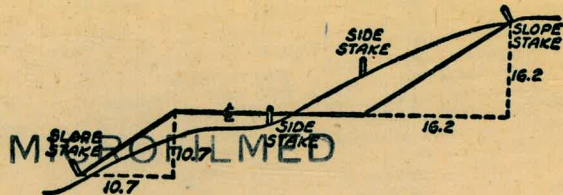


2101

TRANSIT BOOK



DEC 31 1964

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

830 x 22
 22
 1266
 844
 706

INDEXED

to page # 25

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1

Hermosillo Manor	2-
X sec Alley Starkeys Prospect Pk.	10
Survey Road to City Dump	26
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Encroachments - Alley - Blk 9, Pt Loma	60
" Alley Blk 1 - Silver Terrace	61

Hermosillo Manor

6-13-50

P.O.T. 250.00
OK

Pons. St.

249.97
250.00
OK

P.O.T.

Porter St.

119.94
119.91
OK

P.O.T.

202.54
202.52
5.52

308' ±
Set Nail P.O.T.
Sight at Flicker St.
372.09
F.d. Nail on Shingl

Sight at Flicker St.

This disk 0.03 East
will be changed by party
Mr Phelps field 6/14/50

OK
6/20/50
C.H.D.

196°-13'-15"
196°-14'-27"

Identical Point.

953.90
115.02
651.3
107.91
90°

66°38'-35"
66°26'-52"
86°20'-23"
86°00'-22"

125.18
60.00

115.10
56.32
54.22
4.71
F.d. capped 1/2" pipe

82
83
84
85
86
87
88
89
90
91
92

131928 to Job ply

Hermosillo Manor



P.O.T. ^{ok}
438.77

250.00

P.O.T. ^{ok}

Tibbett St.

Cadman St

250.00

72
73
74
75
76
77
78
79
30'
30'
80
81
82

55
55
55
58
53
53
53
63.6
30.5
30.5
53.31
53
53

481.66
481.68

24.24 Fd. 2" pipe
P.O.T. LOK

722.68
722.70

Hermosillo Manor.

1518

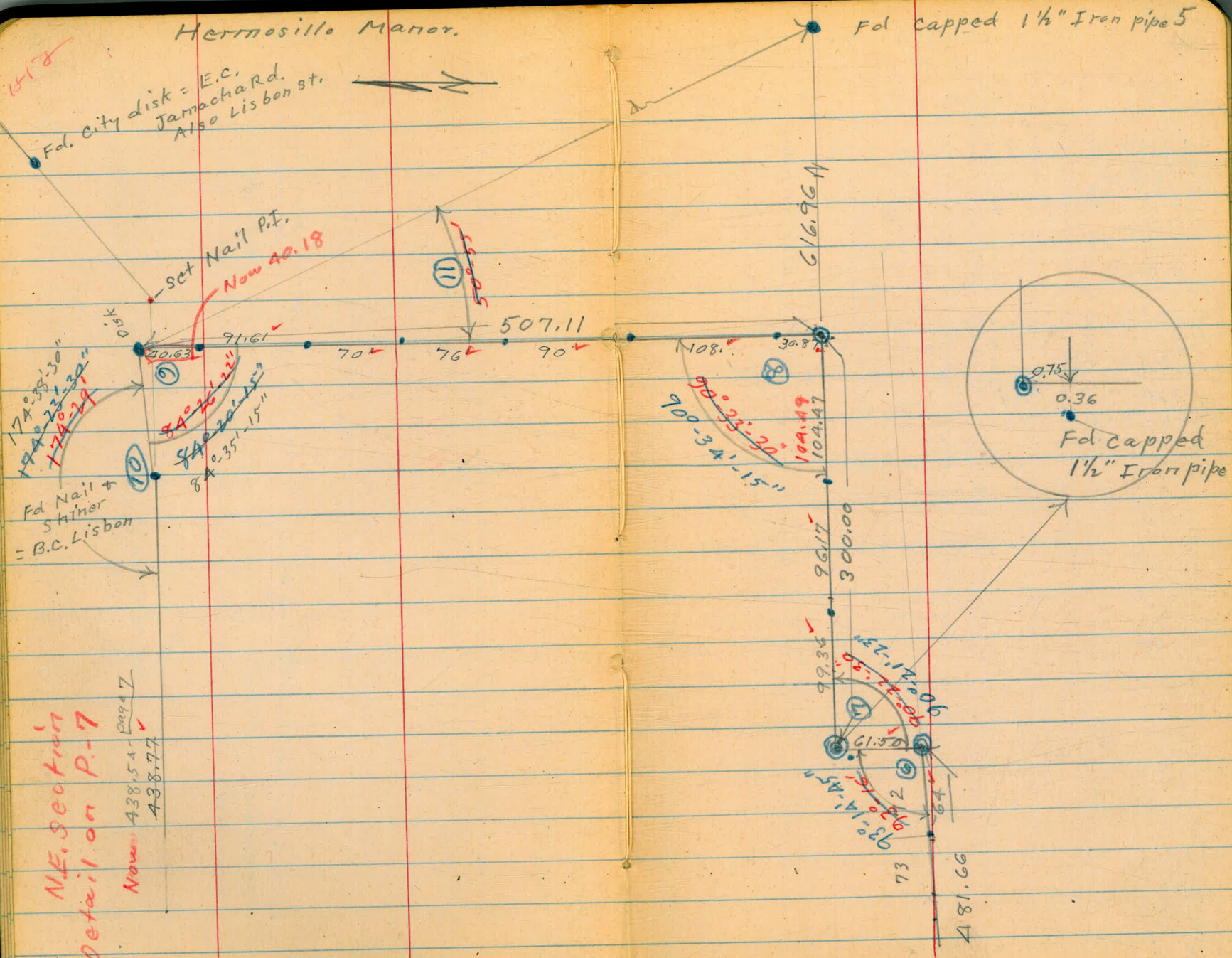
Fd. city disk = E.C. Jamacha Rd. Also Lisbon st.

Set Nail Pt. Now 40.18

Fd Nail to Shiner = B.C. Lisbon

NE. section Detail on P. 7

Now 438.54 - Page 7
438.77



Hermosillo Manor

6/20/50

#9	84-20-15	97°	1A - 22
#10	185-36-30	196	13 - 15
	369-56-45	66	38 - 30
		270	00 - 00
		86	30 - 15
		93	14 - 45
C-23-50		269	38 - 38
		90	34 - 15
#9	84°-35'-15"	←	84 - 20 - 15
#10	185-21-30	← Now	185 - 36 - 30
	369-56-45		
Totals remain		1436	237-22-5
The same	6/23/50	4	3 45"
		1440	
		8x360°	1440

ERROR = 0°-00'-45"

Δ^s Turned 6-20-50
After boundary was reset.

6

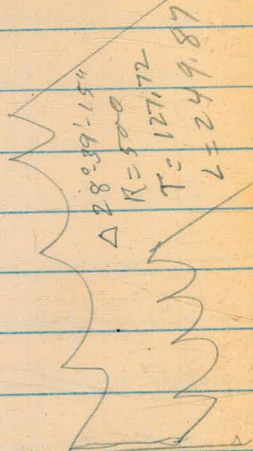
#	Trial A	A Times	Mean Δ	Map Δ
1	97°-14'	388°-57'-30"	97°-14'-22"	97°-14'-49" outside
2	163°-47'	655°-07'	163-46-45	163°-46'-24"
3	66°-39'	266°-34'-30"	66°-38'-37"	66°-38'-30"
4	90°	360°	90°	90° outside
5	86°-30'-30"	346°-01'-30"	86°-30'-23"	86°-30'-30"
6	93°-15'	372°-59'	93°-14'-45"	93°-15' outside
7	90°-20'-30"	361°-25'-30"	90°-21'-22"	90°-21'-30"
8	90°-34'	362°-17'	90°-34'-15"	90°-34'-20"
9	84°-20'	337°-21'	84°-20'-15"	
10	5°-36'	22°-26'	5°-36'-30"	Deflection.
<p>{ Δ^s #9 & #10 not in correct position. Are to be corrected }</p>				
9	84°-35'-30	338°-21"	84°-35'-15"	
10	5°-22'	21°-26'	5°-21'-30"	Deflection- 5°-21'-19"

Hermosillo Mar. 07.

Check ~~2d~~ Restake 6-23-50

INDEXED
JUN 26 1950

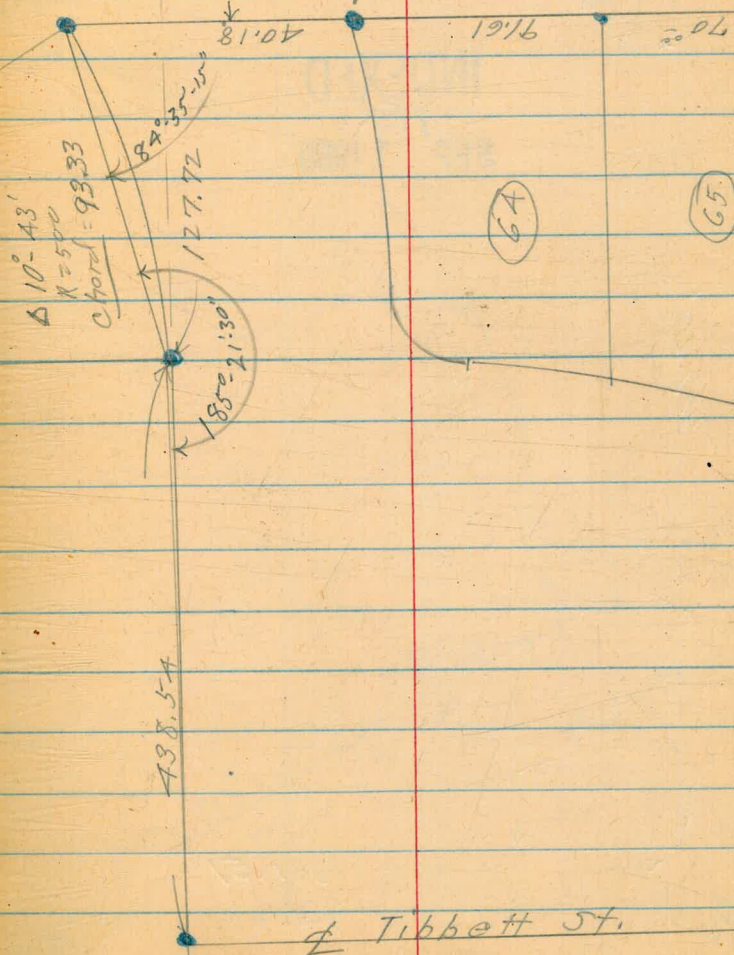
See F.B. 1558
20 + 24
For Tie in.



From
FB 1558
24



- see FB. 1558
20 + 24



8-30-50
Hendricks
Cota
Greer
Crawford
N.O. #23108

Check Exterior Boundary
ALVARADO

(8)

R=540'

PL 2" 11P
RE 4847
NE Cor
Lot 3

⊙ Denotes 2" I.P. Ed

588.35
586.64'

32°49'
22°47'

368.00
Chord
36.881'

32°30'

19°59'30"
190°55'19"

R=460
494.32
Chord
49.413'

32°30'

999.66
999.20'

89°45'
89°44'28"

INDEXED
MK
SEP 1 1950

900°16'30"
90°16'15"

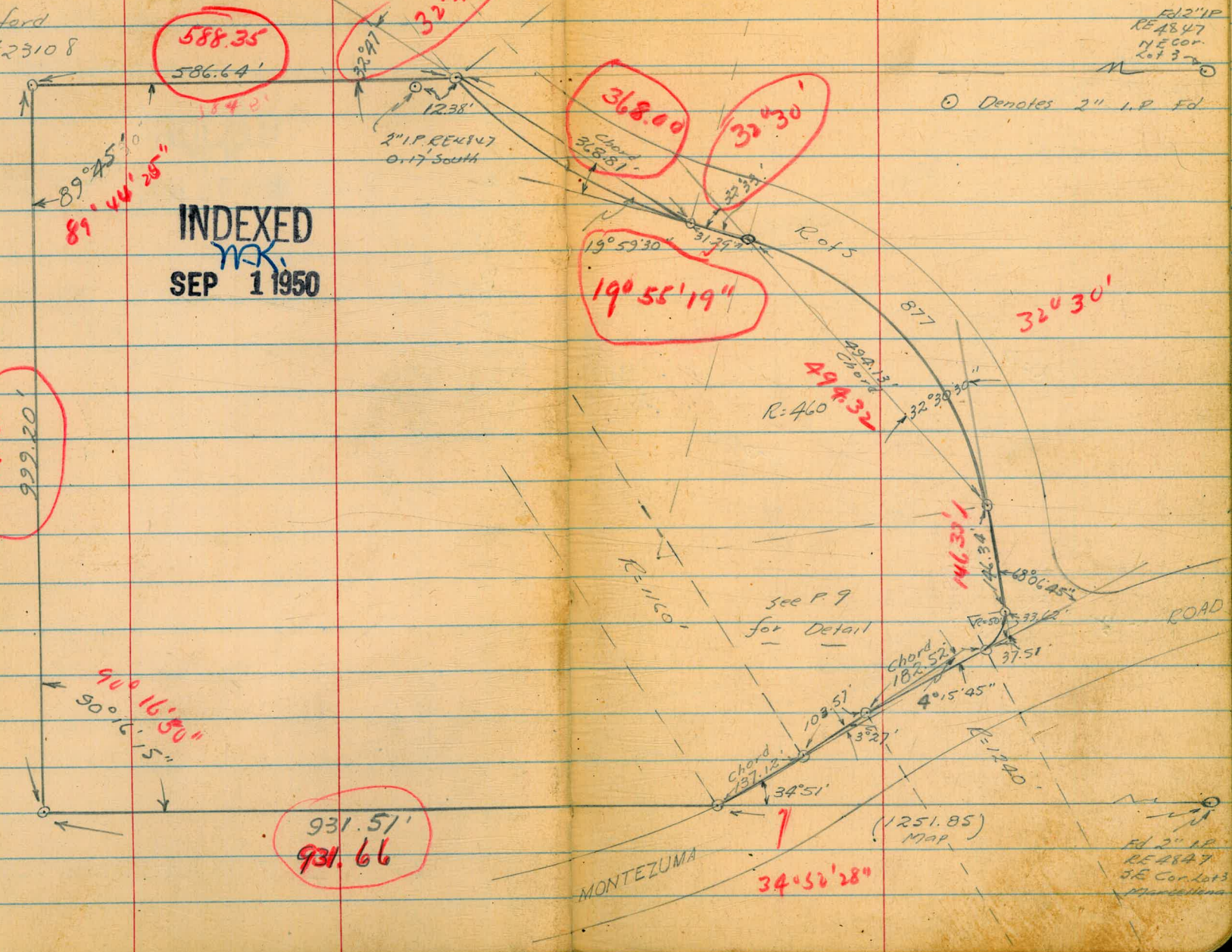
931.51'
931.66

MONTEZUMA

34°52'28"

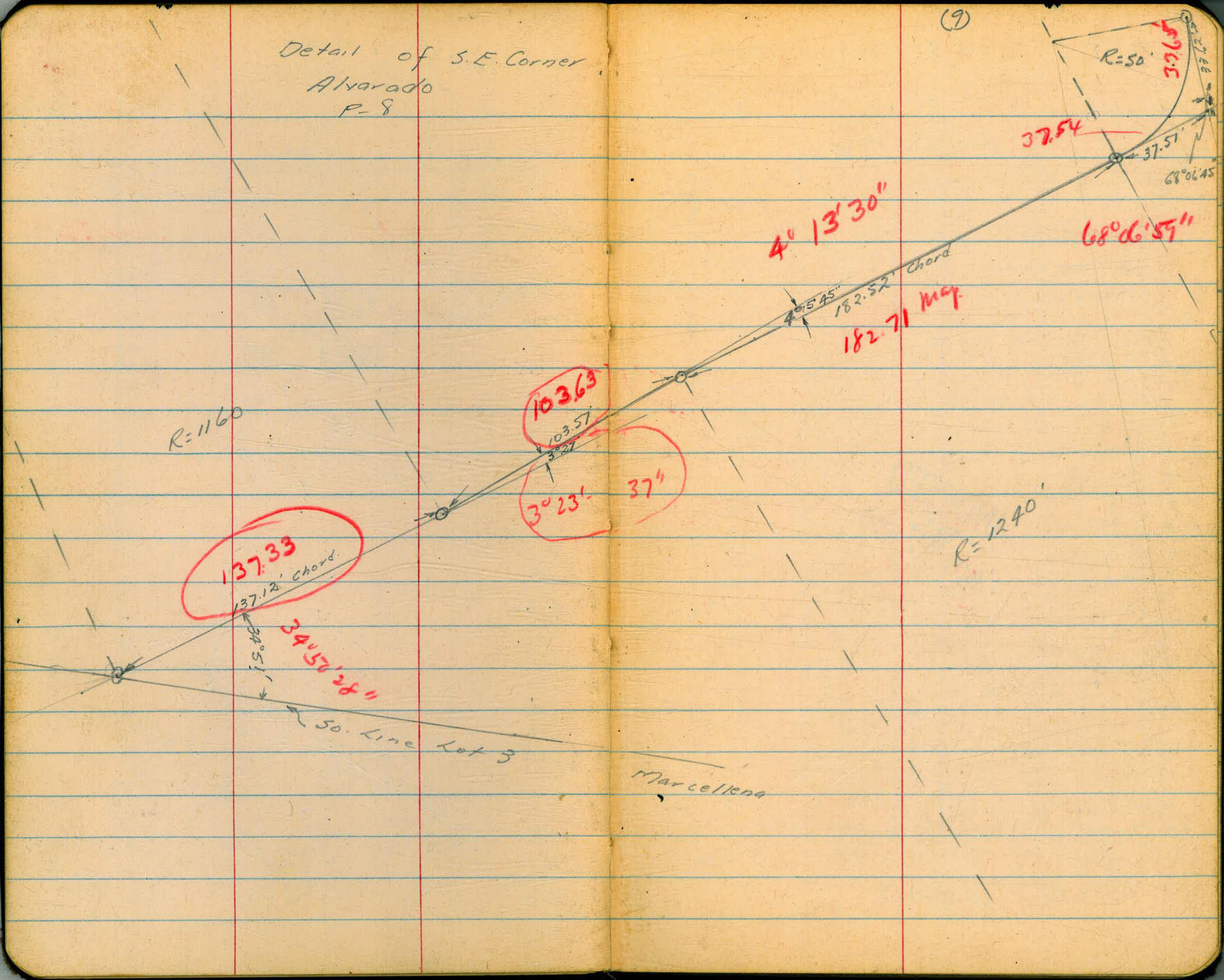
(1251.85)
MAP

PL 2" 11P
RE 4847
SE Cor
Lot 3



Detail of S.E. Corner
Alvarado
P. 8

(9)



X-Section Alley, B.K.C. Starkeys Prospect Park.

Semmermeyer

Begg
Allen
Bunch

Nov. 15, 1950
V.O. 31891

Ref:
T.P. Book # 17
Map # 1729

• = Ed. L.T. - Tie Pt. Book # 17

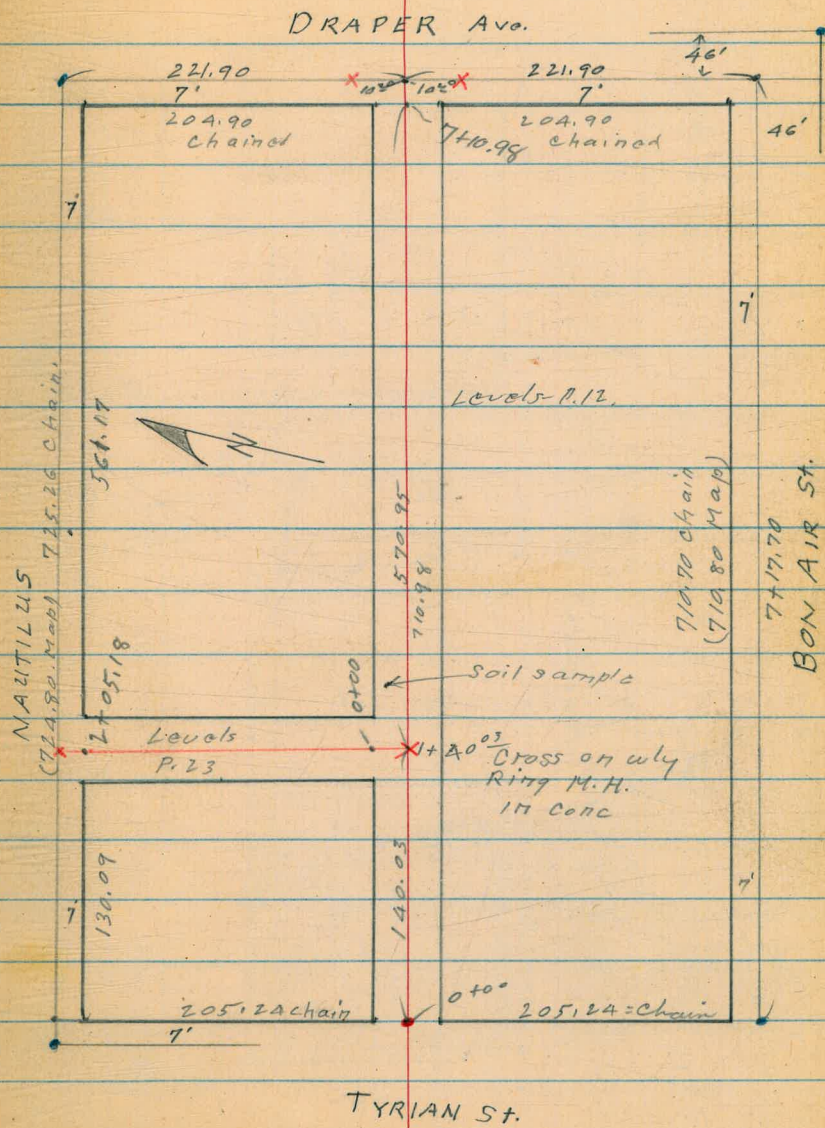
✕ = cut across in conc.

• = Nail in A.C. Pav

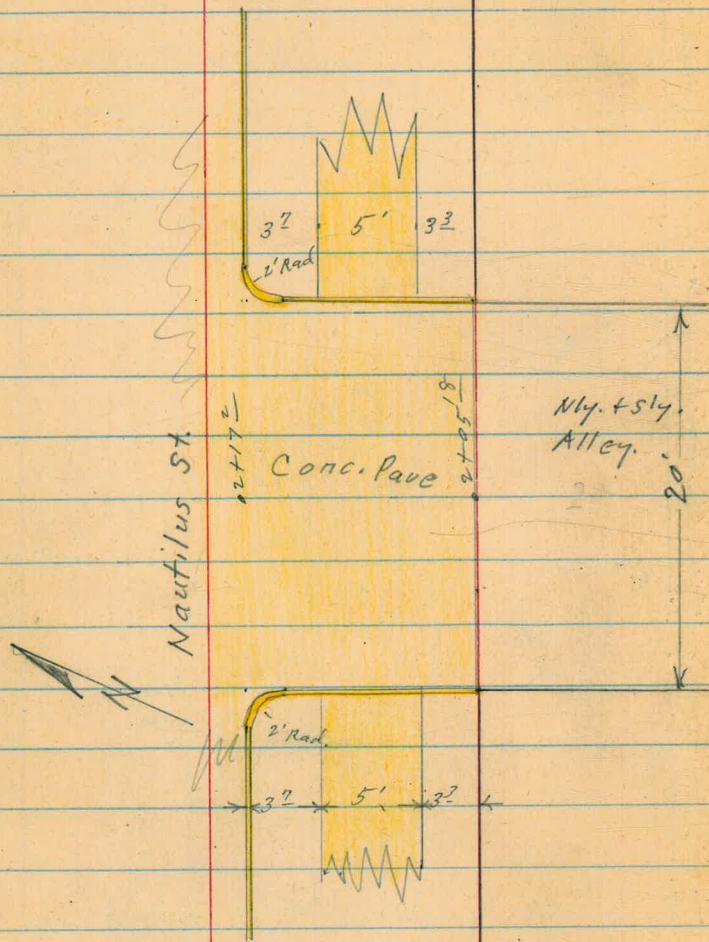
T.W. = Top of wall

B.W. = base of wall footing

INDEXED
NOV 27 1950

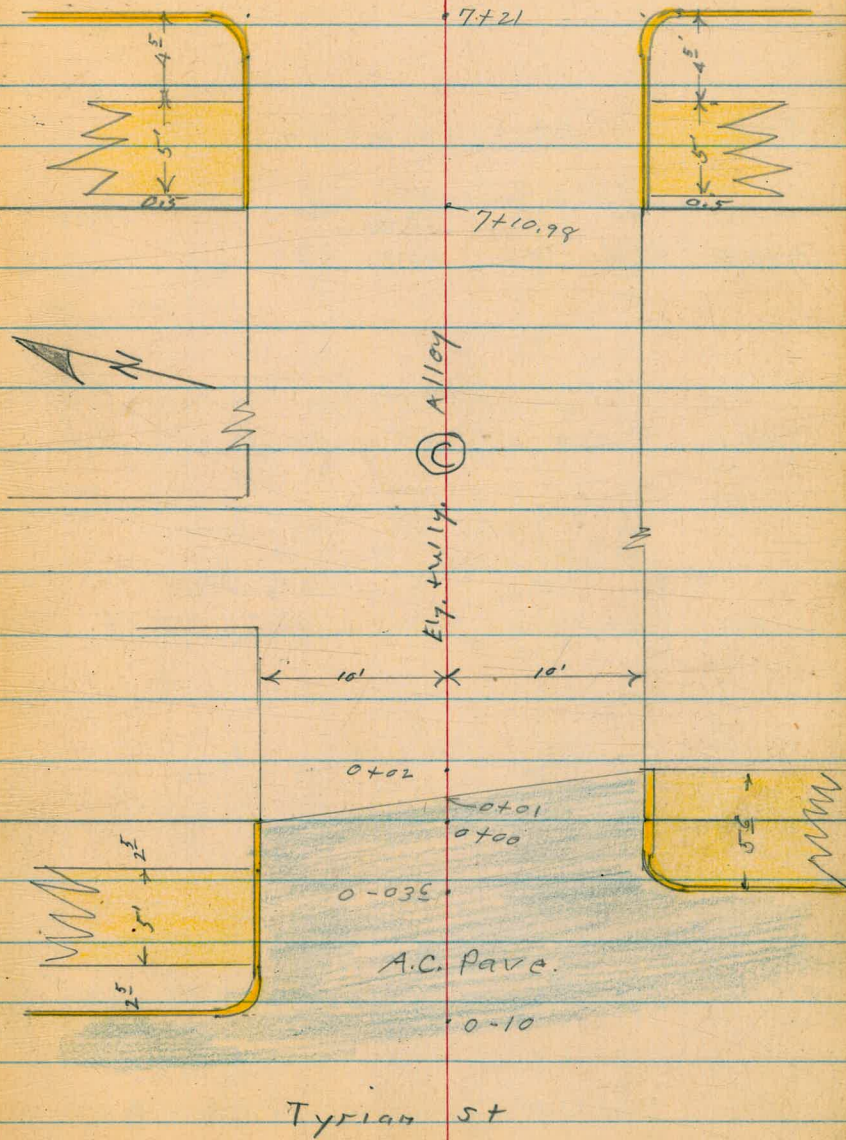


Detail of Curbs - Blk c.
Starkeys Prospect Park



Detail of curbs - Blk c.

Draper Ave
unimproved street.



E.+W. Alley BIK "C"

Starkeys Prospect Park.

0+03 - 8' Rt. = deadman

0+02 { 9 1/2 Lt. = face of wall
(end A.C. Pavc.
10' Rt. = end alley cl.

78.9	77.2	76.5	76.3	76.3	76.4	76.6
2.4	4.1	4.8	5.0	4.97	4.82	4.7
10	92	7		10	10	15
T.W.	at wall			G	cc.	

0+01 = end A.C. Pavc on \pm
9 3/4 Lt. = start 6" wide Conc. wall.

78.8	76.6	77.1	76.4	76.11
2.5	4.7	4.2	4.9	5.15
10	92	92	9	
T.W.	B.W.	End		

0+00 = { 9 1/4 Lt. = end alley cl.
(also = end A.C. Pavc.
+ Tyrian to south
Ely line La Jolla to north.

76.73	76.39	76.07	76.20	76.41
4.53	4.87	5.19	5.06	4.85
92	92		10	10
cc.	G		G	cl.

0+03⁶ = Ely cl. Line Tyrian to south

76.65	76.24	75.91	75.69	76.33	75.29	75.96
4.61	5.02	5.39	5.57	4.93	5.97	5.30
10	10		12	12	50	50
cc.	G		G	cc.B.C.	G	cc.

0-10 Ely cl. line La Jolla to North

76.64	76.09	76.32	75.76	76.11
4.62	5.22	4.94	5.50	5.55
50	50	12	12	
cc.	G	cc.B.C.	G	81.26

9.28 81.26 - 71.98

S.W.B.P. Ben Air + La Jolla Blvd

Sewer Lateral. from house on north.
 0+41 CROSS 4" diam C.I. pipe

12.29	75.27	75.14
6.21	6.23	6.36
8.2 Top of pipe	Top of pipe	6.3 Top of pipe

0+40

80.2	80.2	78.1	79.3	76.5	78.3	78.3	79.8	80.0
4.3	4.3	5.8	5.2	6.0	6.2	6.2	4.7	4.5
12	10	9.8	9.8	8	6.2	6	10	15
	T.W.	B.W.	End					

0+30 - 10' Rt. = 6' wide Lantana hedge

0+25 - 12' Lt. = S.W. cor. stucco house

0+23 - 8' Rt. = Sky edge pole # 537366-H

19.7
4.8
11.2
End.

0+22 - { 10' Lt. = 3' wide conc. walk
 9' Lt. = Face wall
 9' Lt. = Ctr. of 1'x3' conc. step to come out.

19.9	19.9
4.6	4.60
15	10.1
	walk

0+20 9' Lt. = Face of wall

19.1	19.1	18.0	18.1	17.9	16.9	17.0	17.9	18.0
4.8	4.8	6.5	5.8	7.1	7.6	7.5	6.6	6.5
10	9.1	7.6	9.6	8		6	10	15
	T.W.	B.W.	End					

T.P. 7.93 84.50 4.69 76.57

84.50

0+15 8' Lt. = dead man

0+09 9' Rt. = start 6' wide Lantana hedge

0+05 12' Lt. = Ctr. 4' diam. Palm

19.1	19.1	17.3	17.7	16.8	16.5	16.4	17.4	18.6	18.6
2.2	2.2	4.0	3.6	4.5	4.8	4.9	3.9	2.7	2.7
15	10	9.2	9.2	8		8	10	13	20
End	T.W.	B.W.	End						

81.26

E. & W. Alley Bk. 3.

1+14 92 Rt. = dead man.

1+08 16' Rt. = end double Gar.

1+00

0+97 10³ Lt. = end lath + post fence.

0+92 16' Rt. = start double Gar.
Conc. floor - no apron.

0+90 - 11⁵ Rt. = end 7' high batt fence

0+66 - 10' Lt. = start Lath + post fence.

0+64 9² Lt. = end 6" wide Conc. wall
11⁵ Rt. = start 7' high Batt fence.

0+62 9² Lt. = ctr. of 1' x 3' conc. step to
11' Rt. = 6' wide Lantana hedge
come out.

0+57 - 12⁶ Lt. = S.E. Cor. stucco house.

14

81.5	81.0	80.5	80.3	80.5
<u>3.0</u>	<u>3.5</u>	<u>4.0</u>	<u>4.2</u>	<u>4.0</u>
15	10	8		10

81.22
3.28
16
Floor

81.21
3.29
16
Floor

80.1	80.1	79.2	80.1	79.5	79.4	79.7	80.0
<u>3.8</u>	<u>3.8</u>	<u>5.3</u>	<u>4.4</u>	<u>5.0</u>	<u>5.1</u>	<u>4.8</u>	<u>4.5</u>
15	10	9.2	9.2	8		10	15
	T.W.	B.W.	Orl.				

80.6
3.9
12⁶
end

84.50

E. & W. Alley B.K.C.

T.P. 7.11 89.82 1.79 82.71 = Nail in Pole # P.A. 524

1+68 - 11² Rt. = \pm 1⁶ wide Conc. ribbon of drive

82.58	81.46	81.05	80.6
1.92	3.04	3.45	3.9
11 ²	29	40	70

1+63 - 11² Rt. = \pm 1⁷ Conc. Ribbon of drive

82.5	81.45	80.95
2.00	3.05	3.55
11 ²	29	40

Gar. Floor

INDEXED
mk
NOV 27 1950

1+50⁰³

82.1	82.2	82.0	82.3	80.1
2.4	2.3	2.5	2.2	4.4
10		8	10	50

1+40⁰³ = \pm Alley to north

81.7	82.00	81.8	82.0
2.8	2.50	2.7	2.5
10	on cross	7	10

1+33 9³ Rt = sly. side Pole # P.A. 524

82.28

1+30² 13⁵ Lt. = end double Gar.

2.27
13 ⁵
Floor

1+30⁰³ = wly. line N. & S. Alley to north

81.3	81.5	81.5	81.8
3.2	3.0	3.0	2.7
10		7	10

1+16 - 13⁵ Lt. = start double Gar. Conc. floor

82.22
2.28
13 ⁵
Floor

84.50

10² = ± N. + S. CONC. wall. 8" wide
 2+91 - 9⁵ Rt. = back face pole # PA. 544

86.2	85.8	86.9
3.6	4.0	2.9
109	109	109
Qnd	B.W.	Top wall

2+75 10² Lt. = start lath fence.

85.4	85.9	85.12	85.12	85.6	85.7
4.4	4.4	4.7	4.7	4.2	4.1
20	10	7		10	20

2+53 - 9³ Rt. = end Conc. Apron.

84.72	84.74	85.06
5.10	5.08	4.76
92	70	162

2+41 9³ Rt. = start conc. apron to Sing. Bar.

84.62	84.64	85.11	84.92
5.20	5.18	4.71	4.90
92	10	162	63
			Bar Flan

2+31 10³ Rt. = end 16" high conc. wall.

83.8	83.3
6.0	6.5
10	103
	B.W.

2+00

83.2	82.8	82.8	82.8	82.1
6.6	7.0	7.0	7.0	7.7
50	10		10	50

soil sample taken 7' Lt off
 Fence on top.

1+80 10² Rt. = start 16" high Conc. wall.

82.4	82.3
7.4	7.5
102	102
Qnd.	B.W.
89.82	

T.P. 10.10 98.76 1.16 88.66

3+50

89.2	88.8	88.3	88.3	88.7	88.1
$\frac{0.6}{30}$	$\frac{1.0}{10}$	$\frac{1.5}{8}$	1.5	$\frac{1.1}{10}$	$\frac{1.7}{30}$

3+37- 10² Lt. = { start wire fence.
and lath fence3+32 28² Rt. = 6' wide step.

87.2	87.3	87.4	87.9	88.0	88.14	88.97
$\frac{2.0}{10}$	$\frac{2.5}{8}$	2.4	$\frac{1.9}{10}$	$\frac{1.8}{28.2}$	1.68	0.85
					28.2	30.2 on Patch

92Rt

 3+10⁴ = 8" wide N+S. Brick wall.

86.8	86.3	87.9
3.0	3.5	1.9
92	92	92
End	B.W.	T.W.

3+10 7² Rt. = end conc. drive to double Gar.

86.69	86.69	86.82
3.13	3.13	3.0
92	10	61
		Gar. Floor

3+00

86.5	86.5	86.0	86.1	86.4
$\frac{3.3}{25}$	$\frac{3.3}{10}$	$\frac{3.8}{8}$	3.7	$\frac{3.4}{10}$

2+93 10¹ Rt. = start 10" drive to double Gar.

86.25	86.8
3.57	3.0
102	61
	Gar. Floor

89.82

E.+W. Alley

T.P. 8.06 106.58 0.24 98.52

Cont.

5+59 12⁹ Lt. = start Conc. drive to
12⁹ Lt. = end Conc. block wall

double Gar.

5+24 12' Lt. = start 6' high Conc. block wall,

5+00

4+71 9⁹ Rt. = back face pole P.A. 604

4+68 9⁹ Rt. = end post + wire fence.

4+51 10' Rt. = Nly. Face 9" diam. eucalyptus

4+50

4+00 10⁹ Lt. = end wire fence

3+51 9⁹ Rt. = start post + wire fence.

98.59
0.17
12⁹
drive

97.6 98.2 98.1 97.5 98.0 98.4
1.2 0.6 0.7 1.2 9.8 0.4
12⁹ 12⁹ 10 7 10
B.W. End.

96.2 96.6 96.5 96.0 96.0 96.0 96.4
2.6 2.2 2.3 2.8 2.8 2.8 2.7
12 12 10 8 8 10
B.W. End

95.6 95.2 94.8 95.2 95.6
3.2 3.6 4.0 3.6 3.2
10 7 10 15

93.0 93.1 93.01 93.1 92.8
5.8 5.7 5.75 5.7 6.0
50 10 M.H. 10 50
RITT

91.8 91.2 90.7 90.7 90.8 90.5
7.0 7.6 8.1 8.1 8.0 8.3
25 10 8 10 25

98.76

E+W. Alley

6+00

99.9	99.6	99.8
6.7	7.0	6.8
10		10

Cont.

101.66
 4.92
 25
 Gar. floor

12³ Lt. = end. conc. block wall.

5+97 10⁵ Lt. = start apron to 3 car gar.

101.3	100.2	100.5	100.11
5.26	6.4	6.13	6.47
16	122	123	105
on Dr.	B.W.	only	Apron.
		Wtg. edge	drive

5+90 - 10⁹ Rt. = start stucco wall 45' high.

5+89 9⁴ Rt. = back face Pole # P.A. 674

99.7
 6.9
 107
 End. + B.W.

5+86 12³ Lt. = end 4' high conc. block wall = start 6' high conc. block wall

99.5	98.3	99.6
7.1	8.3	7.0
12 ³	12 ³	12 ³
B.W. to east	B.W. to west	end

5+79 12⁴ Lt. = start 5' high conc. block wall

98.3	99.2
8.3	7.4
12 ²	12 ²
B.W.	end
99.28	98.96
7.30	7.62
50	131
on drive	

5+77 - 13¹ Lt. = end conc. drive

106.58

E. + W. Alley

G+52 - 11' Rt. = start board fence.

G+51 - 10⁹ Rt. = \pm north face arch post, 1' x 1' x 9' stucco

G+50

102.0	101.6	101.8
4.6	5.0	4.8
10		10

G+49 11⁸ Lt. = end conc. block wall.

101.9	102.1
5.2	4.5
11 ⁸	11 ⁸
B.W.	End

G+42 - 10³ Rt. = \pm North Face 1' x 1' x 9' stucco arch post.

11⁷ Rt. = \pm 3' wide conc. walk.

G+40 9⁵ Rt. = \pm 3' wide conc. step

101.87	102.12	102.42
4.71	4.40	4.16
9 ⁵	11 ⁹	2 ⁵
step	walk	walk

(11² Lt. = start 18" high conc. block wall.

G+39 } 9³ Lt. = end conc. drive to double Gar.

101.66	101.74	101.5	101.38
4.92	4.84	5.1	5.20
2A ⁷	16	11 ²	9 ⁹
Gar. floor	on Dr.	end + B.W.	drive

G+36 10² Rt. = end stucco wall

101.9
5.2
10 ⁹
end
+ B.W.

106.58

E. + W. Alley

7+19 10' RT. } = B.C. 2' Rad. alley Cl. Ret
99 Lt. }

99 Lt. = start alley curb.

10' Rt. = start alley curb.

10' Rt. = end conc. dr.

7+10 98 wly. line Draper

7+02 10² Rt. = start conc. drive

0.76 105.82

7+00 10² Rt. = end board fence.

T.P. 5.30 111.12 0.76 105.82

6+85 - 17² Lt. = 8' wide conc. apron. to Sing Gar.

6+75

106.86

4.26

99

Cl. B.C.

106.85

4.27

10

Cl. B.C.

107.01

4.11

99

Cl

106.6

4.5

99

End

106.6

4.5

106.82

4.3

80

End

106.97

4.15

10

drive

107.03

4.09

10

Cl.

106.56

4.56

10²

on drive

106.3

4.8

2.5

on drive

105.7

5.4

10

105.7

5.4

111.12

106.2

4.9

10

104.78

1.80

203

Gar. floor.

104.68

1.90

172

104.6

2.0

15

103.9

2.7

10

103.5

3.1

8

103.3

3.3

103.8

2.8

10

106.58

E+W Alloy

Carried Fwd to p. 23

Check Temp B.M.

7.64 82.72 = 82.71

Pole # PA.524 Page 15

T.P. 7.55 90.36 11.33 82.81

T.P. 0.05 94.14 11.76 94.09

T.P. 0.15 105.85 5.42 105.70

S.W. B.P. Nautilus + Draper

7+41 ± Draper

106.7	106.9	107.0	106.8	106.5
4.4	4.2	4.1	4.3	4.6
60	10		10	60

12' RR }
12' Lt. } = E.C. v' Rad. cl. Ret.

7+21 = Wly. cl. line Draper

106.52	106.0	106.81	106.5	106.5	106.3	106.83	105.9	106.5
4.60	5.1	4.31	4.6	4.6	4.8	4.29	5.2	4.64
60	60	12	12		12	12	60	60
cl.	Ord.	E.C.	Ord		Ord.	cl.	Ord	cl.
						E.C.		E.C.

111.12

±

Conc. floor. (Level floor)

0+94 - 51' Lt. = ± double bar.

84.5
51.85
51
Floor0+85 - 13³ Lt. = start double bar. Conc. floor.83.23
7.13
133
Floor0+84 - 9¹ Lt. = end lath fence.0+54 - 9² Lt. = start lath fence

0+50

81.4 82.5 82.7 82.7
9.0 7.9 7.7 7.7
50 10 10 10

dirt floor

0+27 - 9² Lt. = ± 8' wide Car. Port82.2
8.2
92
End.0+22 - 9² Lt. = N.E. Cor. Stucco Bar.82.2
8.2
92
End.0+21 7⁴ Lt. = back edge pole. # JPA 6805

South Front.

0+03⁵ - 9² Lt. = S.E. Cor. Stucco Bar.82.0
8.4
92
End.0+03 - 7⁰ Lt. = lead man

0+00 = Nly. line E. & W. Alley (P 10)

81.3 81.6 82.7
9.1 8.8 8.2
10 10 10

90.36

1+54 15⁵ Lt. = start double Gar. No apron

84.32

6.04
155
Floor

1+50

83.36	84.3	84.5	84.8
7.0	6.1	5.9	5.6
40	10		10

1+28 19¹ Lt. = end conc. apron to double Gar.

83.49	83.51
6.87	6.85
201 Floor	191 Apron

1+12-19¹ Lt. = start conc. apron to double Gar.

83.96	83.73
6.90	7.13
201 Gar Floor	191 Apron

1+04 8⁷ Lt. = Back face of pole # PA 6849

82.8	83.8	83.7	83.6	84.6
7.6	6.6	6.7	6.8	5.8
40	10		10	50

0+99-13¹ Lt. = end double Gar. Conc. floor

83.22
7.14
131 Floor

90.36

N. + S. Alley

Reduced by
Andrew P. Lamore Jr

Check } sw. B.P.
Orig B.M. } La Jolla + Bon Air. 11.24 71.98 (71.98)

T.P. 0.50 83.22 7.64 82.72

2+35¹⁸ = Nautilus

80.31 82.12 82.06 82.54 84.56
10.05 8.24 7.90 7.52 5.80
60 10 10 10 60

2+17² } 12' Lt. } = E.C. 2' Rad alley cl. Ret.
12' Rt. }

79.96 79.69 81.70 81.20 81.63 82.12 82.57 83.88 84.23
10.40 10.67 8.66 7.16 8.73 8.24 7.79 6.48 6.13
60 60 12 12 6 12 12 60 60
cc G cc G cc E.C. cc cc

2+15² } 10' Lt. } = B.C. 2' Rad. alley cl. Ret.
10' Rt. }

81.72 81.36 82.05 82.56
8.64 7.00 8.31 7.80
10 10 10 10
cc G cc

2+05¹⁸ = Sly. line Nautilus = Start Conc. Pavement
10' Lt. } = start alley curbs
10' Rt. }

82.04 81.85 82.7 81.83 82.7 82.39 82.62
8.32 8.51 7.7 8.53 7.7 7.97 7.74
10 10 10 10 10 10 10
cc G end end G cc end

2+00

84.6 83.9 83.0 82.6 82.9 83.6 85.2 85.4
5.8 6.5 7.4 7.8 7.5 6.8 5.2 5.0
10 6 3 7 10 15 25

1+70 - 15³ Lt. = end double bar. Conc. Floor.

84.94 84.5 84.5 84.5 84.1 85.1 85.8
5.92 5.9 5.9 5.9 5.7 4.7 4.6
15 15 70 10 18 25
Floor

90.86 90.36

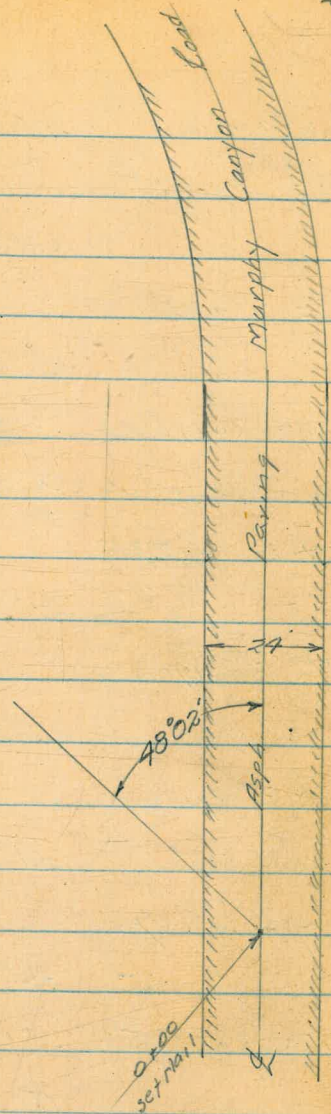
2-19-51 Stadia Survey of Road to proposed
 Hendricks City Dump in lots 3, 4, 5, 6, 7, 8
 Allen & Lots 6, 7, 8 then Riverside
 Shepard set stakes on all angle points
 Huffman

INDEXED

MAR 13 1951

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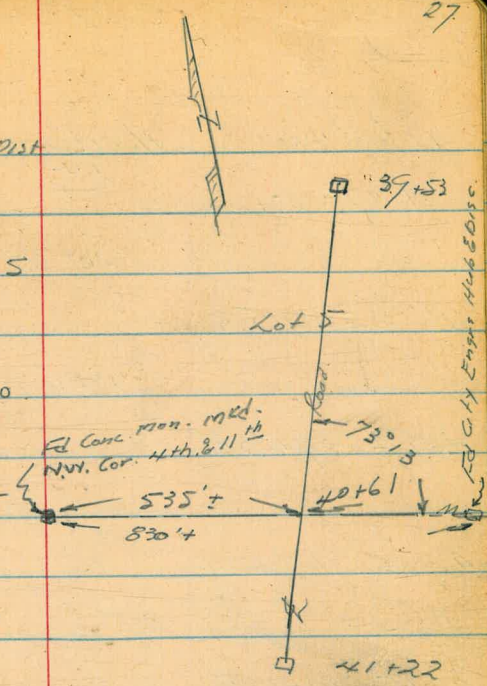
Station	Horizontal \angle Defl.	Vertical \angle	Stadia ^{Mean} Dist	True Dist
0+00 - E Murphy Canyon Rd	48° 02' Lt	-	202 } 202	202
A1 = 2+02	39° 21' Rt	-	192 } 192	192
A2 = 3+94	69° 42' Lt	-	119 } 120	119.5
A3 = 5+13.5	40° 05' Rt	-	161 } 160	160.5
A4 = 6+74	51° 34' Lt	-	216 } 216	216
A5 = 8+90	25° 58' Rt	3° 13'	319 } 318	318.5
A6 = 12+07.5	17° 05' Rt	-	86 } 86	86
A7 = 12+93.8	35° 20' Lt	-	134 } 134	134
A8 = 14+27.5				



Cont'd from P 26

27

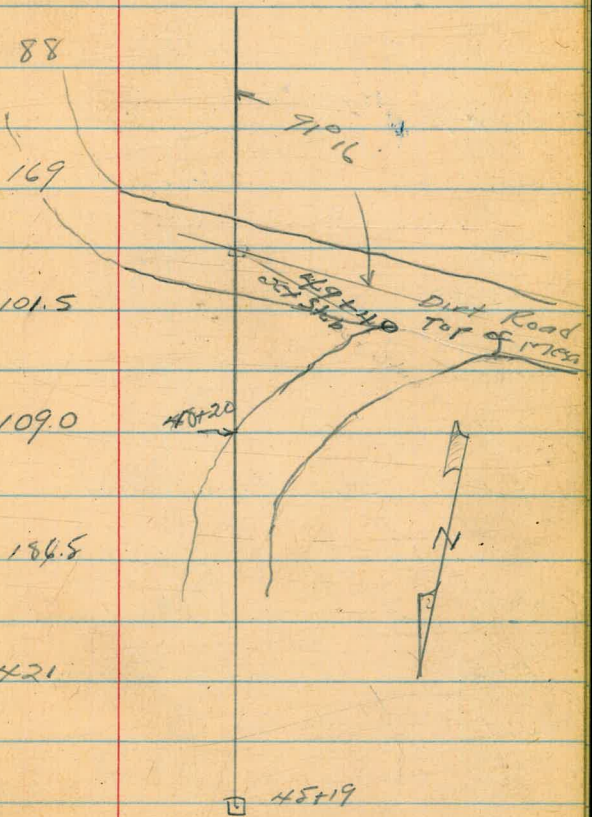
Station	Horizontal \angle Defl.	Vertical \angle	Stadia Dist Mean	True Dist
A 8 = 14+27.5	22° 56' RT.	2° 50'	367 } 366 } 366.5	365.5
A 9 = 17+93.0	19° 13' LT.	3° 15'	305 } 303 } 304.0	303.0
A 10 = 20+96.0	9° 59' LT.	3° 10'	362 } 363 } 362.5	361.5
A 11 = 24+57.5	21° 17' LT	2° 39'	233 } 233 } 233.0	232.5
A 12 = 26+90.0	27° 13' LT	2° 56'	274 } 273 } 273.5	273.0
A 13 = 29+63.0	21° 02' LT.	3° 57'	105 } 104 } 104.5	104.0
A 14 = 30+67.0	26° 09' LT		150 } 149 } 149.5	149.5
A 15 = 32+16.5	15° 18' LT		97 } 97 } 97	97
A 16 = 33+13.5	37° 29' RT.		213 } 213 } 213	212.5
A 17 = 35+26.0				



Cont'd from P. 27

28

Station	Horizontal \angle Def ⁿ	Vertical \angle	Stadia Dist	True Dist.
A 17 = 35+20.0	20° 30' Lt.	3° 24'	340 } 340 } 340	339
A 18 = 38+65.0	9° 51' Lt.		88 } 88 } 88	88
A 19 = 39+53.0	20° 27' Rt.		169 } 169 } 169	169
A 20 = 41+22.0	22° 50' Lt.		102 } 101 } 101.5	101.5
A 21 = 42+235	47° 44' Rt.		109 } 109 } 109	109.0
A 22 = 43+32.5	78° 10' Lt.	4° 41'	188 } 188 } 188	186.5
A 23 = 45+19	39° 09' Rt.	2° 45'	422 } 422 } 422	421
A 24 = 49+40				



2-21-51 Levels Proposed Rubbish
Hendricks Dump road
Allen
Shepard
Huffman

4

29

0198 Beg. 9.7 wide Steel Rail Cattle Guard.

297.5
34

0189

297.3
35

0152

298.5
24

0117 Edge Asph Pavement

299.96
092

0100 Nail Murphy Canyon Road

300.00
093
Nail

BM 0.93 $\frac{300.93}{1}$

300.00

(Assumed)

Nail & Murphy Canyon Road = 0100

300.93

Contd.

3+00

2+50

2+02 L. Rt. (bisector)

1+50

1+15

1+02.5 End Cattle Guard

30093
1

30

293.0
7 2

292.7
8 2

293.9
7 0
7 0
10
(Traveled Road way)

295.6
5 2

296.2
4 2

297.4
3 5

5 + 50

5 + 13.5 L Section on Bisector

4 + 62 Edge of Creek

4 + 42 Edge of Creek

T.P. 745 $\frac{298.74}{\wedge}$ 964 291.29

3 + 94 L Section on Bisector

3 + 60

$\frac{300.93}{\wedge}$

~~4~~

294.6
~~4~~

292.5 292.5
6² 6²
10
(Roadway)

286.7
12⁰

286.6
12¹

on stub 3 + 94 $\frac{298.74}{\wedge}$

290.6 291.2 291.3
10³ 97 96
(12 2)
Roadway

293.7 294.0 294.1
7² 6⁹ 6⁸
(7 3)
Traveled way

Cont'd.

8+74 Beg Board fence 37' Rt

8+25

303.5
78

7+75

301.7
96

7+25

299.7 299.9 300.0
11 11 11
(7 4)
Roadway

6+74 (section on bisector)

298.2 298.6 298.9
13 12 12
(20 8)
Roadway

T.P. 12.71 311.32 0.13 298.61

311.32

6+50

297.2 297.5
1 1
(15 13)
Roadway

6+00

295.7
30

298.74

298.74

Contd.

10+50

	320.6	320.8	320.2
27		27	33
9			16

18+00

	316.8
67	

9+78 36" Euc. Tree 10' H

	315.6	315.1	314.9
79		84	86
6			13

9+50

	314.0	313.2	313.0
95		10	10
15			8

9+42 36" Euc. Tree
End Board fence 6.3' R4'

TP 12.36 323.51 0.17 311.15

323.51

8+90 L (Bisector)

	309.5	308.7	308.1
18		26	32
7			12
		Roadway	
		311.32	

311.32

Cont'd.

12+93.5 L (section on Bisector)

	326.9	327.4	327.9
4	2	4	2
14			10

12+50

	326.5
5	1

12+07.5 L (Section on Bisector)

	325.8	325.8	325.1
5	8	5	8
5			18

11+87

	325.4	325.4	324.9
6	2	6	2
10			12

11+50

	324.2
7	4

T.P. 8.22 $\frac{331.59}{\lambda}$ 0.14 323.37

331.59
λ
322.5
10

11+00

323.51
λ

323.51
λ

Cont'd

35

15+30 Edge Road.

$$\begin{array}{r}
 333.2 \quad 333.6 \\
 10 \frac{7}{8} \quad 9 \frac{8}{8} \\
 \text{Roadway} \\
 \hline
 \end{array}$$

15+05 Bank

$$\begin{array}{r}
 336.4 \quad 332.6 \quad 333.7 \\
 7 \frac{0}{8} \quad 10 \frac{8}{8} \quad 9 \frac{7}{8} \\
 \text{Roadway} \\
 \hline
 \end{array}$$

14+75

$$\begin{array}{r}
 334.6 \quad 334.8 \quad 331.3 \quad 332.0 \\
 8 \frac{8}{8} \quad 8 \frac{6}{8} \quad 12 \frac{2}{8} \quad 11 \frac{4}{8} \\
 \text{Roadway} \\
 \hline
 \end{array}$$

TP. 12.03 $\frac{343.38}{\wedge}$ 0.24 331.35

$$\frac{343.38}{\wedge}$$

14+27.5 Bisector

$$\begin{array}{r}
 330.4 \quad 330.2 \quad 329.0 \quad 328.9 \\
 1 \frac{3}{8} \quad 1 \frac{2}{8} \quad 2 \frac{6}{8} \quad 2 \frac{2}{8} \\
 \text{Roadway} \\
 \hline
 \end{array}$$

14+15 Edge Rd.

$$\begin{array}{r}
 328.7 \quad 328.9 \\
 2 \frac{9}{8} \quad 2 \frac{7}{8} \\
 \text{Roadway} \\
 \hline
 \end{array}$$

13+68

$$\begin{array}{r}
 326.5 \quad 326.6 \quad 326.9 \\
 5 \frac{1}{8} \quad 5 \frac{0}{8} \quad 4 \frac{7}{8} \\
 12 \quad 13
 \end{array}$$

$$\frac{331.59}{\wedge}$$

$$\frac{331.59}{\wedge}$$

Cont'd

30

18+50

352.4	352.4	352.5
20	20	29
15		6

17+93 \angle Bisector

349.3	349.0	349.9
61	64	65
17		7

17+50

346.1	346.1	345.7
93	93	92
14		12

T.P. 12.42 \checkmark 355.42 \checkmark 0.38 343.00

355.42

16+90

341.7	341.3	341.1
17	21	23
14		7

16+50

339.6

16+00

336.5	336.7	337.1
69	67	63
8		17

343.38
 $\overline{\quad}$

343.38
 $\overline{\quad}$

Cont'd.

TP 12.73 $\frac{380.49}{\wedge}$ 0.27 367.76
 21+35

20+96 \angle Bisector

20+50

20+00

19+50

TP 12.75 $\frac{368.03}{\wedge}$ 0.14 355.28

19+00

$\frac{355.42}{\wedge}$

37

\angle

367.1
 $\frac{0.9}{18}$ 367.2 366.9
 $\frac{0.8}{5}$ 1

366.3
 $\frac{1.7}{15}$ 366.28 366.3
 (15 546 5)

363.3
42

358.7 359.0 359.0
 $\frac{9.3}{12}$ 90 90
 (12 9)

357.1
109

368.03
 $\frac{354.7}{12}$ 354.8 354.8
 $\frac{0.6}{8}$

$\frac{355.42}{\wedge}$

Contd.

24 + 57.5 L. (Bisector)

386.6	386.8	386.6
64	62	64
18		5

24 + 00

381.5	381.7	381.4
11	11	11
13		9

TP. 12.92 $\frac{39399}{1}$ 0.42 380.07

379.99
1
379.2

23 + 50

376.9	376.7	376.6
36	38	39
9		13

23 + 00

373.7
6
8

22 + 50

371.0	371.1	370.6
95	94	99
13		10

22 + 00

$\frac{380.49}{1}$

$\frac{380.49}{1}$

Cont'd.

27+50

399.7	399.8	399.7
$\frac{33}{12}$	$\frac{2}{9}$	$\frac{33}{9}$

26+90 \triangle (Bisector)

397.4	397.5	397.5
$\frac{56}{20}$	$\frac{55}{1}$	$\frac{55}{1}$

26+50

396.5	396.7	396.2
$\frac{65}{13}$	$\frac{63}{10}$	$\frac{68}{10}$

26+00

395.6	395.6	394.9
$\frac{74}{11}$	$\frac{74}{7}$	$\frac{81}{7}$

25+50

394.5	394.4	394.1
$\frac{85}{11}$	$\frac{86}{12}$	$\frac{89}{12}$

TP 10.18 $\frac{40302}{\wedge}$ 0.15 392.8x

40302

390.3	390.5	390.2
$\frac{27}{12}$	$\frac{25}{10}$	$\frac{28}{10}$

25+00

$\frac{392.99}{\wedge}$

Cont'd.

T.P. 11.40 $\frac{427.22}{\wedge}$ 0.05 41582

30+00

29+63 \sphericalangle (Bisector)

29+35

29+00

28+50

28+00

T.P. 13.26 $\frac{41587}{\wedge}$ 0.41 40261
 $\frac{403.02}{\wedge}$

~~4~~

413.5

~~24~~

411.4

411.5

411.5

~~45~~

~~44~~

~~44~~

13

4

409.8

410.0

409.7

~~61~~

~~59~~

~~63~~

10

9

407.7

~~83~~

405.2

405.5

405.0

~~107~~

~~104~~

~~109~~

12

10

403.5

~~124~~

41587

$\frac{\wedge}{\wedge}$

Contd

TP 13.42 $\frac{439.60}{\wedge}$ 1.04 426.18

on stub 32+16.5

32+16.5 \triangleleft Bisector

	425.7	426.2	426.4
15			0.8
12		10	

32+00

	424.6	424.8	425.0
26			22
10		24	11

31+50

421.5
57

31+00

	419.5	419.6	420.0
77			73
10		76	9

30+67. \triangleleft Bisector

	418.2	418.7	419.0
90			83
13		85	9

30+50

	417.2	417.6	417.8
100			94
11		96	12

$\frac{427.22}{\wedge}$

427.22

Contd.

34+50

436.4
52

34+00

434.1 433.5 433.8
55 61 58
11 13

33+50

431.7 431.9 431.8
79 77 78
8 17

33+13.5 L. Bisector

429.8 429.8 430.4
98 98 93
1 24

32+75

428.0 428.2 428.0
115 117 115
11 11

32+50

427.4 427.4 427.4
123 123 123
12 9
439.60

439.60
1

Contd.

37+00

449.9	450.2	450.1
15	2	3
16		8

36+50

446.3	446.6	446.8
5	8	6
16		10

36+10

444.0	444.2	444.7
7	7	6
14		7

35+75

442.7	442.7	442.9
8	8	8
13		8

35+26 L. (section on) Bisector

440.9	441.0	440.9
10	10	10
14		10

TP. 12.21 $\frac{451.41}{\lambda}$ 0.40 $\frac{439.20}{\lambda}$

34+80

438.5	438.2	438.1
1	1	5
9		12

$\frac{439.60}{\lambda}$

$\frac{439.60}{\lambda}$

Cont'd.

40+00

39+53 L Section on Bisector

TP 11.80 $\overset{\vee}{474.88}$ 0.47 463.38

39+00

38+65 L Section on Bisector

38+00

37+50

TP 12.62 $\overset{\vee}{463.85}$ 0.18 451.23
 $\overset{\vee}{451.41}$

469.2
57
12
469.0
59
9
468.6
63
9

466.0
87
8
465.9
90
13
465.5
94

474.88
462.8
11
15
463.0
8
7
463.2
06
7

461.0
29
14
461.2
26
7
461.6
73
5

457.0
68
12
457.2
66
8
457.2
67

453.6
103
14
454.0
99
7
454.9
99

463.85

Contd.

42+23.5 L Bisector

$$\begin{array}{r}
 483.4 \\
 \times 2 \\
 \hline
 2
 \end{array}
 \quad
 \begin{array}{r}
 483.4 \\
 \times 2 \\
 \hline
 19
 \end{array}
 \quad
 \begin{array}{r}
 483.1 \\
 \times 5 \\
 \hline
 19
 \end{array}$$

42+00

$$\begin{array}{r}
 481.8 \\
 \times 8 \\
 \hline
 9
 \end{array}
 \quad
 \begin{array}{r}
 482.1 \\
 \times 5 \\
 \hline
 12
 \end{array}
 \quad
 \begin{array}{r}
 482.0 \\
 \times 6 \\
 \hline
 12
 \end{array}$$

41+75

$$\begin{array}{r}
 480.0 \\
 \times 7 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 480.6 \\
 \times 7 \\
 \hline
 7
 \end{array}
 \quad
 \begin{array}{r}
 480.8 \\
 \times 8 \\
 \hline
 7
 \end{array}$$

41+22 L Section on Bisector

$$\begin{array}{r}
 477.0 \\
 \times 10 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 477.1 \\
 \times 10 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 477.2 \\
 \times 10 \\
 \hline
 14
 \end{array}$$

T.P. 13.02 $\overline{487.59}$ 0.31 $\overline{474.57}$

$\overline{487.59}$

40+90

$$\begin{array}{r}
 475.2 \\
 \times 10 \\
 \hline
 11
 \end{array}
 \quad
 \begin{array}{r}
 474.6 \\
 \times 0 \\
 \hline
 9
 \end{array}
 \quad
 \begin{array}{r}
 474.6 \\
 \times 0 \\
 \hline
 9
 \end{array}$$

40+50

$$\begin{array}{r}
 472.6 \\
 \times 12 \\
 \hline
 12
 \end{array}
 \quad
 \begin{array}{r}
 472.4 \\
 \times 2 \\
 \hline
 10
 \end{array}
 \quad
 \begin{array}{r}
 472.0 \\
 \times 2 \\
 \hline
 10
 \end{array}$$

$\overline{474.88}$

$\overline{474.88}$

Cont'd.

$$\begin{array}{r} \downarrow \\ \text{T.P. } 13.35 \quad 513.39 \quad 0.31 \quad 500.0x \\ \hline \end{array}$$

 44+50

44+00

43+50

43+32.5 ← Section on Bisector

43+00

$$\begin{array}{r} \downarrow \\ \text{T.P. } 12.96 \quad 500.35 \quad 0.20 \quad 487.39 \\ \hline \end{array}$$

42+50

$$\begin{array}{r} 487.59 \\ \hline \end{array}$$

£

$$\begin{array}{r} 498.6 \\ 17 \\ \hline 11 \end{array} \quad \begin{array}{r} 499.2 \\ 11 \\ \hline 13 \end{array} \quad \begin{array}{r} 499.4 \\ 0.9 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 495.2 \\ 5 \\ \hline 16 \end{array} \quad \begin{array}{r} 495.8 \\ 5 \\ \hline 9 \end{array} \quad \begin{array}{r} 496.0 \\ 4 \\ \hline 9 \end{array}$$

$$\begin{array}{r} 492.2 \\ 8 \\ \hline 18 \end{array} \quad \begin{array}{r} 492.8 \\ 7 \\ \hline 12 \end{array} \quad \begin{array}{r} 493.2 \\ 7 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 491.4 \\ 8 \\ \hline 26 \end{array} \quad \begin{array}{r} 491.6 \\ 8 \\ \hline 6 \end{array} \quad \begin{array}{r} 491.6 \\ 8 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 489.2 \\ 11 \\ \hline 13 \end{array} \quad \begin{array}{r} 488.6 \\ 11 \\ \hline 6 \end{array} \quad \begin{array}{r} 488.2 \\ 12 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 500.35 \\ \hline \end{array}$$

$$\begin{array}{r} 484.9 \\ 27 \\ \hline 10 \end{array} \quad \begin{array}{r} 485.1 \\ 25 \\ \hline 8 \end{array} \quad \begin{array}{r} 484.8 \\ 2.8 \\ \hline 8 \end{array}$$

$$\begin{array}{r} 487.59 \\ \hline \end{array}$$

47+00

$$\begin{array}{r} 520.2 \\ \times 7 \\ \hline 11 \end{array} \quad \begin{array}{r} 520.1 \\ \times 8 \\ \hline 13 \end{array} \quad \begin{array}{r} 520.3 \\ \times 6 \\ \hline 13 \end{array}$$

46+50

$$\begin{array}{r} 517.1 \\ 78 \\ \hline 12 \end{array} \quad \begin{array}{r} 516.9 \\ 80 \\ \hline 15 \end{array} \quad \begin{array}{r} 516.6 \\ 83 \\ \hline 15 \end{array}$$

$$\begin{array}{r} \checkmark \\ TP. 1174 \quad 524.92 \\ \hline 0.21 \quad 513.18 \end{array}$$

524.92

46+00

$$\begin{array}{r} 513.0 \\ 04 \\ \hline 12 \end{array} \quad \begin{array}{r} 512.6 \\ 08 \\ \hline 13 \end{array} \quad \begin{array}{r} 512.3 \\ 11 \\ \hline 13 \end{array}$$

45+34 Edge Exist Road.

$$\begin{array}{r} 505.8 \\ 76 \\ \hline 24 \end{array} \quad \begin{array}{r} 506.1 \\ 73 \\ \hline 20 \end{array}$$

(Roadway)

45+19 L. Section on Bisector

$$\begin{array}{r} 506.9 \\ 65 \\ \hline 8 \end{array} \quad \begin{array}{r} 504.8 \\ 86 \\ \hline 20 \end{array} \quad \begin{array}{r} 504.9 \\ 85 \\ \hline 20 \end{array}$$

(Roadway)

44+93 Edge Exist Road.

$$\begin{array}{r} 502.6 \\ 108 \\ \hline 22 \end{array} \quad \begin{array}{r} 503.0 \\ 104 \\ \hline 22 \end{array}$$

(Roadway)

$$\begin{array}{r} 513.39 \\ \hline 1 \end{array}$$

$$\begin{array}{r} 513.39 \\ \hline 1 \end{array}$$

Cont'd.

TP.

3.84 527.20

on stub 49+40

48+20

intersection Road to Rt.

	518.7	518.5	518.8
6 ³	6 ⁴	6 ⁵	
6		10	

TP.

6.46 531.04 0.34 524.58

	522.7	522.9	522.9
2 ³	2 ⁰	2 ⁰	
14		10	

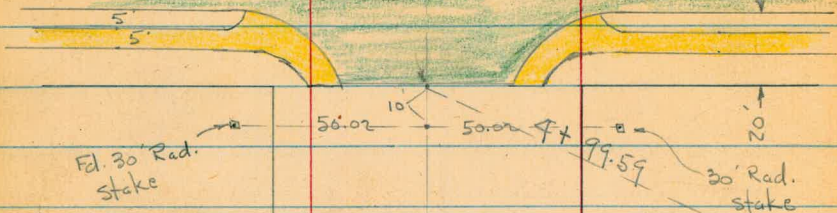
47+50

524.92

524.92
T

Haines New Const. Sec Plan st

A.C. Pav



Ave

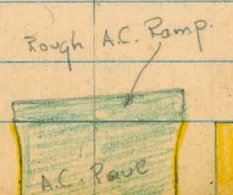
40' 40'

Thomas

Hub.

Mon.

Cresham



30' Rad.

Ingraham

Ld. ect. P & Cone. Pav

st.

Mon. set ld. ect. in A.C. Pav. 11-9-54

7

Ave

40' 40'

Thomas

180' 01' 30"

0+00 = Ang. 0° 01' 30" Lt.

Haines

A.C. Pav st.

INDEXED
MAY 24 1951

Lt. Rt.

X-Sect. Thomas Ave - from Gresham
to Ingraham = 80' st. 20' cbs.

5311 5-23-51 7.0.

W.O. 31760

0+00 = E.L. Gresham
0-01 = 22.7 Rt. = \pm W.M. ? Note Elev. is on pipe at valve
0-05 " " " " " " " " " " " "

0-10

0-40 = \pm

0-60 = w. cb.

pave ends 0.5 E - Rods on edge

0-80 = W.L. Gresham = end of curb + walks

Note: Used Elev. Rod. - Actual Elev. Shown

T.P.		12.78	44.17	
Set. B.M. - NE B.P. Haines +	Thomas	3.27	53.68	
T.P.	1.45	56.95	1.37	55.50
check B.M.		8.53	48.34	= Mon
B.M.	12.72	56.87	44.15	= \pm

38.2	37.8	36.9	36.8	36.6	36.6	36.7	36.5
50	40	20		10	20	40	50
					35.96		35.89
					22.7 = pipe		22.7
37.5	37.2	37.1	36.7	36.4	36.2	35.9	
50	40	20		20	40	50	
37.9	37.1	36.8	36.6	36.2	36.0	35.6	
100	40	20		20	40	75	
37.5	36.6	36.5	36.4	35.9	35.9	36.6	
40	30	20		20	27	40	
37.35	37.25	37.04	36.40	36.58	36.55	36.39	35.99
36.31		21.5	10		10	21.7	36.51
Cor. walk	Top	end cb. gut.				gut.	Top
							end cb.

\pm Thomas + W. 7' Line Ingraham - 48.36 = Book
hd + ct. Ingraham + Reed.

1+69-26' Lt. = ± W.M.

1+65-39.6 Rt. = ± 8' Conc. Dr.

1+62-30.5 Lt. = 6" Acacia

1+55-22.5 Rt. = ± W.M.

1+50

1+14-39.6 Rt. = ± 11' Conc. Dr.

1+00

0+89-21.7 Rt. = ± W.M.

0+64-24 Lt. = ± W.M.

0+61-39.7 Rt. = ± 11' Conc. Dr.

0+50

0+43-39.8 Rt. = ± 3' Conc. Walk

0+40-15.1 Rt. = ± 16" Cypress ✓

0+25-22.5 Rt. = ± W.M.

0+18-15.3 Rt. = ± 18" Cypress ✓

0+02-22.5 Rt. = ± F.H.

Lt. ± Rt.

40.01
26 = pipe

39.62 39.75
39.6 54.5 = floor
Dr. Gar.

38.40 = pipe
22.5

40.5 40.4 39.3 39.3 39.2 39.3 39.3
50 40 20 20 40 50

37.89 37.93
39.6 = Dr. 54.6 floor gar.

39.1 39.0 37.8 38.0 38.0 37.7 37.6
50 40 20 20 40 50

36.81
21.7 = pipe

36.05
24 = pipe

36.96 37.18
39.7 58.8 = floor
Dr. Gar.

38.2 38.0 37.3 37.0 37.2 36.9 37.0
50 40 20 20 40 50

36.95 37.02
39.8 50
walk walk

36.11
22.5
Pipe

Lt. \$ Rt.

3+61-22.6 Rt. = \$ w.M.

3+50 14.5 Rt. = \$ 36" Cypress

3+38-38.2 Lt. = Beq. Rail fence

3+32-39.6 Lt. = \$ 8" Conc. Dr.

3+09-31.6 Lt. = \$ w.M.

3+08-21.6 Rt. = \$ w.M.

3+00

2+50

2+19-23.3 Rt. = \$ w.M.

2+13-39.9 Rt. = \$ 3 Conc. walk

2+00-29 Lt. = \$ 8" Palm

1+99-39.9 Rt. = \$ 2' Conc. Strip

1+93-39.8 Rt. = \$ 4' Conc. Strip

1+87-39.8 Rt. = \$ 2' Conc. Strip - Dr. to Gar.

1+74-29.3 Lt. = \$ 5" Acacia

45.92
22.6=pipe

48.0 47.6 46.9 46.4 46.6 46.07 46.07
50 40 20 20 40= 50=
wly. of 2.7' Conc. walk walk

48.18 47.31
60. Dr. 39.6=Dr.
45.16
21.6=pipe

44.15
21.6=pipe

46.7 46.2 45.2 44.7 45.0 44.7 44.4
50 40 20 20 40 50

44.2 44.0 43.2 43.0 43.3 42.4 42.1
50 40 20 20 40 50

40.99
23.3=PIPE

41.51 41.39
39.9=walk-50

42.5 42.2 41.5 41.1 40.9 40.9 40.9
50 40 20 20 40 50

40.91
39.9
Conc 40.86 } 40.22
39.8 } 72.1 = floor
40.71 } Gar.
39.8 }

Lt. E Rt.

Elev. around Returns -

S.W. Ret. 36.1	around to P.C. -	10' apart.	30	T	52.84
end = W.L. Haines	T = Top	51.97		9	52.21
	9 = gut	51.40	37.5 = P.C.	T	52.96
10' around	T	52.17		9	52.46
	9	51.56			
20	T	52.27	N.E. Ret. - 36.1'		
	9	51.61	end = E.L. Haines	T	53.74
30	T	52.18		9	53.04
	9	51.55	10'	T	53.66
36.1 = P.C.	T	52.08		9	52.95
	9	51.43	20'	T	53.64
				9	52.95
N.W. Ret. - 37.5'			30'	T	53.67
end = W.L.	T	52.38		9	52.99
	9	51.78	36.1 = P.C.	T	53.70
10'	T	52.57		9	53.05
	9	51.92			
20	T	52.72			
	9	52.09			

S.E. Ref. - 36.8'

end = E.L.

T

53.19

9

52.51

10'

T

53.03

9

52.33

20

T

52.86

9

52.17

30

T

52.78

9

52.08

36.8 = P.C.

T

52.74

9

52.09

3+24-40.3 Lt. = end board fence + Reg. picket fence

3+00

58.0
50 57.4 56.4 55.8 54.8 53.9 53.4
40 20 20 40 50

2+98-33.4 Lt. = 4 W.M.

56.15

2+88-38.1 Lt. = 2.5 Conc. Walk

33.4
Pipe 58.05 57.56
55 38.1=walk

2+50-40 Lt. = Reg. Board fence

57.6 57.4 56.2 55.8 54.9 54.5 54.2
50 40 20 20 40 50

2+44-41 Rt. = 7' Conc. Dr.

54.39 54.20
41=Dr. 55=Dr.

2+40-41 Lt. = 8' Conc. Dr.

57.93 57.55
50 41=Dr.

2+27-22.8 Rt. = 4 W.M.

53.60
22.8
Pipe

2+24-40.5 Lt. = 5" Pine

2+07-29.4 Rt. = 6" Lognet ✓

2+04-36 Lt. = 4 W.M.

55.65
36=pipe

2+00

57.2 56.9 55.9 55.3 55.1 54.4 54.0
50 40 20 20 40 50

1+92-39.9 Lt. = 4" Pine ✓

1+70-33.9 Lt. = 4 W.M.

55.10
33.9=pipe

1+50

57.0 56.7 55.9 55.3 55.0 54.5 54.4
50 40 20 20 40 50

1+28-38.5 Lt. = end fence

1+28-21.2 Rt. = 4 W.M. + 34' Rt. = 2" Peach ✓

54.25

1+25-36 Rt. = 3' Conc. walk

54.74 21.2=pipe 54.37
36=walk 50 walk

40' E = \pm of Conc. pave = End.

19.9 E. = edge of Conc. pave

17' E - 22.7 Rt. = \pm P. pole # 4298

15' E. - 42.4 Lt. = \pm 24" Pepper

4+99.73 = W.L. Ingraham St.

4+66 - 41' Lt. = \pm 18" Acacia

4+65

4+60 - 39.9 Lt. = end fence

4+30

4+24 - 38' Lt. = \pm Conc. Dr.

4+00

3+70 - 39.7 Lt. = Beg. picket fence

3+59 39.9 Lt. = end of picket fence

3+54 - 32.4' Lt. = \pm w.M.

3+50 = W.L. of 2.5' Conc. walk on Lt.

59

	Lt.	E	Rt.						
	50.4 90	49.60 40	49.31 20	49.03	48.76 20	48.53 40	47.84 90		
	49.98 90	49.10 40	48.70 20	48.48	48.18 20	47.92 40	47.30 90		
	50.4 50	50.1 40	49.9 32	48.7 20	48.4 20	48.4 20	48.7 20	48.5 40	48.2 50
	50.7 50	50.2 40	49.2 20	49.0	49.5 20	49.8 40	49.7 50		
	53.4 50	52.9 40	51.0 20	51.0	51.3 20	51.7 40	51.7 50		
	54.6 50	54.0 40	52.5 20	52.6	52.7 20	52.8 40	52.7 50		
	54.71 51 floor qtr.	54.12 39 Brk	53.99 38 Dr.						
	55.9 50	55.6 40	53.6 20	53.4	53.1 20	52.9 40	52.8 50		
	58.22								
	32.4 = pipe								
	56.99 50 walk	56.74 39.7 walk	55.4 20	55.1	54.1 20	53.4 40	53.0 50		

9-6-59
Wot 20006

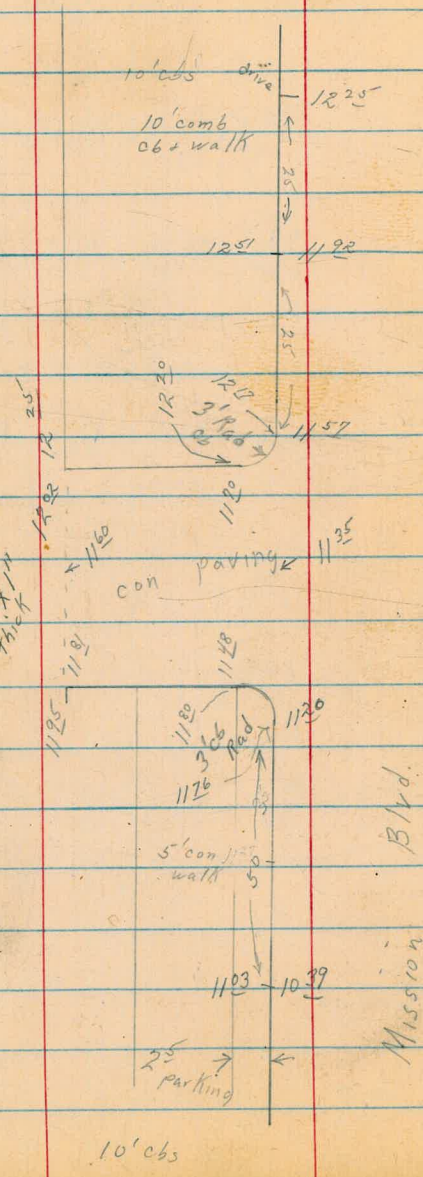
D. Smith
C Allen
H Bruer
Wm Altman

Levels for elev Returns Alley West Side Mission Blvd Ben Garnet + Hornblend

INDEXED

SEP 7 1951

BIKRRG Pacific Beach
old log
approx 1/4
thick



Note: used tape or elev. rod.

BM

1408
SEBP
Mission Blvd
Garnet

D. Smith
C. Allen
P. Taylor
R. Parks

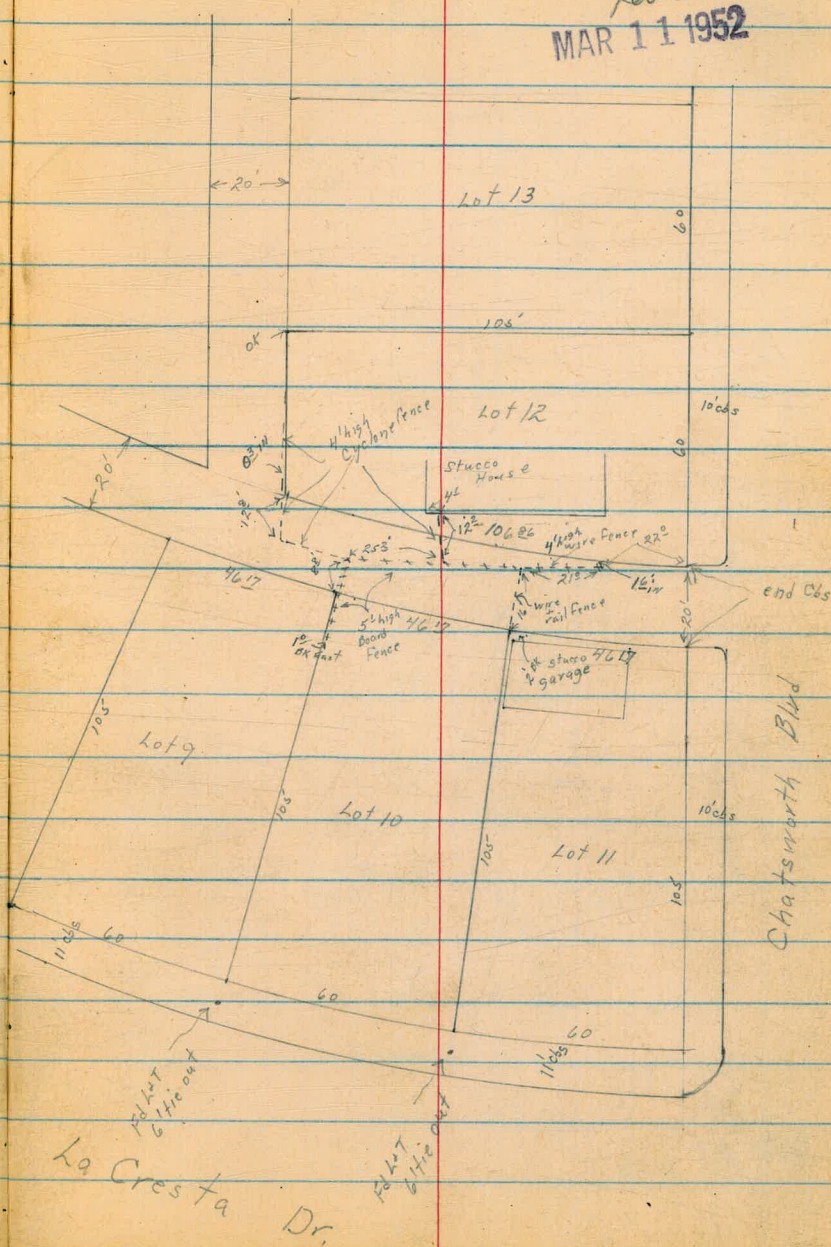
ENCROACHMENTS

Point Loma Hts

Alleys BIRG

wo# 20006
INDEXED
Law
MAR 11 1952

Ref: File Map # 1523



3+39 5' woven wire fence crosses Alley ✓

3+33 1" water stand pipe on & Alley ✓

3+27 End of wood pile in Alley ✓

Begin of big wood pile in Alley ✓

3+07 { 6⁵/₁₂ Lt Begin 6' woven wire fence ✓
4⁵/₁₂ Wood Fence crosses Alley ✓3+06 9¹/₂ Rt End double garage ✓2+86 9⁵/₁₂ Rt Spilled Conc. in front of garage
Begin Double Garage ✓2+53⁵ 7¹/₂ Rt End Wire & Lath Fence ✓2+29 8⁵/₁₂ Rt to Wire & Lath Fence Begins ✓2+28⁵ 9¹/₂ Rt End Double Garage ✓
7¹/₂ Rt End Conc Apron ✓2+09 { 9¹/₂ Rt Begin Double Garage ✓
7¹/₂ Rt to Conc Apron ✓

0+00 East Line Benicia Street ✓

4+17 3' Lt to 12" pepper Tree ✓

4+14.3 2⁵/₁₂ pickett fence on cobble wall crosses Alley ✓

4+12.61 West Line Colusa Street ✓

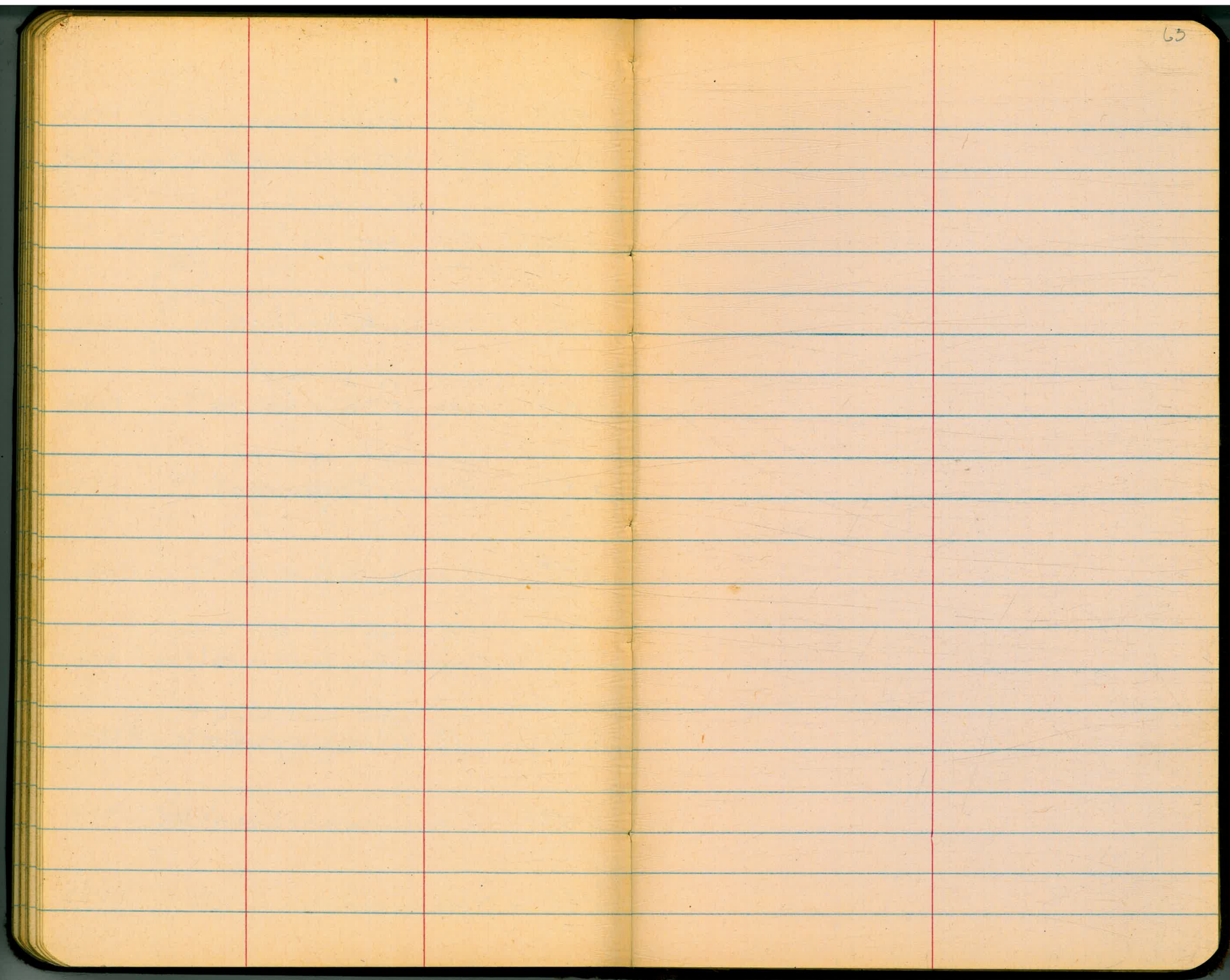
3+96 9' Lt to 5" Fig Tree ✓

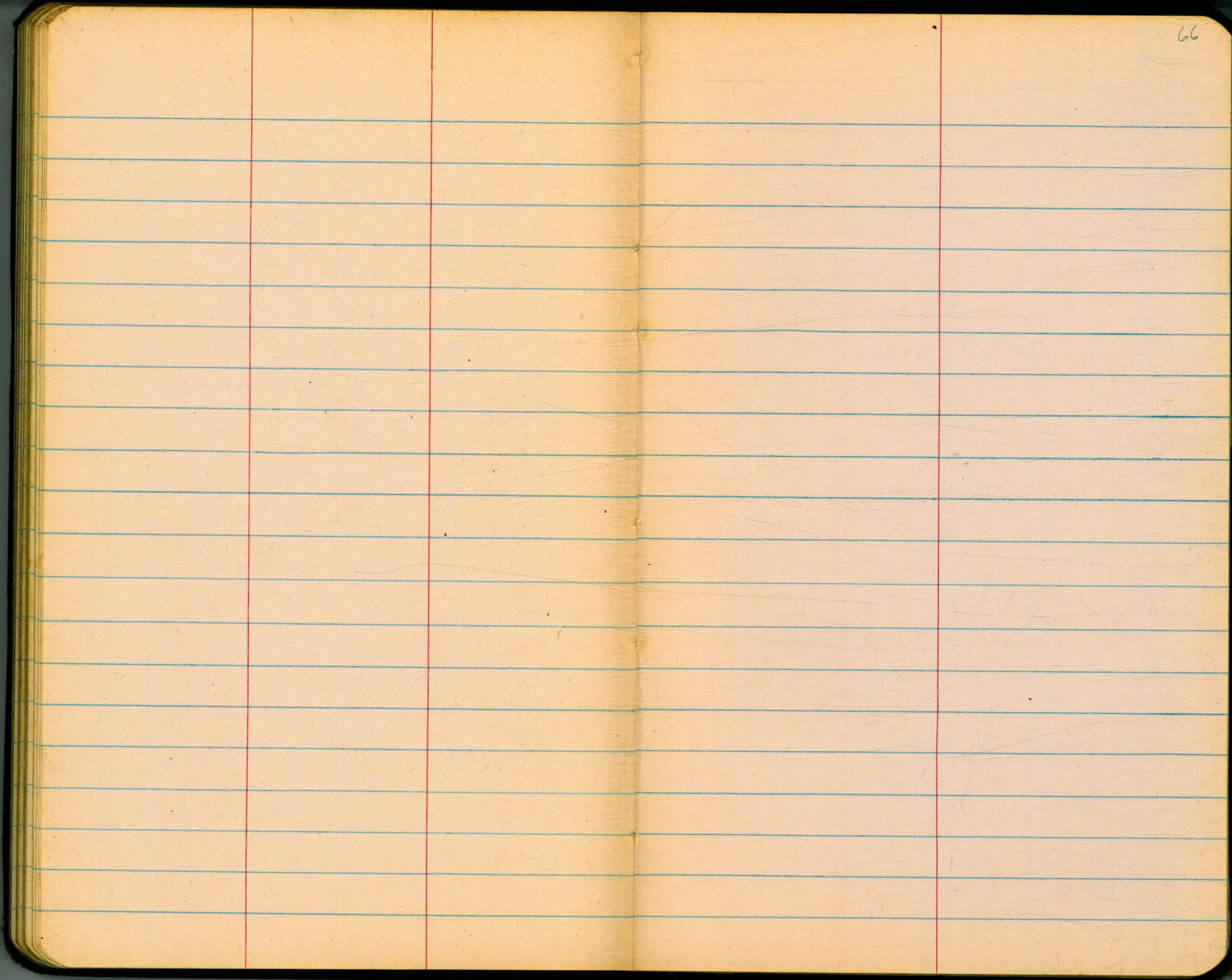
3+95⁵ { 4' Lt to 2" pepper tree ✓
4' Rt to 3" pepper tree ✓3+91⁵ 1¹/₂ Lt to 4" pepper tree ✓3+85⁵ 2" pepper Tree on & ✓3+76 7⁵/₁₂ Lt 6' woven wire fence Ends ✓
6' woven wire fence crosses alley ✓

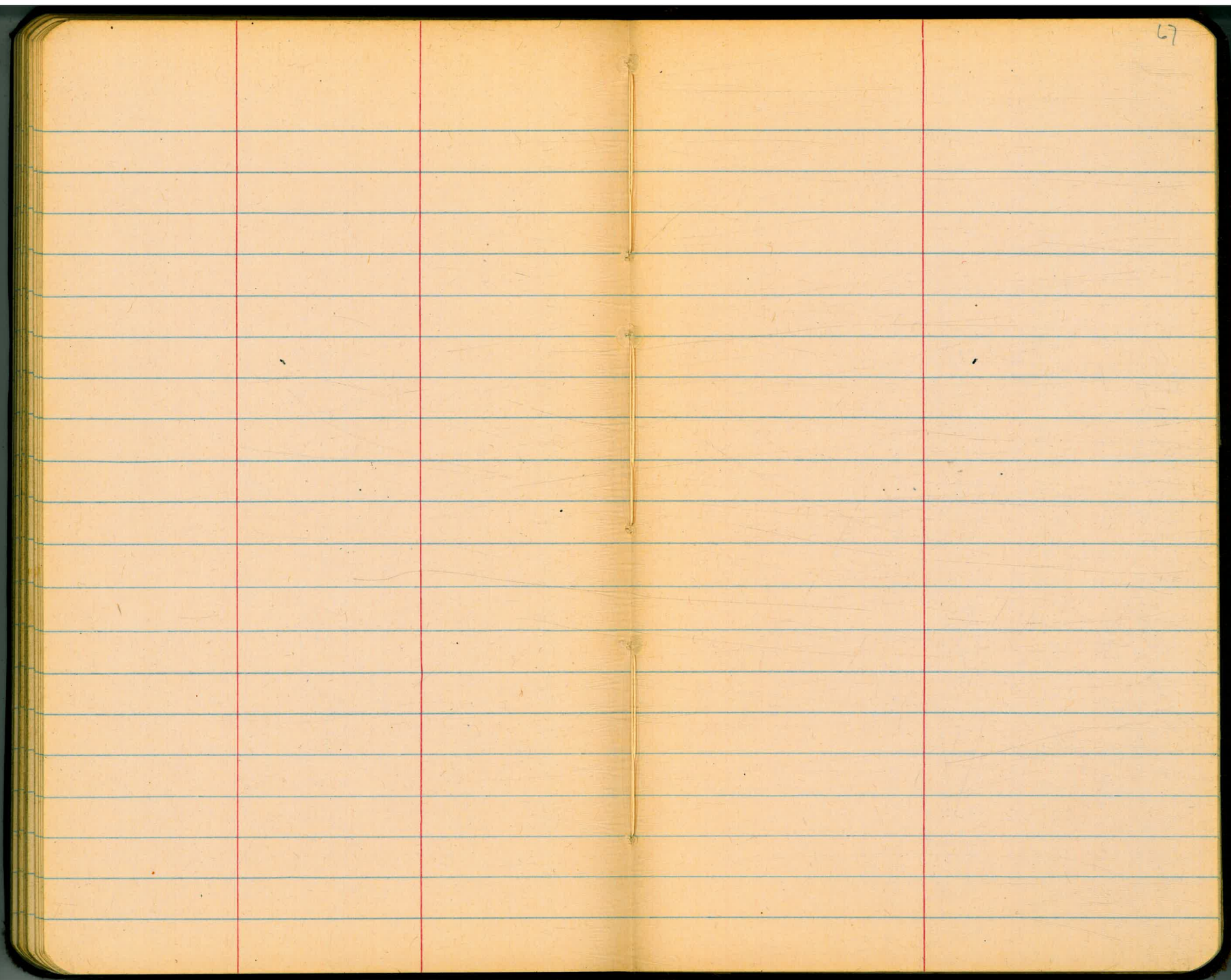
3+71 3' Rt to 6" Orange Tree ✓

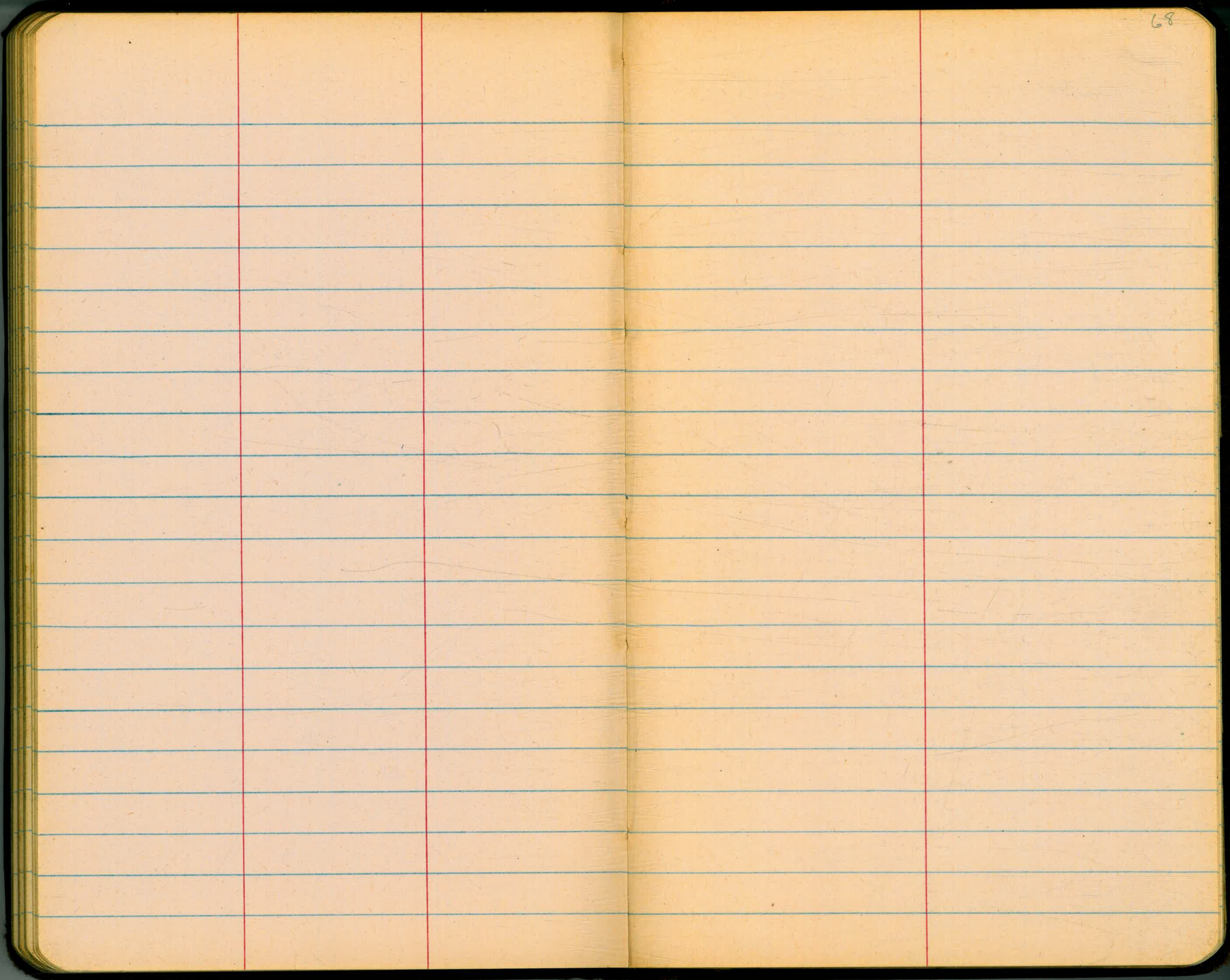
3+57⁵ 6' Woven wire fence crosses Alley ✓

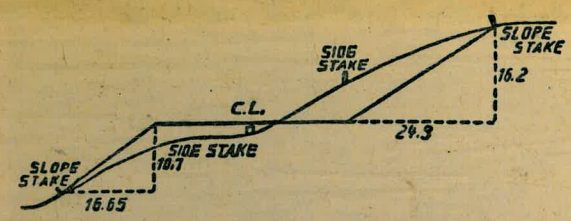
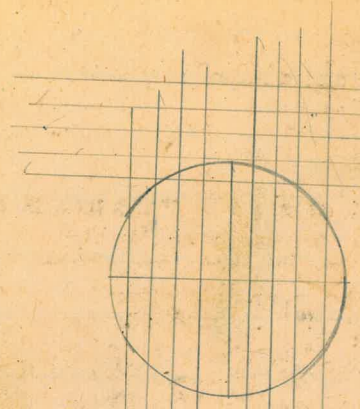
3+50 6' Rt 3" peach Tree ✓











DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50