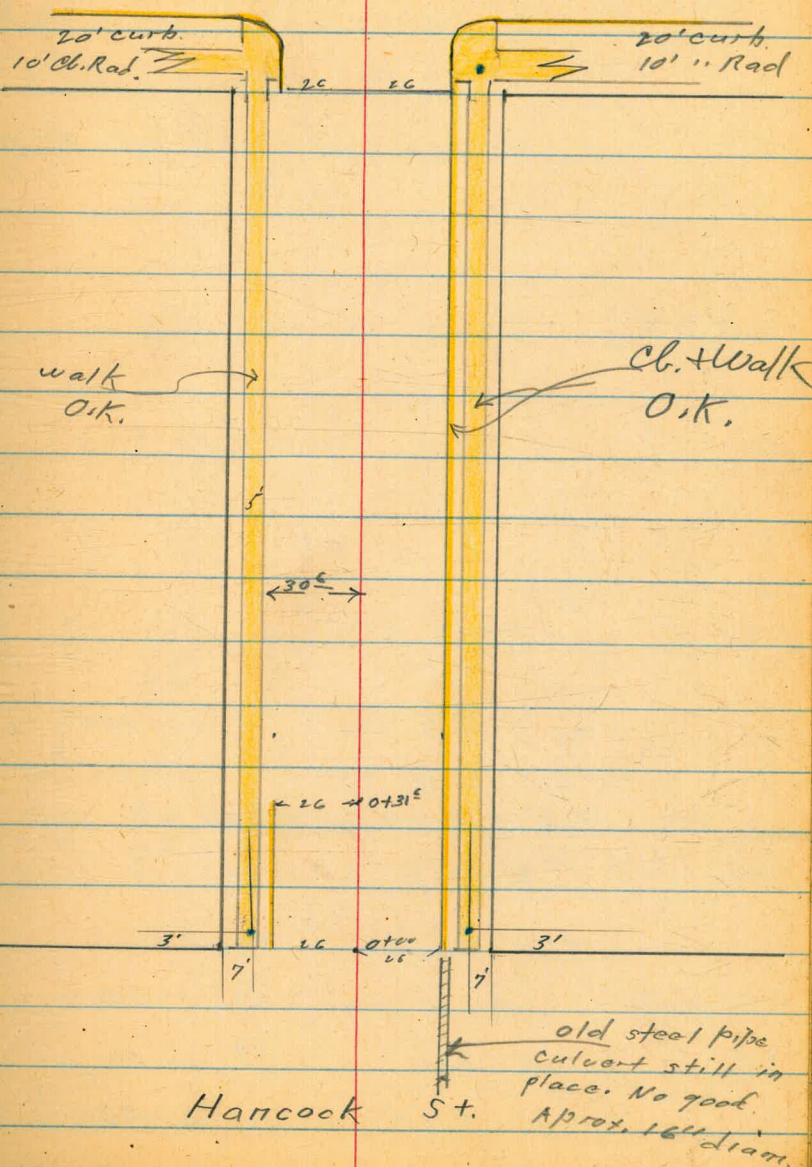
Moore St.

old iron or steel culvert dug up
at 25' Rt. of E at 0-02, at
0-10, and at 0-20.

Aprox. 16" diam. - No good.

W = street edge of walk

B.W. = property " " "



should come out from 0+194

This drive not needed. curb

0+315 26' Lt. = end curb (in drive)

0+28 start drive

0+194 - 26' Lt. = curb broken

0+00 Cont.

(See P 38 for intersection)

26' Lt + 26' Rt. = start conc. curb

0+00 = N. Ely line Hancock

check db. 37' Rt of 2 (0-14-P-38) { EL. Here. = 30.11 }
 { EL. P. 38 = 30.10 }

0.70 38.91 12.80 38.21

Set. B.M. #1 2.44 48.57

T.P. 2.56 51.01 12.97 48.45

1.39 61.42 60.03

5.81 5.91 6.17
 B.W. W. 26
 00.19
 drive

6.32 6.1
 26
 00.1
 31.84
 7.07
 26
 00.1

20.9	20.5	20.27	20.16	20.2	20.37	21.2	21.2
8.0	8.4	8.64	8.75	8.68	8.54	7.6	7.7
40	36	35	30	30	35	37	40
		B.W.	W	W	B.W.	End	
20.3	20.1	20.0	20.1	20.4	20.2	20.2	20.9
8.6	8.80	8.9	8.8	8.5	8.7	8.7	8.0
27	26	26	20	20	26	26	27
End	00.					00.	End.

38.91

sly. 7' Lt. Moore + Clayton

(this should be noted as Wly. cor.)
 N.W. B.P. Clayton + California

Clayton St

2+10 = 26' Lt. } = B.C. 10' Rad. cl. Rot.
26' Rt. }

26' Lt. = start curb.
2+00 = start A.C. Pavc

1+94

T.P. 5.99 52.91 2.92 46.92

1+50

1+00

T.P. 12.25 49.84 1.32 37.59

0+50

47.89	47.89	47.82	47.54	48.00	48.33	48.31	47.96	48.47
5.02	5.02	5.09	5.37	4.91	4.58	4.60	4.95	4.44
B.W	W	CC	G	13		13	G	CC
47.68	47.60	47.5	46.9	47.4	47.6	47.5	47.5	47.97
5.23	5.31	5.1	6.0	5.5	5.3	5.1	5.4	4.94
B.W	W	28	26	17		15	26	CC
<u>52.91</u>								
43.75	43.64	43.6	42.7	42.8	42.8	42.8	42.7	43.89
6.09	6.20	6.2	7.1	7.0	7.0	7.0	7.1	5.95
B.W	W	28	25	15		13	26	CC
29.25	39.09	34.5	37.7	38.2	38.4	38.3	38.0	39.29
10.59	10.75	11.3	12.1	11.6	11.4	11.5	11.8	10.57
B.W	W	27	23	13		13	26	CC
<u>49.84</u>								
34.75	34.63	34.3	33.3	33.7	34.1	33.8	33.8	34.69
4.16	4.28	4.6	5.6	5.2	4.8	5.1	5.3	4.22
B.W	W	27	26	18		20	26	CC
<u>38.91</u>								

Clayton

B.M.#1 - P 45

4.32 48.59 (48.57)

Moore St.

Cont.

36' Lt } = E.C. = 10' Rad. Cl. Ret.
36' Rt }
2+20 Sly. Cl. line Moore St.

5.14 140	4.94 90	4.78 40	4.72 26	4.62	4.37 26	4.15 40	2.77 90	1.27 140
47.77	47.97	48.13	48.19	48.29	48.54	48.76	50.14	51.64
5.32 140 Cl	5.65 140 G	5.11 90 Cl	5.50 90 G	4.89 40 Cl	5.29 40 G	4.33 40 Cl	3.32 90 Cl	2.91 90 Cl
47.59	47.26	47.80	47.41	48.02	47.62	48.58	49.59	50.00
48.03	47.65	47.81	48.10	48.26	48.26	48.19	48.17	48.62
4.88 36 Cl.	5.26 36 G	5.10 26	4.81 13	4.65	4.65 13	4.72 26	4.73 36 G	4.29 36 E.C.
								4.68 40 G

52.91

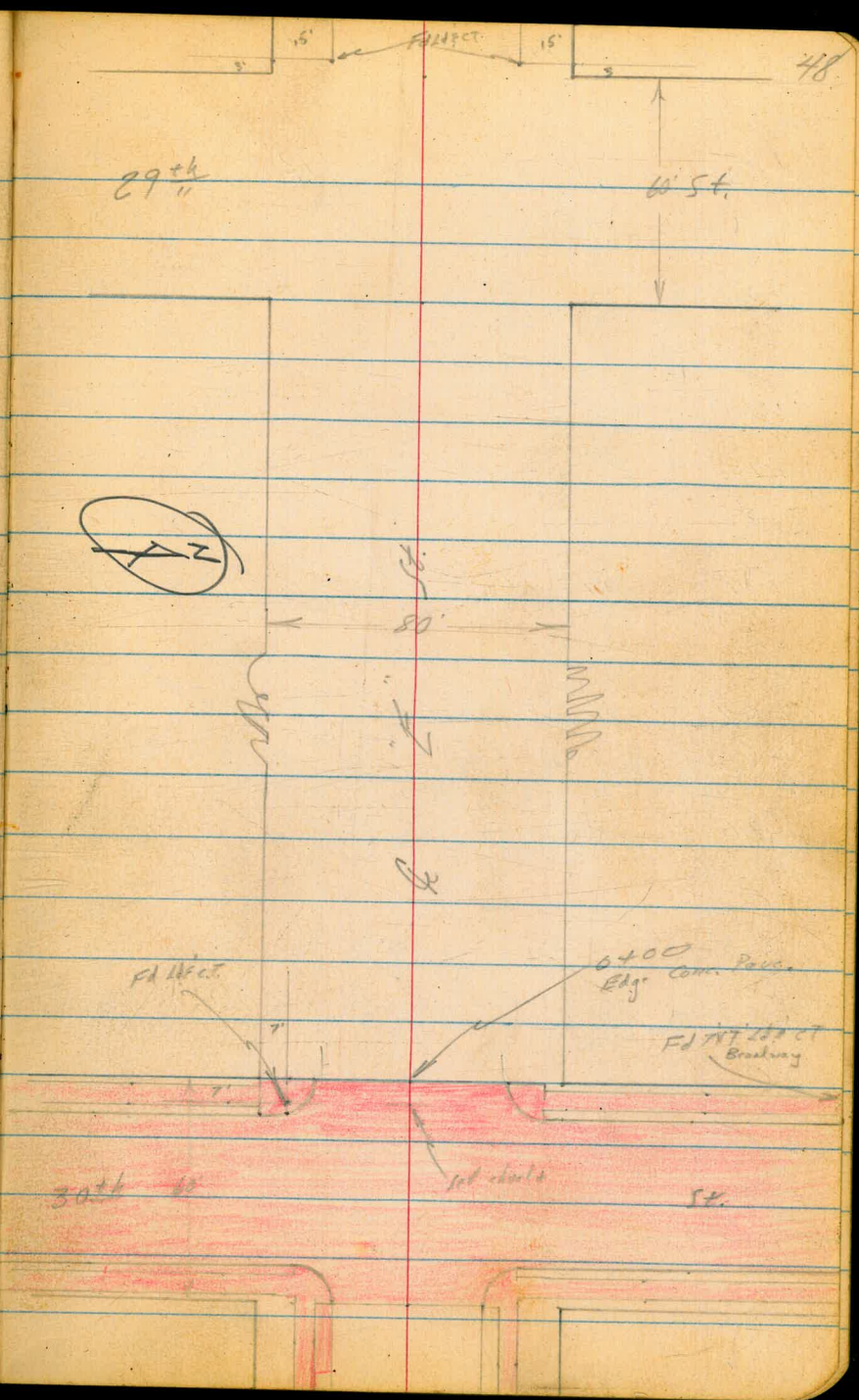
Roberts
Cota
Pollen
Fritz
5-31-51
W.O. 31712

X-Section "E" Street
30th ~ 300' Westerly

See TP 110

Reduced
6-1-51
Ryan

INDEXED
MAY 31 1951



Cont'd. From Page 48

0+53 31^E Rt to Center 12" Pepper Tree

0+51 40' Rt to Fence

0+50

0+44 28^E Rt to Meter Box

0+28 31^E Rt to Center 12" Pepper Tree

0+04 32' Rt to Center 8" Pepper Tree

0+00 W. Line 30th END Paving

Center Curb Return 10' Cb Rad.

0-10 West Curb Line 30th St.

BM

407 191.70A

187.63 NWBP

30th ¹/₂ E St.

191.70A

184.3	185.0	185.6	186.5	186.8	187.7	188.0	189.1
7.4	6.7	6.1	5.2	4.9	4.0	3.7	2.6
60	40	26		23	29	40	60

187.33
4.37
2.52
ON VALVE

185.24	184.99	184.61	185.44	186.13	186.54	186.79	187.24	187.73	187.90
6.36	6.71	7.09	6.26	5.57	5.16	4.91	4.36	3.99	3.8
40 walk	26 cb	26 cut	13		13	26 cut	26 cb	36 walk	40

185.05
6.63
cb

184.56
7.14
cut

186.74
4.94
cut

187.37
4.33
cb

182.33	181.63	184.98	184.29	184.99	184.42	184.75	185.81	186.62	186.82	187.98	186.92	187.58	188.81	189.45
7.31	10.07	6.72	7.41	6.71	7.28	6.95	5.89	5.08	4.88	4.42	4.74	4.12	2.89	2.25
40 cb	40 cut	40 cb	40 cut	36 cb	36 cut	26		26	36 cut	36 cb	40 cut	40 cb	40 cut	40 cb

Cont'd From Page 49

LT R 50

1421 30' Lt to Meter Box

184.26
7.44
30'
CONC
VALVE

1400

184.7 185.00 185.8
7.0 6.7 5.9
60 40 20
186.25 186.4 187.1 187.8 189.2
5.5 5.3 4.6 3.9 2.5
24 27 40 60

0+98 40' Lt to 3' Conc. Walk

184.85 185.10
6.85 6.60
50 40
CONC CONC

0+81 40' Rt. 4' Conc. Walk

188.41 188.80
3.29 2.98
40 50
CONC CONC

0+72 24" Lt to Meter Box

184.61
7.09
24"
ON
VALVE

0+69 28' Rt to Meter Box

187.38
7.32
28'
ON
VALVE

0+56 40" Lt & 3' Conc. Walk

185.00 185.46
6.76 6.24
50" 40"
CONC CONC

191.70X

191.70X

1486 35' Lt to Meter Box

178.17
2.15
35
ON
VALVE

T.P. 0.47 180.32X 11.85 179.85

180.32X

1470 20' Rt to Meter Box

181.60
10.1
20
ON
VALVE

1456 { 58' Rt & 7' Conc Drive
47' Lt & 2 Strip Drive }
strips - 2'
overall - 62'

182.4
181.94
9.1 9.76
57 CONC 47' CONC

185.14 185.6
654 6.1
582 CONC 682

1450

183.3 183.1 182.8 183.2 183.4 184.9 185.6 186.5
8.4 8.6 8.9 8.5 8.3 6.8 6.1 5.2
60 40 29 17 28 30 60

1433 41' Rt & 3' Conc Walk

187.00 188.58
4.30 3.12
41 CONC 51 CONC

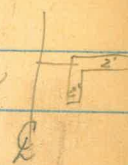
1430 20' Rt to Meter Box

185.31
6.39
20
ON
VALVE

2+37 Rt & Dirt Drive

172.4
7.9
40
172.4
7.9
60

2+30 36' Rt & 2' Conc Walk



172.17
8.5
36
conc
172.23
8.09
46
conc

2+23 40' Lt & 4' Conc Walk

174.72
5.60
502
conc
174.42
5.90
403
conc

2+10E 35' Lt to Meter Box
26' Rt to Meter Box

174.75
5.57
33
ON VALVE

174.95
5.47
26
ON VALVE

2+06 34' Rt to Conc Landing & 5 Steps
STRT to

176.38
3.94
34

2+01E 57' Lt & 7' Conc Drive

175.87
4.45
672
conc
175.78
4.54
572
conc

2+00

175.8
4.5
60
175.9
4.4
40
177.0
3.3
20
177.0
3.3
20
176.5
3.8
20
176.3
4.0
40
176.3
4.0
50

Cont'd From Page 52

Check			3.10	187.62	=	187.63
T.P.	10.17	190.72	0.09	180.55		
T.P.	12.50	180.64	0.11	168.14		
3+25		Creek Bottom				

Lt.

E

Rt. 53

135.2
33.1

3+00

	153.8	153.7	153.0	152.0	152.6	152.0	151.1
	145	146	153	163	157	163	172
	60	40	20		20	40	60

2+85

	164.2	165.3	166.3	157.1	156.3	156.0	155.4	154.1
	4.1	3.0	3.0	11.2	12.0	12.3	12.9	14.2
	60	40	36	20		20	40	60

T.P.

0.64 168.25 π 12.71 167.61168.25 π

2+67

Lt & Dirt Drive

	165.1	166.2
	15.2	14.1
	60	40

2+58

41E' Lt & 21' Conc Walk

	166.82	167.20
	13.5	13.12
	51E conc	41E conc

2+49

35 Lt. to Meter Box

	167.2	169.1	167.97	169.9	171.5	171.7	172.3	172.3
	13.1	11.2	12.85	10.4	8.8	8.6	8.0	8.0
	60	40	35 on velve	20		20	40	60

2+45

1X1 P.O.T.

180.32 π 180.32 π

Garber
Cota
Püller
Bruner

(Cont. from P. 53)

7/3/51

W.O. 25020

JUL 5 1951

INDEXED

57

Lt.

℄

Rt.

+83

Ely side house 60.6 Lt

12.5 Dirt Fl. Garage
60.6 under house

+75

12.19 159.08 0.32 146.89

12.9

40

159.08 T

+6.7

35

+7.0

40

+50

+25

Toe of 1x1 Slope

9.3

40

5.2

3.2

18

+18.7 Top Slope

58

+400

+96

Sewer M.H. on ℄

12.7

9.3

7.6

40

14.2

40

12.2

11.2

40

12.56 Rim

3+50

10.0

14.0

40

30.

13.3

12.5

40

7.00 147.21 12.04 140.21

147.21 T

0.55 152.25 12.44 151.70

0.43
0.14 164.14 12.61 163.71

0.27 176.32 12.79 176.05

1.21 188.84 187.63 NWBP

30th ℄ F

146.6

146.2

137.9

134.5

133.0

137.2

133.2

149.3

142.0

137.9

135.0

133.9

165.8

144.0

139.6

136.0

166.1

165.9

134.7

+31.5

29th

165.2
5.2
40
164.6
5.8
40
165.0
3.1
20.5
167.3
5.4
14
169.2
1.25
40
169.18
+0.96
19.5
171.39
+2.15
40
172.54

6+00

171.4
+1.0
40

+50

158.3
12.1
40
160.3
10.1
32
160.0
10.4
14
165.2
5.2
170.43
170.2
0.2
40

11.68 170.43 0.33 158.75

+34

Water Meter 34.8 Rt.

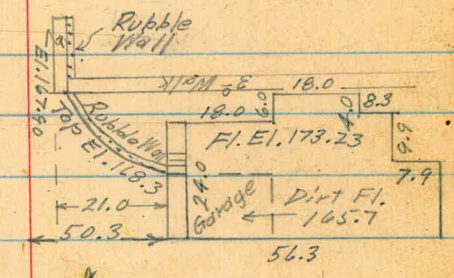
+19

Water Meter 31.4 Lt

5+10

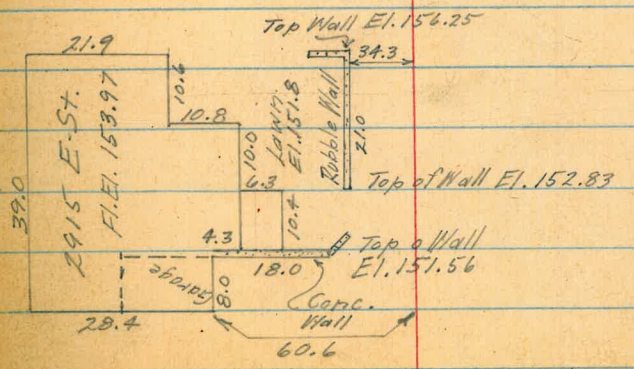
Ely side of house

5+00



4+83.0

159.08



159.08

				NWBP 30° 8' E Rec. 187.63
	3.56	187.62		
8.69	191.18	0.47	182.49	
12.71	182.91	0.23	170.20	
	170.43			

2-13-52

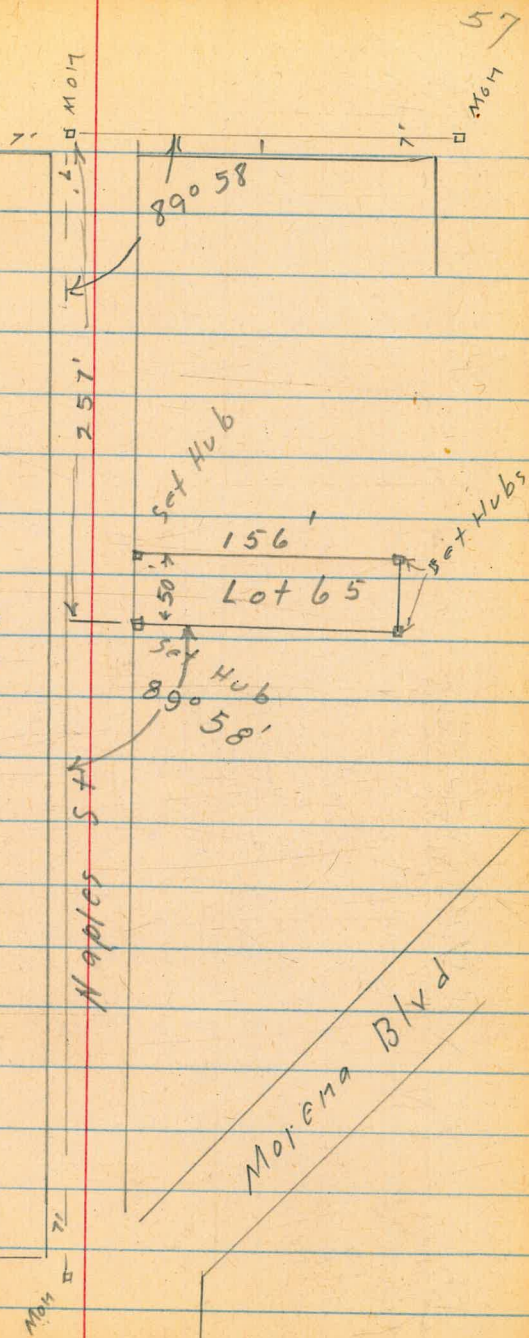
Hardin
Hatch
Pearson

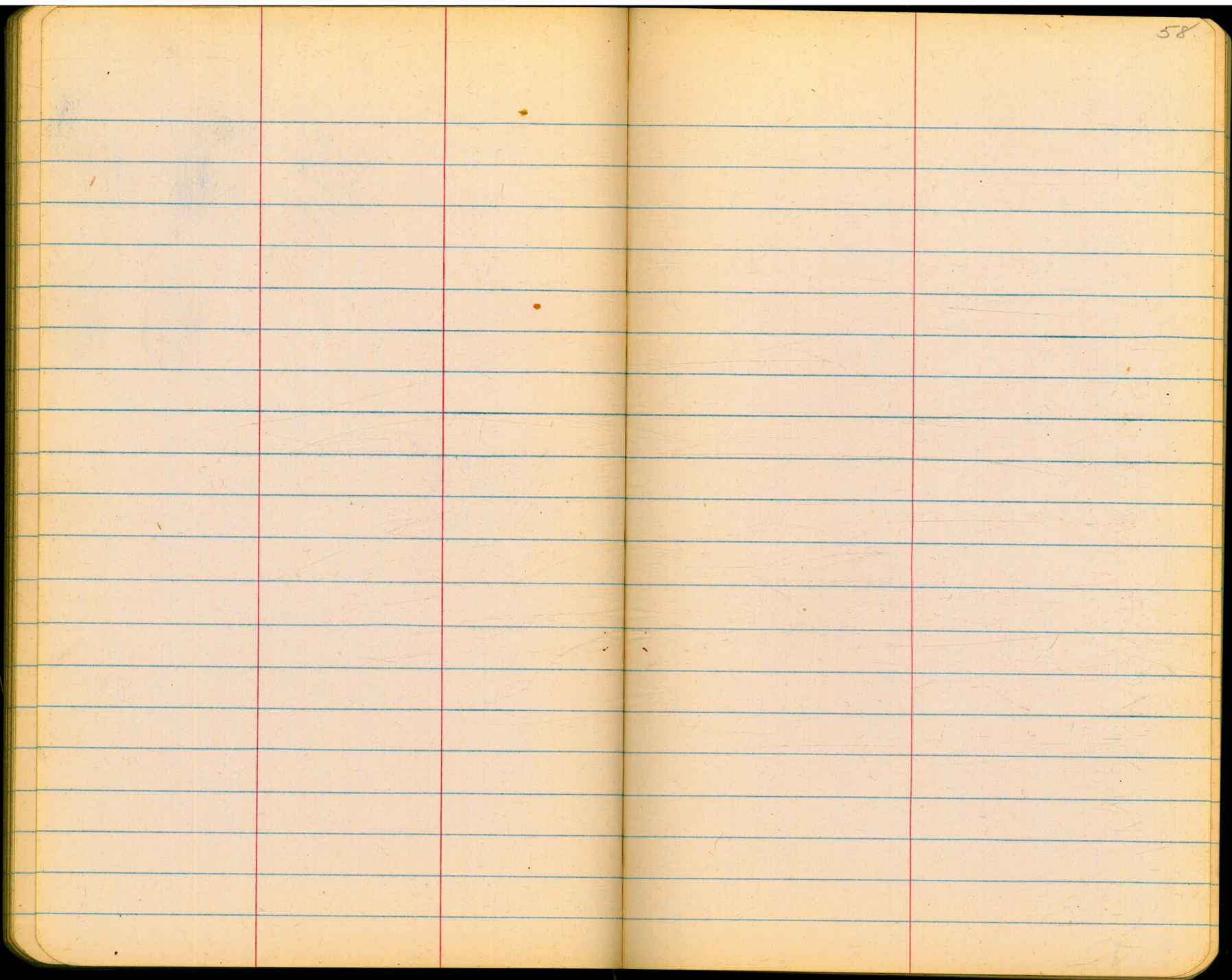
W.O. 22051

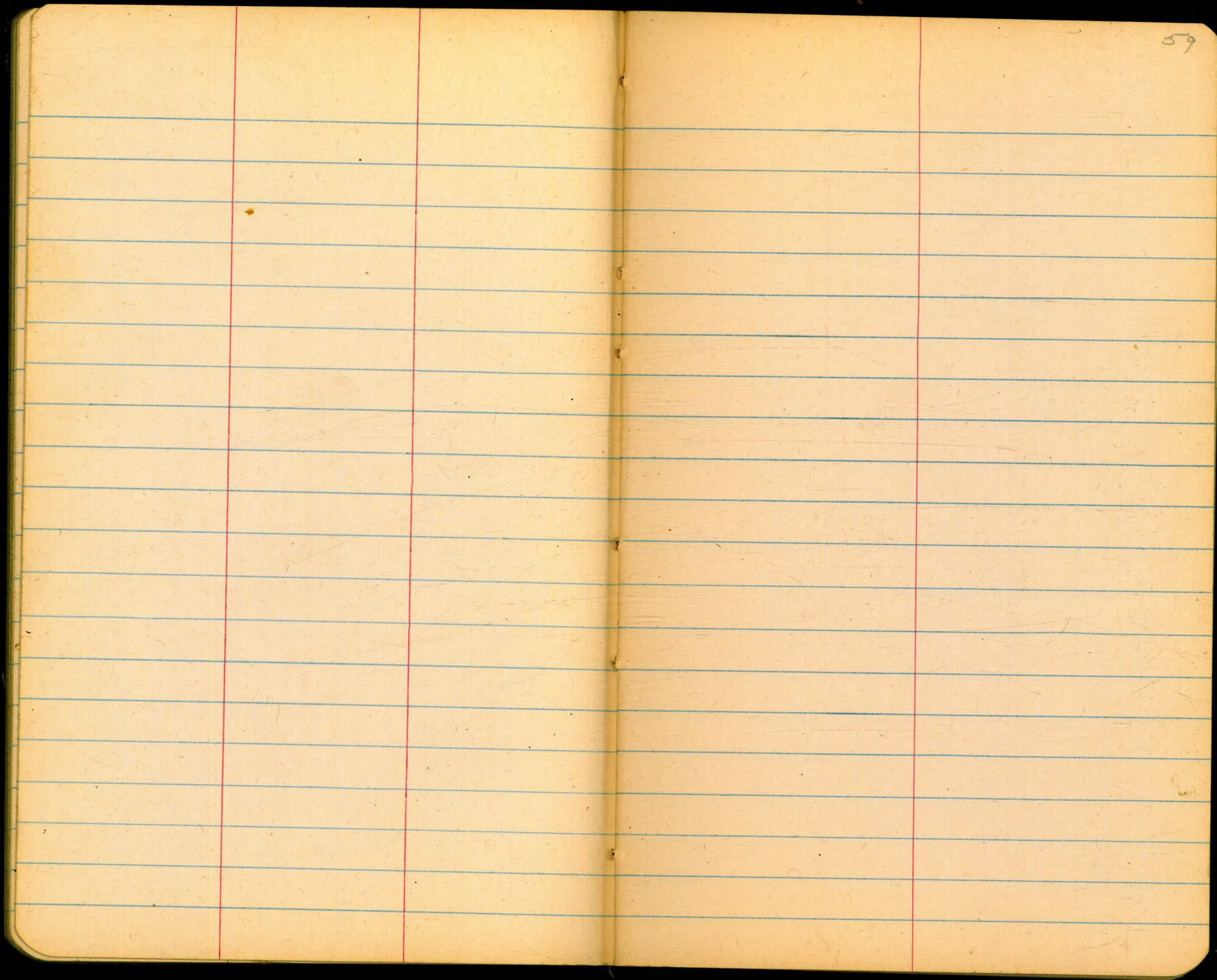
Stake Lot 65
Boulevard Gardens
on Naples Street

Yegga St

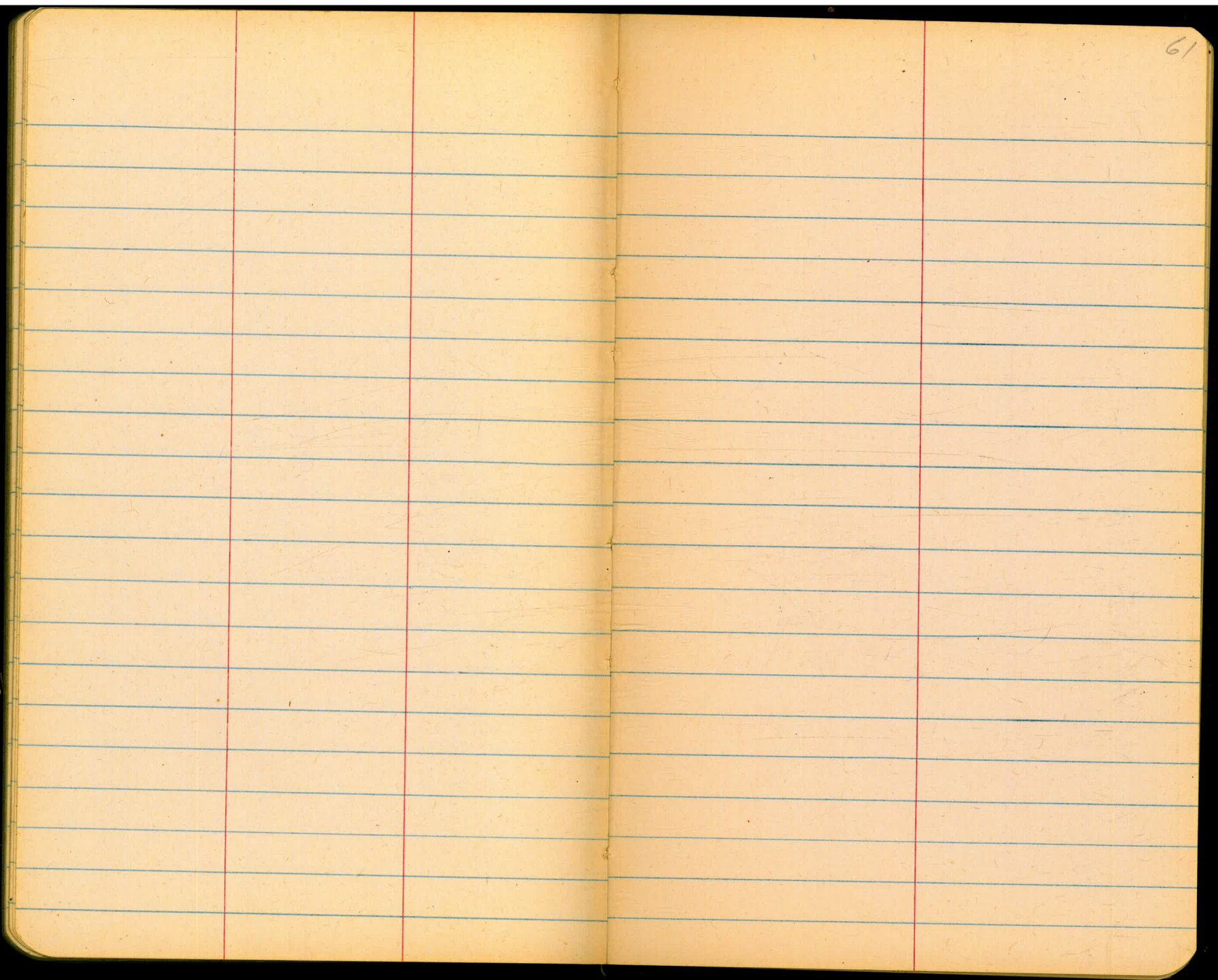
INDEXED
Hub
FEB 15 1952

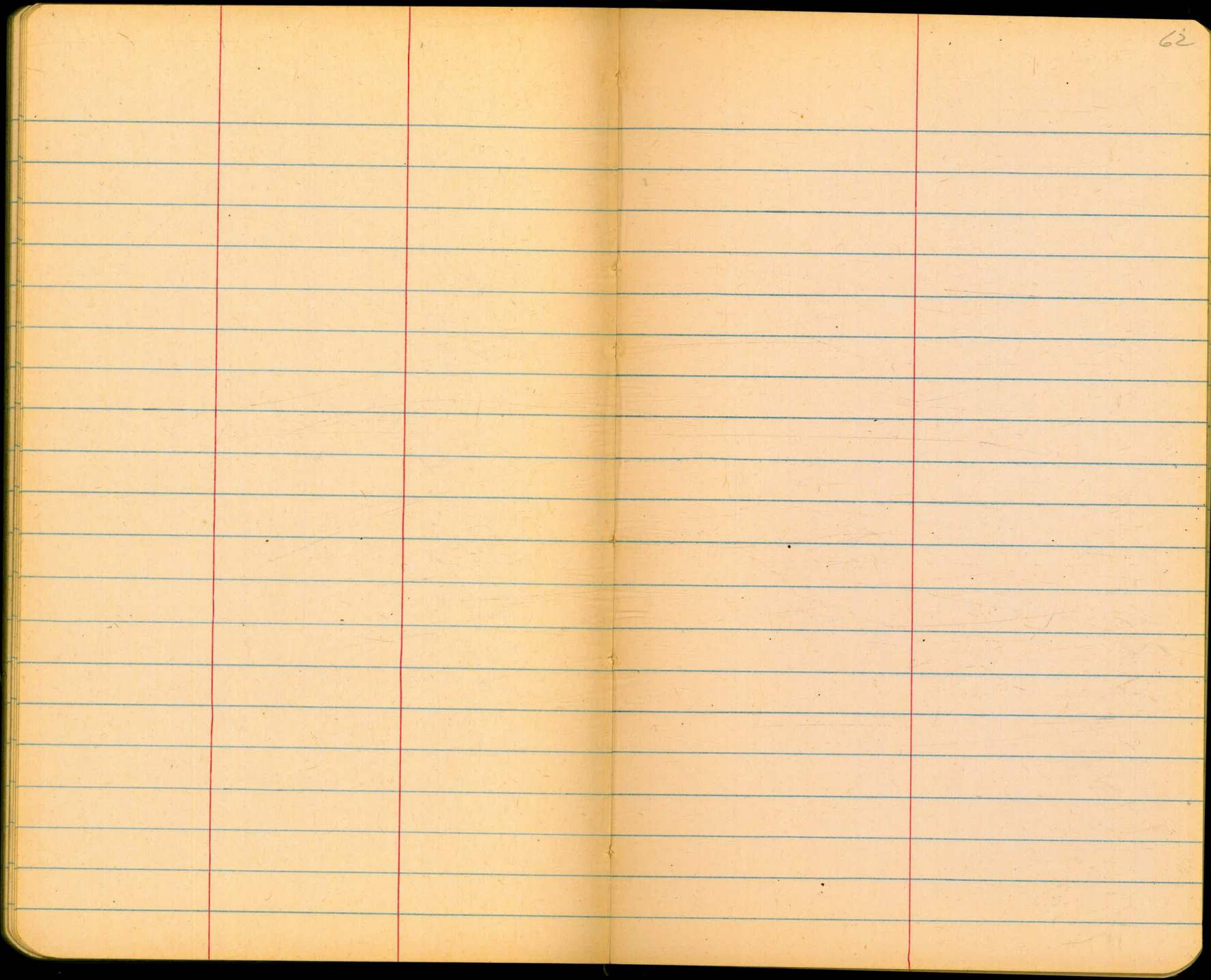


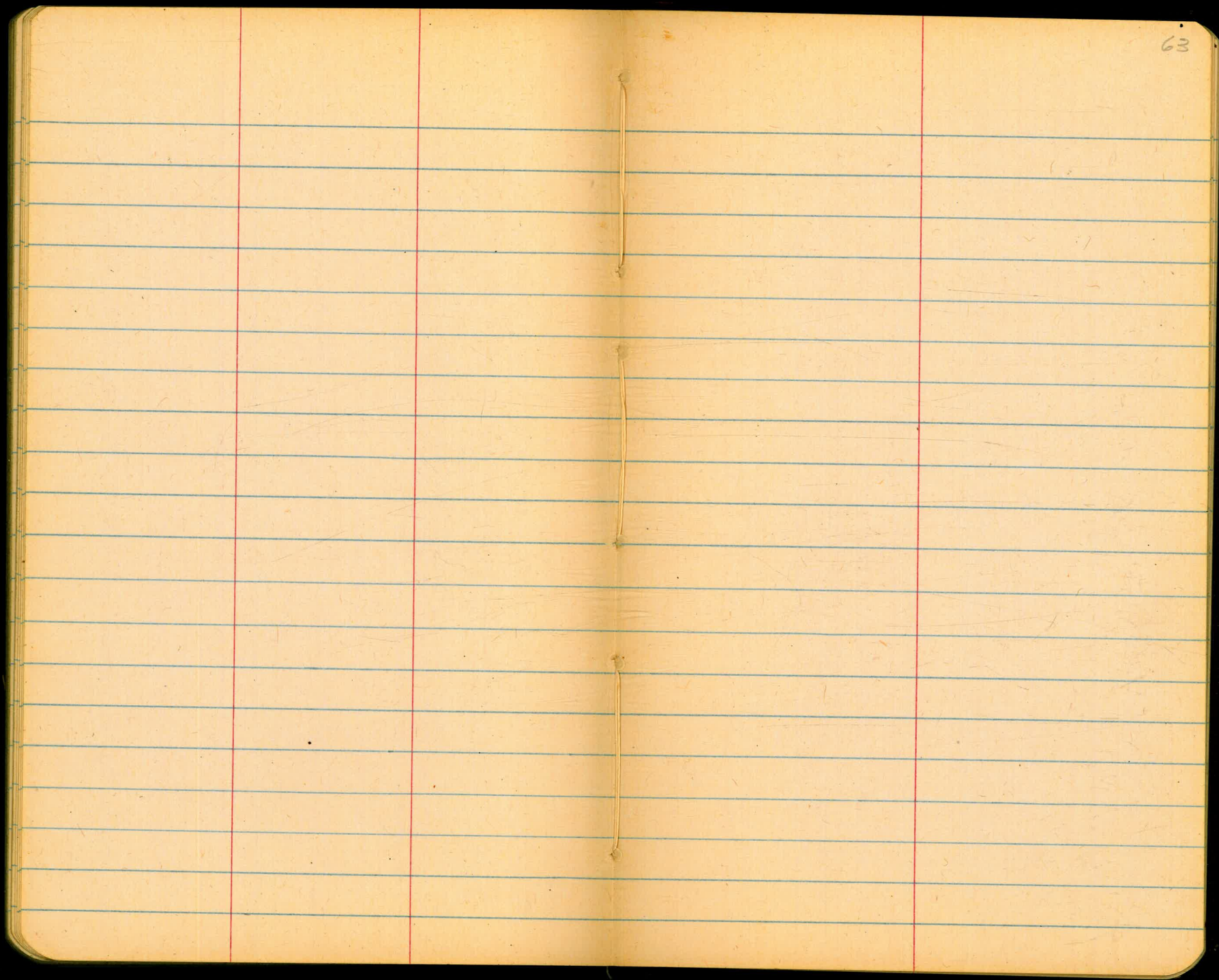


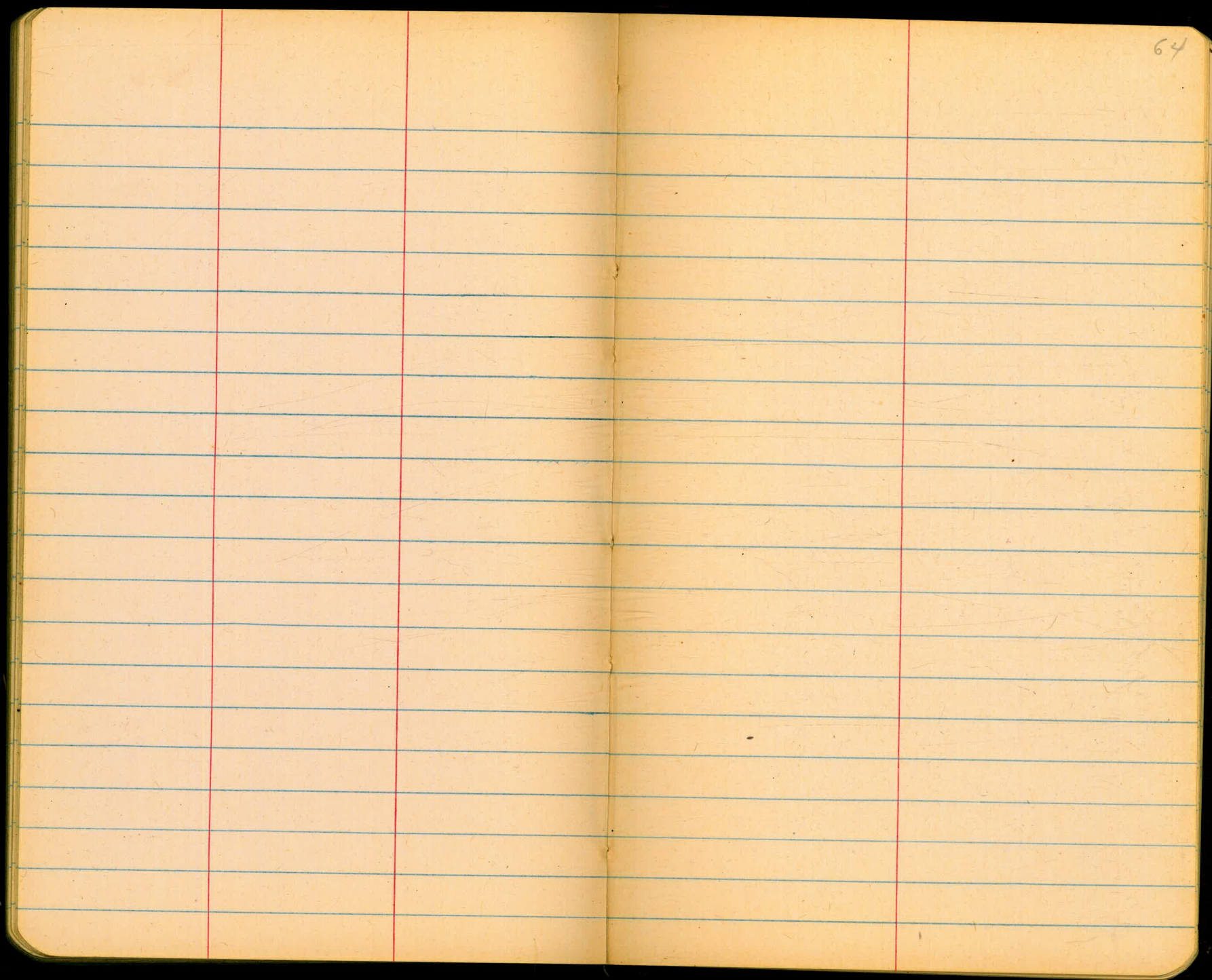


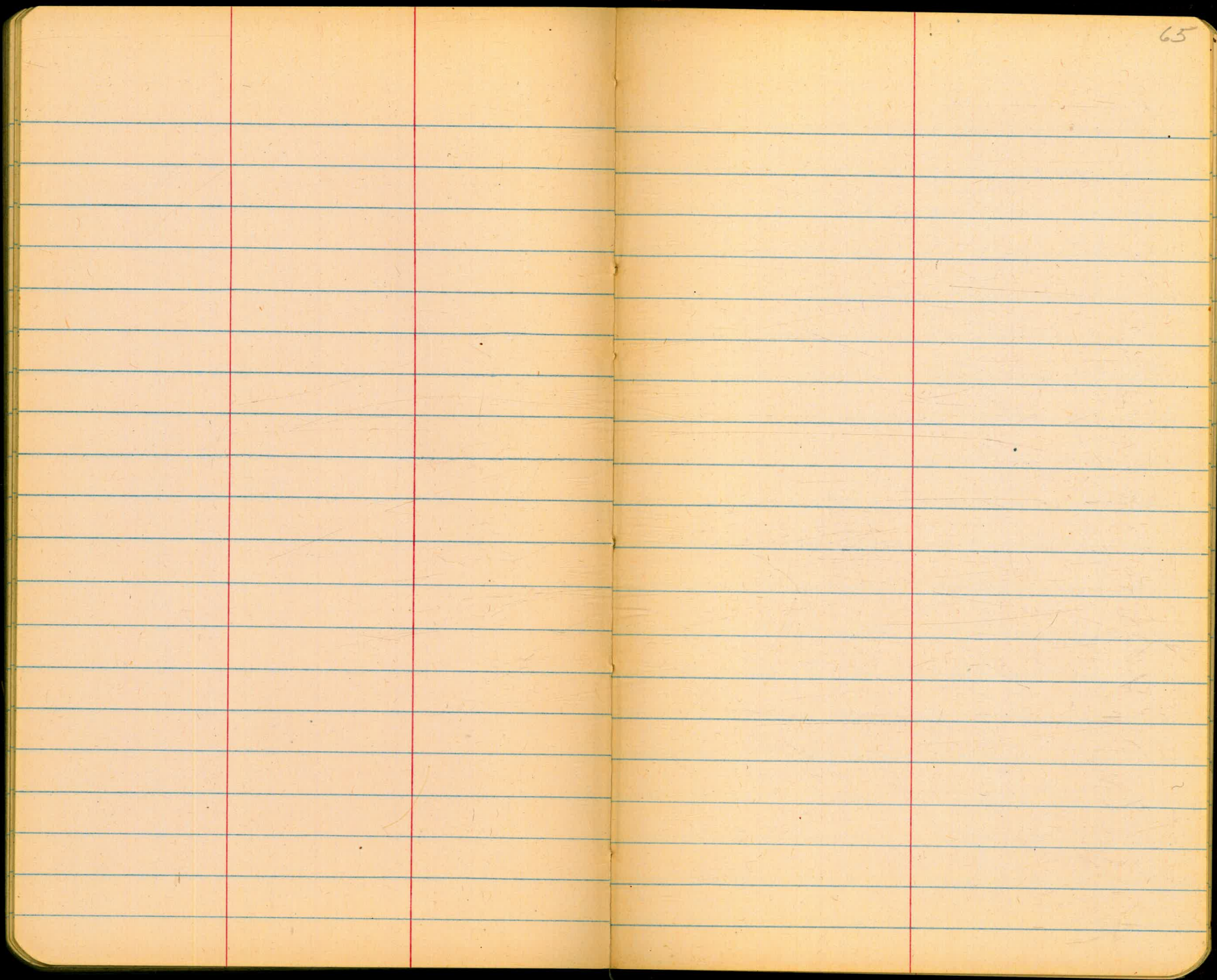
The image shows an open notebook with two facing pages. Both pages are cream-colored and feature horizontal blue ruling lines. Each page is divided into three vertical columns by two vertical red lines. The right page has the number '60' written in the top right corner. The notebook is placed on a black background, and the pages are otherwise blank.

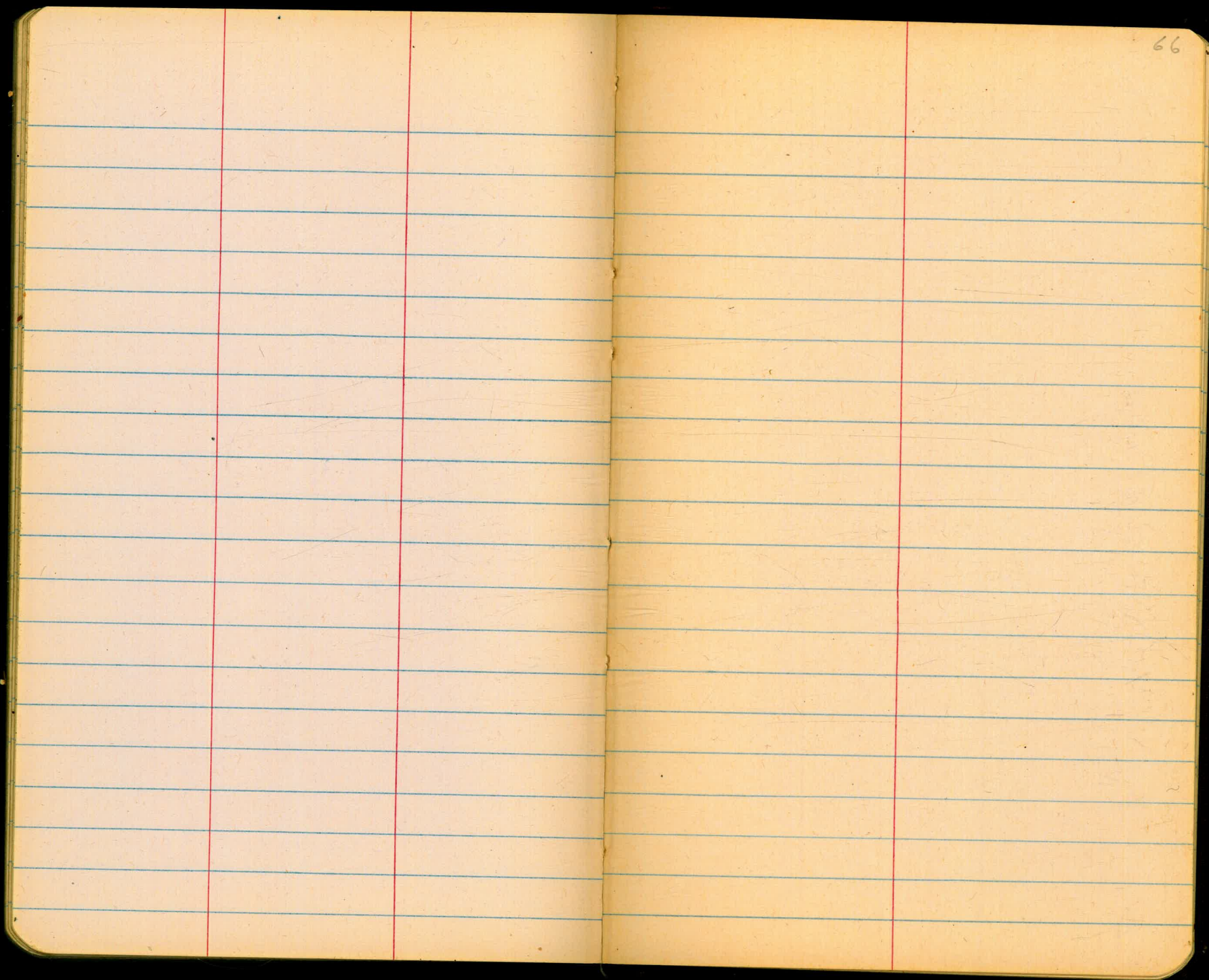


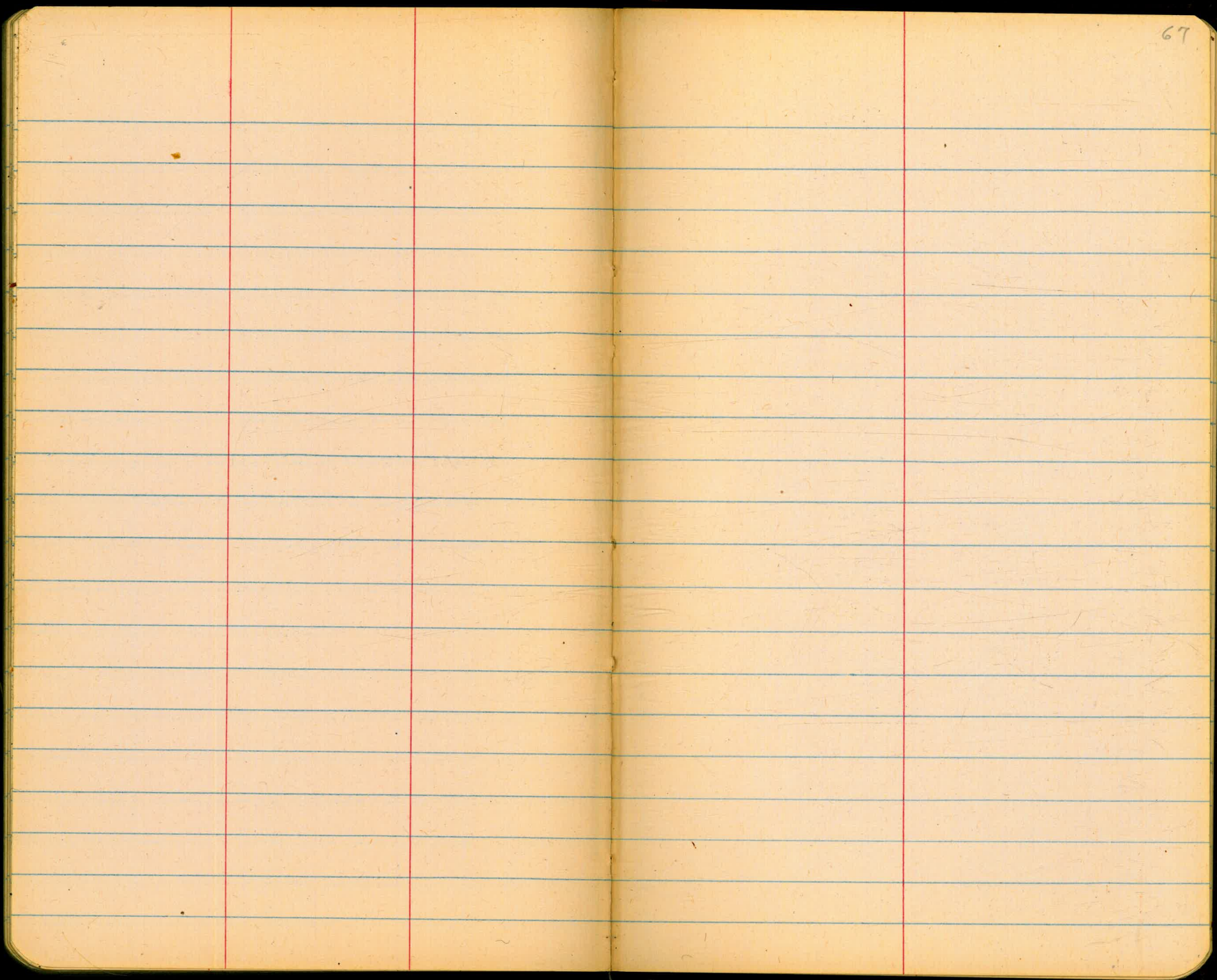


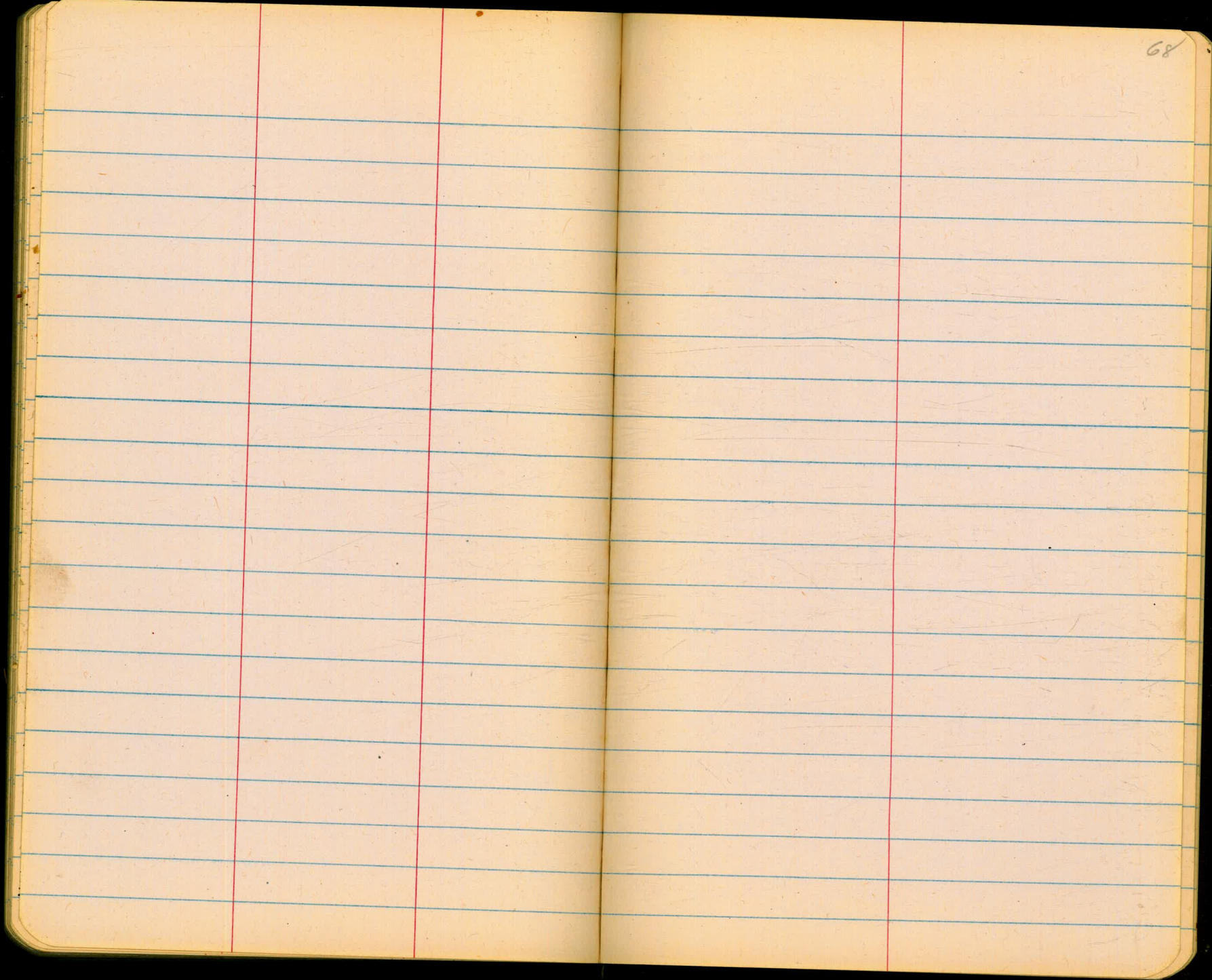


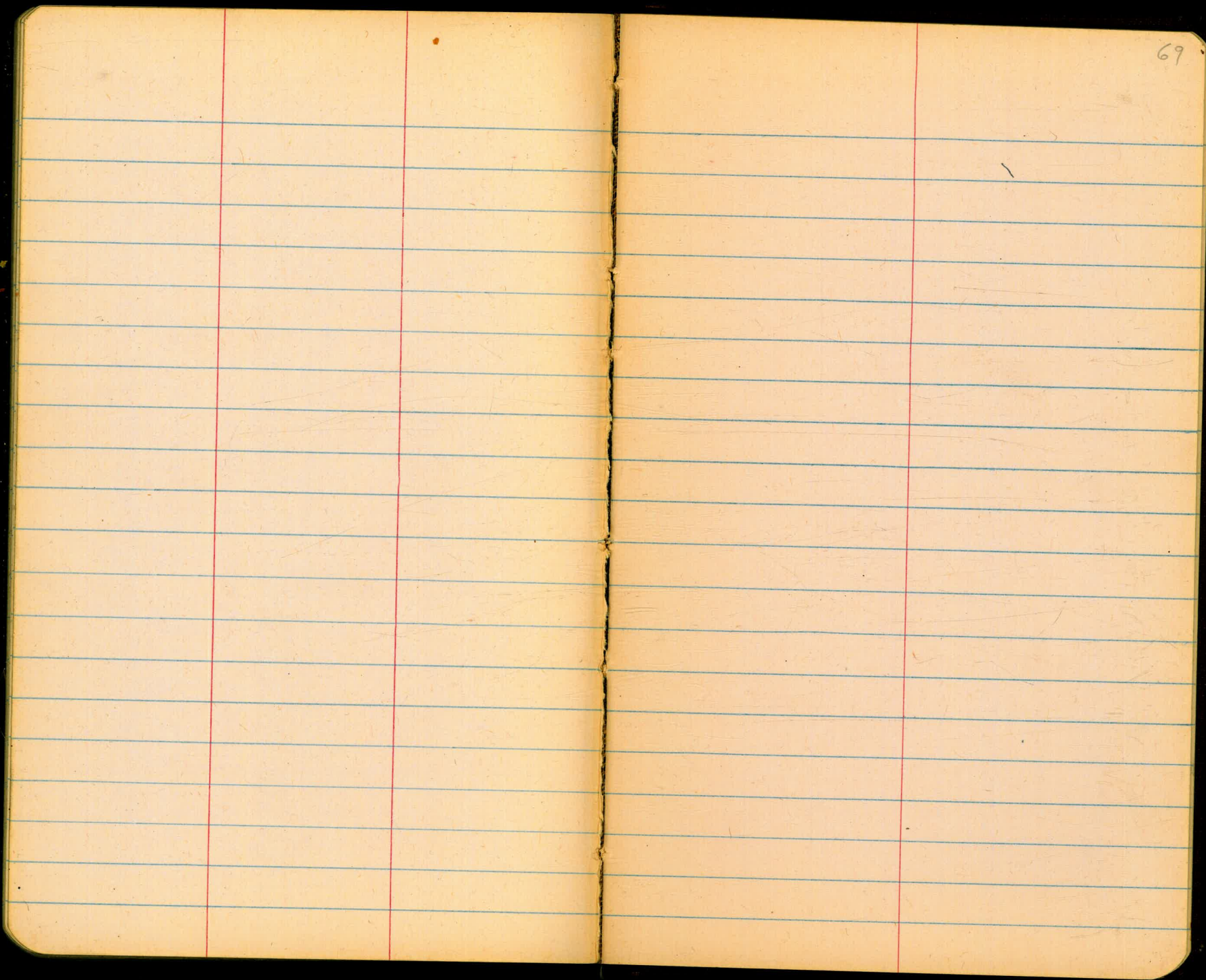




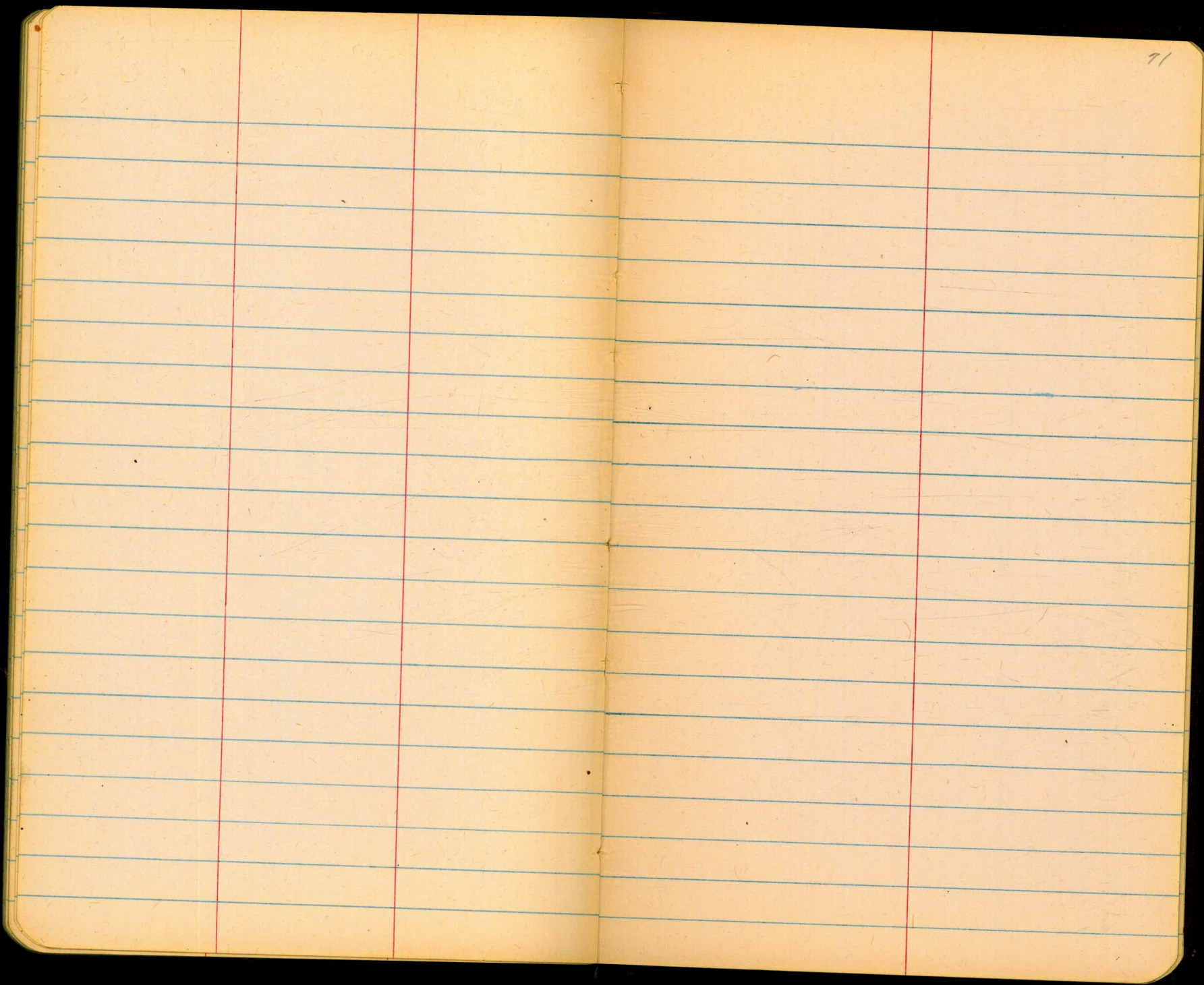


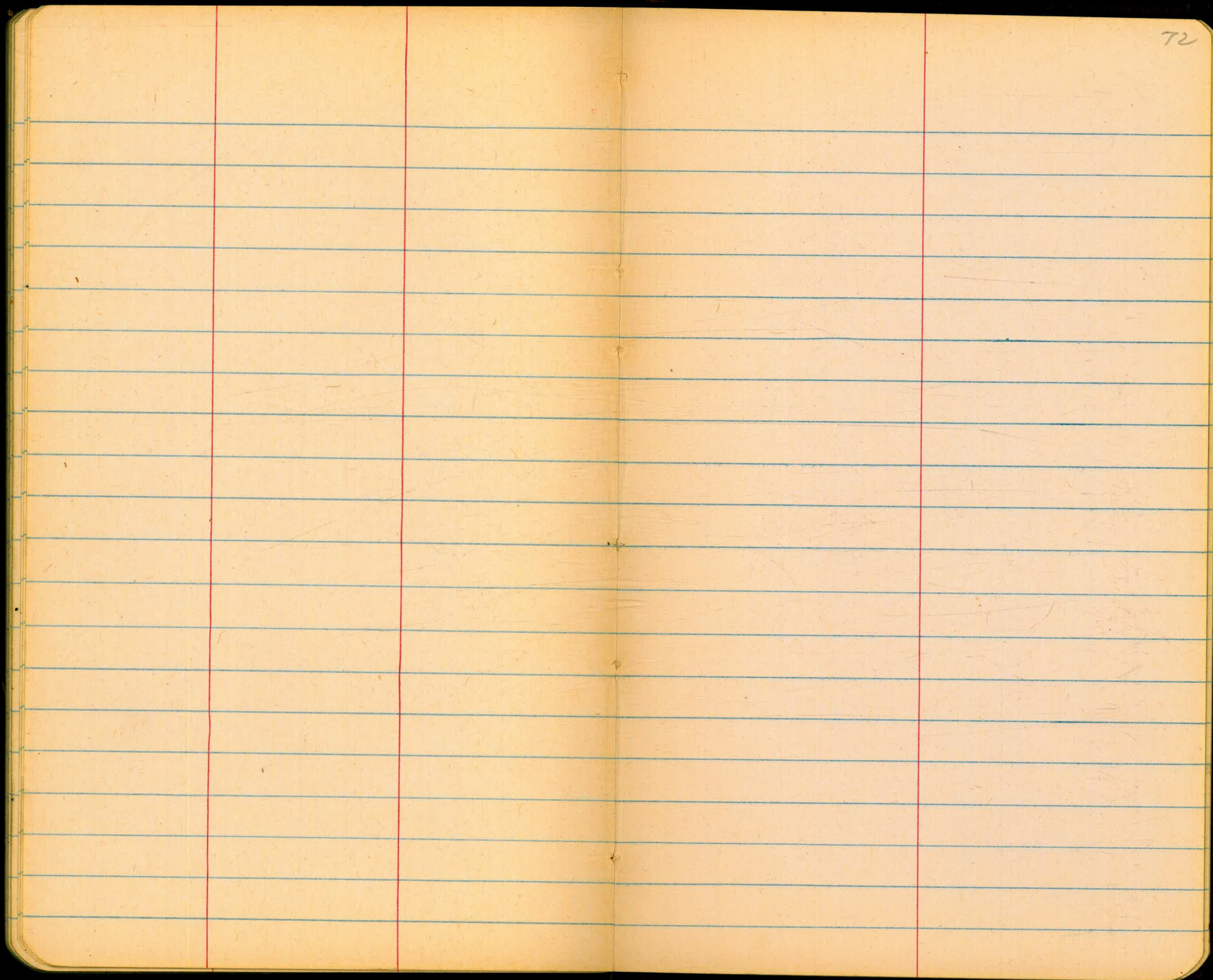


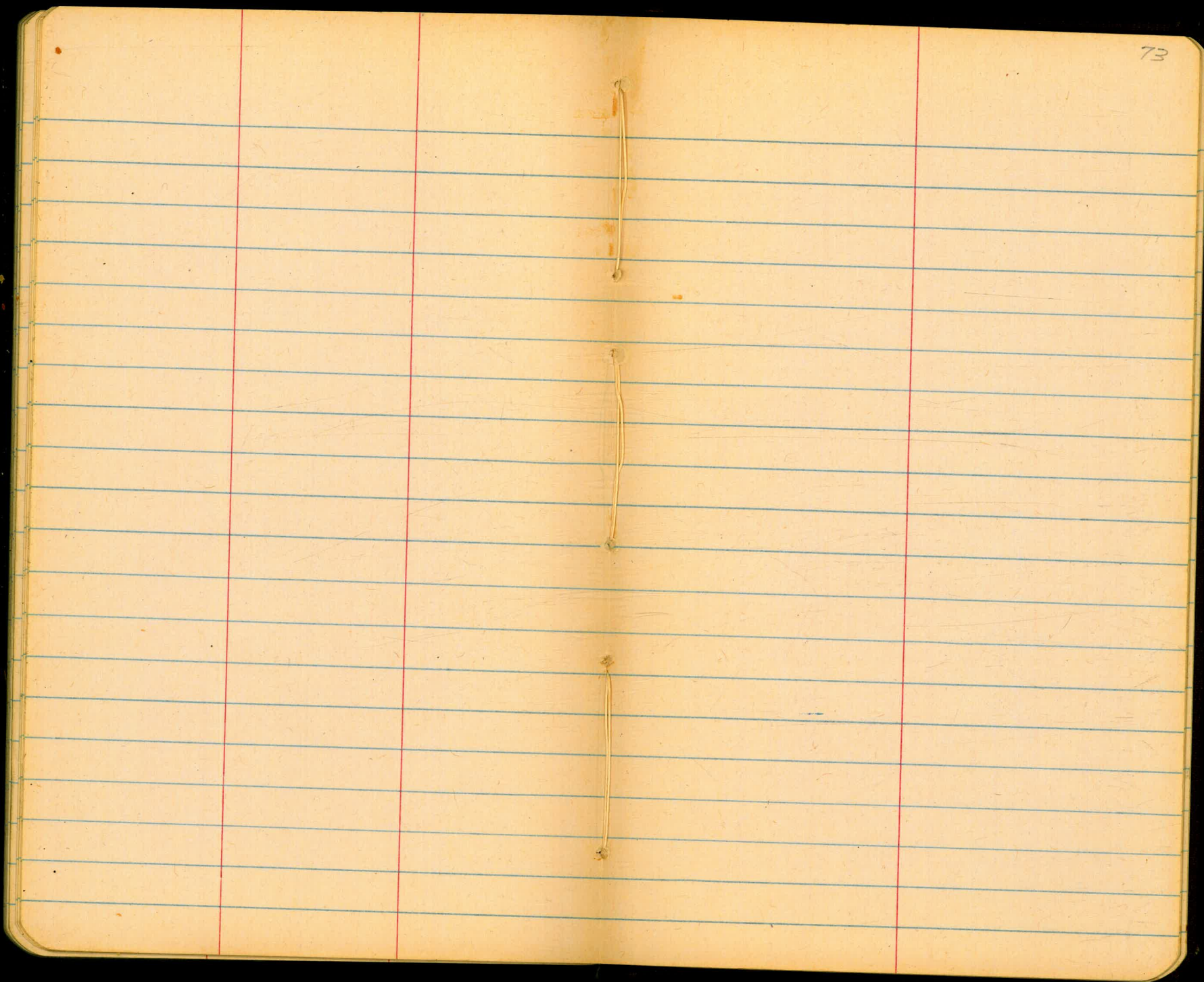


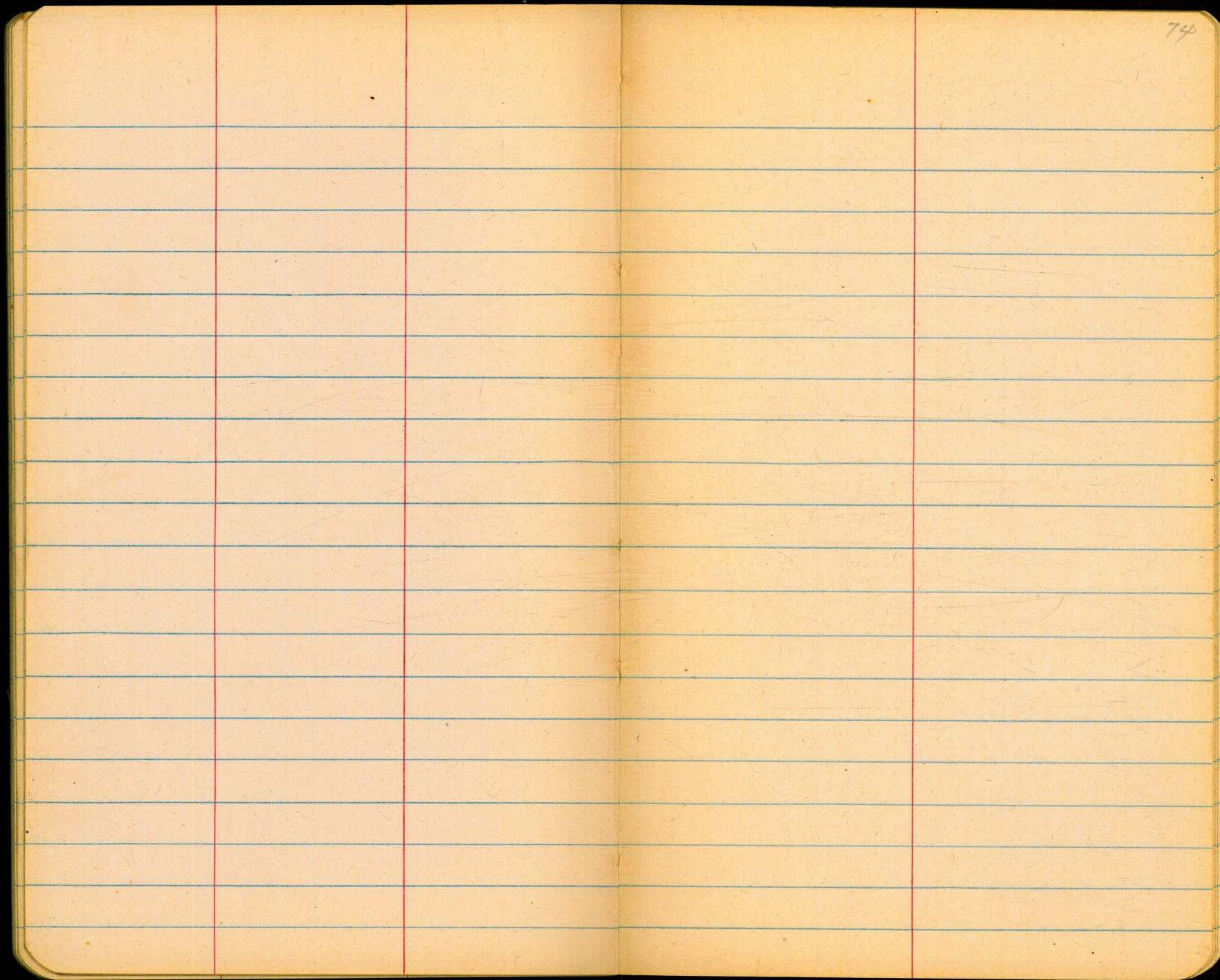


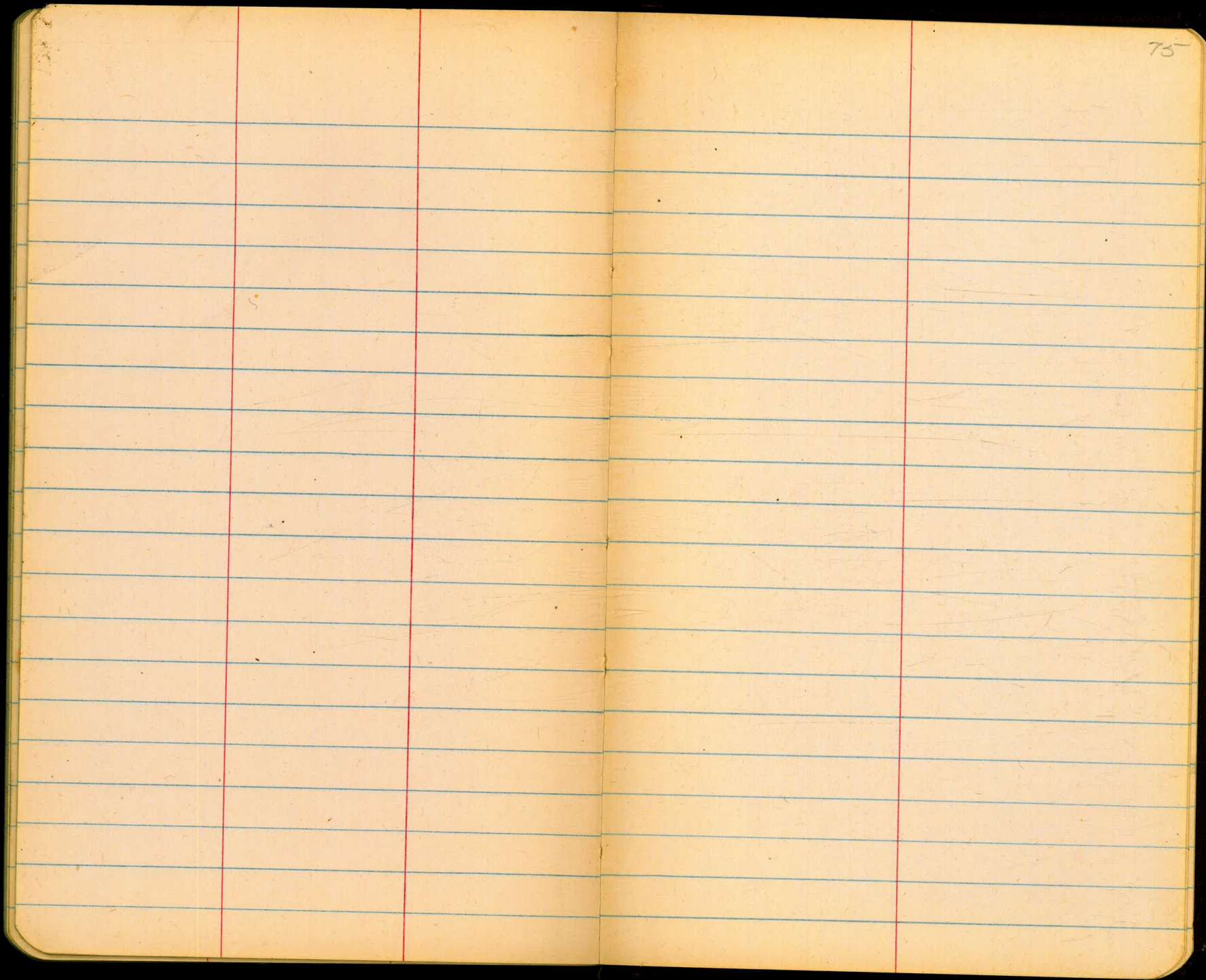
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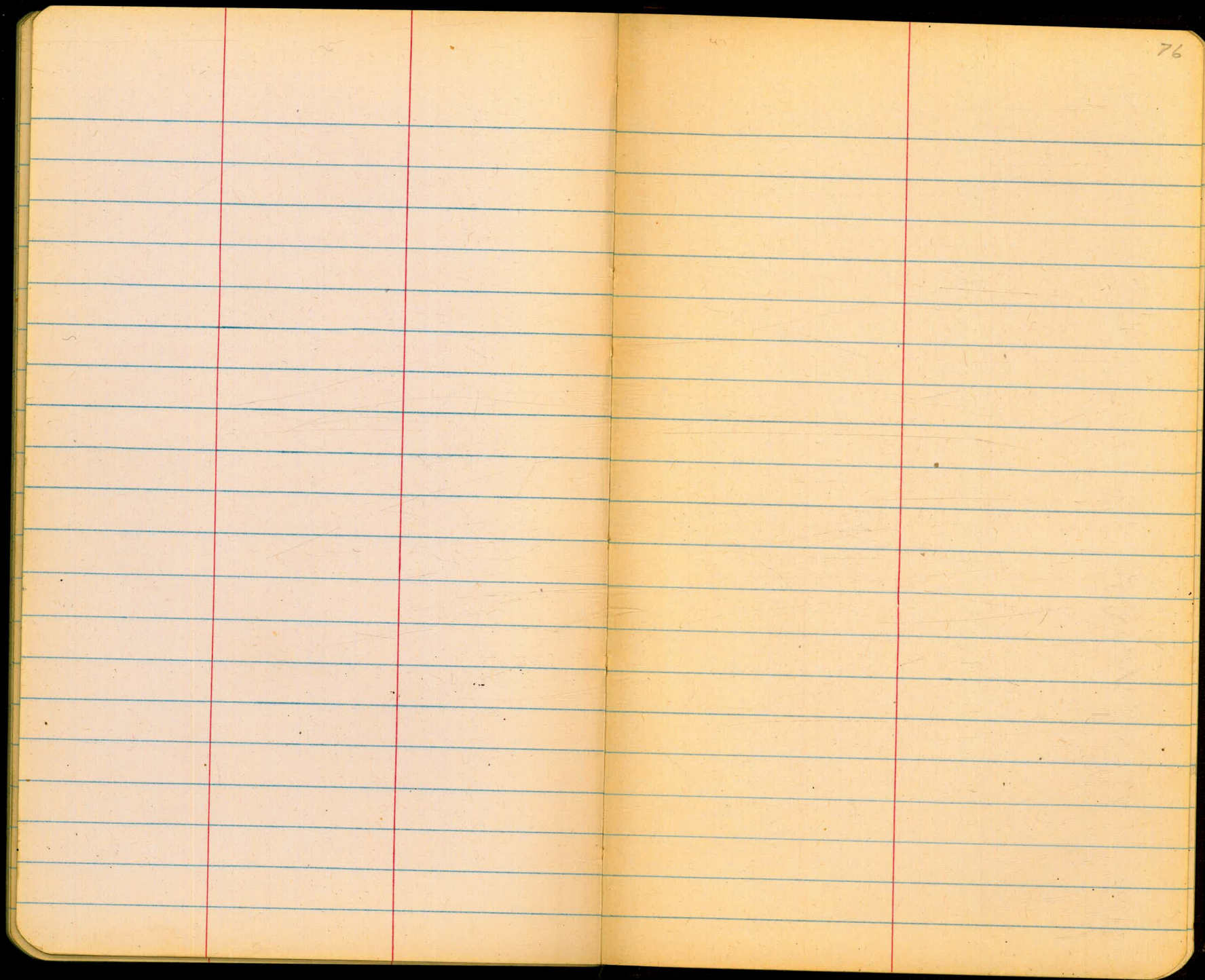


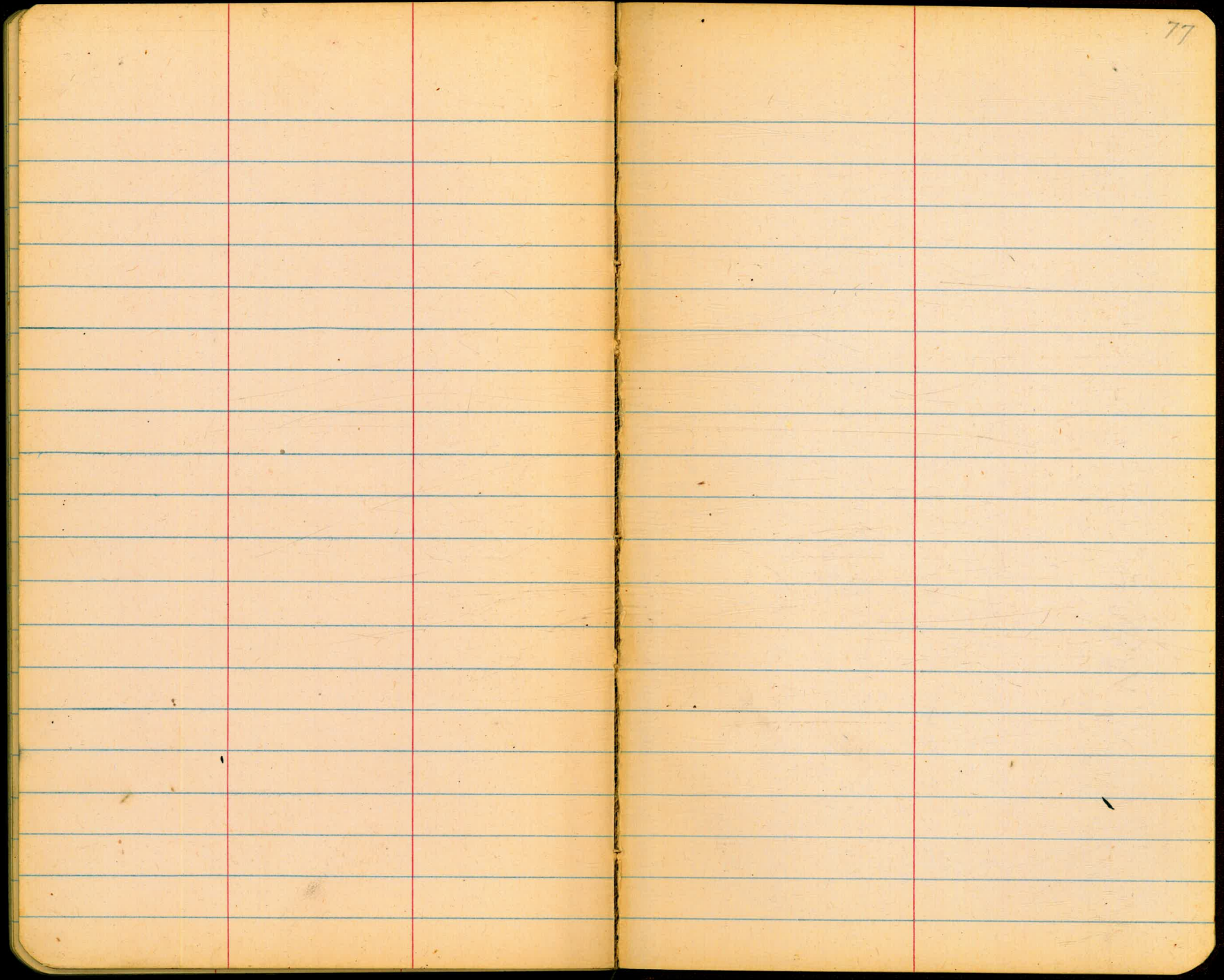












1
294.40
576
288.64

292.82
576
287.66

4024
62-27-30

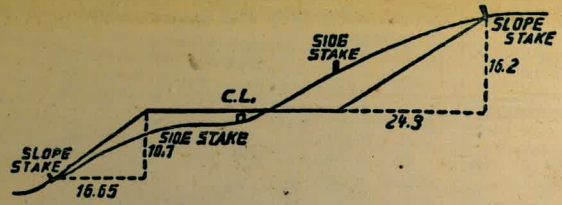
26
- 46

30.6

7 1/2
2 1/2
4 1/2

261.75
- 29.5

91.25



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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