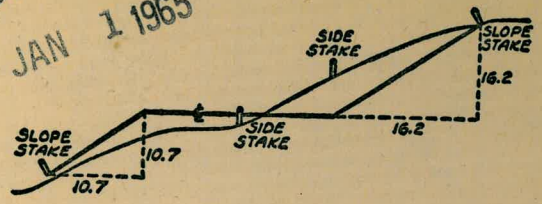
2136



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

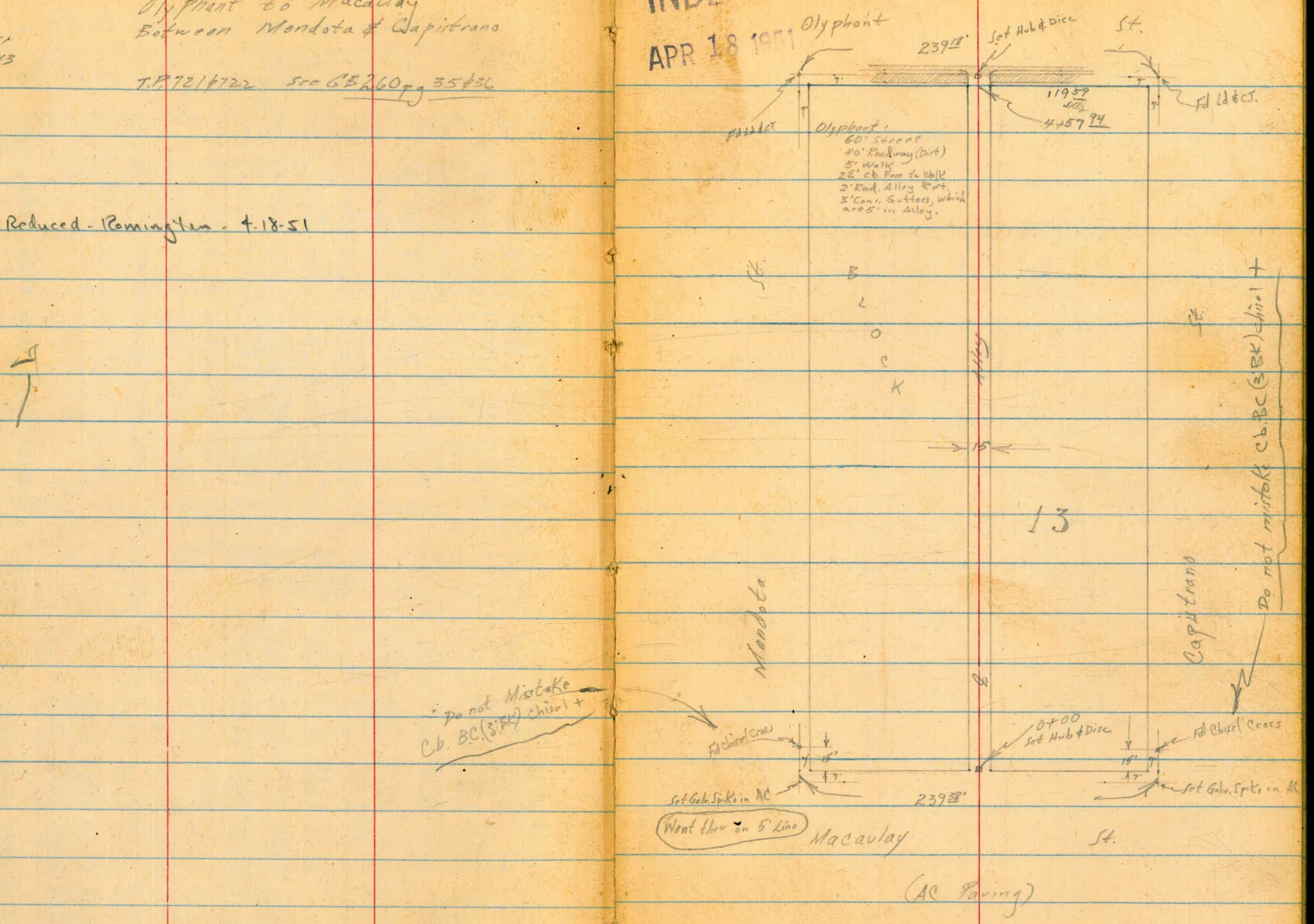
Index

Roberts
Cota
Moore
Pillon
4-16-51
W.O. 31743

X-Section Alley Blk 13, Pt. Loma Hts
Olyphant to Macaulay
Between Mendota & Capistrano

T.P. 721 & 722 Sec 6B 260 pg 35 & 36

Reduced - Remington - 4-18-51



Do not Mistake
C.b. BC (3 BK) chisel +

Cont'd From Page 1

0+27	14.9 Rt & Single Garage			
T.P.	0.76	122.80 ⊼	9.94	122.04
0+03				
0+00	East Line Macaulay			
0-10				
0-12	A.C. Gutter Macaulay (No Curb)			
0-32	AC. Pav. Macaulay			
T.P.	8.09	131.98 ⊼	12.13	123.89
B.M.	2.92	136.02		133.10 N.W.B.P.

Chatsworth & Narragansett

Lt ℄ Rt

122.58
0.22
122.80
Conc.

122.5	123.0	123.8	124.1	123.8
9.5	9.0	8.2	7.8	8.2
20	75		75	20

125.5	125.0	124.3	125.0	126.8
6.5	7.0	7.7	7.0	5.2
20	75		75	20

123.0	125.0	123.9	127.9	129.9
9.0	7.0	6.1	4.1	2.1
100	50		50	100

122.46	124.06	125.62	127.30	129.12
9.52	7.92	6.36	4.68	2.86
100	50		50	100

123.39	125.12	126.73	128.31	130.10
8.59	6.86	5.25	3.67	1.88
100	50		50	100

131.98 ⊼

Cont'd From Page 2

Lt ℄ Rt

1+00		114.9 7.9 20	115.0 7.8 7½	115.2 7.6	115.5 7.3 7½	117.5 5.3 20
0+88	7½' Lt Begin Picket Fence					
0+85	9' Rt End Conc. Apron				117.30 5.50 9' conc	120.07 2.73 2½ Floor
0+70	9' Rt Begin Conc. Apron Double Garage				118.41 4.39 9' conc.	120.05 2.75 2½ Floor
0+60		118.4 4.4 20	118.2 4.6 7½	118.5 4.3	118.9 3.9 7½	120.9 1.9 20
0+58	6½' Lt to Center T. Pole # PA1811					
0+41	6' Lt to Deadman					
0+40		121.5 1.3 20	121.3 1.5 7½	121.1 1.7	121.1 1.7 7½	121.6 1.2 20

122.80 π

122.80 π

Cont'd From Page 3

T.P.	#19	116.57 ℄	10.42	112.38
2+00				
1+85	12.8' Lt ℄ Single Garage			
1+77	6.5' Lt to Center P. Pole ±			
1+69.5	12.8' Lt ℄ Single Garage			
1+61	8' Lt END Pickett Fence			
1+50				
1+36	13' Rt END Conc. Yard			
1+03	13' Rt Begin Conc. Yard			

122.80 ℄

Lt / ℄ Rt

111.9	112.3	112.5	112.7	113.1
10.9	10.5	10.3	10.1	9.7
20	75		75	14 Fence

112.64	112.46
10.16	10.34
12.8 Floor	7.8 Apron

113.09	112.84
9.71	9.96
12.8 Floor	7.8 Apron

113.0	113.2	113.3	113.4	113.9
7.8	9.6	9.5	9.4	8.9
20	75		72	14 Fence

114.27	115.84
8.53	6.96
13	25

115.56	116.70
7.24	6.10
13	25

122.80 ℄

Lt ℄ Rt

2+98	7± Lt End 4± Conc. Block wall		110.7 5.9 7± Foot	111.6 5.0 7± Grd.
2+79	16' to (S.W.) Cor Garage			114.4✓ 2.15 16 Floor
2+73	BRK. in Apron		113.39 3.18 16± conc	
2+61	16± Rt Begin Apron For Single Garage ℙ to Alley ℄ Used to be Double Garage opening on Alley		113.39 3.18 16± conc	113.73 2.84 25± conc
2+58	7± Lt Begin 4± Conc. Block Wall 6± Lt to Center P.P. & P.P. #1855		111.9 4.7 20	112.0 112.7 112.5 112.9 113.8 4.6 3.9 4.1 3.7 2.8 7± 7± 7± 20 Foot
2+46	12' Lt ℄ Single Garage		112.5✓ 4.05 12 Floor	112.3✓ 4.25 7± Apron.
2+10	14± Rt ℄ Single Garage			113.2✓ 3.35 11± Apron 113.4✓ 3.15 14± Floor
		116.57 ℄		116.57 ℄

Lt ℄ Rt

6

3+78 6' Lt to Center P. Pole # PA 1883

108.3 109.5
8.3 7.1
7.6 7.6
Foot Block Wall Grd

3+66 23' Rt ℄ Double Garage

111.10 111.67
5.47 4.90
17.3 23
Apron Floor

3+48 6.5' Lt to Apron

109.30 110.49 110.53 110.6 110.7 111.8
7.27 6.08 6.04 6.0 5.9 4.8
30 7.5 6.5 7.2 20
Floor Apron

3+38 7.8' Lt Begin Conc. Block Wall (5')

109.7 110.7
6.9 5.9
7.8 7.8
Foot GRD

3+31 16' Rt ℄ Single Garage

111.61 112.53
4.96 4.04
12 16
Apron Floor

3+28 12' Lt ℄ Single Garage

110.84 110.75
5.93 5.82
12 7
Floor Apron

3+00

110.9 111.3 111.9 112.1 112.7
5.7 5.3 4.7 4.5 3.9
20 7.5 7.5 16
Wall

116.57 π

116.57 π

Cont'd From Page 6

4466 Edge Gutter

T.P. 5.88 110.33 ℄ 12.12 104.45

4457.94 West Line Olyphant

4430

4418 7.6' Lt End Conc. Block Wall

4400

3+88 6.2' Lt ℄ Conc. Apron

116.57 ℄

Lt ℄ Rt 7

105.23 104.40 104.79 105.21 106.13
5.10 5.93 5.54 5.12 4.20
7.5 7.5 7.5 7.5
CB Gutt Gutt CB

110.33 ℄

105.49 105.6 105.7 106.1 106.32
11.08 11.0 10.9 10.5 10.25
7.5 7.5 7.5 7.5
CB Gutt Gutt CB

107.1 107.4 107.4 107.8 108.8 109.1
9.5 9.2 9.2 8.8 7.8 7.5
15 7.5 7.5 10 20

107.0 108.1
9.6 8.5
7.6 7.6
Foot GRD.

108.8 108.8 109.0 109.7
7.8 7.4 7.6 6.9
7.5 7.5 20

108.27 109.08
8.20 9.49
29.4 6.2
Floor Apron

116.57 ℄

Check 2.24 133.10 = 133.10

T.P.	7.90	135.34	0.45	127.44
T.P.	13.13	127.89	0.04	114.76
T.P.	12.12	114.80	7.65	102.68

West Curb Line Olyphant

110.33 ℄

103.29	102.30	105.08	104.10	104.62	105.20	106.19	107.96	108.93
7.04	8.03	5.25	6.23	5.71	5.13	4.14	2.37	1.40
50	50	95	95		95	95	45	45
Cb	Gutt	Cb	Gutt		Gutt	Cb	Gutt	Cb

110.33 ℄

D. Smith
C. Allen
Nick
D. Shepard

X sec Selma Pl.

Note: 5' parking ± 5' walks through out where there are cbs.

Fd 1" pipe NE cor Selma ± Roswell prop.

1+33 17.5 Lt end cb & walk

1+23 17.5 Lt ℄ 12' drive

TP	10.05	253.85	0.19	243.80
1+00				
0+50				
0+00	Taken on prop line South prop Roswell ℄ Selma Pl			split obs at prop
BM	3.17	243.99	240.82	NW ¾" Pipe Roswell ℄ Hilltop

FB # 2025 pp

Reduced
7-5-51
RYAN

Lt = Ecst

WO # 25020
7-2-51
Rt = West

9

244.87
8.98
17.5
cb
rnf

244.06
9.79
12.5
drive

INDEXED
JUL 3 1951

253.85

244.3	243.99	243.0	242.9	240.0 242.0	242.78	241.3
+0.3	0.00	1.0	-1.1	2.0 / 1.21		2.7
30	17.5 cb	17.5 Cut		17.5 Cut	cb	30

243.8	242.34	241.6	241.2	240.3	241.24	239.7
0.2	1.65	2.4	2.8	3.5	2.25	4.3
30	17.5 cb	17.5 Cut		17.5 Cut	17.5 cb	30

241.5	240.98	240.2	239.6	238.4	238.87	238.6
2.5	3.01	3.8	4.4	5.6	5.12	5.9
30	17.5 cb	17.5 Cut		17.5 Cut	17.5 cs	30

243.99

Lt = East ℄ Rt = West

on split of ℄

3+20.26 L. Rt 28° 27' turned split cbs

3+00

2+50

2+13 Rt ℄ 10' drive

2+00

1+50

249.7	248.7	248.0	248.24	248.2
4.3	5.2	5.2	5.61	5.7
17		17.5 Swt	17.5 cs Lipt	30
249.2	248.5	247.8	248.12	248.0
4.7	5.4	6.1	5.73	5.2
17		17.5 Swt	17.5 cs	30
249.0	248.3	247.4	246.3	246.99	246.8
4.9	5.6	6.5	7.6	6.86	4.1
30	17		17.5 Swt	17.5 cs	30
			245.22		
			8.63		
			17.5 drive Lip		
247.7	246.9	245.7	244.9	245.48	245.2
6.2	7.0	8.2	9.0	8.37	8.7
30	17		17.5 Swt	17.5 cs	30
246.0	244.9	244.3	243.5	244.05	243.6
7.9	9.0	9.6	10.4	9.80	10.3
30	17		17.5 Swt	17.5 cs	30

25385

6+00

5+50 Brk in grade in cb on Lt

5+00

4+50

4+07 Lt Begin cs 2 wa/K

4+00

3+50

Lt = Eq

245.5 244.92 244.0 243.9

8 4 9 03 9 2 10 0

30 19 4 17 4

cs 94t

Rt = Eq

242.7 242.93 242.7

11 2 10 28 11 2

17 4 17 4

94t cs 30

246.9 246.59 245.7 245.3 244.1 244.43 244.1

7 0 7 26 8 2 8 6 9 8 9 42 9 8

30 17 1 17 2 17 3 17 3 30

cs 94t 94t cs

247.8 247.40 246.7 246.3 245.3 245.52 245.2

6 1 6 45 7 2 7 6 8 6 8 33 8 7

30 17 5 17 5 17 3 17 3 30

cs 94t 94t cs

248.5 248.14 247.7 247.3 246.1 246.64 245.9

5 4 5 71 6 2 6 6 7 8 7 21 8 0

30 17 4 17 4 17 1 17 1 30

cs 94t 94t cs

248.75

5 10

17 3

cs rnb

249.1 248.8 247.9 247.1 247.57 247.3

4 8 5 1 6 6 6 8 6 28 6 6

30 17 17 5 30

94t cs

250.2 249.6 248.5 247.7 248.12 248.0

3 2 4 3 5 4 6 2 5 73 5 9

30 17 17 2 17 2 30

94t cs

253 85

BM starting 3.37 240.83 +01

TP4 1.48 244.20 10.18 242.73

TP3 5.24 252.90 0.31 247.66

7+75

17.5 Rt end cb & walk

7+48.5 23.4 Lt end side walk

7+37 17.4 Lt end cb

7+00

6+89 Σ SMH

TP2 5.91 247.97 11.79 242.06

6+50

Lt = East & Rt = West

238.8 237.6 235.9 234.9 234.1

9.2 10.4 12.1 13.1 13.9

30 - 17

240.6 240.06 238.9 237.1 235.1 235.64 235.5 234.5

7.4 7.91 9.1 10.9 12.2 12.43 12.5 13.5

30 23.4 17 17.3 17.3 23.3 30

wgt walk Sat cb cb & walk

240.25

7.72

17.5 cb end

242.7 241.59 240.7 240.0 238.0 238.42 238.4

5.-3 6.38 7.3 8.0 10.0 9.53 9.6

30 17.5 17.5 17.5 17.5 30

cb Sat Sat cb

240.36

7.61

sim

247.97

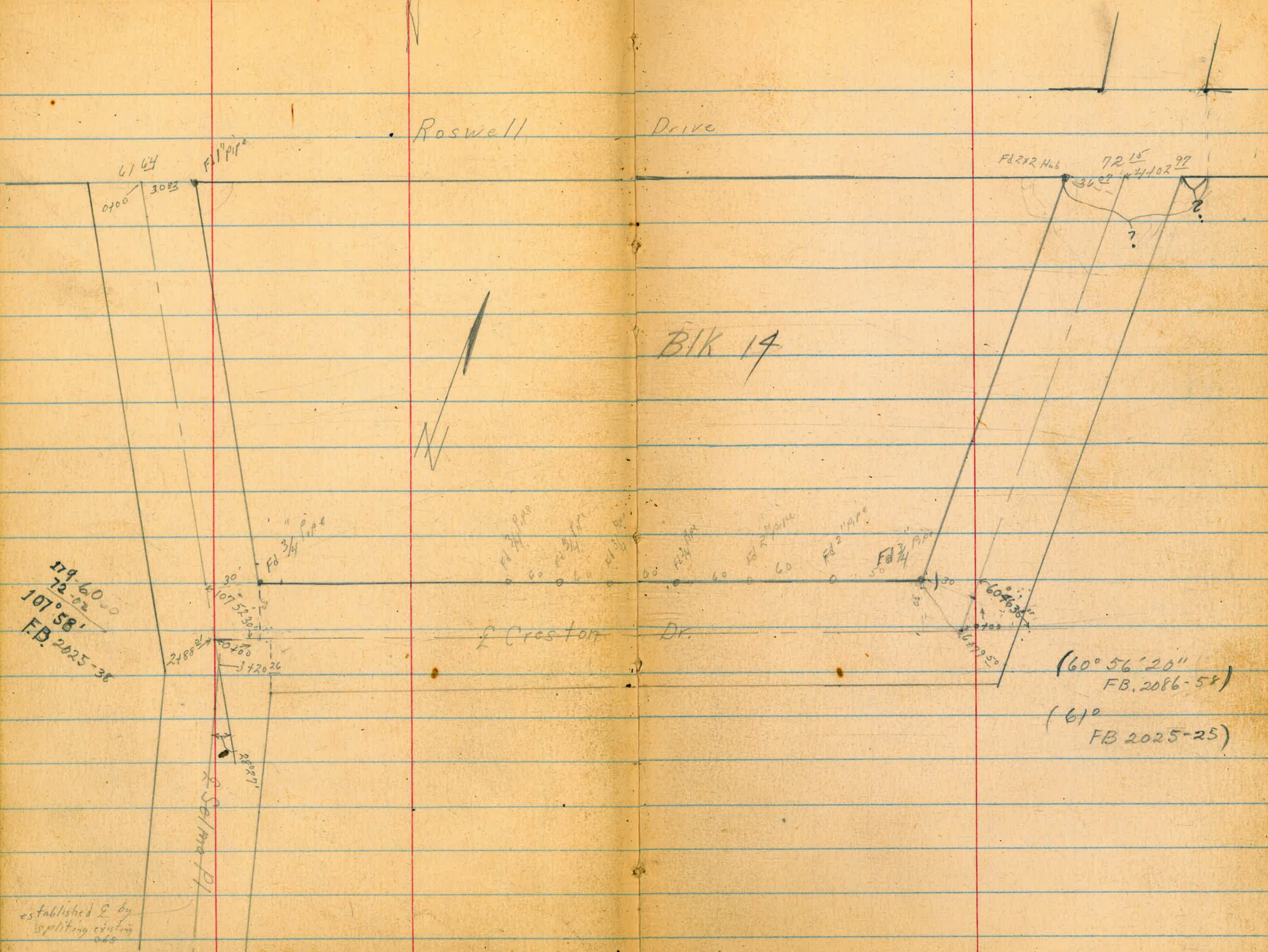
244.4 243.39 242.2 242.2 240.5 240.69 240.5

9.5 10.46 11.2 11.7 13.4 13.16 13.4

30 17.7 17.2 17.3 17.3 30

cb Sat Sat cb

253.85


Roswell Drive
Fd 1" Pipe
Fd 2x2 Hub
Blk 14
N
Fd 3/4 Pipe
℄ Creston Dr.
179-60-00
72-02
107°58'
F.B. 2025-38
(60°56'20"
FB. 2086-58)
(61°
FB 2025-25)
established ℄ by spliting existing

X Sec. Creston

Drive Lt = North ℄ Rt = South

0+80

253.0 252.6 252.27 251.9 251.0 250.8 251.0 251.4 252.0 251.9
2 5/40 2 9/30 3 19/23 wall top 3 6/23 ground 4 5/14 4 6 4 5/14 4 1/25 3 5/30 3 6/40

0+73 22 Lt Begin 4" con retaining wall 1' high

251.4 251.06
4 1/22 footing 3 40/22 Top wall

Reduced
7-9-51
F.P. Finney

0+42 23 Lt ℄ 3' con walk

250.77 250.59
4 69/3 walk 4 87/23 walk

0+41 20 SE prop cor

251.0 250.5 250.5 249.7 249.9 249.8 250.6 250.8
4 5/40 5 0/30 5 3/23 5 8/11 5 6 5 7/15 4 9/30 4 7/40

249.6
5 9

0+31 52 ℄ int + E prop Selma int.

249.1 249.2 249.7 248.8 249.1 249.3 249.2
6 4/40 6 3/30 5 8/20 6 7/16 6 4 6 2/15 6 3/30

248.4
7 1

0+21 84 NE prop Cor

0+00 ℄ int Selma + Creston

BM TP, page 9 11 66 255 46 243 80

255 46

Lt North ℄ Rt = South

2+20

257.1 256.9 256.6 255.6 255.3 255.2 253.0 246.9
8 5/40 8 7/30 9 0/24 10 0/17 10 3/ 10 4/26 12 6/30 18 7/40

2+01 21 8/ Lt. ℄ 6' con drive

256.29 256.12
9 30/ 9 47/
31 8/ drive 21 8/ drive

TP, 10 75/ 265 59/ 0 62/ 254 84/

1+97 19 8/ Rt ℄ 10" tel Pole # 76557

265 59/

255.5 255.2 255.1 254.0 253.9 253.8 251.1 253.5 252.2
0 0/40 0 3/30 0 4/21 1 5/16 1 6/ 1 7/16 1 4/28 2 0/30 3 3/40

1+70

254.58 254.44
0 88/ 10 2/
33 1/ drive 23 1/ drive

1+41 23 1/ Lt ℄ con drive

253.89 253.75 253.61 252.5 252.4 252.6 253.5 253.2
1 57/40 drive 1 21/30 drive 1 86/23 1/ drive 3 0/16 3 1/ 2 9/21 2 0/30 2 3/40

1+20 23 1/ Lt ℄ 8' con drive

252.7 253.48
2 8/22 6/ Footing 1 98/22 6/ Top wall

1+17 22 6/ Lt end con wall

255 46/

Lt = North ℄ Rt = South

3+00

3+97 23$^{\frac{1}{2}}$ Rt end con walk 11 to Line

3+97 21° Rt ℄ 12" Power Pole ⊕ P76558

3+82 19$^{\frac{1}{2}}$ Rt ℄ 4' con walk

3+56 28$^{\frac{1}{2}}$ Lt ℄ 8' con drive

3+54 23$^{\frac{1}{2}}$ Rt Begin 4' con walk 11 to Line

3+50

3+00

2+70

262.0	261.7	260.9	260.2	260.5	260.7	261.1	261.1	261.1
3$^{\frac{1}{2}}$	3$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$
40	30	16	11		14	21	30	40

261.18	261.19
4$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$
23$^{\frac{1}{2}}$ walk	27$^{\frac{1}{2}}$ walk

260.65	260.83
4$^{\frac{1}{2}}$	4$^{\frac{1}{2}}$
19$^{\frac{1}{2}}$ walk	30 walk

260.83	260.40
4$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$
38$^{\frac{1}{2}}$ drive	28$^{\frac{1}{2}}$ drive

260.13	260.08
5$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$
23$^{\frac{1}{2}}$ walk	27$^{\frac{1}{2}}$ walk

260.3	260.1	259.8	259.1	258.9	258.9	259.4	259.3
5$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$	5$^{\frac{1}{2}}$	6$^{\frac{1}{2}}$	6$^{\frac{1}{2}}$	6$^{\frac{1}{2}}$	6$^{\frac{1}{2}}$	6$^{\frac{1}{2}}$
40	30	20	14		15	30	40

258.9	258.6	258.3	257.5	257.5	257.7	257.4	257.1
6$^{\frac{1}{2}}$	7$^{\frac{1}{2}}$	7$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	7$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$
40	30	23	15		25	30	40

258.1	257.7	257.4	256.9	256.6	256.7	255.2	251.3
7$^{\frac{1}{2}}$	7$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	9$^{\frac{1}{2}}$	8$^{\frac{1}{2}}$	10$^{\frac{1}{2}}$	14$^{\frac{1}{2}}$
40	30	23	15		25	30	40

265$^{\frac{1}{2}}$

TP2 8^{25} 274^{01} 0^{33} 265^{25}

5+00

4+91 20^{5} Rt ℄ 10" Power Pole # 373806

4+59 20^{3} Rt ℄ 8" tree

4+50

4+46 24^{0} Rt end con walk 11 to Line

4+24 18^{5} Rt ℄ 3' con walk

4+21 29^{0} Lt ℄ 8' con drive

℄ SMH also

4+08 24^{2} Rt Begin 4' con walk 11 to Line

Lt = North ℄ Rt = South

274^{01}

264.8	264.7	264.4	263.8	263.6	263.7	264.2	264.2	264.2
0^{8}	0^{2}	0^{7}	1^{8}	2^{0}	1^{9}	1^{4}	1^{4}	1^{4}
40	30	20	8		14	24	30	40

263.8	263.6	263.2	262.3	262.1	262.1	262.6	262.8	263.0
1^{8}	2^{0}	2^{4}	3^{3}	3^{5}	3^{5}	3^{0}	2^{8}	2^{6}
40	30	21	9		14	20	30	40

262.75	262.77
2^{84}	2^{82}
24^{0} walk	28^{0} walk

262.87	262.63	262.02	262.09
2^{72}	2^{96}	3^{57}	3^{50}
39^{0} drive	29^{0} drive	18^{5} walk	30 walk

260.88	261.62	261.61
4^{11}	3^{97}	3^{98}
SMH	24^{2} walk	28^{2} walk
265^{5-9}		

Lt = North ℄ Rt = South

6+49 20' Rt ℄ 12" Power Pole # P76559

6+30

269.0 268.6 268.5 267.8 268.4 268.6 268.7 268.7
5.0 5.4 5.5 6.2 5.6 5.4 5.3 5.3
40 30 20 11 19 30 40

6+07 30' Rt ℄ 6' con ribbon drive 2' ea

268.13 267.79
5.88 6.23
30' drive 40' drive

6+00

267.8 267.8 267.2 267.0 267.0 266.9 267.8 267.8 267.6
6.2 6.2 6.8 7.0 7.0 7.1 6.2 6.2 6.4
40 30 18 10 15 19 30 40

5+96 29' Lt ℄ 8' con drive

267.81 267.81
6.20 6.20
30' drive 29' drive

5+92 29' Lt End con block wall

267.3 268.22
6.7 5.79
29' Footing 29' Top wall

5+52 29' Lt Begin con block wall

266.1 267.55
7.9 6.46
29' Footing 29' Top wall

5+50

266.2 266.1 266.0 265.7 265.4 265.7 265.9 266.0
7.8 7.9 8.0 8.3 8.6 8.3 8.1 8.0
40 30 24 13 18 30 40

274.01

0+50

17.63 Rt 6.7

0+76.60 NW Prop Cor

0+00

7+00

6+79.50 ℄ SMH = 0+00 to North ℄ Rt

6+65 21° Rt ℄ dead man

6+61.20 NW prop cor

Lt = West ℄ Rt = East

270.3 270.0 269.5 268.9 269.1 269.1 269.3 268.7 266.7
3.7 4.0 4.5 5.1 4.2 4.2 4.7 5.3 7.3
40 30 21 14 14 27 30 40

269.6 269.7 269.2 269.9 270.1 269.6 268.6
4.4 4.3 4.8 4.1 3.9 4.2 5.4
30 19 14 20 30 40

269.75
4.26
Hub

269.7 270.2 270.1
4.3 3.8 3.9
30 30

269.7 269.75 270.2
4.8 4.26 3.8
30 Hub 30

269.9 269.6 269.5 268.8 269.4 269.6 270.0 270.4
4.1 4.4 4.5 5.2 4.6 4.4 4.0 3.6
40 30 20 15 19 30 40

2.7.4 01

3+00

2+50

2+10 25½ Rt ℄ 12" power pole # 278222

2+09 18± Lt ℄ Telephone Pole # 370190

2+00

1+88 25± Rt ℄ deadman

1+50 24½ Lt ℄ log on drive

1+00

0+99 23½ Lt ℄ 12' con drive

0+67 29½ Lt ℄ 3' con walk

Lt = west ℄ Rt = East

266.0 265.2 264.0 263.4 263.5 263.2 261.1 258.4
8.0 8.8 10.0 10.0 10.5 10.8 12.9 15.6
40 30 16 12 26 30 40

268.1 266.3 265.3 265.0 264.1 264.3 264.1 263.5 260.2
5.9 7.2 8.2 9.0 9.2 9.2 9.9 10.5 13.8
40 30 28 19 14 28 30 40

268.2 266.9 266.3 266.0 265.1 265.5 265.3 263.4 261.3
5.8 7.1 7.2 8.0 8.8 8.5 8.7 10.6 12.7
40 30 28 19 15 25 30 40

269.25 268.07 267.25 266.2 266.5 266.4 264.9 263.0
4.76 5.94 6.76 7.8 7.5 7.6 9.1 11.0
40 drive 30 drive 24½ drive 14 25 30 40

270.0 269.4 268.7 267.6 267.7 267.9 267.8 266.6 265.6
4.0 4.2 5.3 6.4 6.3 6.1 6.2 7.4 8.4
40 30 23 14 14 25 30 40

270.13 269.82 268.40
3.88 4.19 5.11
39 drive 29 drive 23½ drive

~~270.35~~ 270.20
3.66 3.81
40 walk 29½ walk

274.01

Lt = West ℄ Rt = East

BM starting			943	240 85	240 83 Witness Corner Hilltop Roswell
TP 5	0 65	250 28	12 77	249 63	
TP 4	0 04	262 40	13 16	262 36	
TP 3	11 45	275 53	9 94	264 07	NE Prop Mon Brooklyn Roswell

4+20 81 SE prop cor

263.9	262.9	262.9	
10 4	11 1	11 1	
30		30	

4+02 99 ℄ South Prop Roswell

263.7	262.8	262.9	
10 3	11 2	11 1	
30		30	

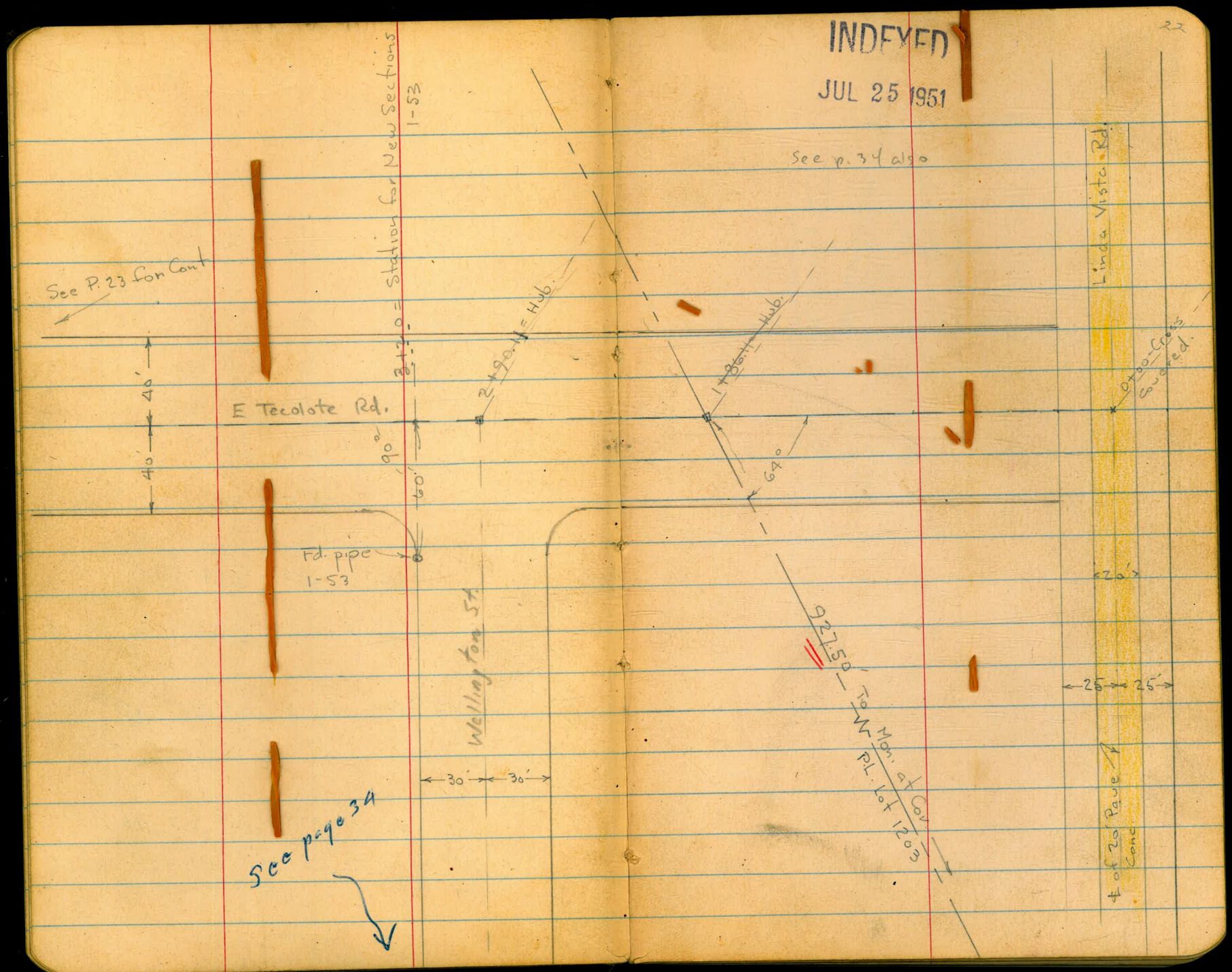
3+85 13 SW prop cor

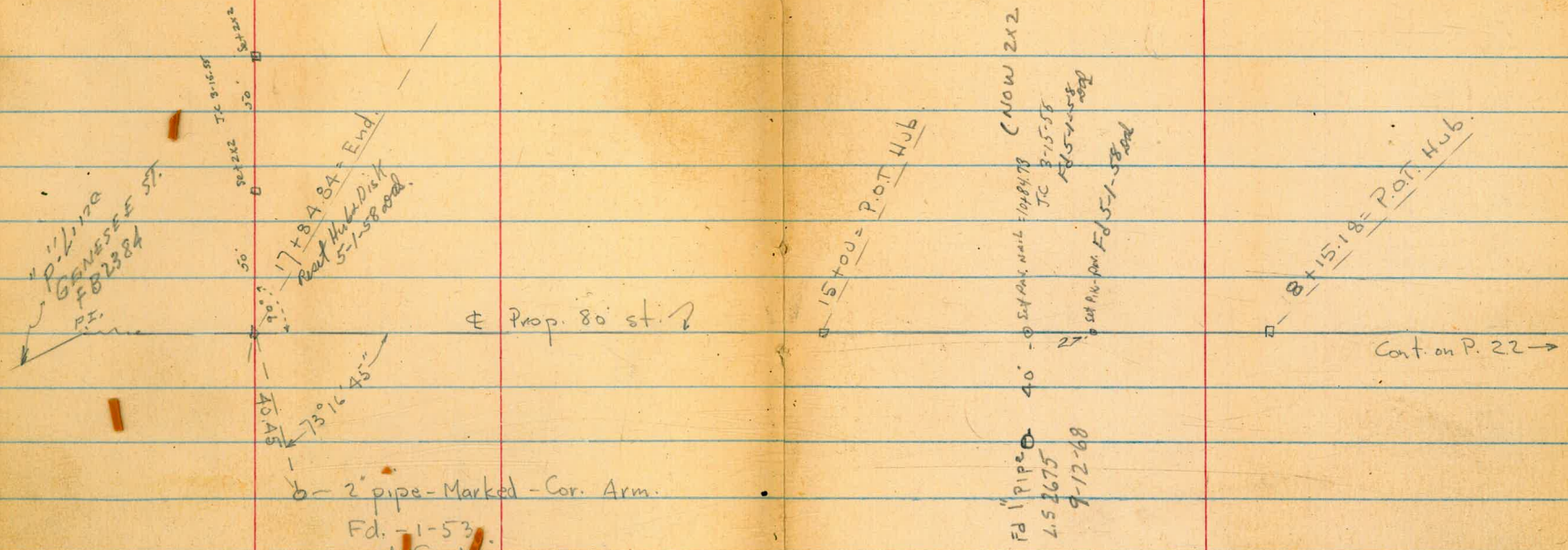
264.4	264.0	263.0	263.0	262.4	261.0	258.2
9 6	10 0	11 0	11 0	11 6	13 0	15 8
40	30	16		26	30	40

3+50

265.4	264.7	263.0	263.0	262.9	262.2	260.6
8 6	9 3	11 0	11 0	11 1	11 8	13 4
40	30	14		26	30	40

274 01





2 - 2" pipe - Marked - Cor. Arm.
Fd. - 1-53.
used for Line

Cont. on P. 22 →

10+84.73
27
70×57.73

Cross Sect. Prop. 80' st. Thru P.L. Lot 1203
from Exist. Conc. Pave on Linda Vista Rd.
To ℄ of Prop. 60' st. to South.
5529 7-24-51 7.0.
W.O. 20847

1+50

1+00

0+50

0+40 - 24.9 Lt. = ℄ P. pole # 178647

0+25 = approx. W.L.

0+10 = edge of Conc.

0+00 = ℄ 20' Conc. strip pave

Used Elev. Rod - Actual Elev. shown. - for Sections

B.M.			4.52	365.47 = Cross - 0+00
	6.66	369.99	4.11	363.33
B.M.	10.83	367.44		356.61 = our Datum — 362.73 = B. 2069 - P. 6 - Ld. + Disk ℄ Linda Vista Rd. + S.L. P.L. 1203

C. + G. Datum.

INDEXED

JUL 25 1951

	Lt.		℄			Rt		
1+50			59.5 (40)		59.9	61.0 (40)	61.8 (50)	63.1 (90)
1+00	60.8 (50)	60.7 (40)			60.7	61.3 (40)	61.5 (50)	62.5 (100) 63.1 (130)
0+50			62.2 (40)		62.2	62.4 (40)	63.5 (90)	
		64.2 (90)	62.5 (40)		62.8	62.3 (40)	63.5 (90)	
0+10 = edge of Conc.	64.86 (140)	64.91 (90)	65.13 (40)		65.29	65.45 (40)	65.56 (90)	65.72 (140)
0+00 = ℄ 20' Conc. strip pave	65.03 (140)	65.08 (90)	65.30 (40)		65.47 (300' figure Not Shown)	65.51 (40)	65.80 (90)	65.88 (140)

	Lt.	℄	Rt
4+70 = end.	59.4 (50) 59.5 (40)	60.1	60.8 (40) 61.0 (50)
4+20	60.0 (40)	60.1	60.5 (40)
3+70	59.1 (40)	60.0	60.2 (40)
3+20.11 = W.L.	58.4 (150) 58.4 (100) 58.6 (60) 58.9 (40)	59.4	59.5 (40) 59.8 (90)
2+90.11 = ℄ St.	57.9 (150) 58.2 (100) 58.5 (60) 58.7 (40)	59.35 on Hub.	59.0 (40) 59.2 (90)
2+60.11 = E.L. of Prop. 60' St. to South	58.1 (150) 58.3 (100) 58.3 (60) 58.4 (40)	58.7	59.1 (40) 59.8 (90)
2+00	59.1 (50) 59.1 (40)	58.7	59.1 (40) 59.3 (50) 60.4 (100) 61.4 (150)
2+00 Cont.			62.6 (200) 63.6 (220)

Additional Notes - Storm drain
N.Ely. from Mission Blvd + Turquoise

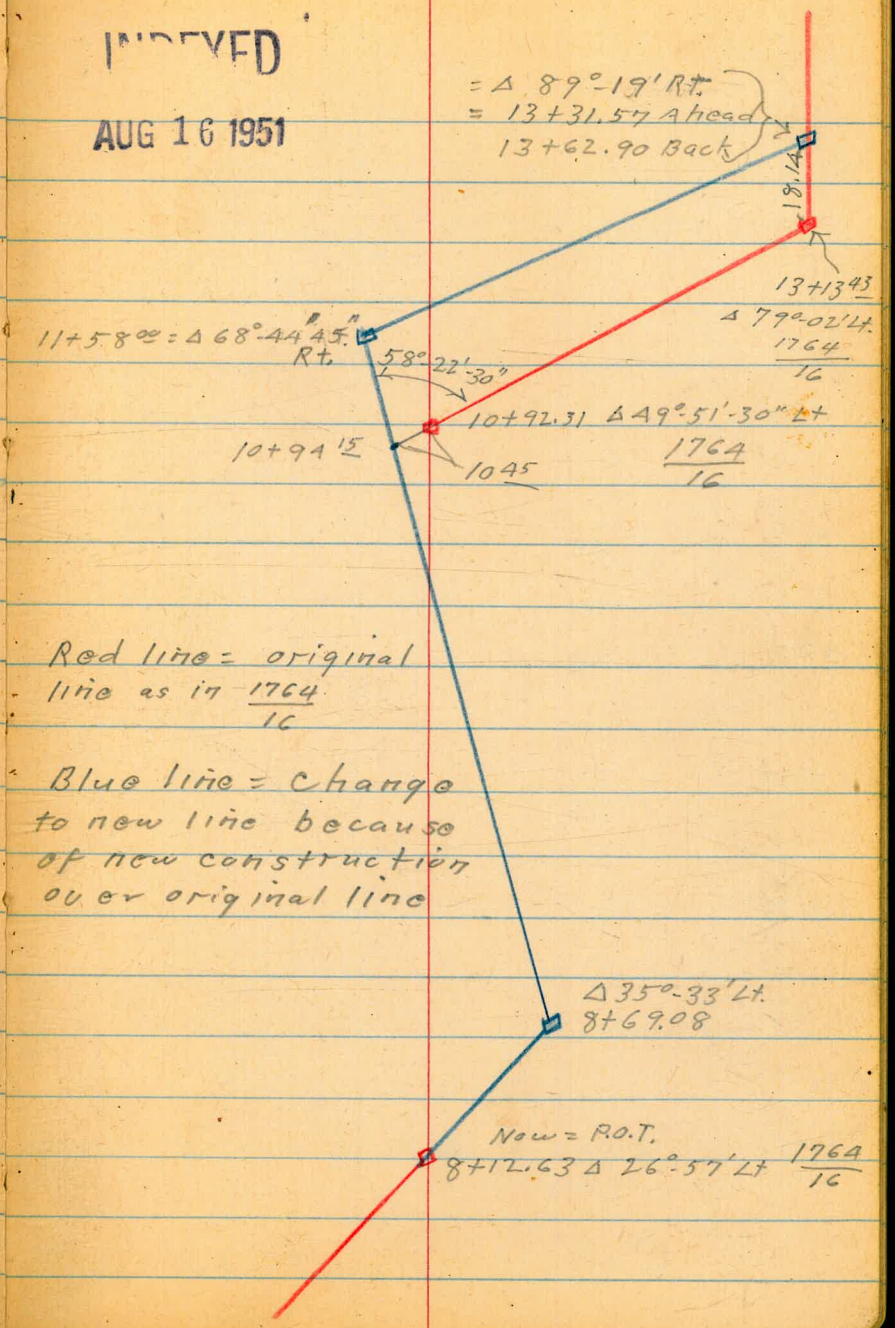
8-13-51

Sommermeyer
Begg
R. Sisson
C. Ford

W.O.#

original sketch in FB 1764 15 = 17

Notes reduced 8-20-51 HR



Red line = original line as in 1764/16

Blue line = change to new line because of new construction over original line

(See detail Next page)

Note. → (Section along water line.)
Δ 51°-43' in N.E. Quad.
coated water line

4+78^{9} = Intersect 2' outside diam conc.

4+60

4+00

3+35

3+18.

2+85

2+52

2+51^{5} 2' Lt. = ℄ 56" conc. pipe (intake)

4.68 132.33 127.65

℄

126.46 126.85 127.19
5.87 5.48 5.14
10 ← Bottom of pipe → 10

127.8 124.6 124.2 128.7 130.3
4.5 7.7 8.1 3.6 2.0
25 20 8 20

130.0 122.1 122.8 127.8 127.8 128.0
2.3 10.2 9.5 4.5 4.5 4.3
57 43 26 7 20

125.0 114.0 123.7 124.0 126.2
7.3 18.3 8.6 8.3 6.1
50 28 11 20

121.7 115.3 114.3 114.6 122.4 122.4
10.6 17.0 18.0 17.7 7.7 9.9
37 26 13 14 20

110.3
22.0

119.9 119.9 110.3 120.4 119.9
12.4 12.4 22.0 11.9 12.4
30 24 10 20

110.11
22.22
I. E.
132.33

B.M. = Δ Hub. Sta. 5+95 — 22

FB 1764

Orig Sec. + Location o.k. 5+95 to 7+11

T.P.	8.12	139.53	6.43	131.41
T.P.	10.19	137.84	4.68	127.65

5+95 Δ 18°-02' Rt. Section on split

5+50

5+25

5+00

4+79

Aprox. 1" per 1' batter - see const. plans

4+78.9 = ℄ pipe - Piers 8"×4' on top.

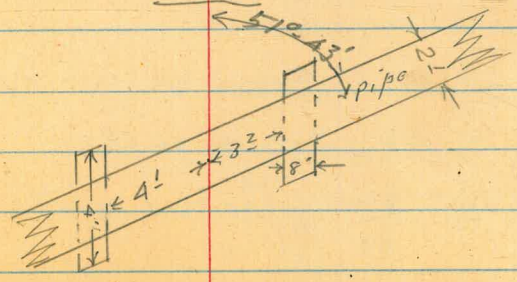
128.5 128.0 126.9 128.3
3.8 4.3 5.4 4.0
10 5 20

128.8
5.5

127.0 126.4 126.5 131.3
5.3 5.9 5.8 1.0
30 17 45

126.2
6.1

126.9 125.9 126.2 130.3 131.0
5.4 6.4 6.1 2.0 1.3
20 5 132.33 10 20



as in 1764-PZC

7+51 ± to (old & New - P.O.T.) 8+12.63 ± remains

7+50 = 5' Lt. = 6" diam pine

7+49 = 19' Rt. = B.C. Conc. wall

7+48 - 8' Lt. = 4" diam. pine

7+52 4.2 Rt. = end fire place

7+48 1.5 Rt. = start conc. block Fire place

7+41 = leave conc. walk at N'ly. corner

7+33.5 leave lath house & start Conc. walk

7+22 = enter lath house

7+19 = Cross 3.5' high prop. line picket fence.

T.W. = top of wall

7+11. 11.5 Rt = start 8" conc. wall

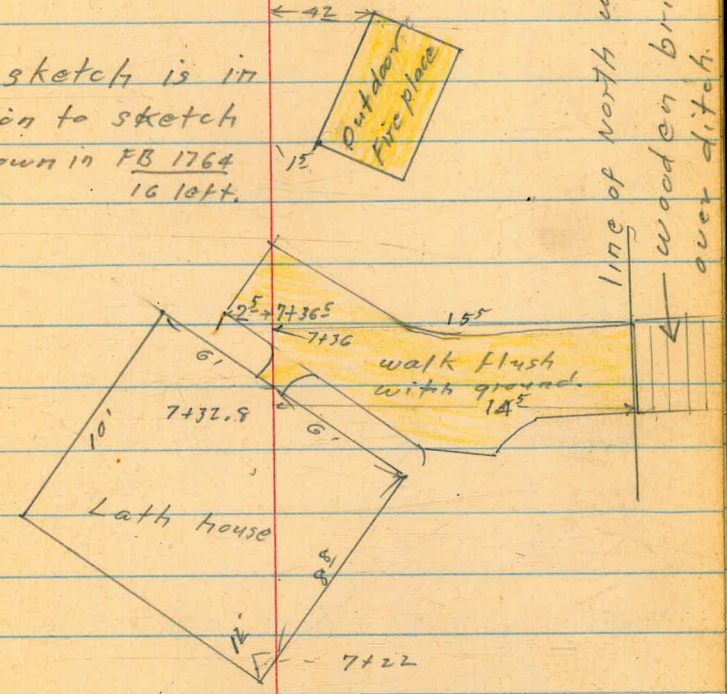
133.6 133.9 135.5 130.5

5.9 5.6 4.0 9.0

19 19 20

End T.W.

This sketch is in addition to sketch as shown in FB 1764 16 left.



134.5 133.7 133.8 135.5 129.5 129.4 131.4 134.4

5.0 5.8 5.7 4.0 10.0 10.1 8.1 5.1

15 11.5 11.5 12° 17.5 1.8 2.5

End T.W. T.W.

139.53

9+00 = intersect top of Wly. wall.

8+98 = intersect bottom of Wly. wall

8+80 = intersect bottom of Ely wall

8+76 = Intersect top of Ely. wall

8+69 9T = Δ 35°-33' Lt. (on split of Δ)

8+60 Lt. = start rubble wall

Note { B.W. = bottom of wall - also ground Elev.
T.W. Top of wall - also ground Elev.

8+40 8 Lt. = start rubble wall

T.P. 10.79 148.59 1.73 137.80

148.59

148.6 140.8 137.6 137.8 139.9 145.1 145.3
0.0 7.8 10,8 10,8 8.7 3.5 3.3
15 T.W. 05 2 3 13 20
+ Gnd. B.W B.W T.W

137.6
11.0
B.W. + Gnd

136.6
12.0
B.W. + Gnd

139.1
9.5
T.W. + Gnd.

148.1 139.3 136.3 136.3 139.3 140.61 144.2 144.6
0.5 9.3 12.3 12.3 9.3 7.98 4.4 4.0
30 9 7 4 3 Hub. 6 15
T.W. B.W B.W T.W

139.3 135.6 135.6 138.2 139.1 143.5 143.9
9.3 13.0 13.0 10.4 9.5 5.1 4.7
8 6 4 2 8 15
T.W B.W B.W T.W

147.4 137.5 135.3 135.5 138.6 141.6 142.1
1.2 11.1 13.3 13.1 10.0 7.0 6.5
30 10 8 6 5 15
T.W. B.W

10+25

10+15

10+00

Temp. B.M. 7.93 161.58 3.69 153.65 (153.62)

TIR 12.56 157.34 3.81 144.78

9'Lt. = end Ely wall
9+59 14' Lt. = end Wly wall

9+37 = Intersect top of Ely. wall.

9+33 = intersect bottom of Ely wall.

9+25 Intersect bottom of Wly. wall

152.3 152.5 145.1 144.6 148.3 153.1 153.4
9.3 9.1 16.5 17.0 13.3 8.5 8.2
35 20 7 10 12 20

151.8 151.8 144.5 145.0 148.4 150.7
9.8 9.8 17.1 16.6 13.2 10.9
35 28 16 8 20

144.4 144.1 146.6 149.5
17.2 17.5 15.0 12.1
35 20 20

161.58

old Δ 10+92.31 FB 1764 / 29

150.2 150.2 145.2 141.9 141.7 144.3 146.0 146.7 147.0
+1.6 +1.6 3.4 6.7 6.9 4.3 2.6 1.9 1.6
30 22 14 T.w 13 B.w 10 B.w 9 T.w 5 20

149.6 149.6 143.6 140.9 140.9 143.7 146.1 146.3
+1.0 +1.0 5.0 7.7 7.7 4.9 2.5 2.3
20 10 4 T.w. 3 B.w 1 B.w T.w 7 15

146.6
8.0
B.w + Cl

147.6 143.0 139.6 139.7 142.6 145.4 145.6
1.0 5.0 9.0 8.9 6.0 3.2 3.0
10 1 T.w. B.w. + Ord. 15 B.w 2 T.w 9 20

148.59

12+03 = Cross 4" sewer lateral.

11+85

Right side drops behind 11+53

11+58.00 = Δ 68°-44'-45" Rt. Section on split.

11+53

11+40

11+35 14' Rt. = N.Wly. Cor Frame Gar.

11+17

11+15 20.5 Rt. = S.Wly. Cor Frame Gar.

10+75

153.1
8.5
Approx. I.E.

159.0	158.1	155.3	153.0	152.8	155.7	155.6
2.6	3.5	6.3	8.6	8.8	5.9	5.8
20	8		6	12	16	20

157.6	157.20	157.V	152.5	151.8	155.5	155.5
4.0	4.38	4.4	9.1	7.8	6.1	6.1
20	Hub	5	13	19	25	28

157.V	158.0	152.3	152.5	155.4	155.6
4.4	3.6	9.3	9.1	6.2	6.0
20		12	21	29	35

157.1	157.1	150.7	151.4	155.6	155.8
4.5	4.5	10.9	10.2	5.8	5.8
30	20		10	15	20

155.6	155.0	148.6	148.6	149.5	155.6
6.0	6.6	12.8	13.0	12.1	6.0
40	30	16		10	18

155.6	155.0	146.6	148.7	151.6	155.6	155.6
6.0	6.6	13.0	12.9	10.0	6.0	6.0
40	30	16		2	18	25

153.6	153.1	148.5	146.V	151.3	154.3	154.6
8.0	8.5	13.1	15.4	10.3	7.3	7.0
35	25	15		6	19	30

161.58

Check B.M. 0.89 168.45 (168.48)

T.P. 7.62 169.34 4.08 161.72

8' Rt = end rubble wall

13+72 7 Rt. = near side pole # 5324

Taken on split

= 13+31.57 Ahead } = Δ 89°-19' Lt.
13+62.90 Back }

13+55 Rt. = B.C. rubble wall - 14' Rad.

13+25

13+07 11' Rt. = start low rubble wall

13+00

12+60

T.P. 4.96 165.80 0.74 160.84

12+40

S.W. 7' Mon. Cass & Van Ness 1764/36

159.6	154.5	158.8	161.1	159.3	165.8
6.2	7.04	7.0	4.7	6.5	0.0
10	Hub	3 B.W.	4 T.W.	7	18

159.6	158.8	159.1	161.0	163.8
6.2	7.0	6.7	4.8	2.0
20		8 B.W.	9 T.W.	20

162.4	160.3	158.2	159.1	160.8	162.8
3.4	5.5	7.6	6.7	5.0	3.0
20	4		9 B.W.	10 T.W.	18

162.1	161.6	157.8	158.3	160.8	161.2
3.7	4.2	8.0	7.5	5.0	4.6
20	3		10	12	20

161.8	161.5	158.9	156.0	158.7	160.6	160.6
4.0	4.3	6.9	9.8	7.1	5.2	5.2
20	9	165.80	6	10	19	25

160.6	160.8	159.9	157.5	155.2	155.5	156.7
1.0	0.8	1.7	4.1	6.4	6.1	4.9
25	12	6		4	9	20

161.58

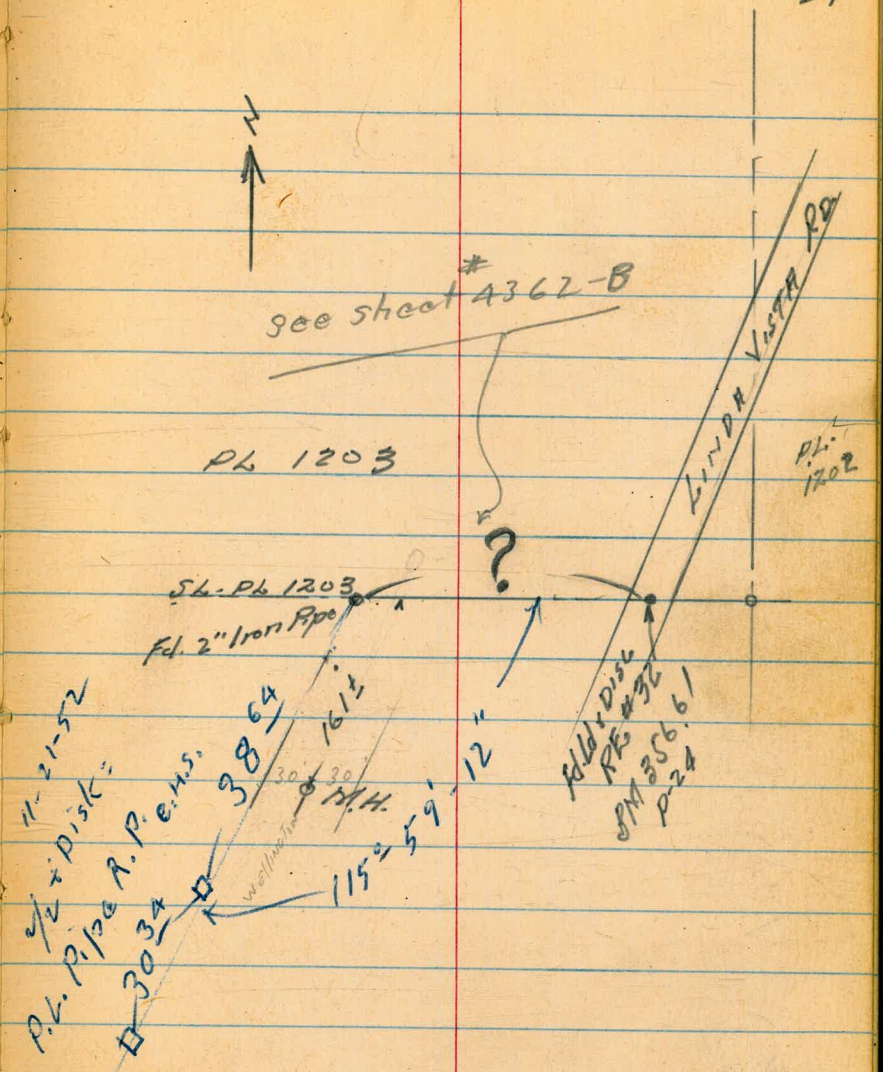
Elevation on Sewer MH.
in Wellington St. Linda Vista

Walker
Pope
Huffman
10-15-51

WO 20847

on Invert 338.30
10 12
on Rim MH. 348.92

356.61



B.M. Ld & Disc. Linda Vista Rd.
on S.L. PL. 1203 P.24

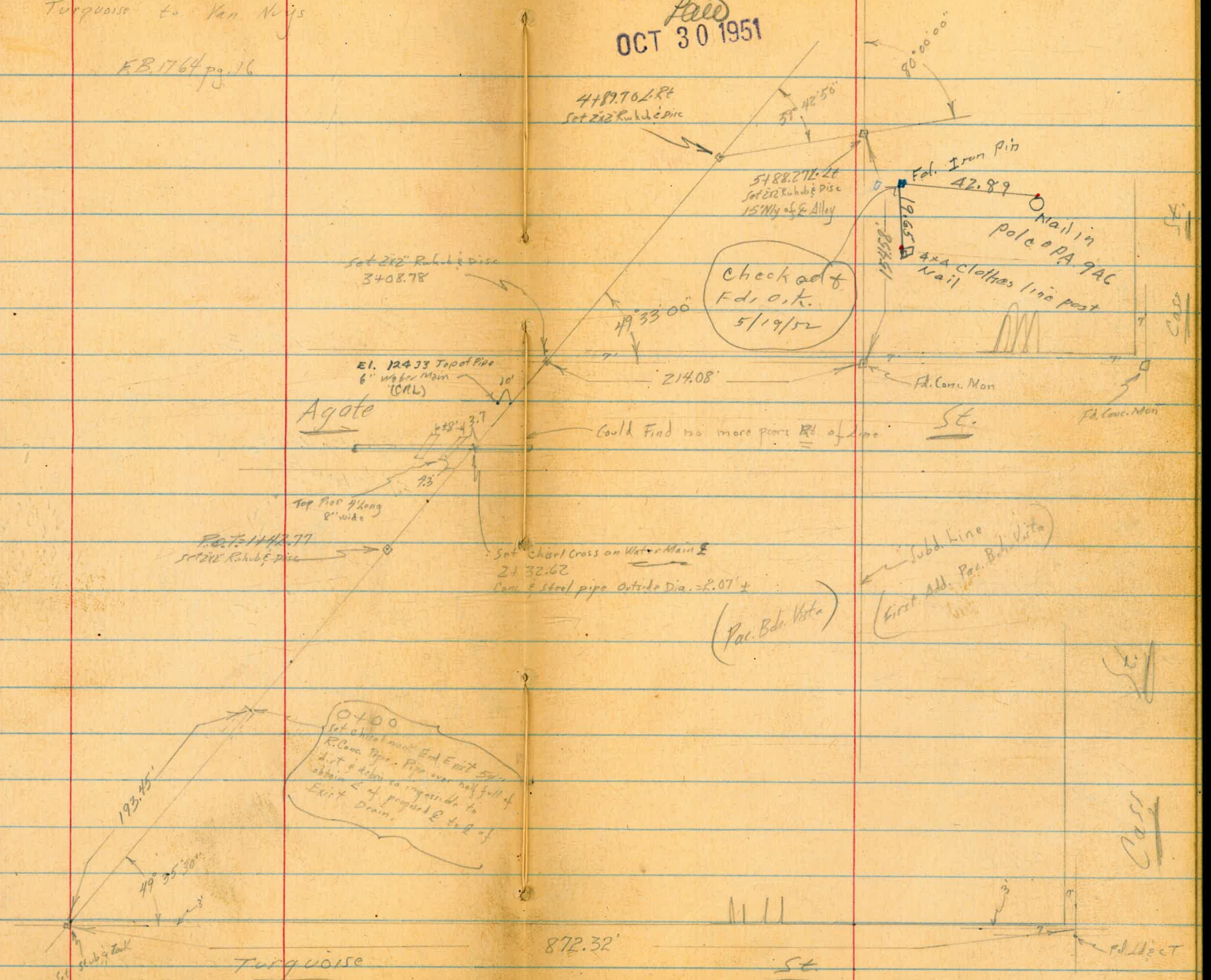
Robert
Cota
Moore
Pillen
October 28, 1951
W.O. 20504

Prelim. Survey Strom Drain
Turquoise to Van Nuys

F.B. 1764 pg. 16

INDEXED
Law
OCT 30 1951

35



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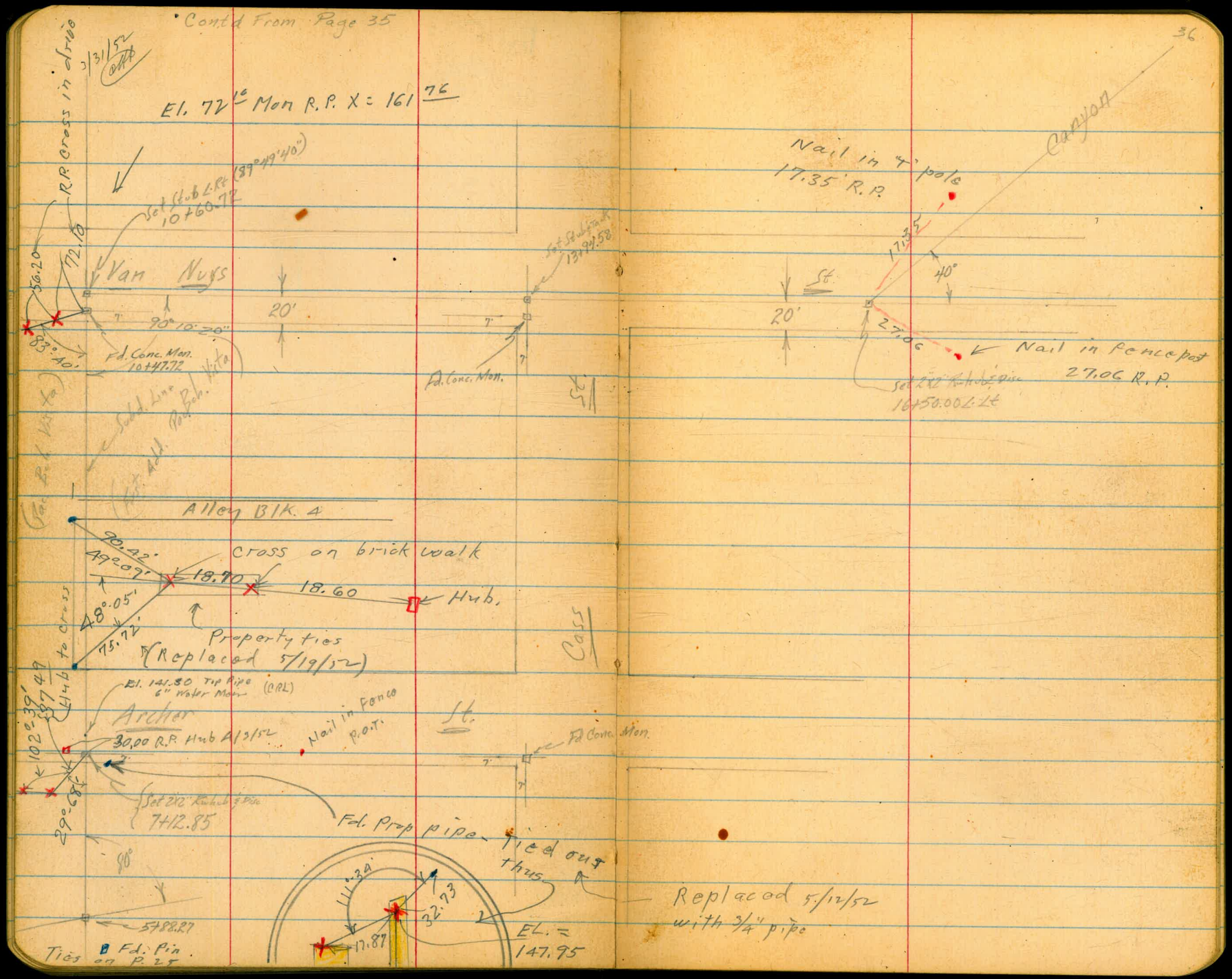


T.P.	12.89	134.99 ℄	1.52	122.10
0+80				
0+70				
0+58				
0+50				
0+00 End existing 54" Storm Drain				
T.P.	12.89	123.62 ℄	0.08	110.73
BM	12.27	110.81		98.54 NWBP

Mission Blvd. & Sapphire

℄ ℄

122.9
0.7
116.4
7.2
114.2
9.4
113.3
10.3
110.31
13.31
Invert

123.62 ℄

Cont'd From Page 37

		Lt	℄	Rt
2+32.62	Top Water Main (O.D=2.07')		129.26	
			5.73	
2+25			126.6	
			8.4	
			128.9	
2+20			6.1	
			128.7	
2+00			6.3	
			128.5	
1+50			6.5	
			126.0	
1+10			9.0	
	Shots Are. Fill			
			129.2	
1+00			10.8	
	134.79 ↑		134.99 ↑ ✓	

Cont'd From Page 38

		Lt	℄	Rt
4+16	5' Lt to center 12" Pepper Tree		128.9	
4+10			6.1	
4+06.2	10' Lt to SE Cor. House	132.2		128.9
4+00.5	Edge Conc. Arch	3.8		6.1
3+96.6	11.2' Rt to NW Cor. House	Top		GRD
3+92	8' Lt to ℄ Conc. Arch.			
3+66	6' Rt to center 1" Avocado			
3+70	3" Tree on ℄			
3+55	6' Rt to center 3" Pepper Tree		128.9	
3+53	3' Lt to 3" Apricot Tree			
3+50			6.1	
3+49	1" Tree on ℄			
3+43.7	Hit ⊥ corner wood Fence			
			126.7	
3+00			8.3	
			126.4	
2+50			8.6	

134.99 ft

134.99 ft

Cont'd From Page 39

		Lt	℄	Rt
5+35	Center Wash		132.7	
			14.9	
5+34	10± Lt to SE Cor Shed (Near Cor.)		132.3	
5+26			15.3	
			135.5~	
5+22			12.1	
5+21	10± Rt to NE Cor. Shed (same shed)			
5+03±	6± Rt to NW Cor Shed		136.3	
4+89.70	L. Rt		11.28 Hub	136.8 10.8 10 on spike
4+82	℄ Hits Picket Fence			
4+80	6' Lt to center P. Pole # PA920			
4+75	15' Rt to NW Cor Lath House			
4+39	6' Lt. to Clothes Line Pole			
T.P.	12.85 147.61 ↑ 0.23 134.76 ↓		147.61 ↑ ↓	
			133.4	
4+20			1.6	
	134.99 ↑		134.99 ↑	

T.P.	12.55	159.68	0.48	147.13
6+47 ℄	12' Lt to S.E. Cor House			
6+27				
6+08	center wash			
5+96				
5+88.27	L. Lt			
5+73				
5+61.5	113 Rt to center MH			
5+55				
		147.61		

Lt ℄ Rt

147.2	
	0.4
135.5	
	12.1
141.6	
	6.6
142.3	
	5.3
142.0	
	5.6
136.0	
	11.6
147.61	

Cont'd From Page 41

	Lt	℄	Rt
8+37.3 35 Rt to SW Cor House		1548	
		4.9	
8+00		151.4	
		8.3	
7+52		150.8	
		8.9	
7+44		146.8	
		12.9	
7+24		146.2	
		13.5	
7+20		148.6	
		11.1	
6+50		147.9	
		11.8	
159.68 ↑		159.68 ↑ ✓	

Contd From Page 42

10+60.72	L Rt				
10+00					
9+66					
T.P.	12.20	171.38 π	0.50	159.18	
9+66	9.5' Rt to SW Cor. House				
9+43					
9+00					
8+66					
		159.68 π			

Lt ℄ Rt 43

164.5	
6.9	
160.9	
10.5	
160.3	
11.1	
171.38 π	
158.1	
1.6	
156.0	
3.7	
155.1	
4.6	
159.68 π	

Small Natural water (mud)

	Lt	℄	Rt
13+50		168.5	
		2.9	
13+00		166.7	
		4.7	
12+50		165.1	
		6.3	
12+00		164.3	
		7.1	
11+50		164.4	
		7.0	
11+00		169.5	
		6.9	
10+69.5	163.02	163.4	160.68
	8.36	8.0	10.70
	38.5 Invert		13 Invert

38.5 Lt. to End culvert
15 Rt to End 30" Corr. Steel Culvert
℄ Crosses Culvert

171.38 ↑

171.38 ↑

Contd From Page 44

			Lt.	℄	Rt.
				173.3	
15+50				7.5	
				171.3	
15+28				9.5	
				170.4	
15+00				10.4	10.8 10 Top Bank
14+77 E	8° Rt to Center Fire Hydrant				
				169.6	
14+50				11.2	
	12.31	180.79 ✓	168.48	180.79 ✓	
T.P.		2.93	168.45 ✓ = 168.48	SW 7" Mon Van Nuys & Cass	See FB 1764 pg 36
				169.5	
14+00				1.9	
		171.38		171.38 ✓	

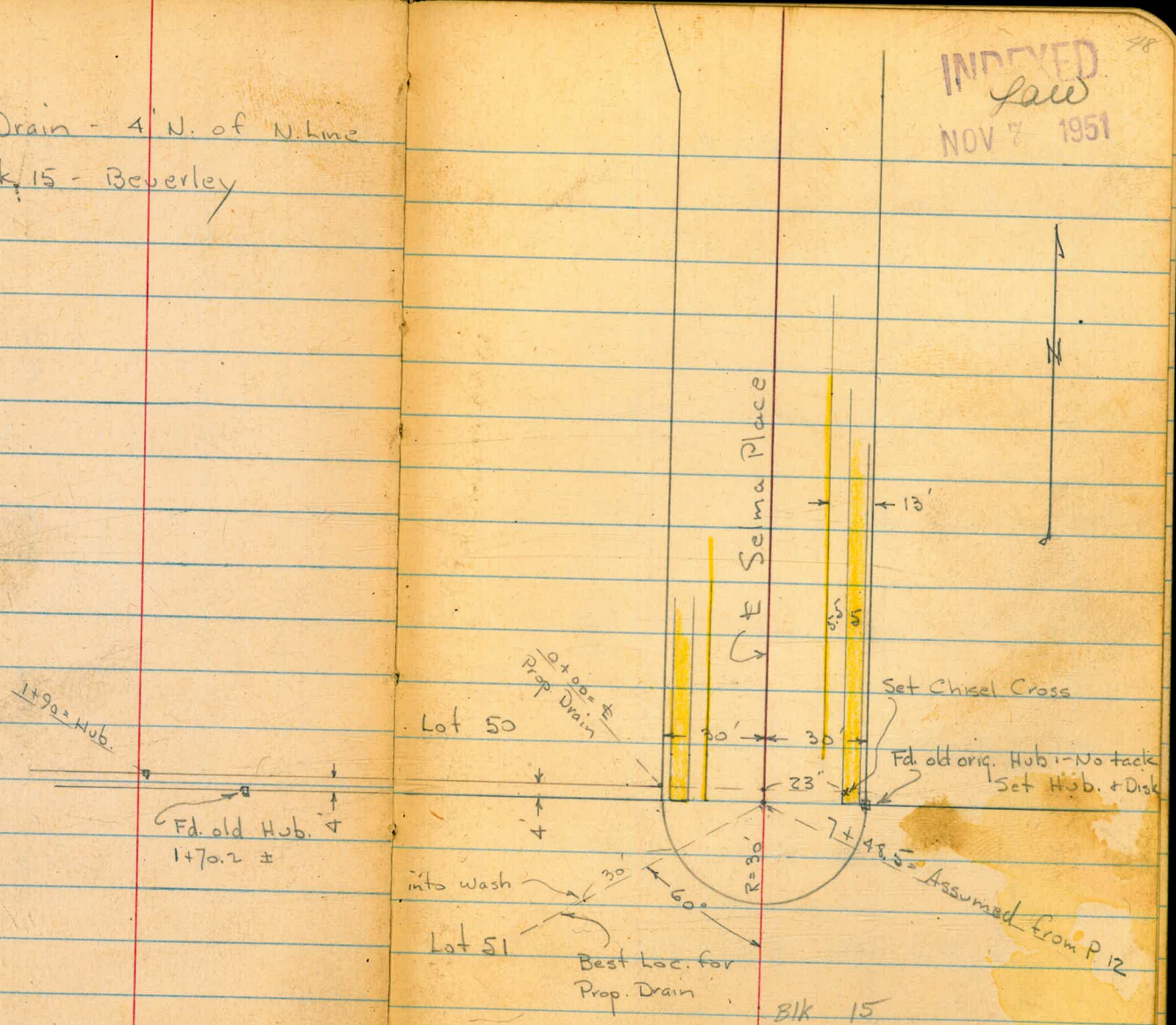
					Lt	℄	Rt
17+50	2.2' Lt to SE Cor. 2" conc. Slab back of Bldg				181.7	180.5	179.6
					9.6 2" conc.	10.8	11.7 18 Top Bank
T.P.	11.37	191.32 ℄	0.84	179.95		191.32 ℄	
17+44	13' Lt to SE Cor. Bldg.						
17+00					178.6		178.5
					2.2		2.3 12 Top Bank
16+67	41' Rt to Center T. Pole # 420682H						
16+50	L. Lt				176.3		176.0
					4.5		4.8 4 Top Bank
16+24					176.2		
					4.6		
16+00					175.0		175.0
					5.8		5.8 5 Top Bank
		180.79 ℄				180.99 ℄	

Cont'd From Page 46

					Lt	℄	Rt
check			10.43	168.47 = 168.48			
T.P.	0.31	178.90	12.73	178.59			
19+00	Into Canyon Floor					186.0	
						5.3	
18+50						185.4	
						5.9	
						182.6	
18+17						8.7	
						T.P. Bank	
18+00						178.5	
						12.7	
						180.4	
17+78						10.9	
						T.P. Bank	
		19132 T				19132 T	

Reduced By CRL
10-30-61

Survey for Prop. Drain - 4' N. of N. Line of Lot 51 - Block 15 - Beverley



Re-X-Sect. Selma Place from 6+50 to 50' S. of End. - See P. 12 for orig. Notes

5696 - 11-6-51 7.0.

W.O. 31502

7+85 - Beg. High Fill on Rt.

7+78.5' = S.Ly of Circle

7+48.5' = P.C. Prop. Curve & Lot Line

7+42 - 17.9 Rt = end cb.

7+38 - 16.8 Lt. = end cb.

7+00 = on 10' Conc. Dr. on Rt.

6+50

B.M. = Cross on E.7' Line 4' N. of Lot Line 240.17

Lt.		℄		Rt.		
39.1 50	38.2 30	37.1	35.1 30	34.6 38	27.4 50	
39.3 50	38.6 30	36.4	34.7 18	33.7 30	33.3 40	27.8 50 Nat. ground
40.26 27.6 walk end.	40.06 22.6	39.5' 18	38.7 17	37.6	36.4 10	35.2 18	35.44 23.7 walk	35.50 28.7 (Busted)
						35.88 17.9 = Top end.		
40.24 16.8 = Top								
41.5' Top	40.6 16.9 gut	39.9	39.0 10	38.04 17.9 gut. in Drive	38.41 23.4 walk	
43.40 Top	42.4 17.4 g.t.	42.2 10	41.9	41.3 10	40.6 17.8 g.t.	40.73 Top	

Actual Elev. shown - 200' Not shown.

Lt. ℄ Rt.

8+60 = Top of Bank - New fill - on ℄

8+28.5

36.0

38.7 / 50 | 37.9 / 30 | 36.3 | 34.7 / 30 | 34.6 / 32 Top | 29.1 / 42 Toe

Beg. Levels along ℄ of Prop. Drain
4' N. of N.L. Lot 51 - See Sketch - P. 48

		Lt.	℄	Rt.
B.M. on old Hub.	223.84			
1+90 = Top of Steep Slope - 150' ± to Bottom			18.2	
1+70 = Top		22.8 10	24.3	25.1 10
1+50		19.1 45 Top of Hill	25.9	26.5 10
1+00		25.6 10	26.6	28.2 10
0+60 - Head of Wash on Lt.		19.4 20 in Wash	24.8 10 Head of wash	27.1 29.1 10
0+20		30.4 10	31.6	32.2 10
0+00 = W.L. Selma			34.9 10	35.8 36.1
B.M. = Cross - P. 49	240.17	0-01.4 = edge of walk	35.76 walk	

Roberts
Moore
Fullen
11-28-51
W.O. 31502

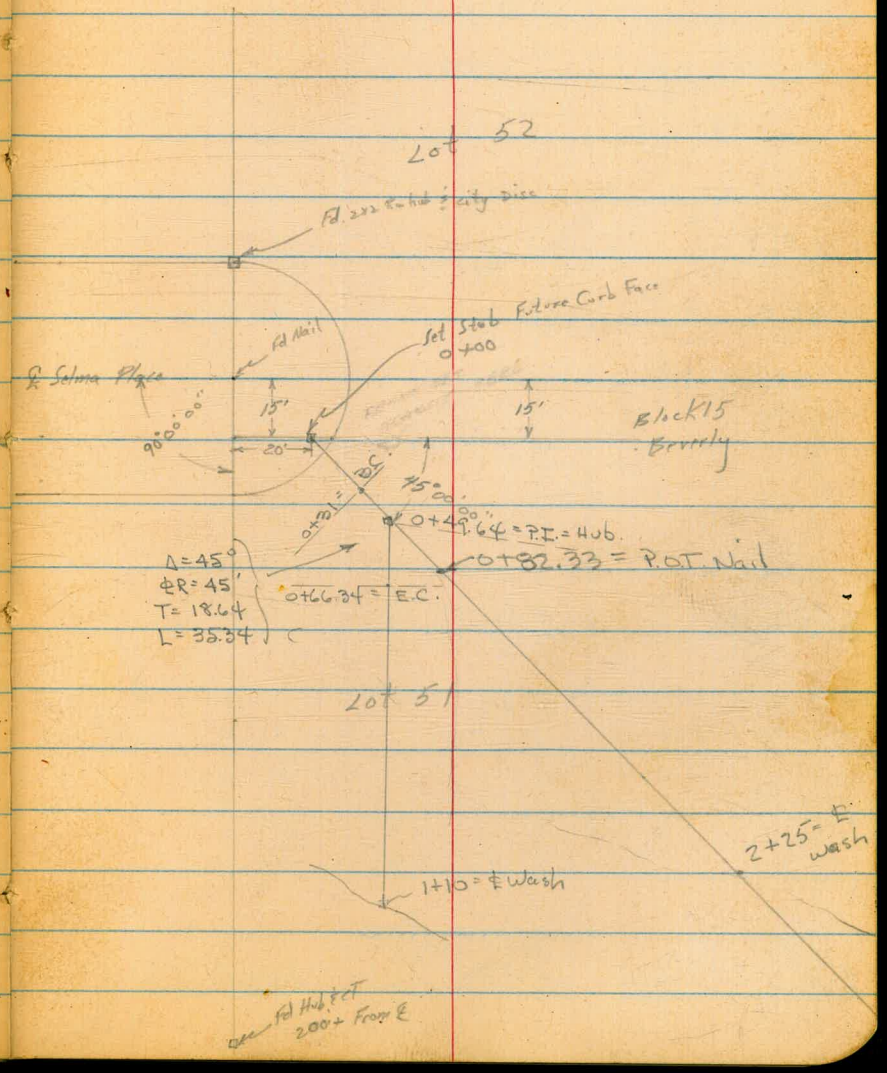
Survey For Storm Drain Dead End of Selma Place. (Beverly)
Lot 51 - Blk - 15

See Page 48

Add. Notes - 2-28-52 - 7.0.

(used split of Curbs)

82.33
.95 28
177.61
+7.39
225.00



Contd From Page 52

					Lt	℄	Rt
1+40						0.0	189.2 15.6 30 = ± wash
T.P.	0.18	204.87	17.86	204.69		204.87	
T.P.	0.14	222.55	18.11	222.41		222.55	
1+10						211.4 29.1	197.7 42.8 36 ± wash
0+85		Edge of Canyon				228.1 18.4	215.9 24.6 10 ± small wash
0+60						225.8 14.7	223.1 17.4 20 edge
0+50		Toe of Fill				227.3 13.2	
0+32		Edge Fill				233.5 7.0	228.1 12.4 18
0+00						235.3 5.2	
BM	0.35	240.52 A		240.17	Chisel Cross in walk E. T'Line Selma & 4'N. Lot Line	240.52 A	See Page 49

Rt	
	207.7 31.8 ± wash 45
	215.5 25.0 50 Head of wash.
	227.3 13.2 50

Lt. ℄ Rt.

2+55 - To show line of wash

2+25 = ℄ Wash

1+80

191.8
33.0
10
℄ wash

179.9
24.9
10

197.4
7.4
10

179.6
30.2

174.8
30.0

192.4
12.4

179.7
25.1
10

181.4
23.4
19 = ℄ wash

204.87

Add. Notes - Profile over New ℄
of Prop. Drain - Begining at sta 0+31
= B.C. - See sketch - P. 52 -

1+20 = slope of W. bank

1+10 = ℄ Wash = end.

1+00

0+92

0+80

0+6634 = E.C.

0+48.67 = Mid. of Curve.

0+31 = E.C.

T.P. 6.31 228.72.

222.41 - P. 53

204.6
24.1

203.5
25.2

206.5
22.2

211.7
17.0

218.9
9.8

225.3
5.4

227.1
1.6

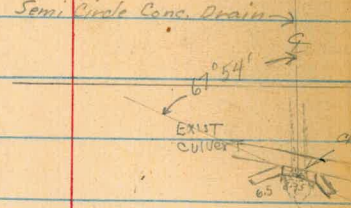
233.6 = Elev.

228.72

Clark
Shepherd
Bruner
Perkins

W.O. 21054
10-31-52

X-SECT. CLAYTON, PAC. HWY to Rwy; EXIST Culvert ETC.



Moore

33'
7'
Fd LAT

5C

KURTZ

3+00.25

℄ "Y" TRACK = 2+02.63

57°34'

1+63.48 ⊠ Set 2x2 = ℒ LT. 57°34' to ℒ Culvert
= 0+00 on Line to Culvert

CLAYTON

40' 80' 40'

X-SECT. CLAYTON ST.
RWY-CULVERT, ETC

0+86 ℄ 4.5' Conc. walk 41' Lt.

0+70 Beg Hedge 2' High 37' Lt.

0+50 ℄ ditch 2' Rt.

0+25 ℄ ditch 5' Rt.

0+21 End Conc. Slab 43' Lt.

0+13 Beg. of ditch 2.5' Rt.

0+06 Beg Conc. Slab 43' Lt.

0+00 Edge of Pavement

0-07 Cb. Inlet 41' Lt.

0-08 Inlet 27' Lt.

0-45 East side of ℄ Island

BM 7.35 13.42

6.07 = C/L □ IN N/Lt
Cb. Pac. & Clayton

8.80 walk 4.62 44.5 | 8.83 walk 4.59 41

7.0 6.4 50 | 7.2 6.2 40 | 7.0 Toe 6.4 19 | 9.5 Top 3.9 14 | 9.2 Top 4.2 6 | 5.8 Toe 7.6 | 5.9 Toe 7.5 4 | 9.1 Top 4.3 9 | 7.6 Toe 5.8 14 | 6.9 Toe 6.5 40 | 6.8 6.6 50

6.7 6.7 50 | 6.7 6.7 40 | 6.2 Toe 7.2 16 | 8.3 Top 5.1 7 | 9.4 Top 4.0 4 | 6.8 6.6 | 5.5 toe 7.9 4 | 5.5 Toe 7.9 6 | 7.6 top 5.8 10 | 6.3 Toe 7.1 16 | 6.16 6.8 40 | 6.4 7.0 50

6.45 Slab 6.97 62.8 | 6.46 Slab 6.96 43

6.51 6.91 50 | 6.5 6.9 40 | 6.2 7.2 | 5.9 ditch 7.5 2.5 | 6.4 7.0 40 | 6.9 7.0 50

6.48 Slab 6.94 62.8 | 6.58 Slab 6.84 43

5.97 walk 7.45 50 | 5.92 walk 7.50 40 | 5.82 Cb. 7.60 31 | Gut. 8.41 31 | 5.01 | 5.38 8.04 | 5.93 Gut 7.59 31 | 6.06 Cb. 7.36 31 | 6.21 walk 7.21 40 | 6.33 walk 7.09 50

5.56 Cb. 7.96 100 | 4.97 Gut. 8.45 100 | 5.90 Cb. 7.52 46 | 5.16 Gut. 8.26 46 | 1.73 Flow 11.69 41 | 5.19 8.23 26 | 5.39 8.03 | 5.60 7.82 26 | 5.57 Gut. 7.85 46 | 6.09 Cb. 7.33 46 | 6.47 Gut. 6.95 100 | 7.13 Cb. 6.29 100

4.68 Flow 11.74 27

6.07 7.35 100 | 6.21 7.21 40 | 6.43 6.99 | 6.69 6.73 40 | 7.28 6.14 100

13.42

1+63.48 ℄ ditch 12.5 Lt.

1+53 End of ditch digger 8' Rt.

1+52 Power Pole 28.2 Rt. #3725

1+43 ℄ ditch 3.5 Lt.

1+30 ℄ ditch 2' Lt.

1+10 Beg. partly dismantled ditch digger 10' Rt.

T.P.	5.71	18.44	0.69	12.73	2"x2" R/w hub ℄ at 1+63.48

End Hedge 37' Lt.

1+00 ℄ ditch 1' Rt.

9.9	9.9	9.9	12.0	11.8	7.0	7.7	12.7	12.7	11.9	12.8
		Toe	Top	Top	Toe	Toe	Top			
8.5	8.5	8.5	6.4	6.6	11.4	10.7	5.4	5.2	6.5	5.6
50	40	34	31	29	15	10	3		40	50

9.3	9.3	10.2	11.7	11.8	6.5	7.2	11.4	12.6	12.4
		Toe	Top	Top	Toe	Toe	Top		
9.1	9.1	8.2	6.7	6.6	11.9	11.2	7.0	5.8	6.0
50	40	20	17	10	5	2		40	50

9.3	9.3	9.6	11.7	12.1	6.3	6.7	11.2	12.4	12.9
		Toe	Top	Top	Toe	Toe	Top		
9.1	9.1	8.8	6.7	6.3	12.1	11.7	7.2	6.0	6.0
50	40	22	19	10	4		5	40	50

18.44

8.6	8.9	8.7	10.7	10.8	2.5	6.0	6.7	10.3	9.2	9.1
		Toe	Top	Top	Toe		toe	Top		
4.8	4.5	4.7	2.7	2.6	5.9	7.4	6.7	3.1	9.2	4.3
50	40	20	14	8	2		4	10	40	50

13.42

1+00 ℄ ditch 5' Rt.

0+60 ℄ ditch 7' Rt.

0+35 ℄ ditch 3.5 Rt.

0+06 ℄ ditch 10' Lt.

℄ ditch 16.5 Lt.

0+00 = 1+63.48 on ℄ Clayton ∠ 57°39' Lt.

Further Cross Section Notes on Drainage Ditch

2+24.50 Westerly track of RR 40' Lt.

℄ ditch 41.5 Lt.

1+99.48 Westerly Track of RR at ℄

℄ ditch 14.5 Lt.

1+20.83 Westerly track of RR. 40' Rt.

10.4 10.4 13.0 13.0 11.3 8.5 8.4 14.2 14.2

Toe	Top	Top		Toe	Toe	Top
8.0	8.0	5.4	5.4	7.1	9.9	10.0	9.2	9.2
20	16	12	3		2	8	13	17

10.1 10.4 12.9 13.0 7.8 7.9 13.6 13.6

Toe	Top	Top	Toe	Toe	Top
8.3	8.0	5.5	5.9	10.6	10.5	9.8	9.8
20	14	9		4	10	13	20

10.3 11.3 12.7 12.9 7.4 6.9 13.2 13.2

Toe	Top	Top	Toe	Toe	Top
8.1	8.1	5.7	5.5	11.0	11.5	5.2	5.2
25	19	15	8		7	11	20

10.0 10.0 12.4 12.0 6.5 6.5 12.7 12.7

Toe	Top	Top	Toe	Toe	Top
8.4	8.4	6.0	6.4	10.9	10.9	5.7	5.7
40	32	27	19	15	5		10

10.1 11.9 11.9 6.9 7.1 12.1 12.7

Toe	Top	Top	Toe	Toe	Top	
8.3	6.5	6.5	11.5	11.3	6.3	5.7
40	35	25	19	14	7	

18.44
T

13.8 15.58 13.6 14.9 15.6 15.4

	Rail				
4.6	2.86	4.8	3.5	2.8	3.0
50	40	16		40	50

7.2 7.3 13.2 13.2 14.58 13.9 13.3 14.4

Toe	Toe	Top		Rail			
11.2	11.1	5.2	5.2	3.86	5.0	5.1	4.0
43	40	29	9		17	40	50

9.7 9.9 11.8 11.6 7.0 7.9 12.9 12.6 12.2 13.57 12.1

Toe	Top	Top	Toe	Toe	Top			Rail	
8.7	8.5	6.6	6.8	11.4	10.5	5.5	5.8	6.2	4.87	6.2
50	40	36	27	17	12	6		32	40	50

18.44
T

T.P. 12.37 6.07 Ch. Sg. N.Ely. Return Pacific + Clayton

1+91.95 Headwall Culvert

1+80 ℄ ditch 7' Lt.

1+75 ℄ ditch 7' Lt.

1+50 ℄ ditch 3' Lt.

7.62 9.6

Flow	Ground
10.82	8.8
	0.0

9.9 10.3 14.1 14.2 9.5 14.8 15.6

	Toe	Top	Top	Toe	Top	
8.5	8.1	4.3	4.2	8.7	3.6	2.8
45	37	27	14	7		7

10.6 10.9 14.1 13.9 10.5 15.2 15.2

	Toe	Top	Top	Toe	Top	
7.8	7.5	4.2	4.5	7.9	3.2	3.2
40	32	23	13	7		7

10.4 10.9 14.5 15.0 8.4 8.6 10.8 14.9 15.2

	Toe	Top	Top	Toe	Toe		Top	
8.0	7.5	3.9	3.4	10.0	9.9	7.6	3.5	3.2
35	27	21	13	5	1		3	10

18.44

W.O. 20847

X-Sect. of E. Tecolote Rd. for

Contractor - 1-13-53 - 7.0

See Sketch - P. 22 - Plan - 9174-L

Wellington

check spike in S.W. Pole 360.49 - marked 360.48

2+50

2+00

1+50

1+00

0+50

0+14 = edge of A.C.

0+00 = ℄ Linda Vista Rd.

Set. B.M. = spike in S.W. Pole - Tecolote → Linda Vista Rd. 363.98

B.M. = Disk. - ℄ + PL. Line 356.61

, See P. 24

61

Lt. ℄ Rt.

INDEXED
Jan 53
FEB 19 1953

58.9 (50)	59.2 (40)	59.1 (20)	59.7	60.3 (20)	60.3 (40)	59.2 (50)
59.2 (40)	59.8 (20)	59.8	60.4 (20)	60.5 (40)		
59.6	59.8 (20)	60.0	60.3 (20)	60.7 (40)		
60.8 (40)	60.8 (20)	60.7	60.9 (20)	61.6 (40)		
62.6 (40)	62.9 (20)	62.9	63.2 (20)	63.1 (40)		
	65.04 (40)		65.25	65.40 (40)		
	65.37 (40)		65.52		65.64	

300' El. Not shown

Actual Elev. Shown.

		Lt.		℄	Rt.	
5+ 5+50	63.06					
7+50		63.3 40	63.9 20	64.1	63.8 20	64.1 40
7+00		63.3 40	63.6 20	64.1	63.7 20	63.9 40
6+50		63.2 40	63.2 20	63.6	63.7 20	63.9 40
6+40.5 = Sewer M.H	363.06 = Rim					
6+00		63.0 40	62.9 20	63.4	63.0 20	63.3 40
5+50		61.0 40	61.0 20	61.4	61.3 20	61.3 40
5+00		59.6 40	60.6 30	60.9 20	61.4	61.0 20
4+50		59.1 42	60.6 34	60.9 20	61.1	60.8 20
4+00		59.7 45	60.2 40	60.7 20	61.2	60.8 20
3+40		59.1 50	59.8 40	60.2 20	60.8	60.8 20
2+90 = on Sewer M.H.		59.6 60	59.6 40	59.6 20	60.02	60.9 20

		Lt.	℄	Rt.
12+50		61.2 (40)	61.5	61.7 (40)
12+00		61.5 (40)	61.9	62.0 (40)
11+50		61.8 (40)	62.3	62.4 (40)
10+84.73 = end		62.8 (40)	62.3 (32) 62.5 (20)	62.9	63.0 (20)	62.9 (40)
10+40		62.4 (40)	62.7 (20)	63.3	63.4 (20)	63.6 (40)
10+00		62.6 (40)	62.9 (20)	63.9	63.3 (20)	63.4 (40)
9+90.5 = on Sewer M.H.	63.91 = Rim			
9+50		63.3 (40)	63.6 (20)	64.0	63.3 (20)	63.3 (40)
9+00		63.4 (40)	63.6 (20)	63.9	63.7 (20)	63.8 (40)
8+50		63.6 (40)	63.7 (20)	64.2	63.6 (20)	63.9 (40)
8+00		63.3 (40)	63.9 (20)	64.0	63.8 (20)	64.1 (40)

	Lt.	℄	Rt.
16+50 = end.	58.3 (50) 58.5 (40)	58.4	58.2 (40)
16+00	60.9 (45) 60.4 (40) 59.0 (38)	59.1	59.9 (40)
15+50	59.9 (40)	59.8	60.3 (40)
15+00	60.1 (40)	60.3	60.3 (40)
14+50	60.6 (40)	60.4	60.8 (40)
14+00	65.3 (50) 61.0 (40) 60.5 (30)	60.7	61.0 (40)
13+50	65.9 (50) Top 62.6 (40) 61.0 (38) 60.8 (30)	61.1	61.2 (40)
13+00	61.1 (40)	61.5	61.6 (40)

Survey Wellington & Levant

7-18-55
C, H.S. III
Begg ↑
Schelin Hd. chain
Flora rear chain

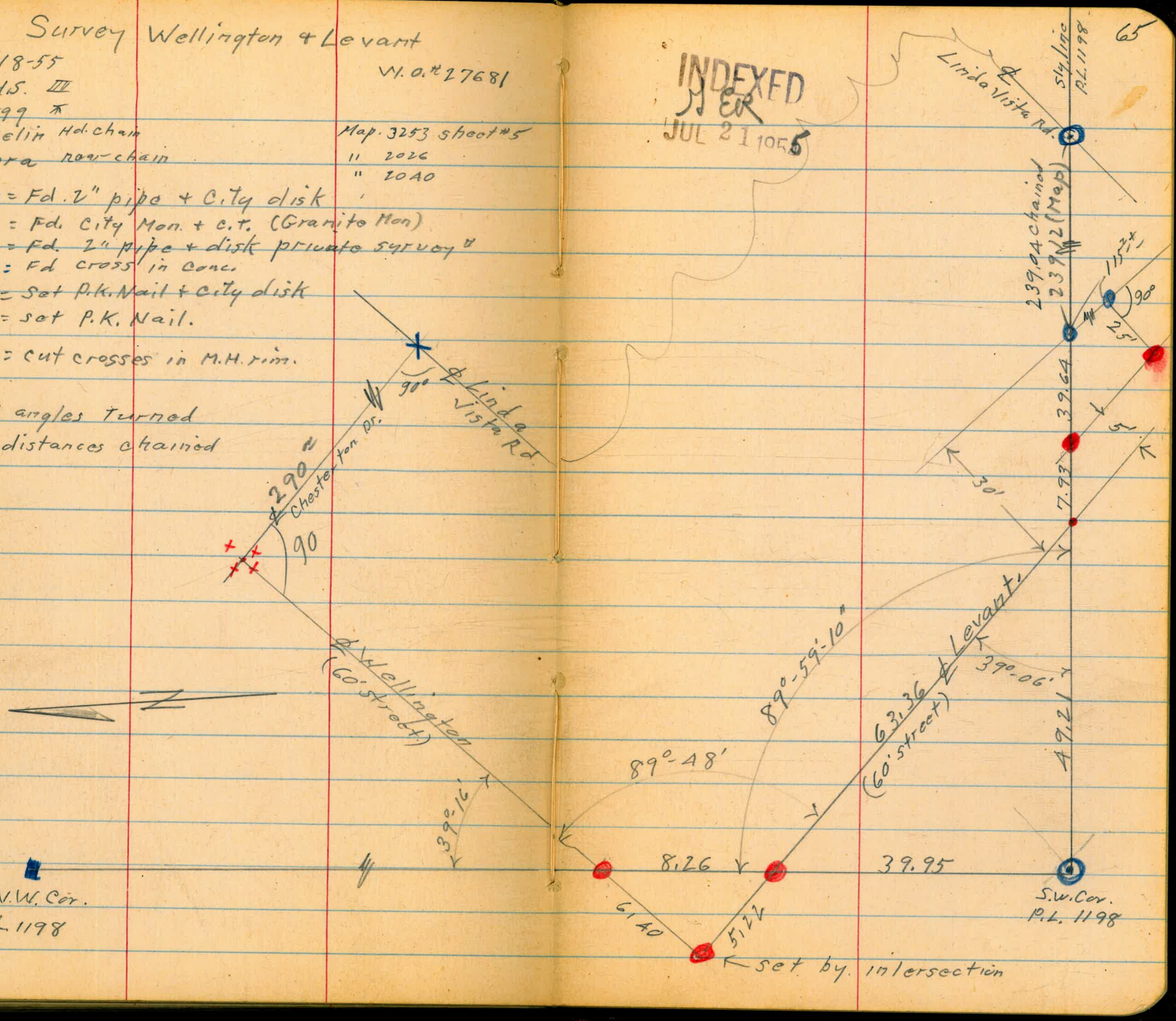
W. O. # 27681

Map. 3253 sheet #5
" 2026
" 2040

INDEXED
JJ ER
JUL 21 1955

⊙ = Fd. 2" pipe + City disk
■ = Fd. City Mon. + c.t. (Granite Mon)
● = Fd. 2" pipe + disk private survey
X = Fd cross in conc.
● = Set P.K. Nail + City disk
• = set P.K. Nail.
✕ = cut crosses in M.H. rim.

All angles turned
All distances chained



40.52
22.41
18.11

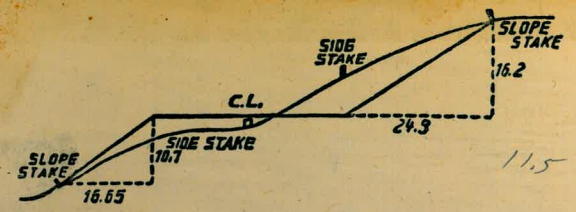
40.52
22.52
18.00

5.05
4.
13.17
22.22

232.62
16.02
216.6

34.90
17.35
15
32.35

45°
881
1531



11.5

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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