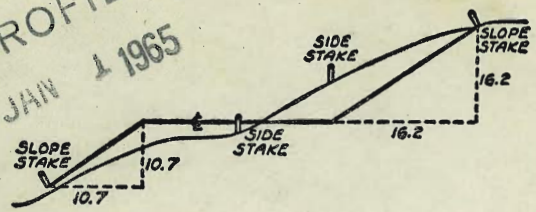


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEX,

1.08

2.52 12 Mly

28.5 12 Sly

4.94 12 Wly

Bond St.

Grand to Figueroa

X-Sec. for grade

3-19-52

W.O. 25020

Balboa FB 181 / 11 = EL 13.67

B.M. = B.P. S.E. Cor. Rose Canyon Bridge at

■ Denotes Fd. Conc. Mon.

□ " " 3/4 " Tack

○ " " Pipe

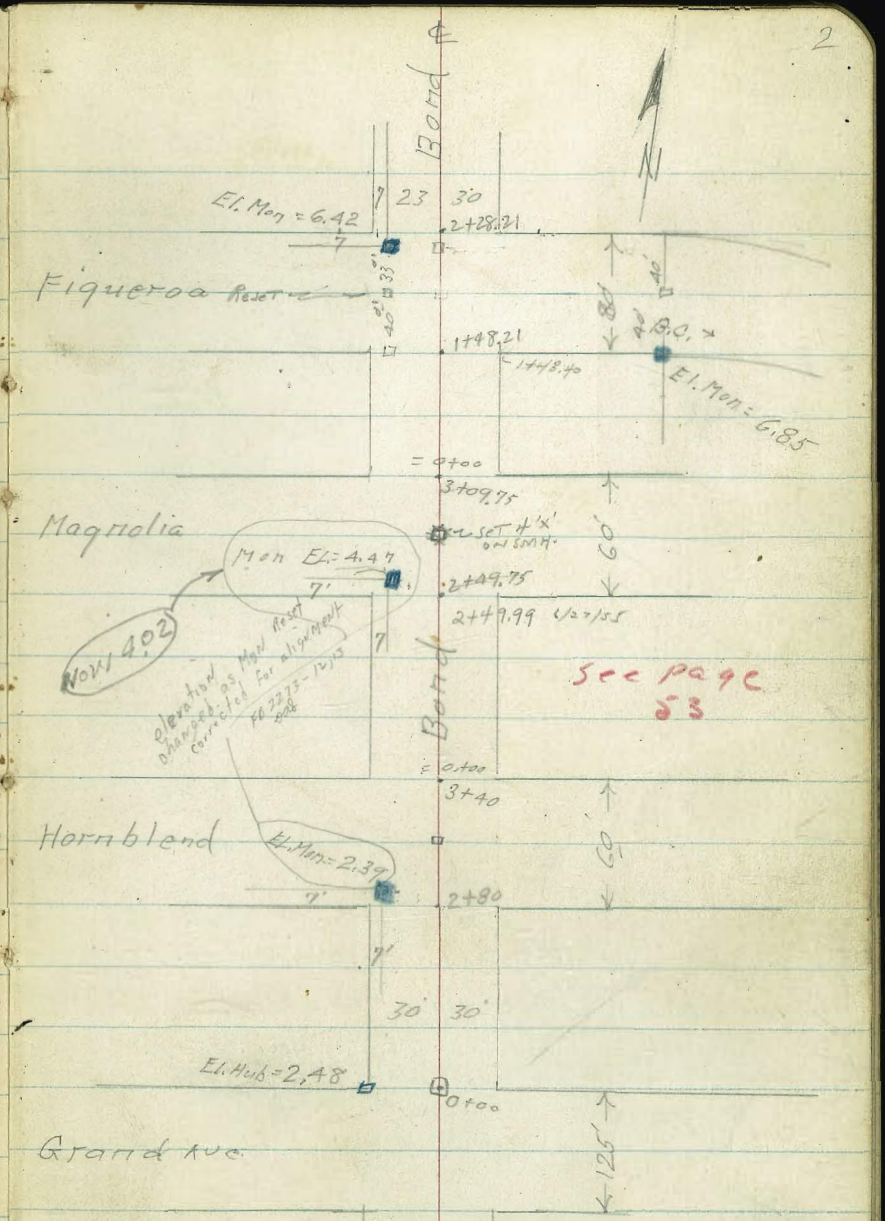
□ - " Set stub & Tack.

Map 1530

T.P. book #20

E. & W. meas. of Bldgs. shown First.

For Re-X-Sec see page 53



Bond St. levels
See Page 53 - 6/28/55

3/20/52

2+00

1+92 20'Lt 20'Rt
1+66 20'Lt 20'Rt
1+41 20'Lt 20'Rt
1+17 20'Lt 20'Rt } = 2' Diam. Palm
1+00

0+92 20'Lt 20'Rt } = 2' Diam Palm.
0+66 20'Lt 20'Rt } = 2' Diam. Palm
on blocks - part foundation (31'x37'
0+65 56'Lt. = S.E. Cor. Frame House part

0+40 20'Lt. 20'Rt } = Ctr. 2' diam. palm.
Frame, dirt floor
0+57 94'Lt. = S.E. Cor Conc. Tile Gar. 20'x18'
0+16 20'Lt 20'Rt } = Ctr. 2' diam Palm
on Conc. slab.
0+15 123 Lt. = S.E. Cor 36'x29' Frame House

19'Rt 18'Lt } = start Conc. curbs
0+00 = N'ly line Grand

Lt

1.7	4.7	2.15	1.3	1.6	2.0	2.25	4.6	4.6	
40	30	18	18		18	18	30	40	
		CL				CL			

3.8	3.8	1.66	1.1	1.4	1.7	1.61	4.2	4.3	
40	30	18	18		18	18	30	40	
		CL				CL			

5.8 Floor
3.8 56 Grd

3.7 57 Floor

4.1 123 Floor
3.6 123 Grd

3.2	2.8	1.5	1.08	0.6	1.0	0.8	1.24	1.8	3.8	3.8
40	30	23	18	18		18	18	28	30	40
			CL				CL			

Bond

= 0+00

3+40 = Nly. line Hornblend

4.6	4.4	2.90	2.0	2.0	2.4	2.82	4.5	4.5
40	30	ol	18		18	18	30	40
		18						

3+38 (20'Lt, 20'Rt) = E.C. ol. Rel

2.87
20
ol. E.C.

2.82
20 ol. E.C.

3+28 (28'Lt, 28'Rt.) = B.C. 10' Rad. ol. Rel

3+28 (30'Rt, 30'Lt) = start Conc. ol.

2.85	2.85	2.73	2.73
30		28	30
st. ol.	28 ol. B.C.	ol. B.C.	start ol.

3+10 = Σ Horn blend

2.5 2.1 2.4
30 30

2+92 (30'Lt, 30'Rt.) = end Conc. ol.

2+92 (28'Lt, 28'Rt) = ol. E.C.

2.52	2.54	2.51	2.52
30	28	28	30
end ol.	ol. E.C.	ol. E.C.	end ol.

2.56
18
ol. B.C.

2.51
18 ol. B.C.

2+82 (18'Lt, 18'Rt.) B.C.

2+80 = S'ly line Hornblend

4.2	4.2	2.55	1.5	2.0	2.2	2.50	4.6	4.5
40	30	18	18		18	18	30	40
		ol				ol		

2+66, 2+41, 2+16 (20'Lt, 20'Rt) = 2' Diam palm

Bond St.

{30' Rt / 30' Lt} = End curb.

2+61.75 {28' Rt / 28' Lt} = E.C. 10' Rad. Cl. Rot.

4.94 30 cc. | 4.90 28 cc. EC. | 4.61 28 EC. | 4.70 30 cc

2+51.75 - {18' Lt / 18' Rt} = B.C. 10' Rad Cl. Rot.

4.77 18 cc. B.C. | 4.52 18 cc. B.C.

2+49.75 = Sly Magnolia

6.2 A0 | 6.2 30 | 4.72 18 cc | 3.7 18 | 3.9 | 4.2 18 | 4.55 18 cc | 6.0 30 | 5.9 40

2+00

6.5 A0 | 6.6 30 | 4.41 18 cc | 3.2 1.8 | 3.7 | 3.7 18 | 4.35 18 cc | 6.0 30 | 6.0 40

1+87 - 21' Lt. = 18" Diam Palm

1+00

6.0 40 | 6.1 30 | 3.65 18 cc | 2.3 18 | 2.9 | 3.0 18 | 3.80 18 cc | 5.4 30 | 5.5 40

0+86 20' Lt. = Ctr. 18" Diam Palm.

108' X 44' -
Conc. block Conc. slab floor.

0+53 46' Lt. = S.E. Cor. Multi-unit Court

6.0 46 floor | 5.3 46 Gnd

0+38 - 28' Lt. = Ctr. 18" diam palm on Conc. slab.

0+02 - 45' Rt. = S.W. Cor. 30'x25' house Under Const

44 A5 Gnd. | 5.2 45 floor

Bond St.

1+60 — 30' Rt. = end curb.
28' Rt. = E.C. 10' Rad. Cl. Ret.

1+50 — 18' Rt. = B.C. 10' Rad. Cl. Ret.

1+48 — = Sly. line Figueroa

1+00

Foundation - Wood floor,
0+70 — 45' Rt. = 38'x24' Frame house Conc.

=0+00
2+09.75 = Nly line Magnolia
3+09.75

3+07.75 — 18' Rt. } = E.C. 10' Rad. Cl. Ret.
~~2+07.75~~ — ~~18' Rt.~~ }

28' Rt. } = B.C. 10' Rad. Cl. Ret.
2+97.75 — 30' Rt. } start 6" conc. Cl.

2+79.75 = ℄ Magnolia

5.99 6.00
28 30
E.C. Cl.

5.87
18
Cl. B.C.

6.6 6.4 5.0 5.1 — 5.1 5.87 6.18 6.9
40 30 17 — 18 18 30 40
Cl

6.4 6.2 4.6 4.8 — 4.9 5.68 6.5 6.6
40 30 17 — 18 19 30 40
Cl

6.6 7.A
45 45
End Floor

6.2 6.0 4.1 4.1 — 4.3 5.10 5.9 5.9
40 30 17 — 18 18 30 40
Cl

5.06
18
Cl. E.C.

~~+8~~
~~Cl. E.C.~~

~~36~~ ~~28~~
~~Cl~~ ~~Cl BC~~

5.20 5.22
28 30
Cl. B.C Cl

4.3 4.2 4.4
30 30

Bond St.

℄

2+28 21 = Nly. line Figueroa

2+26 21 18' Lt. / 18' Rt. } E.C. 10' Rad. Cl. Rot.

2+16 21 28' Lt. / 28' Rt. } B.C. 10' Rad. Cl. Rot. / 30' Rt. / 30' Lt. } start Cl.

1+88 21 ℄ Figueroa

7.2 40 | 7.0 30 | 6.54 18 Cl | 6.0 18 | 6.3 | 6.1 18 | 6.57 18 Cl | 6.5 30 | 6.6 40

6.55 18 Cl. E.C. | 6.58 18 Cl. E.C.

6.57 30 Cl | 6.56 28 Cl. B.C. | 6.54 28 Cl. B.C. | 6.56 30 Cl

5.8 30 | 5.8 | 5.9 30.

HORNBLEND St 4-9-52

W.O. 25020

Cross Sec. for grade Est'mt.

Sommermeyer
Begg
Oltman

See Page 64

Map 1530
T.P. book 20

■ = Fd. Mon. T.P. #20

□ = Set, stub + tack

· = Nail

Ely + Wly. Meas. of houses & other Bldgs. as shown first.

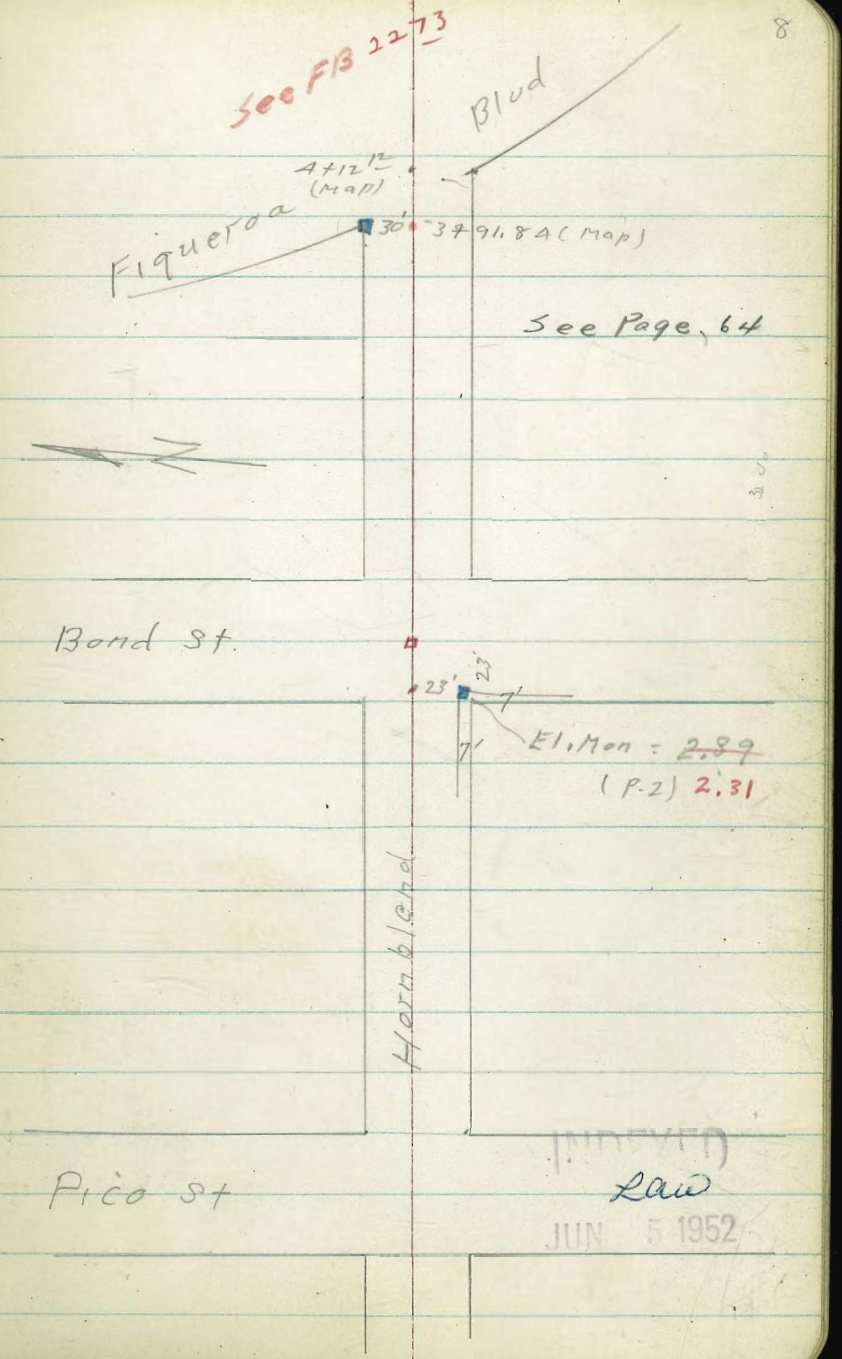
G. = ground

F. = Floor level of Bldg.

Note: Direct Elev. Fid. used

Figures shown are elevations.

See FB 2273



APPROVED
Law
JUN 5 1952

Hornblend

T.P. Rock 4.77

2+00

1+63.5 47' Lt. = S.W. Cor 31'x72 House. Conc. foundation

1+63 93' Lt. = ℄ double Gar.

1+41 31.5' Lt. = 9' wide Conc. Dr.

1+04 51' Lt. = 42'x35' S.W. Cor house. Conc. foundation

1+00

0+55 - 52' Lt. = on Conc. slab S.W. Cor. 33'x24' House

0+25 Top of wash

0+00 = Ely line Pico (in wash)

B.M. El. = 2.39 =

℄

9

5.3 / 30 — 4.8 — 5.0 / 30

7.1 / 47 / F — 5.6 / 47 / G

6.4 / 93 / Gar. Floor

6.07 / 60 / Gar. Floor — 5.74 / 31.5 / drive

7.5 / 51 / F — 5.6 / 51 / G.

5.5 / 30 — 4.4 — 4.5 / 30

5.9 / 52 / F — 5.5 / 52 / G

4.9 / 30 — 3.9 — 4.3 / 30

2.3 / 30 — -0.5 — -0.3 / 30

S.W. 7' Mon. Bond + Hornblend

Horn blend

= = 0+00 18' Lt. / 17½' Rt. } = end Conc. curb

6+60 = Ely. line Bond

6+00 = { 18½ Lt. / 17½ Rt. } = start conc dr. / Wly. line bond

Conc. slab floor
128' Lt. = N.E. Cor. G unit court
5+85 84' Lt. = S.E. Cor. G unit court

5+00

128' Lt. = N.W. Cor. G unit court
84' Lt. = S.W. Cor. G unit court } Conc. Block slab floors
4+75

4+00

3+77 31' Lt. = ± ( ) wide Conc. drive to Ent. Gar.

3+04 46' Lt. = S.W. Cor. 40' x 29' House Conc. foundation

3+00

B.

4.12 / 30 — 2.76 / 18' top cc — 2.5 — 2.55 / 17½' top cc — 1.4 / 30

4.7 / 30 — 2.70 / 18½ cc top — 2.9 — 2.48 / 17½ top cc — 4.4 / 30

5.9 / 128 / F — 5.6 / 128 / G — 5.9 / 84 / F — 5.8 / 84 / G

4.5 — 3.6 — 4.2 / 30

5.9 / 128 / F — 5.6 / 128 / G — 5.9 / 84 / F — 5.4 / G / 84

5.3 / 30 — 4.2 — 4.8 / 30

5.31 / A C / Gar. floor — 5.25 / 31 / drive

6.9 / F. — 5.0 / G

5.2 / 30 — 4.6 — 5.1 / 30

Hornblend

4+12.12 Rt.= Wly line Figueroa to South

3+91.84 Lt.= wly. line Figueroa to North

3+00

2+56 61' Lt.= S.W. Cor. 22' X 45' house. Conc. Foundation

12+42 60' Rt.= ± Sing. Car. dirt Floor

12+37 80' Rt.= N.W. Cor. dwelling (shack)

2+06 51' Rt.= N.W. Cor. 24' X 43' House on + blocks Foundation

2+00

1+00

0+55 34' Lt.= S.W. Cor. 30' X 25' house on Slab. Conc.

0+15 34' Lt.= S.W. Cor. 30' X 25' house on Slab. Conc.

#

5.8 5.7

8.0 5.8 5.7
30 30

6.8 5.2 6.2
30 30

11.0 8.5
61 61
F G

5.5
60 doorway
5.6 5.8
80 80
G F

5.3 7.1
51 51
G F

5.2 4.21 5.0
30 T.P. 30

5.0 3.7 5.0
30 30

5.4 4.6
34 34
F G.

5.1 4.5
34 34
F G

MAGNOLIA

X-Sec. From Pico to Figueroa

Sommermeyer
Bagg
Oltman

W.O. 85020

Map: 1530
T.P. Book 20

■ = Fd. Conc. Mon

● = Fd. pipe L.S. #2416

Direct Elev. Rod used

Figures shown are elevations

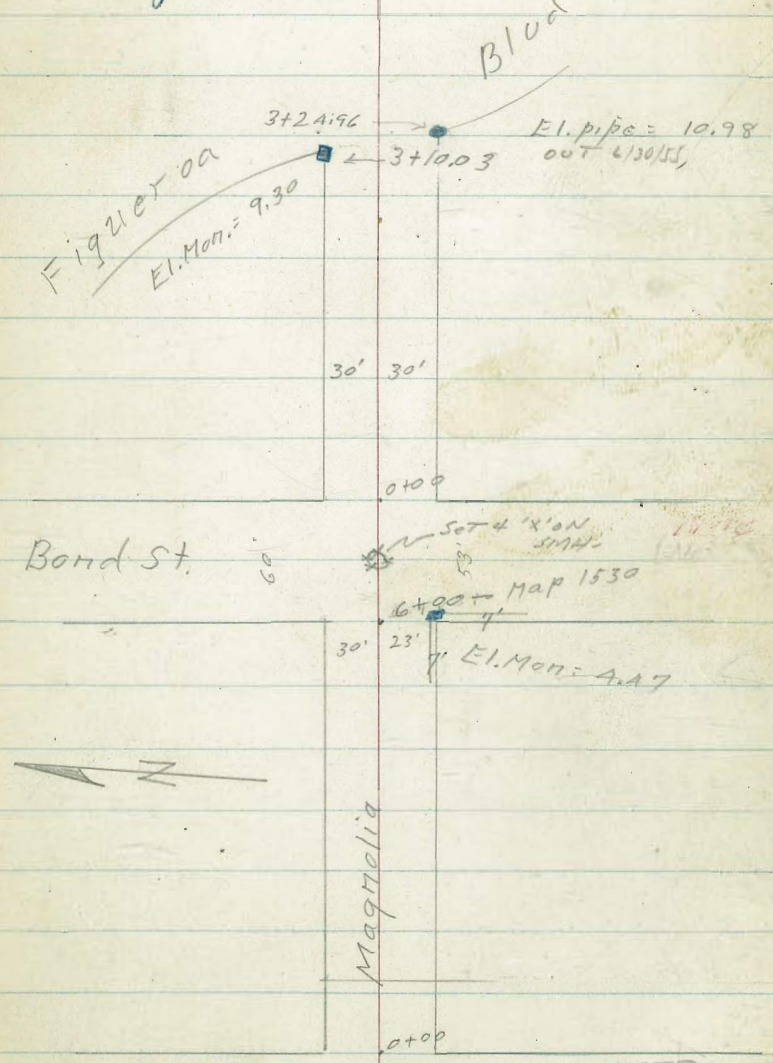
G = ground

F = Floor level

Note #1 Map #1530 seems in error on this distance. This is close enough for grade establishment so did not figure.

This note should be on page 18

Indexed



Magnolia Ave
levels

1+59	61' Rt. = ℄	Floor Slng Gar. Conc. conc. apron to	6.67 61 Apron	7.04 66 Gar floor	
1+31	28.5 Rt. = ℄	3' wide conc. walk	6.46 28.5 on walk	6.50 38.5	
1+19	44' Rt. = N.W. Cor.	conc. foundation ~~and floor~~ 24'x18' Frame house	6.7 44 ~~Gr~~	8.14 44 F	
1+06	52' Lt. = ℄	3' wide conc. step	7.50 52 step	7.2 52 G.	
1+00			6.7 30	6.3	6.3 30
0+93	55' Lt. = S.W. Cor.	house on conc. slab. 22'x20' stucco	7.8 55 F	7.2 55 G	
0+50.9			6.8 30	6.8	6.7 30
0+00 = Ely. Pic.			6.2 30	5.4	6.4 30
0-05		in creek wash	4.0 30	3.2	3.5 30
B.M. El. = 4.47 P.2			S.Wly. 7' Mon. Bond + Magnolia		

Magnolia

House. Conc. foundation
3+96 49' Lt. = S.W. Cor. 21'x24' frame

9.1 7.2
49 49
F Q

3+92 84' Lt. = ℄ double Car. dirt floor

7.3
84
G

3+77 31' Lt. = ℄ 3' wide conc. walk

7.30 6.7
41 31
on walk

3+62 49' Lt. = S.W. Cor. 21'x24' brick house

9.1 7.2
49 49
F Q

3+00

6.6 6.3 6.4
30 30

2+32 29½ = ℄ 3' wide Conc. walk

6.62 6.C
29½ 39½
walk walk

Conc. foundation
2+14 5' Rt. = N.W. Cor. Frame House 24'x26'

6.5 9.1
52 5.2
G F

2+00

6.8 6.4. 6.4
30 30

1+81 29' Rt. = ℄ 3' wide conc. walk.

6.36 6.55
29 39
on walk

House. Conc. foundation
1+70 44' Rt. = N.W. Cor. 24'x18' frame

6.6 8.6
44 44
G F

Magnolia.

from Bond St.

18' Lt. } = End existing curbs
=0+00 17½ Rt }

6+60 = Ely. line Bond St.

Also = Wly line Bond. St.

Bond. St.

6+00 16' Rt. = Start Conc. ch. on

Const. 29'x37' Conc. foundation

5+52 - 36' Rt. = N.W. Cor. house under

Conc. floor

5+32 49' Rt. = ℄ double Gar.

5+09 17' Lt. = ℄ 3' wide Conc. walk

5+00

Conc. foundation

4+98 45½ Lt. = S.W. Cor. 38'x31' frame house

4+07 30' Lt. = ℄ 3' wide Conc. walk

4+00

℄

5.18 5.23 5.28 4.6 4.4 4.1 4.67 4.74 5.9
30 18' 18 17 17½ 30
CC CC

(1)

5.8 4.4 4.2 4.90 5.2
30 16 16 30
C CC.

6.4 8.3
36 36
C F

6.3 6.7
49 49
C F

6.57 5.82
30 17
on walk

6.6 5.2 6.3
30 30

8.9 6.7
45½ 45½
F C

7.10 6.77
40 30
on walk

6.6 5.9 6.5
30 30

Magnolia

2+00

1+71- 27' Rt. = ℄ 3' wide Conc. walk

Conc. Floor East Front

1+05 - 45' Lt. = S.E. Cor. double Gar.

1+00

on Conc. slab.

0+97 33' Rt. = N.W. Cor. 30'x21' house

0+77 - 27' Rt. = ℄ 3' wide Conc. walk.

on Conc. slab.

0+57 33' Rt. = N.W. Cor. 30'x21' House

0+32 - 27' Rt. = ℄ 3' wide Conc. walk

on Conc. slab.

0+15 33' Rt. = N.W. Cor. 30'x21' House

Note: Rods showing 2 decimal places corrected .05' because of error on bench reading. Rods correct as shown.

7.9 7.4 8.2
30 30

7.25 7.32
~~7.30 7.37~~
27 32
on walk

7.59
~~7.64~~ 7.4 7.2
55 55 45
C+T. G G.
doors.

7.1 5.7 6.8
30 30

6.8 7.6
33 33
G F

6.65 6.74
~~6.70 6.79~~
27 32
on walk

6.95
6.1 ~~7.00~~
33 33
G F

6.33 6.49
~~6.38 6.54~~
27 32
walk

6.72
6.0 ~~6.77~~
33 33
G F

Magnolia

Figueroa + Magnolia

3+24.96 30' Rt. = pipe = S. Wly. Cor.

9.7 10.9
30

Figueroa + Magnolia

3+10.03 30' Lt. = Conc. Mon. = N. Wly. Cor.

(page 12)
El = 9.30

B.M. ~~9.35~~ 9.9 9.7 10.9
30 30 30
Mon C

3+00

10.0 9.4 9.8
30 30

FIGUEROA

Pico to Grand

4-14-52

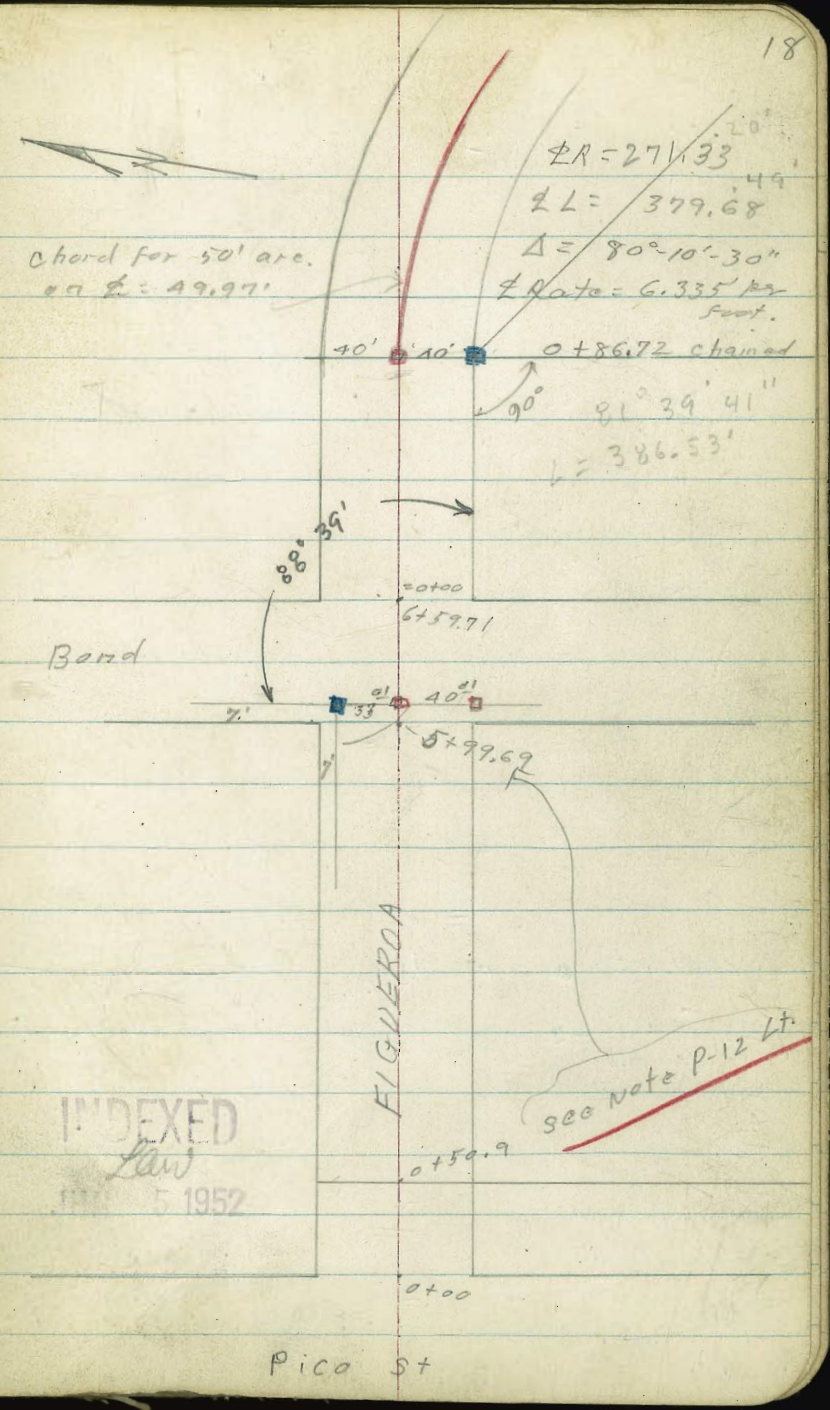
Map 1530

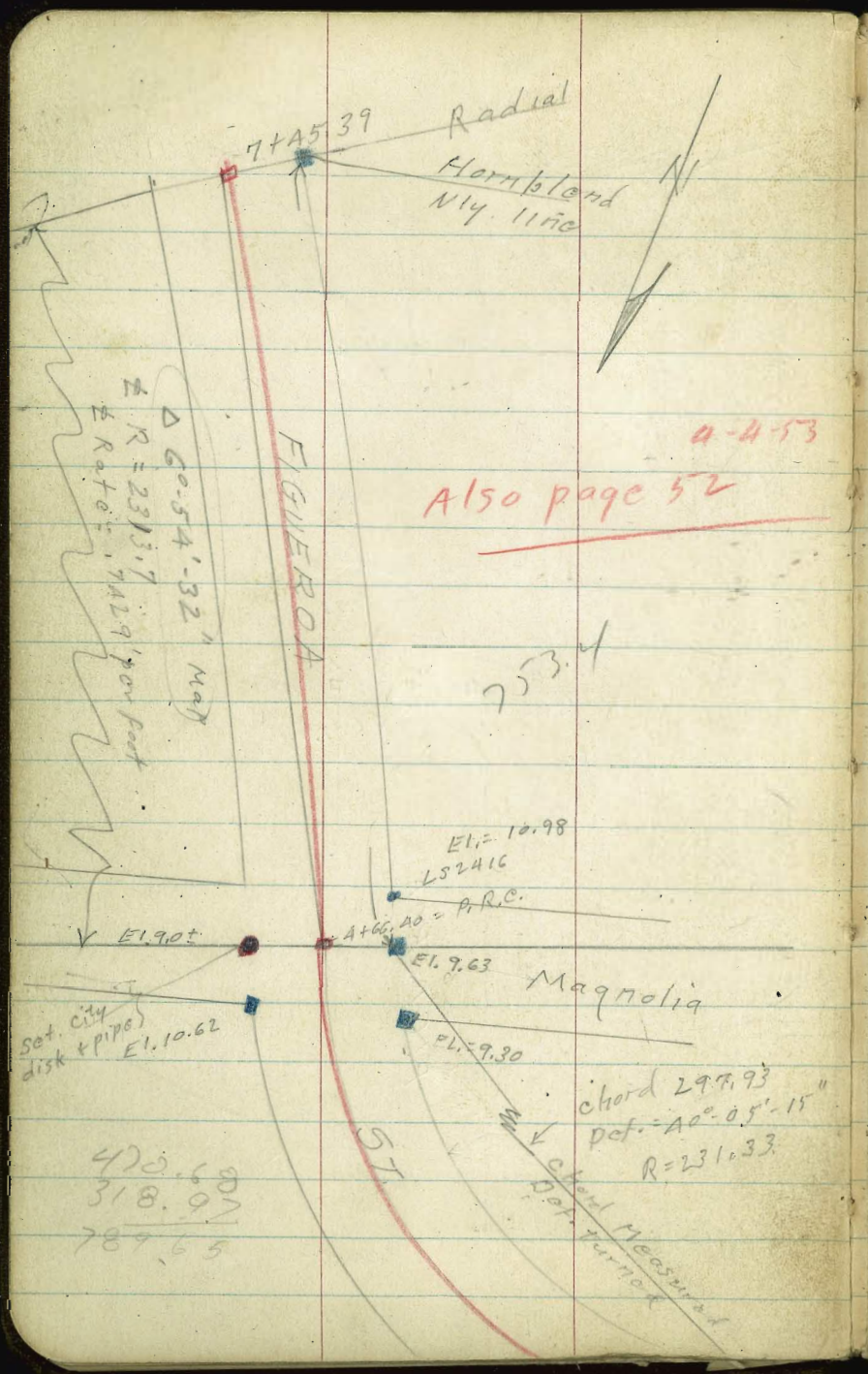
T.P. Book #20

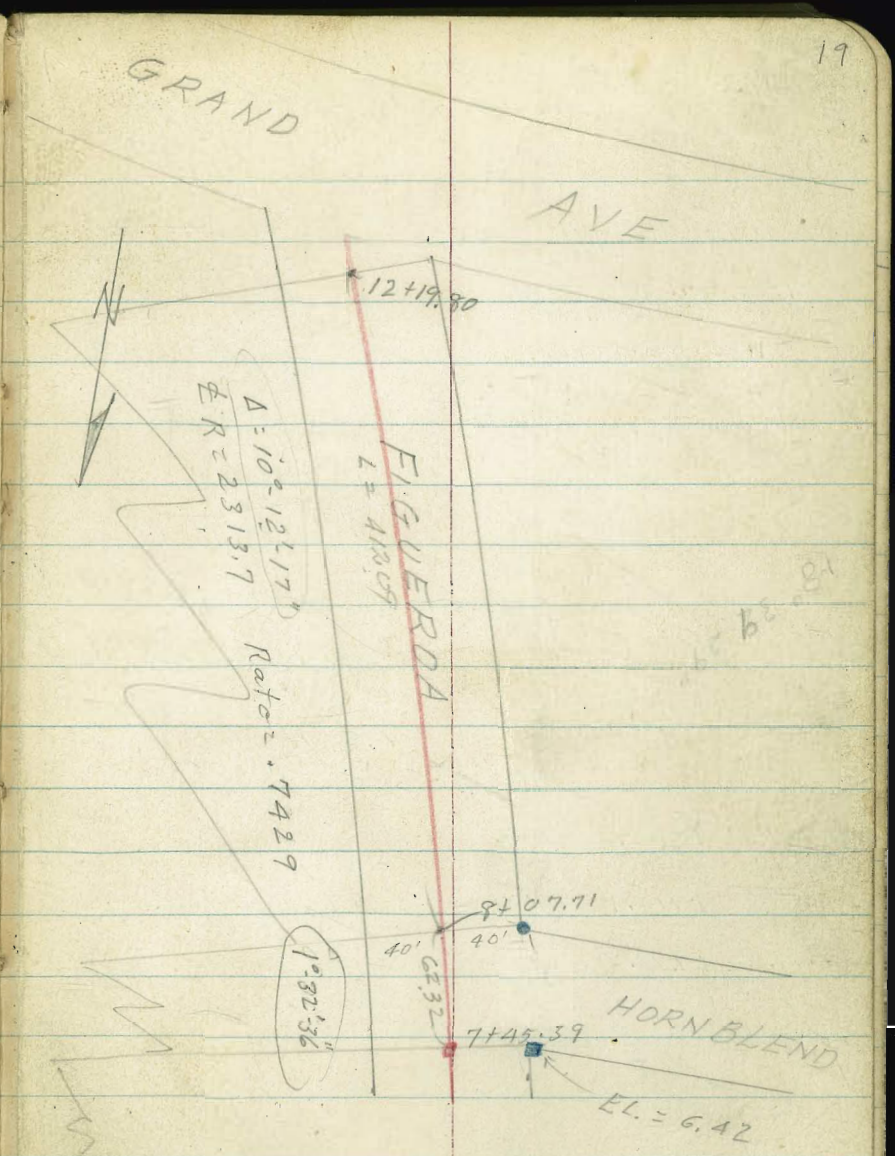
■ = Fd. Conc. Mon

□ = Set. Hub, or stub + tack

See FB 2273 - 7/7/55 & 57




7+A5.39
Radial
Hornblend
N'ly. line
FIGUEROA
Δ 60°-54'-32" Rt
R = 2313.7
Rate = .7429 per foot
a-4-53
Also page 52
753.4
El. = 10.98
LS2416
P.R.C.
A+66.40 = P.R.C.
El. 9.63
El. 9.90±
Magnolia
set. City disk + Pipe
El. 10.62
El. = 9.30
chord 297.93
Δ = A0°-05'-15"
R = 231.33
chord Measured
Def. turned
ST
470.68
318.97
789.65


GRAND
AVE
12+19.80
Δ = 10°-12'-17"
R = 2313.7
Rate = .7429
FIGUEROA
L = 410.09
1°-32'-36"
8+07.71
40'
40'
GE 32
7+45.39
HORNBLEND
EL. = 6.42

322.48

X-Sec. Grand Ave (old Ivy Ave.)
From Pico St. to East & South.

Sommermeyer
Begg
Oltman.

4-24-52
W.O. 25020

■ = Fd. Mon
■ = " ½ hub + Tack or disk
■ = set stub

T.P. Book 20
Map 1120
" 1530

For other work in
this area see.
X F.B. 1647-62X?

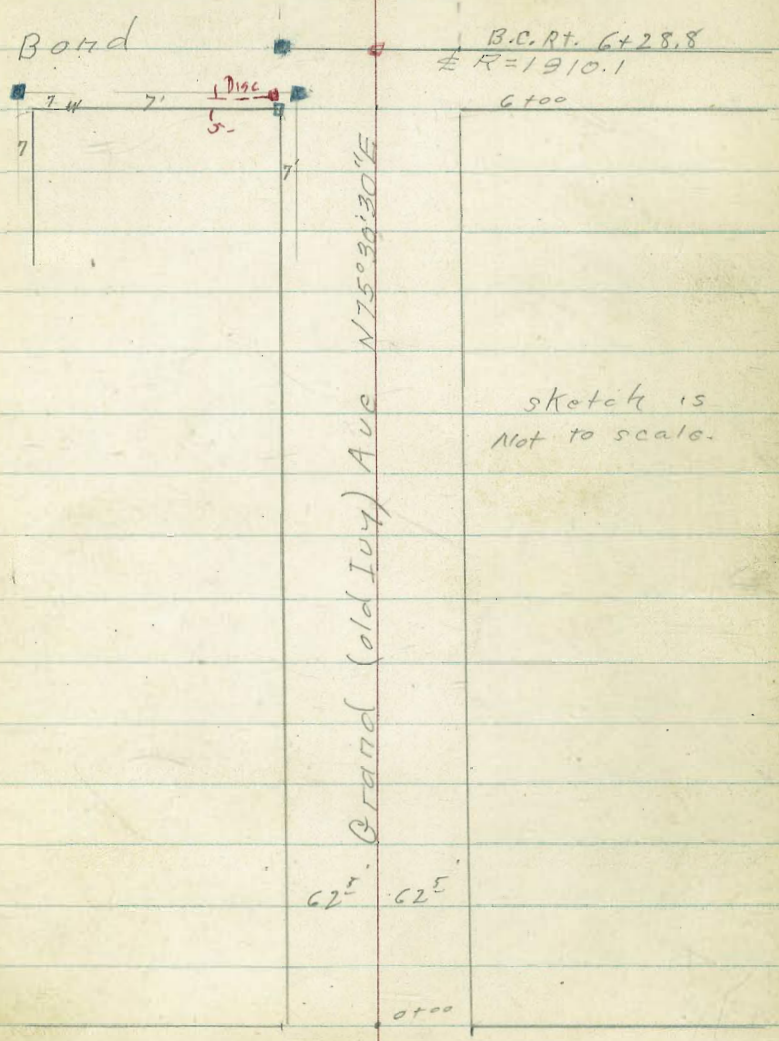
Rad. = 1847.6' Def. = .9303' per foot.

Rad. = 1910.1' Def. = .8999' per foot. ✓

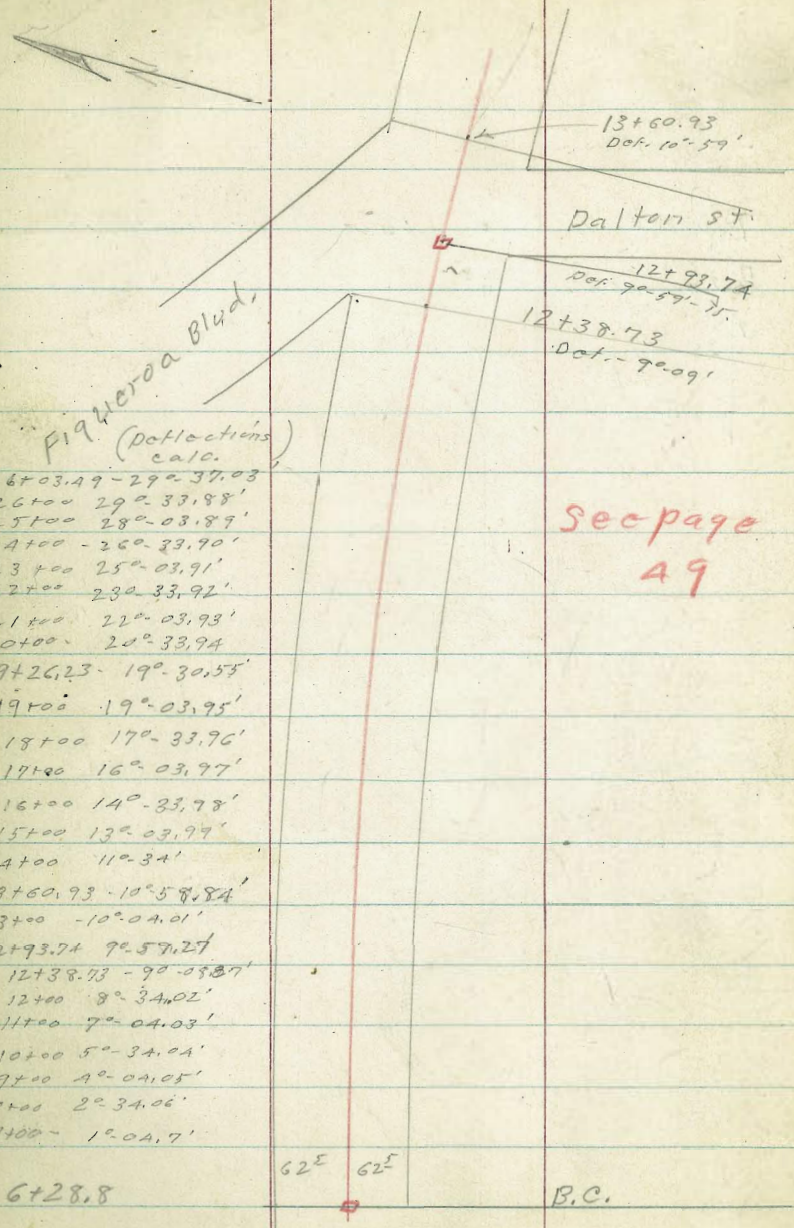
Rad. = 1972.6' Def. = .8714' per foot.

Indexed

20



sketch is
Not to scale.

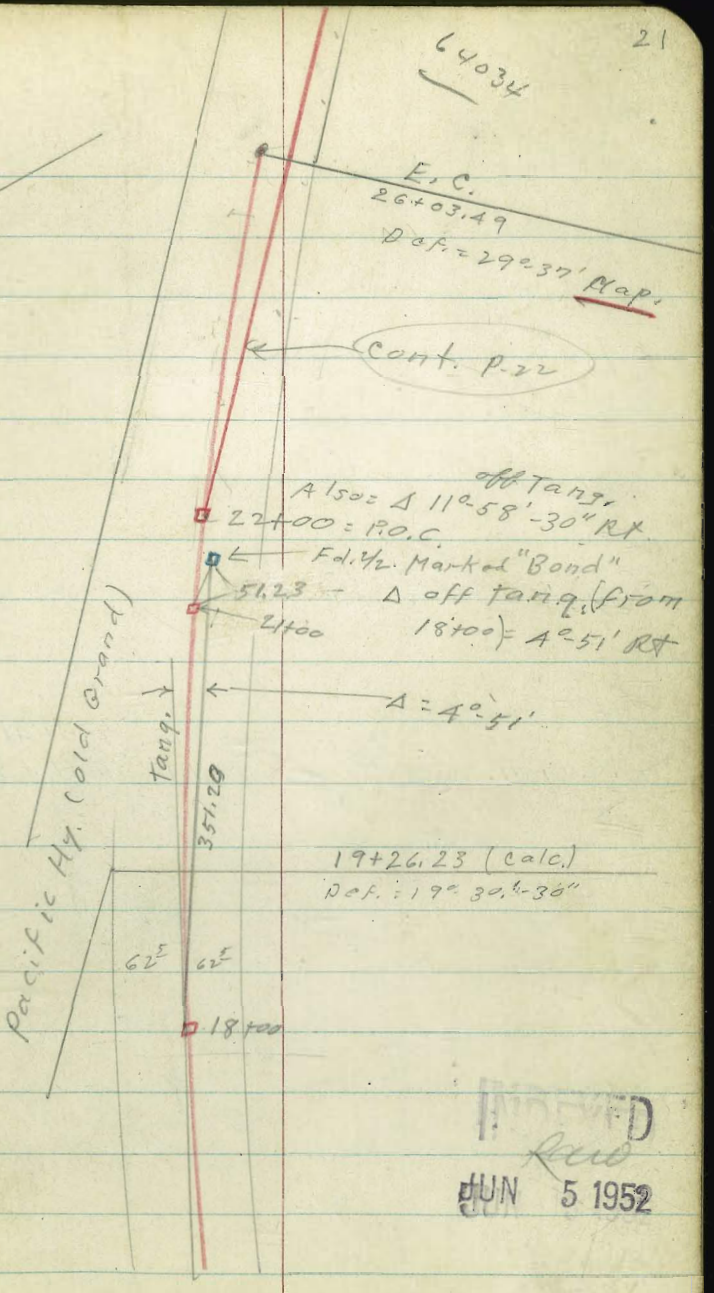


(Deflections calc.

26+03.49 - 29°-37.03
26+00 29°-33.88'
25+00 28°-03.89'
24+00 - 26°-33.90'
23+00 25°-03.91'
22+00 23°-33.92'
21+00 22°-03.93'
20+00 - 20°-33.94
19+26.23 - 19°-30.55'
19+00 19°-03.95'
18+00 17°-33.96'
17+80 16°-03.97'
16+00 14°-33.98'
15+00 13°-03.99'
14+00 11°-34'
13+60.93 - 10°-58.84'
13+00 -10°-04.01'
12+93.74 9°-59.27'
12+38.73 - 9°-08.27'
12+00 8°-34.02'
11+00 7°-04.03'
10+00 5°-34.04'
9+00 4°-04.05'
8+00 2°-34.06'
7+00 - 1°-04.7'

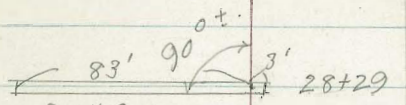
6+28.8

Seepage
49



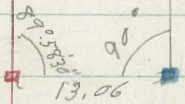
Mon. Sly. Line
P.L. 1208 1647/18

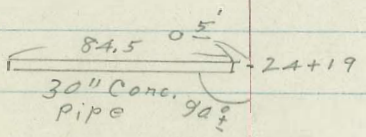
28+50± = Stub.



E.C. Mon. (1647/32) (Sta. 160+41.54 F.B. 1647-P32)

25+99.70





22+00 Δ (P.21)
Δ 11°-58'-30" Rt.

Levels GRAND Jct

	+	HI	−											
Beggs, Altman, Pullen.														
2 + 00				5.8	6.1	5.4	6.6	4.0	4.2	8.5	8.7			
				200	100	62.5	25		15	25	62.5 new fill			
	4.36	9.41	3.65	5.15				9.41						
1 + 00				5.3	5.0	5.2	5.5	5.4	6.3	7.2				
				200	100	62.5			62.5	100	200			
0 + 60 Top of bank					5.5	5.6	5.0		5.1	5.7				
					100	62.5			62.5	100				
0 + 30					10.8	11.5	13.2		17.8	13.6				
					100	62.5			62.5	100				
0 + 00 = Ely line Pico					14.6	13.6	13.6		13.6	13.6				
					100	62.5			62.5	100				
T.R.	3.65	8.80	4.30	5.15				8.80						
~~T.R.~~	~~6.97~~	~~9.45~~	~~4.30~~	~~5.15~~										
	6.97	9.45	—	2.48										

N. W. ¼ Bond + Grand. 12

9.75 12.23 693 2.48

6+00 West line Bird

5+00

4+94 ℄ con wall

4+74 ℄ gbron & garage

4+00

3+00

house level

1 car gar

gbron

Grand

6.02
9.01
(15.03) Diff. = 0.05

Sta. 10+25±
Fd. Temp. B.M. #7 (El. 14.98) 6.32 6.02

10+00

9+00

TP 6.49 12.34 6.38

Top of 10th 9+00
5.85

12.34

8+00

see page 49

7+00

6+28.80 Bk

12.23

12.23

Grand

14+00

13+60 93 62½ Lt.: N.E Figueroa + Grand

13+00

12+93.74 62½ Rt.: S.Wly. Dalton + Grand

12+38 73 62½ Lt.: N.Wly. Figueroa + Grand

T.P. 5.73 11.67 6.40 5.94

12+00

11

11+00

4

3+	13	-.05	0	6	7.6	0	7	
8.0±	10.4	12.2	11.6	4.8	4.1	5.7	4.4	
100	62½	40	30		3 D	8	62½	

7+	2+	0	0	6+	7.5	5.8	6.7	
4.6	9.5	11.5	11.3	5.3	4.2	6.1	5.0	
200	62½	50	35		3 D	10	62½	

7.0	6.8	0	7.8	6.9	7.3	4.4	5	
4.7	4.9	11.4	8.0	4.8	4.4	6.8	5.4	
200	80	62½	11		2 D	10	62½	

	0	2	6.2		7.3	4.9	6.7	
	11.5	9.0	5.40		4.4	6.8	5.4	
	62½	10	Stub.		3 D	10	62½	

0	
11.0	
62½	

11.67

3.7	0	0	5.7		7.6	3.5	4.7	
8.6	11.6	11.4	7.2		4.7	8.4	7.6	
1	62½	50	25		7 D	17	62½	

3.7	0.8		5.2		4.0	3.2	4.1	
7.0	11.5		7.1		4.3	7.1	8.2	
	62½				6 D	25	62½	

12.34

Grand

Now part of Pac. Blvd.
old Grand ave.

19+26.23 $62\frac{5}{}$ Lt. = Intersect wly line
(E. P. = wly edge Pac. Blvd. Pave.)

19+00				
T.P.	6.23	13.53	5.46	7.30
18+00	stub	P.O.C.		
17+00				
16+00				
T.P.	4.23	12.76	3.14	8.53
15+00				

				7.8			
3.9	7.5	7.7	5.6				
91	$62\frac{5}{}$	35					
E.P.							
				7.7			
7.1	8.0		5.7	4.0	5.9	5.0	
$62\frac{5}{}$	35			20 D	30	$62\frac{5}{}$	
				13.53			
				7.30			
7.2	8.9	8.9	5.46	1.4	5.7	5.0	
100	$62\frac{5}{}$	35	stub	9 D	11	$62\frac{5}{}$	
				6.5			
8.8	10.1	10.3	6.3	4.9	6.0	5.2	
150	$62\frac{5}{}$	35		6 D	11	$62\frac{5}{}$	
				6.3			
7.8	8.6	10.5	11.4	6.5	4.5	5.8	4.8
200	150	$62\frac{5}{}$	35		5 D	8	$62\frac{5}{}$
				12.76			
				7.2			
9.4	10.6	10.7	4.5	3.6	4.7	3.4	
$62\frac{5}{}$	55	30		3 D	6	$62\frac{5}{}$	
	120						
				11.67			

Grand

T.P. 1.80 10.92 4.11 9.12

24+00

23+00

Blvd. Pavement.
This Fwd. line is 10' west of Pac.
Δ of 4°-51' Rt.

22+00 = P.O.C. [Also = leave curve on

21+51.23 = ½ hub (marked "Bond")

T.P. 3.92 13.23 4.22 9.31

21+00

20+00

BL

9+4	6+2	9+4	7+2	7+5	
4.8	7.0	3.8	6.0	5.7	
10		9	13	62.5	
E.P.		D			

5+1	6+6	6+1	7+0	7+1	
4.7	6.6	4.6	6.2	6.0	
10		6	12	62.5	
E.P.		D			

5+0	8+4.4	6+9	9+5	7+0	7+6
4.2	4.7.9	6.3	3.7	6.2	5.6
10		18	25	30	62.5
E.P.			D		

5+1
4.68
℄
Bond

13.23

9+1	8+1	6+5	9+4	7+2	7+8
4.3	4.9	7.0	4.1	6.3	5.7
35		23	31	40	62.5
E.P.			D		

9+1	9+2.5	8+9	8+1	9+5	7+8	
4.3	4.3	6.9	5.4	4.0	5.7	
65	62.5	35		30	62.5	
E.P.				D		

13.53

28+50

86' Lt. = Intake 24" Conc. culvert
28+29 3' Rt. = outlet 24" diam conc. culvert

28+00

T.P. 4.63 12.82 2.73 8.19

27+00

26+03 ± 13' Rt 3.96

Mon. LS 1880

26+00

25+70. 115' Rt. = Δ (to south) in dyke

25+50 - 25' Rt. = Δ (to west) in dyke

25+00

85' Lt. = Inlet 30" Conc. culvert
24+19 05' Lt. = outlet 30" Conc. Culvert

Reduced By Lockwood 5-1-52

	B.L				
7½	7½			8½	
5.6	5.2			6.9	
E.P.				100	
3.8	6.2	6.0		2.5	1.6	6.2
9.74	7.1	10.22		10.3	11.2	6.9
86		3		4	75	125
I.E.		I.E.				
7½	7½			5½		
5.4	5.4			6.9		
10				50		
E.P.						
7½	7½		8½	6½		
3.4	3.5		6.1	4.6		
10			100	150		
E.P.						
7½	7½		5½	7½	6½	
3.1	3.8		5.9	3.5	4.9	
10			106	115	120	
E.P.				D		
7½	5½		5½	4½	7½	7½
3.1	5.3		5.9	2.5	3.8	3.6
10			12	25	30	100
E.P.				0		
3½	2½					
7.28	8.43					
85	05					
I.E.	I.E.					

10.92

Figueroa

Pico to Grand

Indexed

sketch - P 18 + 19

2+00	7.4 / 40	7.2	6.9 / 40	
1+82 40' Rt. = ℄ 8' wide Conc. drive		7.29 / 40' Drive	7.84 / 66 Gar. Floor	7.87 House Floor
1+47 44' Rt. = ℄ 4' wide conc. walk		7.35 / 44 walk	7.80 / 54	7.69 House Floor
1+27 43' Rt. = ℄ 8' wide conc. drive		7.65 / 43' Apron	7.70 / 58 Gar. Floor	
1+00	7.6 / 40	7.4	7.2 / 40	
0+15	8.6 / 40	8.0	8.2 / 40	
0+00 = Ely line Pico = Top of bank	5.7 / 40	7.7	8.2 / 40	
0-30 in wash	+0.2	-0.2	-0.6	

B.M. #1 6.42 ?

B.M. = N.W. 7' Conc. Mon. Bond + Figueroa

4+00

3+94 40' Lt. = ℄ 8' wide conc. Dr.

3+85 - 40' Lt. = ℄ 3' wide conc. walk

3+71.36 ~~3' conc walk~~ 3' Lt. = ℄ 3' wide conc. walk

3+17.38 3' Lt. ℄ Conc. walk 4' wide ~~383 H~~

3+00

2+57 41.5 Rt. = ℄ 4' wide conc. walk

2+37 41.5 Rt. = ℄ 8' wide conc. drive

7.3 40

6.7

8.0 40

7.60 60 drive

7.44 40

7.59 50 walk

7.37 40

7.32 36.2 walk

7.56 40 Step

8.15 40

8.18 50 walk

10.0 8.17 7.62

60.0 54.3 38.3

floor walk

house

7.4 40

7.1

7.8 40

7.38 41.5 walk

7.53 5.2

7.72 House floor

7.31 41.5 drive

7.73 60 Gar floor

Figueroa

= 0+00
6+59.71 = Ely. line Bond

B.M. #1 - P 30 — 6.42

5+99.69 = Wly. line Bond

5+21 40' Rt. = ℄ 3' wide conc. walk

3+00

4+95 55' Rt. = ℄ 2 car. Gar. conc. floor

4+27 41.5' Lt. = ℄ 3.5' wide conc. walk

4+05 36.3' Rt. = ℄ 3' wide conc. walk

℄

7.5 / 40 — 5.9 — 6.8 / 40

7.1 / 40 — 5.8 — 6.7 / 40

7.54 / 40 walk — 7.60 / 50

7.6 / 40 — 6.5 — 7.1 / 40

7.74 / 55 floor

7.58 / 50 walk — 7.46 / 41.5

7.36 / 36.3 — 7.56 — 7.81 / 40.5 stop — 8.24 / 50

4+00 Def. 33°-04'-30"

3+50 Def. 27°-48'

3+00 = P.O.C. 22°-31.13'

2+50 Def. 17°-14' 52' Rt. = house under const.

2+00 Def 11°-57'

Def. = 9°-38'

1+78 45' Lt. = ℄ 6' wide conc. walk

1+50 Def. 6°-41'

1+00 Def 1°-24.13'

0+86.72 = B.C. Rt.

10.7		9.2		9.4	
40				40	
10.2		8.8		8.7	
40				40	
9.6		8.1		8.3	
40				40	
9.7	9.3	7.8		8.4	8.9
65	40			40	52
Gnd. at house					Approx Floor Level
8.6		7.4		8.0	
40				40	
9.22	8.98				
55	45				
walk					
8.8		7.0		7.9	
40				40	
7.7		6.7		7.2	
7.7		6.7		7.3	
40				40	

T.P. 8,88

4

34

6+50 Def 2°-16'-30"

9.3 8.2 9.5
40 40

6+00 Def 1°-39'-30"

9.7 8.9 10.6
40 40

5+50 Def 1°-02' Lt.

10.7 9.5 11.1
40 40

5+00 Def. 0°-25' Lt

10.8 10.1 10.8
40 40

4+66.40 P.R.C. Def.= 40°-05'-15" Rt.

10.2 10.0 9.63 ✓
40 40
on Mon
+ Gud

4+50 Def 38°-21'

11.0 9.9 10.1
40 40

9+50.	Lt	5°-59.30'		5.6 / 40	4.0	4.3 / 40
9+00	Lt	5°-22.15'		6.0 / 40	4.4	4.6 / 40
8+50	Lt	4°-45'		5.8 / 40	5.0	5.6 / 40
8+07.71	Lt	4°-13.57'	Sly. on west Hornblend	6.6 / 40	5.6	5.8 / 40
7+76.54	Lt	3°-50.42' Radial	90° p.19	7.0 / 40	6.1	6.0 / 40
7+45.39	Lt	3°-27.27' Rad	Nly. on west Hornblend	7.6 / 40	6.8	7.8 / 40 — 6.42 / 40 Mon.
7+00	Lt	2°-53.56		8.6 / 40	7.4	9.4 / 40

T.P. 4.06

12+00	9°-05.05'	6.8	6.8	2.0	0.8	1.2	2.8	2.8	
		60	50	40		40	41	50	
11+50	8°-27.90'	6.3	6.3	1.9	1.1	3.4	3.4		
		60	50	40		40	50		
11+00	7°-50.75'	6.4	6.4	3.3	2.2	2.0	4.3	4.5	
		60	50	40		40	45	60	
10+90	42' Rt. = ℄ Sing Gar. dirt floor					2.0			
						42			
						Floor			
10+50	Def 7°-13.60	6.1	6.1	3.8	2.8	2.9			
		60	45	40					
	see p-52								
10+00	Def, 6°-36.45'	6.8	6.8	4.5	3.5	3.6			
		60	45	40		40			
9+80	44' Lt. = ℄ Sing. Gar. dirt floor					3.8			
						44			
						Floor			

12+50 Dep 9°-42.20'

6.1	6.1	1.2	0.5	0.3
60	50	40		40

Dep. 9°-20' culvert

12+20 ± 53.5 L.= & 24" diam. E.+W. Conc.

6.6	2.15	1.7	
60	53.5	50	
	I.E.	Out	

Dep. 9°-19.76'

12+19.80 = N.y Grand on west

6.6	6.6	20	1.1	0.8
75	55	40		40

7-30-52

T. Stamper ☐ W.O. 64036

R. Sisson ✗

R. Shorey ∅

A. Sherry ∅

LOCATION & PROFILE OF PROPOSED WATER LINE FROM BOND ST. ALONG GRAND NELY; THENCE SLY. ALONG DALTON TO INTERSECTION PARK BDY. ACCESS ROAD.

CURVE DATA

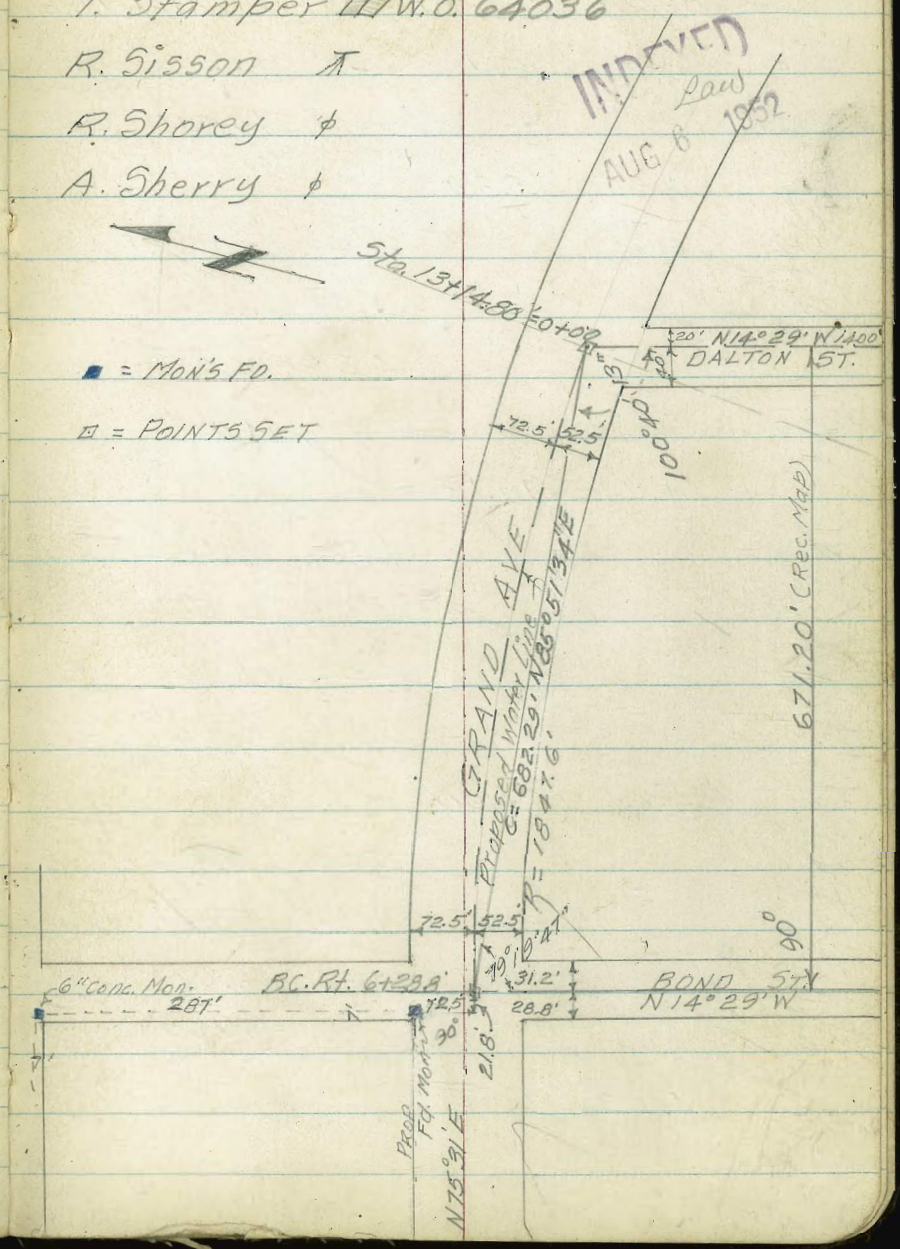
R = 1900.10 Δ = 20°41'09" L = 686.00'

d/ft = .90462259 L.C. = 682.29'

STA	DEF. L	Chord
B.C. Rt. 6+28.8	0°00'00"	
7+00	1°04'25"	71.20
8+00	2°34'52"	100.00
9+00	4°15'20"	"
10+00	5°35'48"	"
11+00	7°06'16"	"
12+00	8°36'43"	"
13+00	10°07'11"	100.00
P.O.C. 13+14.80 =	10°20'34"	14.80
0+00 Dalton St.		

■ = Mon's Fd.

⊡ = Points Set



PROFILE OF PROPOSED WATER LINE

7-30-52

STA	+	H.I.	−	ELEV.	
B.M. #I				14.04	NOTE: See Layout Sketch Page 38
	4.35	18.39			Top 2"x2" Hub See F.B. M.B. No 77-4
Along Dalton 14+00			4.62	13.77	Top 1"x1" flush With Top Ground
Along Dalton 13+00			4.60	13.79	" " " " " "
Along Dalton 12+00			4.34	14.05	" " " " " "
T.P. Dalton 11+00			3.94	14.45	
	4.74	19.19			
Dalton 10+00			4.73	14.46	" " " " " "
Dalton 9+00			4.64	14.55	" " " " " "
Dalton 8+00			4.23	14.96	" " " " " "
T.P. Dalton 7+00			3.70	15.49	" " " " " "
	5.01	20.50			
Dalton 6+00			4.59	15.91	" " " " " "
Dalton 5+00			4.54	15.96	" " " " " "
Dalton 4+00			4.86	15.64	" " " " " "
T.P. Dalton 3+00			4.39	16.11	" " " " " "
	4.03	20.14			

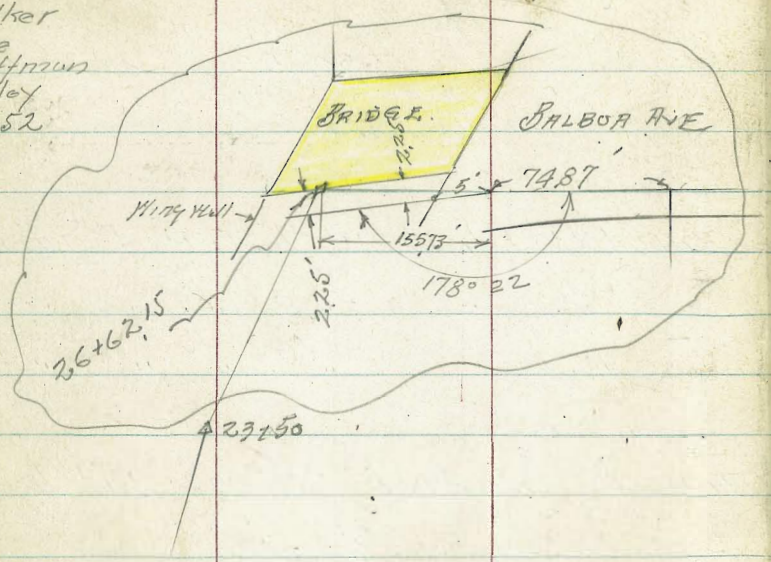
PROFILE OF PROPOSED WATER LINE CONTD

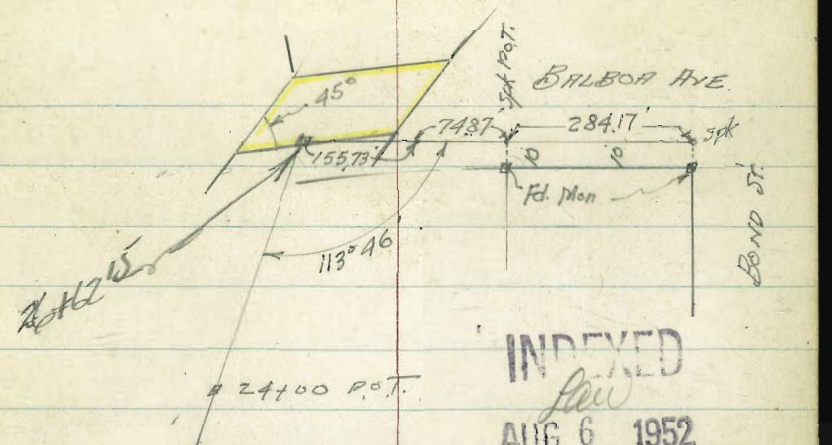
7-30-52

STA	+	H.I.	−	ELEV.		
		20.14				
Along Dalton 2+00			3.75	16.39		Top 1"x1" flush with Top of ground
Along Dalton 1+00			4.24	15.90		" " " " " " "
Dalton 0+00 = 13+14.80 Grand			5.09	15.05		" " " " " " "
T.B.M.			9.81	10.33	10.36	Top 2"x2" Sta 8+00 Drainage Ditch
Along Grand 12+00			5.4	14.7		See M. Bay F.B. #69-12
T.P. Grand 11+00			5.21	14.93		Top 1"x1" Hub flush with top of ground
	4.25	19.18				
Grand 10+00			4.6	14.6		
Grand 9+00			4.7	14.5		
Grand 8+00			4.8	14.4		
Grand 7+00			4.7	14.5		
B.C. Grand 6+28.8			5.69	13.49		Top 2"x2" Hub B.C. 6+28.8 flush.
	3.34	16.83				
T.B.M.			5.38	11.45	11.50	Top 2"x2" Hub Drainage Ditch F.B. #69-12
B.M.			8.00	8.83		Top 6"x6" Conc. 1' off Prop. N.W. Cor. Bond & Grand Ave intersection Mon. is Aprox 1.5' below ground Surface

Cross Section - Rose Canyon Creek

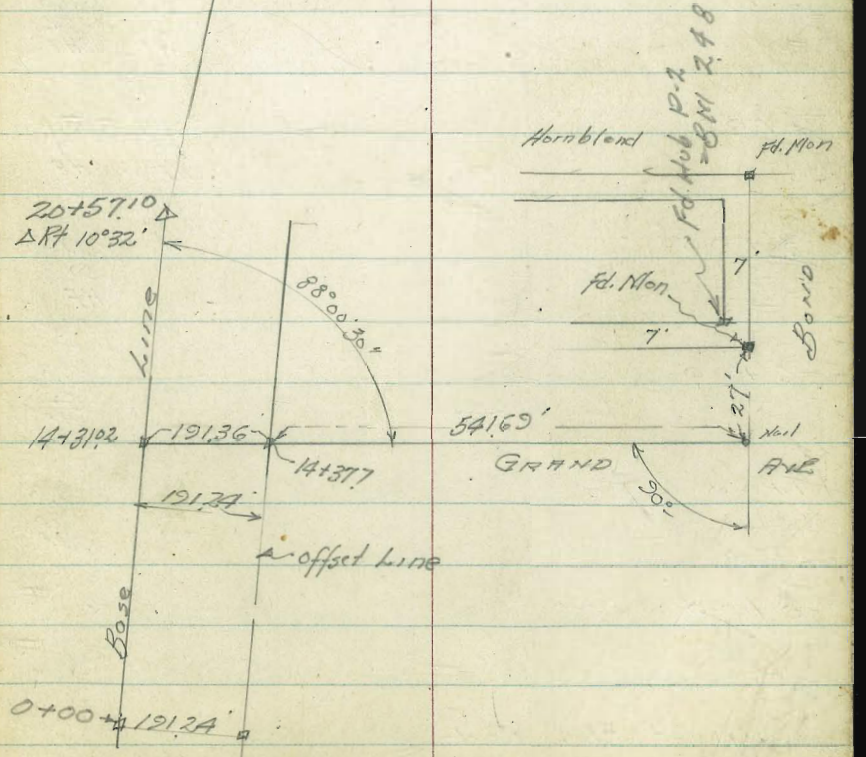
Walker
Pope
Huffman
Presley
8-6-52





24+00 P.O.T.

23+50
Δ Rt 11° 30'



T.P. # 3
Set B.M. on Triang. Sta. "Anza" 5.78 - 1.32

T.P. #2	3.91	4.43	5.39	0.52
T.P. #1	4.76	5.21	6.43	1.65
B.M. on 2"x2" Nail Bond & Grand.	5.60	8.08		2.48

Cross Section Rose Canyon Creek

Note:
BHF = Beg. Hyd. Fill.
H.F. = " "
Muck = Unsuitable Material
H.T.L. = High Tide Line

Lt. | ℄ Base Line | Ft.

7+00
Lt: 4.8 / 29 / HF
℄: 0.1 / 17 / BHF
Ft: -0.6 -1.2 -3.5 (GH 68 Muck W Side Ch.) -4.6 (148 Muck E Side Ch.) -3.0 (152) 0.7 (164) 0.5 (190) -1.2 (234) 0.4 (270 BHF) 2.8 (295 H.F.)

6+00
Lt: 4.4 / 50 / HF ; +4.4 / 28 / HF
℄: -0.3 / 17 / BHF
Ft: -1.2 -1.5 (82) -3.3 (100) -5.2 (103 Muck W Side Ch.) -4.3 (154 Muck E Side Ch.) -1.5 (158) 0.4 (165) 0.6 (190) 0.4 (277 BHF) 2.9 (300 HF)

T.P. #4 0.52

5+00
Lt: 3.8 / 50 / HF ; 3.8 / 26 / HF
℄: -0.8 / 14 / BHF
Ft: -1.4 -1.7 (77) -2.6 (92) -5.0 (98 Muck W Side Ch.) -4.3 (153 Muck E Side Ch.) -2.0 (157) +1.5 (165) +0.7 (175) +0.2 (283 BHF) +1.3 (295 HF)

4+00
Lt: 3.0 / 50 / HF ; 3.0 / 19 / HF
℄: -0.4 / 8 / BHF
Ft: -0.8 -0.4 (85) -4.9 (93 Muck W Side Ch.) -4.6 (158 Muck E Side Ch.) -2.7 (163) 0.0 (175) +0.7 (290 BHF) +1.4 (300 HF)

3+00
Lt: 2.9 / 50 / HF
℄: 2.9 / 13 / HF
Ft: -0.8 BHF -1.5 (78) -4.7 (83 Muck W Side Ch.) -4.6 (167 Muck E Side Ch.) -3.0 (172) -0.2 (191) -0.3 (290 BHF) +1.2 (302 HF)

2+00
Lt: 2.8 / 50 / HF
℄: 2.8 / 10 / HF
Ft: -0.5 BHF -1.6 (88) -5.0 (88 Muck W. Side Ch.) -4.4 (173 Muck E Side Ch.) -2.2 (184) -1.7 (200) -0.5 (209) -0.5 (305 BHF) +1.2 (315 HF)

1+00
Lt: 2.8 / 50 / HF
℄: 2.8 / 10 / HF
Ft: -0.5 BHF -1.3 (75) -4.3 (88 Muck W Side Ch.) -3.8 (175 Muck E Side Ch.) -1.9 (178) -2.7 (203) -4.1 (218) -1.0 (308 BHF) +1.3 (325 HF)

0+00
℄: -1.3 / 20 / ~~BHF~~
Ft: -1.6 0 -1.2 (62) -4.1 (95 W Side Ch.) -4.1 (168 Muck E Side Ch.) -2.2 (172) -2.1 (196) -0.9 (210) -1.8 (300 BHF) +1.0 (330 HF)

Direct Elec. Rod.

Direct Elec. Rod used.

Cross Section Rose Canyon Creek

	Lt.		Base Line				Rt.				
11+90	5.1 50 HF	5.1 42 HF	3.1 31 BHF	-0.5	-1.5 High Tide Line Muck W side ch	-1.5 190 H.T.L. E side ch	-0.1 250	2.0 267	2.7 300		
T.P. #5	0.70										
11+85 = Beg. Wider Channel	5.2 50 HF	5.2 42 HF	2.7 31 HF	1.8	0.2 60	-4.2 80 Muck W side ch.	-4.7 147 Muck E side ch	-3.6 165	-0.6 173	+2.3 240	+3.4 300 BHF
11+00	5.6 50 HF	5.6 39 HF	1.3 25 BHF	0.8	-0.7 74	-4.5 81 Muck W side ch	-1.8 157 Muck E side ch	1.2 190	2.2 240 BHF	2.2 250 HF	
10+00	4.9 50 HF	4.9 39 HF	0.2 27 BHF	0.0	0.2 68	-2.6 82 Muck W side ch.	-3.2 162 Muck E side ch	0.5 168	2.1 220 BHF	2.1 250 HF	
9+00	4.8 50 HF	4.8 34 HF	0.4 24 BHF	-0.4	0.5 62	-3.0 76 Muck W side ch.	-4.2 149 Muck E side ch.	-2.3 155	1.1 166	2.0 220 BHF	2.0 250 HF
8+00	4.3 50 HF	4.3 36 HF	1.3 21 BHF	0.2	-1.0 65	-4.5 72 Muck W side ch.	-4.1 156 Muck E side ch	0.2 164	0.5 263 BHF	2.7 285	

Cross Section Rose Canyon Creek

℄ Base Line

RT

Cont. P-46	17+00	4.8 70 School yd.	5.6 40	0.0 25	-0.4	-2.0 20					
17+00							-1.5 98 H.T.L.	4.3 137	3.8 220	17+00	
16+50		16+50	4.4 60 School yd.	6.4 25	0.0	-1.4 25					
16+17	171' Rt. Tel. Pole #464073-H										
16+00		4.0 50 School yd.		4.0 25 School yard.	3.7	-0.7 18	-1.5 43 H.T.L. Muck. W. side ch.	-1.5 123 H.T.L.	3.8 160	3.4 240	
15+00				3.5 35 School yard.	3.0	0.2 50	-1.5 75 H.T.L. Muck. W. side ch.	-1.5 147 H.T.L. Muck. E. Side Ch.	2.8 179	3.5 240	
14+43	"Bgn. New Hyd. Fill on Lt. "Beg. School Yard.										
14+00		5.6 60 HF	5.6 47 HF	3.2 40 BHF	3.8	3.3 20	-1.5 38 M.H.T. Muck W side Ch	-1.5 176 H.T.L. Muck E. side ch.	3.9 188	3.0 240	
13+60	14.3 Rt. "Power Pole #2599										
13+00		5.9 60 HF	5.9 45 HF	3.9 34 BHF	3.4	3.2 20	-1.5 38 HTL Muck W side ch.	-2.0 180 Muck E side Ch.	2.5 200	2.4 240	2.7 300
12+45		5.6 50 HF	5.6 41 HF	3.5 30 BHF	3.6	-1.5 19 High Tide Line Muck					

Rose Canyon Creek

See next page

Stadia Location Bulkhead from Station 24+00 ℄ Base Line

Angles Left of Forward Tang.

Dist.		
145	78°	NWLY End.
132	77°07'	Δ in Bkhd.
111'	79°05'	" " "
92'	82°50'	" " "
75'	98°30'	" " "
59'	109°34'	" " "
59'	143°30	" " "
68'	159°	" " "
83'	168°35'	" " "
101'	174°50'	" " "
177'	183°47	SELY End.

Rose Canyon Creek

	Lt	Base Line	Rt
22+22 = Beg. Blkd. Wall	6.5 14 on Wall	0.3 14 on Wall	
22+00	3.0 50	0.0 10	-1.0 -0.7 5.1 5.0 +7.0 40 45 68 73
21+00	+6.0 3.4 -0.8 1.1 1.7 2.5 150 138 114 100 84 33	-0.6 10	-0.6 0.9 4.4 4.7 4.5 6.8 6.8 20 34 50 87 95 115
20+57.10 = ΔRt 10°32'		0.72 on stub.	
20+00	5.5 5.5 1.7 0.2 -2.0 -0.7 160 145 School yd. 138 118 108 95	0.4 50	-0.3 -0.4 -1.7 -1.9 2.8 5.0 3.0 3.2 6.5 10 15 33 48 74 92 118 133 5.3 155
19+00	+5.5 2.2 0.6 -2.5 132 115 94 80 School yd.	-0.7 50	0.6 -0.5 -2.1 -2.1 -0.2 3.0 4.0 2.5 5.3 21 24 40 45 77 104 123 138
T.P. #6	-0.64		
18+00	5.2 6.8 0.3 0.6 100 78 62 46 School yd.	-1.3 38	-1.0 -1.5 -2.0 4.3 4.8 22 65 140 190 H.T.
Cont. from P-44			

Rose Canyon Creek

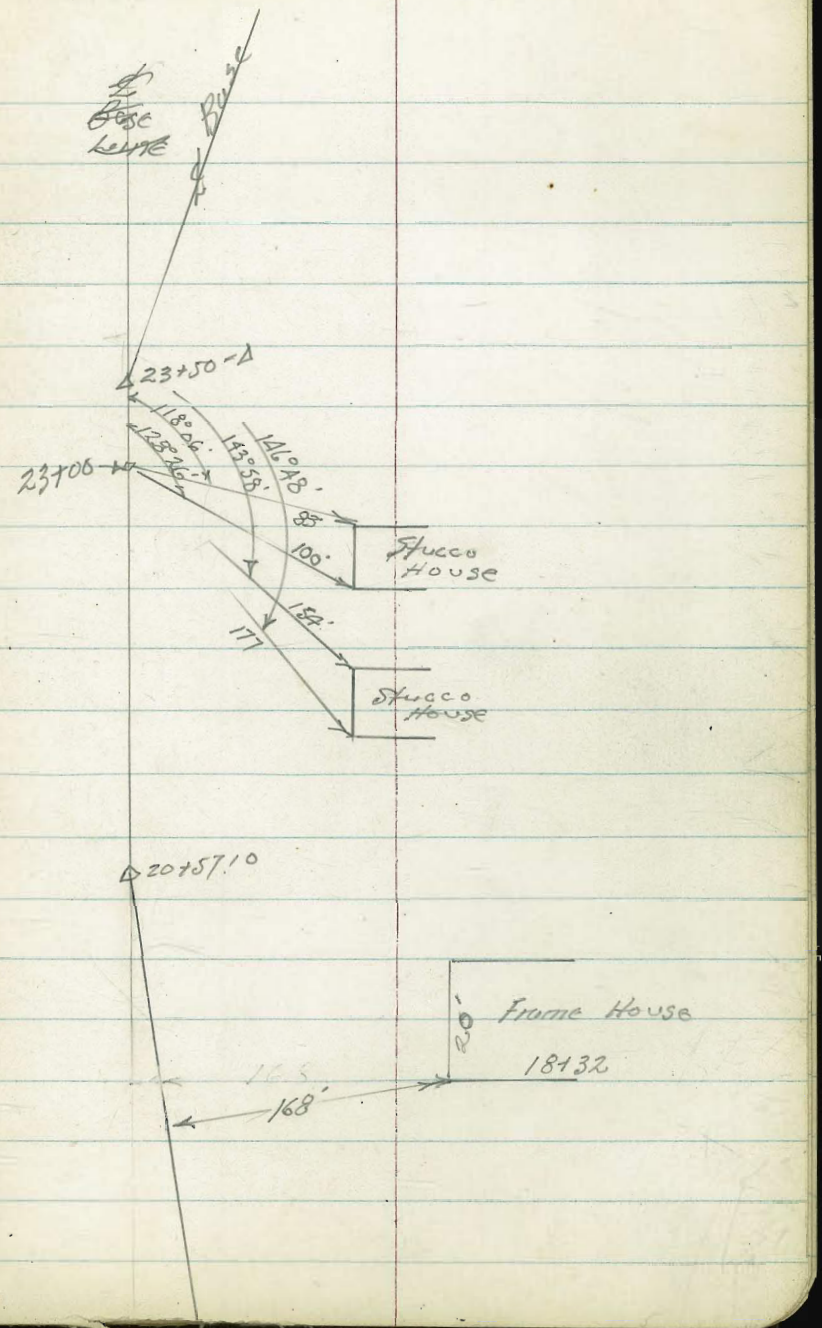
		0.02											
		642 = P.I.											
Chk NH 7' Mon Bond & Figueroa		6.42											
TP #10		13.04											
TP #9		8.66											
2646 2.15													
T.P. #8 on 1"x1" Pine stake		2.27											
Sec. Parallel with Bridge													
2.6+62.15 on 1"x1" Pine stake under Bridge					3.3	2.27		1.1	1.1	2.2	2.4		
					24 at Wing Wall	on Pine stake		37	95	114.	154 at Wing Wall		
2.6+00		9.0	8.0	4.6	-0.5	0.0		0.0	0.6	2.4	4.8	8.0	8.0
		50	27	16	3			18	41	60	82	85	100
2.5+00	9.5	9.5	4.8	1.5	0.8	-0.5		0.9	8.5	2.5			
	120	90	80	65	38			32	44	65			
2.4+00		0.7		0.0	-0.7	+0.1		2.6	7.0	7.6			
		62+ at wall		40	19			26	33	50			
T.R. #7													
2.3+50 = Δ R 11°30'		-1.00				-1.00 on stub.							
2.3+0.0				6.5	-1.0	-1.1		0.0	7.1	7.6			
				18	18			28	50	80			
				Wall	at wall								

Rose Canyon Creek

Studio Location Stucco Houses
Near Ely Bank Creek

Note: Any Material moved from Easterly Bank of Creek may endanger the Houses shown in sketch

8-6-52



Grand Ave 4/4/53
Sketch P-20

T.P.	4.91	10.13	3.74	5.22
8+00				
7+00 Cont.				
7+00				
6+00				
5+00				
4+00				
	6.48	8.96	—	2.48

addl notes

4.0 2.4 1.9 3.0 3.1 5.2 5.2 5.5 5.6
5.0 6.6 7.1 6.0 5.7 3.8 3.8 3.5 3.2
62½ 60 35 33 20 7 15 62½

0.5
4.8 7.4 8.5
62 42 40

0.5 1.4 3.0 6.3 6 5.9 5.5 5.0
8.5 7.6 6.0 2.6 2.9 3.1 3.5 4.0
37 36 24 14 14 17 62½

2.5 3.0 3.0 4.5 4.7
6.5 6.0 6.0 4.5 4.3
62½ 3 5 62½

3.4 2.5 2.5 4.0 4.5
5.6 6.5 6.5 5.0 4.5
62½ 50 25 62½

3.1 2.7 4.8 4.3
5.9 6.3 4.2 4.7
62½ 14 62½

8.96

N.W. cor. ½ Bond + Grand. (Page 1)

Grand

T.P	6.00	11.68	4.45	5.68
12+00				
11+00 Cont				
11+00				
10+00				
9+00 Cont				
9+00				

2.1 1.7 5.1 5.3 5.7 5.6
8.0 8.4 5.0 4.8 4.9 4.5
625 26 5 20 625

3.0 2.0 2.1
7.1 8.1 8.0
625 60 40 0

1.6 2.4 2.5 4.9 4.9 5.8 5.6
8.5 7.7 7.6 5.2 5.2 4.3 4.5
24 23 17 4 20 625

3.3 2.0 1.9 5.7 5.7 5.8 5.4
6.8 8.1 8.2 4.9 4.9 4.3 4.7
625 60 24 4 30 625

3.4 2.3
6.7 7.8
625 59

2.1 2.9 3.6 5.7 5.1 5.5 5.6
8.0 7.2 6.5 4.9 5.0 4.6 4.5
25 24 11 7 40 625

10,13

		Grand	7.54	2.49									
	4.60	10.03	6.25	5.43									
S.S. #1	Nail		8.66	3.02									
16+00					2.4	1.7	1.4	1.8	5.9	9.3	7.1		
					9.3	10.0	10.3	9.9	5.8	4.4	4.6		
					62E	50	29	16		3	62E		
						2.1	1.1	2.4	6.7		6.9		
15+00						9.6	10.6	9.3	5.0		4.8		
						62E	18	11			62E		
					1.6	1.5	1.8	2.7	6.1		6.7		
14+00					10.1	10.2	9.9	9.0	5.6		5.0		
					62E	26	20	11			62E		
				2.0	1.8	0.9	1.7	2.0	4.0	5.7	6.3		
13+35				9.7	9.9	10.8	10.0	9.7	7.7	6.0	5.4		
				62E	32	26	24	12	9		62E		
					2.0	2.0	0.9	1.1	3.4	5.6	6.3		
13+30					9.7	9.7	10.8	10.6	8.3	6.1	5.4		
					62E	32	30	26	18		62E		
					2.0	1.3	1.3	2.4		5.3	6.2		
13+00					9.7	10.4	10.4	9.3		6.4	5.5		
					62E	33	26	24			62E		
											11.68.		

Figueroa 4/4/53

Additions after fill.

See page 18 + 36

Indexed

12+50

1.7	2.2	1.8
6.0	5.5	5.9
40		40

12+00

3.3	1.7	2.4	1.4	3.1
4.4	6.0	5.3	6.3	4.6
40	35		37	40

11+00

5.7	2.6	2.8	2.7	4.2
2.0	5.1	4.9	5.0	3.5
40	35		35	40

10+00

4.7	3.5	3.5	2.7	3.4
3.0	4.2	4.2	5.0	4.3
40	25		25	40

No fill back of here

4.70 7.72 - 3.02

S.S. #1 Nail P.51

Re-x-sec Bond ST- Grand Ave
To Figueroa- X-sec Bond ST
Figueroa to Balboa Ave.
WO# 32-83- 6/28/55

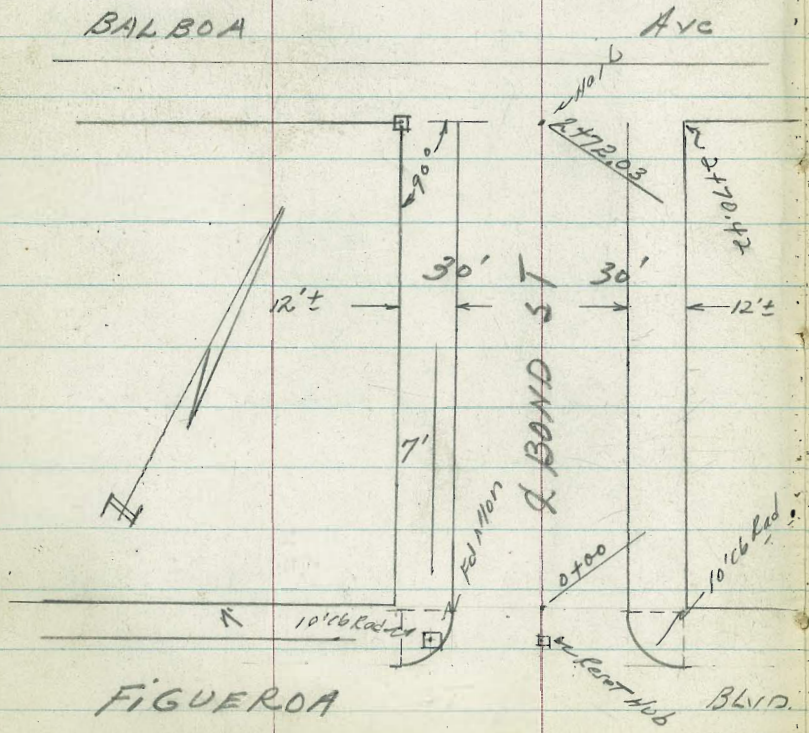
C. Allen, D. Sisson, C. Powell, R. Parks-

See Page 2 + et al-

For Location of Houses See Page 3 + etc.

0+00 = Nly Line Grand Ave

elev. Rim SMH at 4° LT of Stat. 0-20 = 2.82



INDEXED
JUL 11 1956

℄ Nly ℄ RT = 0/y - 53
Bond
ST

Note: Ely Curb is 17' ely of ℄
+ Wly Curb is 19' Wly of ℄-

3°	3 2/5	10 8/10	2 3/10	2 4/10	1 3/10	1 24/100	2 2/10	3 1/10	3 6/10
50	30	19 T.C.	19 WTT	17 DIRT	17 T.C.		23	30	50

Direct elev Rod

Grand Ave under Construction this date-

For sketch of Bond ST - Grand To Figueroa See page 2-

BM = 2" x 2" Hub N Wly Cor Grand & Bond ST. EL = 2.48- Page 2 + 41-

Curbs in Block Grand to Hornblend are covered deeply - impossible to tell condition of curb -

Re X-sec Bond St cont

T.C. = Top curb

1+12 — 18.5 RT = Wly of 12" Power Pole #P4423
20.8 LT = ely of 12" elec anchor pole

1+00

0+92 — 18.5 RT = Wly of 24" Palm tree
20.0 LT = ely of 24" palm tree

0+86 - 30.5 LT = ℄ 4' Wide conc walk steps to
0+78 - 21.2 LT = ℄ 3 water meteres

0+75

0+66 — 18.5 RT = Wly of 24" Palm tree
20.2 LT = Ely of 24" Palm tree

0+50

0+40 — 18.5 RT = Wly of Palm tree (24")
20.7 LT = ely of 24" palm tree

0+25

0+16 — 20.5 LT = ely of 24" Palm tree.
18.2 RT = Wly side 24" Palm Tree

0+11 - 18.5 RT = Wly side Fire Hyd

LT = Wly ℄ Bond, RT = ely

4.1 / 50 — 2.6 / 30 — 2.7 / 20 — 1.66 / 19 T.C. — 2.2 / 17 — 2.4 — 1.8 / 16 — 1.61 / 17 T.C. — 2.7 / 18 — 2.6 / 27 — 4.0 / 30 — 4.1 / 50

4.01 / 42.5 Walk — 3.73 / 32.5 Top Riser + Walk — 2.44 / 30.5 Bottom Riser

2.6 / 30 — 2.6 / 19 — 2.1 / 17 — 2.4 — 1.7 / 15 — 2.8 / 17 — 1.8 / 27 — 3.6 / 30

3.4 / 50 — 2.5 / 30 — 1.48 / 19.0 T.C. — 2.1 / 19 DIRT — 2.3 — 1.8 / 14 — 2.3 / 17 DIRT — 1.46 / 17.0 T.C. — 1.8 / 27 — 3.3 / 30 — 3.9 / 50

2.9 / 30 — 1.8 / 26 — 2.7 / 21 — 2.3 / 19 — 2.2 — 1.6 / 16 — 2.0 / 26 — 2.9 / 30

Direct Rod

Re-X-Sec Bond cont

T.C. = Top C6

2+80 0^{0} = Sly line Horn Blend ℄

2+70 – 18^{2} RT = Wly of 10" Anchor Pole 474482 H

2+66 18^{3} RT = Wly of 24" Palm tree
19^{2} LT = Ely of 24" palm tree

2+50

2+49 – 18^{0} RT = ℄ Deadmon

2+41 18^{4} RT = Wly of 24" Palm tree
19^{8} LT = Ely of 24" palm Tree

2+25

2+16 18^{2} RT = Wly of 24" Palm tree
19^{2} LT = Ely of 24" palm tree

2+00

1+98 – 21^{5} LT = ℄ water meter

1+92 18^{5} RT = Wly of 24" Palm Tree
20^{2} LT = Ely of 24" Palm tree

1+84 – 30^{1} LT = ℄ 9' Conc drive

1+75

1+66 18^{6} RT = Wly of 24" Palm Tree
19^{2} LT = Ely of 24" Palm tree

1+50

1+41 – 18^{6} RT = Wly of 24" Palm tree
20^{2} LT = Ely of 24" Palm tree

1+25

1+17 20^{4} LT = Ely of 24" palm tree
18^{6} RT = Wly of 24" Palm tree

LT = Wly ℄ Bond RT = Ely

3^{9}_{50} 3^{3}_{30} $2^{5\frac{2}{19}}_{T.C.}$ $2^{9}_{19\ DIRT}$ 3^{0} 2^{3}_{14} $3^{2}_{17\ DIRT}$ $2^{5\frac{6}{17}}_{T.C.}$ 3^{4}_{30} 3^{7}_{50}

4^{9}_{40} 4^{3}_{33} 3^{6}_{30} $2^{5\frac{2}{19}}_{T.C.}$ $2^{9}_{19\ DIRT}$ 3^{0} 2^{2}_{14} $3^{2}_{17\ DIRT}$ $2^{4\frac{3}{17}}_{T.C.}$ 2^{7}_{25} 4^{6}_{30} 4^{2}_{50}

4^{2}_{30} 2^{5}_{18} 2^{8} 2^{0}_{15} 2^{8}_{18} 2^{4}_{27} 3^{2}_{30}

4^{6}_{45} 3^{9}_{30} $2^{1\frac{5}{19}}_{T.C.}$ $2^{6}_{19\ DIRT}$ 2^{5} 1^{9}_{15} 2^{8}_{17} $2^{2\frac{5}{17}}_{DIRT\ T.C.}$ 2^{3}_{25} 4^{0}_{30} 4^{3}_{50}

9^{2} at ℄ Ely of House

$4^{1\frac{2}{40}}_{Dr}$ $3^{7\frac{8}{30}}_{Dr}$

3^{7}_{30} 2^{6}_{16} 2^{3} 2^{0}_{15} 2^{7}_{17} 2^{8}_{26} 3^{7}_{30}

4^{2}_{50} 4^{0}_{30} 2^{1}_{27} $1^{2\frac{5}{19}}_{T.C.}$ $2^{7}_{19\ DIRT}$ 2^{4}_{17} 2^{3} 2^{0}_{16} 2^{6}_{17} $2^{0\frac{4}{17}}_{DIRT\ T.C.}$ 2^{5}_{27} 3^{4}_{30} 4^{0}_{50}

2^{7}_{30} 2^{6}_{20} 2^{1}_{17} 2^{3} 1^{8}_{16} 2^{8}_{19} 2^{2}_{27} 3^{1}_{30}

Direct Rod

Re-X-Sec Bond Cont

LT = W'ly   RT = E'ly

30³ RT = end 3' chain Link fence
0+50 — 19⁶ RT = W'ly edge 8" Tel Pole #464083
0+40 = 17³ RT = ℄ 10' Long Break in curb (Poor condition)
0+38 - 19⁵ LT = E'ly edge 24" Palm tree
0+24 - 19¹ LT = ℄ 4" Conc Walk
0+11 - 20° LT = ℄ Water Meter
0+03 - 30± RT = begin 3' chain Link fence

= N'ly Line Hornblend
3+40°° back = 0+00 ahead

18² LT = Curb B.C. 10' Radius
3+38 - 17³ RT = Curb B.C. 10' Radius

29⁵ RT = end Curb NELy Return
3+28 - 29⁵ LT = end Curb NWly Return } 10' Rad

Horn Blend for cuts
3+10°° = ℄ Horn Blend LT - See Sections ok.

29⁵ RT = end Curb Ret. SELy cor
2+92 - 31¹ LT = end Curb Return SWly cor

19° LT = Curb B.C. 10' Radius
2+82°° - 17° RT = Curb B.C. 10' Radius

On 7' Man - SWly cor Bond & Hornblend - 2.31

T.B.M.

5² 4³ 3⁵ 3³¹ 3¹ 3⁸ 2⁹ 3³⁶ 3⁶ 5°
45 30 25 18⁵ T.C. 18⁵ DIRT 9UT 17³ DIRT 9UT 17³ T.C. 27 30

5¹¹ 3²⁵ 3²⁵ 3¹⁶
32⁹ Top Steps 3 Risers 31 30 Conc Walk 19⁴ Conc Walk

4⁶ 3⁹ 2⁹⁶ 3° 3⁴ 2⁶ 2⁹¹ 4² 4³
40 30 18⁷ T.C. 18⁷ DIRT 17³ DIRT 9UT 17³ T.C. 30 40

2⁹⁵ 3° 2⁷ 2⁸⁹
18⁷ T.C. 18⁷ DIRT 17³ DIRT 9UT 17³ T.C.

3° 2⁷³ 3° 2⁹ 3⁷ 2⁶ 2⁹ 2⁸° 2⁹
30 29⁵ T.C. 29⁵ DIRT 19 17 29⁵ DIRT 29⁵ T.C. 30

3³ 2⁸ 2⁹ 3° 2⁷ 2⁷ 3²
50 30 19 17 30 50

2⁵⁴ 3² 2⁷ 2⁹ 2⁴ 3² 3² 2⁵⁹ 3²
31¹ T.C. 31¹ DIRT 16 16 20 29⁵ DIRT 29⁵ T.C. END 30

2⁵³ 3°
19° T.C. B.C. 19° DIRT

3² 2⁵⁷
17° DIRT 17° T.C. B.C.

Direct Rod

Re-X-Sec Bond ST. cont

T.C. = Top C6

1+94 - 30^{5} RT = ℄ 9' Conc drive

1+87 - 18^{6} LT = Ely of 18" Palm Tree

1+82 - 30^{6} RT = ℄ 3' Conc. walk

1+75

1+72 - 19^{0} RT = ℄ water meter

1+50

TBM. 7" Anion SW Wycoff Magnolia & Bond 4.02

1+25

1+00

0+89 - 19^{5} LT = ℄ water meter

0+86 - 19^{5} LT = Ely of 18" palm tree

31^{0} LT = ℄ 4^{0} walk + steps

0+75 - 30^{0} RT = ℄ 3^{5} Conc steps + walk

18^{5} LT = ℄ 10' of Broken curb

0+67 - 17^{3} RT = ℄ 10' of Broken curb

0+63 - 18^{8} RT = ℄ water meter

0+59 - 20^{0} LT = ℄ water Meter

LT = in ℄ | ℄ | RT = ℄

5^{55} 6^{22}
30^{5} Drive 40^{5} Drive

5^{50} 6^{18}
30^{6} Walk 40^{6} Walk

6^{0} 4^{7} 4^{33} 3^{8} 4^{2} 3^{7} 4^{29} 4^{6}
30 28 18^{0} T.C. 18^{0} dirt out 17^{2} dirt out 17^{2} T.C. 30

6^{5} 7^{0} 4^{5} 4^{06} 3^{6} 4^{1} 3^{5} 4^{10} 4^{3} 5^{4} 5^{6}
50 30 25 18^{1} T.C. 18^{1} dirt out 17^{2} dirt out 17^{2} T.C. 30 32 50

4^{8} 3^{81} 3^{4} 4^{0} 3^{3} 3^{88} 4^{9}
30 18^{3} T.C. 18^{3} dirt out 17^{2} dirt out 17^{2} T.C. 30

6^{0} 5^{5} 4^{3} 3^{71} 3^{3} 3^{9} 3^{2} 2^{77} 3^{9} 5^{3} 5^{4}
40 30 26 18^{3} T.C. 18^{3} dirt out 17^{2} dirt out 17^{2} T.C. 28 30 40

5^{68} 5^{64} 4^{16} 3^{9} 3^{49} 3^{2} 3^{9} 3^{0} 2^{54} 3^{80} 5^{40}
44^{2} Walk 34^{2} Top Riser + Walk 31^{0} Bottom Riser 30 18^{0} T.C. 18^{05} dirt out 17^{3} dirt out 17^{3} T.C. 30 Bottom Riser 35^{2} Top Riser + Walk

Direct Rod.

Re - X-sec & Bond. Conf

3+05 - 19.5 LT = ℄ 10 Water Meters

3+07.99 - 17.6 RT = Curb BC - 10 Rad.

3+00 - 31° LT = ely of 12" Powerpole # 2698
29.8 RT = Wly of 12" Powerpole # JP2742

2+97.99 - 30° RT = Ely end of NEly Return
= ℄ Sewer Manhole

2+79.99 = ℄ Magnolia ST } See X-sec Magnolia

2+61.99 = 30° RT = ely end curb
30° LT = Wly end curb
Curb Line (Sly) Magnolia ST

2+54 - 19.8 LT = ℄ 7 Water Meters

2+51.99 17.2 LT = curb B.C. 10' Radius
17.2 RT = Cb B.C. 10' Radius

27.8 LT = end Loose Block wall - No value
19° = ℄ 4 Water Meters

2+49.99 = Sly Line Magnolia ST

2+43 - 19.1 RT = Wly of Fire Hydrant

2+25 - 19.3 LT = ℄ Water Meter

2+17.29 ° LT = ℄ 3' Conc Steps - 3' Wide
Wall - No Motor + No footing.
28° LT = begin Loose granite block

2+00 - 18.4 RT = Wly of 10" Telpole # 464084H

LT = Wly & RT = Ely

4.6 17.6 DIRT OUT BC — 5.12 17.6 T.C. BC

4.8 30 — 4.3 19 — 4.8 17 — 4.5 30° DIRT OUT — 4.9 30° T.C. — 5.28

4.7 30 — 4.7 18 ℄ on SWM — 4.7 — 4.33 — 4.6 17 — 4.7 30

4.99 30° T.C. — 4.95 28 CB BC — 4.61 28 CB BC — 4.70 30° T.C.

4.83 17.7 T.C. B.C. — 4.3 17.7 DIRT OUT — 4.2 17.7 DIRT OUT T.C. B.C. — 4.57

5.5 5.6 6.1 5.0 4.78 4.2 — 4.6 4.2 4.60 5.8 6.2
58 30 29 27.8 17.7 T.C. 17.7 OUT DIRT — 17.7 OUT 17.7 T.C. 30 50

6° 30 — 6° 28 — 5° 27.5 — 4.58 18° T.C. 4° 18° OUT — 4.5 17.1 DIRT OUT 4° 17.1 T.C. — 4.52 — 5.8 30

6.09 40.2 Walk — 5.99 30.2 Top Riser & Walk — 5.02 29° Bottom Riser

6.3 6.0 58 30 — 4.9 28 — 4.49 18° T.C. 3.9 18° OUT — 4.3 4.0 4.41 17.2 OUT 17.2 T.C. 5.6 30 — 6.2 50

Direct Rec.

Re-x-sec Bond ST

LT = W'ly ℄ RT = E'ly.

1+25

$6\frac{8}{30}$ 6^{0} $5\frac{1}{18}$ $5\frac{9}{16}$ $5\frac{3}{17\frac{2}{\text{DIRT OUT}}}$ $5\frac{84}{17\frac{2}{\text{T.C.}}}$ $6\frac{4}{30}$

1+00

$6\frac{9}{50}$ $6\frac{7}{30}$ $5\frac{6}{18}$ 5^{0} $5\frac{5}{17}$ $5\frac{1}{17\frac{2}{\text{OUT}}}$ $5\frac{79}{17\frac{2}{\text{T.C.}}}$ $6\frac{3}{30}$ $7\frac{1}{50}$

0+99-19$\frac{2}{}$ RT = W'ly of 10" tel Pole # 464085H

0+78

$6\frac{4}{30}$ $5\frac{7}{18}$ $4\frac{9}{17}$ $5\frac{5}{17\frac{2}{\text{OUT DIRT}}}$ 5^{0} $5\frac{66}{17\frac{2}{\text{T.C.}}}$ $6\frac{4}{30}$

0+73-18$\frac{3}{}$ RT = ℄ 3' Conc Walk

$5\frac{68}{18\frac{3}{\text{WALK}}}$ $6\frac{34}{30^{0}\text{ WALK}}$

0+71-19$\frac{1}{}$ RT = ℄ Water Meter

0+50

$6\frac{5}{50}$ 6^{0} $5\frac{5}{18}$ $4\frac{8}{16}$ $5\frac{2}{17\frac{2}{\text{DIRT OUT}}}$ $4\frac{9}{17\frac{2}{\text{T.C.}}}$ $5\frac{51}{17\frac{2}{}}$ $6\frac{2}{30}$ $6\frac{8}{50}$

0+44-20° RT = ℄ 3$\frac{5}{}$ Conc Walk

$5\frac{98}{20^{0}\text{ WALK}}$ $6\frac{56}{30^{0}\text{ WALK}}$

0+25

6^{0} $5\frac{7}{21}$ $4\frac{6}{16}$ 5^{0} $4\frac{8}{17\frac{2}{\text{OUT DIRT}}}$ $5\frac{32}{17\frac{2}{\text{T.C.}}}$ $5\frac{8}{26}$ $6\frac{2}{28}$ $6\frac{7}{30}$

0+21-19$\frac{9}{}$ RT = ℄ 3' Conc Walk

$6\frac{34}{19\frac{9}{\text{WALK}}}$ $6\frac{70}{30^{0}\text{ WALK}}$

0+10-19$\frac{4}{}$ RT = ℄ Water Meter

0+01-19$\frac{2}{}$ RT = ℄ 2 Water Meters

No evidence of curb or W'ly

= N'ly Line Magnolia ST

3+09$\frac{99}{}$ Back = 0+00 ahead

$5\frac{8}{58}$ $5\frac{5}{30}$ $4\frac{9}{17}$ $4\frac{6}{16}$ $4\frac{9}{17\frac{6}{\text{OUT}}}$ $4\frac{6}{17\frac{6}{\text{T.C.}}}$ $5\frac{13}{26}$ $5\frac{5}{27}$ $6\frac{7}{30}$ $6\frac{8}{50}$

DIRECT Rod

Re-X-Sec Bond ave ST

0+50

0+41-18² RT= ℄ 8 conc drive

0+25
See sketch page 53
= NlyLine Figueroa ST
2+28 40 Back = 0+00 ahead

17² LT = Cb BC 10' Radius
2+26 40 18² RT = Curb BC. NEly Return

28° LT = Curb B.C.
30° LT = Wly end Curb
28° RT = Curb BC. NElyReturn - 10' Rad
2+16 40 - 30° RT = Ely end Curb -
on ℄ Non NWly Figueroa + Bond 6.50

TBM-

Figueroa is NOT 90° to Bond ST

1+88 41 - ℄ Figueroa ST

30° RT = Ely end curb
1+60 40 - Sly Curb Line Figueroa

1+57 - 21² RT = Wly of 10" pole #JP2741

10' Radius
1+50 40 - 18° RT = Curb B.C. SELy Ret

1+48 40 = Sly Line Figueroa ST

LT = Wly

7 8 / 50 | 7 4 / 30 | 7 38 / 17 5 T.C. | 6 7 / 17 5 90T

7 4 / 18 3 90T | 6 8 / 18 3 T.C. | 7 38 | 7 9 / 30 | 8 5 / 50

6 75 / 18 3 Lip Drive | 7 44 / 21 5 Brk | 7 86 / 30 Dr

7 4 / 30 | 7 00 / 17 2 T.C | 6 4 / 17 7 90T

7 0 / 18 3 90T | 6 4 | 6 98 / 18 3 T.C. | 7 6 / 30

7 3 / 50 | 7 0 / 30 | 6 4 / T.C. 17 2 | 6 3 / 17 2 90T

6 8 | 6 2 / 18 2 90T | 6 65 / 18 2 T.C. | 7 2 / 30 | 7 5 / 50

6 4 / 17 2 T.C. BC | 6 3 / 17 2 90T

6 2 / 18 2 90T DIRT | 6 65 / 18 2 T.C. BC

6 65 / 30 T.C. 30 DIRT 90T | 6 2 / 30 | 6 2 / 28 BC T.C. | 6 3 / 18

6 4 | 6 5 / 28 90T | 6 60 / 28 BC | 6 62 / 30 T.C. | 6 4 / 30 90T DIRT

6 0 / 30 | 6 0 / 18 | 6 3 | 6 3 / 18 | 6 2 / 30

6 3 / 30 | 5 4 / 16 | 6 0 | 5 6 | 5 7 / 18 | 6 06 / 30 30° end curb

5 4 / 18° 90T DIRT | 5 92 / 18° T.C. BC

6 6 / 30 | 5 8 / 19 | 5 3 / 16 Direct | 6 0 | 5 4 | 5 95 / 18° 90T | 6 8 / 18° T.C. | 30 Rid

X-sec Bond - Figueroa ST to Balboa Ave

1+10 - 29.8 LT = end Clay Brick wall

1+00

Opening thru Brick Wall for Drive

0+92 - 17.7 RT = ℄ Drive - see sketch

0+88 - 30.0 LT = ℄ 2.1 Conc Walk (opening in Brick wall)

0+75

0+74 . 19.1 LT. = ℄ Water Meter

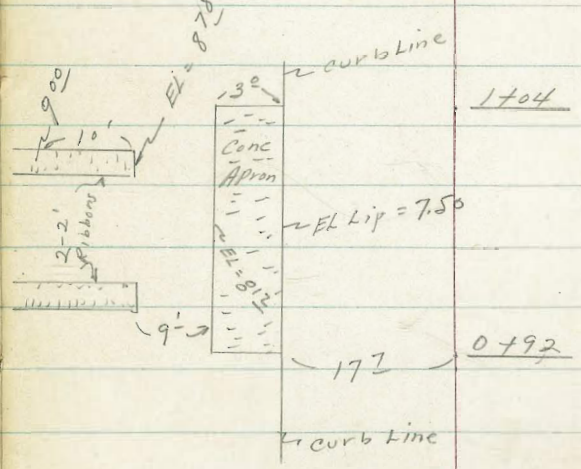
20.0 RT = Wly of 10" Power Tel. pole #464087H.

0+76 . 29.8 LT = begin Clay Brick wall

$\angle T = w/y$ ℄ $\angle ET = o/y$

1.39 7.9 8.4
29.8 29.8 29.8
Top Foot 9r

8.9 8.7 7.55 8.4 7.4 8.10 8.2 8.6
50 30 17.7 9r T Lip 18.3 9ut 18.3 T.C. 30 50



1+04

0+92

8.76 8.63
40.0 Walk 30.0 Walk

7.8 7.79 7.2 7.6 7.1 7.80 8.1
30 17.2 T.C. 17.2 9ut 18.3 9ut 18.3 T.C. 30

11.26 7.3 7.7
29.8 29.8 29.8
Top W. Foot 9r direct Rod

X-Sec Book Cont

Ely & Wly Curbs apparently extend to Skyline of Balboa - under 25± of Dirt

2+62 - 19.9 RT = Wly of Fire Hydrant
19.0 LT = Ely of 24" Palm tree

2+50 - 24.3 LT = ℄ 3' Conc Walk

2+54 - 29.7 LT = end 4' Chain Link fence

2+50

2+48 - 21.3 RT = ℄ Deadman

2+27 - 21.0 RT = Wly of 10" Tel pole #464088H

2+25

2+17 - 29.8 LT = begin 4' Chain Link

2+10 - 17.7 LT = end Broken curb

2+00

Broken OUT entirely
1+83 - 17.7 LT = begin Broken curb

No opening thru curb
1+75 - 26.3 LT = ℄ Ribbon Drive - 2 - 2' Ribbons

1+50

1+38 - 20.0 LT = ℄ 2 Watch Markers used for drive

1+28 - 18.0 LT = ℄ of 14" Broken curb

1+25

LT = Wly ℄ RT = Ely

10.7 3 / 34.3 Walk — 10.5 2 / 24.3 Walk

10.6 / 30 — 10.0 / 30 — 10.2 7 / 17.5 T.C. — 9.6 / 17.7 — 10.8 / 18.5 Dirt — 10.6 / 18.5 T.C. — 10.2 6 / 30 — 10.4 / 30 — 10.6 / 50

10.2 / 30 — 9.9 7 / 17.5 T.C. — 9.2 / 17.5 Gut — 10.0 / 18.5 Gut — 9.4 / 18.5 T.C. — 9.89 / 30 — 9.9

9.8 / 58 — 9.6 / 30 — 9.0 / 18 No curb — 9.5 / 18.4 Gut — 9.0 / 18.4 T.C. — 9.54 / 30 — 10.2 / 50 — 10.7

9.56 / 30.0 Dr — 9.44 / 26.3 Dr — 9.26 / 17.2 Top Co. — 8.5 / 17.2 Gut — 9.1 / 18.8 Gut — 8.6 / 18.3 T.C. — 9.20 / 30 — 9.4

9.0 / 50 — 9.0 / 30 — 8.8 7 / 17.2 T.C. — 8.2 / 17.2 Gut — 8.8 / 18.2 Gut — 8.1 / 18.3 T.C. — 8.86 / 30 — 9.0 / 50 — 9.8

8.7 / 30 — 8.0 / 18 No curb See Above — 8.4 / 18.3 Gut — 7.8 / 18.3 T.C. — 8.52 / 30 — 8.8

Direct R.d.

X-sec Bond St cont.

LT = W'ly & RT = E'ly.

Levels turned Back to Starting BM.

TBM. 10.99 ON Prop. Mon 5 W'ly cor Balboa + Bond.

2+82 = S'ly edge A.C. Paving Balboa Ave

$13\frac{20}{65}$ $13\frac{08}{30}$ A.C. $12\frac{94}{18}$ A.C. $12\frac{91}{}$ A.C. $12\frac{97}{18}$ A.C. $13\frac{08}{30}$ A.C. $13\frac{24}{50}$ A.C. $13\frac{26}{100}$

2+73. 25 ± LT = E'ly of 12" power pole # 2699

2+72.03 = S'ly of Balboa Ave to W'ly

$12\frac{5}{30}$ $12\frac{5}{30}$ $12\frac{4}{18}$ $12\frac{2}{}$ $12\frac{6}{20}$ $13\frac{4}{30}$

2+70.42 = S'ly of Balboa Ave to E'ly

$11\frac{7}{30}$ $12\frac{0}{18}$ 12^{0} $12\frac{4}{18}$ $13\frac{0}{20}$ $13\frac{4}{30}$ $13\frac{7}{50}$

2+64 - 20 ± RT = W'ly of 24" Palm tree

Direct Rod

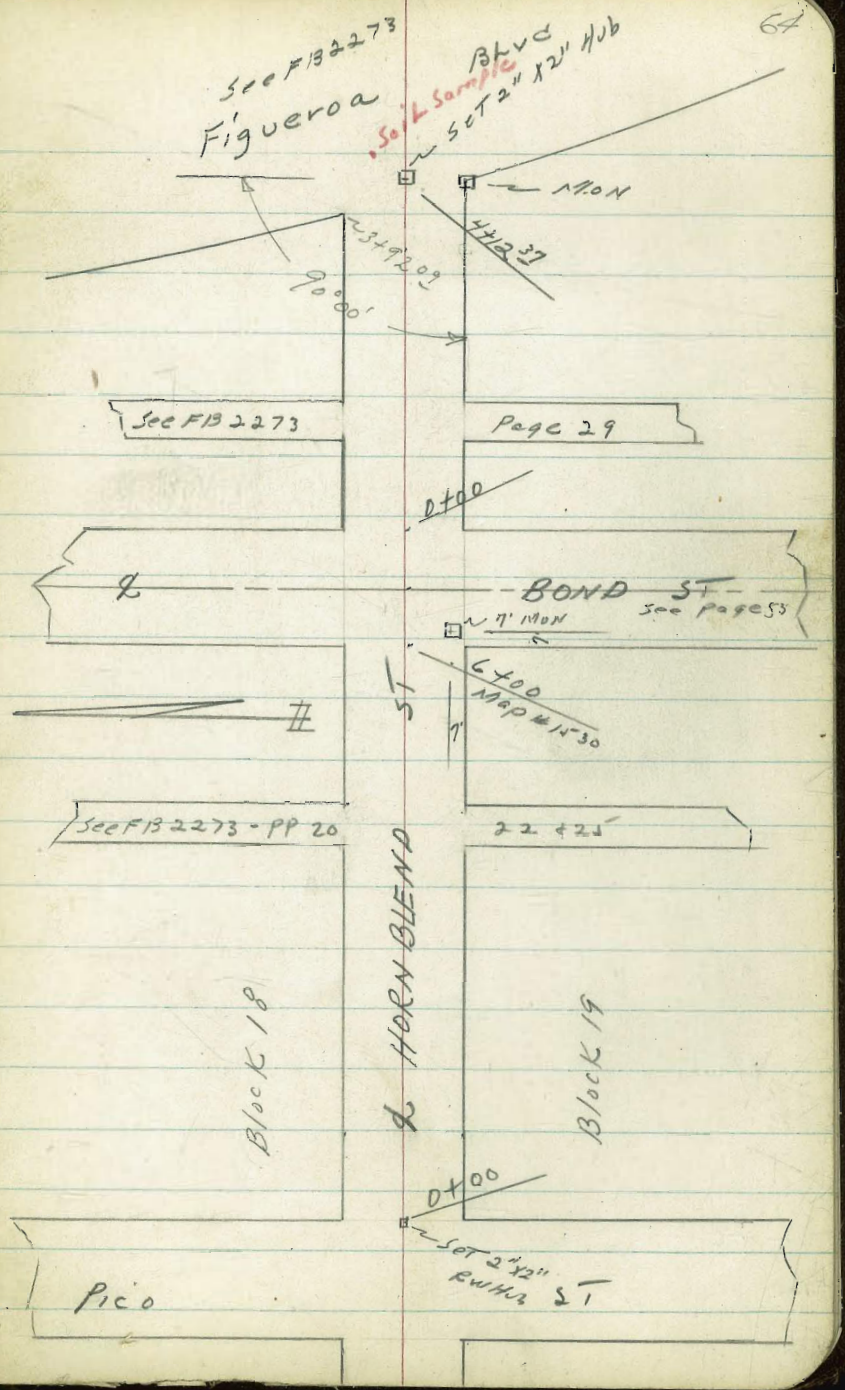
INDEXED
JUL 11 1955

X-Sec Horn blend ST - Pico to Figueroa Blvd - 7/7/55 -

See FB 2273 - Map # 15-30 -

X-Sec Bond ST Page 53 -

W/O # 32583 - C. Allen, D. Sisson, C. Powell R. Parks



X-Sec Hornblend ST
See Sketch Page 64
Water Meters are in street

LT= N½ RT= S½

2+50

5 1/50 5 1/30 4 7/18 4 7/10 4 6/12 5 0/30 4 7/50 4 3/50

2+44 - 31° LT = ℄ 7' conc drive

5 21/41° or 5 15/31° or

2+00 - LT = end Small Wood fence easy to Move

5 6/50 5 4/30 5 2/20 4 8/10 4 7/12 5 4/30 5 0/50 4 4/50

1+66 - 20° LT = begin Small Wood fence

1+50

5 6/50 5 5/30 5 0/18 4 6/18 4 8/30 4 7/50 4 2/50

1+40 - 30° LT = ℄ 8.0' conc drive

5 6.6/40° or 5 8.1/30° or

1+00

5 9/50 5 7/30 4 5/30 4 5/50 4 4/50

0+98 - 32° LT = ℄ 6" Euc Tree (young)

0+50

5 4/50 5 0/30 4 2/30 4 2/50 4 3/50

0+00 - = Ely Top Bank Rose creek

5 2/30° Top of Bank 5 3/Top of Bank 5 9/30° Top of Bank

0+00 = Ely P.L. Pico ST - on Bank of creek

2 8/50 on Bank of creek 1 9/30 on Bank of creek 4 0/on Hub 4 0/30° on Bank of creek 3 1/50 on Bank of creek

0 - 06 = Ely Bottom of Rose creek

- 0 4/30° in Bottom 0 0/Bottom of creek 0 1/30° in Bottom

TBM on 2"x2" Hub 0+00 4.01

Direct elev Rod - All elevs are true

BM. 2.31

1' NON SWly cor Hornblend Bond - P 56

X-Sec Hornblend Court

LT=N'ly & RT=S'ly-

= ℄ Sewer Manhole

4+60 = ℄ N-S Alley - See FB 2273 - 20-22-25

4+48 - 20° RT = ℄ 10" Power Pole # P2674

4+30 - 20$\frac{5}{}$ LT = ℄ anchor pole (8") # 464079H

4+10 - 20° LT = ℄ deadman

4+07 - 30° RT = ℄ 9$\frac{5}{}$ conc driveway

4+05 - 20° LT = ℄ deadman

4+00

3+50

Foundation

3+49 - 30° LT = end fence with conc

3+38 - 30° LT = ℄ 10' conc drive

Changes from Brick to conc

30$\frac{2}{}$ LT = ℄ 3' Conc Walk

3+20 - 14$\frac{4}{}$ LT = ℄ 3' Brick Walk

Fence has 6" conc Foundation

30$\frac{3}{}$ LT - begin 4' Wood Fence

3+00 - Floral Plantings on Left

2+57 - 30$\frac{8}{}$ LT = ℄ 7$\frac{5}{}$' conc drive

5$\frac{0}{}$	4$\frac{6}{}$	3$\frac{9}{}$	4$\frac{2}{}$		3$\frac{4}{}$	3$\frac{7}{}$	3$\frac{9}{}$
50	30	15	R. Mtg S. MH.		12	30	50
4$\frac{8}{}$	5$\frac{0}{}$	5$\frac{-3}{}$	3$\frac{8}{}$	4$\frac{e}{}$	3$\frac{8}{}$	4$\frac{4}{}$	4$\frac{4}{}$
50	30	22	14		12	30	40
				4$\frac{34}{}$	4$\frac{38}{}$		
				30° Dr	40° Dr		
4$\frac{8}{}$	5$\frac{0}{}$	4$\frac{3}{}$	4$\frac{0}{}$	4$\frac{3}{}$	4$\frac{4}{}$	4$\frac{5}{}$	4$\frac{5}{}$	4$\frac{5}{}$
50	30	16	14		10	12	30	50
5$\frac{2}{}$	5$\frac{-2}{}$	4$\frac{7}{}$	4$\frac{5}{}$	4$\frac{3}{}$	4$\frac{5}{}$	5$\frac{1}{}$	4$\frac{7}{}$	
50	30	12		10	12	30	50	
5$\frac{30}{}$	5$\frac{0}{}$	5$\frac{-2}{}$						
30° Top Foun.	30° Foot	30° gl						
	5$\frac{37}{}$	5$\frac{32}{}$						
	40° Dr.	30° Dr						
5$\frac{30}{}$	5$\frac{30}{}$	4$\frac{6}{}$						
40$\frac{2}{}$ Walk Conc	30$\frac{2}{}$ Conc Walk	14$\frac{4}{}$ Brick Walk						
5$\frac{1}{}$	5$\frac{41}{}$	5$\frac{0}{}$	5$\frac{-2}{}$	4$\frac{0}{}$	4$\frac{6}{}$	4$\frac{5}{}$	4$\frac{9}{}$	5$\frac{-2}{}$	4$\frac{4}{}$
50	30$\frac{3}{}$ Top Found	30$\frac{3}{}$ Foot	30	16		10	12	30	50
	5$\frac{16}{}$	5$\frac{11}{}$							
	40$\frac{8}{}$ Dr.	30$\frac{8}{}$ Dr							

Direct Rod - True elev.

	Lt = Nly	℄	Rt = Sly.
6+30 = ℄ Bond ST	3^{4}_{30}	2^{9}	3^{0}_{30}
See X-Sec Bond ST - Page 56			
6+00 = Wly Line Bond ST	18^{3} Lt = Wly end Curb NWly Ret 17^{6} Rt = Wly end Curb SWly Ret.		
	4^{0}_{50} 3^{8}_{30} $2^{6}_{18^{3}\ T.C.}$ $2^{6}_{18^{3}\ gr}$	2^{8}	$2^{6}_{17^{6}\ Dirt}$ $2^{5}_{17^{6}\ Top\ CB}$ 3^{3}_{30} 3^{4}_{50}
5+95 - 25° Rt = ℄ 14" Power pole # P2698			
5+76 - 24^{4} Rt = ℄ dead "Tree"			
5+55 - 26^{6} Lt = Sly end of N+S Lateral Conc Block wall	$6^{7}_{26^{6}\ Top\ Wall}$ $4^{3}_{26^{6}\ Foot}$ $4^{5}_{26^{6}\ gr}$		
5+50 - 21 Lt = ℄ 8" Tele pole # JP2687	5^{3}_{40} 4^{8}_{30} 3^{3}_{17}	3^{7}	3^{0}_{14} 4^{4}_{30} 4^{7}_{40}
5+48 - 30° Rt = ℄ 9' Conc driveway			$4^{5^{0}}_{30°\ Dr.}$ $4^{7^{6}}_{40°\ Dr.}$
5+08 - 29^{8} Lt = ℄ 4" yellow acacia Tree			
5+00	5^{3}_{40} 5^{0}_{30} 4^{7}_{22} 3^{7}_{18}	3^{5}	3^{3}_{12} 3^{6}_{14} 4^{7}_{30} 4^{7}_{50}
4+88 - 30° Lt = ℄ 4' Conc walk	$5^{4^{1}}_{40°\ Wlk}$ $5^{3^{6}}_{30°\ Wlk}$		
4+79 - 30° Rt = ℄ 10^{5} Conc driveway			$4^{5^{9}}_{30°\ Dr}$ $4^{9^{2}}_{40°\ Dr}$

Direct elex Rod

X-Sec HORNBlend Cont

LT = Nly ℄ RT = Sly

= ℄ Sewer Manhole

1+40 $^{05}_{--}$ = ℄ N+S alley See FB 2273-29

1+30-22$^{6}_{--}$ RT = ℄ 12" Power Pole # P2727

1+14-23$^{0}_{--}$ RT = ℄ dead man

1+15- 28$^{0}_{--}$ LT = ℄ 4' conc walk

1+00

0+72-28$^{0}_{--}$ LT = ℄ 4' Conc walk

0+50

0+44-20$^{0}_{--}$ LT = ℄ 2 deadmen-

0+33-28$^{0}_{--}$ LT = ℄ 4 Conc walk

0+19-20$^{1}_{--}$ LT = ℄ 8" anchor Pole # 464481H-

0+04-24$^{3}_{--}$ RT = ℄ 10" Tele Pole # 604687H

Could be Fire Hyd-

0+03-19$^{5}_{--}$ RT = ℄ 2" Water Stand Pipe

18$^{2}_{--}$ LT = ely end curb NEly Ret- 10' Rad

17$^{6}_{--}$ RT = ely end curb SEly Ret- 10' Rad

Bond St

6+60$^{0.0}_{--}$ Back = 0+00 ahead = Ely Line

5^{5}_{50} 4^{8}_{30} 3^{8}_{21} $3^{94}_{R\ MH}$ 3^{8}_{9} 4^{2}_{12} 4^{3}_{30} 3^{9}_{50}

$5^{53}_{35^{0}\ W/K\ at\ Porch}$ $5^{42}_{30^{0}\ W/K}$ $5^{35}_{28^{0}\ W/K}$

5^{2}_{30} 4^{5}_{22} 3^{8}_{18} 3^{8}_{10} 3^{9}_{15} 4^{7}_{30} 4^{5}_{50} 4^{6}

$5^{24}_{35^{0}\ W/K\ at\ Porch}$ $5^{14}_{30^{0}\ W/K}$ $5^{08}_{28^{0}\ W/K}$

5^{0}_{40} 4^{7}_{30} 4^{4}_{21} 3^{2}_{17} 3^{3}_{9} 3^{4}_{13} 4^{2}_{30} 4^{1}_{50} 4^{6}

$4^{92}_{35^{0}\ W/K\ at\ Porch}$ $4^{90}_{30^{0}\ W/K}$ $4^{88}_{28^{0}\ W/K}$

4^{1}_{30} $2^{81}_{18^{2}\ T.C.}$ $2^{9}_{18^{2}\ gr}$ 2^{7} $3^{2}_{17^{6}\ gr}$ $2^{58}_{17^{6}\ T.C.}$ 3^{4}_{30}

Direct elev Rod-

3+50 - 20^{6} RT = ℄ 10" Power pole # P2747

3+40 - 29^{8} RT = ℄ 9° Conc driveway

3+20 - 26^{2} LT = ℄ 4' Conc 5 Risers steps + walk

3+00 - 30^{1} RT = end Conc Block Wall

2+95 - 14^{2} RT = ℄ Small Palm tree

2+66 - 20^{7} LT = ℄ 8" Acacia Tree

2+50

2+24 - 20° RT = ℄ 4' Conc walk

2+06 - 31^{2} LT = ℄ 9' Conc driveway

2+00 - 30^{3} RT = begin Conc Block wall

1+90 - 31° LT = ℄ 10' Conc driveway

1+70

9^{5} 8^{8} 6^{3} 6^{1} 5^{5} 5^{6} 5^{5} 5^{8} 5^{5}
50 30 26 18 16 8 30 50

6^{15} 6^{16} 6^{40}
29^{8} Dr 30^{0} Dr 40^{2} Dr

9^{40} 9^{27} 6^{80}
40° On Walk 30° To Riser 26° Bottom Riser

9^{3} 9^{0} 7^{8} 6^{4} 5^{5} 4^{9} 5^{3} 2^{4} 5^{9} 5^{9} 5^{3} 8^{29} 5^{7}
50 33 30 26 18 15 12 30 30L 9r 30L Foot 30L T.W. 50

6^{8} 6^{1} 6^{0} 4^{6} 5^{0} 5^{0} 5^{2} 5^{4}
50 30 27 15 14 30 50

5^{44} 5^{44} 5^{41}
20° Walk 30° Walk 40° Walk

6^{24} 6^{01}
41^{2} Dr 31^{2} Dr

5^{9} 5^{5} 4^{3} 4^{3} 4^{5} 5^{1} 5^{1} 4^{8} 8^{02} 5^{3}
50 30 16 11 30 30^{3} 9r 30^{3} Foot 30^{2} Top Wall 50

6^{10} 5^{97}
41^{1} Dr 31^{0} Dr

6^{1} 5^{7} 3^{9} 4^{0} 4^{1} 4^{6} 4^{7} 5^{0}
50 30 17 7 14 30 50

Direct elevs.

Levels checked back to starting BM.

For X-sec Figueroa see FB 2273: 42 + 43

4+12.37 - 90°00' to Swly COR Figueroa + Hornblend

3+92.09 - 90°00' to NWly COR Figueroa + Hornblend

3+65 - 30 RT = ℄ 10' Conc driveway

3+60 - 26.3 LT = ℄ 4' Conc steps + walk

6.7 / 50 6.2 / 30 5.8 5.9 / 30 6.1 / 50

8.6 / 50 8.0 / 30 6.7 / 27 5.9 / 22 5.8 / 13 5.7 / 30 6.0 / 40 6.0

6.00 / 30 L DV 6.14 / 40 L DV

9.62 / 40e WIK 9.22 / 30e Top Riser 6.73 / 26.3 Bot. Riser Direct. elev Rod

Storm drain Survey - WO# 32583 - 7/8/55

Grand Ave under construction - Ground elevations around 0+00 will be changed.

0+00 is approx. ely end of Drain to be Constructed

End Bridge - 23+14.2 Grand Ave Plan #2318-D

0+00 = 23465± on Grand Ave - Approx. Ely end of Rose Canyon Drain to be Constructed per Dwg 2318-D

℄ & Prelim storm Drain survey

5'

Alley Block 19 See F13 2273+20

Rose Channel Bridge

GRAND AVE - Under Construction 7/8/55

71

8+54.97

℄ HORNBLEND ST.

Set Hub

Mon

& Prelim storm drain survey

7'

17'

℄ BOND ST

See X-sec Page 53

90°02'30"

Fd Hub

5+39.27

Set Hub

Levels Prelim Storm Drain in Grand Ave & Bond ST - See Sketch page 71

		LT = N'ly		RT = S'ly
1+61 - 20± LT = SE'ly Cor Stucco Dwelling				
1+50		5.5 / 20.5 9" AT House	5.2 / 6	4.0	3.8 / 12 Toe Fill	6.2 / 16 Top Fill
1+30 - 20.5 LT = S'ly Cor Stucco dwelling		5.9.5 / 20.5 Floor		
1+25				3.0
1+00		3.4 / 25		2.8	2.9 / 8.0 Toe Fill	5.8 / 13 Top Fill -
0+75				3.3
0+50		3.5 / 25		2.7	2.2 / 6 Toe Fill	3.9 / 8 Top Fill -
0+25 - 5.0 RT - begin Present Fill - Grand Ave	Will be changed	3.3 / 25		1.7	1.6 / 5 Toe Fill	2.2 / 10
0+00 = approx Station 2376.5 Grand Ave		2.7 / 10		2.7	2.7 / 10
TBM -	2.34	On 2"x2" hub 0+00			
0 - 21.5 = Fly end of Rose channel Bridge					
BM -	2.48	2"x2" Hub N'wly Cor Grand Ave & Bond - Direct elev Rod			

Page 2 -

Levels Drain Grand Ave

	LT = N'ly ℄	RT = S'ly
3+98 - 5.2 LT = ℄ 8' Conc Drive	3.1	
	5.2 Dr	
3+83 - 15° RT = ℄ Sewer Manhole approx ℄ Line To N'ly Alley		-2.25 15° IE of Pipe from N'ly
3+75 - 4° LT = ℄ deadman.	3.2	
3+50	3.2 2.5	3.0 2.7 20 Toe Fill 4.8 23 Top Fill
3+25	2.9	
3+00	3.4 2.5	2.9 3.0 18 Toe Fill 5.4 21 Top Fill
2+75	3.1	
2+50	3.1 25	3.0 3.1 16 Toe Fill 5.6 20 Top Fill
2+25	3.2	
2+00	3.6 25	3.4 3.6 14 Toe Fill 6.2 18 Top Fill
1+75	3.4	

Direct elev Rod - True elevs

Drain cont -

	LT	℄	RT
5+50		2 4	
See page 54 for detail for X-sec of Bond (Trees improvements & sidewalk)			
5+39 97 = L Point - 90°02'30" inside (Taken 90° to Back Tangent)		2 6	3 0 · 5 4 2 5 · 31 Toe Fill · Top Slope.
5+22 97 = W/y Line Bond ST extended	3 3 · 3 1 50 · 25	2 7	
5+00	3 3 · 3 1 50 · 25	2 7	2 7 · 5 0 24 · 28 Toe Fill · Top Fill
4+75	3 6 · 3 3 50 · 25 INLET #14	2 5	
4+50	3 6 · 3 4 50 · 25 INLET #14	2 6	2 8 · 5 4 22 · 27 Toe Fill · Top Fill
4+25		2 8	
20' LT = ℄ Frame House 4+18 - 5 2 LT = ℄ 3' conc walk	4 0 2 · 3 5 4 20' · 5 2 Floor · walk		
4+00		2 9	2 8 · 5 1 20 · 24 Toe Fill · Top Fill

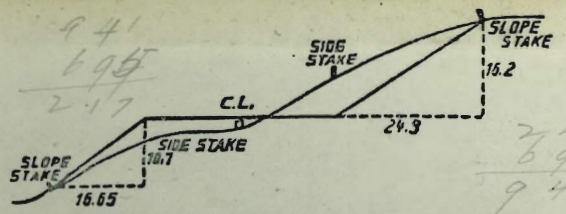
Direct elev Rod

Levels Drain cont LT = Hilly 2 RT = Cl 75

8+54 97 = ℄ Horn Blend ST		2 9
8+00		2 8
7+50		2 6
7+00		2 4
6+50		2 3
6+00		2 2

Direct elev Rod

21 + 51 23 22°-25' Dft. = Bond"



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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