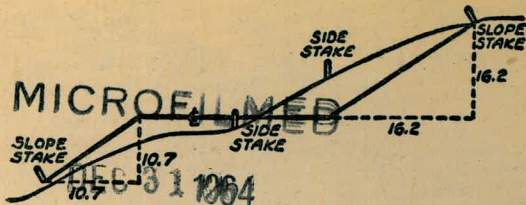


2108

1912



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEXED

to page #49

X-sec. FELSPAR { Events to } Fanuel } 2-8

" Emerald Dawes to Events 9-16

" Dawes - Garnet to Felspar 17-23

" Felspar - Cass to Dawes 24-30

" Felspar - Fanuel to Ingraham 30-49

" { BIK. 32. Normal Hgts 58-60
Also FB 1573.
66

" ALLEY BLOCK 'A' - BELMONT 51-57

FELSPAR

Everts to Fannuel

X-sec. for Imp. W.D. # 31445

7-24-50

Sommermeier

Begg

Acuna

Bunch

INDEXED

YRK

JUL 31 1950

F.B. 1820
30

Tie sheet # 1761

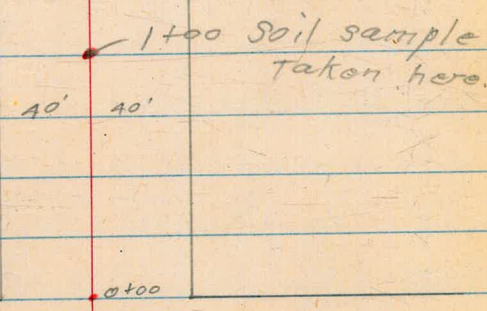
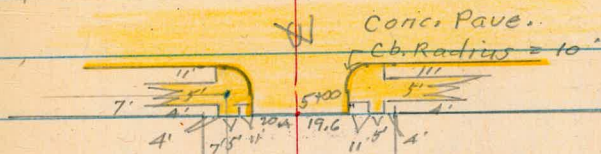
- = Fd. L+T
- ◻ = Fd. 1/2 Hub
- = set Nail

⊙ = Ctr. water meter box

Soil sample from # at 1+00

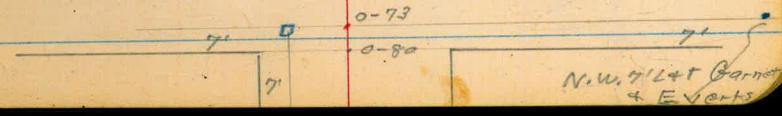
⊕ Fannuel

Felspar



⊕ EVERTS

(unimproved street)



FELSPAR Levels

0419 24 Rt. = (W) 7-24-50

0412 - 27^E Rt. = 15" Eucalyptus

0406 28' Lt. = 6" diam acacia tree

0405 28' Rt. Ctr. Fire Hydr.

26^E Rt. = 5" diam Eucalyptus

0400 = Fly line Everts

(W) = Ctr. water meter box

0-16

0-20

0-400 ♀ Everts

0-80 = wly line Everts

4.98 51.55 1.17 46.57 B.M.#1

8.21 47.74 — 39.53

47.6	46.9	46.3	46.6	46.0	46.6	46.5
$\frac{3.9}{40}$	$\frac{4.6}{18}$	$\frac{5.2}{16}$	4.9	$\frac{5.5}{18}$	$\frac{4.9}{20}$	$\frac{5.0}{40}$

46.9	46.5	46.1	46.3	46.5	46.1	46.0
$\frac{4.6}{40}$	$\frac{5.0}{20}$	$\frac{5.4}{17}$	5.2	$\frac{6.0}{19}$	$\frac{5.4}{25}$	$\frac{5.5}{40}$

46.1	46.2	45.9	45.4	45.1
$\frac{5.4}{40}$	5.3	$\frac{5.6}{13}$	$\frac{6.1}{20}$	$\frac{6.4}{40}$

46.3	45.8	45.3	43.1
$\frac{5.2}{40}$	5.7	$\frac{6.2}{40}$	$\frac{8.4}{140}$

46.4	45.1	45.0	44.4	45.1	44.7
$\frac{5.1}{40}$	$\frac{6.4}{17}$	6.5	$\frac{7.1}{21}$	$\frac{6.4}{23}$	$\frac{6.8}{40}$
		<u>51.55</u>			

Nail in pole #4598 S.W. Cox. Everts + Felspar

N.W.B.P. Garnet & Everts

Felspar

E

4

1+42 - 24 RT. = (W)

1+36 - 25^E RT. = oleander

1+22 - 26 RT. = oleander

Tp. 37² RT1+13 07 6.35 54.59 3.31 48.24

drive.

54.591+09 - 37² RT. = \pm 8' Conc. drive

48.15	48.10	47.75
3.40	3.45	3.80
<u>372</u>	<u>40</u>	<u>79</u>
		at Cor.

1+00

0+92 - 27' RT. = small palm.

0+87 - 24 RT. = (W)

Note { across - E only is shown.
where driveways are level }

49.0	48.4	48.0	48.4	47.7	48.0	47.9
2.5	3.1	3.5	3.1	3.8	3.5	3.6
<u>40</u>	<u>19</u>	<u>18</u>		<u>17</u>	<u>19</u>	<u>40</u>

0+58 37² RT. = \pm 8' wide conc. Dr.

49.40	49.37	49.02
4.15	4.18	4.53
<u>372</u>	<u>40</u>	<u>65</u>
		Cor.

0+50

0+36 27' RT. = 18" Eucalyptus

0+23 - 27' RT. = 14" Eucalyptus

48.2	47.7	47.3	47.6	47.1	47.4	47.1
3.3	3.8	4.2	3.9	4.4	4.1	4.4
<u>40</u>	<u>18</u>	<u>16</u>		<u>18</u>	<u>19</u>	<u>40</u>

51.55

Felspar

5

2+55	40 ⁴ Lt. = \pm 8' wide Conc. Dr.	$\frac{52.6A}{1.95}$ 110 Gar Floor	$\frac{50.96}{3.63}$ 40 \pm					
2+50	25' Mt. = N. end N. + S. lath fence	50.8	50.0	49.6	49.7	49.3	49.6	49.1
2+43	24' Mt. = shrub	$\frac{3.7}{40}$	$\frac{4.5}{19}$	$\frac{5.0}{16}$	4.8	$\frac{5.2}{17}$	$\frac{4.9}{19}$	$\frac{5.4}{40}$
2+08	37 ² Mt. = \pm 8' wide Conc. Drive					49.18	49.08	48.53
2+00	1+96 - 28' Mt. = shrub	50.0	49.7	49.0	49.3	48.9	49.2	48.8
1+92	23' Mt. = \textcircled{W}	$\frac{4.5}{40}$	$\frac{4.8}{21}$	$\frac{5.5}{17}$	5.2	$\frac{5.6}{15}$	$\frac{5.3}{18}$	$\frac{5.7}{40}$
1+65	30' Mt. = shrub					48.64	48.57	48.09
1+59	37 ⁵ Mt. = \pm 8' wide Conc. drive					$\frac{5.95}{37.6}$	$\frac{6.02}{40}$	$\frac{6.50}{65}$ Gar Floor
1+50		49.8	49.0	48.5	48.9	48.3	48.6	48.3
		$\frac{4.7}{40}$	$\frac{5.5}{19}$	$\frac{6.0}{17}$	5.6	$\frac{6.2}{17}$	$\frac{5.9}{20}$	$\frac{6.2}{40}$

54.59

Felspar

±

6

3757 40' Lt. = ± 8' wide Conc. Dr.

52.77	51.58
<u>1.82</u>	<u>3.01</u>
91	40
Gar. floor	

3750

3748 - 22' Rt. = ± N. & S. Hedge

3736 - 23' Rt. = (W)

3711

Rt. = ± 2' wide Conc. drive ribbon

49.99	49.62
<u>4.60</u>	<u>4.97</u>
265	40

3706

Rt. = ± 2' wide Conc. Dr. ribbon

49.97	49.59	49.04
<u>4.62</u>	<u>5.00</u>	<u>5.55</u>
265	40	71
		Bar floor

3700

2799 - 25^s Rt. = N. End N. & S. lath fence

2796 24' Rt. = (W)

2777 21' Lt. = (W)

51.0	50.5	50.0	50.1	49.5	49.8	49.2
<u>3.5</u>	<u>4.0</u>	<u>4.5</u>	4.4	<u>5.0</u>	<u>4.7</u>	<u>5.3</u>
40	20	17		16	18	40

2759

75' Rt. = ± Sing. Cr. Conc. floor

49.03
<u>5.56</u>
75
Gar Floor

54.59

Felspar

7

4+84 35³ Rt. = End E+W. Fence
also = E.N.T.S. board fence

T.P. 4.47 $\frac{54.82}{40}$ 4.24 50.35

4+72 - 23' Rt. = (W)

23' Rt. = end hedge.

35.3 Rt. = start board fence

4+50 23.3 Rt. = E.N.T.S. slat fence

36⁴ Lt. = N.T.S. rail fence

4+43 36³ Lt. = E 11' wide Conc. Drive

+15 23' Rt. = (W)

4+12 23' Lt. = (W)

4+01 36² Lt. = N.T.S. rail fence

{ 23' Rt. also = E.N.T.S. slat fence

4+00 { 23' Rt. = start hedge

3+92 - 22' Rt. = (W)

3+81 - 40' Lt. = E 4' wide Conc. walk

3+74 - 21' Lt. = (W)

3+71 - 29² Rt. = E 2' wide Conc. walk

51.8	51.1	50.8	50.8	50.6	50.9	50.7
2.7	3.4	3.7	3.7	3.9	3.6	3.8
<u>40</u>	<u>20</u>	<u>18</u>		<u>17</u>	<u>22</u>	<u>40</u>

52.26	51.80	51.71
2.33	2.79	2.88
<u>58</u>	<u>40</u>	<u>362</u>

0.71 Dr.

51.5	51.1	50.6	50.5	50.2	50.1
3.0	3.4	4.0	4.0	4.3	4.4
<u>40</u>	<u>20</u>	<u>18</u>		<u>20</u>	<u>40</u>

51.68	51.56
2.91	3.03
<u>50</u>	<u>40</u>

50.14	49.94	49.79
4.45	4.65	4.80
<u>29²</u>	<u>40</u>	<u>50</u>

54.59

See Page 30 Felspar

		9.48	39.54	39.53
3.35	49.02	6.41	45.67	= s.w. 7' Lt
4.11	52.08	6.85	47.97	
Felspar + Fanuel.				
Set. B.M. N.W. 7' Lt.		3.61	51.21	

5+40 = Φ Fanuel.

Cont

5+20 = Wly. cl. line Fanuel

5+10 } $\left. \begin{array}{l} 20\text{ Lt} \\ 19\text{ Rt} \end{array} \right\} = \text{B.C. } 10' \text{ Rad. Cl. Ret.}$

Cont.

$\left. \begin{array}{l} 36' \text{ Rt} \\ 36' \text{ Lt} \end{array} \right\} = \text{back edge of walk}$
 $\left. \begin{array}{l} 31' \text{ Rt} \\ 31' \text{ Lt} \end{array} \right\} = \text{start conc. walk}$

$\left. \begin{array}{l} 20\text{ Lt} \\ 19\text{ Rt} \end{array} \right\} = \text{start curb}$
 5+00 = start Conc. Pav.
 = Wly. line Fanuel

orig B.M. .07 off. Φ
 Garnet + Fanuel 45.60

8

53.58	51.34	50.79	50.19	48.81
1.24	3.48	4.07	4.63	6.01
1.40	4.0		4.0	1.40

53.65	52.90	50.97	49.85	48.88	48.98
1.17	1.92	3.85	4.97	6.94	6.34
1.40	1.40	4.0	4.0	1.40	1.40
cl	G	cl	cl	G	cl

50.38	50.80	50.21	49.84	49.45	50.02	49.19
4.44	4.02	4.61	4.98	5.37	4.80	5.63
4.0	3.0	3.0	3.0	3.0	3.0	4.0
G	cl. E.C.	G	G	G	cl. E.C.	G

50.80	50.20	50.20	49.75	50.31
4.02	4.60	4.62	5.07	4.51
2.05	2.05		1.94	1.94
cl	G		G	cl

51.6	51.42	51.32	50.39	50.47	50.5
3.2	3.40	3.50	4.43	4.35	4.3
4.0	3.62	3.4	3.05	3.55	4.0
	walk	walk	walk	walk	

50.95	50.28	50.53	50.45	50.23	49.98	50.41
3.87	4.54	4.29	4.37	4.59	5.04	4.41
2.03	2.03	1.0		1.0	1.98	1.98
cl	G			G	G	cl

54.82

EMERALD St.

Dawes to Events

X-sec. for Imp.

Sommermeier
Begg
Allen
Bunch

W10.31445

7-26-50

FB. 1795
51

▣ = Fd. 1/2 Hub
● = Fd. disk

Soil sample from 20' RT of 2+50

INDEXED
WJK
JUL 31 1950

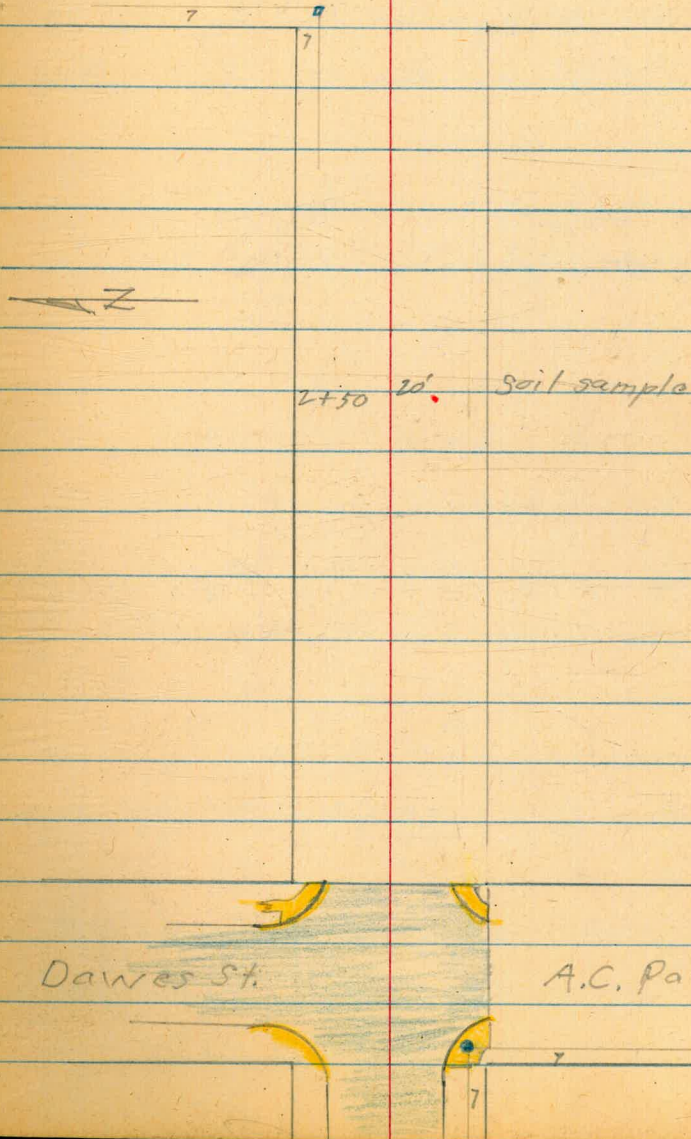
~~INDEXED
JUN 11 1953~~

9

Events

street

Emerald



Dawes St.

A.C. Pave.

Emerald St.
Daws to Events

36° Lt. = N.E. Cor. walk
36° Rt. = S.E. Cor. walk
27° Lt. = ~~end~~ cl. (Comb walk + cl.)
27° Rt. = end cl.

0+00 = Fly line Daws. = End Pave.

40' Lt. = Face cl. Ret.
0-15th 40' Rt. = Start cl. Ret.

0-20 Court

56' Lt. = B.C. 30' Rad cl. Return
0-20 = Fly Curb line Daws

0-40 = ± Daws - 40' Rt. = end of Pave.

T.P. 5.58 50.66 11.20 45.08 B.M.#2
T.P. 3.02 56.28 0.13 53.26 = B.M.#3
6.82 53.39 — 46.57
B.M.#1 P3

	96.3	96.20	95.48	95.6	10
	4.3	4.46	5.18	5.0	
	4.0	36	36	40	
		N.E. Cor. walk	S.E. Cor. walk		
46.09	45.31	45.36	45.65	45.61	45.30
4.57	5.35	5.30	5.01	5.05	5.36
27° cl	27° G	26	13	13	26
					44.91
					44.84
					45.53
					5.82
					278
					G
					5.13
					278
					cl

46.06	45.34	44.65	45.33
4.60	5.32	6.01	5.33
40	40	40	40
cl	G	G	cl

47.06	47.53
2.60	3.13
156	156
cl	G

46.35	45.68	45.44	45.26	45.06	44.94	44.70
4.81	4.98	5.22	5.40	5.60	5.72	5.96
56 cl.	56 G	40	20	20	20	40

47.96	45.66	45.30	.81	42.5
3.20	5.00	5.36	5.85	8.1
140	40	50.66	40	140
			End pave	

S.W. 7' disk Daws + Emerald
Temp. B.M. - Nail in street sign + Emerald

Emerald

0+91. 39.6 LT = ϕ 8' wide Drive

0+72. 27.8 RT = (W)

0+72 39.9 LT = ϕ 3' wide Walk

0+57 ϕ Easterly Ribbon of Drive

0+51 ϕ westerly Ribbon of drive

0+50

0+44 28 RT = (W)

0+18 40.6 RT = ϕ 3' walk

0+05 27.7 RT = F.H.

0+00⁵ - 27⁴ LT = End curb.

99.36
1.30
60
Garage
Floor

98.86
1.80
39.6
 ϕ Dr

98.81
1.85
58
on W.K.

98.55
2.11
39.9
 ϕ W.K.

98.3
2.3
40

97.7
2.9
24

97.0
3.6
22

97.3
3.3
10

97.1
3.5

96.40
46.33
4.33
91.9
on
E Ribbon

4.26
41.9

4.28
50
on dr.

46.35
4.31
50
on drive

96.4
4.2
13

96.2
4.4
18

96.6
4.0
20

96.4
4.2
40

97.7
2.9
40

97.1
3.5
24

96.9
4.2
22

96.7
3.9
13

96.4
4.2

95.9
4.7
13

95.4
5.2
18

95.8
4.8
26

96.1
4.5
40

96.34
4.32
40.6
on
WALK

96.39
4.27
60
W.K.

96.11

4.55
27.4
End of ch.

50.66

Emerald

1797. 40.2 RT = 3' walk

1774 - 28.2 LT = (W)

1766. 40.5 RT = ♀ 8' wide Drive

1758 - 39.8 LT = ♀ 8' wide Drive

1750

T.P. 6.40 54.73 2.33 48.33

1749 39.9 LT = N+S steel fence

1746 39.3 LT = ♀ 7' wide drive

1730 26' RT = (W)

36.7 LT = beginning of cactus plant

1700 39.7 LT = N+S steel fence

12

48.78
5.95
40.2
♀ WK

48.92
5.81
53
ON WK.

47.82
6.51
40.5
♀ DRIVE

48.39
6.34
55
Garage
Floor

49.60
5.13
55
ON Dr.

49.50
5.23
39.8
♀ Dr.

49.3
5.4
40

49.0
5.7
25

48.4
6.3
22

48.3
6.4

47.6
7.1
19

47.9
6.8
25

48.0
6.7
40

54.73

49.53
1.13
60.
ON DRIVE

49.53
1.13
39.3
ON ♀
DRIVE

48.6
2.0
40

48.9
2.2
25

47.8
2.8
22

47.7
2.9

47.0
3.6
19

47.2
3.4
20

46.9
3.7
40

50.66

Emerald

13

2+65, 39.9 LT = \$ westerly Ribbon of Drive

51.98
2.75
60

51.85
2.88
39.9

€

2+57. 25.2 RT = (W)

2+51. 40' RT

2+50

51.3
3.4
40

50.9
3.8
25

49.9
4.8
22

50.0
4.7

50.05
4.68
40
on Dr.
WK.

50.09
4.64
50
on Dr.
WK.

49.3
5.4
18

50.0
4.7
25

50.0
4.7
40

2+31 - 40.0 RT = \$10' Drive

49.70
5.03
40
€ Dr

49.17
5.56
80
on Dr.
€K.

49.85
5.88
Garage
Floor

2+25 27.2 LT = (W)

2+18. 24.5 LT = \$ 3' Stone Walk

50.63
4.10
63
on conc
WK.

50.65
4.08
40
Begin.
conc WK.

50.3
4.4
24.5
€ WK
(Stone)

2+16. 40.1 RT = \$ 10' Wide Drive

2+02 { 28.8 LT = Shrub Tree (2")
40.2 LT = N+S hedge

49.30
5.43
40.1
€ Dr.

49.38
5.35
60
Garage
Floor

2+01. 27.4 RT = (W)

2+00

50.1
4.6
40

50.0
4.7
25

49.2
5.5
22

48.9
5.8

48.3
6.4
18

49.2
5.5
22

48.69
6.04
40

54.73

Emerald

3486 - 40.0 LT = 8' Drive

53.98
0.75
60
Garage Floor

53.68
1.05
40
Dr.

51.45
3.20
36.7
ON WK

51.38
3.35
40
ON WK

51.17
3.56
55
ON WK

3473 - 36.7 RT = 3' Walk

3465 - 28 LT = (W)

3453 - 27 RT = (W)

3450

53.2
1.5
40

52.6
2.1
25

51.9
2.8
22

51.9
2.8

50.5
3.2
18

51.8
2.9
25

51.0
3.7
40

3442 39.9 LT = 2 1/2' wide walk

53.32
1.41
52

53.12
1.61
39.9

3430 - 29.7 LT = (W)

3425 - 27.2 RT = (W)

3400

52.1
2.6
40

51.8
2.9
25

50.9
3.8
22

51.1
3.6

50.7
4.0
18

51.2
3.5
25

50.6
4.1
40

2474 - 40.0 LT = N+S hedge

2470 39.9 LT = E easterly Ribbon Drive

52.08
2.65
60
ON Dr.

51.83
2.90
39.9
ON E Ribbon

54.75

Emerald

A+33 - 29' Lt. = (W)

A+26 39' Lt. = \pm 3' wide Conc. walk

54.51	53.89	53.89
<u>2.94</u>	<u>3.56</u>	<u>3.56</u>
49	40	39.9

A+09 - 40' Lt. = \pm 2' Conc. drive ribbon

54.19	53.79
<u>3.26</u>	<u>3.66</u>
63	40.2

A+04 - 40' Lt. = 2' Conc. drive ribbon

54.23	53.78
<u>3.22</u>	<u>3.67</u>
63	40.4

A+00

53.1	53.0	52.4	52.1	51.8	52.0	51.2
<u>3.7</u>	<u>4.4</u>	<u>5.0</u>	5.3	5.6	5.4	6.2
40	26	22		17	21	40

3+99 - 36.7 RT = \pm Easterly Ribbon Drive

51.49	51.43	51.01
<u>5.96</u>	<u>6.02</u>	6.44
36.7	40	60

3+93 - 36.7^{RT} \pm Westerly Ribbon of Drive

51.53	51.38	51.01
<u>5.92</u>	<u>6.07</u>	6.44
36.7	40	60

T.P. 5.94 57.45 3.22 51.51

57.45

54.73

Emerald

16

check B.M.

7.72 46.57 (46.57)

orig B.M. page 10 (2 B.M. #1 - p-3)

T.R

1.04 54.29

4.20

53.25 (53.26)

Temp

B.M. in street sign - page 10

For intersection see $\frac{FB 1820}{30}$

5+00 = wly line Everts

5A ²	53.5	53.1	52.8	52A	52.0
$\frac{3.2}{40}$	3.9	4.3	4.6	$\frac{5.0}{19}$	$\frac{5.4}{40}$

4+72 38⁵ RT = 4' wide Conc walk

51.95	51.93	51.70
$\frac{5.50}{38.5}$	$\frac{5.52}{40}$	$\frac{5.25}{54}$

4+65 - 25' RT = (W)

53.8	53.2	52.6	52A	51.8	52 ²	51.8
$\frac{3.6}{40}$	$\frac{4.2}{26}$	$\frac{4.8}{24}$	5.0	$\frac{5.6}{19}$	$\frac{5.2}{21}$	$\frac{5.6}{40}$

57.45

X-sec. Dawes Street

Garnet to Felspar 7-27-50
W.O. 31445

Sommermeier
Beeg

Allen

Bunch

Tie sheet #1752

□ = Fd 1/2 hub + Tack

• = Fd L+T

• = set nail

Soil sample

150' N. of N. line Garnet El. top. sample = 35.0

15' East of E Dawes " Bottom of " = 34.0

INDEXED
W.K.
JUL 31 1950

N.W. 7 1/2 → 33° 31' 41.70

Felspar 3409.70 street

↑ Dawes

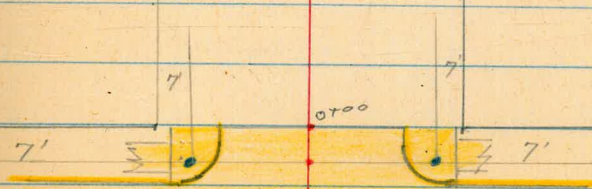
269.70

40'

40'



1450 15' → soil sample



A.C. Paue
Garnet Street

Dawes
Garnet to Felspar

36' Lt. } = Back edge of walk
36' Rt. }

Lt. } = end curb + walk

Rt. } = End curb + walk

0 + 100 = Nly line Garnet = End of Pav

0-04 198 Lt. } = E.C. 10' Rad. Cl. Ret.
Rt. }

0-14 (cont)

30' Lt. } = B.C. 10' Rad. Cl. Ret.
30' Rt. }

0-14 = Nly Cl. line Garnet.

0-40 = † Garnet

T.P. 5.01 37.55 8.76 32.54
1.77 41.30 — 39.53

32.8 32.81 33.78 34.2
4.7 4.74 3.77 3.3
40 36 36 40
walk walk

32.70 32.35 32.75 33.05 33.14 33.00 33.59
4.85 5.20 4.80 4.50 4.41 4.55 3.98
20 20 10 10 198 198
Cl. G Cl. G Cl.

32.63 32.26 32.95 33.47
4.92 5.29 4.60 4.08
20 20 198 198
Cl. E.C. G Cl. E.C.

31.56 31.00 32.45 32.04 33.49 34.18 34.62
5.89 6.55 5.10 5.51 4.06 3.37 2.93
40 40 40 140 140 140
Cl. G Cl. G Cl. G Cl.

32.55 32.18 32.37 32.26 32.41 32.64 32.89 33.44 32.97
5.00 5.37 5.18 5.29 5.14 4.91 4.66 4.11 4.58
30 30 20 16 20 30 30 40 40
Cl. G Cl. G Cl. G Cl. G Cl. G

31.59 32.33 32.14 32.10 32.44 32.89 33.31 34.63
5.96 5.22 5.41 5.40 5.11 4.66 4.24 2.92
140 40 20 10 20 40 40 140
37.55

N.W.B.P. Dawes & Garnet
N.W.B.P. Everts & Garnet

to frame dwelling
 0+57 40^s Rt. = 5'x5' Conc. porch

35.6 36.14
 1.9 1.41
 40 40^s
 porch

0+50

33.9 33.1 33.0 33.6 33.9 33.9 35.3
 3.6 3.4 4.5 3.9 3.6 3.6 2.2
 40 20 14 10 20 40

service station yard.

0+49 - 18^s Rt. = end plant mix

33.80 35.19 35.31
 3.75 2.36 2.24
 18^s 40 45

0+46 41^s Lt. = 1/2 Sing. Car. dirt floor0+40 - 41^s Lt. = end lath fence

0+34 - 37.5 Lt. = Δ in lath fence

0+35 - 44^s Rt. = Cap. + Fill pipe. For ~~under~~0+31 - 39^s Rt. = } underground gasoline0+26 - 44^s Rt. = } tank.

0+25 - 28' Rt. = 1/2 Pole # D-18405T

0+17 38' Lt. = 8' high lath fence

3A.9
 3.6
 41^s
 Floor

(service station yard.)

0+00⁰¹ 19³ Rt. = start plant mix

33.05 33.64 34.93 34.52
 4.50 3.91 3.12 3.03
 19³ 22 40 45

37.55

1+47 29⁸ RT. = ϕ pole # 436677H1+35 = Approx ϕ E+W. alley.

33.8	35.0	35.1	35.6	35.3	36.3	37.6
6.6	5.4	5.3	4.8	5.1	4.1	2.8
140	40	20		17	40	140

1+27

1+26 - 39² Lt. = ϕ pole 505904H1+23 - 45³ RT. = N.W. Cor. Frame Garage.1+22 - 27² Lt. = ϕ pole # 4548

T.P. 4.17 40.48 1.24 36.31

40.48

35.0	35.3	34.8	35.3	34.9	36.0	36.6
5.4	5.1	5.6	5.1	5.5	4.4	3.8
40	20	18		16	18	40

64⁷ RT. = S.E. Cor Frame Gar.64⁷ RT. = N.E. Cor. Apron1+05 45⁷ RT. = S.W. Cor Frame Gar.45⁷ RT. = N.W. Cor Apron

36.67	36.67
0.88	0.88
45 ⁷	64 ⁷
Floor	Floor

1+00

34.7	35.3	33.8	34.6	34.4	35.3	36.1
2.8	2.2	3.7	2.9	3.1	2.2	1.4
40	17	15		16	20	40

64⁷ RT. = S.E. Cor. same.

to double Gar.

0+95 45⁷ RT. = S.W. Cor conc. apron

36.40	36.40
1.15	1.15
45 ⁷	64 ⁷
S.W. Cor.	S.E. Cor.

37.55

2+32 - 39⁸ Lt. = start picket fence

(30⁵ Lt. = ctr. telephone Man hole
2+29 } 39⁸ Lt. = 2' wide Conc. walk

37.08	36.98	36.98
3.40	3.50	3.50
50	40	398

2+15 - 39⁸ Lt. = 3⁵' wide Conc. walk

2+12 - 40² Lt. = end picket fence

37.26	36.98	37.09	37.09
3.22	3.50	3.57	3.59
51	46	40	398

2+00

36.4	36.6	35.6	36.2	35.8	37.4	38.1
4.0	3.8	4.8	4.2	4.6	3.0	2.3
40	18	15		17	20	40

1+95 - 40¹ Lt. = start picket fence

1+92 - 39⁹ Lt. = 3^{wide}' Conc. walk

36.43	36.38	36.38
4.05	4.10	4.10
50	40	398

1+79 - 39⁹ Lt. = 2⁵' wide Conc. walk

36.10	36.05	36.05
4.38	4.43	4.43
50	40	398

1+60

35.5	35.7	35.3	35.6	35.2	36.5	36.9
4.9	4.7	5.1	4.8	5.2	3.9	3.5
40	17	15		17	19	40

40.48

3+30⁷3+09⁷ = \pm Felspar

2+92

2+85

2+72 29⁵ Lt = \pm pole # 82432 H2+69⁷ = sly line Felspar2+67 - 27⁰ Lt = pole # 45982+54 39⁸ Lt = end picket fence.2+50 39⁹ Lt = \pm 3⁵' wide Conc. walk

38.1	38.3	38.7	38.7	38.7
$\frac{2.3}{40}$	$\frac{2.1}{20}$	1.7	$\frac{1.7}{20}$	$\frac{1.7}{40}$

37.9	38.1	38.4	38.5	38.7	40.0
$\frac{2.5}{40}$	$\frac{2.3}{20}$	2.0	$\frac{1.9}{20}$	$\frac{1.7}{40}$	$\frac{0.4}{140}$

37.5	37.3	37.9	38.0	38.1
$\frac{2.9}{40}$	$\frac{3.1}{20}$	2.5	$\frac{2.4}{20}$	$\frac{2.3}{40}$

37.9	38.3	37.0	37.6	37.7	39.0	39.1
$\frac{2.5}{40}$	$\frac{2.1}{19}$	$\frac{3.4}{17}$	2.8	$\frac{2.7}{17}$	$\frac{1.4}{19}$	$\frac{1.3}{40}$

37.4	38.1	36.9	37.2	37.2	38.2	38.9
$\frac{3.0}{40}$	$\frac{2.3}{18}$	$\frac{3.7}{17}$	3.2	$\frac{3.2}{17}$	$\frac{2.2}{19}$	$\frac{1.5}{40}$

37.5 ⁸	37.3	37.4 ²	37.3	36.2	37.0	36.7	38.0	38.9
$\frac{2.90}{50}$	$\frac{3.05}{40}$	$\frac{3.06}{39.8}$	$\frac{3.1}{16}$	$\frac{4.2}{15}$	3.4	$\frac{3.7}{17}$	$\frac{2.4}{18}$	$\frac{1.5}{40}$

40.48

Dawes

N.W. 7 1/2 Hub;
Dawes + Felspar

1.75 38.73 TIP #1

4+30

40.48
0.0

36⁴ RT = 2 ply end N.W.S. board fence

3+49² = Nly line Felspar

38.9	39.1	38.9	38.9	38.7	40.1	40.3
$\frac{1.5}{40}$	$\frac{1.3}{20}$	$\frac{2.0}{16}$	$\frac{1.5}{17}$	$\frac{1.7}{20}$	$\frac{0.3}{20}$	$\frac{0.1}{40}$

38.9	39.1	38.9	38.8	38.7	39.6	40.2
$\frac{1.5}{40}$	$\frac{1.3}{20}$	$\frac{2.0}{16}$	$\frac{1.6}{16}$	$\frac{1.7}{16}$	$\frac{0.8}{21}$	$\frac{0.2}{40}$

3+43

40.48

Felspar St W.O. 31445
Cass to Dawes X-sec. 7-28-50

see P. 17

24

Dawes' St.

unimproved

Sommermeier

Beqq

Allen

Bunch

INDEXED

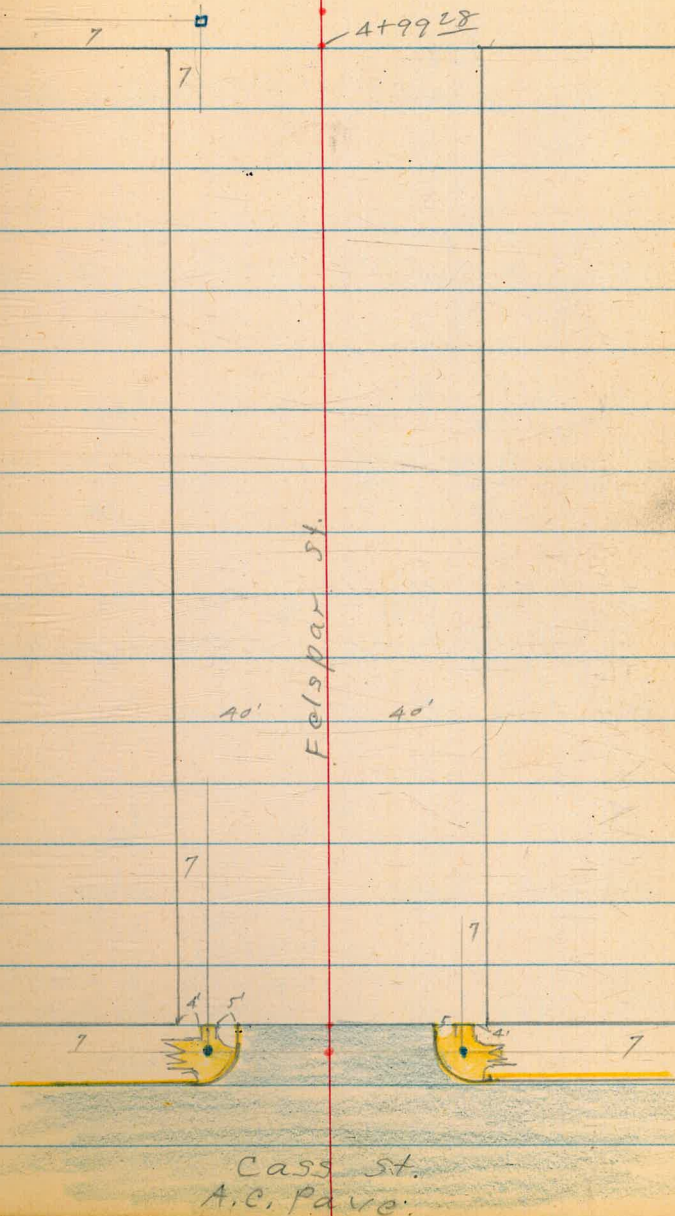
JUL 31 1950

- = Ed. L+T.
- = Ed. 1/4 Hub
- = Nail set

(W) = Ctr. water meter box.

Soil sample taken 200' west of west
line line Dawes + 20' north of Felspar.
started sample 0.7 below Exist. Grd.

where drives are level
across, only is noted.



Felspar.
Cass to Dawes

7-28-50

LT =
North

±

RT =
south

25

0-04 }
26 LT } = E.C. 10' Rad. Cl. Ret.
26 RT }

33.91
4.72 33.12
26 5.57
26 26
cl G

32.39 33.06
6.30 5.63
26 26
G cl

0-115 }
29° RT } 3' x 2' grate
29° LT } = E. grate to cl. inlet.

33.99
4.70 33.01
cl 5.68
29 G
29 29

32.05 33.01
6.64 5.68
G cl
29 29

0-14. Cont.

35.46 34.69
34.07 33.25
3.23 4.00 4.62 5.44
140 140 40 40
G G cl G

32.39 33.06 30.68 31.44
6.30 5.63 8.01 7.25
40 40 140 140
G cl G cl

36' LT }
36' RT } = B.C. 10' Rad. Cl. Ret.
0-14 = Ely. Cl. line Cass

37.07 33.15 33.13 33.45
4.62 5.54 5.56 5.24 5.56
36 36 26 13 5.56
cl G

33.13 32.73 32.28 32.21 33.03
5.96 6.41 6.48 5.63
13 26 36 36
G cl

0-40 = ♀ Cass. (A.C. Pavé.)

35.19 33.80 33.26 32.74 31.10
3.50 4.89 5.43 5.95 7.59
140 40 38.69 40 140

(Bench book shows 32.06 - Use as 32.08)
S.W. 3' tie Back Lt. Cass & Felspar.

B.M.#1 6.61 38.69 6.61 32.08 ✓

T.P. 3.49 38.69 6.10 35.20

2.57 41.30 — 38.73 T.P.#1
A23

Felspar

±

1+33 28' Lt. = (W)
 1+29 39' Lt. = ± 7' wide Concr. Dr.

36.46 36.22 36.22
 4.11 4.35 4.35
 60 40 397

1+20 40' Lt. = ± 2' wide Concr. walk

36.78 36.92
 4.29 4.65
 60 40

1+12 28' Lt. = (W)

1+00

35.8 35.2 34.4 34.8 33.8 34.6 34.2
 4.7 5.3 6.1 5.7 6.7 5.9 6.3
 40 28 16 40.57 24 27 40

T.P. 6.18 40.57 4.30 34.39

0+83 28' Rt. = (W)

0+50 41' Rt. = small tree *ok*

0+05 28' Rt. = F. Hydt.

35.0 34.8 33.8 34.0 33.2 33.9 33.6
 3.6 3.8 4.8 4.6 5.4 4.7 5.0
 40 27 25 25 27 40

0+00 Cont

34.4 34.09 34.07 33.23 33.2
 4.2 4.60 4.62 5.46 5.4
 40 36 31 36 40
 N.E. Cor. S.E. Cor.
 walk walk walk

31 Lt. } = End Concr. walk
 31 Rt. }

26 Lt. } = End Curb.
 Also 26 Rt. }

0+00 = Ely. line Cass. = End Pavc.

34.03 33.30 33.39 33.29 32.98 32.52 33.05 33.15
 4.66 5.39 5.30 5.42 5.71 6.17 5.64 5.54
 26 26 13 13 26 26 31
 6 6 6 6 6 6 N.E. Cor.
 walk

38.69

Felspar

€

27

2+00 Cont.

$$\begin{array}{r} 36.3 \\ 4.2 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 35.69 \\ 4.88 \\ 3.42 \\ \hline 517. \text{ edge walk} \end{array}$$

$$\begin{array}{r} 35.2 \\ 5.3 \\ \hline 40 \end{array}$$
2+00 28³ Rt. = end Hedge
$$\begin{array}{r} 36.1 \\ 4.4 \\ \hline 27 \end{array} \quad \begin{array}{r} 35.5 \\ 5.0 \\ \hline 25 \end{array} \quad \begin{array}{r} 35.8 \\ 4.7 \\ \hline 17 \end{array} \quad \begin{array}{r} 35.1 \\ 4.8 \\ \hline \end{array}$$

$$\begin{array}{r} 34.8 \\ 5.7 \\ \hline 24 \end{array} \quad \begin{array}{r} 35.1 \\ 4.8 \\ \hline 26 \end{array} \quad \begin{array}{r} 35.74 \\ 4.83 \\ \hline 30.5 \end{array}$$

1+96 - 28' Lt. = (W) 35' Lt. = shrub

$$\begin{array}{r} 30.5 \\ 114. \text{ edge walk} \end{array}$$
1+75 25² Rt. = \pm 3' wide N. + S. Conc. walk
$$\begin{array}{r} 35.56 \\ 5.01 \\ \hline 252 \end{array} \quad \begin{array}{r} 35.40 \\ 5.17 \\ \hline 40 \end{array} \quad \begin{array}{r} 35.34 \\ 5.23 \\ \hline 50 \end{array}$$

1+72 - 37' Lt. = shrub. ✓

$$\begin{array}{r} 37.21 \\ 3.36 \\ \hline 85 \end{array} \quad \begin{array}{r} 36.25 \\ 4.32 \\ \hline 40 \end{array} \quad \begin{array}{r} 36.22 \\ 4.35 \\ \hline 39.5 \end{array}$$
1+67 - 39⁶ Lt. = \pm 7' wide Conc. drive

1+53 - 39' Rt. = 5' high shrub. ✓

31' Rt. = start 4' wide E. + W. Conc. walk.

$$\begin{array}{r} 36.1 \\ 4.4 \\ \hline 40 \end{array} \quad \begin{array}{r} 35.1 \\ 4.8 \\ \hline 28 \end{array} \quad \begin{array}{r} 35.0 \\ 5.5 \\ \hline 25 \end{array} \quad \begin{array}{r} 35.4 \\ 5.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 35.3 \\ 5.2 \\ \hline \end{array} \quad \begin{array}{r} 34.4 \\ 6.1 \\ \hline 24 \end{array} \quad \begin{array}{r} 35.1 \\ 5.4 \\ \hline 26 \end{array} \quad \begin{array}{r} 35.20 \\ 5.37 \\ \hline 31 \end{array} \quad \begin{array}{r} 35.12 \\ 5.45 \\ \hline 35 \end{array} \quad \begin{array}{r} 34. \\ 5.6 \\ \hline 40 \end{array}$$
1+58 28⁵ Rt. = start 4' high hedge ✓

29' Rt. = (W)

1+46 - 39² Lt. = \pm 3' wide Conc. walk
$$\begin{array}{r} 36.38 \\ 4.19 \\ \hline 50 \end{array} \quad \begin{array}{r} 36.25 \\ 4.32 \\ \hline 40 \end{array} \quad \begin{array}{r} 36.26 \\ 4.31 \\ \hline 39.3 \end{array}$$

40.57

Felspar

3+00 cont

3+00 31' Lt. = start 5' wide Conc. walk

3

T.P. 5.42 41.88 4.11 36.46

2+61 - 39⁸ Lt. = ~~3~~ 3' wide Conc. walk,

2+50 cont.

2+50 30' Rt. = end 4' wide Conc. walk

2+42 27⁸ Rt. = 3 1/2" diam Cypress ✓

+35 - 27' Lt. = (✓)

+30 28 Rt. = 3 1/2 diam Cypress ✓

2+11 - 40' Lt. = ~~3~~ 3' wide Conc. walk

28

37.1 37.14
 $\frac{4.7}{40}$ 474
 36
 N.W. Cor
 walk

39.0 36.7 36.1 36.4 36.4 35.8 36.2 35.6
 $\frac{4.80}{31}$ 5.1 5.7 5.4 5.4 $\frac{6.4}{22}$ 5.6 6.2
 S.W. Cor
 walk 26 17 24 40
41.88

37.61 37.31 37.31
 $\frac{2.96}{50}$ 3.26 3.26
 40 398

36.9 35.65 35.1
 $\frac{3.6}{40}$ 4.92 5.4
 34 40
 S.E. Cor
 Conc. walk

36.5 35.9 36.1 36.0 35.1 35.7 35.59
 $\frac{4.0}{28}$ 4.6 4.4 4.5 5.4 4.8 $\frac{4.98}{30}$
 15 23 25 N.E. Cor
 walk

36.84 36.67
 $\frac{3.73}{50}$ 3.90
 40

40.57

Felspar

4

29

3+94 39^E RT. = 3' wide Conc. walk

3+87 28' RT. = (W)

3+86 28' RT. = (W)

3+85 - 28' RT. = (W)

3+50 Cont.

Flowers
41' RT. = end yard of shrubs +
3+50 31 Lt. = end 5' wide Conc. walk

3+09 - 28' Lt. = (W)

Flowers
40' RT. = start yard of shrubs +
36^E RT. = 6' high shrub

3+06 28' RT. = (W)

3+01 Cont.

3' board fence on wall

3+01 32^I RT. = 6" wide N.T.S. Conc. wall

36.74
5.14
39^E

36.74
5.14
40

36.53
5.35
50

37.5
4.3
40

37.68
4.20
36
N.E. Cor
walk

4.60
4.28
31
S.E. Cor
walk

37.3
4.5
28

36.5
5.3
26

36.8
5.0
18

36.8
5.0

36.2
5.6
21

36.6
5.2
22

36.3
5.5
40

35.5
6.3
40
End.

35.1
6.7
40
Base
wall

36.4
5.4
40
Top

35.8
6.0
32^I
End

35.2
6.6
32^I
Base
of wall

36.5
5.3
32^I
Top

41.88

Felspar

4

30

TIP #1 - P 23 (38.73)

3.15 38.73

see p-17 for Dawes

4+99²⁸ = Wly line Dawes

4+50

4+13 28' RT. = (W)

4+12 28' RT. = (W)

4+11 28' RT. = (W)

4+06 39' RT. = ± 3' wide N.45. Conc. walk

4+00

39.0	38.9	38.2	37.9	37.5	37.8	37.4
<u>2.8</u>	<u>2.9</u>	<u>3.6</u>	3.9	<u>4.3</u>	<u>4.0</u>	<u>4.4</u>
40	32	21		18	25	40

38.5	38.3	37.5	37.6	37.2	37.1	36.9
<u>3.3</u>	<u>3.5</u>	<u>4.3</u>	4.2	<u>4.6</u>	<u>4.1</u>	<u>4.9</u>
40	27	26		20	22	40

36.96	36.96	36.94
<u>4.92</u>	<u>4.92</u>	<u>5.14</u>
392	40	50

38.1	37.9	37.0	37.2	37.2	36.9	37.1	36.8
<u>3.7</u>	<u>3.9</u>	<u>4.8</u>	<u>4.6</u>	4.6	<u>4.9</u>	<u>4.7</u>	<u>5.0</u>
40	28	26	19		21	24	40

41.88

FELSPAR ST.

Cross section for Imp. No 31445
Fanel to Ingraham.

Sommermeier

8-8-50

Beag

Allen

INDEXED

AUG 11 1950

Soil samples taken

x = Fd. Cross in Conc.

■ = " " Conc. Mon.

□ = Fd. 1/2 Hub

• = Fd. L+T.

• = set. disk in lead plug in conc.

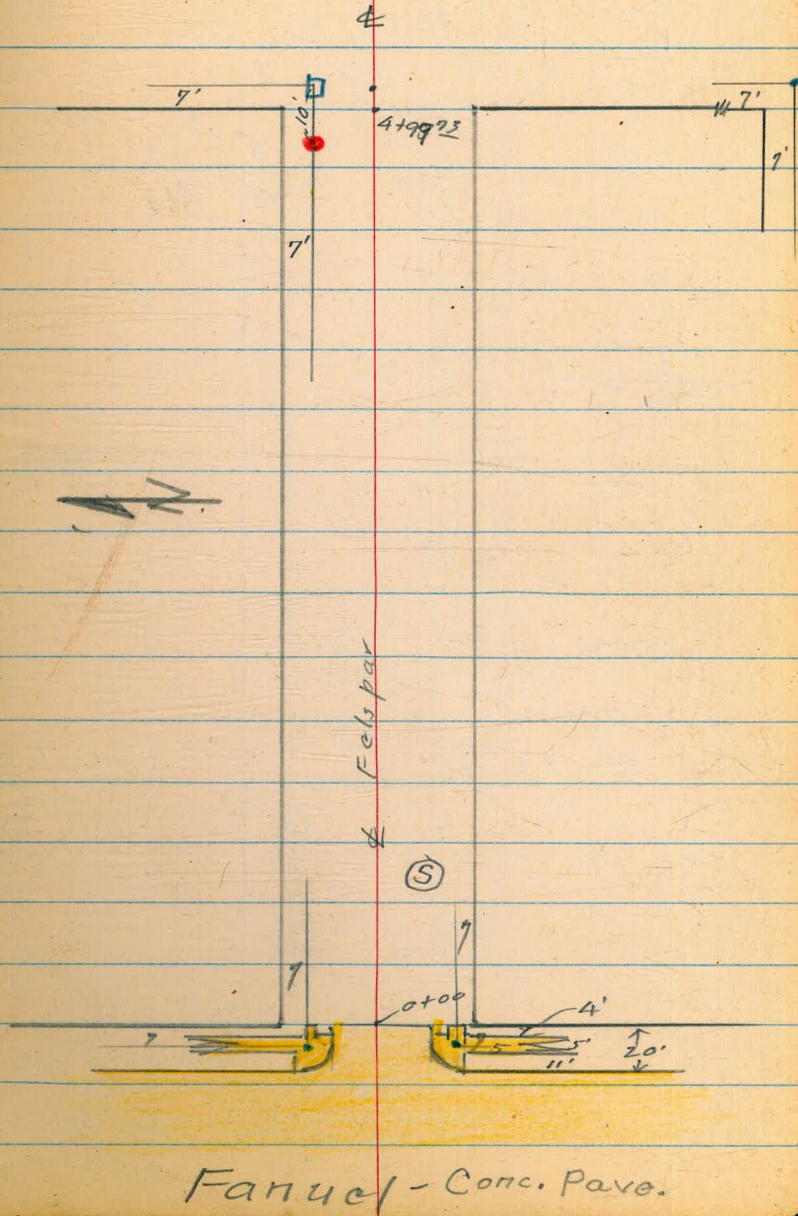
⑤ = Soil sample taken

Ⓜ = water meter box ctr.

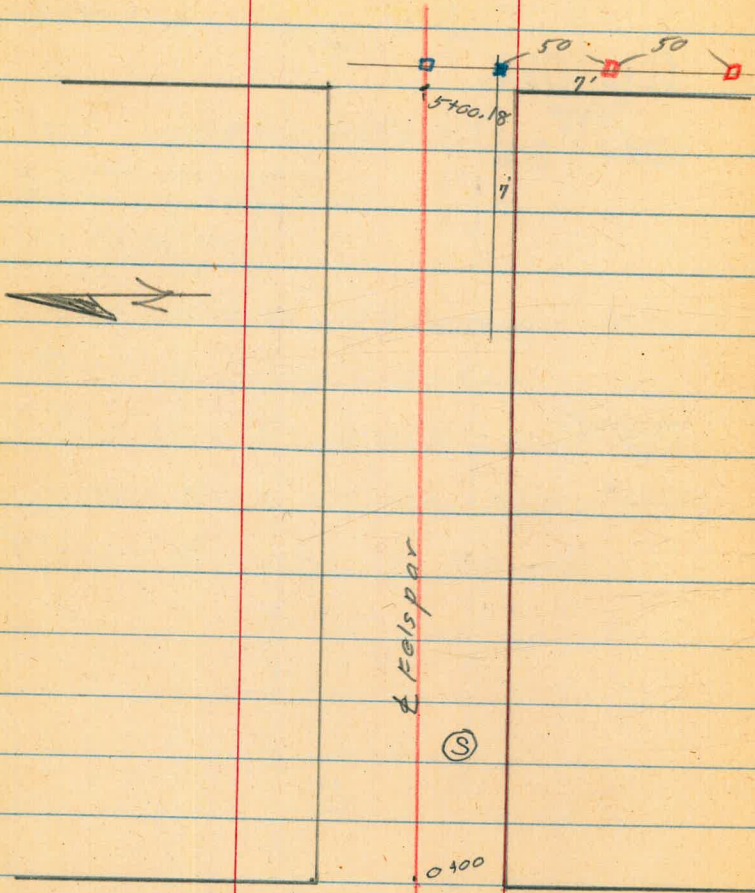
Where Conc. drives are level
across - \notin only is shown.

Grestham
Unimproved

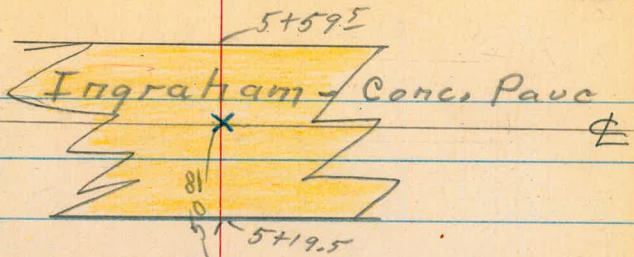
31



Haines Unimproved



Gresham - unimproved



Haines St. Unimproved

Felspar. St.
Sketch - P. 30

(A' walk Runs Nly. + Sly)
property owner

Conc. walk put in by
0+00 - 31' Lt. = start short piece

walk put in by city
This walk is standard
36' Rt. } = End. back edge of walk
36' Lt. }
31' Lt. } = street edge end of walk
31' Rt. }
20' Lt. } = End curbs
20' Rt. }
0+00 = End Pavc.

0-10 20' Rt. } = E.C. 10' Rad cl. Ret
20' Lt. }

0-20 Cont.

30' Lt. } = B.C. 10' Rad cl. Ret.
30' Rt. }

0-20 = Ely. cl. line Fanuel

4,127 55,48

51,21

see pages 2-8

52.35 52.24
3.13 3.24
36 31

52.6 52.35 52.24
2.8 3.13 3.24
40 36 31
N.E. Cor. S.E. Cor.
walk walk

51.31 51.35 51.2
4.17 4.13 4.2
31 36 40
N.E. Cor. S.E. Cor.
walk walk

51.88 51.33 51.41 51.37 51.06 50.53 51.06
3.60 4.15 4.07 4.11 4.42 4.95 4.42
20 20 10 10 20 20 3
cl. G G cl.

51.75 51.12 50.40 51.06
3.73 4.36 5.08 4.42
20 20 20 20
cl. E.C. G cl. E.C.

54.01 53.37 51.97 51.29 50.08 50.83 48.73 49.37
1.47 2.11 3.51 4.19 5.40 4.65 6.75 6.11
140 140 40 40 40 40 140 140
cl G cl G cl cl

51.83 51.10 50.93 50.67 50.36 50.24 51.02
3.65 4.38 4.55 4.81 5.12 5.24 4.46
30 30 20 20 30 30
cl. B.C. G cl. B.C.

55.48

N.W. 7' Lt Felspar & Fanuel - page 8

Felspar

0+90 - 36' Rt. = \pm 7' wide Conc. Dr.

51.75	51.67	51.37
<u>6.03</u>	<u>6.11</u>	<u>6.41</u>
36 =	40	57
		Bar.
		Floor

0+79 - 40' Lt. = \pm 3' wide Conc. Walk

54.17	53.58
<u>3.61</u>	<u>4.20</u>
53	40
at steps	

0+75 - 23' Lt. = (W)

0+59 - 39' Lt. = \pm 7' wide Conc. Dr.

54.30	53.27	53.26
<u>3.48</u>	<u>4.51</u>	<u>4.52</u>
62	40	39.8
Bar. Floor		

0+50 - 39' Lt. = \pm N.W.S. wove wire fence

53.1	52.4	51.7	51.6	51.1	51.7	51.5
<u>4.6</u>	<u>5.3</u>	<u>6.0</u>	<u>6.1</u>	<u>6.6</u>	<u>6.0</u>	<u>6.2</u>
40	23	19		18	20	40
<u>57.78</u>						

0+36 - 22' Lt. = (W)

0+16 - 39' Rt. = Ctr. 24" Diam pine

T.P. 6.15 57.78 3.85 51.63

0+04 cont.

52.70
<u>2.78</u>
40
on walk

N.W. + S.W. conc. walk

0+04 - 31' Lt. = Ely line 4' wide

52.53	52.36	52.3	51.3	51.3	50.7	51.5	51.2
<u>2.95</u>	<u>3.12</u>	<u>3.1</u>	<u>4.1</u>	<u>4.1</u>	<u>4.7</u>	<u>3.9</u>	<u>4.2</u>
36	31	28	19		16	17	40
N.E. Cor walk		S.E. Cor walk					

0+02 } 22' Rt. = (W)
0+01 }

55.48

Felspar

2+58 Cont.

53.07
4.71
65
Car. floor

2+58 39⁸ RT. = 7' wide Conc. drive

54.4	54.2	53.6	53.5	52.8	53.5	53.20	53.20
3.3	3.5	4.2	4.2	4.9	4.2	4.58	4.58
<u>40</u>	<u>18</u>	<u>17</u>		<u>14</u>	<u>15</u>	<u>398</u>	<u>40</u>
						Drive	

2+32 39⁷ RT. = 3' wide Conc. walk

52.90	52.88	52.51
4.88	4.90	5.19
<u>397</u>	<u>40</u>	<u>55</u>
		at porch

2+24 - 22' RT. = (W)

2+00

53.9	53.3	52.8	52.6	52.3	53.0	52.5
3.8	4.4	4.9	4.9	5.4	4.7	5.2
<u>40</u>	<u>18</u>	<u>17</u>		<u>13</u>	<u>14</u>	<u>40</u>

= N. end + E of 3' wide Conc. walk.
34⁴ RT. End of 2' walk also =

1+71 20² RT. = 2' wide Conc. walk

52.52	52.43	52.39	52.35
5.26	5.35	5.39	5.43
<u>20</u>	<u>344</u>	<u>40</u>	<u>56</u>
			at porch

1+59 23' RT. = (W)

1+50

53.4	52.7	52.2	52.3	51.9	52.6	52.0
4.3	5.0	5.5	5.4	5.8	5.2	5.7
<u>40</u>	<u>18</u>	<u>17</u>		<u>13</u>	<u>14</u>	<u>40</u>

1+00

53.2	52.5	51.8	51.8	51.7	52.2	51.6
4.5	5.2	5.9	5.9	6.0	5.5	6.1
<u>40</u>	<u>19</u>	<u>18</u>		<u>14</u>	<u>15</u>	<u>40</u>

57.78

Felspar

3+50 Cont

31' Rt = start ^{conc. walk.} 5' wide E+W.

3+50 17' Lt = start ^{Area.} improved parking

3+27 - 22' Rt. = (W)

3+14 39' Rt. = 3' wide Conc. walk

T.P. 7.53 61.71 3.60 54.18

3+00

2+80 - 40' Rt. = 3' wide Conc. walk.

2+75 22' Rt. = (W)

56.1
5.6
40

55.78
5.93
36
NW. cor.
walk

55.92
5.99
31
S. w. cor.
walk

55.4
6.3
17

54.8
6.9
16

54.6
7.1

53.8
7.9
16.

54.9
6.8
17

54.5
7.2
40

54.54
7.17
39.2

54.54
7.17
40

54.38
7.33
52
At steps

61.71

55.3
2.4
40

54.8
2.9
18

54.0
3.7
17

54.1
3.6

53.4
4.3
15

53.9
3.8
16

53.9
3.8
40

53.44
4.34
40

53.91
4.37
53
At steps

57.78

Felspar.

⊕

4+48 40' Rt. = ⊕ 2⁵' wide Conc. walk

55.96	56.06
<u>5.75</u>	<u>5.65</u>
40	55

4+47 - 20⁸ Lt. = ⊕ 3' wide Conc. walk

57.26	57.16
<u>4.45</u>	<u>4.55</u>
31	208

sly edge of
E+W. walk

4+43 22 Rt. = (W)

4+12 - 40' Rt. = ⊕ 3' wide Conc. walk

55.55	55.55
<u>6.16</u>	<u>6.16</u>
40	55

at steps

4+04 40' Rt. = ⊕ 8' wide Conc. Dr.

55.37	55.03
<u>6.34</u>	<u>6.68</u>
40	60

4+00

56.6	56.56	56.3	55.4	55.3	54.4	55.0	55.1
<u>5.1</u>	<u>5.15</u>	<u>5.4</u>	<u>6.3</u>	6.4	<u>7.3</u>	<u>6.7</u>	<u>6.6</u>
40	31	17	76		15	19	42

sly.
Edge walk

3+82 20⁸ Lt. = ⊕ 3' wide Conc. walk

56.18	55.96
<u>5.53</u>	<u>5.75</u>
31	208

Also S. Edge
E+W. walk

61.71

Felspar

±

38

5+24

56.1	56.4	56.4	56.4	55.9	55.9	55.3
$\frac{6.8}{40}$	$\frac{7.1}{14}$	$\frac{7.1}{13}$	7.1	$\frac{7.6}{18}$	$\frac{7.6}{19}$	$\frac{8.2}{40}$

5+22

57.9	57.7	56.8	56.6	56.2	56.9	56.2
$\frac{5.6}{40}$	$\frac{5.8}{14}$	$\frac{6.7}{13}$	$\frac{6.9}{63.50}$	$\frac{7.3}{18}$	$\frac{6.6}{19}$	$\frac{7.3}{40}$

T.P. 5.41 63.50 3.62 58.09 B.M.#2

N.W. cor. Felspar + Gresham
3' wly. tie back - Nly. 7' line = Disk

4+99⁷³ cont.

57.9	58.17
$\frac{3.8}{40}$	$\frac{3.54}{30}$
	N.E. cor walk

4+99⁷³ { 31' Lt. = end 5' wide E.+W. Concr. walk
(shrubs - trees - grass etc.)
18' Lt. = end improved Area
= wly. line Gresham

58.14	57.4	56.7	56.4	55.9	57.0	56.2
$\frac{3.57}{31}$	$\frac{4.3}{15}$	$\frac{5.0}{14}$	5.3	$\frac{5.8}{19}$	$\frac{4.7}{21}$	$\frac{5.5}{40}$
S.E. cor walk						

4+50

57.3	57.29	56.8	56.1	56.0	55.1	56.1	55.7
$\frac{4.4}{40}$	$\frac{4.42}{31}$	$\frac{4.9}{19}$	$\frac{5.6}{17}$	5.7	$\frac{6.6}{18}$	$\frac{6.6}{19}$	$\frac{6.0}{40}$
S. Edge E+W. walk							
							61.71

Felspar st.

0+48 - 23' Mt. = (N)

0+47 - 23' Mt. = (N)

0+10 Cont.

0+10

0+08 - 39⁵ Mt. = start 8' high Cypress Hedge

0+05 - 23² Mt. = Ctr. Fire Hydt.

= 0+00

5+79⁷³ = Ely line Gresham

5+63

5+60

5+39⁷³ = ~~E~~ Gresham

39

±

64.9	64.8	62.2
<u>+1.4</u>	<u>+1.3</u>	<u>1.3</u>
60	52	49

60.5	59.0	58.7	58.4	58.5	58.3	58.9	58.5
<u>3.0</u>	<u>4.5</u>	<u>4.8</u>	<u>5.1</u>	5.0	<u>5.2</u>	<u>4.6</u>	<u>5.0</u>
40	33	14	13		14	16	40

59.0	58.8	58.6	58.2	58.2	57.9	58.6	58.5
<u>4.5</u>	<u>4.7</u>	<u>4.9</u>	<u>5.3</u>	5.3	<u>5.6</u>	<u>4.9</u>	<u>5.0</u>
40	33	13	12		14	15	40

58.5	58.1	57.9	57.8	57.7	58.2	57.7
<u>5.0</u>	<u>4.8</u>	<u>5.6</u>	<u>5.7</u>	<u>5.8</u>	<u>5.3</u>	<u>5.8</u>
40	14	13		15	16	40

58.0	57.7	57.9	57.6	57.3	57.3	57.9
<u>5.5</u>	<u>5.8</u>	<u>5.8</u>	<u>5.9</u>	<u>6.2</u>	<u>6.2</u>	<u>5.6</u>
40	14	13		15	16	40

60.0	58.1	57.5	56.8	55.4
<u>3.5</u>	<u>5.4</u>	<u>6.0</u>	<u>6.7</u>	<u>8.1</u>
140	40	63.50	40	140

Felspar

1+26 - 40' RT. = 8" wide, N. & S. Conc. wall.

63.7	62.9	64.9
8.1	8.9	6.9
<u>40</u>	<u>40</u>	<u>40</u>
Grd	Base	top
	of wall	

1+23 - 41⁴ RT. = N.E. Cor. Conc. Dr.

63.68	63.58
8.15	8.25
<u>41.4</u>	<u>75</u>

1+15 - 41⁴ RT. = N.W. Cor. Conc. Drive

63.42	63.47
8.41	8.36
<u>41.4</u>	<u>75</u>

1+00 - 25' RT. = (W)

64.1	63.2	62.8	61.9	62.1	62.0	62.4	62.5
7.7	8.6	9.0	9.9	9.7	9.8	9.4	9.3
<u>40</u>	<u>35</u>	<u>13</u>	<u>12</u>		<u>13</u>	<u>15</u>	<u>40</u>

0+76 - 38⁷ RT. = 6" wide N. & S. Conc. wall

61.0	60.6	61.5
10.8	11.2	10.3
<u>38.1</u>	<u>38.1</u>	<u>38.1</u>
Grd	Base	top of wall
	of wall	

Tip. 9.68 71.83 1.35 62.15

71.83

0+58 - 39⁶ RT. = end cypress hedge

61.9	60.6	60.5	59.6	59.9	59.6	60.5	60.0
1.6	2.9	3.0	3.9	3.6	3.9	3.0	3.5
<u>40</u>	<u>34</u>	<u>12</u>	<u>11</u>		<u>13</u>	<u>16</u>	<u>40</u>

0+50

63.50

Felspar

T.P. 6.55 77.09 1.29 70.54

2+56 - 23' RT. = (W)

2+52 - 39' = ± 3' wide Conc. walk

2+50

2+49 - 31' RT. = 6" diam acacia

2+21 - 30' RT. = 14" diam. acacia

2+11 - 52' RT. = ± 3' wide Conc. step

2+00

1+95 - 23' RT. = (W)

1+68 - 23' LT. = (W)

1+59 - 23' RT. = (W)

1+50

1+31 - 40' RT. = ± 3' wide Conc. walk

41

69.7	69.3	68.6
<u>2.1</u>	<u>2.5</u>	<u>3.2</u>
40	15	12

69.13	69.13	68.97
<u>2.70</u>	<u>2.70</u>	<u>2.80</u>
398	40	50
- on walk -		

68.9	69.0	69.5	69.1
<u>2.9</u>	<u>2.8</u>	<u>2.3</u>	<u>2.7</u>
13	20	40	

67.43
<u>4.40</u>
52
Top of step

67.9	67.4	66.6	66.8	66.8	67.0	67.2
<u>3.9</u>	<u>4.4</u>	<u>5.2</u>	<u>5.0</u>	<u>5.0</u>	<u>4.8</u>	<u>4.6</u>
40	15	12		13	16	40

65.9	65.5	64.9	64.4	64.5	64.4	64.8	65.0
<u>5.9</u>	<u>6.3</u>	<u>6.9</u>	<u>7.4</u>	<u>7.3</u>	<u>7.4</u>	<u>7.0</u>	<u>6.8</u>
40	36	14	13		13	16	40

63.87	64.04
<u>7.96</u>	<u>7.79</u>
40	50

71.83

~~4+99 - 40' RT. = end row of Cypress~~4+38 - 39⁵ RT. = £ 3' wide Conc. walk
Cypress (4" to 14" diam.)4+01 - 39⁵ RT. = start row of
4+00

3+50 - 40' RT. = end picket fence.

3+25 - 40⁵ Lt. = start 8' high woven-
- wire fence.3+2A - 39⁷ RT. = £ 3' wide Conc. walk

3+09 - 23' RT. = (W)

3+00 - 40' RT. = start picket fence

2+95 - 39⁸ RT. = £ 3' wide Conc. walk

72.55	72.54	72.49
4.54	4.55	4.60
39 ⁵	40	50

72.5	72.2	71.9	72.1	71.9	72.5	72.5
4.5	4.8	5.1	4.9	5.1	4.5	4.5
40	14	12		14	16	40

72.0	71.7	71.4	71.6	71.5	71.7	71.9
5.0	5.3	5.6	5.4	5.5	5.3	5.1
40	15	13		13	20	40

71.38	71.39	71.53
5.71	5.70	5.56
39 ²	40	53

71.1	70.6	70.1	70.5	70.3	70.6	69.8
5.9	6.4	6.9	6.5	6.7	6.4	7.2
40	14	12		13	20	40

69.78	69.77	69.54
7.31	7.32	7.55
39 ⁸	40	50

77.09

Felspar

⊕

43

5+54

$\frac{70.8}{6.2}$	$\frac{70.8}{6.2}$	70.7	$\frac{70.4}{6.6}$	$\frac{70.3}{6.7}$
$\frac{40}{20}$	$\frac{20}{20}$		$\frac{20}{20}$	$\frac{40}{40}$

5+40¹⁸ ⊕ Haines

$\frac{71.3}{5.7}$	$\frac{71.1}{5.9}$	70.9	$\frac{70.3}{6.7}$	$\frac{69.9}{7.1}$
$\frac{40}{40}$	$\frac{20}{20}$	61	$\frac{40}{40}$	$\frac{140}{140}$

5+22

$\frac{71.6}{5.4}$	$\frac{71.5}{5.5}$	$\frac{71.1}{5.9}$	$\frac{71.0}{6.0}$	$\frac{70.4}{6.6}$	$\frac{70.9}{6.6}$
$\frac{40}{40}$	$\frac{16}{16}$	$\frac{12}{12}$		$\frac{17}{17}$	$\frac{40}{40}$

5+11

$\frac{71.6}{5.4}$	$\frac{71.6}{5.4}$	$\frac{71.2}{5.8}$	$\frac{71.2}{5.8}$	$\frac{70.6}{6.4}$	$\frac{71.5}{5.5}$	$\frac{71.2}{5.8}$
$\frac{40}{40}$	$\frac{13}{13}$	$\frac{11}{11}$		$\frac{17}{17}$	$\frac{19}{19}$	$\frac{40}{40}$

5.88 71.21

Set. B. 1/2 S.W. 7' Conc. Man. Haines & Felspar.

5+00¹⁸ = Wly. line Haines

5+00 23' Lt. = (N)

4+99 - 40' Rt. = End row of Cypress

$\frac{71.7}{5.3}$	$\frac{71.9}{5.1}$	$\frac{71.3}{5.7}$	71.4	$\frac{71.0}{6.0}$	$\frac{71.7}{5.3}$	$\frac{71.5}{5.5}$
$\frac{40}{40}$	$\frac{13}{13}$	$\frac{11}{11}$		$\frac{15}{15}$	$\frac{17}{17}$	$\frac{40}{40}$

4+50

$\frac{72.4}{4.6}$	$\frac{72.3}{4.7}$	$\frac{71.9}{5.1}$	$\frac{72.0}{5.0}$	$\frac{71.8}{5.2}$	$\frac{72.5}{4.5}$	$\frac{72.6}{4.4}$
$\frac{40}{40}$	$\frac{14}{14}$	$\frac{12}{12}$		$\frac{14}{14}$	$\frac{16}{16}$	$\frac{40}{40}$

77.09

Felspar

£

44

1+05 20' RT. = (W)

1+00

0+88- 20' RT. = (W)

0+79- 21' Lt. = (W)

0+58 - 39' RT. = £ 17' wide Conc. Drive

0+50

0+41- 20' RT. = (W)

0+26- 21' Lt. = (W)

0+08 39' RT. = £ 8' wide Conc. Drive

TIP. 4.33 75.08 6.34 70.75= 0+00 } = Ely line Haines
5+80.18 }

5+60

70.5	70.0	69.8	69.9	69.7	70.0	69.7
$\frac{4.5}{40}$	$\frac{5.0}{15}$	$\frac{5.2}{13}$	5.1	$\frac{5.3}{16}$	$\frac{5.0}{18}$	$\frac{5.3}{40}$

69.73	69.73	69.84
$\frac{5.35}{39.2}$	$\frac{5.35}{40}$	$\frac{5.24}{63}$
		Bar. Floor

70.5	70.3	70.0	69.9	69.9	69.7
$\frac{4.5}{40}$	$\frac{4.7}{15}$	$\frac{5.0}{13}$	5.1	$\frac{5.1}{20}$	$\frac{5.3}{40}$

70.04	70.04	70.04
$\frac{5.04}{39.2}$	$\frac{5.04}{40}$	$\frac{5.04}{50}$

75.08

70.6	70.8	70.3	70.7	70.4	70.6	70.1
$\frac{6.4}{40}$	$\frac{6.2}{16}$	$\frac{6.7}{11}$	6.3	$\frac{5.6}{15}$	$\frac{6.4}{20}$	$\frac{6.9}{40}$

70.9	71.2	70.9	70.4	71.4	71.0
$\frac{6.1}{40}$	$\frac{5.8}{20}$	6.1	$\frac{6.6}{20}$	$\frac{5.6}{24}$	$\frac{6.0}{40}$

77.09

Felspar

45

2+40 - 22' RT. = (W)

2+08 - 40' RT. = ± 7' wide Conc. drive

70.19
5.32
40

70.43
5.08
66
Car. floor

75.51

T.P. 5.27 75.51 4.84 70.24

2+00

70.5
4.5
40

70.1
4.9
15

69.8
5.2
13

70.2
4.8

69.5
5.5
13

70.0
5.0
16

69.9
5.1
40

1+95 39' RT. = ± 3' wide Conc. walk.

69.96
5.12
39.8

69.96
5.12
40

69.77
5.31
50

1+75 22' RT. = (W)

1+54 - 39' RT. = ± 3' wide Conc. walk

~~5.12
13~~

69.84
5.24
39

69.83
5.25
40

69.67
5.11
55

1+50

70.2
4.8
40

70.0
5.0
15

69.6
5.4
13

69.8
5.2

69.4
5.6
12

69.9
5.1
15

69.7
5.3
40

1+26 - 21' RT. = (W)

1+12 - 18' RT. = ± 3' wide Conc. walk.

69.83
5.25
18.2

69.62
5.46
40

69.68
5.40
51

75.08

Felspar

3+88 - 37' Lt. = \pm 15" diam. peppertree

3+87 - 21' Rt. = (W)

3+73 - 26' Rt. = 2" diam sycamore

3+58 - 39⁴ Rt. = \pm 8' wide Conc. drive

$\frac{69.88}{5.63}$	$\frac{69.87}{5.64}$	$\frac{69.56}{5.95}$
$\frac{394}{40}$	$\frac{66}{40}$	$\frac{66}{40}$
		Car. floor

3+50

$\frac{71.1}{4.4}$	$\frac{70.1}{5.4}$	$\frac{69.2}{6.3}$	$\frac{69.6}{5.9}$	$\frac{68.9}{6.6}$	$\frac{69.5}{6.0}$	$\frac{69.7}{5.8}$
$\frac{40}{13}$	$\frac{20}{17}$	$\frac{16}{17}$		$\frac{13}{17}$	$\frac{17}{40}$	$\frac{40}{40}$

3+43 - 21' Rt. = (W)

3+09 - 39³ Rt. = \pm 4' wide Conc. drive

$\frac{69.93}{5.58}$	$\frac{69.93}{5.58}$	$\frac{69.73}{5.78}$
$\frac{392}{40}$	$\frac{68}{40}$	$\frac{68}{40}$
		Car. floor

3+00 - 40' Rt. = end picket fence

$\frac{71.0}{4.5}$	$\frac{70.0}{5.5}$	$\frac{69.6}{5.9}$	$\frac{69.9}{5.6}$	$\frac{69.3}{6.2}$	$\frac{69.7}{5.8}$	$\frac{69.9}{5.6}$
$\frac{40}{13}$	$\frac{17}{16}$	$\frac{15}{16}$		$\frac{13}{16}$	$\frac{16}{40}$	$\frac{40}{40}$

2+90 - 21' Rt. = (W)

2+58 - 40³ Rt. = \pm 8' wide Conc. Drive

$\frac{70.19}{5.32}$	$\frac{70.21}{5.30}$
$\frac{403}{66}$	$\frac{66}{66}$
	Car. floor.

2+50 - 40' Rt. = start picket fence.

$\frac{70.8}{4.7}$	$\frac{70.5}{5.0}$	$\frac{69.7}{5.8}$	$\frac{70.1}{5.4}$	$\frac{69.7}{5.8}$	$\frac{70.2}{5.3}$	$\frac{70.0}{5.5}$
$\frac{40}{13}$	$\frac{17}{16}$	$\frac{13}{16}$		$\frac{13}{16}$	$\frac{16}{40}$	$\frac{40}{40}$

75.51

Felspar.

47

4+97

$\frac{70.4}{3.4}$	$\frac{69.4}{4.4}$	$\frac{67.8}{6.3}$	$\frac{67.5}{6.3}$	$\frac{67.3}{6.5}$	$\frac{67.8}{6.0}$	$\frac{68.1}{5.7}$
40	22	14		11	16	40

4+95 - 21' RT = Ctr. Fire Hydt.
wall to east is 15' High
4+86 - 40' RT = step down in wall

$\frac{68.8}{5.0}$	$\frac{68.1}{5.7}$
40	40
End	Base

4+58 - 40' RT = step down in wall
wall to east 25' High

$\frac{69.2}{4.6}$	$\frac{68.7}{5.6}$	$\frac{67.9}{5.9}$
40	40	40
End	Base to west	Base to East

4+50

$\frac{71.0}{2.8}$	$\frac{69.6}{4.2}$	$\frac{68.8}{5.0}$	$\frac{68.9}{4.9}$	$\frac{68.3}{5.5}$	$\frac{69.2}{4.6}$	$\frac{69.2}{4.6}$
40	17	13		9	16	40
			<u>73.83</u>			

T.P. 4.74 73.83 6.42 69.09

4+22 - 37' Lt = Ctr. 18" diam. pepper tree

4+14 - 40' Lt = end 8ft. high fence. woven-wire

4+05 - 21' Lt. = (W)

4+00

$\frac{71.3}{4.2}$	$\frac{69.3}{6.2}$	$\frac{68.8}{6.7}$	$\frac{69.1}{6.4}$	$\frac{68.5}{7.0}$	$\frac{69.1}{6.4}$	$\frac{69.3}{6.2}$
40	19	16		11	15	40

$\frac{69.3}{6.2}$	$\frac{68.3}{7.2}$
40	40
End	Base

3+98 - 40' RT = start conc. wall 5' high, 8" wide

3+95 - 37' Lt = Ctr. 12" diam. pepper tree

75.51

Felspar

±

48

5+39⁵ ± Pauc

$\frac{3.60}{140}$	$\frac{5.88}{40}$	6.40	$\frac{6.86}{40}$	$\frac{8.26}{140}$
70.23	67.95	67.43	66.97	64.57

5+19⁵ = wly edge Ingraham Pauc.

$\frac{4.15}{140}$	$\frac{6.43}{40}$	7.03	$\frac{7.51}{40}$	$\frac{8.71}{140}$
69.68	67.40	66.80	66.32	64.92

5+18

$\frac{5.18}{40}$	$\frac{5.9}{23}$	$\frac{6.8}{18}$	6.9	$\frac{7.3}{20}$	$\frac{6.6}{23}$	$\frac{6.8}{40}$
68.0	67.9	67.0	66.9	66.5	67.2	67.0

5+17⁵ 39⁸ Rt. = Ctr. Pole # 4548

5+06

$\frac{5.18}{40}$	$\frac{6.1}{16}$	$\frac{6.6}{13}$	6.6	$\frac{6.9}{20}$	$\frac{7.2}{40}$
68.0	67.7	67.2	67.2	66.9	66.6

4+99⁷⁵ cont.

$\frac{7.5}{40}$
base of wall

4+99⁷⁵ 40' Rt. = end Conc. wall.
= wly. line Ingraham

$\frac{4.7}{40}$	$\frac{5.0}{22}$	$\frac{6.5}{14}$	6.4	$\frac{6.6}{11}$	$\frac{6.1}{16}$	$\frac{5.7}{29}$	$\frac{6.8}{40}$
69.1	68.8	67.3	67.4	67.2	67.7	68.1	67.0

73.83

Felspar

62.60

±

49

7.04 62.65

B. Plyg gone (EL old B.P. = 62.60)
East and S.E. of Rot. Garnet + Ingratam

T.P. 4.30 69.69 8.44 65.39

X - in Pav
Set. B.M. (5+49.75)
± 6.37 67.46

Cross in pave. ± Ingratam ± Felspar

5+59[±] = Ely edge Ingratam Pav.

70.42	67.93	67.39	66.86	65.46
3.41	5.90	6.44	6.97	8.37
1.40	.40		.40	1.40

73.83

F.A.
D. Smith
J. Hardin
C. Hatch

W0#2077A 50
1-27-51
Pt=North
Pt=South

Survey Proposed Culvert Dead End Plumosa Way

0+60.04
Set Hub

INDEXED
JAN 29 1951

2988

FD 1/2" pipe

0+85

220.3
10.1
10 15.8 10 17.2 10 20.6

0+67

229.5 226.3 222.0 225.5 224.6
6.4 9.6 13.2 10.2 11.3
10 4 6 10

0+60.04

231.7 230.6 228.22 224.2 228.7
4.3 5.3 7.69 6.2 7.3
10 3 4.46 4 10

Reduced by
F.H. 2-5-51

TP3

235.91 1300 235.66

0+34

246.4 243.3 243.3
2.3 5.4 5.4
10 10

TP2 -200

248.66 12.61 250.66

0+09

261.6 258.1 251.7 251.6
1.2 5.3 5.5 5.7
10 4 10

0+07.0

257.65
5.62
5.46

0+00

261.6 257.7 257.3 257.6
1.2 5.6 6.0 5.7
10 5 10

BM

5.21 257.36

see sketch
Chisel # on walk
0.50 South
0.50 West

TP1 030

263.27 8.29 262.97

BM

1.95 274.26

SWBP
Plumosa
Palmetto

Plumosa Way

Plumosa Way

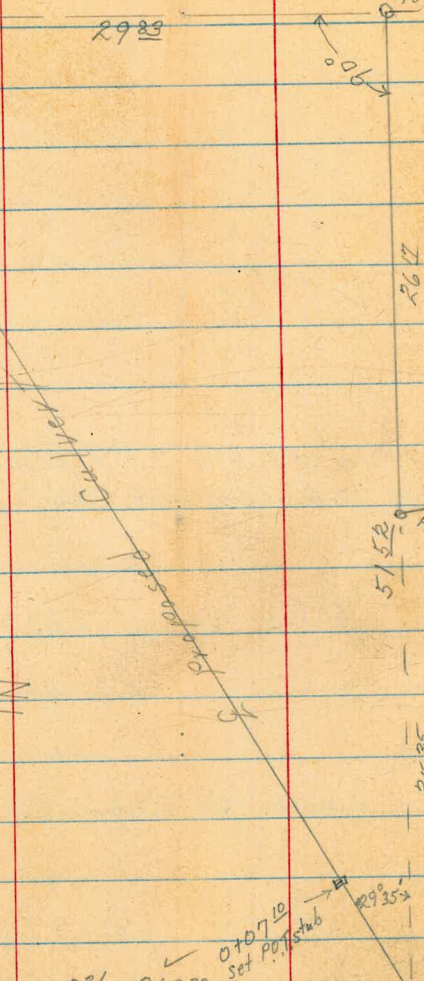
Chisel # BM

Start BM.

TP 5.93 271.51 187 265.58

New BM 10.09 267.45 257.26

Level check

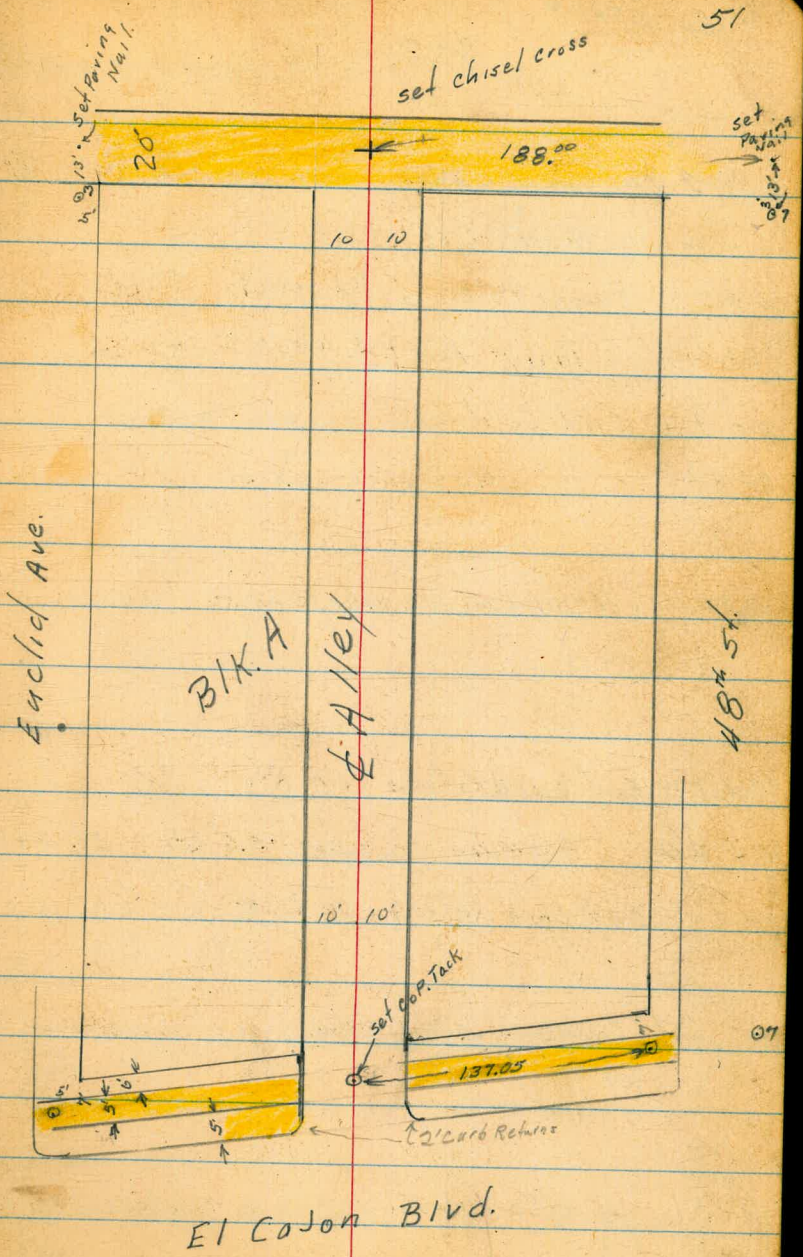


3-6-51
Pope
Clark
Huffman

W.O. 25020

X-Sections Alley
B.K.A Belmont Subdivision
INDEXED

MAR 13 1951



NO. 25020

X-section Alley BIK. A
Belmont Sub

(Note) self Reading Rod was used & All Elevations are Actual

TP

349.98

Lt. = West & Rt. = East

1+00	End conc. Blk. Bldg. Begin conc. Apron 10' Rt.	3496	3503	3500	34992	349.94
0+76	Guy wire 8' Lt.	20	10		10' Edge con. Apron	20.4 Back Apron
0+57	Power Pole J PA 4409 8' Lt.					
0+52	Guy Pole P.A. 4409 8.2 Lt.					
0+47	End Cold Lay	349.40	349.50			
0+42	Guy wire 8.5 Lt.	25	10			
0+28	Begin conc. Blk. Bldg. 10' 28 Rt.	349.35	349.44	349.3	349.5	349.79
		25 Cold lay	10' Cold lay		10	21' Floor El.
0+12	End curb Return on Rt.					
0+00	Gas Main Valve Box 5.5 Lt. El. 348.69				349.28	349.18 349.6
0-12	End curb Return on Left			348.60	9.9 Curb.	9.9 Gutter 25'
0-16.7	Curb Line El Cajon Blvd	349.14	348.80	348.84		
		25' Cold lay Parking Lot	10' Gutter	10' Curb		
		348.57	347.19	348.33	348.19	348.28
		50' Curb.	50' Gutter	10' LIP	10' Edge	349.13
				Conc. Drive	Conc. Drive	348.39
						349.52
						348.85
						50' Gutter
						50' Gutter
						2' Curb. Return
0+51	& El Cajon Ave. shots Taken Parallel To El Cajon	349.92		348.66		349.37
TP		50'				50'
BM = N.W. B.P. Estrella & El Cajon		348.49				351.53

X-section Alley BKA Belmont sub

			Lt. = West		±	Rt. = East	
4450			359.4	359.5	359.5	359.4	359.3
TP		359.71	25	10'		10'	20
4400			359.3	359.3	359.3	359.4	359.4
3+81	Guy Pole A 4441	8.5 Lt.	15	10		10	20
3+80	End Fence	9.7 Lt.					
3+76	Power Pole JPA 4441	8.2 Lt.					
3+50			359.1	359.1	359.2	359.1	
3+07	Begin chicken wire fence	9.7' Lt.	20	10		10'	At Bldg.
3+00			358.7	358.8	358.5	358.9	359.3
			20	10'		10'	20'
2+93	End 4 Car Garage	18.1' Lt.					
					358.00 Floor		
2+62	Begin 4 Car Garage	18.1 Lt.			358.79 Floor		
2+66			357.3	357.3	357.4	358.0	358.2
2+58	Power Pole # JPA 4425	8.2 Lt.	18'	10'		10'	20'
			At Bldg.				
2+50.5	Man Hole ± Alley				357.27 M.H. Rim		
2+30			355.8	356.6	356.5	356.8	357.4
			25'	10		10'	25

X-Section Alley Blk. A Belmont Sub.

Lt. = West



Rt. = East

6+70		360.53 14.1 Floor	359.90 9.7	359.9	360.2 10
6+50	End. 2 Car Garage 12.4 Rt				360.58 12.4 Edge slab
					360.95 22.5 Floor
6+35	Begin 2 Car Garage 12.4 Rt. & 4 Car Garage	360.53 14.3 Floor	360.26 9.9 Edge slab	360.77 12.4 Edge slab	360.97 22.5 Floor
6+30		360.20 15'	360.26 9.9 Edge slab	360.3	360.7 10'
					360.7 20
6+25		360.51 15' Floor	360.31 9.9 Edge slab		
6+00		360.49 Floor	360.33 9.9 Edge slab	360.3	360.4 10
					360.5 20
5+81	Begin conc. Slab 5 Car Garage				
					360.47 15' Floor
5+81	Power Pole #PA. 4465 8.2 Lt.				360.39 9.9 Edge
5+50		359.8 20	359.9 10'	359.9	360.5 10
					360.5 20
5+00					
					359.4 20'
4+57	Power Pole #JPA 4453 8.5' Lt.				359.8 10
					359.5 20

X-sections Alley Blk. A Belmont Sub.

Lt. = West $\frac{1}{2}$ Rt. = East

TP

359.43

8400	End 2 Car Garage 10.3' Lt.	358.84	358.71	359.1	359.4	360.2	360.2
		11.1'	10.3'		8	10	20
		Floor	Edge Apron				
7484	Begin 2 Car Garage 10.2' Lt.	358.91	358.79				
7480	Power Pole # PA 4491 7.8' Lt.	11.1'	10.2'				
		Floor	Edge Apron				
7457	$\frac{1}{2}$ 3' conc walk 12' Rt.	360.85					
		12					
7450		358.7	359.6	359.8	360.1	360.8	
7434	Power Pole JPA 4491 8.7' Lt.	22	10'		10'	15	
Note - Conc. slab runs continuous from 5+81 to 7+30							
7+30	End 4 Car Garage	359.77	359.53				
		17.5'	9.5'				
		Floor	Edge slab				
7+11		359.78	359.63				
		17.5	9.5				
		Floor	Edge slab				
7+06	3' conc. walk 12' Rt.	360.79					
7+00		359.80	359.70	360.0	360.3	360.3	
		17.5	9.5	$\frac{1}{2}$	10	20	
		Floor	Edge slab				
6+81	Low Spot In slab - Begin 4 Car Garage Power Pole # PA 4473 8.8' Lt.	359.77	359.70	359.68			
		17.5	17	9.7			
		Floor	At Bldg.	Edge slab			

X-section Alley Blk. A Belmont sub.

Lt. = West † Rt. = East

BM N.W. B.P. Estrella & El Cajon ^{.05}
 351.53
 T.P. 354.50
 T.P. 358.43

8+91.15 † Existing conc. Alley

356.46 357.77 358.06 358.35 358.97
 50 10' 10 50

8+81.15 Sly. Edge Existing conc. Alley

357.74 356.71 358.99 358.01 358.33 358.63 359.25
 50 50 10' 10' 10' 50
 Top Wall Bottom Wall Top Wall Bottom 6" Conc. Ret. Wall

8+77 End 1 Car Garage Apron

359.62 359.57 359.2 359.7 360.3
 12.4 10.4 10 20
 Floor Edge Apron

8+70 Begin 1 Car Garage Apron

359.67 359.61
 12.3 10.3
 Floor Edge Apron

8+50 Guy Wire 7.4 Lt.

359.3 360.3 359.6 360.1 360.1
 20' 10' 10' 20'

8+31 Power Pole # JPA 4493 8' Lt.

Additional notes E. & W. Alley
Blk. 32 Normal Hqts.

9-18-51

See P.B. $\frac{1573}{66}$

C.H.S.
Boggs
Oltman

stationing same as in EB 1573-66

start of alley at
3+56± 7² = sly. edge drive at

also = start drive (E. & W.)
3+42 - 7⁵ Rt. = end Gar. (west front.)

also = start frame Gar. west front.

3+22 - 7⁶ Rt. = end picket fence

2+61^E - 7⁰ Rt. = start picket fence

2+61 - 7⁹ Rt. = end wire fence.

1+66 - 7⁸ Rt. = start wire fence.

1+33 - 7⁹ Rt. = end house

1+13 - 8' Rt. = start house

0+94 { 7⁵ Rt. = end Conc. slab.
7³ Rt. = end wire fence

{ 7⁵ Rt. = start Conc. slab
0+61 { 7² Rt. = start wire fence

INDEXED

SEP 19 1951

58

389.46
77
drive

370.21 390.2A
76 16E
Floor + & door.
drive on floor

389.55 388.52
7E 77E

389.38 389.40
.75 176

Additional Notes

N. + S. Alley - BIK 32

Normal Hgts

Stationing same as in F.B 1573-66

1+73 - 8² Rt = start board fence.

1+50 - 8² Rt = end board fence.

1+00 - 8² Rt. = start board fence.

0+98 - 9⁵ Rt. = end conc. apron.

0+81 - 9⁵ Rt. = start Conc. Apron.

0+78 - 7² Rt. = end board fence.

7⁶ Lt = end wire fence.

0+50 { 7² Rt. = start board fence
end wire fence

0+46 - 7² Rt. = start wire fence

0+44 - 7² Rt. = end conc. apron

0+28 - 7² Rt. = start. ^{Double Bar} conc. Apron to

0+26 - 7⁸ Rt = end wire fence.

0+13 - 7⁸ Rt = start wire fence

0+06² - 7⁶ Lt. = start wire fence.

Indexed

59

389.90

9⁵
Apron

389.85

9⁵
Apron

390.07

11⁵
Bar floor

389.97

7²

389.95

7²
Apron

390.20

11²
Bar floor

+ conc drive
5+50⁵ 7¹/₂ Lt = end wire fence.

5+20 7²/₂ Lt = end conc drive

7⁸/₂ Lt = start wire fence

4+98 7¹/₂ Lt = end north front Gar.

dirt floor - conc. drive

4+80⁸ { = start North front Frame Gar.
= end stucco shed

7²/₂ Lt = start stucco + frame shed

4+70⁵ 7¹/₂ Lt = end double Gar

South front dirt floor

4+50 - 7⁸/₂ Lt = start double Gar.

4+15 8⁵/₂ Lt = A in fence.

2+50 { 8⁵/₂ Lt = start picket fence.
8⁸/₂ Lt = end board fence.

shed shown ^{is gone.} in orig. notes

2+37 8²/₂ Lt = start board fence

1+99 8²/₂ Lt = end board fence.

373.88
7.9 on drive

394.14 394.46
12 7⁸/₂
Floor drive

393.4
15
dirt floor

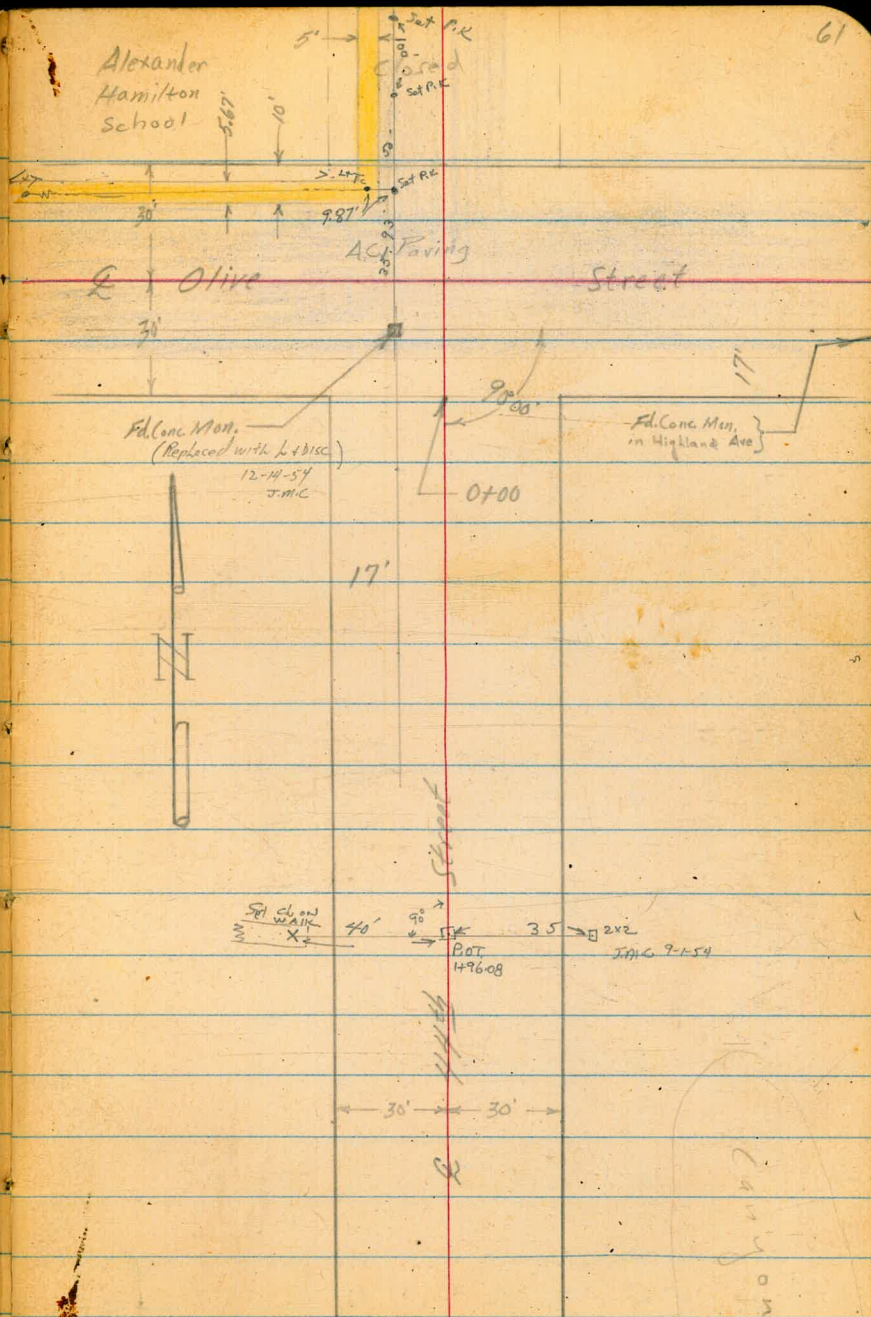
Roberts
Cota
Moore
Marble
6-10-53
W.A. # 32369

X-Section #44 Street
From Olive Stly to Canyon

T.P.3619

INDEXED
JUN 11 1953

Revised
Illustration
6-16-53



0+00 { 30' Lt begin conc. Edn for future wall
South Line Olive Street

296.2	296.3	296.0	296.4	296.1	296.1	296.0	296.1	296.5
5.7	5.6	5.9	5.5	5.8	5.8	5.9	5.8	5.4
50	30 Top	30 Foot	30 GRD	15		15	30	50

0-10 Rough Edge A.C. Paving

295.10	296.31	296.25	296.40	296.68
6.83	5.22	5.68	5.53	5.25
100	50		50	100

0-30 ± Olive

295.55	296.44	296.44	296.47	296.48
6.38	5.49	5.49	5.46	5.45
100	50		50	100

0-50 North Curb Line Olive

295.8	296.7	296.7	296.69	296.69	296.35	296.54	296.20	296.47	296.01	295.28
6.1	5.2	5.2	5.24	5.24	5.58	5.37	5.73	5.46	5.92	5.15
100	50	30	152		172	172	30	30	100	100
					6.44	6	6.44	6	6.44	6

Set TBM { Conc. Mon. }
Olive & 4th 5.85 296.08

0-60 North Line Olive Street

297.3	297.3	297.01	296.74	296.72	297.0
4.6	4.6	4.92	5.19	5.21	4.9
30	24		172 walk	222 walk	30

T.P. 6.48 301.93 K 6.98 295.45

301.93 A

BM 424 301.43

SEB.P.
297.19 Fairmont & Quince

1796 √29' Rt Q 3 1/2' Conc Walk

29446
2.68
294
conc

29469
2.45
394
conc

1792 278' Lt to center 30" Pepper Tree

29444
2.7
302
QED

29444
2.7
302
Foot

292.8
40.3
302
Top

1775 √30' Rt begin Conc Blockwall

29208
5.06
394
conc

29205
5.09
294
conc

1764 √29' Lt Q 4' Conc Walk

29441
2.53
298
conc

29474
2.40
398
conc

1754 √29.5' Rt Q 3' Conc Walk

291.7	292.0	292.5	292.2	292.8	293.1	294.1	294.6
54	51	46	49	43	40	30	25
40	30	17	15		17	30	40

√1737 29' Rt Q 10 1/2' Conc Drive

29415
2.79
29
conc

29444
2.70
30
conc

29483
2.31
40
conc

1729 27' Lt to center Pepper Tree (24")

29714 X

29714 X

TP 3.88 288.39A 12.63 284.51

3+00

286.5	286.7	287.4	287.5	288.1	289.3	290.1
10.6	10.4	9.7	9.6	9.0	7.8	7.0
40	30	11		22	30	40

2+75 30[±] RT End Conc Block wall

291.2	290.7	293.8
5.9	6.4	3.3
30 [±] GRD	30 [±] Foot	30 [±] Top

2+50

290.8	291.4	291.7	290.9	291.8	292.1	291.8	292.2	292.5	292.8	293.3
6.3	5.7	5.4	6.2	5.3	5.0	5.3	4.9	4.6	4.3	3.4
40	30	25	23	20	12	10		18	30	40

2+46 28[±] RT 6 3' Conc Walk

295.4	293.6
3.60	3.53
28 [±] Conc	38 [±] Conc

2+25

30[±] RT End Conc Block wall
29[±] RT Begin Conc Block wall

291.5	292.0	292.1	291.4	292.6	292.9	292.6	293.1	293.4	293.9	293.3	294.4	293.6	294.1	293.9
5.6	5.1	5.0	5.7	4.5	4.2	4.5	4.0	3.7	3.2	3.8	2.7	3.5	0	3.2
40	30	25	23	20	13	11		18	29 [±] GRD	29 [±] Foot	29 [±] Top	30 [±] Foot	30 [±] Top	40

2+00

291.7	292.1	292.4	291.5	292.5	292.7	292.6	293.2	293.5	294.4	294.7
5.4	5.0	4.7	5.6	4.6	4.4	4.5	3.9	3.6	2.1	2.4
40	30	24	22	19	14	13		18	30	40

29714A

29714A

No Points found at $44\frac{1}{2}$ and Maple - Tie Point. Distance Used!

For Extension of sections to Maple See Next Page.

check 410 297.19 = 297.19

T.P. 5.90 301.29 4.81 275.49

T.P. 12.33 300.30 0.42 287.97

4450

277.0

11.4

4400

257.4	269.1	272.1	273.3	277.2	278.5	283.1	284.5
31.0	19.3	16.3	15.1	11.2	9.8	5.3	3.9
63	40	30	15		10	30	40

Bottom

3475

272.9	278.0	279.5	281.2	282.3	284.2	285.4
15.5	10.4	8.9	7.2	6.1	4.2	3.0
50	30	11		18	30	40

3450

280.7	281.2	283.1	285.6	287.2
7.7	7.2	5.3	2.8	1.2
50	30		30	40

288.39

288.39

Robert
6-19-53

Cont'd from Page 66
Extend Sections to Maple

5+20 21° Rt to center 2-4" Acacia Trees

5+09 17° Rt to center 3" Acacia Tree

5+00 25° Rt to center 12" Euc. Tree

4+94 17° Rt to center 5" Euc. Tree

4+82 24° Rt to center 8" Acacia Tree.

4+78 18° Rt to center 3" Acacia Tree

4+68 19° Rt to center 8" Euc. Tree

(Not showing saplings.)

4+54 21° Rt to center 8" Euc. Tree

4+50

T.P. 0.69 284.69 π 12.99 284.00

TBM 0.91 296.99

Cont. Mon.
Olive #44

Lt

67

264.0

20.7

50

271.1

13.6

30

276.6

8.1

8

277.7

7.0

8

282.7

2.0

30

283.0

1.7

40

262.4

22.6

50

261.2

13.5

30

277.0

7.7

14

272.3

7.4

14

281.7

3.0

30

284.0

0.7

40

284.69 π

Check 0.60 296.06 = 296.08

T.P. 12.17 296.66 0.20 284.49

South Line of Maple plus 20° feet South. 45° Rt to Northeast Corner House

289.0
+4.3
45
Floor

Sly. Line Maple

269.1 272.8 278.8 280.7 280.3 282.2 283.3 287.5
15.6 11.9 5.9 4.0 4.4 2.5 1.4 12.8
50 30 5 20 21 30 80

£ Maple Street

268.3 272.7 275.6 278.3 282.9 285.4 288.3
16.4 12.0 9.1 6.4 1.8 10.7 13.6
50 30 15 20 50 100

6+00.30 Nly Line Maple Street
Tie point Distance Used

277.6 272.1 265.1 272.7 274.0 277.9 281.2 283.7 287.8
37.1 22.6 19.6 12.0 10.7 6.8 3.5 1.0 13.1
100 74 62 30 25 11 30 80

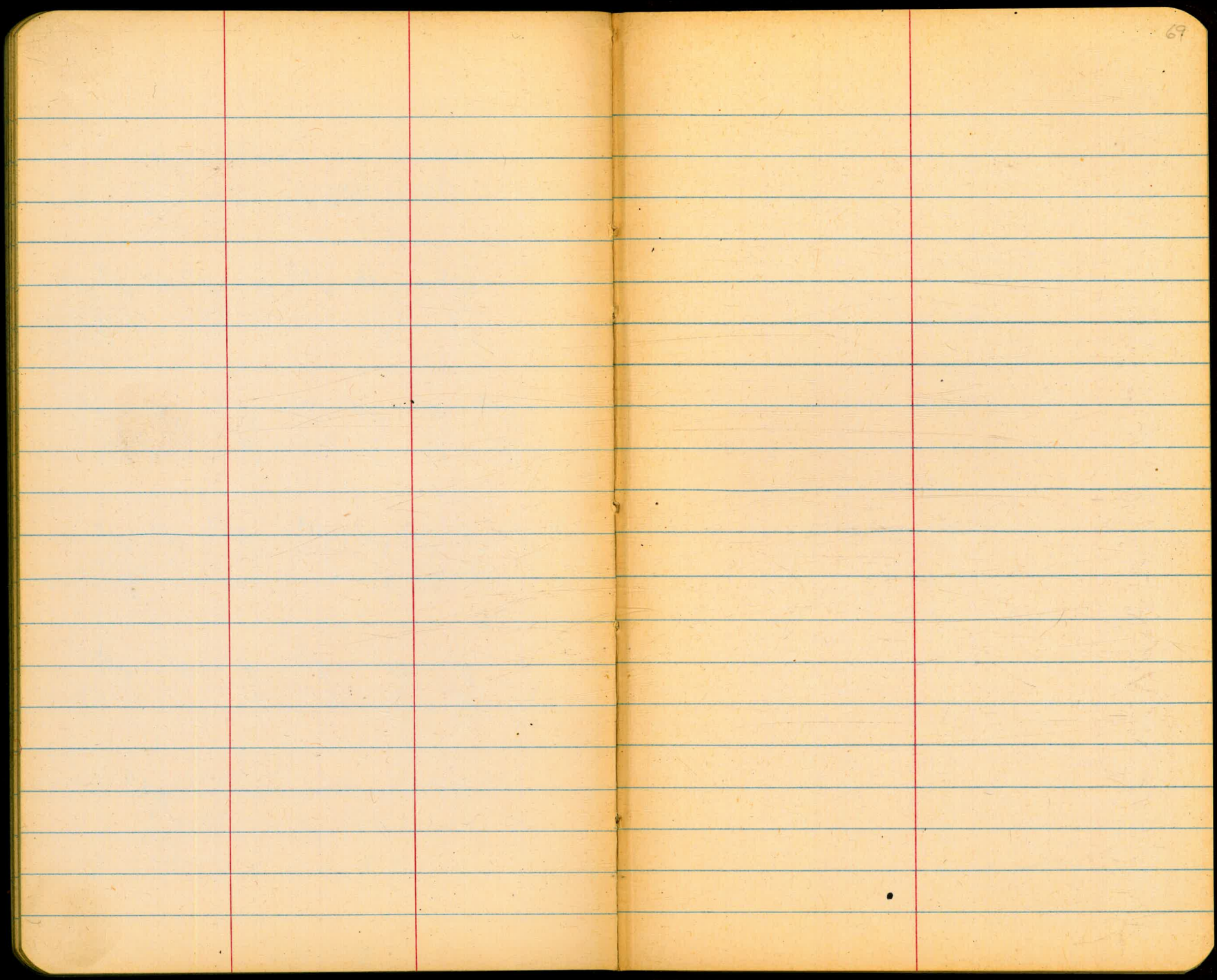
Not Bottom

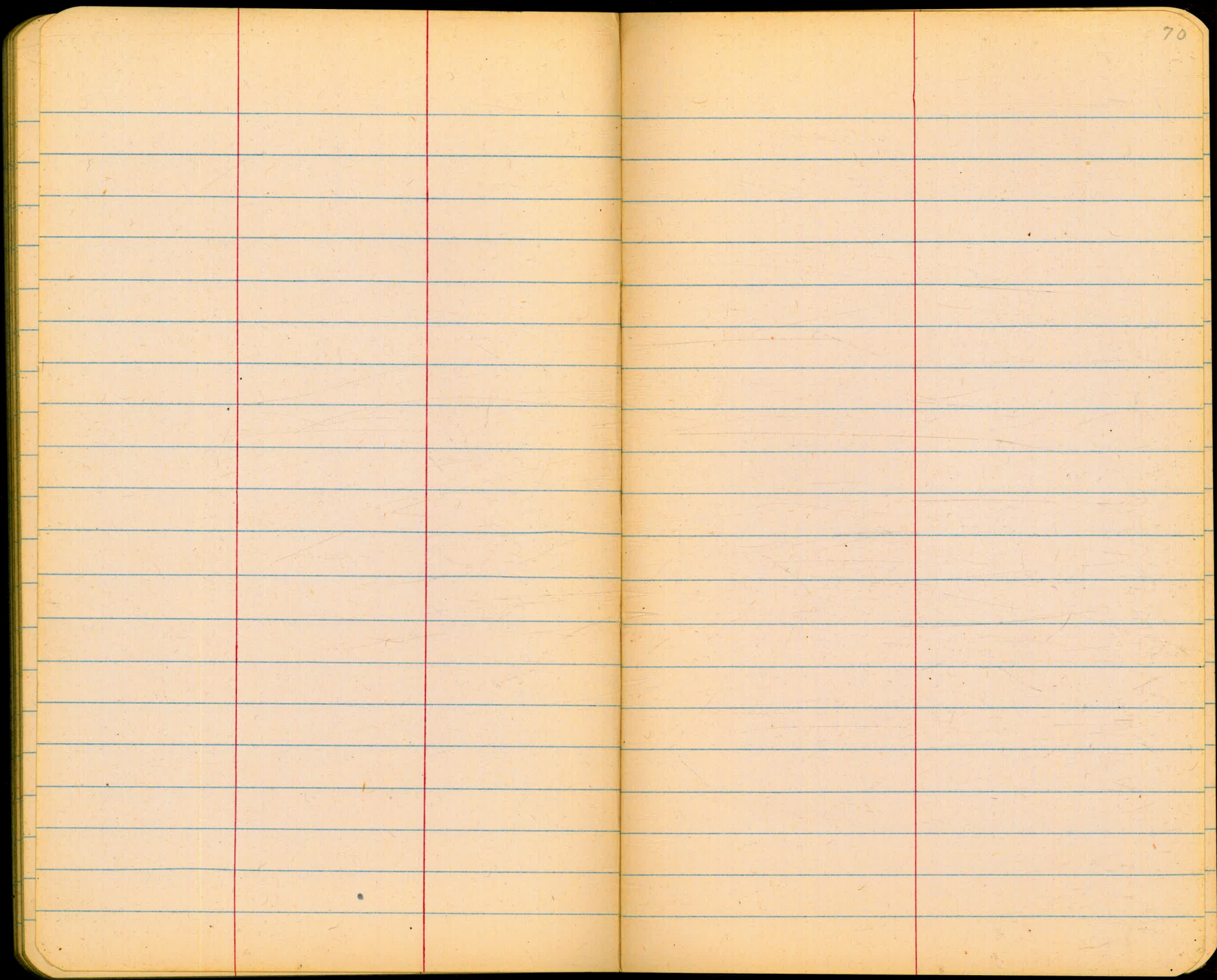
5+50

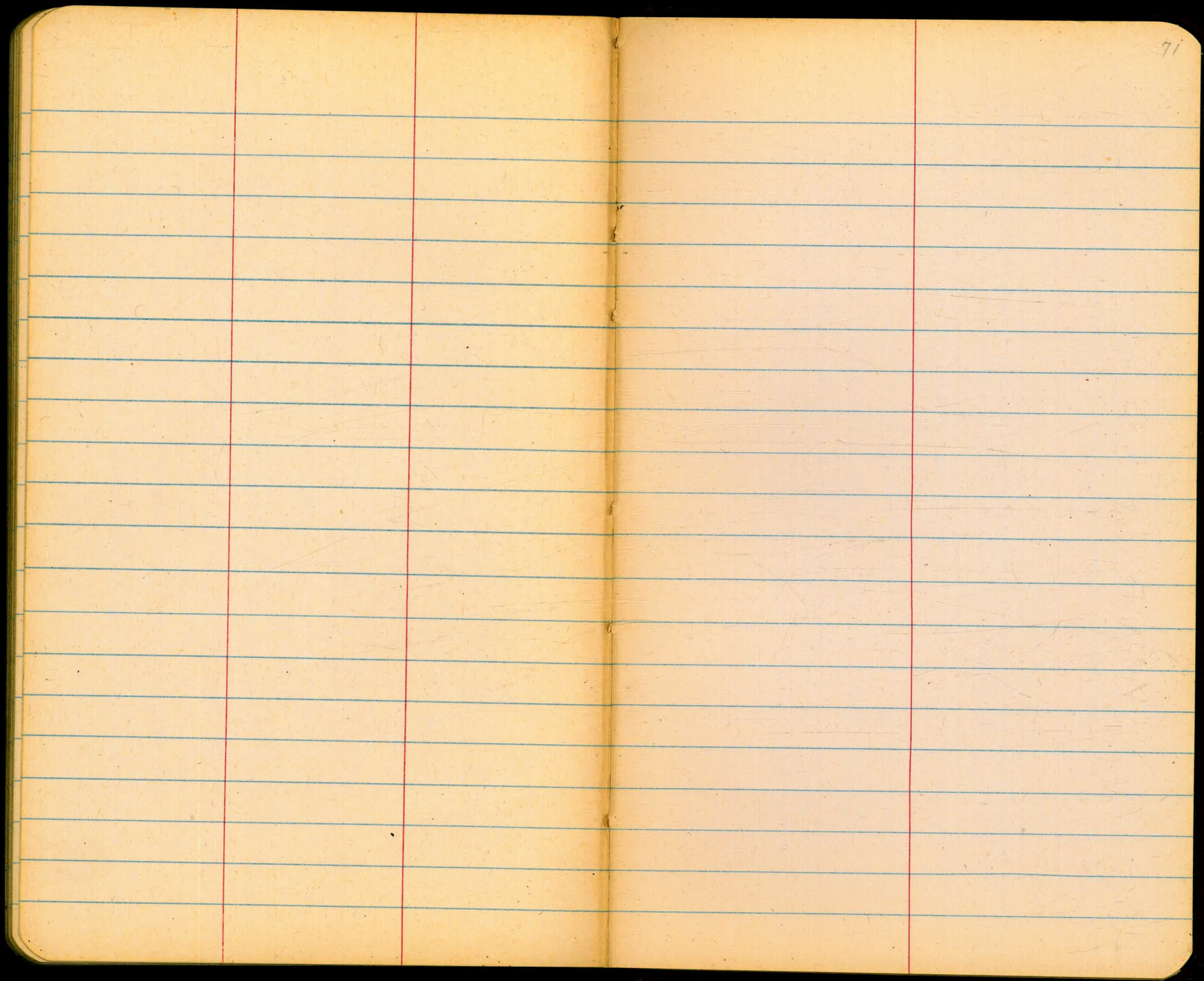
269.1 271.9 275.1 276.7 280.6 283.2 283.6
15.6 12.8 9.6 8.0 4.1 1.5 1.1
50 30 15 18 30 40

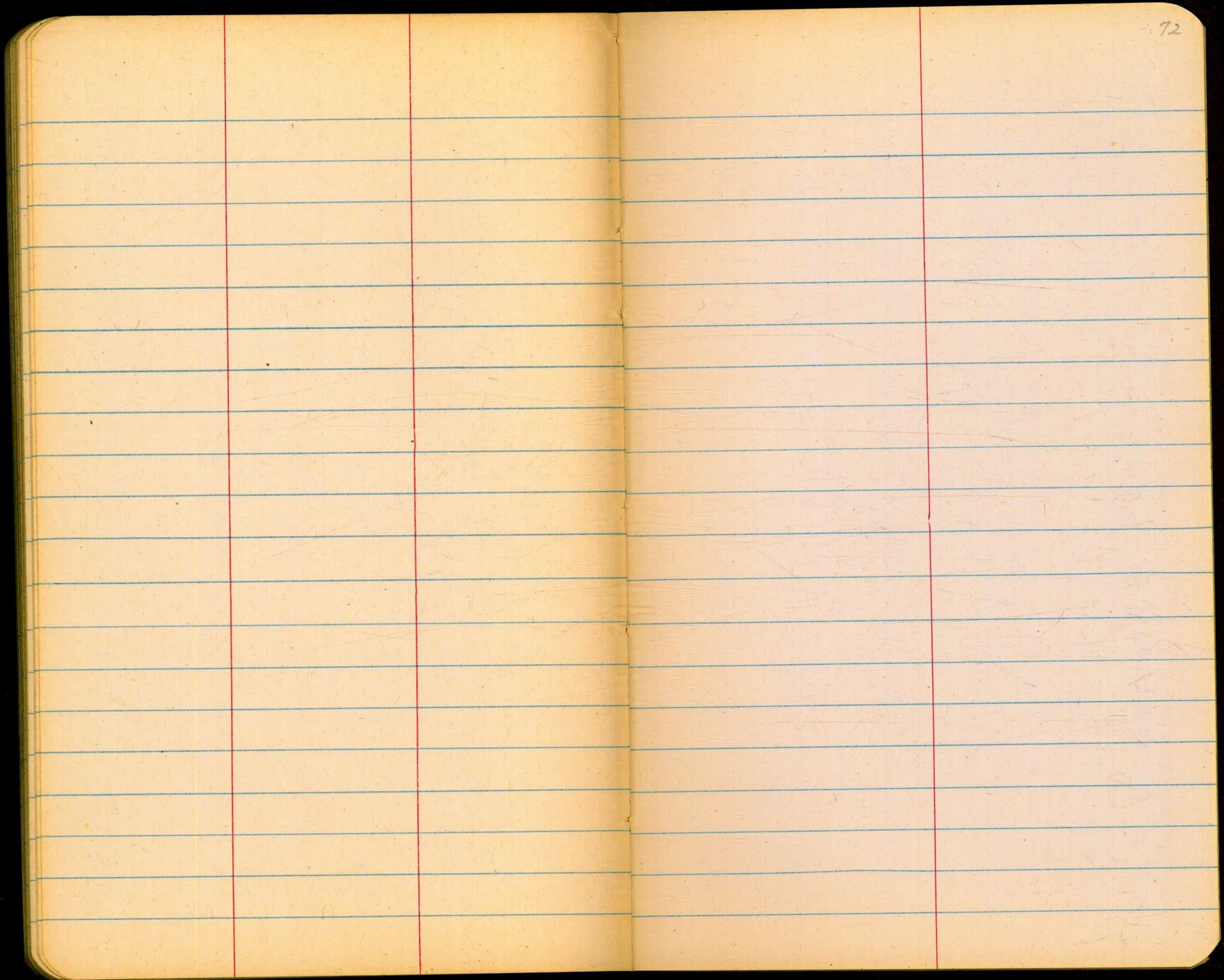
5+41 } 22° Rt to center 4" Acacia Tree
49° Rt to Northeast Corner of House
5+28 } 21° Rt to center 8" Euc. Tree

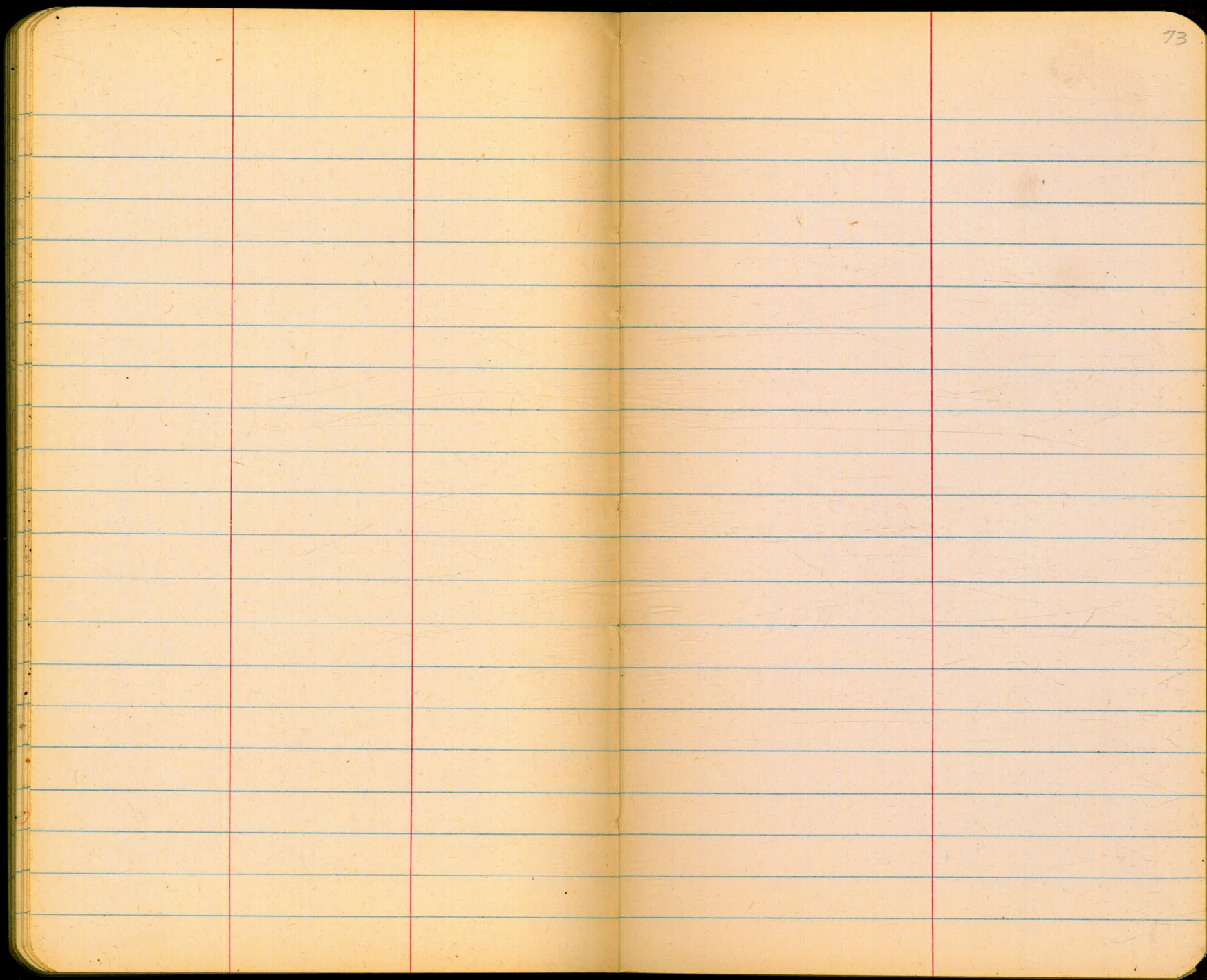
287.5
+2.8
49.5
Floor



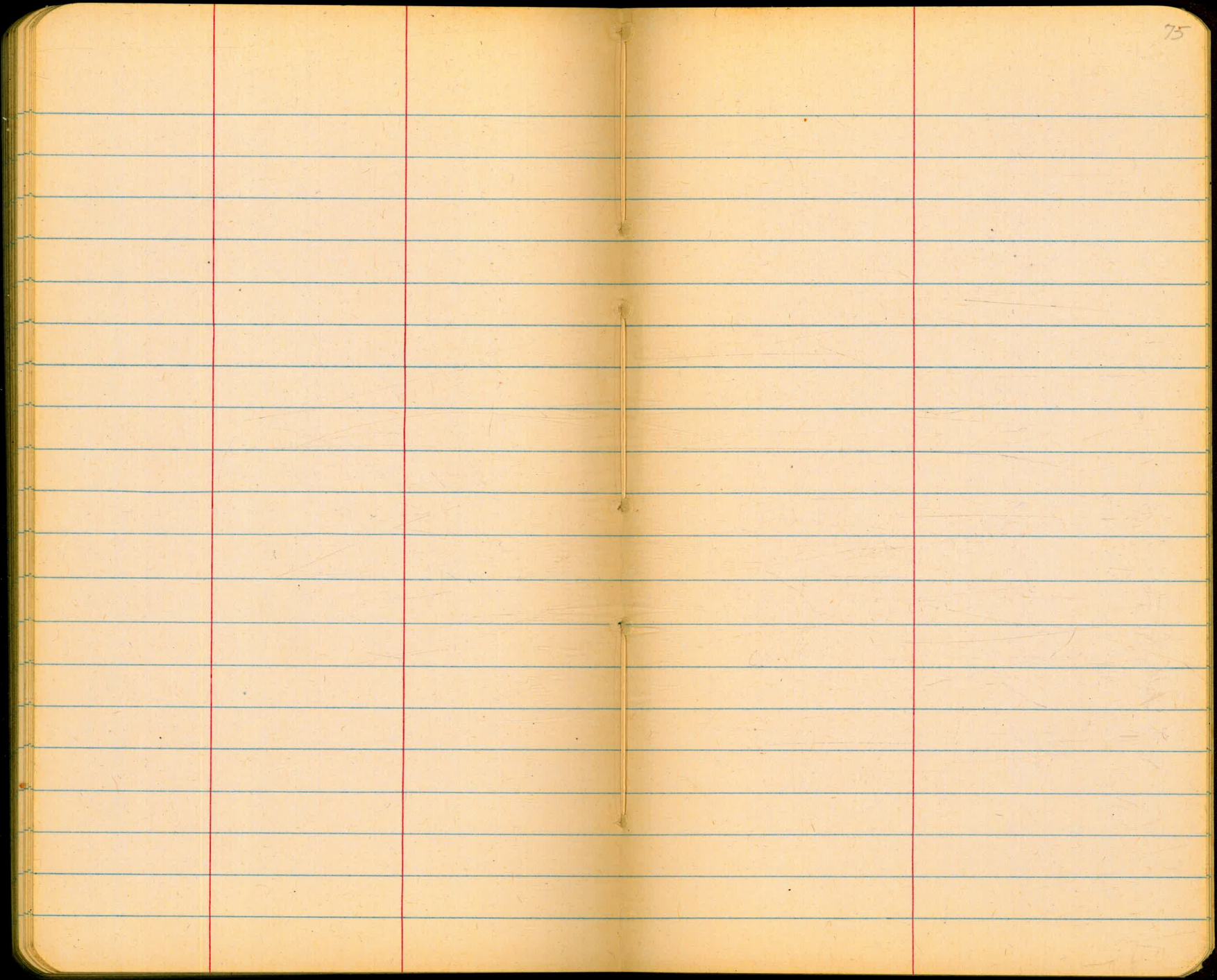


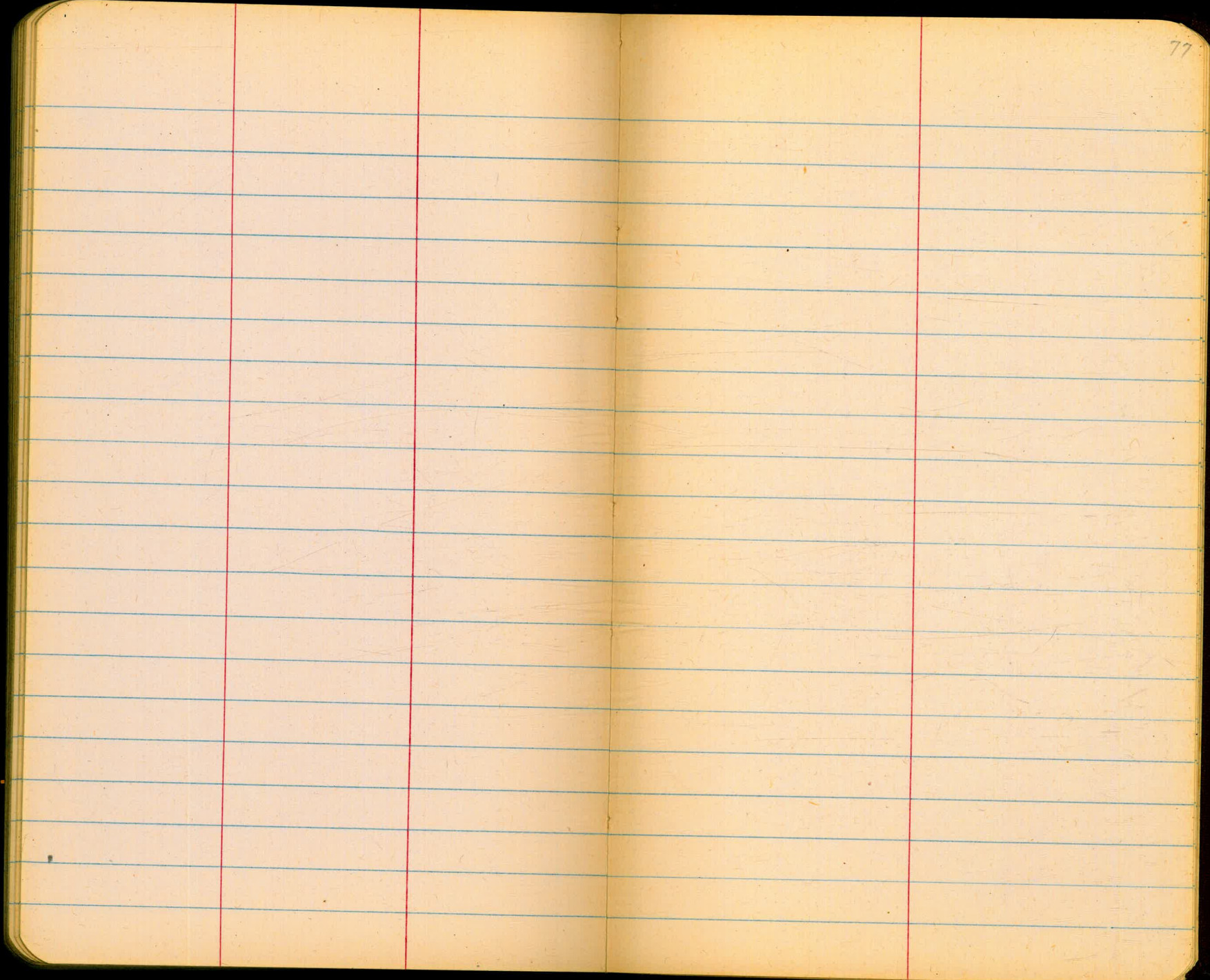


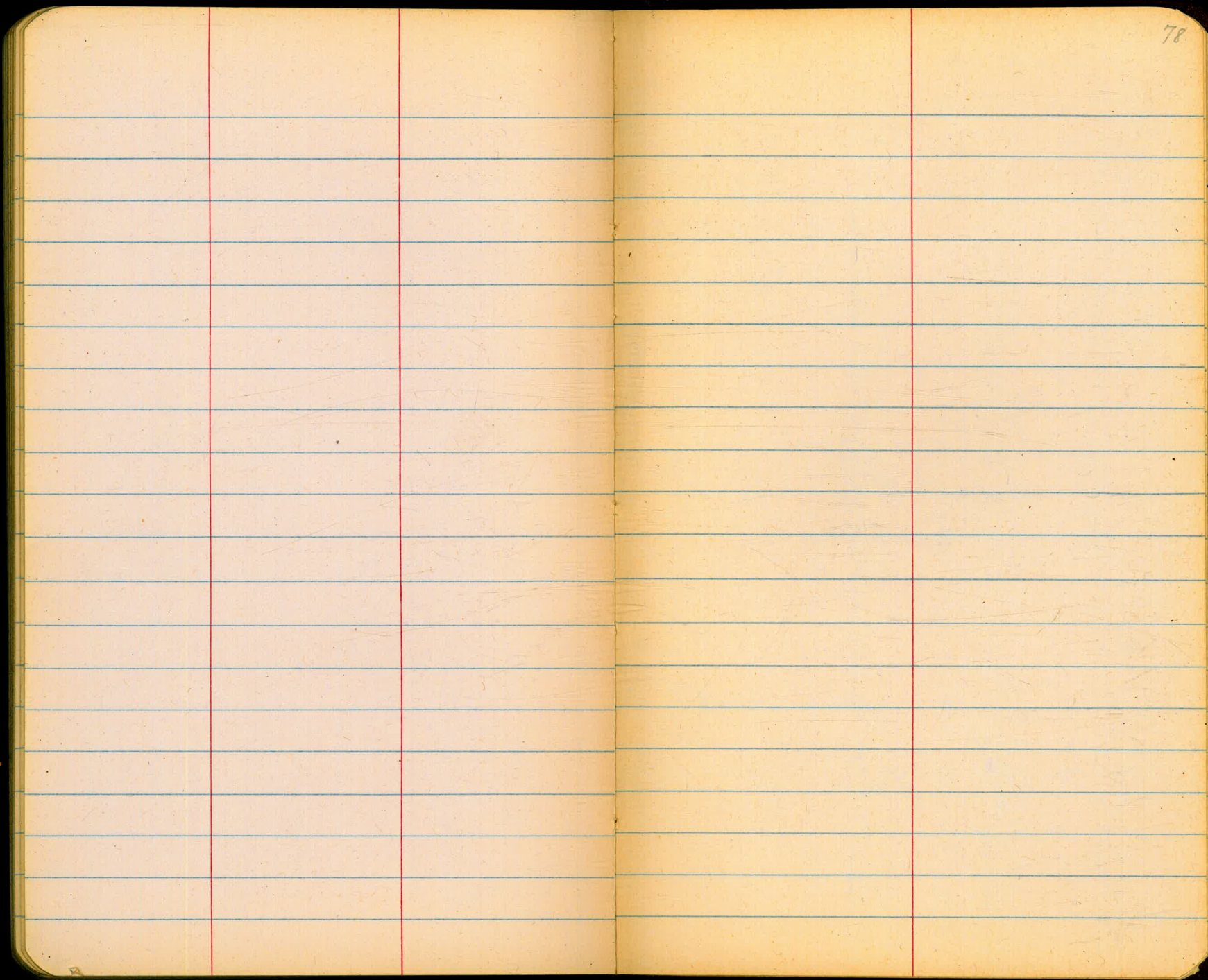




The image shows an open notebook with two facing pages. Both pages are cream-colored and feature a grid of horizontal blue lines. Each page is divided into three vertical columns by two red lines: one on the left side and one on the right side. The pages are otherwise blank, with no handwriting or printed text. The notebook is set against a dark background, and the pages show some minor wear and discoloration.







FAIRMOUNT

06102

13
Pa C.E.D. Pic Pa

370.14

Set

Set

89° 59' 40"

H3

90°

100.00

477.4

670.46

HIGHLAND

670.30

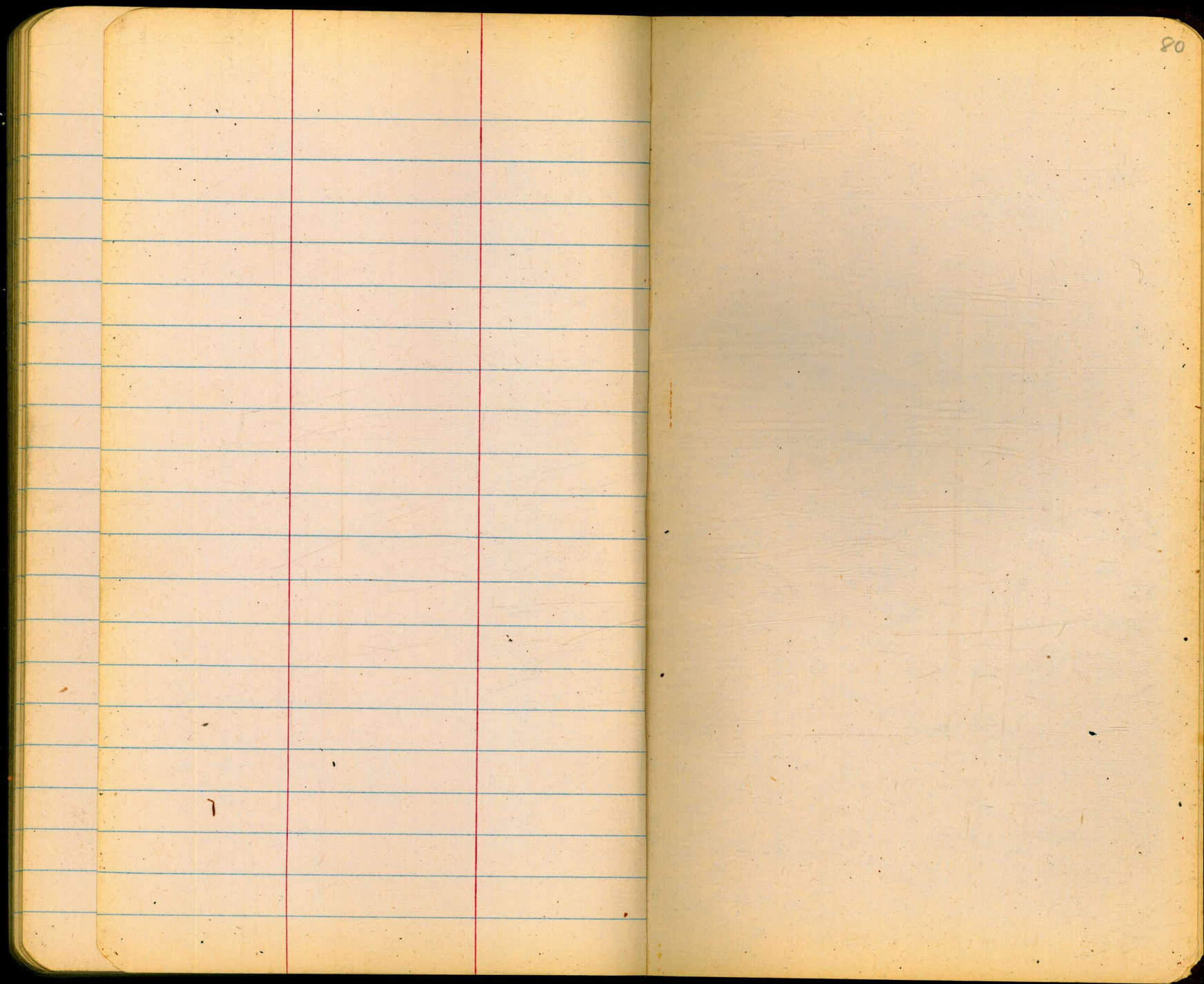
Set
3
MAPLE
Ed. PK 9.018

89° 59' 40"

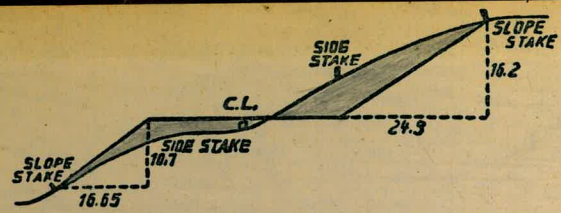
370.28

Ed. PK 20.18

ROSEVIEW



20017
 157.4
 358 35
 35
 48



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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