

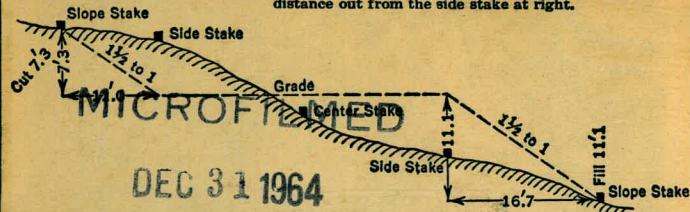
2105

K & E
FIELD BOOK
1930

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

Roadway of any Width. Side Slopes 1 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



DEC 31 1964

Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

702105

The paper in this book No. 360A is made of 50% high grade rag stock with a WATER RESISTING surface sizing.

KEUFFEL & ESSER CO., N. Y.

For Curve Tables see end of book.

X- Sec Altadena }
 Sterling Ct. } 20-36
 Nightmare }

Location existing culvert across 37
 Lots 1 & 2, B.K. 57, H.M. Higgins

29th & C, survey of Storm drain 38

LOCUST - Lowen to Macaulay 40-43

X Sec Texas - Camino del Rio to
 Trans Road 48-58

X - Sec West St. @ V. Blu to Logan 59

X - Sec Ark St for Safeway Store 72

In the f
 from th

Cut 7.3

Out or
 Fill

- 0
- 1
- 2
- 3
- 4
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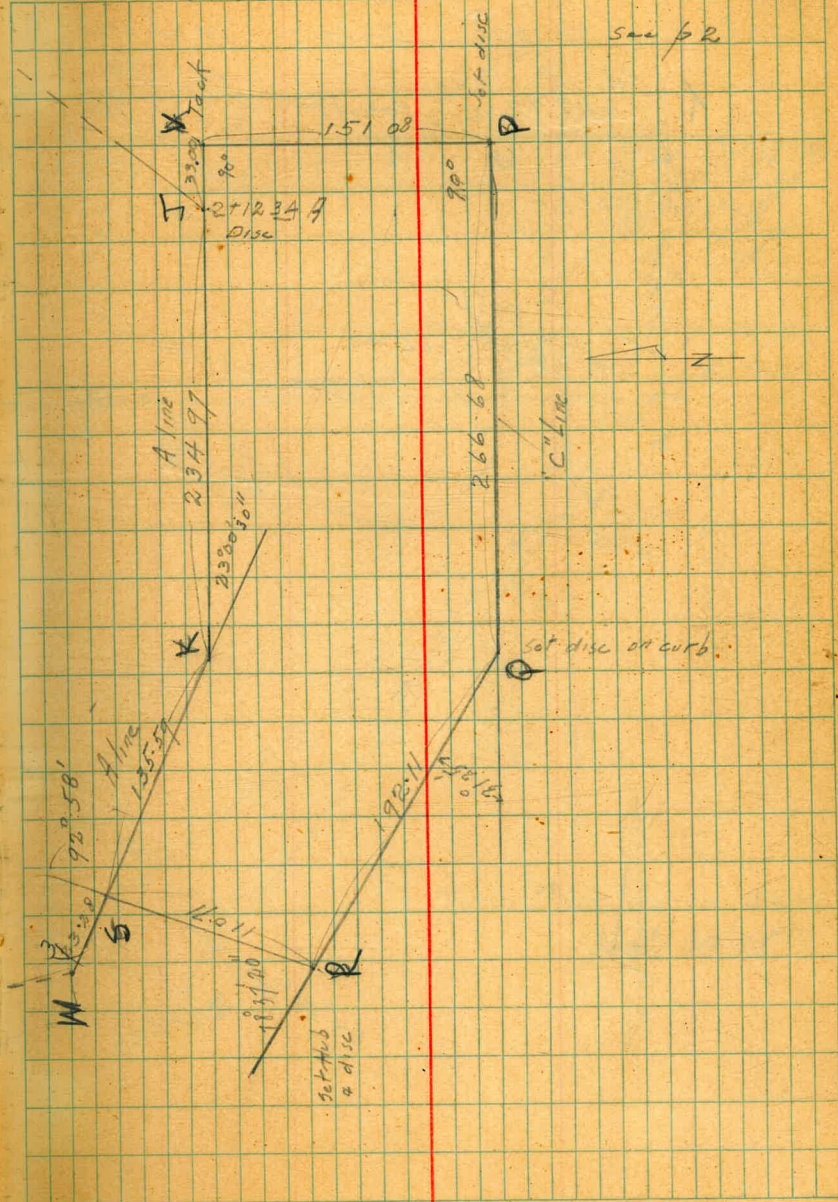
Moore
Begg
Sherman
Crawford

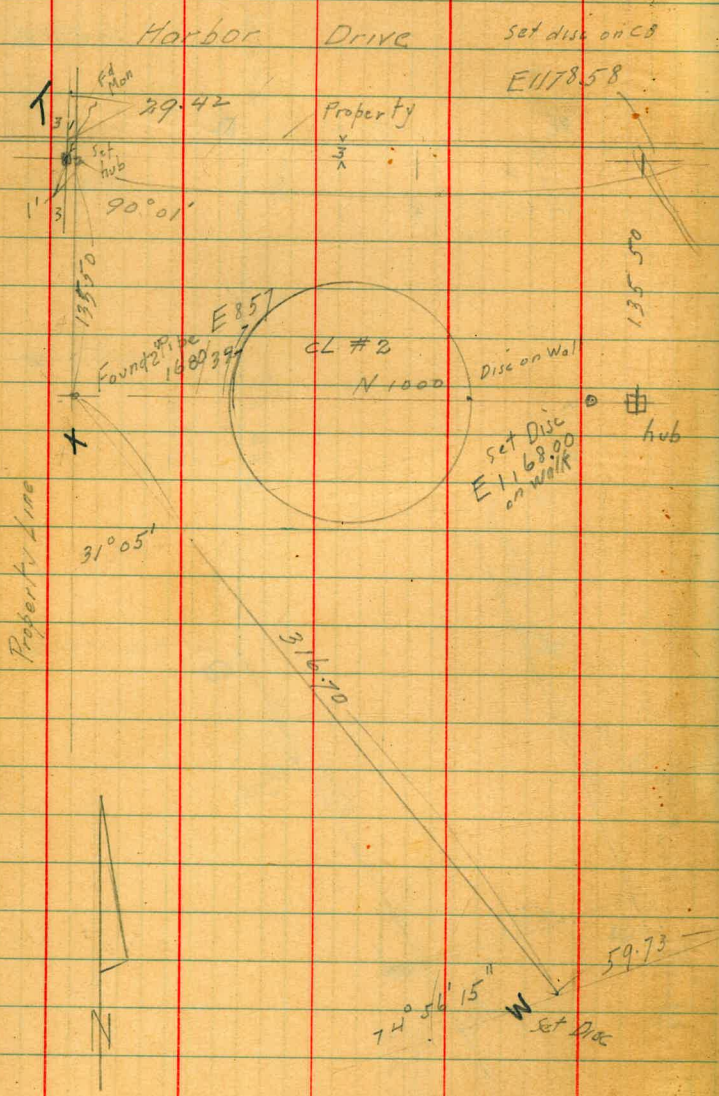
Mar 28 1950

Set

Base Line "C"

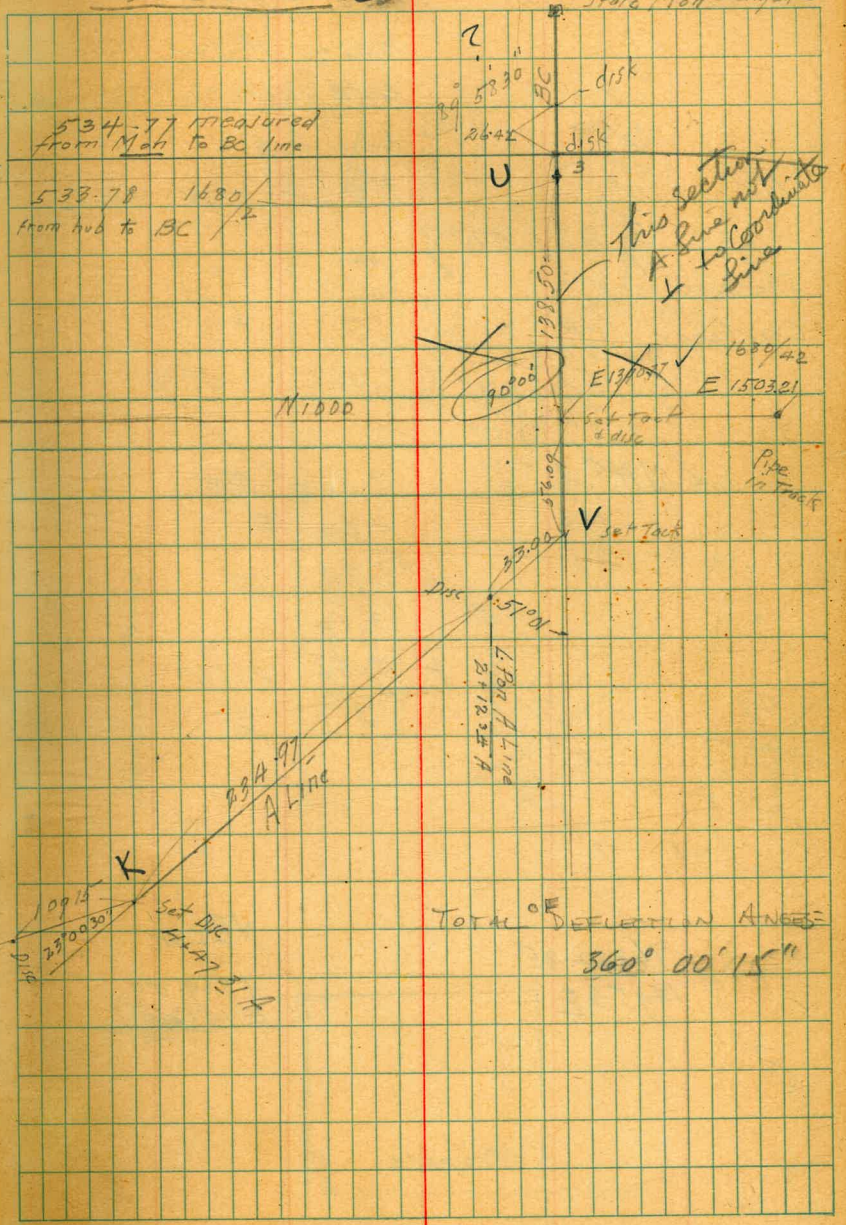
Mar 28 1950





RE SURVEY + SETTING
BASE LINES D

MARCH 22, 1950
MOORE SHERRILL
Begg
State Men Crawford



Locat 1071

Fire Hydrant
Water Meter
Gate Post
hose bib
MH A elev shelf

Moore

Begg 3/28/50

Sherman

Crowford

MH "A"	9.26	BM
	472	
	1398	HI
	13.12	
	0.86	shelf

2

2

8372 ±

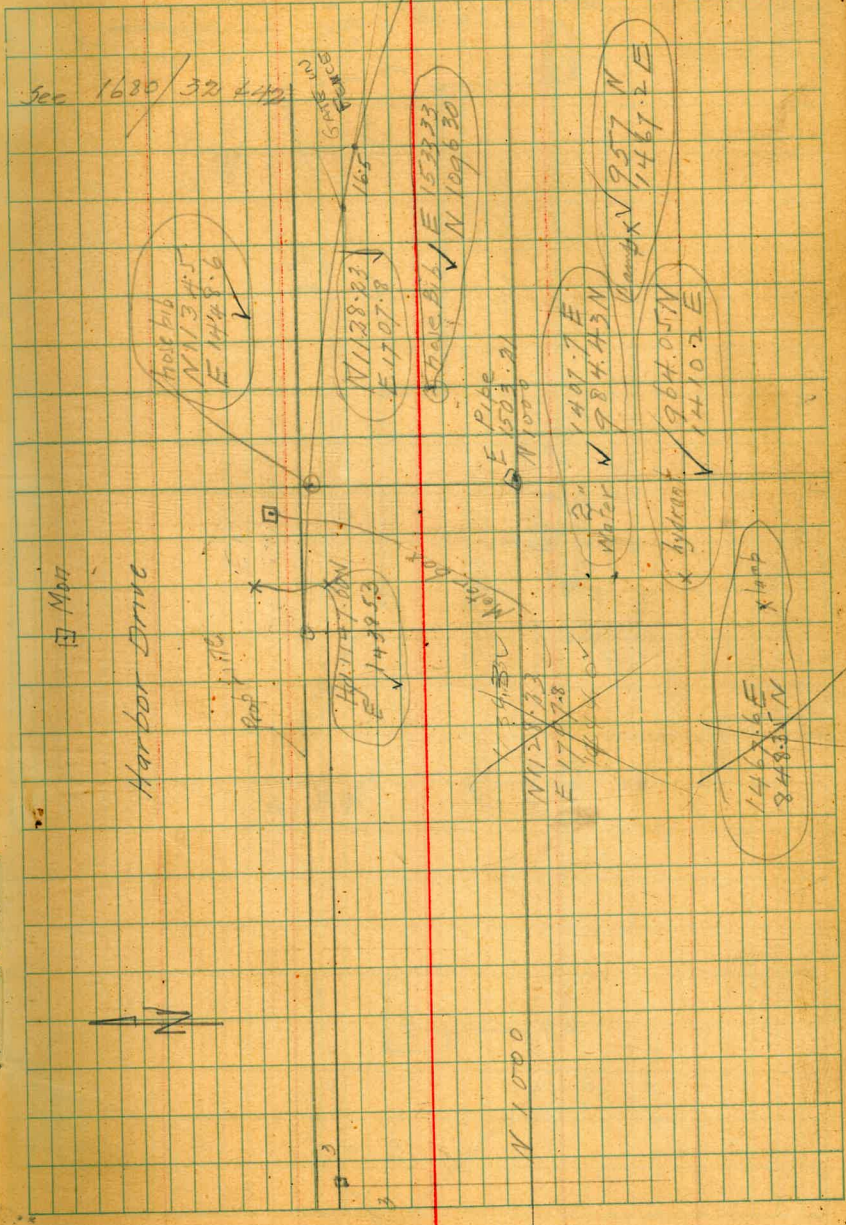
N 882.25
E 1495.8

NECOR ?

N 869.00
E 1512.0

8514 ±

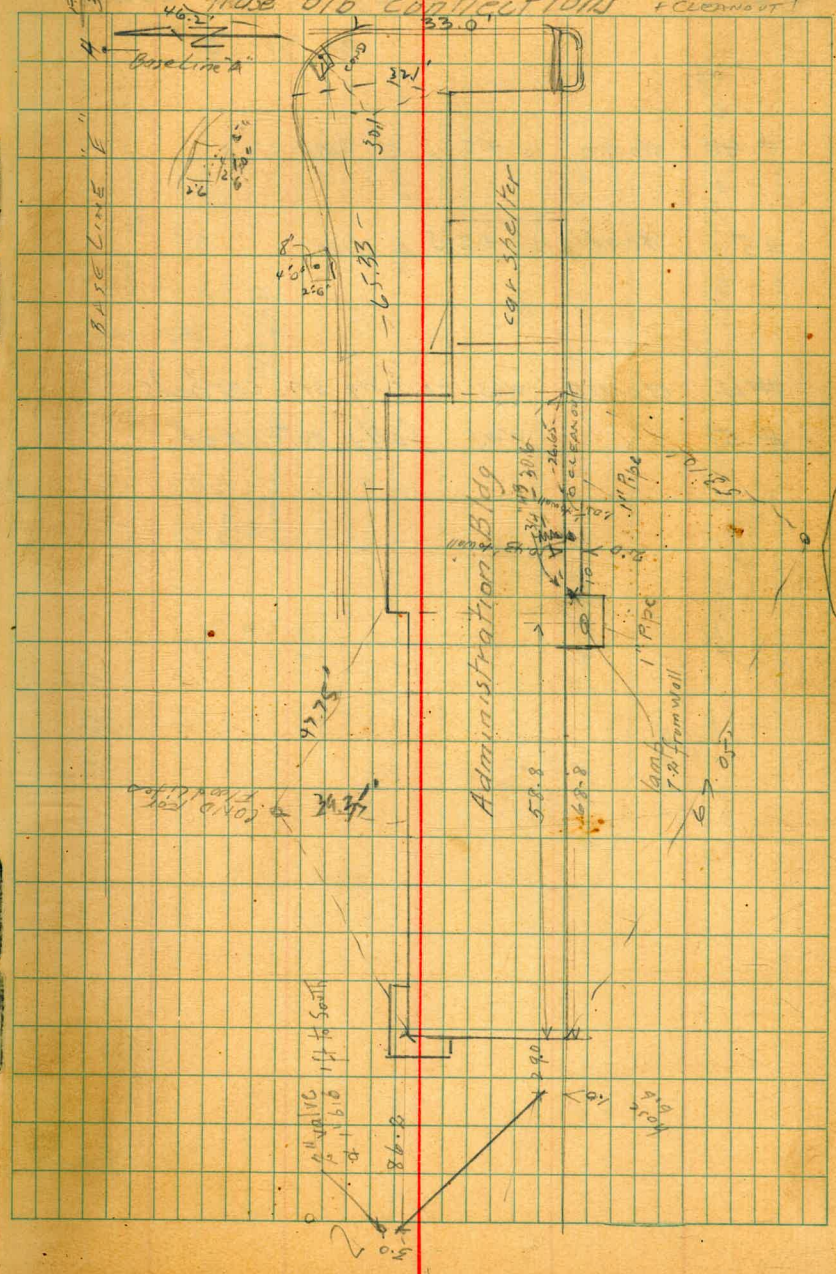
Propose



Plane
4 31.05

Base Line "D"
ADT. BLDG

Have bib connections 4



2
4" supply
off to South
86.10
29.0
1.8
2.8

1.8
2.8

50.8
24.65
1" Pipe
1/2" Pipe

Administration Bldg

car shelter

46.27
Baseline A

BASELINE E

#5+
 CHECK Location #4 Digester Dome
 3-31-50

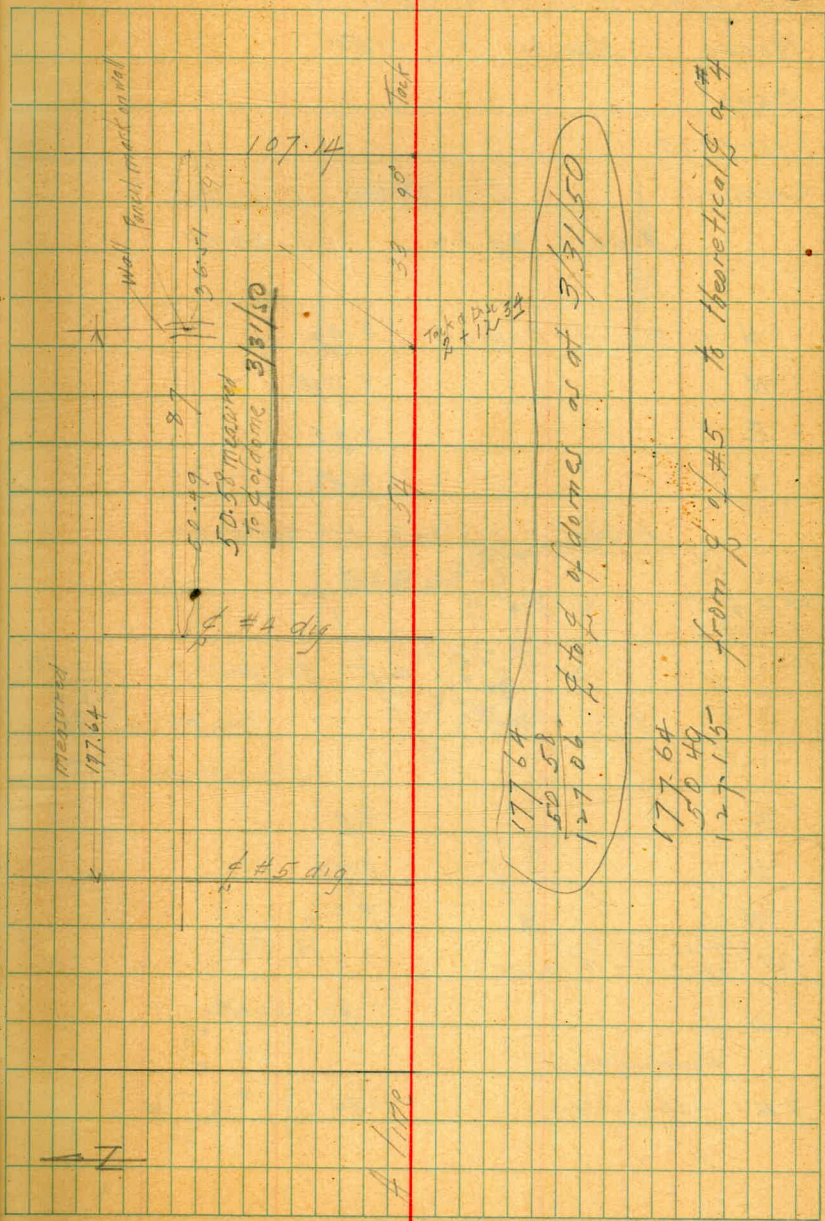
#4 dome 15.02 S of line

#5 dome 15.02 S of line

#4 dome was resting on corbels

#5 " was fully extended

5



Levels on Dig #4 + #5

Moore	Mar 31	1950	
Begg			
Sherman			
Crawford	Dig #4		
	3-62	39-62	26.00

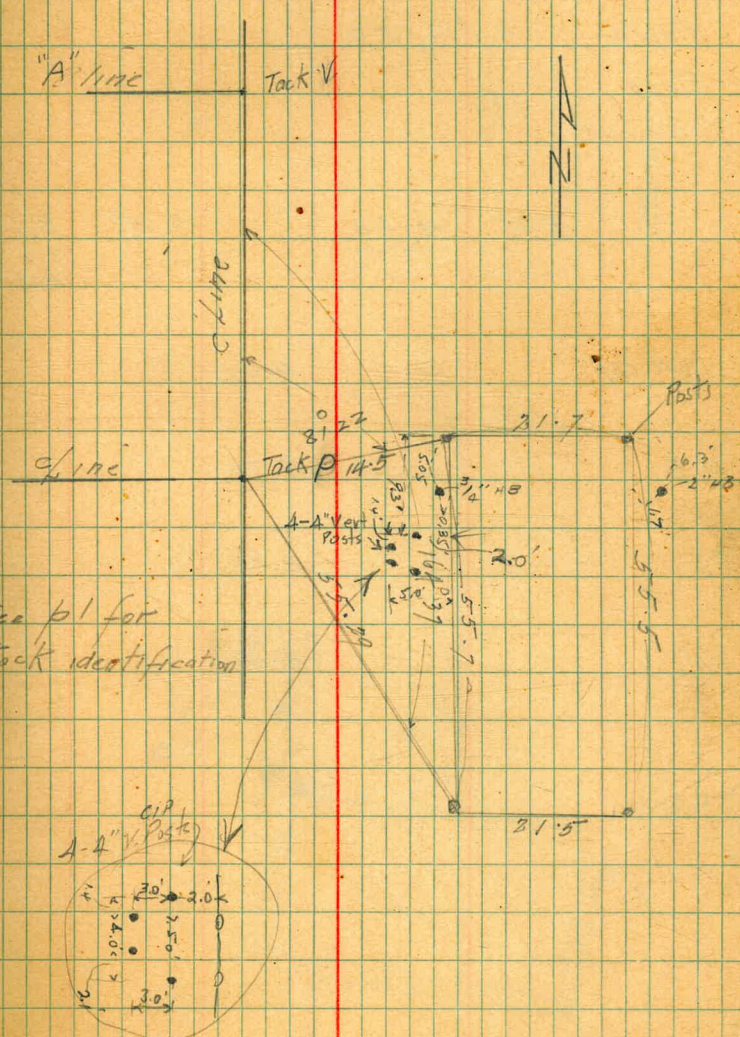
W on Rim of Dome	8.92
N	8.94
E	8.95
S	8.93

probably resting on corball

	Dig #5 gal pressure		3.50"
	8.71	34.71	26.00
			6.30

E	6.91	
N	6.92	
W	7.02	
SW approx opposite 8" pipe	7.03	7.03
S	6.91	
diametrically		
NE opposite	6.90	6.00

Location of Fence around Propane Tank



Location Conc Slab used
by Contractor for Pipe Shop

Moore 4/11/50

Begg
Crawford

5.15 14.40 9.25 Bolt
on
Gantry

N.W cor 4.67

N.E. 4.70

S.E. 4.68

S.W. 4.69

Location of slab

"A" Line

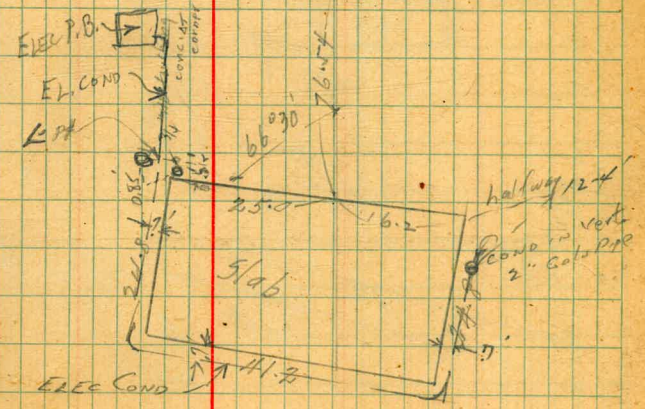
Track A



C Line

C Line

Track B



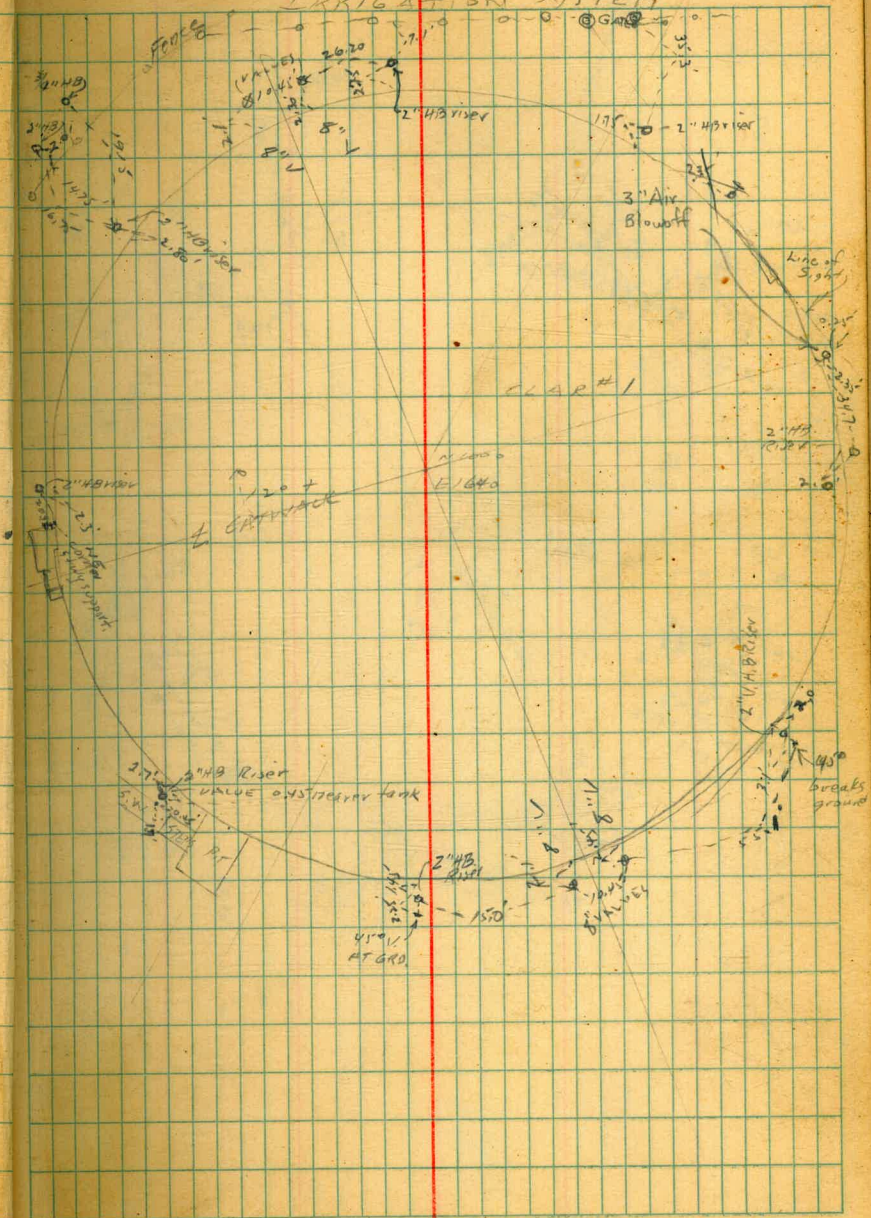
Brown

Sept 22, 1950

Hose Bib Risers CLAR #1

9

IRRIGATION SYSTEM

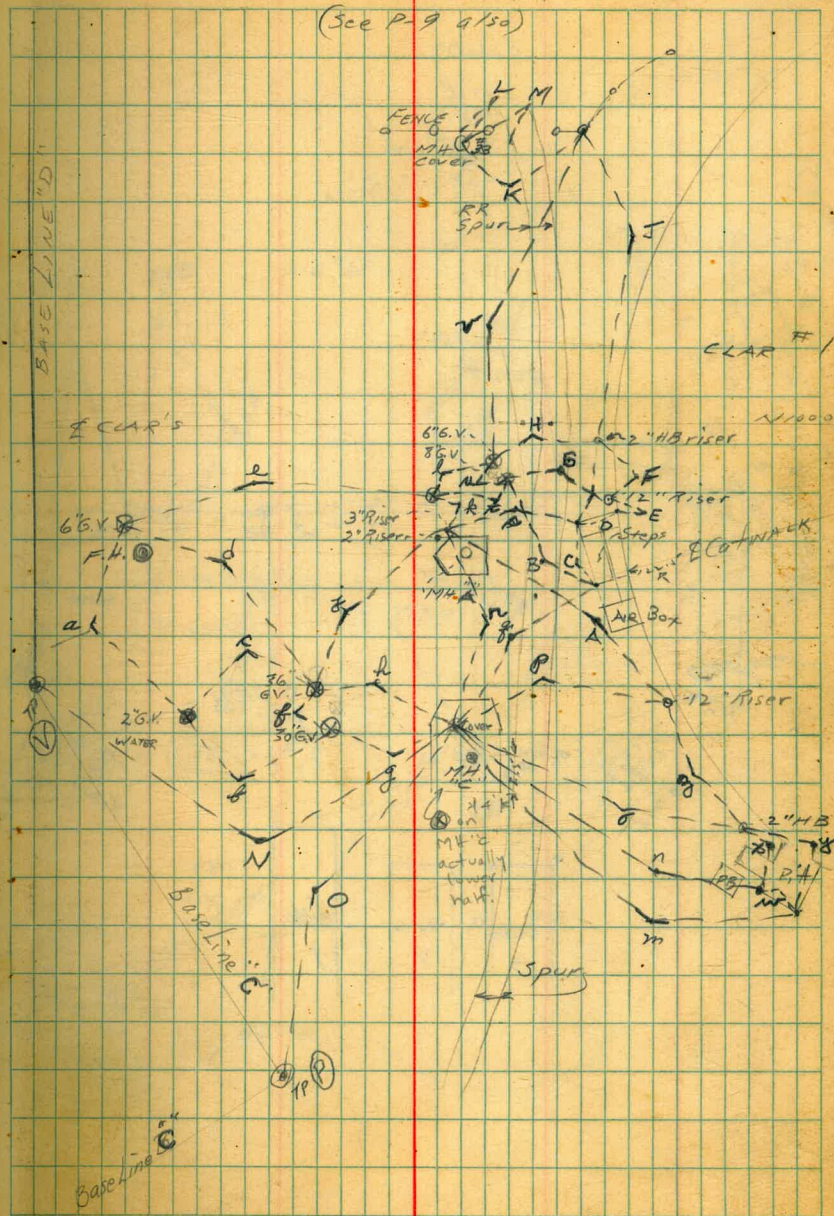


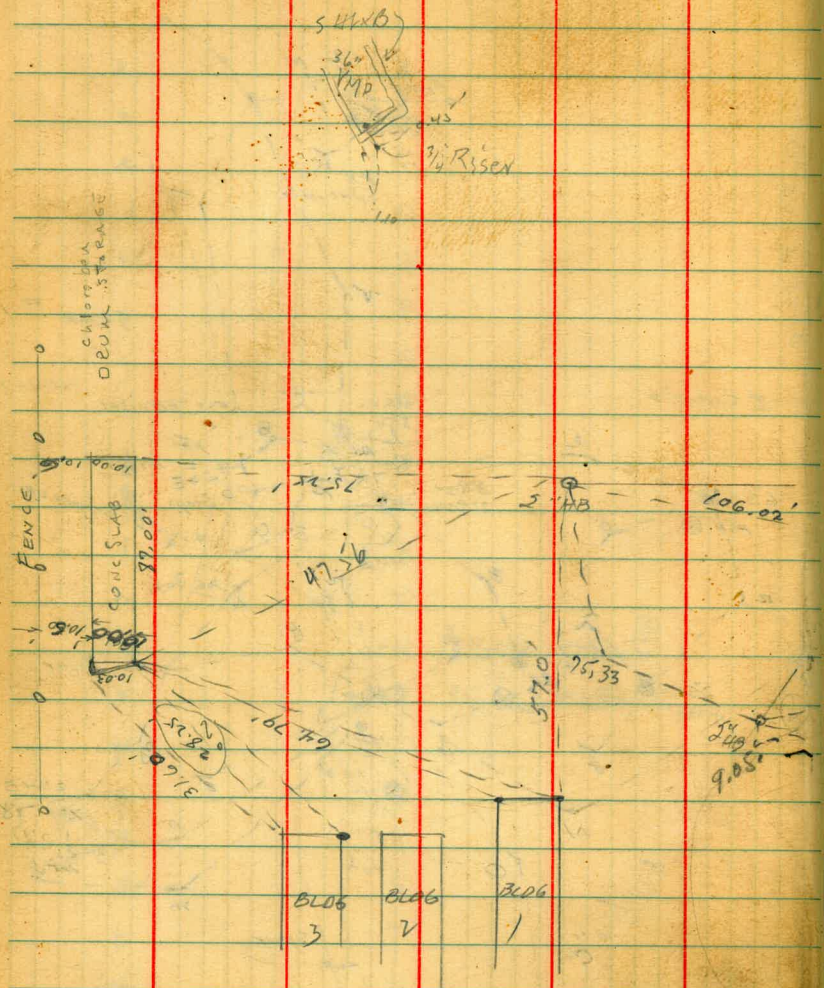
DISTANCES MEASURED

a	A	
b	B	
c	C	
d	D	
e	E	
f	F	
g	G	
h	H	
i	I	
j	J	
k	K	
l	L	
m	M	
n	N	100.00 TP (D) to "C"
o	O	95.00 TP (D) to "C"
p	P	
q	Q	
r	R	
s	S	
t	T	
u	U	
v	V	
w	W	
x	X	
y	Y	
z	Z	

Tape Distances to Valves etc.
 AREA WEST CLAR #1
 (See P. 9 also)

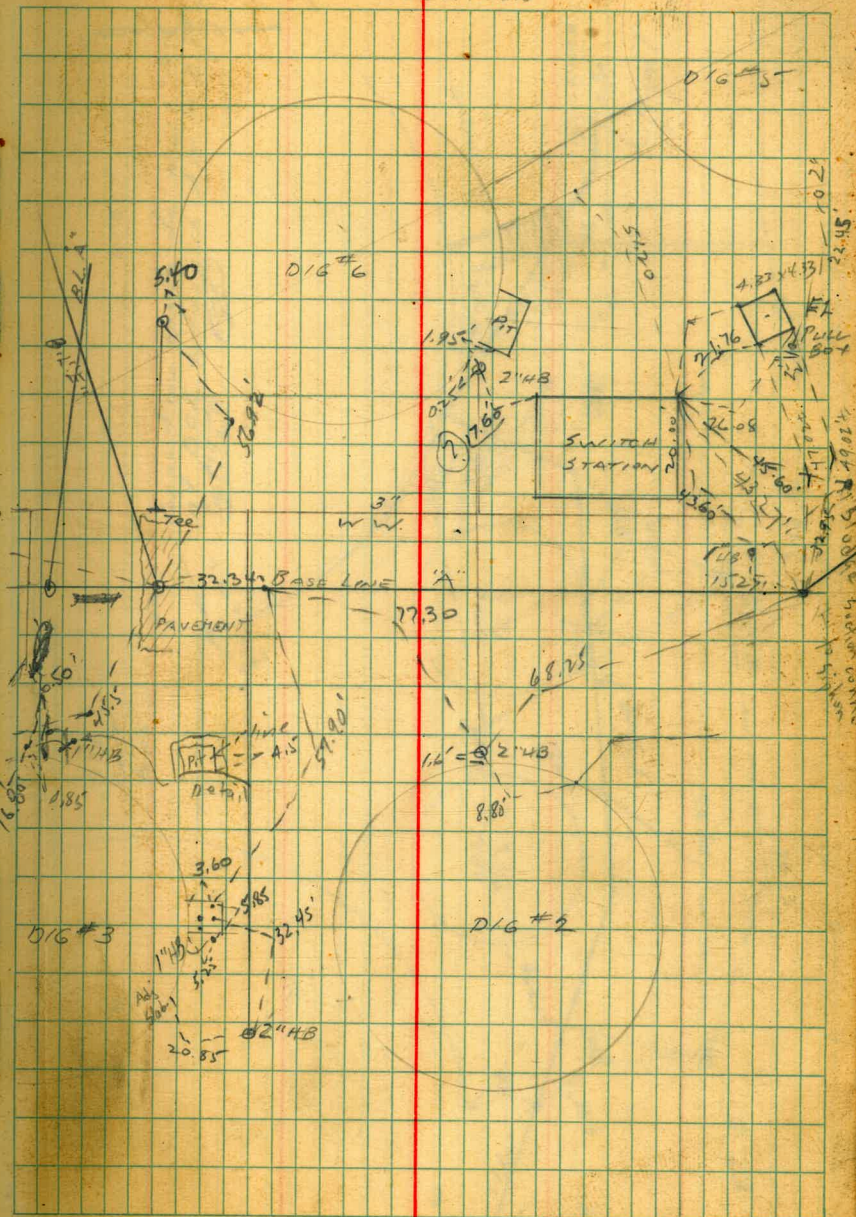
Brown
 Sept 28, 1950





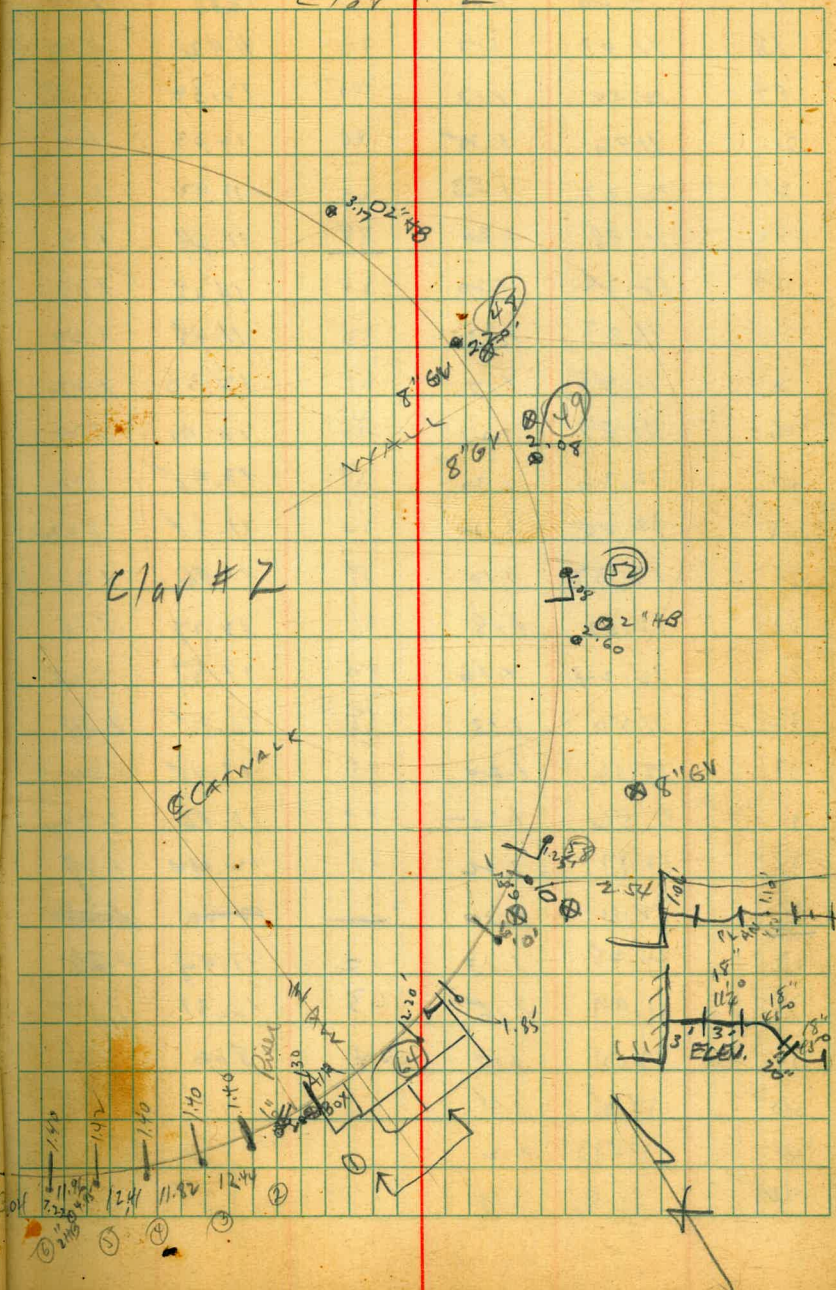
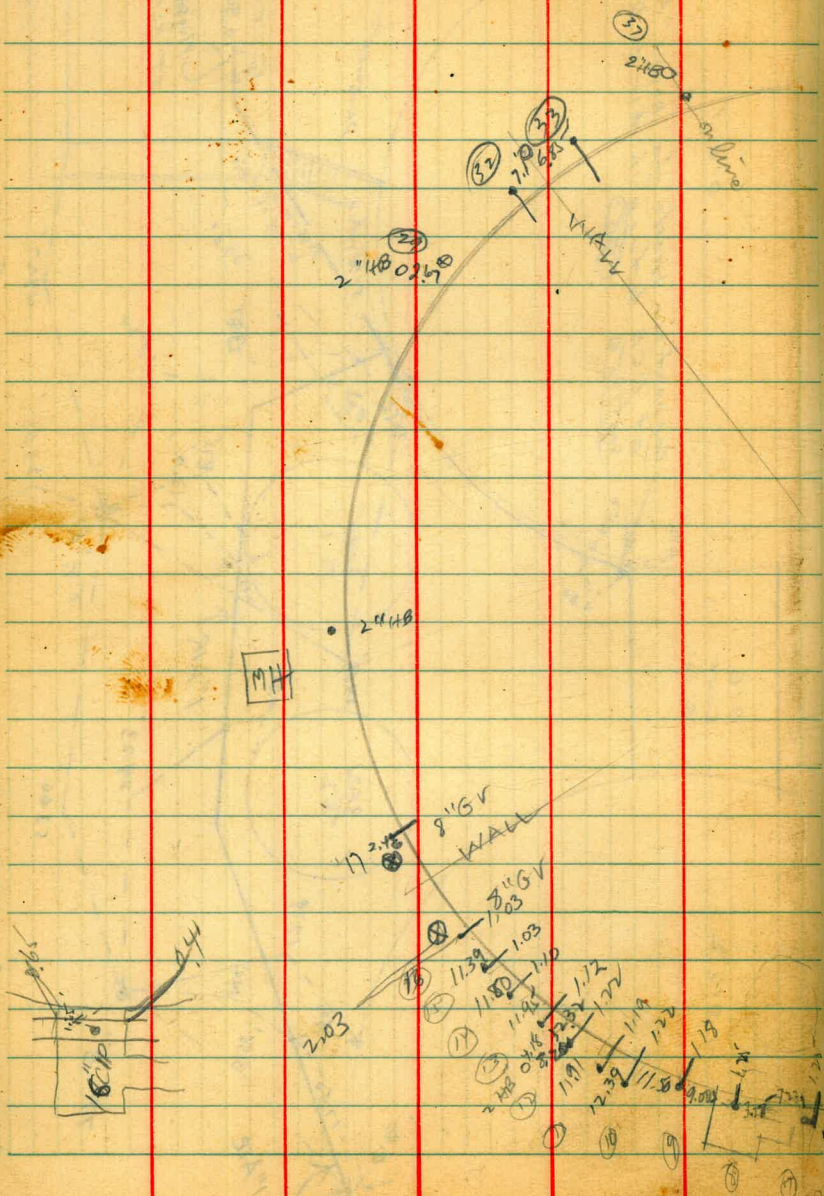
3" WASH WATER + H.B.'s
LOCATION

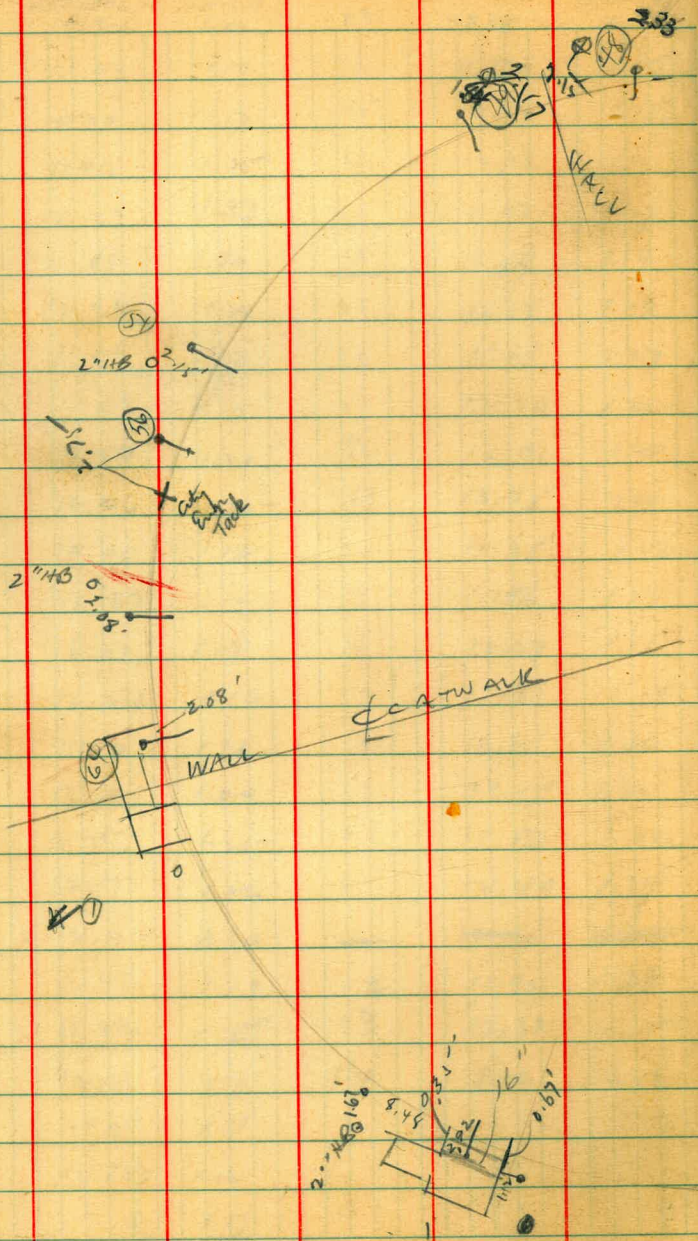
Brown 12
9-28-50



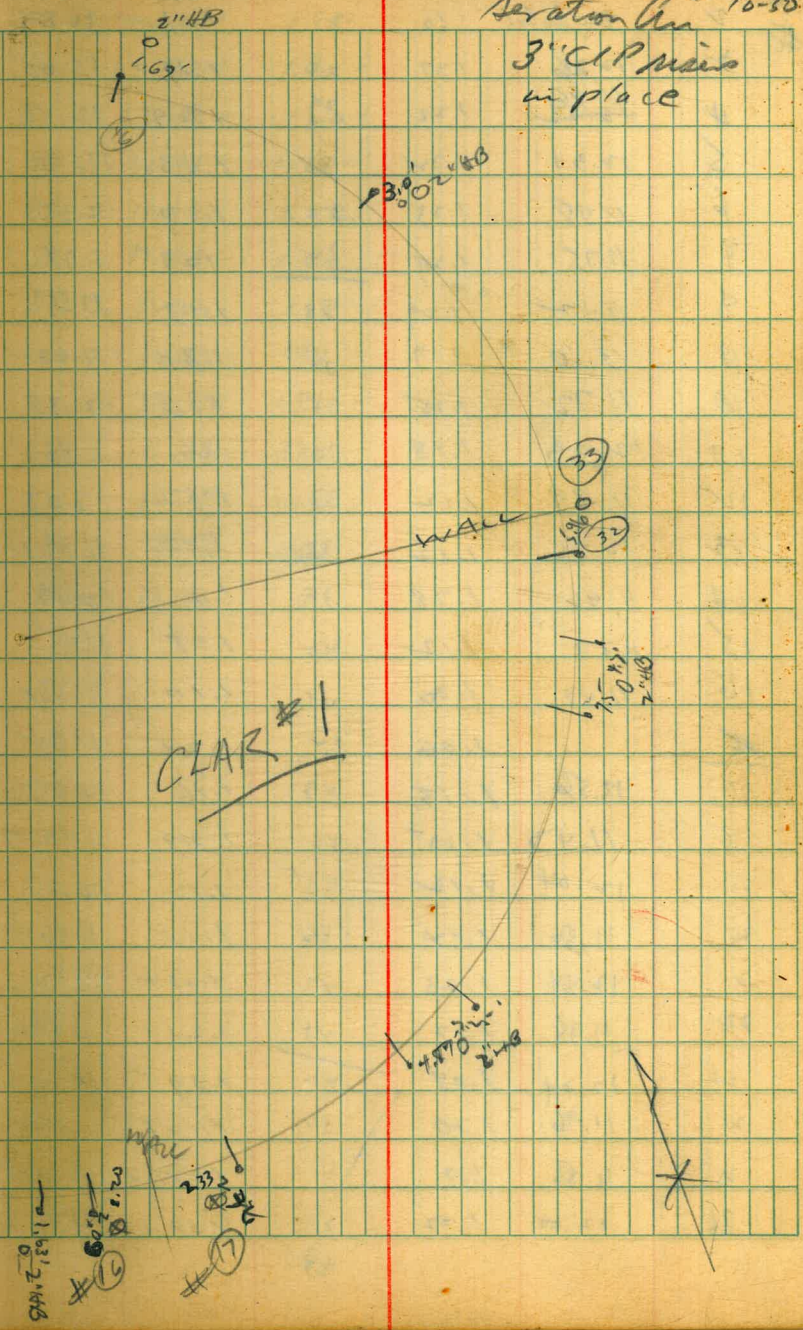
3" Risers Aeration Air
Clay # 2

14
10-31-50
C Brown





Location C48
 Section line 10-50
 3" CIP pipes
 in place

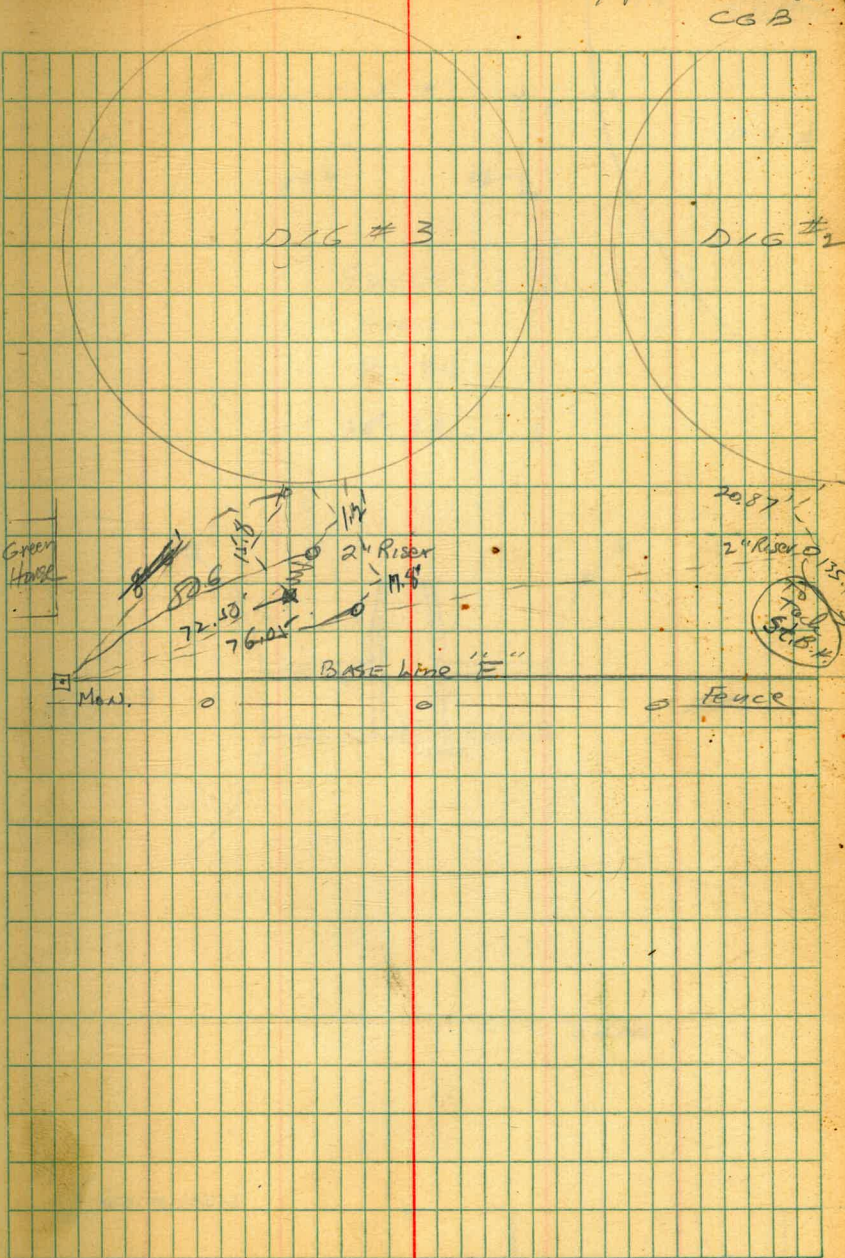


at An. Box #	DIST Fr. Proc #	DIST Fr TK		DIST Fr TK	DIST Fr Proc #
1					
2	920 lin box	1.60	27	1.24	12.23
3	12.26	1.37	28	1.29	12.05
4	11.96	1.22	29	1.29	12.17
5	12.31	1.32	30	1.23	11.99
6	11.98	1.23	31	1.17	12.35
7	11.75	1.29	32	1.17	11.74
8	11.42	1.29	33	1.17	13.35
9	13.50	1.19	34	1.30	11.62
10	11.72	1.25	35	1.10	12.31
11	12.23	1.18	36	1.30	11.86
12	11.99	1.12	37	1.15	12.43
13	12.26	1.12	38	1.25	11.89
14	11.96	1.28	39	1.11	12.43
15	11.77	1.12	40	1.28	11.95
16	11.49	1.20	41	1.10	11.73
16		1.06	42	1.21	11.94
17	13.50	1.18	43	1.16	12.34
18	11.43	1.25	44	1.29	11.99
19	12.04	1.12	45	1.12	12.23
20	11.80	1.14	46	1.15	11.96
21	12.44	1.23	47	1.17	12.12
22	11.98	1.17	48	1.21	11.79
23	12.24	1.08	49	1.09	11.04
24	11.96	1.20	50	1.16	11.59
25	11.86	1.17	51	1.05	12.26
26	12.00	1.22	52	1.34	11.96

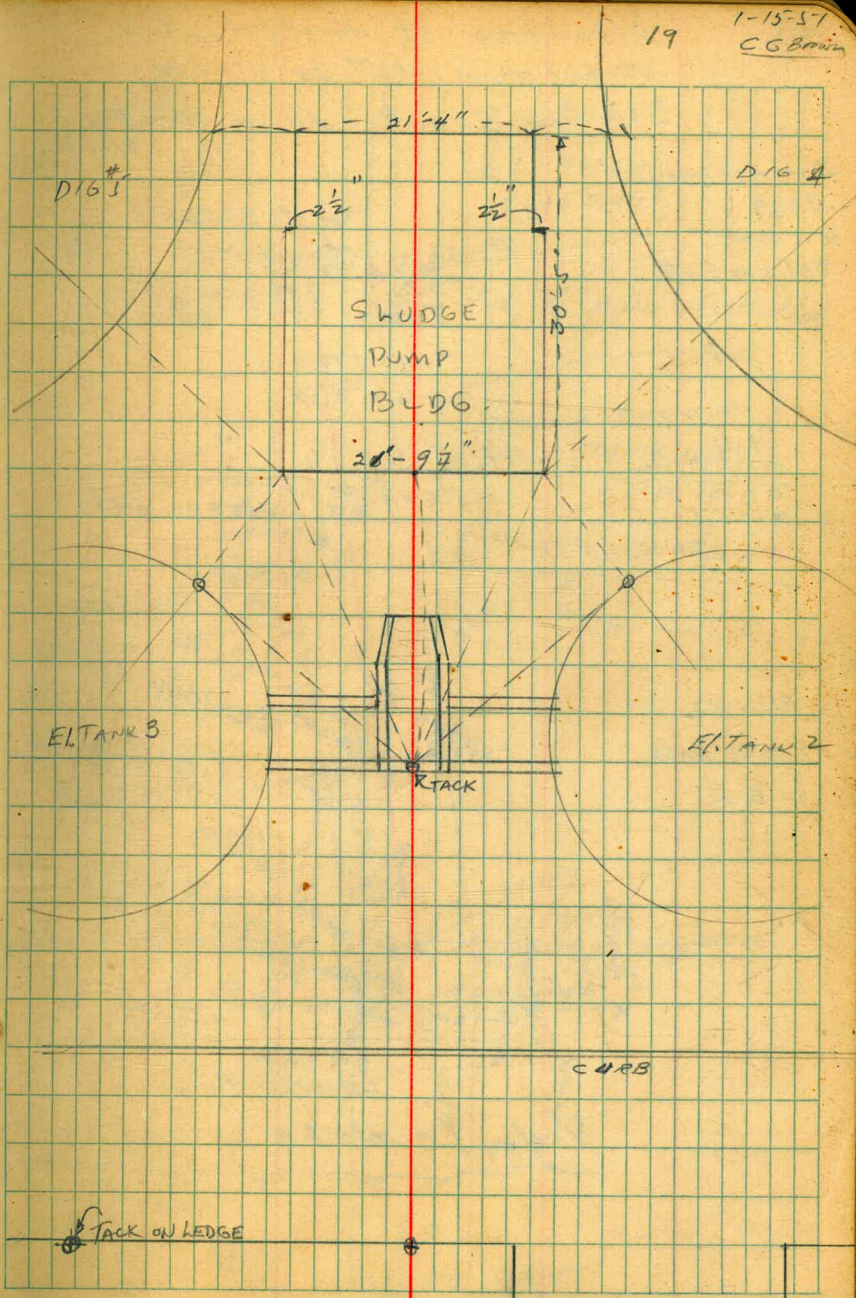
	DIST Fr Proc #	DIST Fr TK
53	12.27	1.18
54	12.03	1.46
55	12.18	1.20
56	11.91	1.34
57	11.93	1.22
58	11.94	1.42
59	12.23	1.28
60	12.00	1.34
61	12.32	1.31
62	11.93	1.24
63	12.33	1.22
64	8.78	1.30
6 Box	13.81	

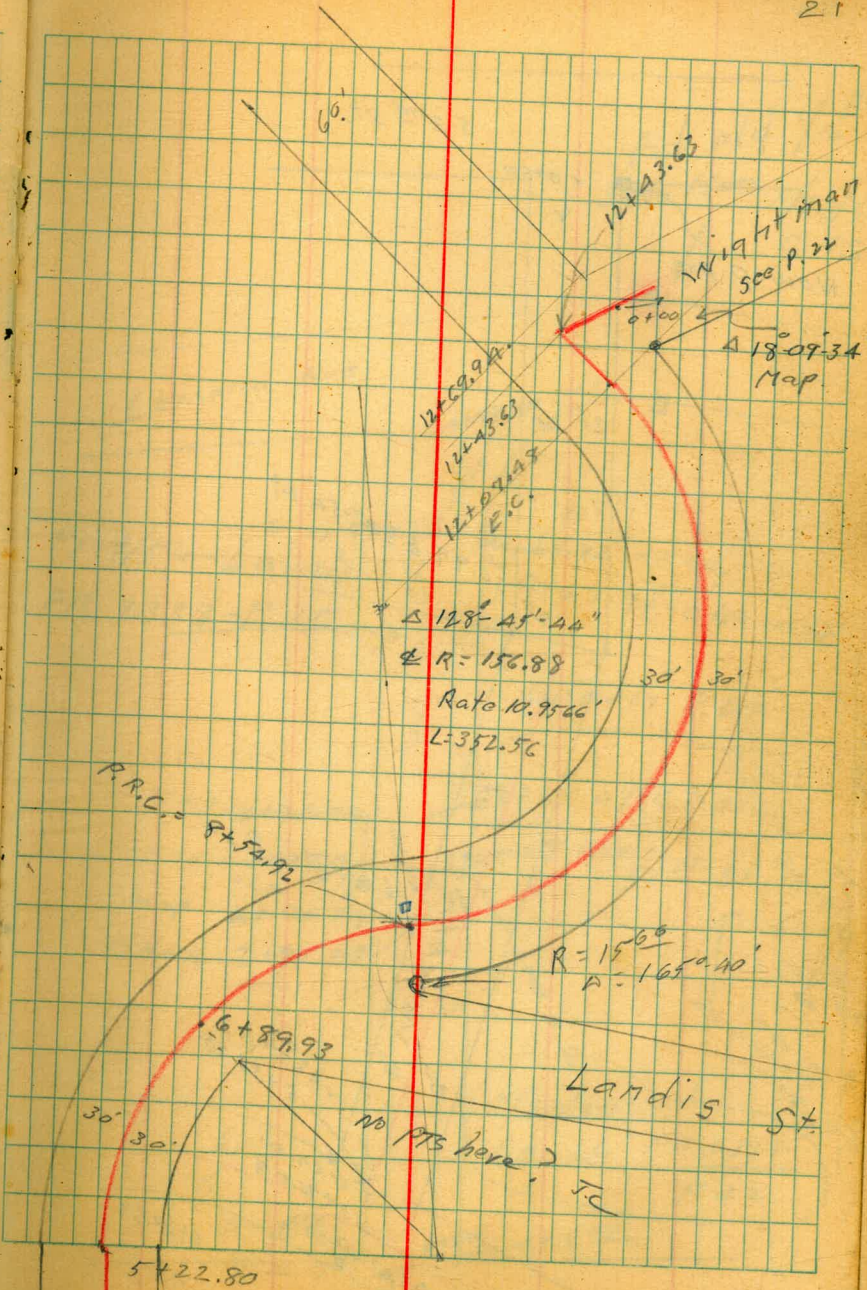
13.6 Connecting Valve
 4" Drain 30.5 NW D155
 43.7 Tack Sideralk

19 11-21-50
CGB

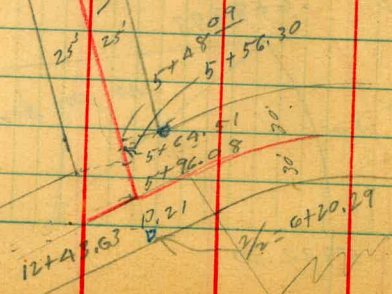
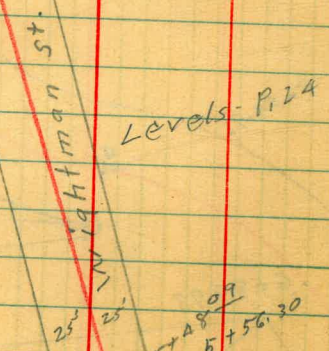
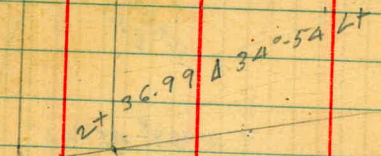
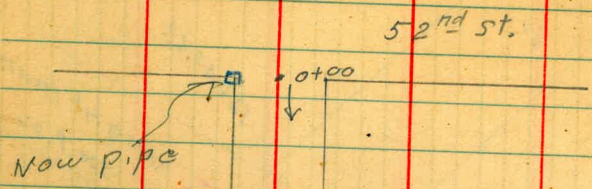


19 1-15-57
CG Brain

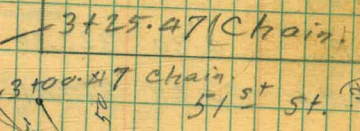
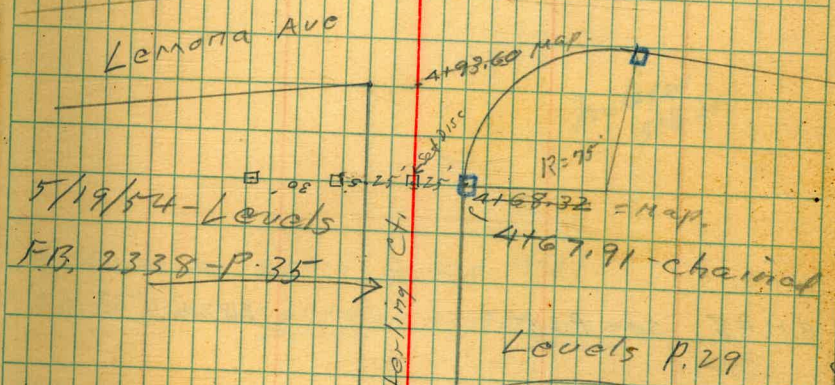




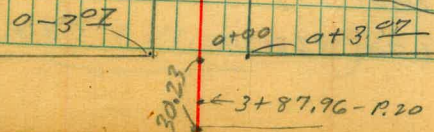
~~12+43.63~~
~~12+59.92~~
~~156.88~~
~~10.9566~~
~~352.56~~



Fd old 1/2
Set. Mon. 5/13/54
C.H.S.



5/20/54
Levels FB 2338
P.42



Benchies

			1	321.36	†
B.M.#8	see P.25			287.06	
B.M.#7		6.22		316.28	
T.P.	6.80	322.50	2.21	315.70	
B.M.#6	0.68	317.91	3.47	317.23	(Gone)
B.M.#5	7.67	320.70	10.27	311.03	
B.M.#4	1.53	321.30	1.80	319.77	✓
T.P.	1.71	321.57	5.85	319.86	
T.P.	0.45	325.71	10.48	325.26	
B.M.#3	8.62	335.74	12.13	327.12	
B.M.#2	8.14	339.25	6.47	331.11	
T.P.	10.03	337.58	0.72	327.55	
B.M.#1	12.70	328.27		315.57	

Top Nail

Indexed
5-8-52

(shows as 287.19 in F.B. ¹⁵⁶⁹)
S.E. $\frac{3}{4}$ " pipe Wightman & Altadena

$\frac{3}{4}$ " pipe N.W. Cor. Sterling Ct. (west) & 50th St.

Nail in pole # P3624 - Altadena & Sterling St. (west)
5' west of 51st St.
disk in wall 26' N. of Sterling Court (East)
Nail in pole # 36.88 Altadena & Landis

Nail in street sign post Lemona & Landis
 $1\frac{1}{2}$ " pipe S.E. Cor. Landis & 52nd
 $\frac{3}{4}$ " pipe N.W. Cor. Wightman & 52nd

N.W. B.P. 52nd & University

2+36.99 L-34°-54' Lt. (Sec on split.)

2+00

T.P. 1.03 321.52 12.28 320.49

1+50

1+00

0+86 - 33 ft. = end double bar.

conc. floor - no apron

0+67 - 32¹ ft. = start double bar.

0+66 - 25 ft. = end brick wall

0+50

conc. base

25' ft. = start brick wall 0+7

0+00 = wly line 52 (Page 24)

BM#2

1.66 332.77

331.11

P.23

317.5	315.62	322.0
4.0	5.90	+0.5
25	M.H.	205
	RITT	

322.5	317.8	320.4
+1.0	3.7	1.1
25		25
	321.52	

322.6	321.7	323.9
9.2	11.1	8.9
25		25

326.2	325.1	327.7
6.6	7.7	5.1
25		25

328.8	329.14
4.0	3.63
32	33
End	Floor

328.9	329.12
3.9	3.65
32	32
End	Floor

325.7	327.9
4.1	4.9
End	25 Base of wall

329.2	328.0
3.6	7.8
25	
	3.5
	25

331.9	330.3
9.9	2.5
25	25
	base of wall

332.77

Sterling Court
West of Altadena

1+00

0+90 Ely- 50th to north.

0+65 - E 50th to north

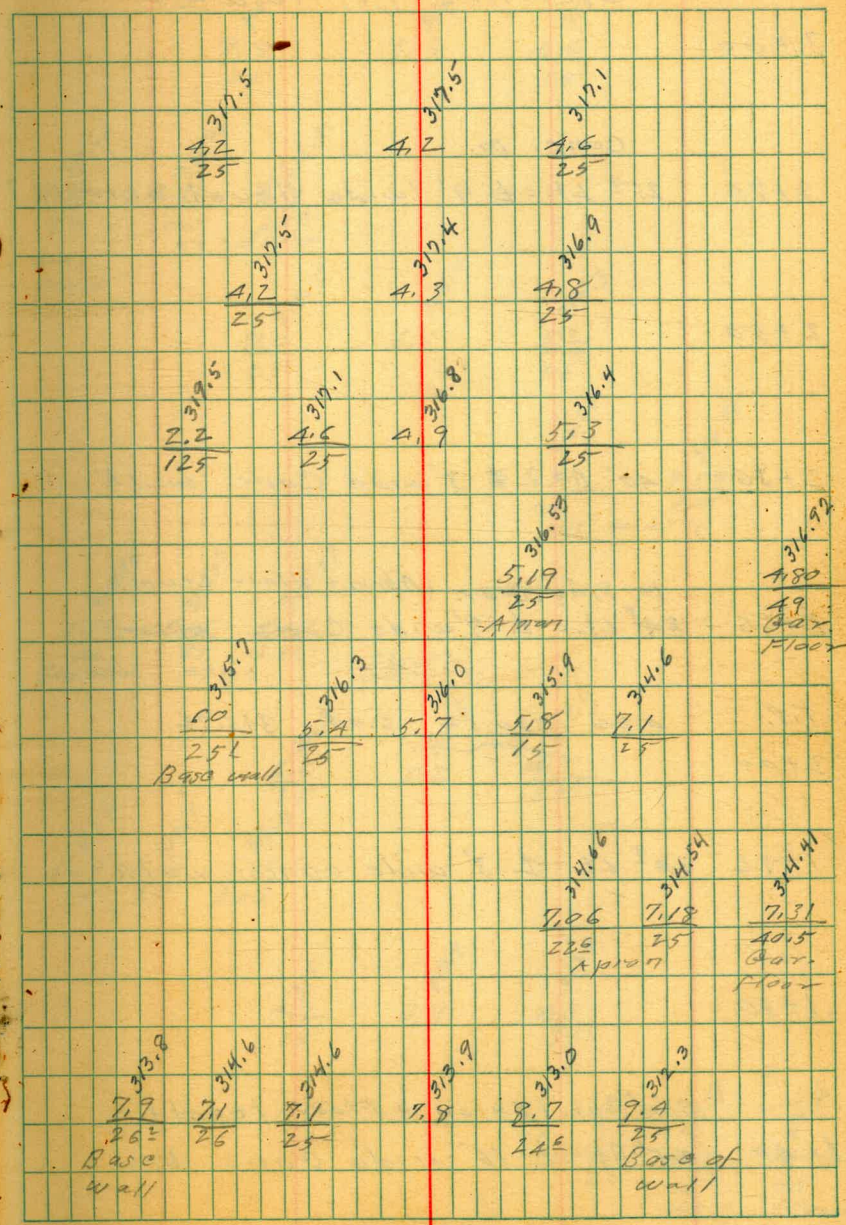
To garage. (Apron + Floor level)
0+58 25' Rt. - E 12' wide conc. drive

25th Lt. = end Conc. wall
0+40 Wly. 50th to Left.

to double Gar. (Floor + Apron Level)
0+39 22nd Rt. - E 14' wide conc. apron

26th Lt. = Face Conc. wall
24th Rt. = start Conc. wall
0+00 = Wly end Sterling court.

BM #7
R23 5.44 321.72 - 316.28



321.72

Stearling Ct. to west

3+00

Conc. Dr.

2+74 25th Lt. = ± 9' wide (level across)

2+50

2+36- 40' Rt. = ± 3' wide Conc. walk

to Sing. Car. (Apron + Floor level)

2+26 24th Lt. = ± 8' wide Conc. apron

T.P. 4.80 320.52 6.00 315.72

2+00

1+92 24th Lt. = ± 3' wide conc. walk

1+50

Sing. Car. (Apron + Floor level)

1+40 25th Rt. = ± 10' wide Conc. Dr.

	310.17	±	312.2	313.9
	9.8	8.3	6.6	
	25		25	
	310.62			
	9.90	8.77	8.21	
	87	50	25	
	Car. floor	drill		
		311.75	312.31	
		7.0	6.1	315.3
		25		52
				25
		313.5		
			314.4	
				316.1
				3.91
				40
				012 walk
				316.98
				3.57
				50
				Car. floor
				320.52
				316.5
				5.2
				4.7
				25
				317.0
				316.1
				5.6
				25
				316.7
				5.05
				24.8
				317.5
				4.2
				25
				317.8
				3.9
				317.4
				4.3
				25
				317.2
				4.5
				25
				317.57
				4.21
				25
				drill
				317.68
				4.04
				45
				Floor
				321.72

Sterling Ct.
west

check B.M. #6 - P 23

3.28

317.24

317.23

5+00 = wly. Altadena

4+50

4+28 25' Rt. = ± 3' wide walk

4+00

3+50

3+47 - 25' Rt. = ± 3' wide Conc. walk

37

28

313.7
6.8
25

314.9
5.6

316.3
4.2
25

311.0
9.5
25

312.2
8.6

313.8
6.7
25

314.22
7.30
25

313.78
6.74
25

34
07
walk

305.6
11.9
25

310.7
9.8

312.4
8.1
25

309.0
11.5
25

310.7
9.8

312.5
8.0
25

312.1
8.4
25

312.90
7.62
25

313.52
7.00
29
07
walk

320.52

Sterling Court
(East of Altadena)
Sketch p 22

Map distances used

1+00 25' Lt. = 3' wide Conc. walk

~~0+92 27' Rt. = 2' wide Conc. walk~~

0+83 25' Lt. = 10' wide Conc. drive

0+50

0+03⁰⁷ 25' Rt. = S. Ely. Altadena + Sterling

0+00 = Ely line Altadena

0-03⁰⁷ 25' Lt. = N.E. Altadena + Sterling

BM#5 10.07 321.10 - 311.03

P.23

29

$$\begin{array}{r} 318.10 \\ 3.00 \\ \hline 47 \\ \text{walk} \end{array}$$
$$\begin{array}{r} 319.80 \\ 3.30 \\ \hline 25 \\ \text{E} \end{array}$$
$$\begin{array}{r} 317.6 \\ 3.5 \\ \hline 25 \end{array}$$
$$\begin{array}{r} 317.2 \\ 3.9 \end{array}$$
$$\begin{array}{r} 317.1 \\ 4.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 317.8 \\ 27 \\ \hline \text{walk} \end{array}$$
$$\begin{array}{r} 3.6 \\ 27 \end{array}$$

$$\begin{array}{r} 319.4 \\ 1.7 \\ \hline 130 \\ \text{Gar.} \\ \text{Floor} \end{array}$$

$$\begin{array}{r} 317.89 \\ 3.21 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 317.5 \\ 3.6 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 319.0 \\ 4.1 \end{array}$$

$$\begin{array}{r} 316.8 \\ 4.3 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 317.0 \\ 4.1 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 316.3 \\ 4.8 \end{array}$$

$$\begin{array}{r} 315.9 \\ 5.2 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 316.9 \\ 4.2 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 316.3 \\ 4.8 \end{array}$$

$$\begin{array}{r} 316.9 \\ 4.2 \\ \hline 25 \end{array}$$

321.10

sterling court

T.P. 2.06 313.09 10.07 311.03

2+75th = wly 5th to south

2+50

(level across)

2+36 26³ Lt. = ± 10⁸ wide Conc. Dr.

2+00

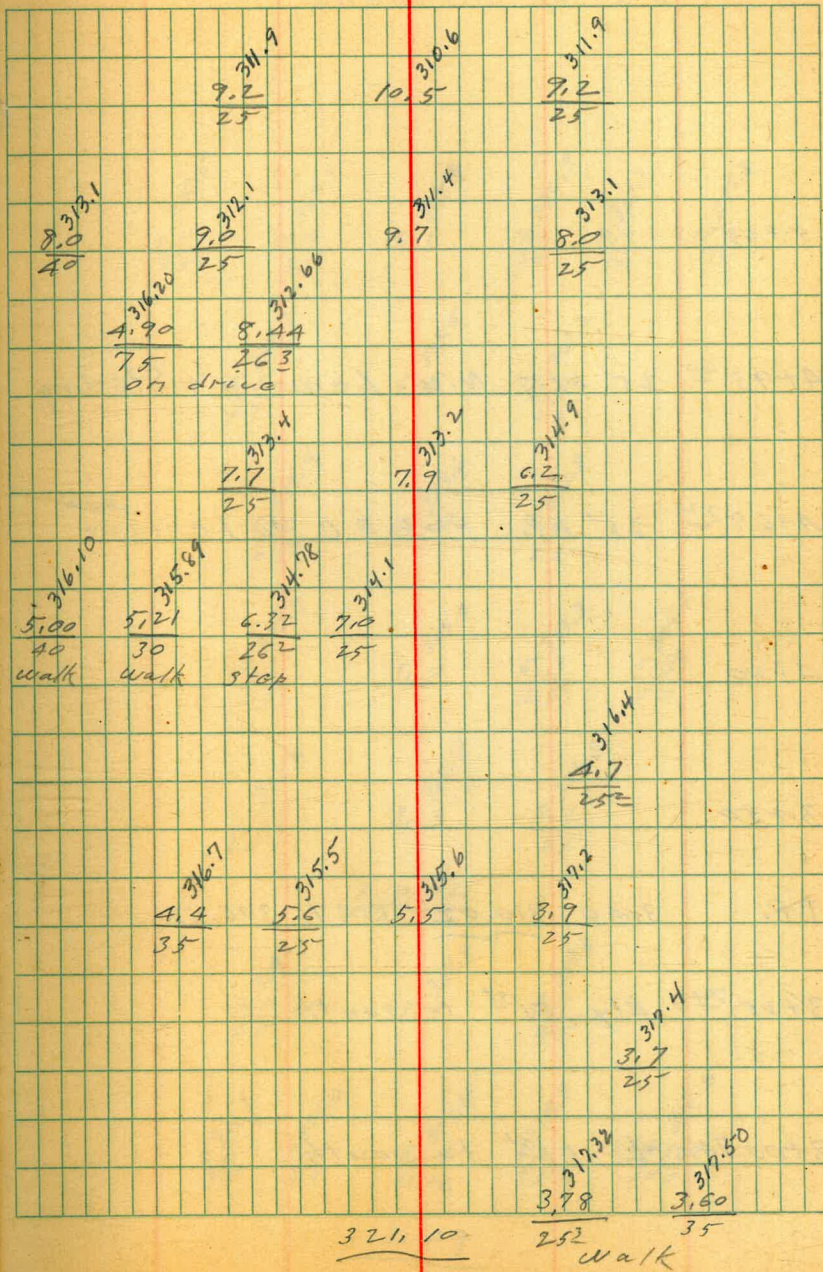
1+76 25³ Lt. = ± 3' walk.

1+58 25³ Rt. = ± sing Bar dirt floor

1+50

1+45 25³ Rt. = sing Bar dirt floor

1+30 25³ Rt. = ± 2' walk



Altadena

Sly line oak park Annex
to Wightman

1+49.74 £ sterling Ct. Produced

1+25t: sly. sterling Ct.

T.P. 4.46 321.69 4.48 317.23 = B.M.#6

T.P. 3.52 321.71 13.16 318.19

1+00

0+75 30' Mt. = £ 3' wide conc. walk

0+50

0+00 = sly line oak Park Annex

0-100

T.P. 9.21 331.35 1.00 322.14

B.M.#6 5.91 323.14 — 317.23

R23

$$\begin{array}{r} 314.9 \\ 6.8 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 316.0 \\ 4.9 \\ \hline 011.14 \end{array}$$

$$\begin{array}{r} 319.5 \\ 2.2 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 316.3 \\ 5.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 317.7 \\ 4.0 \\ \hline 321.69 \end{array}$$

$$\begin{array}{r} 320.3 \\ 1.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 318.8 \\ 12.6 \\ \hline 30 \end{array}$$

$$12.6$$

$$\begin{array}{r} 320.8 \\ 10.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 321.91 \\ 9.44 \\ \hline 30 \end{array}$$

$$8.80$$

$$\begin{array}{r} 322.55 \\ 4.80 \\ \hline 40 \end{array}$$

on walk

$$\begin{array}{r} 321.11 \\ 10.3 \\ \hline 30 \end{array}$$

$$9.9$$

$$\begin{array}{r} 322.9 \\ 8.31 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 326.6 \\ 4.8 \\ \hline 30 \end{array}$$

$$5.5$$

$$\begin{array}{r} 326.9 \\ 4.7 \\ \hline 30 \end{array}$$

$$3.0$$

$$\begin{array}{r} 326.4 \\ 3.0 \\ \hline 331.35 \end{array}$$

Altadena

~~6+32~~ - 34' Lt. = \pm 1' wide ribbons
 should be 6+28

6+00 32' Lt. = \pm 4' wide Conc. walk.

5+50

Radial sections from here on

29' Lt. = \pm 3' wide Conc. walk

5+22⁸⁰ = B.C. Rt.

5+00

4+95 25' Rt. = \pm 2' wide Conc. walk.

4+50

4+13.18 Nly sterling ct. produced

	$\frac{4.53}{65}$ Mean of Ribbons	$\frac{3.88}{34}$			
	$\frac{4.35}{40}$ walk	$\frac{4.33}{329}$	$\frac{4.4}{30}$	$\frac{4.3}{318.5}$	$\frac{3.7}{30}$ $\frac{3.19.1}{30}$
		$\frac{6.0}{30}$	$\frac{4.8}{318.0}$		$\frac{4.1}{30}$ $\frac{3.18.7}{30}$
		$\frac{5.99}{30}$	$\frac{6.00}{291}$	$\frac{5.2}{29}$	$\frac{5.1}{317.7}$
			$\frac{5.3}{30}$	$\frac{5.3}{317.5}$	$\frac{4.9}{30}$ $\frac{3.17.9}{30}$
	$\frac{4.38}{40}$	$\frac{4.70}{30}$	$\frac{4.79}{255}$		$\frac{4.6}{30}$ $\frac{3.18.2}{30}$
			$\frac{6.0}{30}$	$\frac{6.0}{316.8}$	$\frac{5.3}{30}$ $\frac{3.17.3}{30}$
		$\frac{7.8}{3023}$	$\frac{6.5}{3023}$	$\frac{6.5}{316.3}$	$\frac{5.8}{3023}$ $\frac{3.17.0}{3023}$

322.82

Altadena

9+50

9+00

T.P. 1188 312.92 12.20 311.04

= P.R.C. on $\frac{1}{2}$
 8+54.92 30' At. = Prop. P.C.C. = $\frac{1}{2}$

8+00

7+50

7+00

6+89.23 30' R.A. = S.E. Landis + Altadena

T.P. 3.45 323.24 3.03 319.79

6+50

4

35

$\frac{7.0}{30}$	5.6	$\frac{4.2}{16}$	$\frac{0.5}{30}$	$\frac{0.2}{40}$
$\frac{2.5}{30}$	2.9	$\frac{2.6}{14}$	$\frac{10.8}{30}$	$\frac{1.0}{40}$
	<u>312.92</u>			
$\frac{9.9}{30}$	10.8	$\frac{8.99}{30}$	Hub + End	
$\frac{5.3}{30}$	7.1	$\frac{7.0}{30}$		
$\frac{3.5}{30}$	4.7	$\frac{5.0}{30}$		
$\frac{3.4}{30}$	4.8	$\frac{4.2}{30}$		
$\frac{3.3}{30}$	4.4	$\frac{4.3}{30}$		
	<u>323.24</u>			
$\frac{3.4}{30}$	8.8	$\frac{3.3}{30}$		
	<u>322.82</u>			

Altadena

#

3C

check BM #8 7.38 287.07
 3/4" pipe - P25

12+69⁷⁴ 30' RT. = Nly Wightman

12+43⁶³ = Wightman produced

12+07⁴⁵ 30' RT. = 3/4" pipe = sly Wightman
 T.P. 5.92 294.45 12.32 288.53

11+50

11+00

10+50

T.P. 0.81 300.85 12.88 300.04

10+00

(387.06) - P-25

$\frac{294.2}{40}$	$\frac{291.8}{30}$	$\frac{284.4}{12}$	$\frac{283.9}{10.5}$	$\frac{8.2}{30}$	$\frac{8.2}{30}$	$\frac{286.2}{30}$
$\frac{294.4}{40}$	$\frac{292.0}{30}$	$\frac{295.0}{13}$	$\frac{294.7}{9.7}$	$\frac{7.1}{30}$	$\frac{7.1}{30}$	$\frac{287.3}{30}$
	$\frac{289.6}{30}$	$\frac{290.7}{30}$	$\frac{289.6}{11.2}$	$\frac{8.2}{18}$	$\frac{7.38}{30}$	$\frac{287.07}{30}$
	$\frac{293.1}{30}$	$\frac{297.5}{30}$	$\frac{292.7}{8.1}$	$\frac{6.0}{30}$	$\frac{294.8}{30}$	$\frac{297.9}{10}$
	$\frac{295.8}{30}$	$\frac{297.1}{30}$	$\frac{297.5}{3.3}$	$\frac{3.7}{30}$	$\frac{297.1}{30}$	
	$\frac{301.9}{11.0}$	$\frac{302.8}{10.1}$	$\frac{304.16}{8.3}$	$\frac{307.6}{5.3}$	$\frac{307.9}{5.0}$	
	<u>30</u>	<u>30</u>	<u>18</u>	<u>30</u>	<u>40</u>	
		<u>312.92</u>				

Robert
Cota
Moore
Patten
Aug 1, 1951
WB. 2000

Location of Existing Culvert
Across Lots 1 & 2 BK 57 HM Higgins

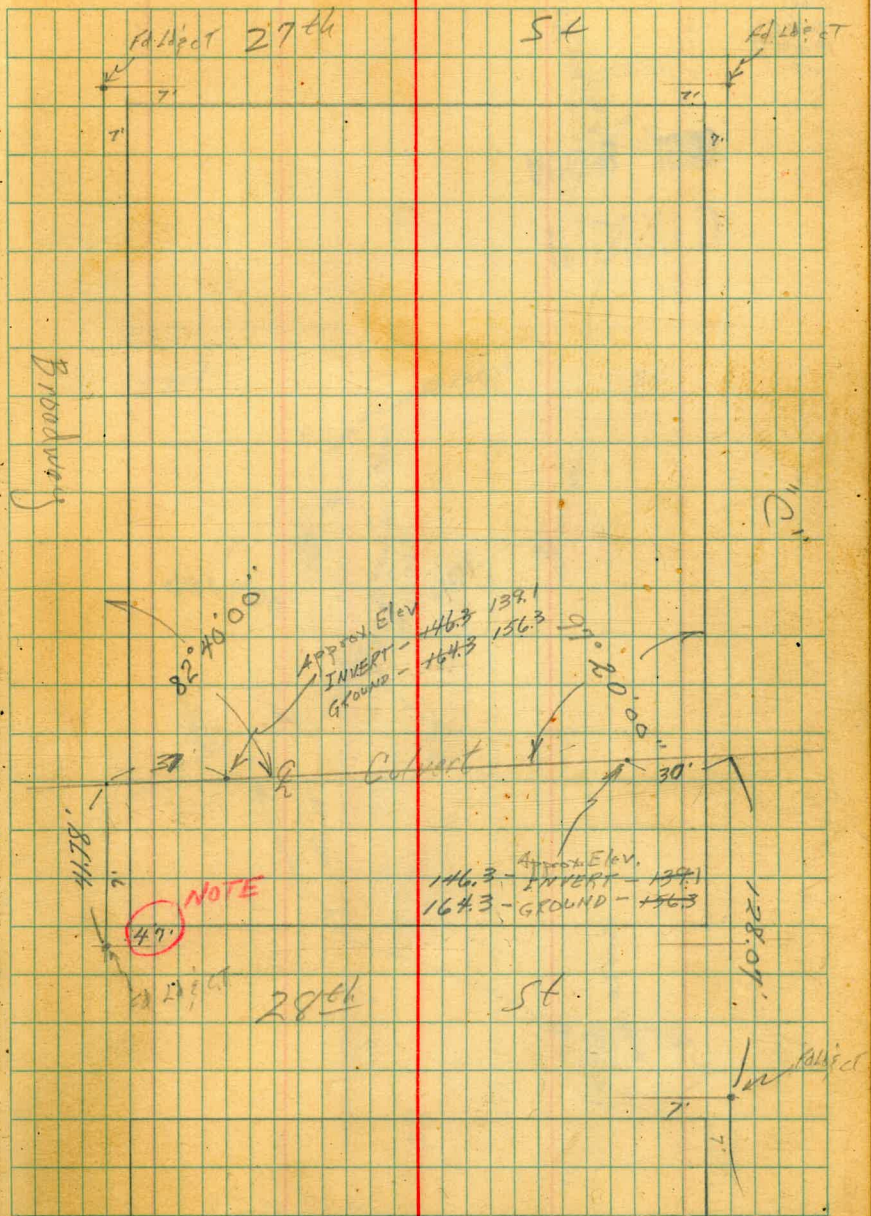
INDEXED

AUG 2 1951

BM

17665

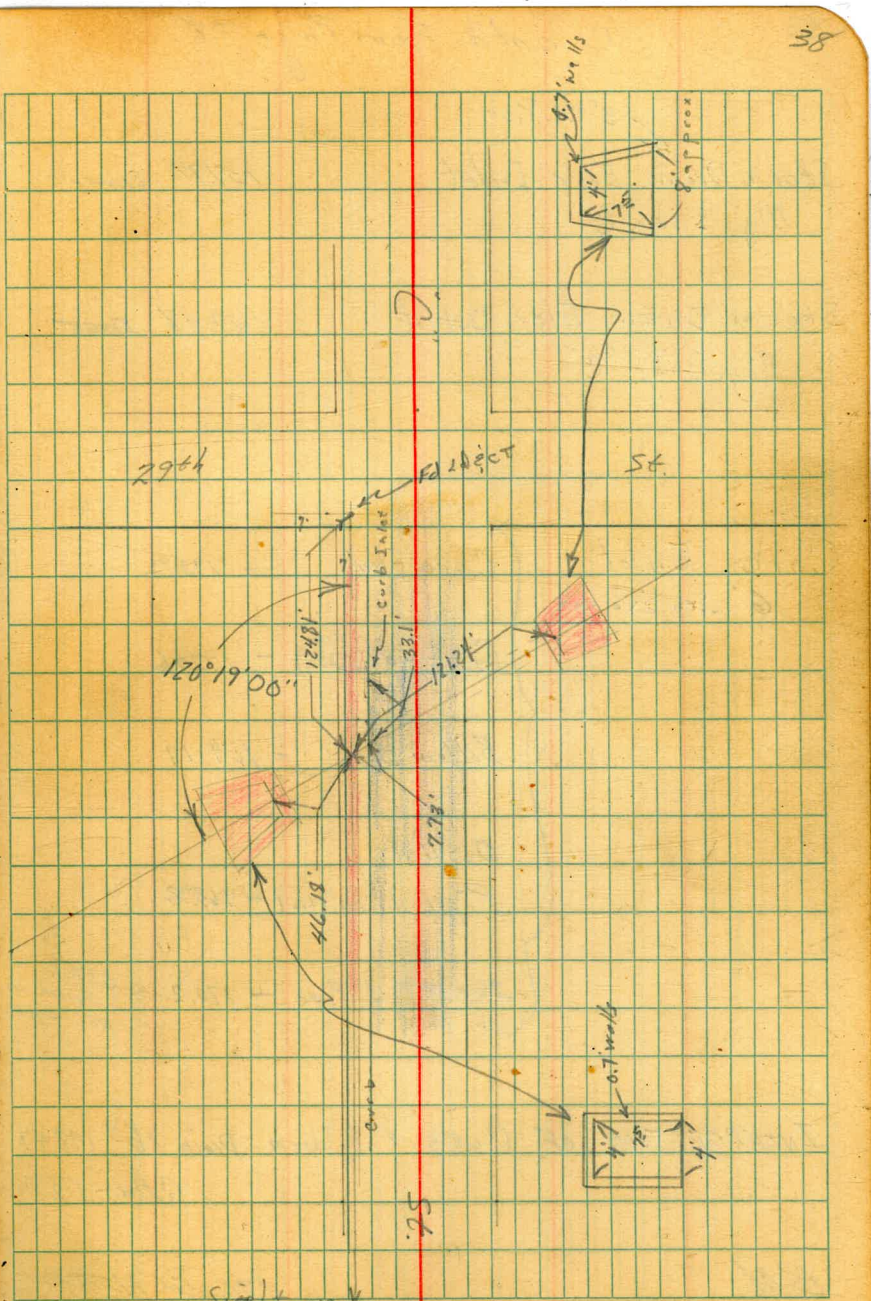
NEBP
285C



Roberts
Lala
Seoro
Fuller
Aug 8, 1951
wrb

Survey of Storm Drain 29th St

INDEX D
AUG 8 1951



C ont'd From Page 38

3' R.C. Pipe

Storm Drain Elev. Inlet 151.98 INVERT
Nly Side "C"

Storm Drain Elev. Outlet 149.48 INVERT
Sly. Side "C"

Curb Inlet { Curb Elev. - 172.72
6' with 2x2 box

Gutter (Top GRATE) - 172.06

Bottom Box - 169.11

Outlet of
Pipe 1" Cor. Steel - 163.93

INVERT 1" Pipe - 170.2 ← GRATE
at Box Tapped in.
ONLY APPROX.

INTERSECTION OF CURB & Storm Drain cb - 173.47
Gutter - 173.17

BM 176.05 NFBP

39

284 5' 0"

Locust St. 8/16/51
X-sec. Pot grade Est. W.P. 25020

Sommermeier
E. Begg
R. Sissen
C. Ford

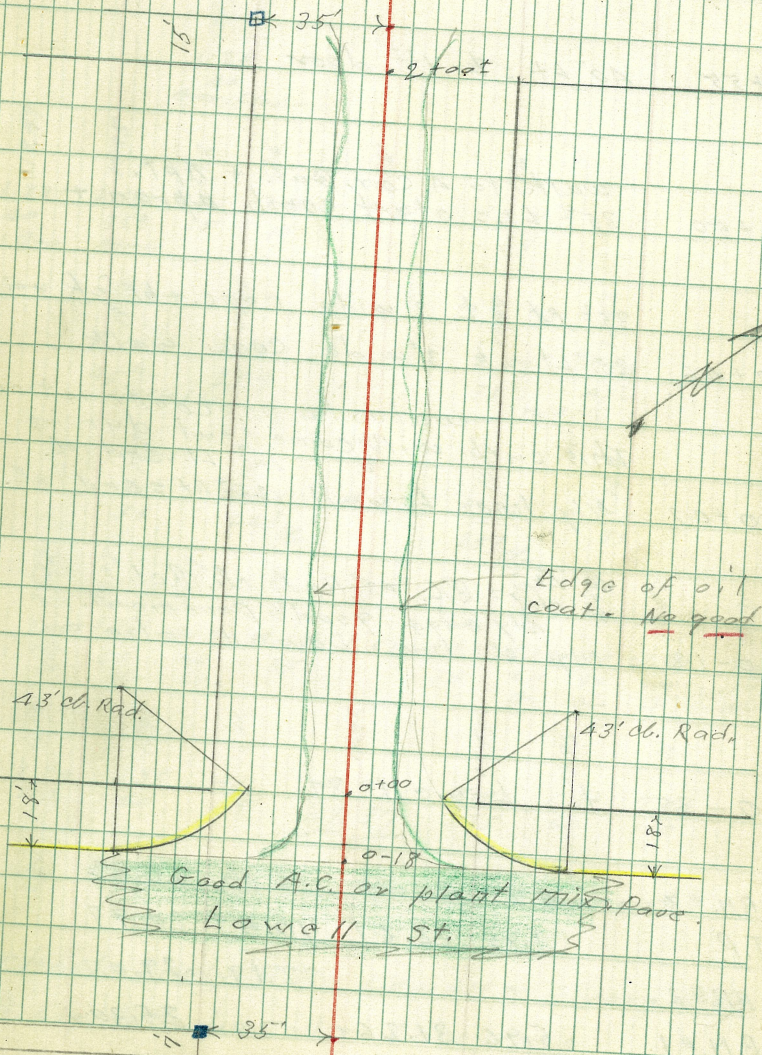
T.P. sheet 702
703

■ = Fd. Man.
□ = Fd. Hub

INDEXED

AUG 20 1951

Macaulay St.



1+24 33^E Rt. = end conc. apron.

1+15 35' Rt. = \pm double Car.
33^E Rt. = edge apron

1+07 37^S Lt. = \pm Sing. Car. CONC. Floor
33^E Rt. = start apron to double
no Apron
Gar. conc. Floor

T.P. 5.21 23.11 3.47 17.90

1+00

0+90 43.2 Rt. = \pm Single Car. no apron
35⁴ Lt. = end comb apron + walk

0+85 40' Lt. = \pm 4th Car. door

0+76 40' Lt. = \pm 3rd Car. door

to upstairs Apt.

0+70 38' Lt. = \pm 3rd wide conc. steps

				17.87		
				5.27		5.11
				33 ^E		35
				Apron.		Car. floor
				17.78		17.97
				5.33		5.14
				33 ^E		35
				Apron		Car. floor
				17.80		17.99
				5.31		5.12
				33 ^E		35
				Apron.		Car. floor
				19.77		
				3.62		
				37 ^E		
				Car. floor		
					23.11	
				19.2		
				2.2		
				35		
				17.7		
				3.7		
				8		
				3.5		
				17.8		
				3.6		
				35		
				19.56		
				1.81		
				40		
				At. Car.		
				19.45		
				1.92		
				35 ⁴		
				Apron		
				19.57		
				1.80		
				40		
				Car. floor		
				1.87		
				40		
				Car. floor		
				19.56		
				1.81		
				38		
				Apron		
				19.35		
				2.02		
				35 ⁴		
				Apron		
				at steps.		
					21.37	

Locust

orig. B.M.	1.28	25.30	✓
check B.M. # 3-PA1	9.96	16.62	✓
T.P.	9.02	26.58	5.55 17.56

Intersection
See Macaulay X-sec. for

2+002 = sly line Macaulay

1+66 29⁸ = ± 3' wide conc. walk

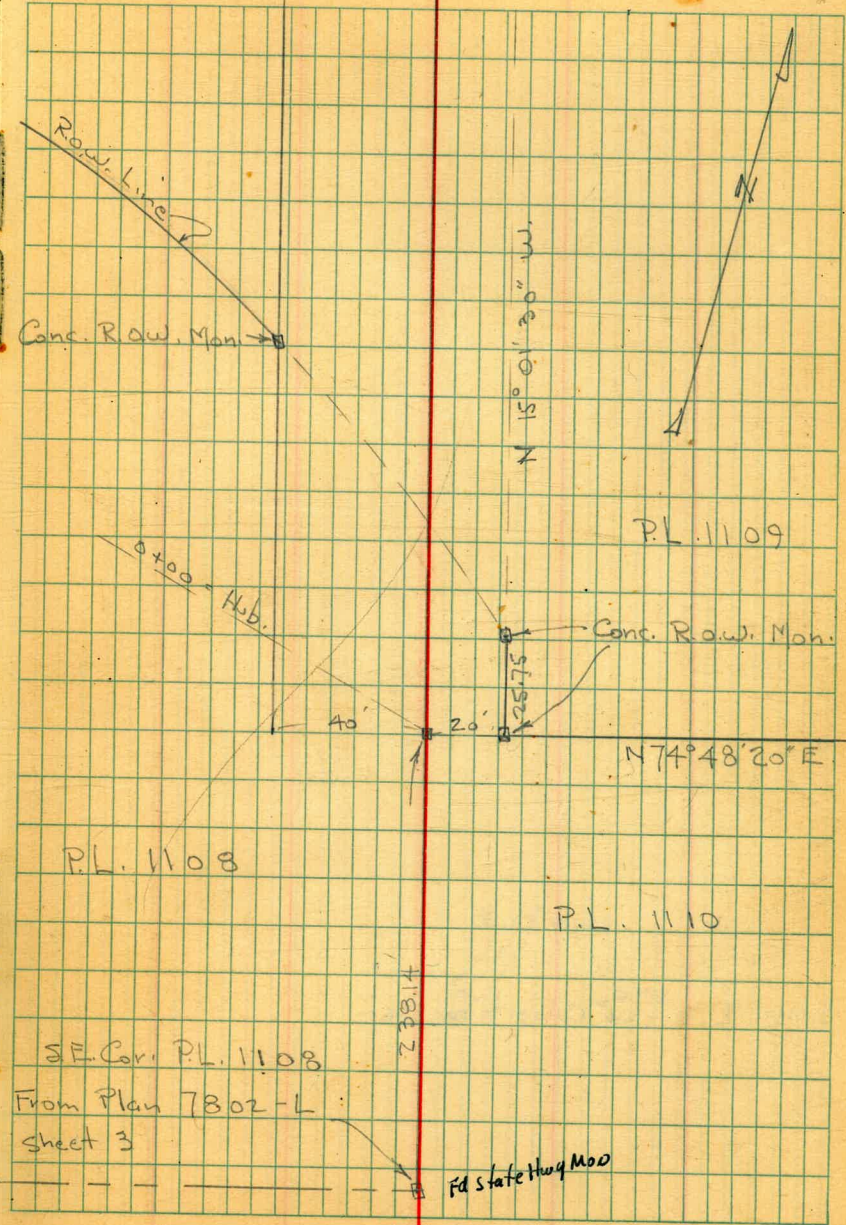
1+50

1+18 34⁸ Lt. = ± 2⁵' wide Conc. walk

1924	1916	1905	1812	1725	1619
3.87	3.95	4.06	4.9	5.6	6.2
40	35	29 ⁸	29		35
↑	walk	→	Conc		
188	1818	1812	5.128	1717	
1.3	4.3	4.9	5.3	5.4	
40	35	30		35	
1936	1927				
3.75	3.84				
44.9	34.8				
	walk				

23. 11

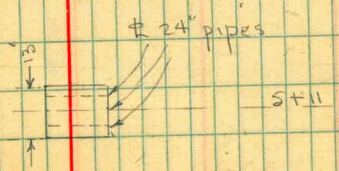
o+00 = Set Hub. = S.W. Cor. of P.L. 1109
Reproduced from Ties shown on Plan 7802-L
sheet 3



SE. Cor. P.L. 1108
From Plan 7802-L
sheet 3

Fd State Hwy No. 238.14

5+11 = 4 24" Culverts in Conc.



14+50 = P.O.T. Hub. + Gene 7-52

~~46~~
46

E = P.L. Line ↗

26+40.42 = Fd. Id. t.ct. in Large Rock
shown on P. 23 - Book 607 = N.W. Cor. PL. 1109

23+75.92 = Fd. Conc. Mon. - Brass Cap.
= N.L. PL. 1108

Set L&D.

Fd L&D Disk



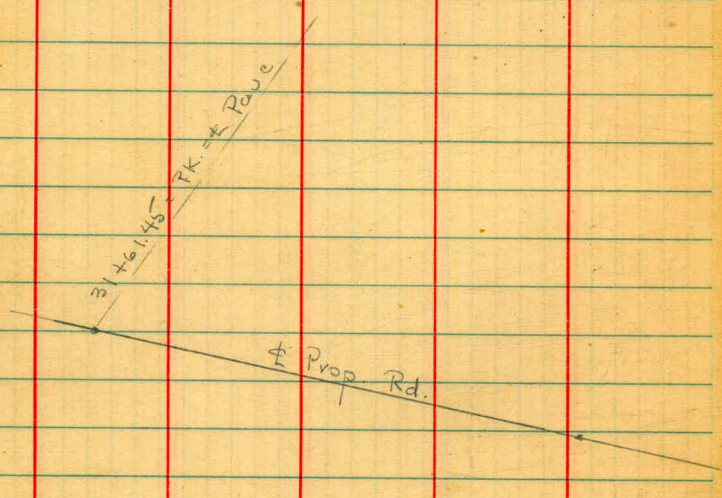
30'

Fd Mon 2/11/66 JBL

2" pipe
LS 2201

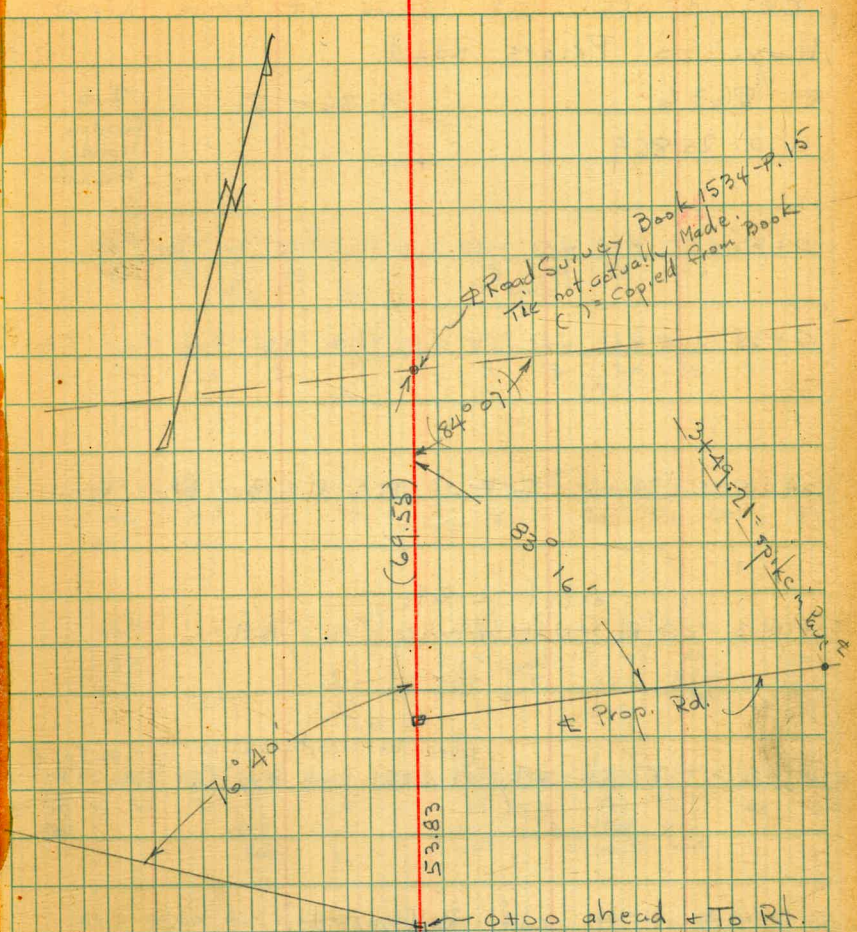
INDEXED

SEP 28 1951



27+36.53 = Hub. = Ang. $76^{\circ} 40'$ Lt. = p100-stub to Rt.
 Note: 120 is about largest Radius that will
 Miss Cor. of Conc found. - will take sections
 from Tang.

26+40.42 = Ld + ct. in Rock



Beg. Sect. of Texas St. from New Hwy. to Friars Road.

5636

9-26-51

7.0

W.O. 20869

Hardin Hatch Pearson

0+65

0+35

0+00 = N.L. Row To E. - 22.2' Rt. = Beg. Wire fence

= end of C.L. Rolls

0-14.3 - 2.3' Rt. = N.W. Cor. Wing wall - B.M.

Face of Headwall - 10'

0-22.6 - 7.7' Rt. = wly. of 4x5.4 Doub. Box Culverts - 35.3

54
BE

0-36 = ± at edge of Roll shoulder.

Sect. along Curved edge

0-62 = Wly. of Reg. Lane of Hwy.

Used Elev. Rod - Actual Elev. shown - City Datum

See State Plans for Culvert. + Pave

B.M. = N.W. Cor. of wing wall of Doub. Box Culvert

N.E. Cor. of Texas St. Int.

Lt.

#

Rt.

49

35.0	35.4	40.21	40.39	40.28	40.2	33.6	33.6	36.6	37.3
40	29	20	12	1		13	14	21	40
		edge		edge		Ditch			
34.8	35.2	42.2	42.60	42.55	39.5	37.9	33.6	33.4	37.4
40	37	24	16	7		4	12	20	22
		edge		edge			Ditch		40
35.4	44.11	43.95	43.70	38.96	38.7	33.5	33.6	37.7	36.7
46	31	21	10	on top	5	12	20	23	40
Toe	edge		edge						50
			CL						
35.3	44.29	44.22	44.07	39.5	39.87	37.7	34.3	33.7	34.4
50	34	22	11		2.3	Inside	9	15	40
Toe	edge		edge		top	point	Ditch	4+5	Edge
			CL						Ditch
			Pave						
44.3	45.18	44.35	44.30	45.07	44.1	42.9	39.87	33.83	39.83
40	37	26	10	9	6.5		7.7	I.E.	19.7
Top			Top	edge			Top	of Box	Top
			Roll				wall	wall	wall
									end
									wall
44.0	45.30	44.55	44.47	44.49	45.25	44.4	43.8	38.9	37.6
50	46	44	23		2		5	13	30
	Top	edge	Roll		Top	CL	edge		50
					Roll		Dirt		
44.11	44.30	44.30	44.44	44.52					
80	40		40	80					
39.87	= City Datum = - 6.12								
45.99	= C + G. Datum - used by State for Hwy.								

Texas

11+27-17.5 Rt. = nail in Post. = B.M. 34.79

11+00

10+50 - 30.4 Lt. = fence

10+00

9+84 - 38.5 Lt. = # Tel. pole # 537310-H

9+50

9+00

8+50

8+00

7+50

7+00 - 28.4 Lt. = fence

6+84 - 38.9 Lt. = # Tel. pole # 537309-H

6+50

6+10 - 37 Rt. = Beg. wire fence

Noted.

6+00 - Willow Trees and Brush along edges not

5+50 - 27.7 Lt. = fence

Lt.

+

Rt.

51

31.2 40	32.1 20	32.2 9.1 edge		32.4	32.4 13.5 edge	32.1 20	30.7 40		
33.5 40	32.0 30	32.6 20	32.2 7 edge	32.3	32.4 14.6 edge	32.3 20	31.2 40		
34.2 40	33.6 20	33.7 7	32.3 4.0 edge	32.4	32.4 15.7 edge	32.7 20	31.2 40		
34.2 40	33.4 20	32.4 2.8 edge		32.4	32.5 16.4 edge	33.5 20	32.0 40		
	34.7 40	33.9 20	32.6 2 edge	32.7	32.7 16.7	34.3 20	34.5 40		
34.0 40	34.0 20	32.5 2 edge	32.4	32.4 1.8		33.2 40			
	30.0 40	31.7 20		32.1 edge	32.0 19.3	32.4 2.5	31.9 40		
31.8 40	31.4 18	33.7 10		32.0	31.8 2 edge	31.8 22 edge	32.9 30	30.9 40	
32.2 50	32.6 40	32.2 28	32.8 9	32.2	31.8 4.8 edge	31.9 24 edge	32.0 40		
32.6 40	32.2 30	34.2 22		32.2	31.6 6 edge	31.8 24 edge	33.8 40		
32.6 50	32.1 40	31.6 28	31.0 11	30.4	30.2 3.7 edge	30.9 24.3 edge	31.5 40	32.9 50	
	28.7 40	27.5 20		28.4	28.5 14.3 edge	29.0 2.5	29.1 40	29.2 50	

Texas

17+00

16+50

16+00

15+50

15+10-39.5 Lt. = ± Teb pole # 5373 12-H

15+08-2' Lt. = ± Pole # P79910

15+00

14+50 = P.O.T. Hub.

34.98 on Hub.

14+00

Plowed field on Rt.

13+50 = Thru Dirt Dr. to farm

13+00 = Wly. of frame House

12+73-38.8' Lt. = ± Tel. Pole 5373 11-H

12+50

12+41-33.5' Lt. = ± 2' Cottonwood.

12+20-33.3' Lt. = end fence

12+00

11+91-23' Rt. = end fence

11+50

Lit.

±

Rt.

52

36.3 40	36.4 25 edge	36.8 3 edge	36.7	33.8 8 ± Ditch	37.1 17 edge	36.9 40		
36.3 40	36.4 26 edge	37.0 4	37.0	33.6 5 ± Ditch	37.0 16 edge	37.0 40		
36.0 40	36.4 26 edge	37.0 4.7	36.9	33.4 6 ± Ditch	36.7 17 edge	36.5 40		
36.6 40	36.5 25 edge	36.7 5	36.5	33.5 6 ± Ditch	36.2 14 edge	36.3 40		
34.8 40	35.6 24 edge	35.6 5.5	36.0	33.3 8 ± Ditch	35.9 18 edge	35.8 40		
35.0 50	34.4 40	34.6 24 edge	34.9 2 on Hub.	34.98 8 ± Ditch	35.1 20 edge field	35.0 40		
	34.5 45	34.1 2 edge	34.0	34.2 3 ± Ditch	32.3 8 edge	34.5 19 edge	34.3 40	
36.2 60	34.8 40 in Dr.	33.7 19.5 edge	33.5	33.5 15 edge	32.3 8 ± Ditch	34.6 15 edge of field	33.6 22 edge of field	33.6 40
36.5 65.4 along house.	36.2 40	36.0 35	33.5 25	33.3 16.5 edge	32.9 3.5 edge	31.8 8 ± Ditch	33.7 15	33.1 40
35.2 40	34.8 30	33.4 15	32.4 16.2 edge	32.2 6.5 edge	32.0 6.5 edge	32.6 20	32.2 40	
30.2 40	31.0 20	32.0 13.3 edge	32.2	31.9 9 edge	31.4 20	31.1 40		
29.7 40	31.3 20	32.0 12 edge	32.3	32.1 11.2 edge	30.6 20	30.2 40		

Texas

= end of Cold lay Pave - Begs gravel yard

27+04 - 69.1 Lt. = N.E. Cor. of Warehouse - Conc. floor

27+00

26+50 - 66' Lt. = S.W. Cor. of Warehouse Bldg.

Ditch full of water - use same Sect. for yardage

26+20 = Ang. in Ditch - Goes E. along field.

26+00 = end Planted field on Rt.

25+79 - 39.4 Lt. = ± Tel. pole # 537316 - H

25+50

25+00 = ± of Dirt Dr. = Ent. to Block Plant.

24+50

24+00

23+75

23+74 - 18' Lt. = ± P. pole # 179911

23+50

23+45 - 18' Lt. = ± Dead man

23+35 - 18.7 Lt. = ± Dead man

23+20 = ± Dirt Dr. = entrance to Premix plant.

Lt.

#

Rt.

54

39.37 35.8
69.1 = 69.1 = ground.
Conc floor35.9 35.9 35.9 35.6 35.4 35.4
57 40 27 20 4036.5 35.6 35.7 35.6 35.3 35.1
40 21 25 20 4037.5 36.6 35.5 35.8 35.9 33.5 35.7 35.4
40 30 21 edge 7 ± Ditch 18 E. My. field36.6 35.7 35.7 35.7 35.9 33.6 35.3 35.3
40 18 edge 1 6 ± Ditch 18 E. 4036.5 36.4 36.3 36.0 35.7 35.7 35.8 33.6 35.4 35.4
50 40 25 15 edge 1 5 ± Ditch 17 E. 4036.1 36.0 35.8 35.8 35.7 35.7 33.6 35.5 35.4
40 25 15 edge 2 6 ± Ditch 17 E. 4036.0 35.8 35.7 35.6 35.6 33.5 35.4 35.4
40 13.5 edge 3 6 ± Ditch 17 E. 4036.2 35.9 35.9 35.7 35.6 35.4 33.8 35.4 35.4
40 20 14 edge 3 9 ± Ditch 17 E. 4037.5 37.6 36.0 35.8 35.7 35.2 33.9 35.5 35.6
40 25 15 edge 3 8 ± Ditch 17 E. 40

C.L.

Texas

Lt.

±

Rt.

5

spike in Pole # 489043-H

55.07

50' W. along ± of pave - sect. 90° to Pave

31 + 61.45 = ± of Paving - Sect. at 90° to back Tang

53.9
17

53.96
12

53.90

53.62
10.2

edge

54.5

24

Top bank

54.28

12

53.94

edge

53.62

12

X-Section Roadway of Wightman
to check yardage - 39th to 40th

W.O. 31587 - 12-21-51 - 70.

3+00 ± = w.L. 40th = edge of A.C.

2+85 = P.C. of 20' Rad. New Ret. - Type G curb.
on Lt. only

2+50

2+00

1+50 = Alley

1+00

0+50

0+00 = E.L. of 39th = edge of A.C.

B.M. N.W. B.P. Central & Wightman 343.67

This is same Datum as used in orig. Sections

Lt.

±

Rt.

58

43.07 31.8 Top Co.	42.41 gut.	42.45 13	42.39	42.15 13	41.97 31.4 gut (A.C.)	42.75 Top
--------------------------	---------------	-------------	-------	-------------	--------------------------------	--------------

42.85 26 Top	42.25 gut	42.35 24.5 edge	42.42.5 13	42.3 13	No gut	41.8 26	42.46 26
--------------------	--------------	-----------------------	---------------	------------	--------	------------	-------------

41.8 26 gut	42.2 13	42.2	41.9 13	41.2 26
-------------------	------------	------	------------	------------

41.3 26 gut	41.5 13	41.7	41.3 13	40.7 26 gut
-------------------	------------	------	------------	-------------------

41.7 40	41.2 26	41.1 13	41.2	40.9 13	40.2 26	41.3 40
------------	------------	------------	------	------------	------------	------------

40.3 26 gut	40.6 13	40.9	40.2 13	39.5 26 gut
-------------------	------------	------	------------	-------------------

39.9 26 gut	40.3 13	40.3	39.8 13	38.9 26 gut
-------------------	------------	------	------------	-------------------

39.74 Top	39.15 26 gut	39.48 13	39.52	38.56 26 gut	39.07 Top Cl.
--------------	--------------------	-------------	-------	--------------------	---------------------

Actual Elev. shown. 350' Elev. Not shown

D. Smith
C. Allen
J. Bishop
R. Taylor

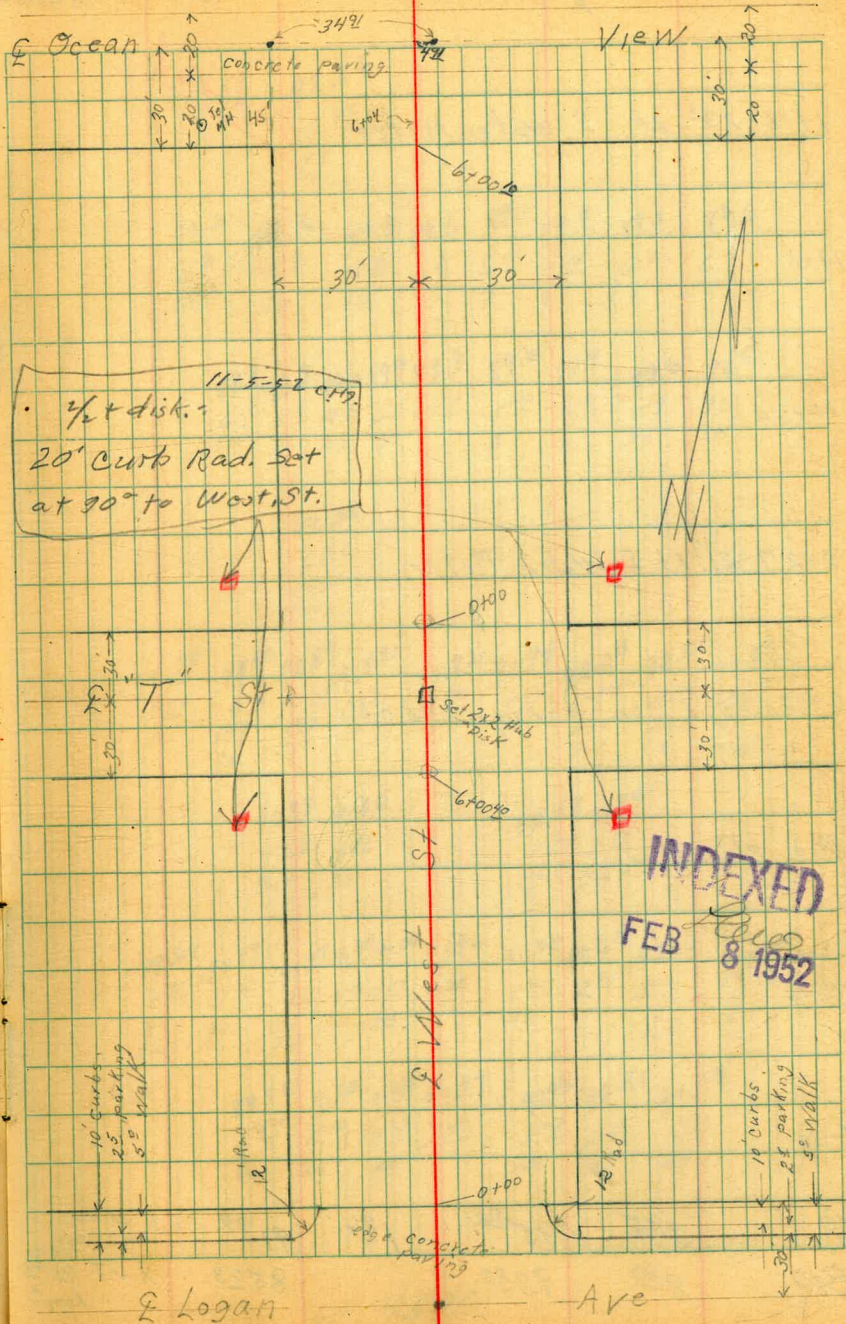
Cross Sec. West St

Logan to Ocean View

W10th
31752

2-6-52

Soil Samples taken @ 3+00 10' ft or west
in both Blks



2121 19⁴ Lt E Water Meter

2100

1484 19³ Lt E water Meter

1476 20⁶ Rt E Water Meter

1475 28⁸ Rt E 3' con walk

1459 29³ Lt E 8' con drive

1454 20⁴ Rt E 9' con drive

1450

1440 29³ Lt E 8' driveway

1432 29⁰ E 3' walk

Lt West

E

Rt East

61

88.97

6⁵⁷

19⁴
value

89.4	89.3	89.6	89.1	89.6	89.4	89.7	90.3	90.9
6 ⁴	6 ³	5 ²	6 ⁴	5 ²	6 ⁴	5 ²	5 ²	4 ⁶
50	30	16	12		8	10	30	50

88.17

7³⁵

19³
value

89.19

6³³

20⁶
value

90.35	90.57
5 ¹⁷	4 ⁹⁵
28 ⁸ walk	38 ⁸ walk

89.77 89.69

5⁷⁵ 5⁸³

39⁵ 29⁴
drive drive

89.81 90.06 90.32

5²⁴ 5¹⁶ 5²⁰
20⁴ 21⁶ 31⁸
drive

89.8	89.6	89.4	89.5	89.4	89.4	90.3	90.6
5 ²	5 ²	6 ⁴	6 ²	6 ⁴	6 ⁴	5 ²	4 ⁹
50	30	9		8	11	30	50

89.92 89.70

5⁶⁰ 5⁸²
39² 29³

90.01 89.81

5⁵¹ 5²⁴
39² 29³
walk walk

7 95⁵²

3150

3142 30° RT & 8' con drive

3137 20° RT End Floral planting

3125 20° RT & Water Meter

3125 18° LT & Water Meter

3120 30° RT & 35' con walk

3100 20° RT Begin Floral planting

2173 19° LT & Water Meter

2155 29° LT & 8' con drive

TP₂ 42 94⁵³ 52° 89⁸²

2150

2141 29° LT & 8' con drive

LT West

RT East

62

89.8	89.8	90.1	89.2	89.8	89.4	90.1	90.6	90.8
42	42	44	53	42	51	42	32	32
50	30	16	14		8	12	30	50

90.66
387
30
drive

90.81
322
40
drive

89.20

89.88
465

533
109
valve

90.76
327

91.06
342

90.4	90.2	90.1	89.4	89.7	89.4	90.0	90.0	90.1
44	43	44	51	48	51	45	45	44
50	30	15	13		9	12	30	50

89.96

457
19
valve

89.81 89.82

422 424
398 298
drive drive

94⁵³

89.7	89.6	89.6	89.3	89.7	89.3	89.9	90.0	90.8
58	52	52	62	58	62	56	55	47
50	30	15	12		8	12	30	50

89.61 89.47

53 65
392 292
drive drive

95⁵²

5420 29° LT & 3 con walk

5417 18° RT & Water Meter

5400

4474 19° RT & Water Meter

4474 16° LT & Water Meter

4471 29° LT & 3' con walk

4450

4441 29° LT & 5" tree

4426 16° LT & Water Meter

4424 30° LT & 3' con walk

4419 22° LT & 6" apple tree

4400

Lt-West

RT-East 63

90.27 90.17
4²⁶ 4³⁵
29° walk 29° walk

90.62
3²¹
18°
valve

89.7	89.8	89.8	89.0	89.5	90.1	90.1	90.9	91.3	91.6
4 ⁸	4 ²	4 ²	5 ⁵	5 ⁰	4 ²	4 ²	3 ⁶	3 ²	3 ²
50	30	15	12	10		11	16	30	50

89.95
4⁵⁸
19°
valve

89.26
5²⁷
16°
valve

89.88 89.80
4⁶⁵ 4²³
40° walk 29° walk

89.3	89.5	89.6	89.1	89.9	89.7	90.2	90.6	91.1
5 ³	5 ⁰	4 ²	5 ⁴	4 ⁶	4 ⁸	4 ³	3 ²	3 ²
50	30	15	12		12	16	30	50

88.96
5⁵³
16°
valve

89.20 89.40
5³³ 5¹³
40° walk 30° walk

89.2	89.2	89.7	89.1	89.8	89.5	90.5	90.7	90.7
5 ³	5 ³	4 ⁵	5 ⁴	4 ²	5 ⁰	4 ⁰	3 ⁸	3 ⁸
50	30	16	14		11	14	30	50

π 94.53

6113

TP₃ 569 95⁸⁰ 4⁴² 90⁴

6750⁴⁰ Sly Line T" ST

5781 18" RT & water meter

5777 30" LT & 3' con walk

5765 15" LR Water Meter

5761 29" RT & 8' con drive

5750

5724 29" RT & 8' con walk

5724 16" LT & water meter

Lt. West

Σ

Rt. East

LT

88.2	89.6	90.0	88.8	89.6	89.9	90.0	90.8	90.8	91.1
76	62	58	70	63	52	52	50	52	47
80	30	18	15	12		9	15	50	80

95⁸⁰

89.3	89.8	89.9	88.8	89.4	90.1	89.8	90.8	91.0	91.4
52	42	45	52	51	42	42	32	35	31
50	30	16	14	12		9	14	30	50

90.58
395
150
valve

90.05 90.09
448 444
40 walk 302

89.43
513
155
valve

91.47 91.70
320 223
295 392
drive

89.8	90.0	90.0	89.7	89.0	89.6	90.3	90.2	91.0	91.4	91.5
42	45	45	45	55	42	42	43	35	31	30
50	30	17	14	12	10		13	15	30	50

91.42 91.53
311 300
272 372
walk

89.64
489
165
valve

94⁵³

0+19 19° Lt & Water Meter

0+16 30° Rt & 8 con drive

6+00 11y T" ST

6+49

6+47

6+45

6+30⁹⁰ 1" T" ST

6+21

6+17

Lt West

2

Rt East

65

90.05

52¹

19¹

value

91.6⁰

42⁰

30²

drive

91.7⁰

42⁰

40²

89.7	90.0	89.6	89.0	89.5	90.0	90.2	90.6	91.1	91.4
61	58	62	68	63	58	56	52	42	44
50	30	17	13	11	8	11	30	50	

88.1	89.5	89.7	89.0	89.1	89.9	90.0	90.7	90.8	91.5
74	63	61	68	62	52	52	51	50	42
80	30	21	16	13	8	14	30	80	

87.3	88.6	89.3	89.8	90.0	90.2	91.1
85	72	65	60	58	56	42
80	30	12		12	30	80

88.0	89.0	89.5	89.9	90.1	90.2	91.1
72	68	63	52	52	52	42
80	30	12		12	30	80

88.4	89.6	89.9	90.0	90.2	90.4	91.2
72	63	52	52	52	52	42
80	30	12		12	30	80

88.0	89.4	89.8	90.1	90.1	90.3	91.1
72	62	62	52	52	55	42
80	30	12		12	30	80

87.4	88.5	88.9	89.3	89.3	90.0	90.5
82	72	62	65	65	52	52
80	30	12		12	30	80

95.80

1750

2

1421 16² RT & Water Meter

2

T. 1410 34² RT & 8' con drive

1

1400

1

0471 17² RT & Water Meter

0

0468 19² LT & Water Meter

0

0465 29² LT & 3' con walk

0

0460 29² RT & 8' con drive

04

B. 0450

P.

Lt = West \$ Rt = East

66

89.3	89.6	90.2	89.8	90.4	90.2	90.7	91.1	91.0
6 ⁵	6 ³	5 ⁶	6 ⁰	5 ⁴	5 ⁶	5 ¹	4 ²	4 ³
50	30	15	13		7	9	30	50

89.88
5⁹²
16²
valve

91.16
4⁶⁴
34² drive

91.23
4⁵⁷
44²

89.8	90.3	90.3	89.8	90.3	90.2	90.4	90.7	91.3
6 ⁰	5 ⁵	5 ⁵	6 ⁰	5 ⁵	5 ⁶	5 ⁴	5 ⁴	4 ⁵
50	30	16	14		7	10	30	50

90.10
5⁷⁰
17²
valve

89.69
6⁴
19²
valve

90.18
5⁶²
39² walk

90.37
5⁴³
29²

91.20
4⁶⁰
29² drive

91.32
4⁴⁸
39²

89.8	90.3	90.2	89.7	90.4	90.5	90.9	90.7	91.1
6 ⁰	5 ⁵	5 ⁵	6 ¹	5 ⁴	5 ³	4 ²	5 ¹	4 ²
50	30	15	13		8	11	30	50

95.80

3750

3426 16' RT E Water Meter

3413 30' LT E 8' con drive

3400

2499 16' RT E Water Meter

2471 20' RT E Water Meter

2450

2432 31' LT E 2' con walk

2400

LT = West

RT = East

67

90.8	91.5	91.4	90.9	91.3	91.1	91.5	92.1	92.5
50	43	42	42	45	42	43	37	33
50	30	19	14		9	14	30	50

91.47
433
16' valve

90.70	90.93
510	482
402	303
drive	

90.4	90.7	90.9	90.7	90.9	90.8	91.5	92.2	92.6
54	54	42	52	42	50	43	36	32
50	30	17	15		8	11	30	56

90.31
549
16' valve

89.87
523
20' valve

90.7	90.9	90.8	90.5	91.0	90.9	91.2	92.0	92.2
54	42	50	53	48	49	46	30	36
50	30	16	13		8	11	30	50

90.79 90.89
501 42
11' walk

90.8	91.1	90.9	90.2	90.9	90.6	91.3	91.9	91.8
50	44	42	56	42	52	45	32	40
50	30	15	13		8	11	30	50

95.80

Lt-West

Σ

Rt-East

68

4120 30² Rt & 3⁵ con walk

4120 17⁸ Rt & Water Meter

4110 30² Lt & 6^c con ribbon drive 2' ca.

4100

3189 30² Lt & 13⁵ con drive

3174 29² Rt & 3⁵ con walk

3173 19⁸ Rt & Water Meter

3158 29³ Rt & 10⁵ con drive

3155 29² Lt & 3 con walk

T.P. 4

6²⁴

97⁷²

4³²

91⁴⁸

3126 H.O. meter
valve
16' RT

92.84
4⁸⁹
91.71
6⁰¹
17⁸
walk

92.96
4⁷⁴
30² walk
40²

92.05
5⁶⁷
40⁵
drive

92.09
5⁶³
30⁵

92.1
5⁶
50

92.2
5⁵
30

91.2
6⁵
15

91.7
6⁰

91.5
6²
8

92.0
5⁷
14

92.6
5¹
30

92.7
5⁰
40

92.20
5⁸²
30²
drive

92.30
5⁴²
30²

92.83
4⁸⁹
29²

92.93
4⁷²
39²
walk

91.85
5⁸⁷
19⁸
valve

92.41
5³¹
29²
drive

92.58
5¹⁴
39²

91.73
5⁹⁹
40 walk 29²

91.98
5⁷⁴

97⁷²

4792 30' LT E 7' con ribbon drive 1²ca

4788 20' RT E water Meter

4771 30' LT E 3' con walk

4766 20' LT E water Meter

4760 30' RT E 26' con drive ribbons 2'ca

4750

4745 30' RT E 8' con drive

4735 19' LT E water Meter

4730 30' LT E 3' con walk

Lt = West

E

RT = East

69

92.70 92.84
5 102 4 98
40' 30'
drive

92.90
4 82
20'
valve

92.80 92.75
4 92 4 97
40' 30'
walk

91.55
6 17
20'
valve

93.30 93.45
4 42 4 27
30' 40'
drive

92.7	92.5	91.7	92.2	92.3	92.1	92.5	93.1	93.4
5 2	5 3	6 0	5 5	5 4	5 6	5 3	4 6	4 3
50	30	16	9		8	17	30	50

93.12 93.36
4 60 4 36
30' 40'
drive

91.76
5 96
19'
valve

92.35 92.27
5 37 5 45
40' 30'
walk

97.72

5756 30³ Rt Begin rock & con wall

5755 29^E Rt & 2^o con walk

5750

5745 30³ Rt & 8^o con drive

5742 30³ Lt & 7^o con drive

5726 20^E Rt & Water Meter

5720 30^o Rt & 3⁵ con walk

5717 20³ Lt & Water Meter

5700

Lt = West

E

Rt = East

73

94.6
32
30³
footing

95.10
29³
30³
700

95.12
260
29³
walk

95.16
256
30³
walk

92.1	93.0	92.7	93.0	93.1	92.9	93.5	93.9	94.8	95.1
46	42	52	42	46	42	42	32	22	26
50	30	17	10		9	13	22	30	50

94.95
222
30³ drive

95.11
241
40³

94.21
351
30³ drive

94.02
322
30³

92.50
522
20^E
valve

94.66
302
30³
walk

94.86
286
40³
walk

92.09
563
30³
valve

92.7	92.1	92.4	92.2	92.6	92.8	92.5	93.2	94.0	94.6
50	50	53	55	51	49	53	45	37	34
50	30	17	15	9		10	18	30	50

7 97.72

BM

725 47° 95³⁷ 705 90⁶⁷ 85⁴² 847.4511
Ocean View Wd
55-44

6+30¹⁰ 2 paving

6+20¹⁰ sly edge paving

6+14

6+12 32² L+E 14" Power 10/10 P95825

6+00¹⁰ sly line Ocean View

5797 30⁵ RT End rock and con wall

5795

5758 19² RT-E Water Meter

Lt - Voss 8 Rt - East 71

91.63 92.44 92.50 92.57 92.60 92.66 92.71 92.82 93.09
609 5-31 5-22 5-15 5-12 5-06 5-01 4-90 4-63
80 30 20 10 10 20 20 30 80
on lat

91.58 92.33 92.43 92.50 92.58 92.65 92.65 92.75 93.00
614 5-29 5-29 5-22 5-14 5-07 5-07 4-92 4-22
80 30 20 10 10 20 30 80

91.8 92.1 92.9 92.4 92.4 92.4 92.6
5-2 5-6 5-2 5-3 5-3 5-3 5-1
50 30 20 20 30 50

92.1 92.7 92.5 92.0 92.4 92.5 93.3 93.3 93.1
5-6 5-0 5-2 5-2 5-3 5-2 4-4 4-4 4-6
50 30 23 18 11 14 30 50

92.4 92.9 92.9 92.3 92.6 92.6 93.3 93.3 93.4
5-3 4-2 4-2 5-4 5-1 5-1 4-4 4-4 4-3
50 30 21 18 10 13 30 50

93.8 94.3 94.1 92.4 92.7 92.7 94.1 94.0 94.0 94.80 95.0
3-2 3-2 3-2 5-3 5-0 5-3 3-6 3-2 3-2 2-30 2-2
50 30 21 17 10 13 30 30 30 30 50
cutting 100

93.8 94.2 93.6 92.5 93.0 93.0 92.8 94.3 93.8 94.3 95.0
3-2 3-5 4-1 5-2 4-2 4-2 4-3 3-4 3-3 3-2 2-3
50 30 20 18 10 10 12 21 30 50

92.33
4-39
192
valve

7 9772

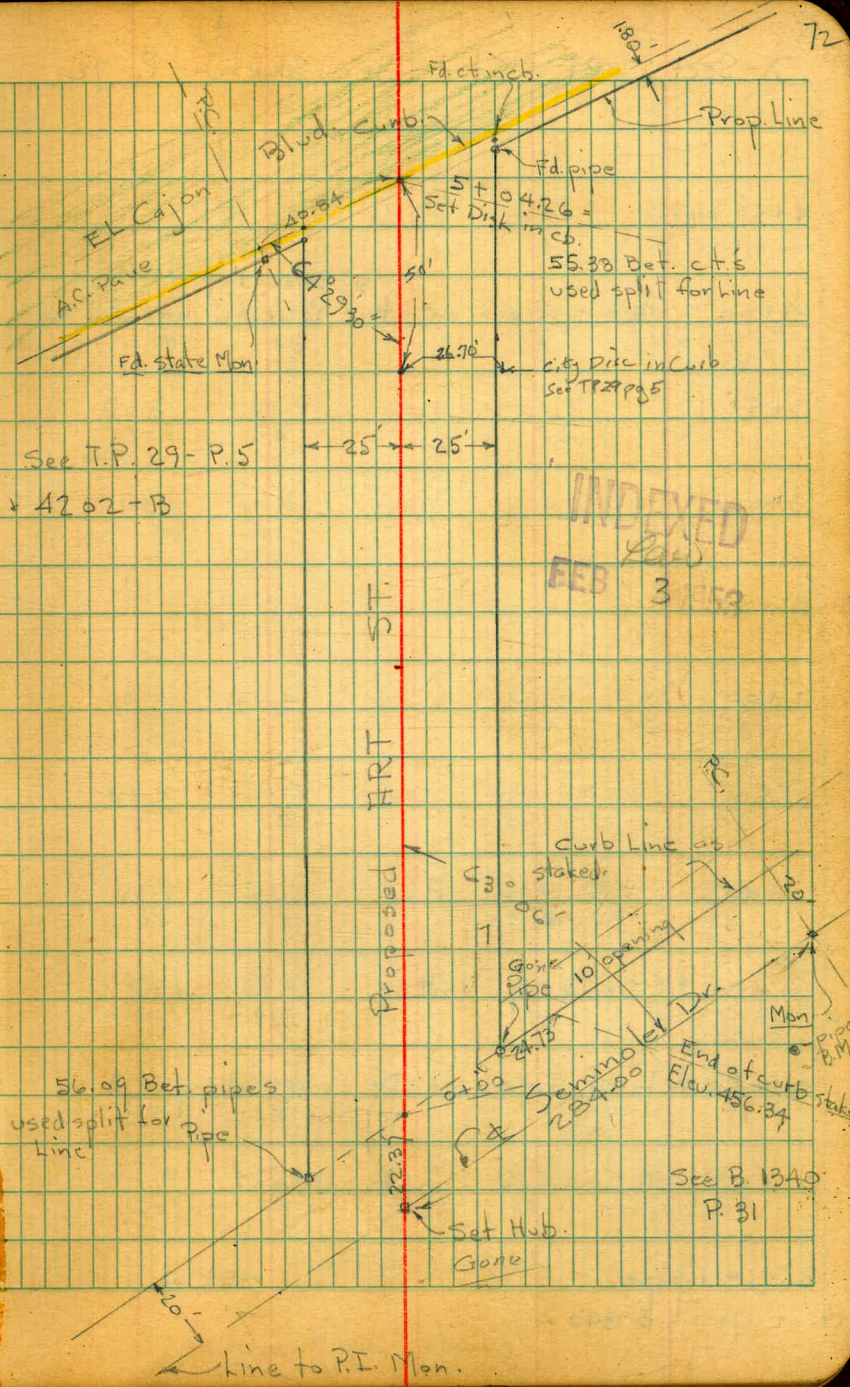
X- Sect. Proposed ART St. - 50' wide
 7' curbs. for Grade Est. - See Elev. of
 Curbs as staked for Safeway Store. on
 sketch- opp. page.

W.O. 25020

7-3-52

7.0.

INDEXED
 FEB 3 1953



X-Section TART St. - See Sketch P. 72

4+50

4+00 = Parking curb on Rt. - ^{8" Below top:} Pavc for Lot will be

3+50

3+00

2+50

2+00

1+50

1+00

0+50 - Sect. 90° to †

0+00 = W.L. of Seminole Dr. - outs along W.L.

0-22.37 = † Seminole - outs along †

B.M. = 1" pipe
Rt. of 17+00 = B. 1340

458.07

Lt. † Rt. B

	62.5 25	62.2	62.1 25	63.41 26.5 = Top cb.	
	62.5 35	62.2 25	61.8 25	63.02 26.5 = Top of cb.	
	62.5 30.5 along Court.	62.5 25	62.2	61.7 25	
	62.6 35	62.5 25	61.9	61.6 24	61.1 25
		62.7 25	61.9	61.5 23	60.9 25
	62.4 35	62.5 25	62.0	62.0 23	60.5 25
					60.6 35
	61.8 35	61.7 25	61.3	61.4 23	60.4 25
					Hot 35
	60.7 35	61.0 25	60.5	60.4 25	59.8 25
					Lit. 35
	59.1 35	59.4 25	59.5	59.4 25	59.4 35
					ingraded Lot (Parking)
	57.1 70	57.2 28	58.1	58.7 28	59.6 70
					prop cot.
	56.0 70	56.7 28	57.5	58.2 28	59.2 70

400 Elev. Not Noted.

Actual Elev. Shown.

HRT

Lt.

±

Rt.

74

El Cajon:
Set B.M. on Mon. - on S.L. at P.C. 463.19

Sect. in gutter.

outs along curb
5+04.4 = S. curb face of El Cajon.

4+82-

62.73 gut.	62.60 gut.	62.37 gut.	62.26 gut.	62.03 gut.
62.31 60 Top	63.29 27.7 Top	63.00 Top	62.88 27.7 Top	62.70 70 Top
	63.0 25	62.1	62.5 25	63.67 26.5 = Top ch. Ang. pt.

Texas

Rt. 11+27 - P. 51
check B.M. = nail in post

34.79

Rest. is same - End.

9+50 = Beg. old pave

9+00

8+50

8+00

Lt.

#

Rt.

76

	34.2	33.4	32.3	32.4	32.5	33.5	32.0
	40	20	2.8	edge	16.4	20	40
34.7	34.4	32.4	32.3	32.6	32.6	33.8	34.5
40	30	10	5	edge	18	20	40
34.0	33.7	32.1	32.2	32.3	32.6	32.7	33.2
40	30	10	4	edge	19	30	40
30.0	32.1	32.1	32.1	32.1	32.1	32.9	
40	15	5	edge	19	40		

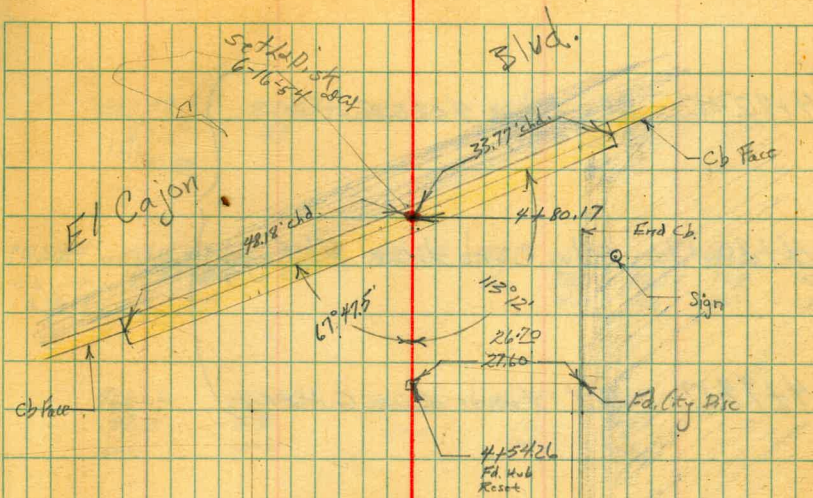
Roberts
Cota
Moore
Morales
2-23-54
W.D. 20005

Re-X-Section Art Street at El Cajon Blvd.

See Pg. 72 this FB, T.P. 29 pg 5

See State Plans For Curve - We had no data!

INDEXED
ER
FEB 26 1954



El Cajon Blvd

Curb setback
Parking lot.

Cont'd From Page 77

4+82.49 Nly Edge 4' Conc. Gutter

Parallel

4+80.17 Sly Curb Line El Cajon

El Cajon 413.39
100
cb

4+78.17 Hit 4' wide Conc. Gutter

4+78.5 26[±] Rt End Curb

4+77.3 31.8 Rt to center Safeway Sign

4+67.5 23[±] Lt to center P. Pole # 70533

4+50

4+45 22[±] Lt to headman

4+21 26[±] Rt to center light Pole

4+00

Direct Elevation Rod Used

Lt

E

Rt

78

462.57 50 462.43 25 462.30 462.22 16[±] 462.13 33

462.74 462.15 462.52 462.37 462.24 462.13 462.06 462.71 462.66 462.22
100 461.8 461.8 24 16 33.77 33.77 105 105
Gut cb Gut Gut cb Gut cb

462.62 462.46 462.30 462.19 462.16
47.4 24 16 34.3
conc conc conc conc conc

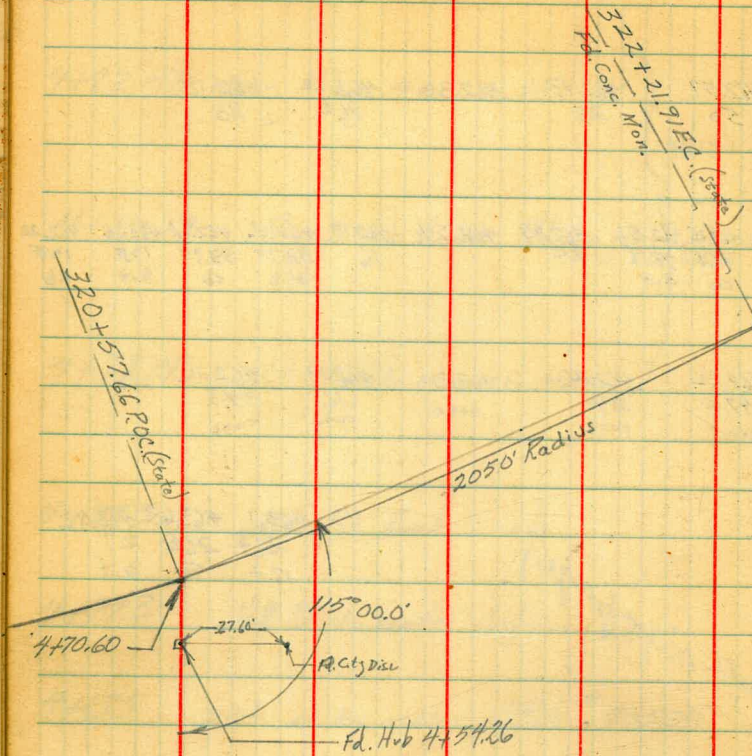
463.1 463.63 463.02
26[±] 26[±] 27
Gut cb Gut

(all next page)

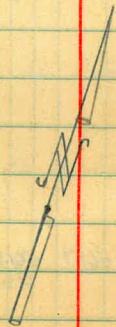
462.7 25 462.1 462.5 462.7 462.8 463.41 462.77
24 25 26[±] 26[±] 27
AC Gut cb Gut

462.2 25 461.9 461.6 462.3 462.4 463.02 462.40
23 25 26[±] 26[±] 27
AC Gut cb Gut

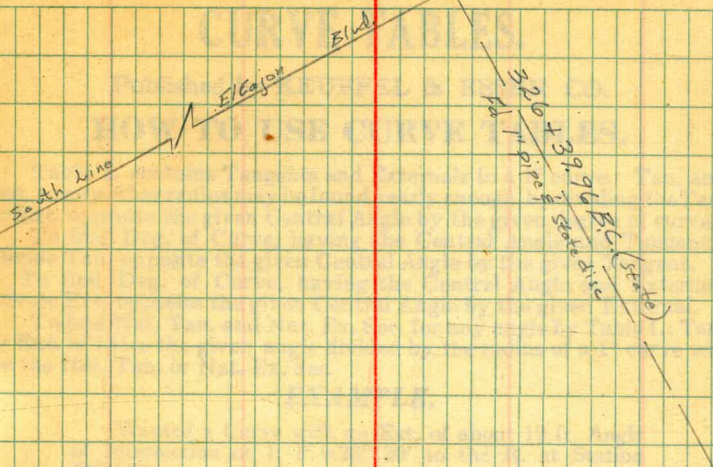
Contd From Page 78



C. Ave Street



79



CURVE TABLES.

Published by KEUFFEL & ESSER CO.

HOW TO USE CURVE TABLES.

Table I. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and External: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table I.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P. = 23° 20' to the R. at Station 542+72.

Ext. in Tab. I opposite 23° 20' = 120.87
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. I opp. 23° 20' = 1183.1
 $1183.1 \div 10 = 118.31$.

Correction for A. 23° 20' for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47$ = corrected Tangent.

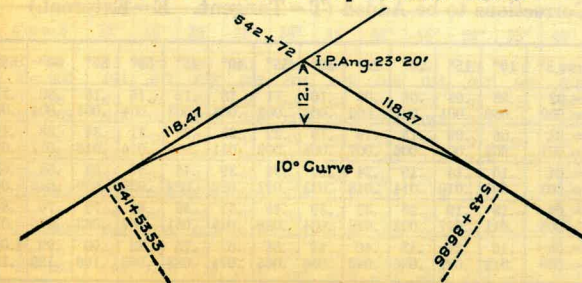
(If corrected Ext. is required find in same way)
 Ang. 23° 20' = 23.33° ÷ 10 = 2.3333 = L. C.

2° 19½' = def. for sta.	542	I. P. = sta.	542+72		
4° 49½' = " " "	+50	Tan. =		1	.18.47
7° 19½' = " " "	543	B. C. = sta.		541	+53.53
9° 49½' = " " "	+50	L. C. =		2	.33.33
11° 40' = " " "	543+	E. C. = Sta.		543	+86.86
	86.86				

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^\circ \text{ Cur.}) = 139.41' =$
 $2^\circ 19\frac{1}{2}' = \text{def. for sta. } 542.$

Def. for 50 ft. = 2° 30' for a 10° Curve.

Def. for 36.86 ft. = 1° 50½' for a 10° Curve.



Natural Trigonometrical Functions

Angle. Sin. Tan. Sec. Cosec. Cotg. Cosin.							Angle. Sin. Tan. Sec. Cosec. Cotg. Cosin.						
32	.5299	.6249	1.1792	1.887	1.600	.84805	58	.6293	.8098	1.2868	1.589	1.235	.77715
10	.5324	.6289	1.1813	1.878	1.590	.84650	50	.6316	.8146	1.2898	1.583	1.228	.77531
20	.5348	.6330	1.1835	1.870	1.580	.84495	40	.6338	.8195	1.2929	1.578	1.220	.77347
30	.5373	.6371	1.1857	1.861	1.570	.84339	30	.6361	.8243	1.2959	1.572	1.213	.77162
40	.5398	.6412	1.1879	1.853	1.560	.84182	20	.6383	.8292	1.2991	1.567	1.206	.76977
50	.5422	.6453	1.1901	1.844	1.550	.84025	10	.6406	.8342	1.3022	1.561	1.199	.76791
33	.5446	.6494	1.1924	1.836	1.540	.83867	57	.6428	.8391	1.3054	1.556	1.192	.76604
10	.5471	.6536	1.1946	1.828	1.530	.83708	50	.6450	.8441	1.3086	1.550	1.185	.76417
20	.5495	.6577	1.1969	1.820	1.520	.83549	40	.6472	.8491	1.3118	1.545	1.178	.76229
30	.5519	.6619	1.1992	1.812	1.511	.83389	30	.6494	.8541	1.3151	1.540	1.171	.76041
40	.5544	.6661	1.2015	1.804	1.501	.83228	20	.6517	.8591	1.3184	1.535	1.164	.75851
50	.5568	.6703	1.2039	1.796	1.492	.83066	10	.6539	.8642	1.3217	1.529	1.157	.75661
34	.5592	.6745	1.2062	1.788	1.483	.82904	56	.6561	.8693	1.3251	1.524	1.150	.75471
10	.5616	.6787	1.2086	1.781	1.473	.82741	50	.6583	.8744	1.3284	1.519	1.144	.75280
20	.5640	.6830	1.2110	1.773	1.464	.82577	40	.6604	.8796	1.3318	1.514	1.137	.75088
30	.5664	.6873	1.2134	1.766	1.455	.82413	30	.6626	.8847	1.3352	1.509	1.130	.74896
40	.5688	.6916	1.2158	1.758	1.446	.82248	20	.6648	.8899	1.3386	1.504	1.124	.74703
50	.5712	.6959	1.2183	1.751	1.437	.82082	10	.6670	.8952	1.3421	1.499	1.117	.74509
35	.5736	.7002	1.2208	1.743	1.428	.81915	55	.6691	.9004	1.3456	1.494	1.111	.74314
10	.5760	.7046	1.2233	1.736	1.419	.81748	50	.6713	.9057	1.3492	1.490	1.104	.74120
20	.5783	.7089	1.2258	1.729	1.411	.81580	40	.6734	.9110	1.3527	1.485	1.098	.73924
30	.5807	.7133	1.2283	1.722	1.402	.81412	30	.6756	.9163	1.3563	1.480	1.091	.73728
40	.5831	.7177	1.2309	1.715	1.393	.81242	20	.6777	.9217	1.3600	1.476	1.085	.73531
50	.5854	.7221	1.2335	1.708	1.385	.81072	10	.6799	.9271	1.3636	1.471	1.079	.73333
36	.5878	.7265	1.2361	1.701	1.376	.80902	54	.6820	.9325	1.3673	1.466	1.072	.73135
10	.5901	.7310	1.2387	1.695	1.368	.80730	50	.6841	.9380	1.3711	1.462	1.066	.72937
20	.5925	.7355	1.2413	1.688	1.360	.80558	40	.6862	.9435	1.3748	1.457	1.060	.72737
30	.5948	.7400	1.2440	1.681	1.351	.80386	30	.6884	.9490	1.3786	1.453	1.054	.72537
40	.5972	.7445	1.2466	1.675	1.343	.80212	20	.6905	.9545	1.3824	1.448	1.048	.72337
50	.5995	.7490	1.2494	1.668	1.335	.80038	10	.6926	.9601	1.3863	1.444	1.042	.72136
37	.6018	.7536	1.2521	1.662	1.327	.79864	53	.6947	.9657	1.3902	1.440	1.036	.71934
10	.6041	.7581	1.2549	1.655	1.319	.79688	50	.6967	.9713	1.3941	1.435	1.030	.71732
20	.6065	.7627	1.2577	1.649	1.311	.79512	40	.6988	.9770	1.3980	1.431	1.024	.71529
30	.6088	.7673	1.2605	1.643	1.303	.79335	30	.7009	.9827	1.4020	1.427	1.018	.71325
40	.6111	.7720	1.2633	1.636	1.295	.79158	20	.7030	.9884	1.4061	1.422	1.012	.71121
50	.6134	.7766	1.2661	1.630	1.288	.78980	10	.7050	.9942	1.4101	1.418	1.006	.70916
38	.6157	.7813	1.2690	1.624	1.280	.78801	52	.7071	1.0000	1.4141	1.414	1.000	.70711
10	.6180	.7860	1.2719	1.618	1.272	.78622	50						
20	.6202	.7907	1.2748	1.612	1.265	.78442	40						
30	.6225	.7954	1.2778	1.606	1.257	.78261	30						
40	.6248	.8002	1.2808	1.601	1.250	.78079	20						
50	.6271	.8050	1.2838	1.595	1.242	.77897	10						

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

Lat
Ocean View
West 45

85° 44'

83° 16'

78 v 8
10 v 8
68 00

9083866

50

75,4193300

13.04
6.04
9.45
23.53

1285
452
1737

15400
952
14948

26240
25775

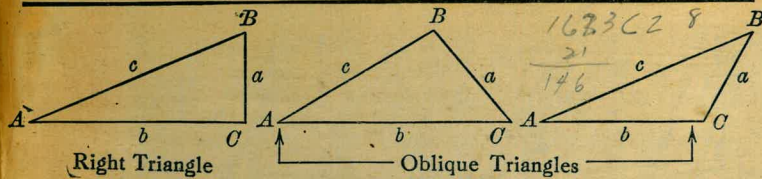


9914024
51
8714024
4590120
45,4615227
320.0
21.2
2366
16.4
410058
2,86155.2

166.97
386
163.11
285
16026
212
13906
2408
786
1422

RT 17.00
RT 17.00
RT 17.00
RT 17.00
RT 17.00

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

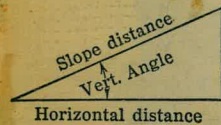
For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\text{cosec} = \frac{c}{b}$

Given a, b	Required A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given A, B, a	Required b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10'. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\cos 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft.

When the rise is known, the horizontal distance is approximately:— the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.