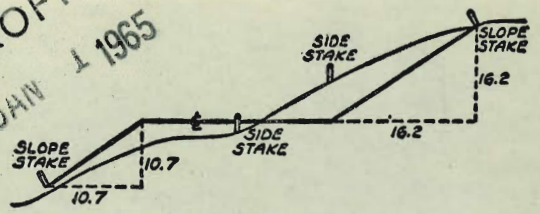
2190



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34 20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35 10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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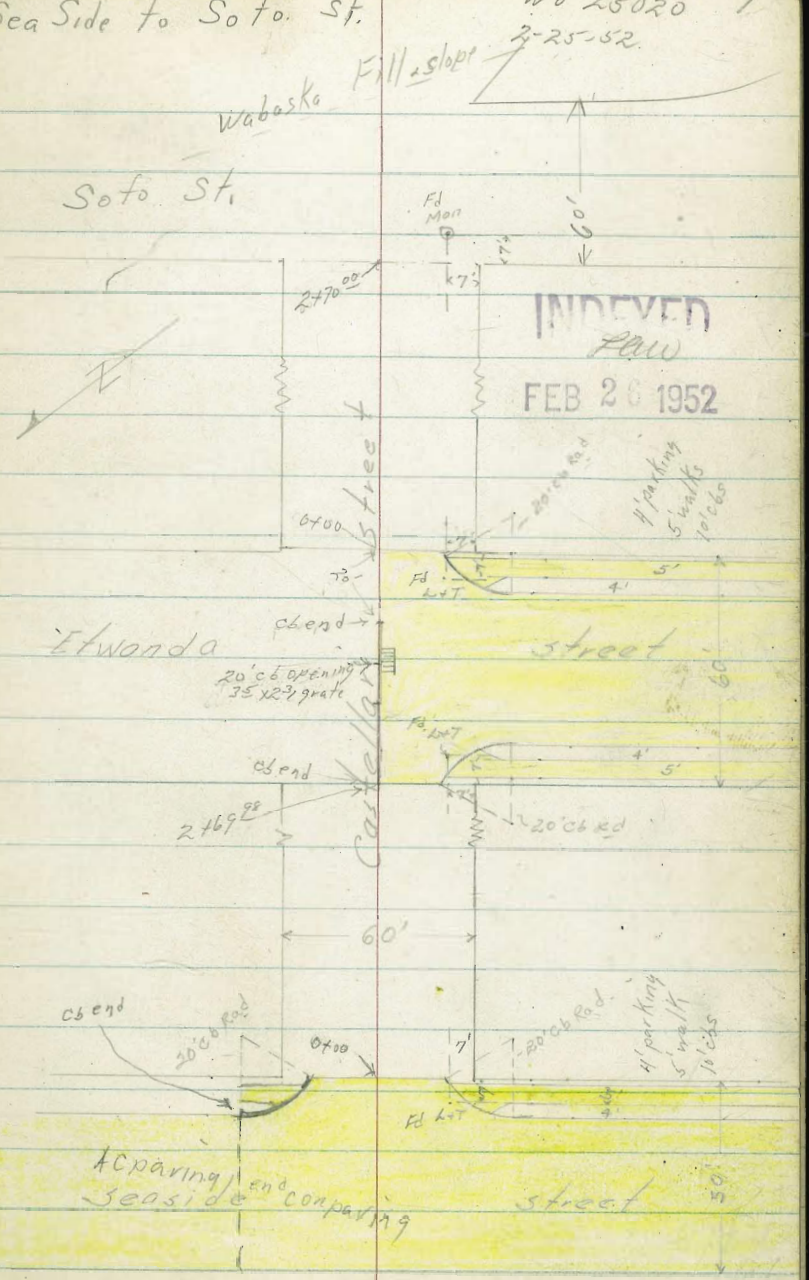
D. Smith
C. Allen
R. Taylor

Cross Sec Castellar St

W = concrete

Sea Side to Soto. St.

Wo # 25020 1
2-25-52.



Lt = North ℄ Rt = South

0+50
44.7 3^{6} 40 · 45.1 3^{2} 30 · 44.7 3^{6} 10 · 43.8 4^{5} 8 · 44.0 4^{3} · 45.1 3^{2} 30 · 45.2 3^{1} 40

0+25 27^{4} Rt ℄ 14" Pepper Tree

0+03 5^{3} Lt ℄ 5^{0} x 4^{0} gas & elec valve box
43.24 5^{19} 5^{3} rim

0+00 East Sea Side end con paving & cbs
42.3 6^{0} 80 · 42.90 5^{43} 30 walk · 42.91 5^{42} 22^{9} cb end · 42.44 5^{89} 22^{9} gut · 43.19 5^{14} · 43.20 5^{13} 22^{6} gut · 43.65 4^{68} 22^{6} cb · 43.70 4^{63} 30 walk

43.00 5^{53} cb · 42.31 6^{02} gut · 43.19 5^{14} gut · 43.60 4^{73} cb

Mid point Ret as exists 10^{5} on curve

0-10 East Cb Line Sea Side
41.3 7^{0} 80 dirt · 40.88 7^{45} 80 par · 42.64 5^{69} 40 cb end · 42.21 6^{12} 40 gut · 42.41 5^{92} 30 · 42.70 5^{63} 20 · 43.11 5^{22} · 43.31 5^{02} 20 · 43.20 5^{13} 30 · 43.17 5^{16} 40 gut · 43.65 4^{68} 40 cb · 42.88 5^{45} 80 gut · 43.34 4^{99} 80 cb

0-25' ℄ Sea Side
41.18 7^{15} 80 · 42.77 5^{56} 40 · 42.78 5^{55} 30 · 43.04 5^{29} · 43.25 5^{08} 30 · 43.10 5^{23} 80

TP,	5^{30}	48^{33}	2^{40}	43^{03}	
BM	11^{75}	45^{43}		33^{68}	SWBP Castellar & Etiwanda

Reduced 3-14-52
RMW

π 48^{33}

1+50

1+25

1+16 31.8 Rt & 2.5 con walk

1+01 30.9 Rt & single garage con floor apron

1+00

0+93 31.2 Rt & 2' con walk.

0+84 31.2 Rt & double garage con floor

Lt = North

37.9	39.1	40.8	41.2	41.1	41.2
10.4	9.3	7.5	6.4	7.3	7.1
40	30	17	6	2	

Rt = South

42.3	43.6	44.0
6.0	4.1	4.3
18	30	40

40.1	41.5	42.7	43.3	42.6	42.8
8.2	6.8	5.6	5.0	5.2	5.5
40	30	21	6	3	

43.7	44.6	44.7
4.6	3.2	3.6
20	30	40

45.07 3.26 31.8 walk

45.17 3.16 42

45.41 2.92 30.2 apron

45.47 2.86 32.3 floor

42.5	43.0	44.2	44.6	43.8	43.9
5.8	5.3	4.1	3.2	4.5	4.4
40	30	23	6	4	

44.4	45.2	45.4
3.9	3.1	2.9
15	30	40

45.43 2.84 31 walk

45.93 2.38 31.1 floor

4/8.33

2+80 Wly C6 Line

Midpt of existing ret on Rt 10.5 length on C.
25' Lt & dead man
2+78.13 Lt & 8" gay pole # 519093 H

31° Rt end 8" con block Retaining wal
2+69.98 Wly Etiwanda edge con paving + C6s

2+50

2+42 31° Rt Begin 8" Con 2block retaining wall

2+25

2+00

TP2 1.03 39.32 10.04 38.29

Lt = South

13.0	14.2	18.3	26.3	32.9	32.53
26.3	25.1	21.0	13.0	6.4	6.77
50	37 Toe	30	16	5	C6

Rt = South

31.88	32.29	32.62	32.91	33.63	34.83	35.44
7.44	7.03	6.26	6.35	5.09	4.49	3.88
Sat	20	30	40 Sat	40 C6	80 Sat	80 C6

32.56	33.13
6.76	6.19
Sat	C6

12.8	13.8	17.6	33.7	32.57	32.15	32.52	33.15	33.45
26.5	25.5	21.7	5.6	6.75	7.17	6.80	6.19	5.87
50	38 Toe	30	7	C6	Sat	22.6 Sat	22.6 C6	30 Walk

13.0	23.0	34.0	34.7	34.1	33.9	35.8	35.8
26.3	16.3	5.3	4.6	5.3	5.4	3.5	3.5
46 Toe	30	13	3		16	23	30

36.4	35.1	38.42
2.9	4.2	0.9
31 Sd	3' Footing	Toe

24.3	31.5	35.3	36.2	35.7	36.4	37.2	39.0	39.9	38.1
15.0	7.8	4.9	3.1	3.6	2.9	2.1	6.3	10.6	0.6
40	30	22	1		14	24	26	30	40

32.3	36.0	36.5	37.7	38.7	37.4	37.4	38.7	40.52	40.82
7.0	3.3	2.8	1.6	0.6	1.9	1.9	0.6	+1.2	+1.5
40	34	30	16	3	1		15	30	40

T 39.32

TP3 2.50 35.36 6.46 32.86

0+70 30.3 Rt ℄ 23' con drive

0+50

0+00 Ely Etiwanda edge con paving + cbs

Mid pt existing return 10.5 Length of arc

3+20 Ely Cb Etiwanda

3+10 end ℄ on ℄

3+00 ℄ Etiwanda 24" corrigated pipe outlet Filled over

Lt = North ℄ Rt = South

32.85 34.24
6.47 5.08
30.2 · 40.2
drive

26.4 30.6 31.3 31.9 32.8 33.8
12.9 8.2 8.0 7.4 6.5 5.5
40 30 23 30 40

13.62 19.9 26.3 31.2 32.3 31.84 32.47 32.62 33.13 33.34
25.7 19.4 13.0 8.1 7.0 7.48 6.85 6.70 6.19 5.98
44 30 18 12 1 15 22.2 22.2 30
Toe Sut cb walk

13.0 13.8 16.6 26.3 31.6 32.5 31.69 32.52 32.7 33.04 33.59 34.74 35.38
26.3 25.6 22.7 13.0 7.2 6.8 7.63 6.80 6.62 6.28 5.73 4.58 3.24
50 37 30 14 5 1 20 30 40 40 80 80
Toe Sut cb Sut cb

32.62 31.62
6.70 7.70
Cb end Sut

13.9 14.0 18.6 26.5 32.5 24.56 32.61 31.58 32.17 32.89 33.31 35.14
25.4 25.3 20.7 12.8 6.8 14.76 6.7 7.74 7.15 6.43 5.95 4.18
50 37 30 16 5 10 Cb Sut grate 15 30 40 80

39.32

BM starting 168 33.68 33.68 seem to
Please check Wabaska plans as slopes encroach

3+00 ℄ Soto St

2+70 Wly Soto St

2+42 28.5 Rt℄ 10" Power Pole #4435

2+35

2+00

1+50

1+35 27.9 Rt℄ 10" Power Pole #4475

1+00

0+93 30.2 Rt℄ 3' walk

Lt= North ℄ Rt= South

22.8	24.5	31.6	31.6	31.9	31.8	32.8
12.6	10.2	3.8	3.8	4.0	3.6	2.6
40	30	15		15	30	72
17.8	24.2	30.2	31.5	31.6	31.7	33.9
17.6	11.2	5.2	3.9	3.8	3.7	1.5
40	30	20		15	30	72
22.8	28.5	29.9	30.8	31.1	31.5	32.6
12.6	6.9	5.5	4.2	4.3	3.9	2.8
40	30	28		15	30	40
19.8	26.5	29.4	30.6	30.9	31.2	32.4
15.6	8.9	6.0	4.8	4.5	4.2	3.0
40	30	25		15	30	40
19.8	27.3	28.9	30.2	30.7	31.2	31.8
15.6	8.1	6.5	5.2	4.7	4.2	3.6
40	30	28		15	30	40
25.5	29.7	30.2	30.4	30.7	31.3	32.1	33.8
9.2	5.7	5.2	5.1	4.7	4.1	3.3	1.6
40	35	30	15		15	30	40
32.63	34.34
27.3	1.02
30.2	40
walk	

T 35.36

Soap Box Derby run.
Collier Park

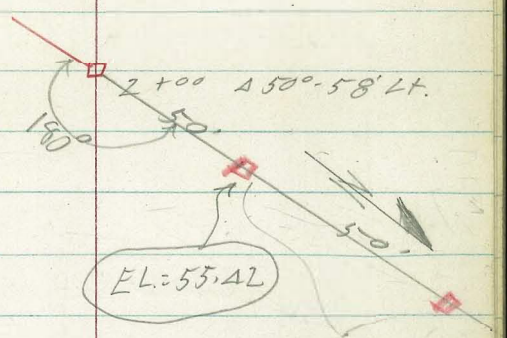
5-16-52

C.H.S.
Bc99
Altman
Johns

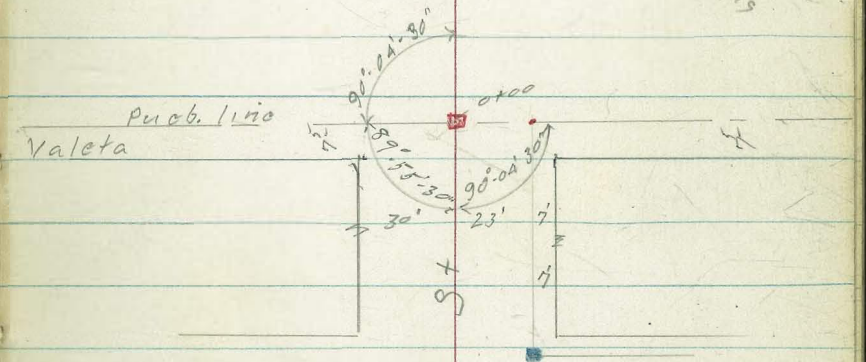
■ denotes Fd. Conc. Mon
□ " " 3/4" Tack
□ " Set 1/2" + disk
• " Nail

Ref.
FB 1375
4-7

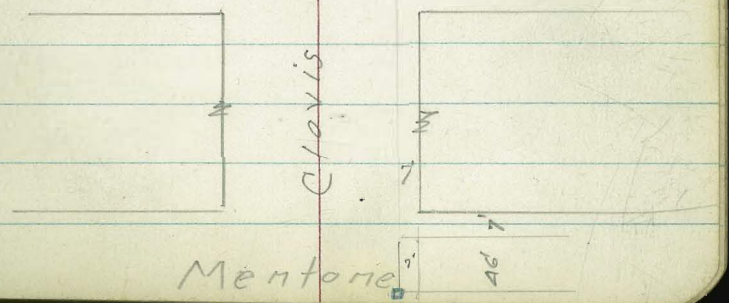
WO 20992



R.R. Hub & disk
Set 9/29/52
C.H.S.

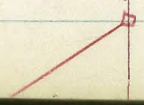


Montalvo



8+00 = P.O.T.

2+00 ∠ 50°-58'-17 (Page 8)



T.P. #8	5.62	62.44	10.48	56.82
1+00				
0+50				
0+00 = Pueb. line (P-8)				
T.P.#7	4.70	67.30	5.01	62.60
Set				
B.M.#3	S.S.		8.35	59.26
T.P.#6	5.01	67.61	3.38	62.60
Set.				
B.M.#2	9.16	65.98	3.33	56.82
T.P.#5	10.02	60.15	0.59	50.13
T.P.#4	12.56	50.72	0.51	38.16
T.P.#3	12.94	38.67	0.12	25.73
T.P.#2	9.54	25.85	11.75	16.31
T.P.#1	5.48	28.06	12.87	22.58
B.M.#1	1.77	35.45	—	33.68

#

55.6 63.2 60.1 60.7 56.0
1.8 4.1 7.2 6.6 11.3
50 26 20 50

64.1 61.8 62.1 62.1 57.6
1.2 5.15 5.2 5.2 9.7
50 17 12 50

55.2 63.9 59.8
2.1 4.4 7.5
30 30

67.30.

= T.P. #6

S.W. 7' Conc. Mon. Montalvo + Clovis

℄ Hub. Sta. 0+00

A' Hub. Sta. 2+00 ℄ (also set. B.M. on 50' R.P. - page 8 ↗ 4-29-54)

B.P. wly ol. Etiwanda at Castellar

#9

T.P.	2.02	40.89	12.78	38.87
5+00				
4+00				
T.P. #9	1.72	51.65	12.51	49.93
3+00				
2+18	Lt. = ∠ in top of bank			
2+14.3				
2+00 = Δ 50°-58' Lt.	on split of ∠			
1+85.7				
1+75	38' Lt. = ∠ in top of bank			

∠

60.1 59.7 47.9 45.1 41.6 42.9 40.9 25.2
+8.4 +8.0 3.8 8.0 10.1 10.8 10.8 26.5
45 41 34 28 20 44 100

63.7 63.3 51.7 48.9 46.8 45.8 45.8 29.7
+12.0 +11.6 0.0 2.8 4.9 6.5 5.9 22.0
55 52 45 32 32 56 100

51.65

63.9 63.7 53.0 51.1 50.5 49.6 52.7 37.4
+1.5 +1.3 9.4 11.3 11.9 12.8 9.7 25.0
55 53 48 42 35 68 120

61.6 61.3 54.7 55.2 54.5 53.4 48.2
0.18 1.1 7.7 7.2 5.9 7.0 14.2
50 44 30. 32 50 100

54.9 55.5 54.6 53.2
7.5 6.9 5.8 9.2
30 25 50

54.9 56.9 54.2 51.8
7.5 5.5 8.2 10.6
33.23. 33.23 60

54.9 57.5 57.8 54.5
7.5 4.9 4.6 5.9
30 8 30

62.0 61.3 56.3 57.8 58.2 57.3 53.8
0.4 1.1 6.2 4.6 4.2 5.1 8.6
50 38 30 8 15 50

62.44

T.P.# 12	5.83	23.~~44~~ 43	9.70	~~17.58~~ 17.60
12+00				
11+00				
10+00				
T.P. #11	6.60	~~27.78~~ 27.30	9.30	~~20.68~~ 20.70
9+00				
8+00 = ℄ P.O.T.				
T.P.#10	1.22	~~39.98~~ 30.00	12.11	28.~~76~~ 78
7+00				
6+00				

23.6 24.3 14.6 16.0 14.1
3.7 6.0 10.7 11.3 11.2
100 80 40 100

29.1 16.0 16.2
+1.8 11.3 14.4
100 100

27.3 20.8 16.8 16.1
0.0 6.5 10.5 11.2
100 35 100

~~27.78~~ 30.
27.

33.0 30.0 23.6 18.1 16.8
+3.0 0.0 7.4 14.9 14.2
80 50 40 100

40.5 40.0 33.0 24.3 25.0 22.8 17.3 15.9
+10.5 +10.0 +3.0 3.1 5.0 7.2 12.7 14.1
60 55 52 38 40 58 100

~~39.98~~ 30.00

51.1 50.9 39.2 33.6 30.6 28.6 15.9 14.9 14.9
+10.2 +10.0 2.7 7.3 10.3 12.3 25.0 26.0 26.0
52 49 43 33 34 82 100 125

51.4 56.9 42.9 39.0 35.5 34.6 20.5
+16.5 +16.0 +2.0 1.9 5.4 6.3 20.4
60 56 53 46 35 100

~~87~~ 89
40.

			3.11	83.73
T.P. #17	3.65	36.84	3.18	33.19
T.P. #16	7.14	36.37	0.42	29.23
T.P. #15	7.99	29.65	1.06	21.66
T.P. #14	5.40	22.72	3.05	17.32
T.P. #13	4.18	20.37	7.24	16.19

33.68 = B.M. #1 - P.10.

16+00

31.6	21.4	16.6	16.6	16.5	25.4	
+8.2	2.0	6.8	6.8	6.9	+2.0	
75	40	15		50	75	

15+00

29.6	20.0	17.8	16.2	16.6	20.1	
+6.2	3.4	6.2	7.2	6.8	3.3	
70	50	25		90	100	

14+00

23.4	14.6	16.2	16.8	17.9	23.4	
0.0	6.8	7.2	7.2	5.5	0.0	
100	50		95	100	110	

13+00

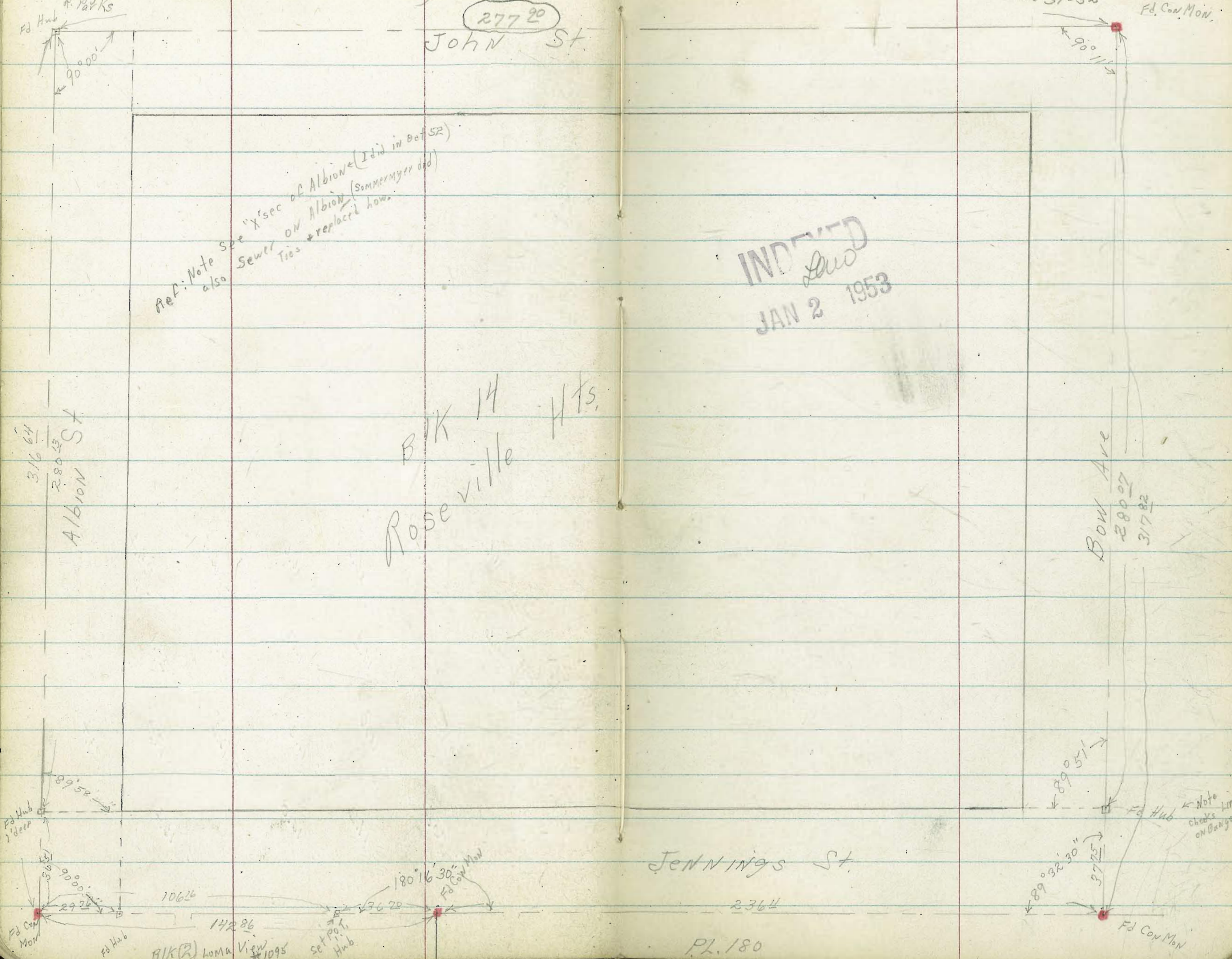
23.4	17.8	16.0		16.4
0.0	6.2	7.4		7.0
100	60			100

23.43

D. Smith
C. Allen
R. Taylor
R. Parks

Survey Blk 14 Roseville Hts

WO#23239 14
12-31-52



277 20
John St
Fd Hub
90°00'
Fd. Con Mon.
90° 11'
Ref: Note See "X'sec of Albion" (I did in Oct 52)
also Sewer on Albion (Sommermyer did)
Ties & replaced how.
INDEXED
JAN 2 1953
Blk 14 Roseville Hts.
Albion St
316 64
280 13
Bow Ave
280 07
317 82
89°52'
Fd Hub 1' deep
36 51
90°00'
29 24
106 16
142 86
76 20
180°16'30"
Fd Con Mon
Fd Con Mon
Fd Hub
Set Pot. Hub
Blk (2) Loma View #1095
Jennings St
236 4
PL. 180
89°51'
Fd Hub
Note checks line on Dangor
89°32'30"
37 25
Fd Con Mon

X-Sec Alley Blk 4 - Washington Hts.

C. Allen

D. Sisson

C. Powell

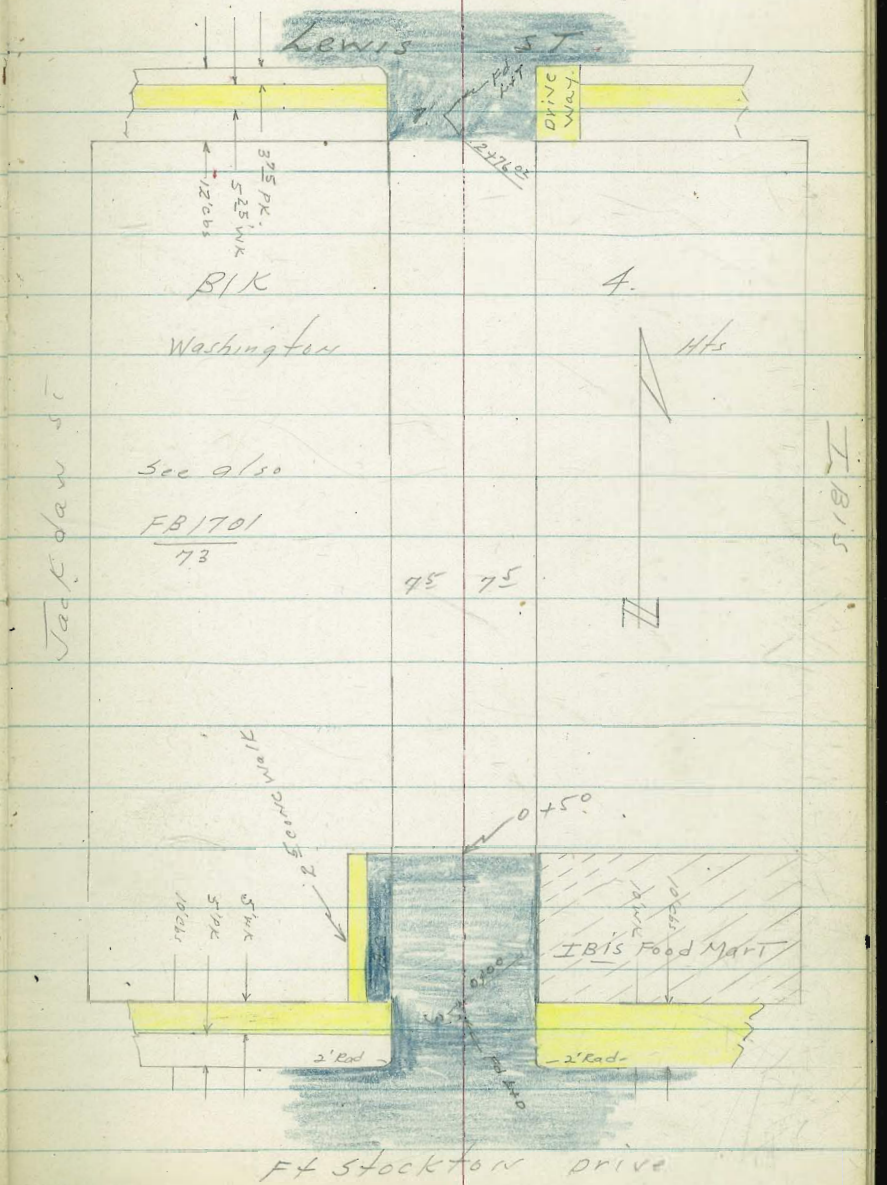
4-15-53

W.O.# 32167

Ref. FB 1701 - Page 73

A.C. P.T.

Portland Concrete



X-Sec Alley Blk 4- Washington Hts

0+25

A.C. Pave in Alley extends to ely walk on West

0+00 5 - 10 3 Lt SE cor 2 5 wide conc walk ⊥ to ℄

Curb on Left in poor condition

0+00 - 7.8 Rt = S.W cor IBIS Food Mart

0-08 - Alley Returns - B.C.'s

Redwood
I.G. Cotton
4-17-53

0-10 - N'ly Curb. line Ft Stockton Dr.

BM. 6.24 276.76 NW BP. Jack Davis Ft Stockton Dr 270.52

Lt = W'ly ℄ Rt = E'ly

272.42 4 34 10 0 W'ly edge AC

272.09 4 69 7 5 7 0

271.99 4 77

271.70 5 06

272.90 4 86 7 5

271.91 4 85 7 85 W'ly edge Bldg + Ely AC

272.73 4 53 10 3 SE cor Walk

271.80 4 96 7 5 Cb

271.80 4 96 7 5 Gut

271.43 5 33

271.57 5 19 7 5 Gut

271.68 5 08 7 5 Cb

271.65 5 11 7 6 Cb

271.23 5 53 7 5 Gut

271.17 5 59 Gut 7 4

271.52 5 24 7 4 cb

270.51 6 22 100 Gut

271.00 5 76 100 cb

271.98 .478 100 Cb

271.44 5 32 100 Gut

271.74 5 02 50 cb

271.17 5 59 50 G

271.64 5 15 95 cb

271.12 5 64 95 Gut

271.10 5 66 7 5

271.07 5 69

271.04 5 74 7 5

270.99 5 77 95 Gut

271.50 5 26 95 cb

270.75 6 01 50 Gut

271.29 5 47 50 cb

276.76 ⊥

X-sec Alley Blk 4 - Washington Hts

0+72 - 7.2 Rt = end 5.5 high board fence

6.9 Rt = begin 5.5' high board fence

0+52 - 6.7 Rt ℄ 8" telephone pole # 472419H-

TP1 5.37 277.83 4.30 272.46

0+50.5 } 7.5 LT = begin 4' high Lath fence

6.5 LT = ℄ 10" power pole # No Number

7.5 Rt = outlet down spout from Bldg -

7.8 Rt = NW Cor Ibis Food Mart

0+50 } = N'ly edge A.C. shotson header board.

0+47 - 7.9 Rt = ℄ 4' wide doorway to Ibis Food Mart

AC continues 7' N'ly.

0+43 - 10.0 LT = NE Cor 2.5 Conc Walk ⊥ to ℄

0+35.5 - 7.2 Rt = outlet down spout from Bldg.

LT = W'ly ℄ Rt = E'ly -

277.83 +

272.36 / 4.40 / 13.0 NW Cor AC Pave

272.35 / 4.41 / 7.5

271.96 / 4.80

272.20 / 4.56 / 7.5

272.21 / 4.55 / 7.8 at Bldg

272.26 / 4.50 / 7.9 Floor

272.26 / 4.50 / 10.3 NE Cor Wk

276.76

X-sec Alley Blk 4 - Washington Hts.

1+29 - 15⁴ LT = ℄ single garage - dirt floor

1+19 - 7³ Rt = N W cor frame house

1+14 - 8³ LT = end 4' high chicken wire fence

1+00

0+99 - 7³ Rt = S.W. cor Frame House

0+97 - 7⁸ LT = begin chicken wire fence - 4' high

0+89 - 10⁴ LT = ℄ Single garage Conc Floor

0+83 - 10⁴ LT = end 4' high Lath fence

19' wide

0+85 - 8³ Rt = ℄ Double garage conc floor

273.0
4⁸
15⁴
Dirt Floor

273.0 4⁸ 25

272.8 5⁰ 75

272.6 5²

272.3 5⁵ 75

272.3 5⁵ 25

272.76
5.07
10⁴
Floor

272.63
5.20
8³
Floor

277 8³ x

X-Sec Alley Blk 4 - Washington Hts

1+56 } 8 3 Rt = ℄ 1 5 conc walk
6 5 Rt = ℄ 4'x5' Rough Conc slab

1+54 - 8 3 Rt = begin 5' high board fence

1+53 11 0 LT = begin 3 car garage Conc Floor

1+53 - 8 8 LT = end 4' high Lath'd fence

1+50 - 8 5

1+48 - 7 7 Rt = ℄ Single garage - Dirt floor

1+43 - 6 2 LT = ℄ 14" power pole # A4079

1+41 - 6 2 = ℄ 10" Tel pole # 305-8764

1+40 - 8 5 LT = begin 4' high Lath'd fence

1+33 - 11 0 Rt = ℄ Single Conc floor

LT = W'ly ℄ Rt = E'ly 19

273.00
4 8 3
6 5
℄ Slab

273.07
4 7 6
8 3
Walk

273.01
4 8 2
11 0
Floor

272.9
4 9
25

273.0
4 8
7 5

273.2
4 6

273.0
4 8
7 5

273.0
4 8
2 5

273.0
4 8
7 7
Dirt Floor

272.70
5 13
11 0
Floor

27 7. 8.3

2+25

2+24- 7^{6} LT= S.E. COR shed-

2+14- 7^{2} Rt= ℄ Doorway frame house

2+00

7^{1} RT= S.W. COR Frame House

7'x11' Rough Conc. Slab in front of garage

1+93- 11^{2} LT= ℄ Single garage - Conc floor

1+85- 8^{3} Rt= end 5' high board fence

1+81- 10^{9} LT= end 3 car garage Conc floor

1+67- 10^{8} LT= ℄ 3 car garage - Conc floor

LT = W'ly		℄	Rt = E'ly
	272.6 5^{2} 7^{5}	272.4 5^{1}	272.3 5^{5} 7^{5}
			273.71 4^{12} 7^{2} Floor
273.1 4^{2} 25	273.1 4^{2} 7^{5}	273.1 4^{7}	273.0 4^{8} 7^{1}
	273.22 4^{60} 11^{2} Floor		
	273.11 4^{72} 10^{9} Floor		
	273.09 4^{74} 10^{8} Floor		

277.83

Lt = W'ly & Rt-ely.

TP2	5,65	276.14	9.34	270.49	276.14

2+71 - 6° Rt = ℄ Dead Man.

2+53 - 8° Rt = ℄ 2.5' wide Euginia hedge over hangs Alley.

2+52 - 6° Rt = ℄ 10" Tel pole # No Number

2+51. 7.4 Rt = N.W. COR garage opening to Lewis

2+50

2+45 - 7.7 Lt = ℄ N+S hedge (3' wide) over hangs Alley.

2+40 - 7.6 Lt = NE COR shed

2+31 - 7.2 Rt = S.W. COR garage opening to Lewis

2+29 - 7.3 Rt = N.W. COR Frame house

7 1.9	7 1.8	7 1.7
5.9	6.0	6.1
7.5		7.5

277.83 x

X-Sec Alley Blk 4 - Washington Hts.   LT = W'ly   ℄   Rt = E'ly -   22

				(270.52)
TP4 Start. B.M.			5.92	270.53
TP3	3.95	276.45	3.64	272.50

2+88.02 Sly Curb Lewis St

271.64 / 4.50 / 50 Cb; 270.97 / 5.17 / 50 GuT; 270.70 / 5.44 / 95 Cb BC; 270.03 / 6.11 / 95 GuT BC; 269.98 / 6.16 / 75; 269.74 / 6.40; 269.62 / 6.52 / 75 No Return; 268.55 / 7.59 / 50 GuT; 269.32 / 6.82 / 50 Cb

Ely B.C. Replaced by Drive
2+86.02 Alley Return BC ON West

270.71 / 5.43 / 77 Cb; 270.20 / 5.94 / 77 GuT; 269.74 / 6.40; 270.04 / 6.10 / 74 ON Drive

2+79 - 8.6 Rt = end 2.5' wide Eugenia hedge

2+76.02 = Sly Line Lewis + Sly edge A.C.

270.98 / 5.16 / 72 Cb; 270.89 / 5.25 / 72 GuT; 270.42 / 5.72; 270.57 / 5.57 / 74 GuT; 270.59 / 5.55 / 74 Cb

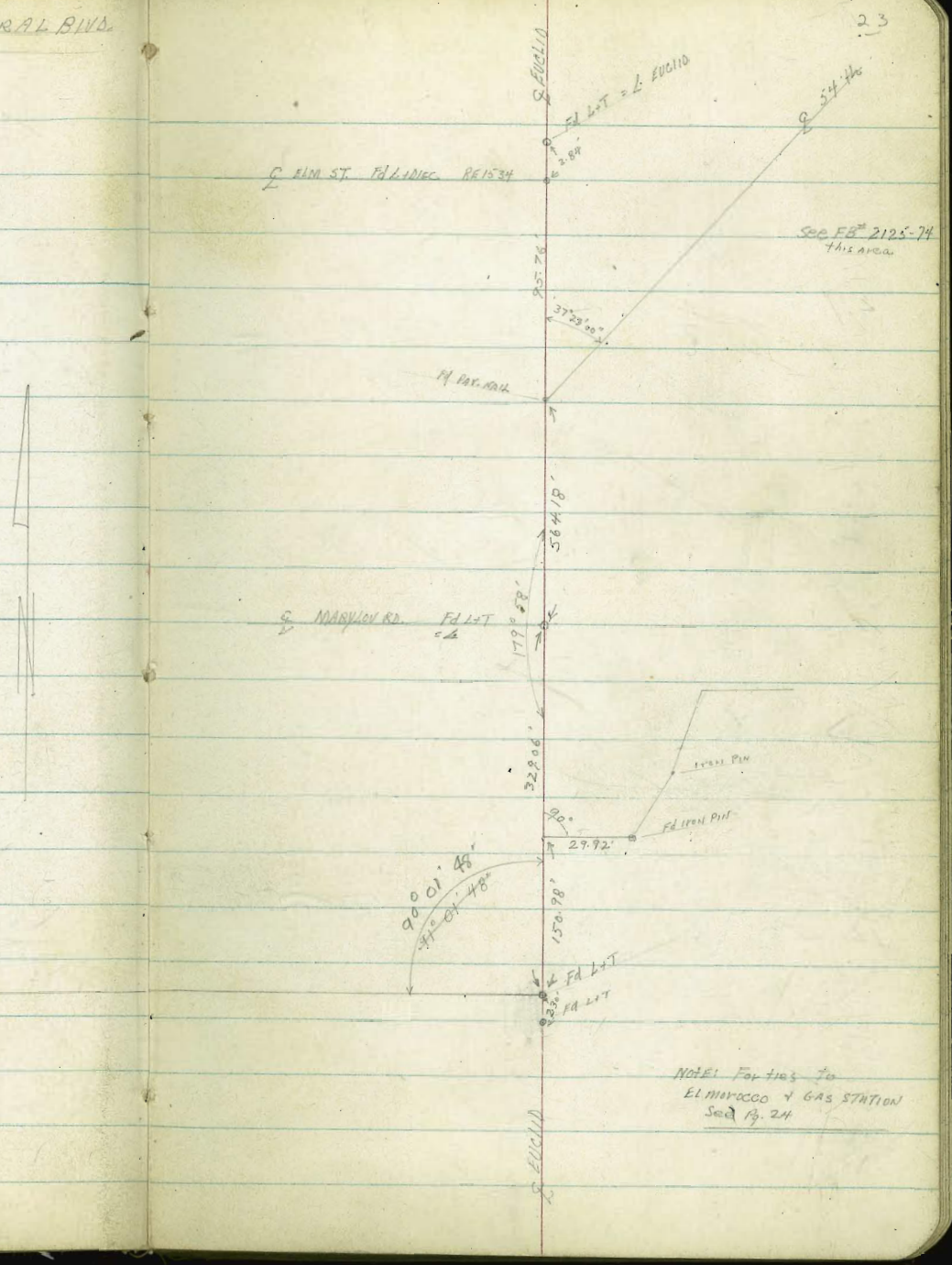
2+73.5 - 8.2 LT = end 3' wide hedge

2+73 - 6.9 LT = ℄ 12" Power pole A 4089 -

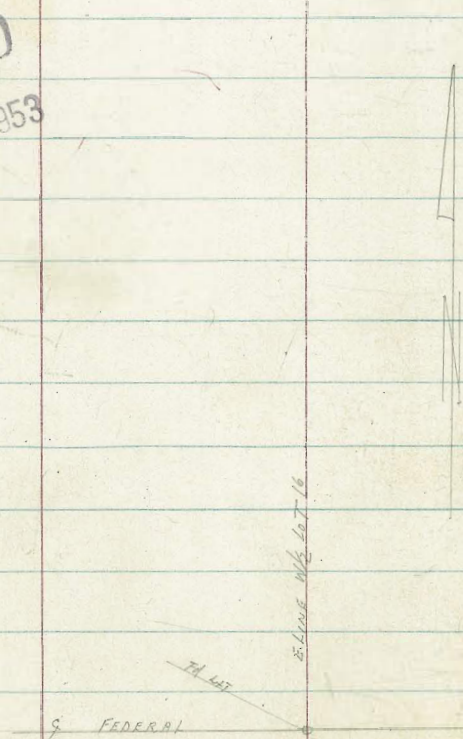
276.14 +

Clark
Shephard
Bruner
O'Neil
7-29-53
W.O. 22048

Ties - EUCLID AVE & FEDERAL BLVD.

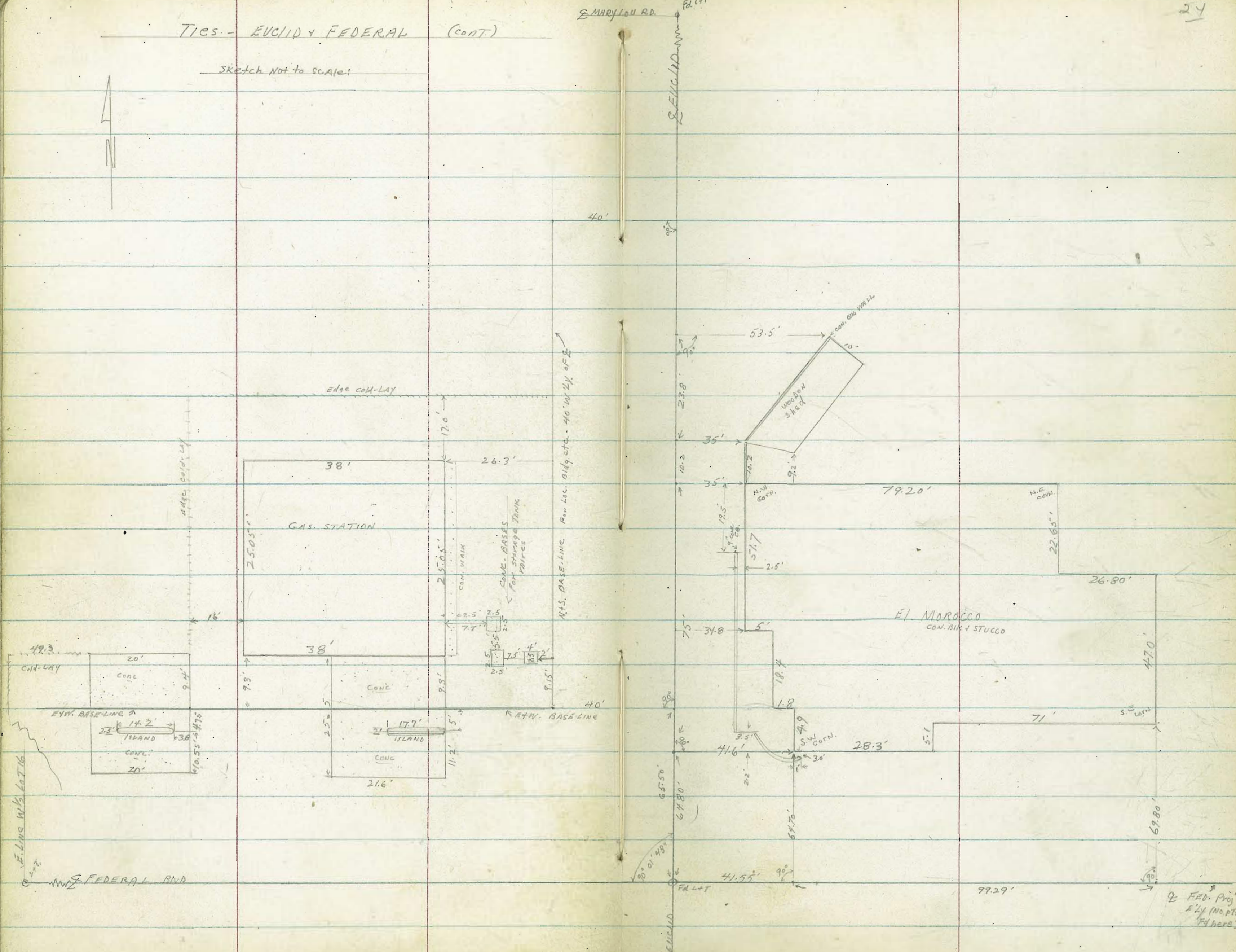


NOTE: For ties to El Morocco & GAS STATION See Pg. 24



Ties - Euclid + Federal (cont.)

Sketch Not to scale:



INDEXED
YER
AUG 27 1954

X-Sec Nashville ST - LaSalle to Lapwai ST

X-sec Jupiter ST, La Salle ST, Western ST and Lapwai ST for entire length

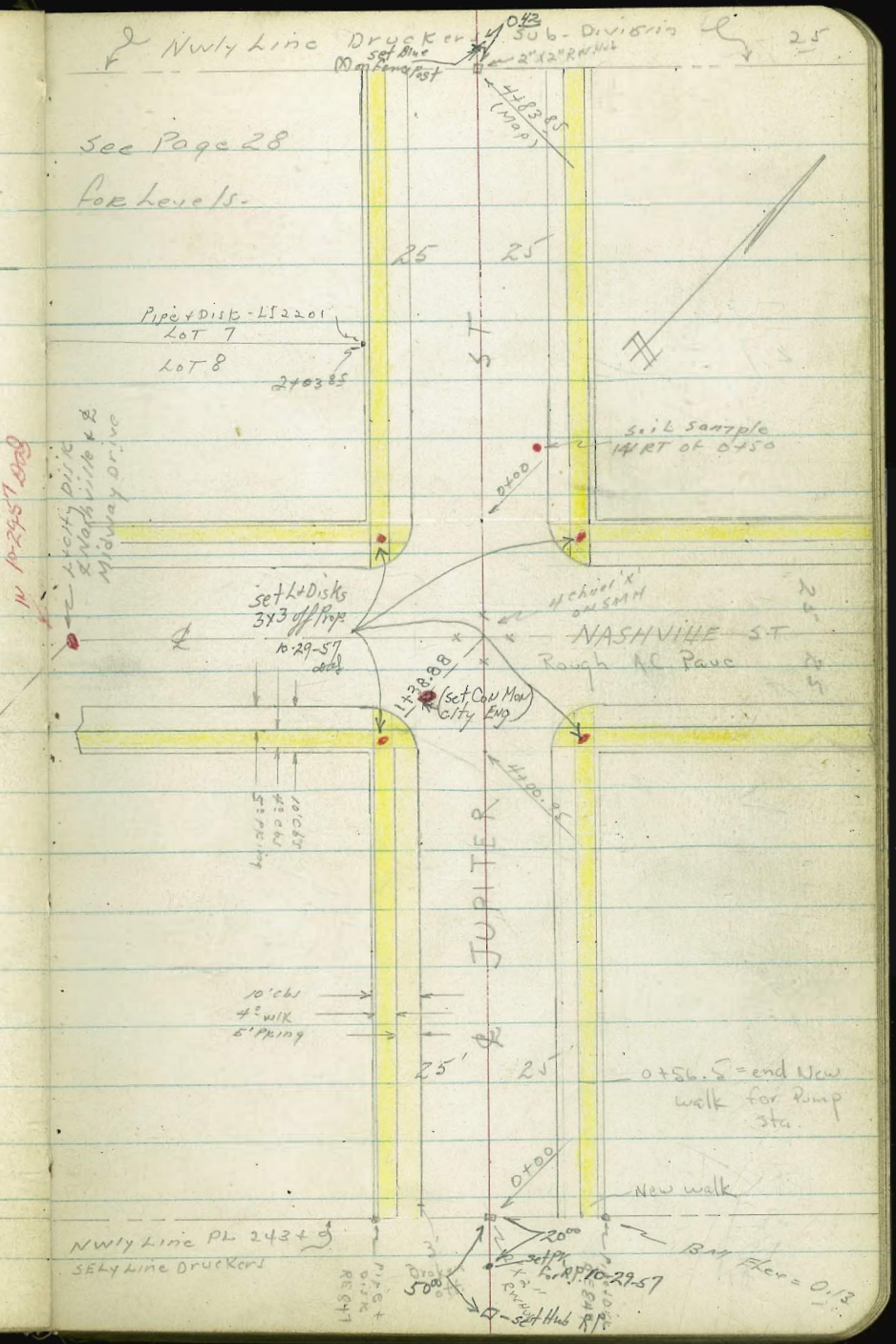
WO # 31971- Aug 24, 1954.

C. Allen, d Sisson, C. Powell-

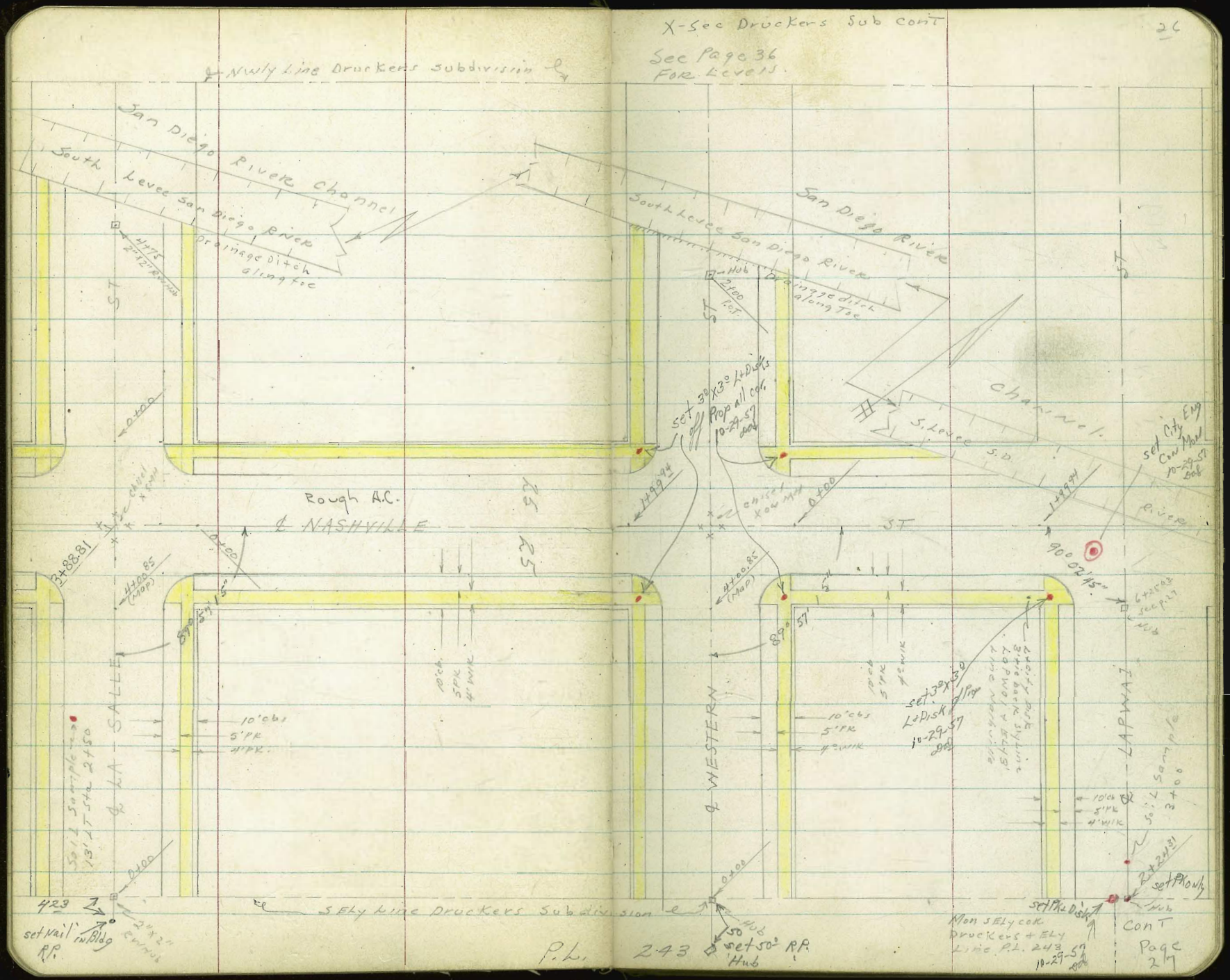
Ref- TP sheet 649, File Map # 1584, FB 572.

See P. 27 For Detail

See Page 28 for Levels-



See Page 36 FOR Levels.

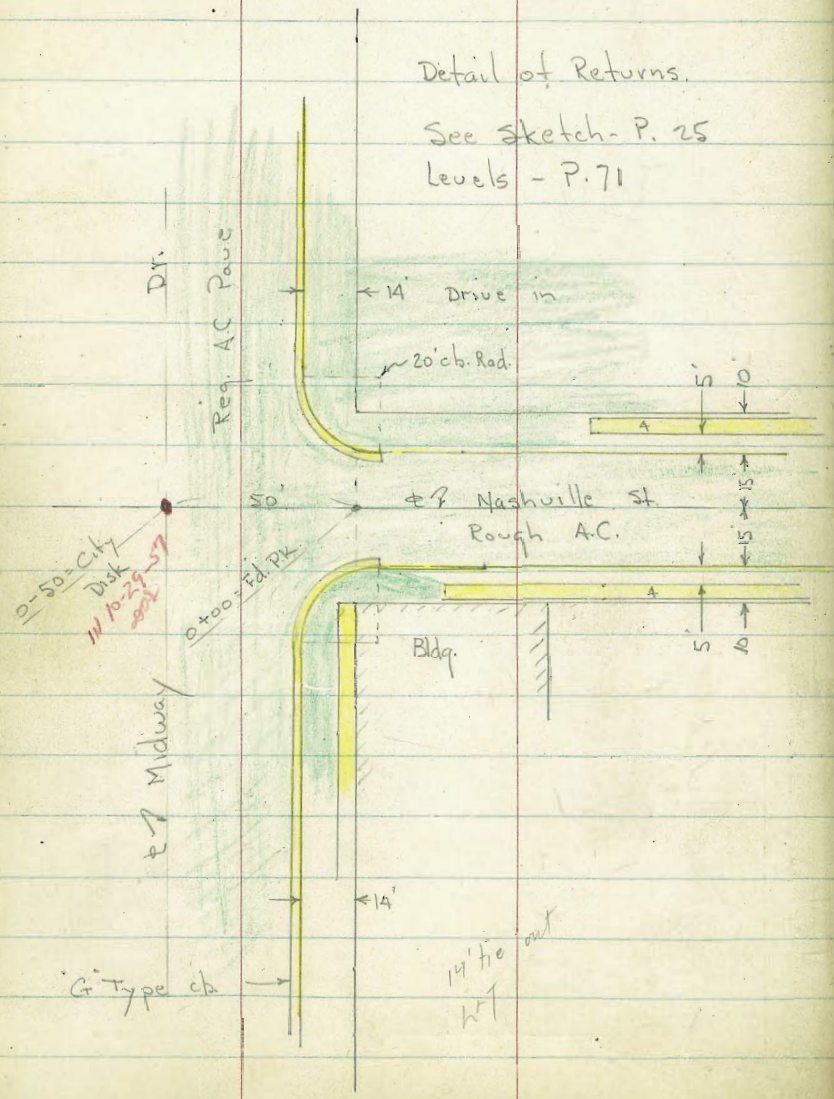


X-sec Nashville, Western, La Salle, Lapwai Sts Cont.

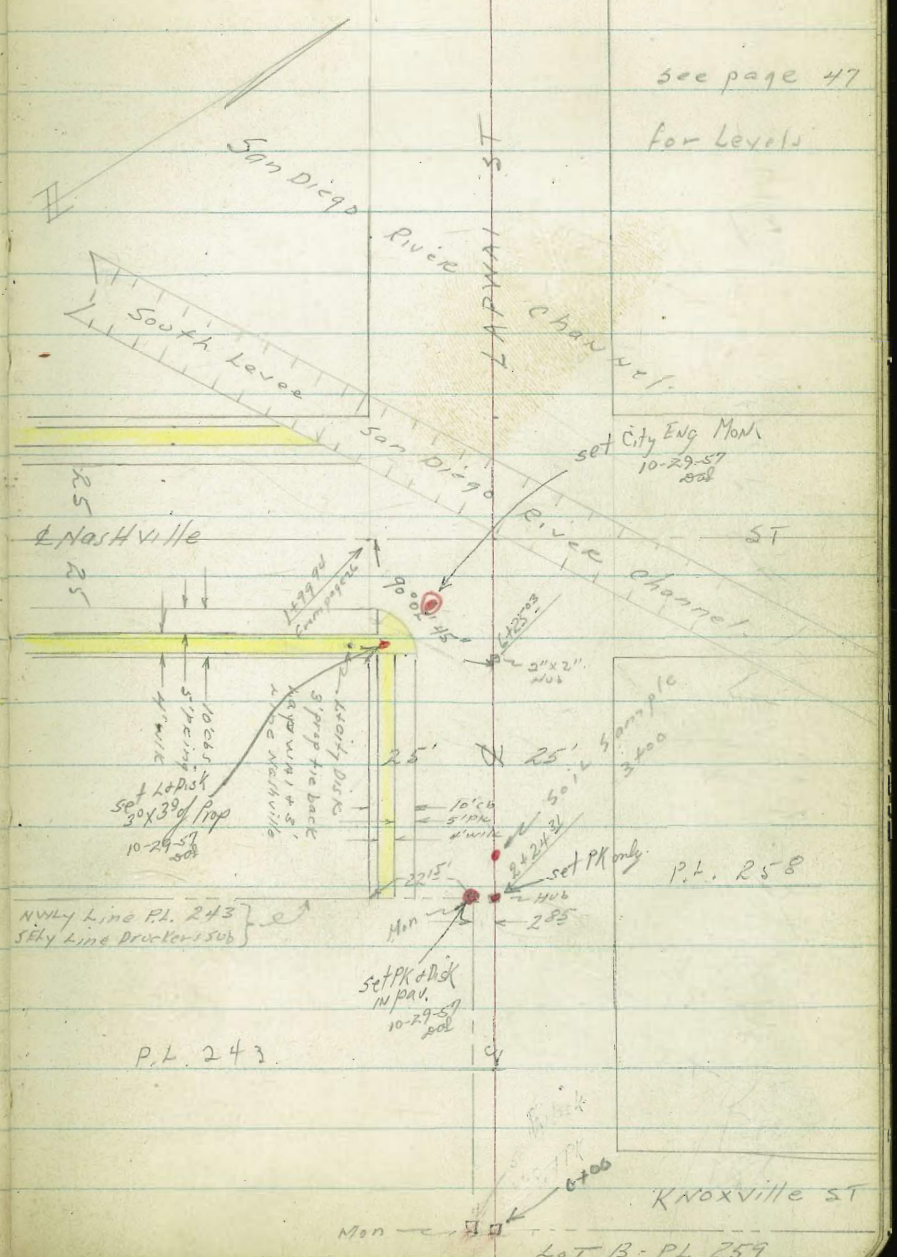
Detail of Returns.

See Sketch - P. 25

Levels - P. 71



NWly Line Drocker Sub div



X-Sec Jupiter St. See Page 25 for Sketch

1+00

0+82 - 24 6 RT = begin 8" hollow tile retaining wall ✓

0+50

0+31 - 0 4 = ℄ Sanitary Sewer manhole. ✓

0+03 = Beg. cb on Lt. - Broken - 5-56 - 7.0.

0+02 - 18° LT = ℄ 10" Power pole # H5-75 ✓

15 4 LT - begin curb
14 5 RT = begin curb
31 y 2 5 Curb broken on Left

0+00 = SELy Line Druckers Sub + begin Jupiter

Side walk + Curbs in poor Condition - Little value

check Elev. Before Reducing →

BM- 6.37 6.50 0.19 = 0.13

LT ℄ Jupiter RT 28

0.2 -0.1 -0.24 -0.94 -0.74 -0.24 -0.19 0.00 0.16 1.70
6 4 6 7 6 80 7 5 7 3 6 8 6 75 6 6 6 7 4 85
25 20 3 W/K 15 3 Top cb 15 3 Dirt out 14 5 Dirt out 14 5 Top cb 19 5 W/y W/K 24 6 gr 25°

0.1 -0.24 1.81 1.66
6 5 6 8 4 75 4 2
24 6 Ground 24 6 Foot 24 6 Top wall 26 gr

-0.04 -0.24 -0.29 -1.04 -0.74 -0.64 -0.38 -0.20 -0.14 0.1
6 6 6 80 6 85 7 6 7 3 7 2 6 94 6 70 6 5
25 20 3 Ely W/K 15 3 Top cb 15 3 Dirt out 14 3 out Dirt 14 3 Top cb 19 3 W/y W/K 25

-0.30
6 86
Rim
0 4

0.9 0.4 -0.14 -0.84 -0.84 -0.44 -0.37 -0.34 -0.19 -0.17 0.2 1.66
5 7 6 2 6 7 7 4 7 4 7 0 6 80 6 75 6 73 6 4 4 8
50 25 15 4 Broken cb 15 4 out 14 5 out 14 5 Top cb 19 5 W/y of walk 23 5 Ely W/K 25 50

6 50 → Use 6.56

Our Elev. - See P. 71

No information on source of elev. on 1" Pipe Ely and Jupiter + SELy Line Druckers (see p. 25.) (RE 847)

X-Sec Jupiter

2+40 - 24.8 RT = end Hollow tile Retaining Wall

2+16 - 15.2 = LT = ℄ 25' Drive - Conc in parking

2+00

1+59 - 16.5 LT = ℄ 12" Power pole #JP455

1+50

LT ℄ RT

Jupiter

29

0.06 -0.24 1.42 1.46
6.5 6.8 5.4 5.1
gr at wall 24.8 | Foot 24.8 | Top wall 24.8 | 26

0.01 0.79
6.5.5 7.3.5
20.2 Brk | 15.2 Lip D-

7.16
4.4
5.0

0.76 0.26 0.11 0.04 0.64 0.44 0.04 0.06 0.06 0.14 1.76
5.0 6.3 6.4.5 6.6.0 7.2 7.0 6.6 6.5 6.5 6.4 4.8
50 25 20.2 15.2 Topcb 15.2 Dirt Out 14.6 Dirt Out 14.6 Topcb 19.6 Wlk 24.2 gr at Wall 25

1.34
5.2
50

1.61 1.66 1.26
4.9.5 4.2 4.3
24.6 25 50

0.1 0.1 0.22 0.74 0.44 0.14 0.12 0.00 0.16
6.7 6.7 6.7.8 7.3 7.0 6.7 6.6.8 6.5.6 6.4
25 20.2 Wlk | 15.3 Topcb | 15.2 Dirt Out | 14.6 Dirt Out | 14.6 Top cb | 19.6 Wlk | 24.6 gr at Wall

6.5.0 6.56/54

X-Sec Jupiter

15^{2} LT = cb BC - 10' Radius } Poor
14^{5} RT = cb BC - 10' Radius } Condition

4+00 9^{5} = SELy Line Nashville ST

3+50

TP, 5.34 5.40 6.44 0:06

3+00

2+83 - 17^{0} LT = ⊄ 12" Power Pole # PH535 ✓

2+50

LT ⊄ RT

Jupiter

1.36	0.36	0.21	0.21	-0.04	-0.14	-0.04	0.11	0.26	0.68	1.16
4^{1}	5^{1}	5^{15}	5^{25}	5^{5}	5^{6}	5^{5}	5^{35}	5^{2}	4^{8}	4^{3}
50	25	20^{2} walk	15^{2} Top cb BC	15^{2} Dirt gut BC		14^{5} Dirt gut BC	14^{5} Top cb BC	19^{5} wlk	25	50

2.3	0.26	0.16	0.10	-0.34	-0.14	0.06	0.09	0.26	0.56	2.86
3^{2}	5^{0}	5^{3}	5^{36}	5^{8}	5^{6}	5^{4}	5^{37}	5^{2}	4^{9}	2^{6}
50	25	20^{3} wlk	15^{3} Top cb	15^{3} Dirt gut		14^{7} Dirt gut	14^{7} Top cb	19^{7} wlk	25	50

5.40 ⊼ 5.46

1.56	0.46	0.16	0.04	-0.44	-0.14	0.06	0.04	0.16	0.36	0.06
5^{0}	6^{1}	6^{4}	6^{50}	7^{0}	6^{7}	6^{5}	6^{52}	6^{4}	6^{2}	6^{5}
50	25	20^{3} wlk	15^{3} Top cb	15^{3} Dirt gut		14^{7} Dirt gut	14^{7} Top cb	19^{7} wlk	25	50

0.96	0.26	0.04	-0.04	-0.64	-0.24	0.04	0.10	0.21	0.56	2.16
5^{6}	6^{3}	6^{5}	6^{60}	7^{2}	6^{0}	6^{5}	6^{46}	6^{35}	6^{0}	4^{4}
50	25	20^{3} wlk	15^{3} Top cb	15^{3} Dirt gut		14^{7} Dirt gut	14^{7} Top cb	19^{7} wlk	25	50

6.50 ⊼ 6.56

X-sec Jupiter

LT ℄ Jupiter RT

0.70	0.24		-0.34	0.11
4^{76}	5^{22}		5^{8}	5^{35}
125 in Drive	125 gut		125 gut	125 Top cb

Nwly edge Rough A.C. pave

4+40 95 = Nwly Curb Line Nashville ST

0.32	-0.04	0.18	-0.14	-0.24	-0.24	-0.34	-0.34	0.04	-0.14	0.16
5^{14}	5^{5}	5^{28}	5^{6}	5^{7}	5^{7}	5^{8}	5^{8}	5^{42}	5^{6}	5^{30}
75 Top cb	75 gut	25 Top cb	25 gut	15		15	25 gut BC	25 Top cb BC	75 gut	75 Top cb

℄ Sewer Manhole

4+25 95 = ℄ Nashville - Rough A.C. Pav.

0.94	0.56	0.56	0.31	0.36	0.46	0.36
4^{5}	4^{9}	4^{9}	5^{15}	5^{1}	5^{0}	5^{1}
125	25	15	Rim SMH	15	25	100

0.64	0.2	0.14	-0.04	-0.34	0.08
4^{82}	5^{3}	5^{32}	5^{5}	5^{8}	5^{38}
115 Top cb	115 gut	100 Top cb	100 gut	125 gut	125 Top cb

SELy edge Very Rough A.C. Paving Nashville ST

4+10 95 = SELy Curb Line Nashville ST

0.23	-0.04	0.20	-0.04	-0.14	-0.04	-0.14	-0.04	0.01	-0.14	0.10
5^{23}	5^{5}	5^{26}	5^{5}	5^{6}	5^{5}	5^{6}	5^{5}	5^{45}	5^{6}	5^{36}
75 Top cb	75 gut	25 Top cb	25 gut	15		15	25 gut BC	25 Top cb BC	75 gut	75 Top cb

5^{40} x 5-46

X-See Jupiter

1+50 Walk to Nwly No good
20° RT = end good conc sidewalk

1+23 16.5 LT = ℄ 12" Power pole # 4139. ✓

1+00

0+95 - 14.9 RT = ℄ 7' wide conc Drive ✓

0+50 - Walk on Right in good condition

15.1 LT = BC curb RET
14.7 RT = B.C. curb RET
= Nwly Line Nashville ST

4+50.95 back = 0+00 Ahead

Walk on Right in good condition
Curb on Right in very Poor condition
Curb + Walk on Left in poor condition

32

Jupiter

LT				℄	RT			
-0.04	-0.24	-0.27	-0.24	0.06	-0.54	-0.28	-0.19	-0.14
5.5	5.7	5.73	5.7	5.4	6.0	5.74	5.65	5.6
50 25	20 Walk	15 Topcb	15 DirtQut		15 Dirt Out	15 Top Cb	20 Wlk	25

					-0.06	-0.05		
					5.52	5.51		
					20 Wlk	24 Wlk		
0.16	-0.04	-0.14	-0.44	0.06	-0.54	-0.12	0.02	0.26	1.26
5.3	5.5	5.60	5.9	5.4	6.0	5.58	5.44	5.2	4.2
25	20 Wlk	Topcb 15	dirt Out 15		14.9 dirt Out	14.9 Topcb	19.9 Wlk	25	50

					-0.55	0.06	0.18	1.21
					6.01	5.40	5.28	4.25
					14.9 Lip	19.9 Brk	25	40 Floor gar

0.16	0.04	0.04	-0.44	0.16	-0.54	-0.09	0.15	0.36
5.3	5.42	5.42	5.9	5.3	6.0	5.55	5.31	5.1
25	20.1 Wlk	15.1 Top Cb	15.1 dirt Out		14.9 Dirt Out	14.9 Topcb	19.9 Wlk	25

0.14	0.13	0.18	-0.34	0.14	-0.44	0.02	0.13	0.16
5.1	5.2	5.28	5.8	5.6	5.9	5.44	5.33	5.3
25	20.1 Ely Wlk	15.1 Topcb BC	15.1 Dirt Out BC		14.7 Dirt Out BC	14.7 Topcb BC	19.7 Wlk Wlk	25

5.40 T 5.46

X-sec Jupiter

Frame APT
2+62 - 27.0 LT = ℄ entrance way to 2 story

dirt - use top curb
No shots on walk due to depth under

2+50

2+43 - 16.5 LT = ℄ 12" Power pole 4169

2+19 - 25.1 LT = ℄ 3.0 wide Conc walk
11' Conc. Dr To S. Now Same Elev.
4-56

TP2 5.16 5.18 5.38 0.02

Walk on Left deep under Dirt

2+00

LT ℄ Jupiter RT

1.22 / 4.02 / 27.0 Floor elev
0.56 / 5.0 / 27.0 gr

0.66 / 5.9 / 25
0.04 / 5.2 / 20.0 ground over walk
0.69 / 5.93 / 15.0 Top Cb
0.04 / 5.2 / 15.0 ground over Cb
0.06 / 5.3
0.76 / 6.0 / 15.0 Dirt gut
0.64 / 5.88 / 15.0 Top Cb
0.66 / 5.9 / 20.0 walk
0.16 / 5.4 / 20 gr over walk
0.06 / 5.3 / 25
0.44 / 4.8 / 50

0.65 / 4.59 / 35.1 walk
0.48 / 4.76 / 25.1 walk

5.18 x 5.24

0.26 / 5.2 / 25
0.06 / 5.4 / 20 ground over walk
0.35 / 5.81 / 20.0 walk
0.44 / 5.95 / 15.0 Top Cb
0.06 / 5.5 / 15.0 Dirt gut
0.06 / 5.4
0.44 / 5.9 / 15.0 dirt gut
0.24 / 5.70 / 15.0 Top Cb
0.32 / 5.78 / 20.0 walk
0.34 / 5.8 / 25

5.40 x 5.46

X-sec Jupiter

4+43.8 - 25.3' Lt. = Beg. Conc. Slab

4+40

27.8 LT = ℄ Frame House

4+24 - 24^{4} LT = ℄ 4' wide Conc Steps ✓

4+00

3+50

3+49 - 16^{5} LT = ℄ 10" P.P. # H211. ✓

3+00 - Due to depth of Dirt, No Shot on walk

LT ℄ Jupiter RT

4.98 / 0.26 / 45 — 4.89 / 0.35 / 25.3 — Conc.

	LT					℄	RT				
4+40	0.34	0.14	0.04	-1.32	0.12	-0.16	-0.36	-1.41	-0.66	-0.36	0.24
	4^{9}	5^{1}	5^{2}	6^{56}	5^{1}	5^{4}	5^{6}	6^{65}	5^{9}	5^{6}	5^{0}
	50	25	20.0 gr over Wlk	15.0 Top Cb	15.0 gr over curb		15.0 gr. over curb	15.0 Top Cb.	20 gr over Wlk	25	50

4+24	-0.06	0.37	3.11
	5^{3}	4^{87}	2^{13}
	24^{4} groun	24^{4} Lower Riser	27.8 Floor Frame House

	LT					℄	RT				
4+00	1.14	0.24	0.04	-1.24	0.04	-0.06	-0.76	-1.13	-0.66	-0.16	0.34
	4^{1}	5^{0}	5^{2}	6^{48}	5^{2}	5^{3}	6^{0}	6^{37}	5^{9}	5^{4}	4^{9}
	50	25	20.0 gr over Wlk	15.0 Top. Cb	15.0 gr over Cb		15.0 ground over cb	15.0 Top cb	20.0 gr over Wlk	25	50

	LT					℄	RT				
3+50	0.24	0.04	0.04	-0.94	0.04	0.04	-0.76	-1.03	-0.46	-0.06	0.24
	5^{0}	5^{2}	5^{2}	6^{18}	5^{2}	5^{2}	6^{0}	6^{27}	5^{7}	5^{3}	5^{0}
	50	25	20 gr over Wlk	15.0 Top Cb	15.0 gr over curb		15.0 ground over cb	15.0 Top cb	20.0	25	50

	LT					℄	RT				
3+00	-0.06	-0.16	-0.16	-0.78	0.04	0.14	-0.56	-0.81	-0.26	0.04	0.34
	5^{3}	5^{4}	5^{4}	6^{02}	5^{2}	5^{1}	5^{8}	6^{05}	5^{5}	5^{2}	4^{9}
	50	25	20	15 Top Cb	15.0 gr over cb.		15.0 Dirt	15.0 Top cb	20 gr over Walk	25	50

$5^{18} \approx 5^{24}$

X-sec Jupiter St

LT ℄ RT 35

Jupiter

This Height of instrument carried foward to X-sec La Salle St See page 36.

TP_4	4.71	4.72	5.94	0.01
TP_3	5.67	5.95	4.90	0.28

4 72

253 Lt - end Conc. Slab.

$4+83\frac{85}{40}$ = Nwly Line Druckers Sub & Wlyend.

Jupiter

0.14 0.14 0.02 / 25.3 = Conc. Slab. -0.20

5.1	5.1	5.2	6.7	5.1	5	3.8	5.3	6.9	5.4	5.5	5.0	
		-0.04	-1.47	0.14		-0.14	-0.06	-1.67	-0.16	-0.26	0.24	
50	25	20° gr over WIK	15° Top Cb	15° grover Curb	ow gr	Hub same	15° grover Cb.	15° Top Cb	20 gr over WIK	25	100	

5.18 x 5.24

X-Sec La Salle ST - See page 26 for sketch

P.P.= Power pole.

1+50

1+00

0+90 - 15° ± LT = ℄ 12' broken curb

0+50

0+25 - 16½ ± LT = ℄ 12" P.P. # P45 75 ✓

0+06 - 16½ LT = ℄ Deadman - ✓

Curbs & Walks in fair Condition - Mostly worth Saving

15° RT = begin 6" std. curb & 4" conc walk

LT = begin 6" std curb & 4" conc walk

0+00 = SELy line Druckers subdiv. & begin La Salle

RT

0.68	0.43	0.47	0.08	0.18
4½	4 35	4 36	4 7	4 6
25	20 Wlk	15° Top Cb	15° dirt gut	

1.98

2 0

50

0.78	0.57	0.52	−0.12	0.38
4°	4 26	4 26	4 9	4 4
25	20° ELy Wlk	15° Top Cb	15° Dirt gut	

0.78	0.58	0.58	−0.22	0.18
4°	4 20	4 20	5°	4 6
25	20° ELy Wlk	15° Top Cb	15° dirt gut	

2.78

2 5

50

0.98	0.64	0.61	0.78	0.69
3 0	4 12	4 17	4°	4 09
25	20° ELy Wlk	15° Top Cb	15° dirt gut	on Hub 9" Some

La Salle

−0.22	0.42	0.48	0.78
5°	4 36	4 30	4°
15° dirt gut	15° Top Cb	20° Wly Wlk	25

3.28

2 5

50

0.38	0.08	0.59	0.64	0.78
4 4	4 7	4 19	4 14	4°
	15° gut Dirt	15° Top Cb	20° Wly Wlk	25

0.18	0.08	0.69	0.72	0.88
4 6	4 7	4 09	4 06	3 9
	15° dirt gut	15° Top Cb	20 Wly Wlk	25

1.78

3 1

50

0.69	0.58	0.73	0.70	0.58
4 09	4 2	4 05	4 08	4 3
on Hub 9" Some	15° gut	15° Top Cb	20° Wly of Wlk	25

4.72 4 72

H.I. brought forward from page 35

X-Sec La Salle ST

℄ La Salle

Garage has been converted to Room

3+21 - 15° LT = ℄ 12' wide Conc drive ✓

0.33	0.16	−0.46
4^{45}	4^{62}	5^{24}
24° Dr	20° Brk Dr.	15° Lip Drive

3+00

1.38	0.68	0.72	0.13	−0.62	−0.57	−0.62	0.03	0.04	0.88	1.58
3^{4}	4^{1}	4^{53}	4^{65}	5^{4}	5^{3}	5^{4}	4^{75}	4^{74}	3^{9}	3^{2}
50	25	20° Wlk	15° Top Cb	15° dirt gut		15° dirt gut	15° Top Cb	20° Wlk	25	50

2+50

0.48	0.12	0.14	−0.52	−0.42	−0.42	0.02	0.08	0.08
4^{3}	4^{66}	4^{64}	5^{3}	5^{2}	5^{2}	4^{76}	4^{70}	4^{7}
25	20° Wlk	15° Top Cb	15° dirt gut		15° dirt gut	15° Top Cb	20° Wlk	25

2+01 - 17° LT = ℄ 14" P.P. # P4551 ✓

2+00

1.58	0.28	0.28	0.20	−0.42	−0.02	−0.32	0.15	0.31	0.58	1.18
3^{2}	4^{5}	4^{50}	4^{58}	5^{2}	4^{8}	5^{1}	4^{63}	4^{47}	4^{2}	3^{6}
50	25	20° Wlk	15° Top Cb	15° dirt gut		15° dirt gut	15° Top Cb	20 Wlk	25	50

1+95 - 15° RT = ℄ 10' conc drive ✓

−0.30	0.28	0.40
5^{08}	4^{50}	4^{38}
15° Lip Dr	20° Brk	24° Ely of Wlk & Drive

4.72 ⊼ 4.78

X-Sec La Salle ST

SELy edge Rough A.C. Pav.

4+10 85 = SELy Curb Line Nashville ST

15° LT = B.C. Ch RcT

15° RT = B.C. Ch RcT

4+00 85 SELy Line Nashville ST

TP5 3.76 5.62 2.86 1.86

3+50

LT ℄ RT

La Salle

0.17	-0.22	0.05	-0.22
5.51	5.9	5.63	5.9
150 Top cb	150 GUT	100 Top cb	100 GUT

0.02	-0.32	0.09	-0.32	-0.42	-0.22	-0.42	-0.42	0.02
5.66	6.0	5.77	6.0	6.1	5.9	6.1	6.1	5.70
50 Top cb	50 GUT	25 Top cb EC	25.0 GUT EC	15		15.0	25.0 GUT EC	25.0 Top cb E

For outs See X-sec Nashville This Book

0.28	0.03	-0.10	-0.62	-0.32	-0.62	-0.07	0.16	0.19	0.18
4.9	5.65	5.78	6.3	6.0	6.3	5.75	5.52	5.49	5.5
25	20.0 WK	15.0 Top cb	15.0 GUT BC		15.0 GUT BC	15.0 Top cb BC	20.0 WK	24	25

5.62 x 5.68

Top Fire Hyd NWly Cor Western + Nashville

1.08	0.17	0.09	0.03	-0.42	-0.22	-0.52	-0.04	0.06	0.11	1.18
3.7	4.61	4.69	4.75	5.3	5.0	5.4	4.82	4.72	4.67	3.6
25	24 WK	20 WK	15.0 Top cb	15.0 GUT		15.0 dirt GUT	15.0 Top cb	20.0 WK	24.0 WK	25

4.72 4.78

X-Sec La Salle ST

LT ℄ RT

La Salle

under dirt- Top of curb only exposed for shirt

Note- Walk & Curb on left side Western

15° RT - BC. Curb ReT - 10' Rad.

15° LT - BC curb ReT - 10' Rad.

La Salle ST is paved with Rough Cold Lay Pave.

Nwly edge A.C. (Rough) Paving Nashville

4+50.85 back = 0+00 ahead - Nwly Nashville

0.98 0.94 0.83 0.28 0.58 0.02 0.16 0.28 0.28

4.7 4.74 4.85 5.4 5.1 5.7 5.84 5.4 5.4

25° 20° Walk 15° Top Cb BC 15° Gut BC 15° Gut BC 15° Top Cb BC 20° Dirt over walk 25

New Cb & walk

0.12 0.22

5.56 5.9

100 Top Cb 100 Gut

0.33 0.12 0.90 0.74 0.28 0.48 0.48 0.22 0.52 0.11

5.35 5.8 4.88 5.4 5.2 5.2 5.9 6.2 5.79 sec

50 Top Cb 50 Gut 25° Top Cb BC 25° Gut BC 15 15 25° Gut BC 25° Top Cb BC

Nwly edge Rough A.C. Pave Nashville

4+40.85 = Nwly Curb line Nashville

0.38 0.38 0.38 0.38 0.38 0.26 0.12 0.32

5.3 5.3 5.3 5.3 5.3 5.42 5.8 6.0 } For outs see x-sec Nashville

150 100 50 25 15 Rim SMH 15 25

5.62 + 5.67

X-Sec La Salle ST

$1+04$ - 25^{3} LT = ℄ Stucco House ✓

$1+00$ - 25^{3} LT =

$0+81$ - 15^{0} LT = ℄ 10' Conc Drive ✓

$0+50$

Poor condition
Walk + Curb on to Nwly is old Curb + walk

$0+45$ - 15^{0} LT = end New Curb + walk

$0+04$ - 17^{6} RT = ℄ Fire Hyd. ✓

LT- ℄ RT 40

La Salle

Station 1+04

Elevation	1.78	-0.22
Rod	3^{90}	5^{9}
Distance / note	25^{3} Floor	25^{3} grat House

Station 1+00

Elevation	-0.22	-0.135	-0.29	-0.32	0.18	-0.36	-0.36	0.07	-0.42	0.28	1.08
Rod	5^{9}	6^{03}	5^{97}	6^{0}	5^{5}	6^{04}	6^{04}	5^{7}	6^{1}	5^{4}	4^{6}
Distance / note	25	20 Wlk Poor Cond	15^{0} Top Cb	15^{0} gut		15^{0} edge coldlay	15^{0} Top Cb	15^{0} Dirt	20^{0} Dirt over wlk	25	50

Station 0+81

Elevation	0.18	-0.16	-0.28	-0.32
Rod	5^{50}	5^{84}	5^{96}	6^{0}
Distance / note	25 Brk in Dr	20^{0} Brk	15^{0} Lip Dr	15^{0} gut

Station 0+50

Elevation	0.18	-0.11	-0.18	-0.32	0.28	-0.22	-0.16	0.08	0.08	0.38
Rod	5^{5}	5^{79}	5^{86}	6^{0}	5^{4}	5^{9}	5^{84}	5^{6}	5^{6}	5^{3}
Distance / note	25	20^{0} Wlk	15^{0} Top Cb	15^{0} gut		15^{0} gut edge cold lay	15^{0} Top Cb	15^{0} Dirt over cb	20^{0} Dirt over walk	25^{0}

Station 0+45

Elevation	-0.02	-0.09	-0.05	-0.32
Rod	5^{70}	5^{77}	5^{73}	6^{0}
Distance / note	24^{0} Wly Wlk	20^{0} Ely Wlk	15^{0} Top Cb	15^{0} gut

5 62 [illegible] 5.68

X-Sec La Salle ST

4+75 = 2x2 hub and toe of dirt dike

4+30 ~ 15 Lt. angle in cold lay

4+00 ~ Unable to find Curb or walk from here on

3+64 ~ 16.5 Lt = ℄ 8" Power Pole # 4223 ✓

3+50

3+05 ~ .3 Lt = ℄ Sewer Manhole ✓

3+00

2+62 ~ 16.5 Lt = ℄ Deadman ✓

2+50

= B.M. - 0.33 = Spike

2+44 ~ 16.4 Lt = 8" P. pole 4175

2+00 ~ 15 Lt. = ℄ 16' Conc. drive ✓

1+50 ~ Curb very poor condition on Lt.

1+22 ~ 17' Lt. = ℄ 8" P. pole ✓ 4143

See P. 74 for New walks & Dr. - 4-56

LT — ℄ La Salle — RT

0.48 0.18 -0.32 0.48 -0.62 -1.72 -1.49 -0.52 3.18 5.68 7.18 11.68
5.2 5.5 6.0 5.2 6.3 7.4 7.17 6.2 2.5 0.0 +1.5 +6.0
50 25 20 15 7 6 on hub | 3 in ditch | 15 20 25 56 Top dike

-0.22 -0.82 -1.12 -1.12 -0.12 -0.82 -0.42 -1.62 -0.92 11.68
5.9 6.5 6.8 6.8 5.8 6.5 6.1 7.3 6.6 +6.0
50 25 20 15 | 15 edge cold lay | 25 | 30 | 35 Toe dike in ditch | 80 Top dike

0.98 -0.42 -1.12 -1.35 -1.02 -0.02 -0.52 -0.62 -0.52 -0.22 11.68 +6.0
4.7 6.1 6.8 7.03 6.7 5.7 6.2 6.3 6.2 5.9 5.4 7.1
50 | 25 | 20 dirt over walk | 15 Top Curb | 15 gut. | 15 gut | 17.5 edge Cold lay | 20 dirt over walk | 25 | 50 | 58 Toe dike in ditch | 110 Top dike

0.48 -1.02 -1.07 -1.12 0.08 -0.72 -1.12 -0.42 -0.32 0.28
5.2 6.70 6.75 6.8 5.6 6.4 6.80 6.7 6.0 5.8 6.3
25 | 20 edge walk | 15 top Cb | 15 gut. | 15 gut | 15 Top Cb | 20 dirt over walk | 25 | 50 | 115 Toe dirt dike & 6' drainage ditch -0.12 -0.62

0.11
5.57
.3

-0.72 -0.89 -0.99 -1.02 0.18 -0.62 -0.91 -0.72 -0.32 0.08
6.4 6.57 6.67 6.7 5.5 6.3 6.59 6.4 6.0 5.6
25 | 20 edge walk | 15 top Cb. | 15 gut | 15 gut | 15 Top Cb | 20 dirt over walk | 25 | 50

-0.32 -0.69 -0.80 -0.80 0.38 -0.62 -0.72 -0.62 -0.42
6.0 6.37 6.50 6.5 5.3 6.3 6.40 6.3 6.1
25 | 20 edge walk | 15 Top Cb | 15 gut. | 15 gut | 15 Top Cb | 20 dirt over walk | 25

-0.59 -0.62 -0.74 -0.72 0.18 -0.62 -0.45 -0.72 -0.22 0.38
6.27 6.30 6.42 6.4 5.5 6.3 6.13 6.4 5.9 5.3
25 in drive | 20 edge walk | 15 lip drive | 15 gut | 15 gut. | 15 Top | 20 dirt over walk | 25 | 50

0.32 -0.41 -0.45 -0.62 0.18 -0.52 -0.50 -0.72 -0.52
6.0 6.09 6.13 6.3 5.5 6.2 6.18 6.4 6.2
25 | 20 edge walk | 15 Top Cb | 15 gut | 15 gut. | 15 Top Cb. | 20 dirt over walk | 25

5.62 ⊼ 5.68

X-Sec Western - See Sketch p. 26

Drive - 2 conc strips back of Prop

1+15 15° LT = ℄ broken out curb for

1+00 -

0+86.5 - 16.6' Lt. = ℄ P. pole # J.P. 4565 ✓

0+75.5 - 16.5 Lt. = ℄ Deadman ✓

0+50 -

0+41 - 16.4 LT = ℄ 12" PP # P4567 ✓

~~0+24 - 16.4 LT = ℄ Deadman~~

0+04 - 16.6 RT = ℄ Fire Hyd. ✓

Lightly oiled surface.

15° LT } begin curbs & walks
15° RT }

℄ Begin Western ST

0+00 = SELy Line Druckers Sub

TP_6	5.39	4.66	6.33	-0.71

X-Sec Western ST

2T ℄ Western RT #2

1.12 -0.38 -0.46 -0.58 -0.78 -0.38 -0.48 -0.58 -0.46 -0.28 0.92

3⁶ 5⁰ 5¹⁸ 5³⁰ 5⁵ 5¹ 5⁴ 5³⁰ 5¹⁸ 5⁰ 3⁸

50 25 20° WIK 15° Top CB 15° GUT 15° GUT Dirt 15° Top CB 20° WIK 25 50

1.02 -0.38 -0.57 -0.58 -0.98 -0.38 -0.58 -0.55 -0.44 -0.48 0.92 1.02

3⁷ 5¹ 5²⁴ 5³⁰ 5⁷ 5¹ 5³ 5²⁷ 5¹⁶ 5² 3⁰ 3⁷

26 25 20° WIK 15° Top CB 15° GUT 15° GUT 18° Top CB 20° WIK 25 26 50

0.72 -0.08 -0.39 -0.57 -0.38 -0.03 -0.48 -0.64 -0.30 -0.28 1.02

4⁰ 4⁸ 5¹¹ 5²⁹ 5¹ 4⁷⁵ 5² 5³⁶ 5¹² 5⁰ 3⁷

50 25 Ely WIK 15° Top CB 15° GUT Dirt ON NW 15° DIRT GUT 15° Top CB 20° WIK WIK 25 50

4 66 T 4 72

5 6² T 5 6¹

X-Sec Western

LT — Western — RT — #3

3+50

1.47	1.47	0.78	0.50	0.56	1.28	0.88	0.78	0.55	0.49	0.38	0.52
3 3	3 3	5 0	5 22	5 28	6 0	5	6	5 5	5 27	5 21	5 1	4 2
50	30	25	20 WIK	15° Top CB	15° 90T			15° 90T	15° Top CB	20° WIK	25	50

3+00

0.92	0.18	0.51	0.58	1.18	0.48	0.68	0.58	0.55	0.08	0.08
3 8	4 9	5 23	5 30	5 9	5 2	5 4	5 30	5 27	4 8	4 8
50	25	20° WIK	15° Top CB	15° 90T		15° 90T	15° Top CB	20° WIK	25	50

2+81 - 16° LT = ℄ 12" PP # P4531 -

2+50

1.12	0.48	0.61	0.70	0.98	0.48	0.68	0.77	0.62	0.58	0.42	0.63
3 6	5 2	5 33	5 42	5 7	5 2	5 4	5 44	5 34	5 3	4 3	4 1
50	25	20° WIK	15° Top CB	15° 90T		15° 90T	15° Top CB	20° WIK	25	26	50

2+00

1.22	1.07	0.48	0.56	0.64	0.78	0.58	0.68	0.61	0.53	0.38	0.62
3 5	3 7	5 2	5 28	5 38	5 5	5 3	5 4	5 33	5 25	5 1	4 1
50	26	25	20° WIK	15° Top CB	15° 90T		15° 90T	15° Top CB	20° WIK	25	50

1+39
1+~~62~~ - 17° LT = ℄ 14" PP - # P4561 - New.

1+50

1.22	1.17	0.38	0.43	0.59	0.78	0.48	0.68	0.58	0.46	0.08	0.62
3 5	3 6	5 1	5 15	5 31	5 5	5 2	5 4	5 30	5 18	4 8	4 1
50	26	25	20° WIK	15° Top CB	15° 90T		15° 90T	15° Top CB	20° WIK	25	50

4 66 π 4 72

X-Sec Western

Poor cond.

25° RT
25° LT } Curb EC. - Returns in very

4+40 85 = Nwly edge Rough A.C. Pave
Nwly Curb Line Nashville

4+25 85 = ℄ Nashville ST

25° RT
25° LT } = EC Curb Rets.

SELy edge Rough AC Pave Nashville

4+10 85 = SELy Curb Line Nashville ST

TP 7. 3.01 4.71 2.96 (1.70) out = old Pole

- 0.33 Corr. Elev.

15° LT
15° RT } = BC's Rets.

4+00 85 = SELy Line Nashville

LT ℄ RT

Western

0.56 1.03 1.0 0.8 0.9 1.03 0.67

5 33 5 8 5 8 5 6 5 7 5 8 5 39

25° Top CB EC 25° OUT EC 15 15 25° OUT EC 25° Top CB EC

See X-S Nash.

1.13 1.13 1.0 0.8 0.73

5 9 5 9 5 8 5 6 5 5

25 15 15 25

0.71 1.3 1.3 1.1 1.0 1.03 0.66

5 48 6 1 6 1 5 9 5 8 5 8 5 43

See X-Sec Nashville

25° Top CB EC 25° OUT EC 15° 25° OUT EC 25° Top CB EC

For OUT's See X-Sec Nashville.

4 71 T 4 77

New

Nail in Pole SWly Power Pole - Western & Nashville

0.48 0.60 0.68 1.28 1.08 1.08 0.62 0.50 0.48

5 2 5 3 2 5 4 0 6 0 5 8 5 8 5 3 4 5 2 2 5 2

25 20 WIK 15° Top CB BC 15° OUT BC 15° OUT BC 15° Top CB BC 20 WIK 25

4 66 T 4 72

X-Sec Western ST

36° RT = Toe dyke

1+73 - 15° RT = end poor curb

1+71 - 15° LT = ℄ 12' Wide Conc drive

1+25 - 122 - RT = toe dirt dyke (U.S. Govt) San Diego River
Drainage ditch along toe dyke

1+21 - - 15° LT = ℄ 8' wide broken curb

1+00

0+54 - 16° LT - ℄ 8" p.p. # JP4121

0+50

0+10 - 16° LT = ℄ dead man out

0+02 - 16° LT = ℄ Anchor pole.

Cbs in poor Condition

LT	℄ Western	RT	45
0.69	0.74	1.21	1.23
5.46	5.61	5.98	6.0
25 indr	20 WLK	15° IN Drive	15° OUT
1.23	1.03	1.05	0.63
6.0	5.8	5.82	5.4
15° OUT	15° TOP cb	20° WLK	25
0.63	0.43		
5.4	5.2		
25	Toe Dyke		
0.69	0.84	1.21	
5.46	5.61	5.98	
25° Dr	20° WLK Brk in Dr	15° LIP Dr	
0.37	0.53	0.77	0.73
4.4	5.3	5.54	5.50
50	25	20° WLK	15° TOP cb
1.13	1.43	0.80	0.68
5.9	6.2	5.57	5.45
15° OUT	15° TOP cb	20° WLK	25
0.43	0.07		
5.2	4.7		
25	122° Toe dyke		
0.33	0.43	0.65	0.63
4.4	5.2	5.42	5.40
50	25	20° WLK	15° TOP cb
1.23	0.93	1.13	0.67
6.0	5.7	5.9	5.44
15° OUT	15° OUT	15° TOP cb	30 WLK
0.67	0.43	0.53	
5.44	5.2	4.2	
25	50		
0.23	0.61	0.56	1.23
5.0	5.38	5.33	6.0
25	20 WLK	15° TOP cb	15° OUT
1.03	1.13	0.61	0.60
5.8	5.9	5.38	5.37
15° OUT	15° TOP cb	20 WLK	25
0.23			
5.0			
25			

4 71 ✱ 477

X-sec Western ST

TP9	5.50	7.73	3.31	2.23. (2.30 = New Elev.)
TP8-	6.41	5.54	5.58	- 0.87 (- 0.80 = New Elev.)

2+20 - 17° LT = ℄ deadman - ✓

2+12 - ℄ Western ST intersects Toe dyke -

2+08 - 20° LT = end conc walk

2+05 15° LT = end Curb

2+03 - 17° LT = ℄ 12" pp # 4169 - ✓

12° RT = toe dyke
Swly toe River dyke
2+00 = ℄ Ely + Wly Drainage ditch along

LT ℄ Western RT 46

This H.I. Carried foward to page 47-

7.73 x 7.79

ON Mon. Nly COR P.L. 243 - also SEly Line Druckers
3' Prop tie back
ON City L & Disk ON Sly COR Lapwai + Nashville

-0.03 / 4.0 / 50; -0.63 / 5.4 / 25; -1.23 / 6.0 / 20; -1.73 / 6.5 / 15; -0.73 / 5.5 / Toe dyke; 4.77 / 0.0 / 15; 8.13 / + 3.4 / 25; 11.17 / + 6.4 / 32 Top Dyke

-0.92 / 5.69 / 24° wlk; -0.99 / 5.76 / 20° wlk

-1.07 / 5.84 / 15° Top Cb; -1.63 / 6.4 / 15° gut

-0.83 / 5.6 / 25; -0.88 / 5.65 / 20° wlk; -0.95 / 5.72 / 15° Top Cb; -1.33 / 6.1 / 15° gut; -1.73 / 6.5; -0.33 / 5.1 / 12° Toe dyke; 4.73 / 0.4 / 25 Onside Dyke

4.71 x 4.77

X-Sec Lapwai ST

See Sketch Page 27

1+50 - 4^{1} LT = Hogwire fence

1+00 - 4^{2} LT = Hogwire fence

0+63 - 3^{6} LT = ℄ Water meter -

0+50 - 6^{0} LT = fence

0+31 - 16^{2} RT = ℄ Fire Hyd.

0+25± = Nwly Line Knoxville ST

0+00 { 31^{0} RT = ℄ Deadman
14^{5} RT = ℄ 14" Pole - P4600
SELy Line P.L. 258 + SELy Line Knoxville ST(?)
6^{6} LT = begin 5' high Hogwire fence }

X-Sec Lapwai ST

LT ℄ RT

Lapwai ST

LT				℄	RT				
	25		4.94 / 2^{85} P.L.	1.49 / 6^{3}	1.89 / 5^{9} / 15	2.89 / 4^{9} / 17	1.39 / 6^{4} / 20	1.19 / 6^{6} / 25	
1.79 / 6^{0} / 50	1.79 / 6^{0} / 25		1.59 / 6^{2} / 2^{85} P.L.	1.59 / 6^{2}	1.8 / 6^{0} / 13	3.3 / 4^{5} / 16	1.9 / 5^{9} / 19	1.9 / 5^{9} / 25	2.0 / 5^{8} / 50
	1.09 / 6^{7} / 25		1.49 / 6^{3} / 2^{85} P.L. Line	1.49 / 6^{3}	1.59 / 6^{2} / 12	2.59 / 5^{2} / 15	1.39 / 6^{4} / 19	1.59 / 6^{2} / 25	
	1.59 / 6^{2} / 25		1.69 / 6^{1} / 2^{85} P.L. Line	1.59 / 6^{2}	1.69 / 6^{1} / 25				
1.59 / 6^{2} / 25	1.59 / 6^{2} / 2^{85} gr		1.04 / 6^{75} / 2^{85} GN Mon	1.59 / 6^{2}	1.79 / 6^{0} / 5	2.89 / 4^{9} / 14	1.79 / 6^{0} / 16	1.69 / 6^{1} / 25	1.49 / 6^{3} / 50

7^{73} ⊼ 7^{79}

H.I. brought foward to X-sec Lapwai

X-Sec Lapwai ST

2+60 - 21^0 LT = ℄ water meter.

2+58 · 26^5 LT = ℄ 2^5' wide Conc walk

2+57.5 - 26.6 Lt. = ℄ 2' Conc. walk

2+50. 24^0 LT = begin 4" Conc base for fence

✓ B.M. = 5.27 = Nail = New Elev.

2+25 - 17^3 RT ℄ 14" P.P. # P4566 -

Note! due to depth of curb under dirT
+ Hardness of ground. Curb only Located
occassionally - walk NoT dug up at all -

24^0 LT = begin 3' high picket fence ✓

15^0 LT = begin curb ✓

SELy Line Drucker's Sub ✓

2+24^31 · 2^85 LT = Nly COR P.L. 243

2+23 - 3^0 LT = end 5' high Hog wire fence

2+00 - 3^7 LT = Hog wire fence

LT ℄ Lapwai ST RT 48

2.35 2.33
5^44 5^46
36^5 26^5
wlk wlk

2.2 2.3 1.7 2.2 2.3 2.37 = walk 5.4 2.4 2.34 5.45 26.6 = walk 2.80 3.2 3.0
5^6 5^50 6^1 5^6 5^5 - 35 5^4 5^0 4^6 4^8
25 24^0 24^0 24^0 20 15 19 25
Top Base Foot gr DirT

2.1 2.3 2.3 0.28 2.4 2.9 2.9 3.1 3.8 3.1 2.8 1.6
5^7 5^5 5^5 7^51 5^4 4^9 4^9 4^7 4^0 4^7 5^0 6^2
50 25 20 15^0 15^0 2^85 14 18 22 25 50
Top Cb DirT over cb P.L. COR

2.3 2.4 2.3 2.3 2.9 2.6 1.59
5^5 5^4 5^5 5^5 4^9 5^2 6^2
50 25 2^85 17 25 50
P.L.

7^73 ⊼ 7^79

X-Sec Lapwai ST

3+67 - 24⁴ LT = 2 2⁵ wide Conc walk — Now gone

3+50

3+46 - 24° LT = begin 3' high picket fence

3+06 - 24° LT = end 3' high picket fence

3+00 -

2+89 - 25.6' Lf. = ± 23' Conc. walk

2+75

Fence continues Newly-

2+67 - 24° LT = end Conc Base under Fence

LT

0.89 0.87

6 9⁰ 6 9²

34⁴ Walk 24⁴ Walk

1.4 1.3 1.2

6⁴ 6⁵ 6⁶

50 25 15

1.4 1.6 1.7 1.7

6⁴ 6² 6¹ 6⁴

50 25 20 15

2.17 1.83

43 walk 25.6

1.9 2.0 2.0

5⁹ 5⁸ 5⁸

25 20 15

2.15 1.7 2.7

5 6⁴ 6¹ 5⁶

24° Top Base 24° Foot 24° 9L

RT

1.3 1.3 3.2 3.5 4.2

6⁵ 6⁵ 4⁶ 4³ 3⁶

14 22 25 50

2.0 2.6 2.6 3.9 9.49 9.7

5⁸ 5² 5² 3⁹ +1⁷ +1⁹

15 21.25 41 50

Top Bank

2.4 2.7 2.7 1.9 9.59

5⁴ 5¹ 5⁵ 5⁹ +1⁸

15 25 68° 80°

Toe bank Top Bank

7 7³ 7²⁹

X-sec Lapwai St

TP_{10}	13.00	13.25	7^{48}	0.25

5+00 - 15.0 LT = curb

No Apron.

4+99 - 25.0 LT = ℄ single gar. conc floor

4+94 - 24.1 LT = end 3' high picket fence ✓

4+80 - 15.0 LT = ℄ water meter -

4+86 - 24.1 Lt = ℄ 3.2' Conc. walk 1.12 / 30 / walk

4+50

4+20 - 16.5 LT = ℄ water meter -

4+00 = 15.0 LT = curb

3+99 - 17.3 RT = ℄ 14" p.p. # P1540 ✓

LT ℄ RT 5+0

Lapwai

13.25 π 13.31

+.7 / +.07 -0.67 -0.70 0.6 0.7 0.99 0.79

7^1 8^{46} 7^1 7^2 7^1 6^8 7^0

25 15.0 Top Cb 15.0 grover cb 13 25 50

1.05

6^{74}

25.0 conc floor

0.81 / 0.98 .80 .9 1.0 1.0 0.79 0.79 1.1

24.1 walk 7^0 6^9 6^8 6^8 7^0 7^0 6^7

25 20 15 14 15 25

0.89 0.89 -0.46 1.2 1.0 1.0 1.7 1.5 2.4

6^9 6^9 8^{25} 6^6 6^8 6^0 6^1 6^3 5^4

50 25 15.0 Top Cb. 15.0 dirt over cb 15 18 25 50

7^{73} π 7^{79}

X-sec Lapwai ST

LT ℄ RT — Lapwai — 51

6+00 - RT = toe dyke

1.41	-0.80	-0.78	-0.82	-0.39	0.11	1.01	1.11	1.91	8.41	12.11
11.9	14.11	14.09	14.13	13.7	13.2	12.3	12.2	11.4	4.9	1.2
25.0	24.0	20.0	15.0	15.0		15	25	34	50	62.0
	wlk	wlk	Top cb	Dirt over cb				Toe dyke	on side Dyke	Top Dyke

5+75 - 65.0 RT = toe dirt dyke 12.0 / 50

1.01	-0.63	-0.68	-0.69	0.11	0.41	0.61	1.31	1.01	3.61
12.3	13.94	13.99	14.0	13.2	12.9	12.7	12.0	12.3	9.7
25	24	20.0	15		14	15	21	25	65.0
	wlk	wlk	Dirt over cb						Toe dyke

5+57.24.6 LT = ℄ single garage - Dirt floor

0.61
12.7
24.6
Dirt Floor

5+50

0.31	-0.58	-0.78	-0.29	0.11	0.71	0.81	1.21	0.71
13.0	13.89	14.09	13.6	13.2	12.6	12.5	12.1	12.6
25	20.0	15.0	15.0		14	15	21	25
	wlk	Top cb	gr over cb					

5+26.0 20.0 LT = begin exposed lateral walk ✓

-0.49	-0.56
13.80	13.87
24.0	20.0
walk	walk

13.25 ⊼ 13.21

X-Sec Lapwai ST

Part of curb under dyke

6+65 0.3 = Nwly Curb Line Nashville ST

Approx toe dyke

6+50 0.3 = ℄ Sewer Manhole

25.0 LT = Curb EC

6+35 0.3 = SEly Curb Line Nashville ST (To Wly-)

41.0 RT = top dyke

10.0 RT = toe dyke

15.0 LT = Cb B.C

6+25 0.3 = SELy Line Nashville

6+20 - 17.5 RT = ℄ Deadmen ✓

6+07 - 16.7 RT = ℄ 14" pp # P4500 ✓

LT — ℄ Lapwai ST — RT

-1.2	2.4	4.7	10.6 ✓	11.8	12.1	12.1 ✓
14.5±	10.9	8.6	3.2	1.5	1.2	1.2
25.0 Top Cb BC	25.0 Dirt over cb BC	15	on dyke	4.0 Top dyke	15 on Dyke	25 on Dyke

FOR OUTS see Nashville ST

0.0	0.4	0.7	2.5	1.78	11.8	12.1 ✓
13.3	12.9	12.6	10.8	11.53	1.5	1.2
25	15	11	℄ ground Toe dyke	℄ Rim SMH	20.0 Top Dyke	25 on Dyke

1.04	0.39	0	0.9 ✓	7.61	9.51 ✓	11.9 ✓
14.35	13.7	13.3	12.4	10.7	3.8	1.4
25.0 Top Cb BC	25.0 Dirt over Cb BC	15		8	25	35 Top dyke

1.21 ✓	-0.89	-0.96	-1.04 ✓	-0.29 ✓	0.41 ✓	1.71	7.81 ✓	12.01
12.1	14.30	14.27	14.35	13.6	12.90	11.6	5.5	1.3
25	24.0 Wlk Walk Broken	20.0 Wlk	15.0 Top Cb	15.0 gr over Cb	Hub gr. Same	10 Toe dyke	25 on Dyke	41 Top dyke

13.25 ⊼ 13.31

X-sec Lapwai ST

TP 11	2.88	6.02	10.11	3.14

6+75.03 = NWly Line Nashville ST

LT ℄ RT 53

Lapwai

See page 53

This H.I Taken Foward to page 54 for X-sec Nashville ST

6.02 T 6.08

0.1	5.4	7.9	12.1	12.1	12.3
13.2	7.9	5.4	1.2	1.2	1.0
45 Toe Dyke	25	15 on Dyke		1.5 on dyke	2.5 on dyke

13.25 T 13.31

X-Sec Nashville ST
See Sketch page 26.

	LT	℄ Nashville ST	RT
0+86 - 15° RT = ℄ 10' wide conc drive ✓			-0.65 / 6^{73} / 15° Lip Dr; -0.21 / 6^{29} / 20° Dr; -0.12 / 6^{20} / 24° Dr.
0+79 - 16.5 LT = ℄ 10" P.P # P625 ✓			
0+74 - 15° LT = ℄ 11' wide conc drive ✓	-0.03 / 6^{11} / 24° Brk Dr; -0.07 / 6^{15} / 20° Brk Dr; -0.55 / 6^{53} / 15° Lip Dr		
0+50	0.28 / 5^{8} / 25; -0.01 / 6^{09} / 20° WIK; -0.10 / 6^{18} / 15° Top Cb; -0.72 / 6^{8} / 15° gut	-0.5 / 6^{6}	-0.62 / 6^{7} / 15° gut; -0.08 / 6^{16} / 15° Top Cb; -0.09 / 6^{17} / 20° WIK; 0.9 / 5^{2} / 25
0+38 - 15' RT = ℄ 10' drive way ✓	0.11 / 5^{97} / 24 Dr; -0.03 / 6^{11} / 20° Dr; -0.54 / 6^{62} / 15° Lip Dr		
Nashville ST Paved Very Rough AC 0+00 - = NELy Line La Salle ST See X-sec La Salle ST page 36	0.38 / 5^{7} / 25; 0.08 / 6^{00} / 20° WIK; -0.08 / 6^{16} / 15° Top Cb BC; -0.42 / 6^{5} / 15° gut BC	-0.3 / 6^{4}	-0.52 / 6^{6} / 15 gut BC Cb; 0.0 / 6^{08} / 15° Top BC Ret; 0.12 / 5^{96} / 20° WIK; 0.18 / 5^{9} / 25

6.02 π 6.08

H.I. brought foward from page 53.

X-Sec Nashville ST

See X-Sec Western ST page 42 for intersection
15° RT cb BC
15° LT cb BC

1+99.94 - = S wly Line Western ST

~~1+98~~ 2+00 - 16⁵ RT = ℄ 15" P.P. HP649 ✓

1+50

1+49 - 15° RT = ℄ 11' wide Conc drive ✓

1+31 - 15° LT = ℄ 10' wide Conc drive ✓

1+22 - 16⁵ LT = ℄ 10" pp # 606473H (Tel. Pole) ✓

1+00

LT | ℄ Nashville ST | RT | 55

0.58 / 5⁵ / 25 — -0.40 / 6⁴⁸ / 20° WlK — -0.52 / 6⁶⁰ / 15° Top CbBC — -0.92 / 7⁰ / 15° gut BC — -1.12 / 7³ (℄) — -1.32 / 7⁴ / 15° gut BC — -0.70 / 6⁷⁸ / 15° Top CbBC — -0.58 / 6⁶⁶ / 20 — -0.54 / 6⁶² / 24 — -0.02 / 6¹ / 25

-0.32 / 6⁴ / 25 — -0.34 / 6⁴² / 20° WlK — -0.36 / 6⁴⁴ / 15° Top cb — -0.82 / 6⁹ / 15° gut — -0.72 / 6⁸ (℄) — -0.72 / 6⁸ / 15° gut — -0.57 / 6⁶⁵ / 15° Lip Dr — -0.35 / 6⁴³ / 20° WlK Dr — -0.22 / 6³ / 25

-0.57 / 6⁶⁵ / 15° Lip Dr — -0.35 / 6⁴³ / 20° Dr — -0.25 / 6³³ / 24° Dr

-0.27 / 6³⁵ / 24° Dr — -0.27 / 6³⁵ / 20° Dr — -0.79 / 6⁸⁷ / 15° Lip Dr

0.5 / 5⁶ / 25 — -0.22 / 6³ / 24 — -0.20 / 6²⁸ / 20° WlK — -0.32 / 6⁴⁰ / 15° Top cb — -0.72 / 6⁸ / 15° gut — -0.52 / 6⁶ (℄) — -0.62 / 6⁷ / 15° gut — -0.24 / 6³² / 15° Top cb — -0.26 / 6³⁴ / 20° WlK — -0.22 / 6³ / 20 — 0.08 / 6⁰ / 25

6.02 ⌅ 6⁰¹

X-Sec Nashville ST

1+26 - 15^{8} RT = ℄ 10' conc drive ✓

1+00

0+80 - 16^{5} RT = ℄ 15" PP # P671 ✓

0+50

15^{0} LT } = cb BC
15^{0} RT }

0+00 = ℄ Nashville + N'Ely Line Western

For Intersection Nashville + Western
See page 42 etal - (X-Sec Western)

Sta.	LT				℄ Nashville ST	RT				
1+26							-0.98 / 7^{06} / 15^{3} Lip Dr	-0.72 / 6^{80} / 20^{0} Dr	-0.70 / 6^{78} / 24^{0} Dr	
1+00	-0.22 / 6^{3} / 25	-0.69 / 6^{77} / 20^{0} WLK	-0.79 / 6^{87} / 15^{2} Top Cb	-0.92 / 7^{0} / 15^{2} GUT	-0.62 / 6^{7}	-1.02 / 7^{1} / 15^{2} GUT	-0.74 / 6^{82} / 15^{3} Top Cb	-0.69 / 6^{75} / 20^{3} WLK	-0.62 / 6^{70} / 24 WLK	1.9 / 4^{2} / 25
0+50	0.08 / 6^{0} / 25	-0.54 / 6^{62} / 20^{0} WLK	-0.59 / 6^{67} / 15^{0} Top Cb	-0.92 / 7^{0} / 15^{0} GUT	-0.72 / 6^{8}	-1.12 / 7^{2} / 15^{0} GUT	-0.62 / 6^{70} / 15^{0} Top Cb	-0.64 / 6^{72} / 20 WLK	0.08 / 6^{0} / 25	
0+00	0.08 / 6^{0} / 25	-0.49 / 6^{57} / 20 WLK	-0.58 / 6^{66} / 15^{0} Top Cb BC	-1.02 / 7^{1} / 15^{0} GUT BC	-0.72 / 6^{8}	-1.12 / 7^{2} / 15^{0} GUT BC	-0.62 / 6^{70} / 15^{0} Top Cb BC	-0.54 / 6^{62} / 20 WLK	-0.32 / 6^{4} / 25	

6.02 x 6^{0r}

X-Sec Nashville ST

			(0.13)	
TP13		5.35	0.17	
TP12	5.20	5.52	5.70	0.32

For Intersection see X-Sec Lapwai

1+99.94 = Sply Line Lapwai ST

1+77.5 - 18.5 Lt - ℄ Pole # 635652-H ✓

1+93 - 16.3 RT - ℄ Fire Hyd ✓

1+75 - 16.6 RT - ℄ Deadman

1+61 - 16.6 RT - ℄ 10" P.P. TP681. ✓

1+50

LT ℄ Nashville RT 57

Reduced Notes 5-14-56

Starting B.M. Page 28. (?)

1.27	2.4	0.9	0.02	0.42	1.04	1.07	1.22	
7.3	3.7	5.3	6.1	6.5	7.12	7.15	7.2	
15° Top CB	15° Dirt over CB	Toe Dyke		15° Out BC	15° Top CB BC	20° Wik	25	

1.08	0.72	0.76	0.86	0.92	0.87	1.12	0.86	0.80	0.80	1.08
5°	6.8	6.84	6.94	7°	6.9	7.2	6.94	6.88	6.88	5°
25	24	20° Wik	15° Top CB	15° Out		15° Out	15° Top CB	20° Wik	24 Wik	25

6.02 = 6.0+

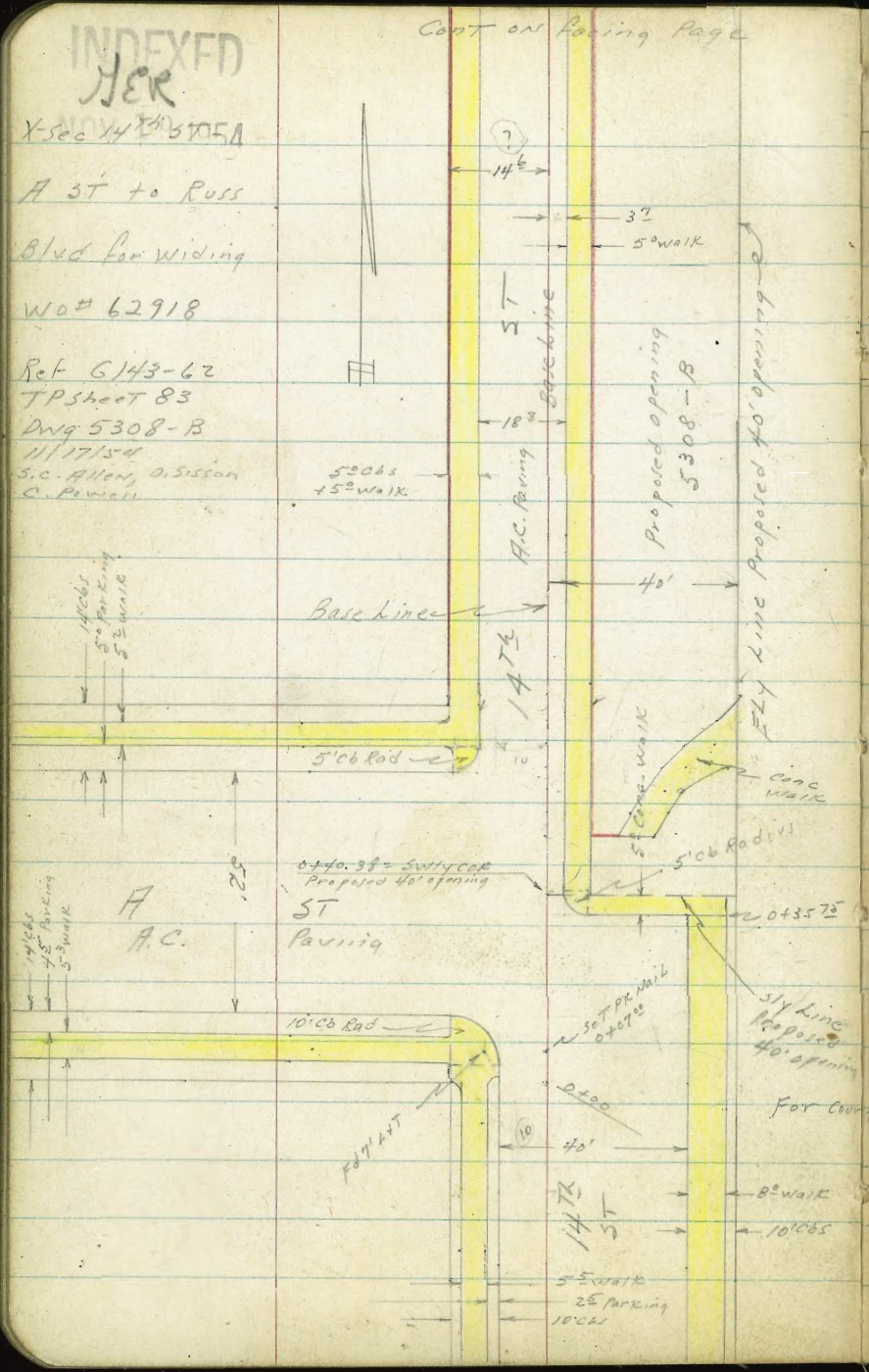
X-Sec 14th St

A St to Russ Blvd for widing

WO# 62918

Ref 6143-62
TP Sheet 83
Dwg 5308-B
11/17/54
S.C. Allen, Division C. Powell

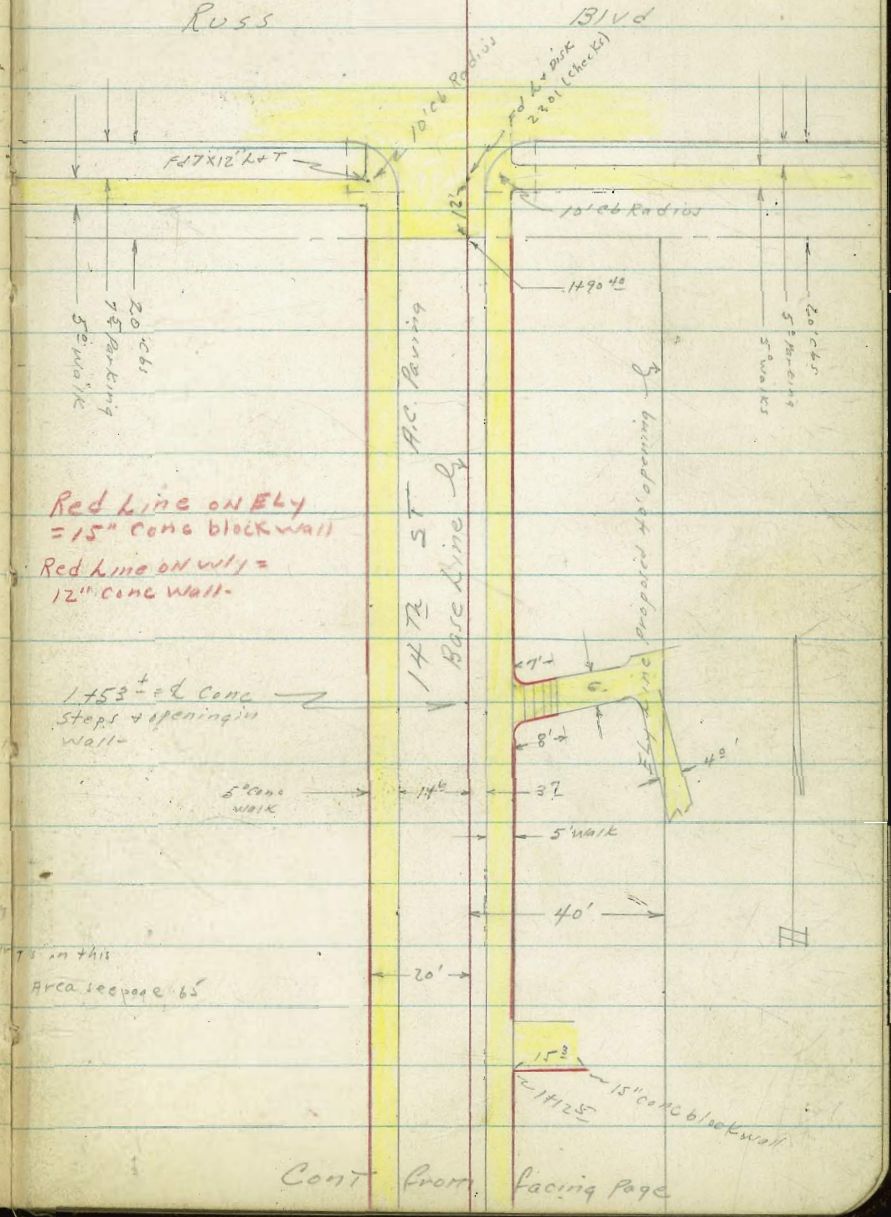
Cont on Facing Page



5-8

Nly line Ross Blvd

Ross Blvd



Cont from Facing Page

X-Sec A-ST, 14th to Ross Blvd
See sketch Page 58
Base Line is 20' Ely of Wly Line 14th ST

40.0 RT = Wly of Stucco Court dwelling
See sketch Page 58

0+35.75 = E+W Curb on Ely of street

Power co-
0+32 - 31.4 RT = ℄ 10" Anchor pole

0+14 = Sly Curb Line to West

Return in poor condition
Mid point + 10' Radius Return — 14th + A Swly cor

0+04 10.0 LT = B.C. Swly Return 14th + A

Stucco Courts on Ely of 14th ST are on the ely Property Line of 14th ST - See sketch page 65

0+00 = { 40.0 RT = Wly of Stucco court dwelling; 30.0 RT = Ely Curb A ST; Sly Line A ST to Wly- }

0-02 - 31.5 RT = ℄ Fire Hyd.

9.34 146.81 137.47

LT = wly | Base Line | RT = ely

Base Line is 20' East of West Line 14th ST

0+35.75:

Rod	Dist / Point	Elev.
10^{48}	20 LT	136.33
9^{92}	Base Line	136.89
9^{71}	8.1 gut E.C.	137.10
9^{16}	8.1 T.C. E.C.	137.65
9^{09}	30.0 gut at P.I. of Cbs.	137.72
8^{52}	30.0 T.C.	138.29
8^{28}	38.0 Ely Walk	138.53
7^{7}	40 gr	139.11

0+14:

Rod	Dist / Point	Elev.
14^{19}	50 T.C.	132.62
13^{87}	50 gut	132.94
11^{33}	20.0 T.C. BC	135.48
11^{79}	20.0 gut BC	135.02
11^{24}	10	135.57
10^{50}	Base Line	136.31
9^{88}	15 A.C.	136.93
9^{68}	30.0 gut	137.13
9^{06}	30.0 T.C.	137.75
8^{82}	38.0 Ely of Walk	137.99
8^{4}	40 gr	138.41

Mid point:

Rod	Point	Elev.
11^{26}	Mid Point Top curb	135.55
11^{56}	Mid point gutter	135.25

0+04:

Rod	Dist / Point	Elev.
11^{27}	10.0 Top Cb	135.54
11^{50}	10.0 gut	135.53

0+00:

Rod	Dist / Point	Elev.
11^{1}	20 Wly P.L. 14 st	135.71
11^{05}	18 Wly of Walk	135.76
11^{27}	10.0 Top Cb	135.54
11^{64}	10.0 A.C. gut	135.17
11^{15}	A.C.	135.66
10^{46}	15 A.C.	136.35
10^{17}	30.0 A.C. gut	136.64
9^{50}	30.0 Top Cb	137.31
9^{29}	38.0 Ely Walk	137.52
9^{3}	40.0 gr at Wly Stucco Court	137.51

146.81 ⊼

NW BP 14th + A ST

X-Sec 14TH - A to Russ Blvd

22' RT = SELy COR Conc walk
15' RT = SWly COR Conc walk } See sketch
15" Wall is contigious with Ely edge of walk
8' RT = Wly of 15" Wall (E&W)
Retaining Wall - See Red Line in sketch
0+52.5 8' RT = W ly side of 15" Conc block

Conc is in poor condition
0+47 3' RT = opening for 10' wide Conc drive

BPNW 14TH & A

T.P.	11.79	149.26	9.34	137.47

old Retaining Wall -
0+41 - to show ground at Nly side of

Retaining Wall -
8' RT = Wly end of old 6" Conc

Nly edge of E&W Walk on Ely of 14TH

0+40.75 3' RT = curb BC.

5308-B

0+40.38 = SWly COR proposed 40' opening

LT = Wly Base Line RT = Ely. 60

137.94 — 11.32 — 8' Ely edge Walk
140.16 — 9.1 — 8' Top Wall
139.55 — 9.71 — 15' SWly COR Walk
139.89 — 9.37 — 22' SELy COR Walk

137.27 — 11.99 — 3' Lip
137.84 — 11.42 — 8' Brim Drive
138.96 — 10.3 — 16 Brk Indr
139.46 — 9.8 — 22' Ely edge 18' drive

149.26 T

134.16 — 12.65 — 50
136.46 — 10.35 — 20

136.96 — 9.85 — 3' Out
137.06 — 9.75
137.69 — 9.12 — 3' T.C.
137.86 — 8.95 — 8' Ely of Wlk
139.0 — 7.8 — 16
139.8 — 7.0 — 24
140.51 — 6.3 — 40

138.18 — 8.13 — 38° Nly of Walk
140.41 — 6.4 — 38° Top Wall
139.21 — 7.6 — 40

134.15 — 12.66 — 50
136.47 — 10.34 — 20

137.95 — 9.86 — 3' Out BC
137.05 — 9.76
137.48 — 9.13 — 3' T.C. BC
137.81 — 9.00 — 8' Nly of Wall + Ely edge N+S Walk
139.21 — 7.6 — 8' Top Wall

146.81 T

X-Sec 14½ ST. A ST to Russ Blvd

LT = Wly | Base Line | RT = Ely

0+96 - 21½ LT = SELy COR Large 2 story Frame house

147.51 | 139.96
5.75 | 9.3
21½ Floor | 21½ gr

0.5 RT = ℄ 8" water gate Valve cover

138.26 | 136.52 | 140.46 | 142.66
11.0 | 12.2 | 8.8 | 6.6
35 Top Ednw Wall | 35 gr at Slywall | 10.0 gr at Ely of wall | 40

Nly edge of side walk

12" Conc Wall is contiguous with Wall

19.6 LT = begin 12" Conc Retaining

138.96 | 137.64 | 137.41 | 137.0 | 138.2 | 138.20 | 138.35 | 139.07 | 139.16 | 141.36
10.3 | 11.62 | 11.85 | 12.26 | 11.06 | 11.00 | 10.91 | 10.19 | 10.10 | 7.9
20.0 Top 12" Wall | 19.6 Wly of Wlk+Wall | 14.6 T.C. | 14.6 gut | 0.5 Top Valve Cov. | 3.7 gut | 3.7 T.C | 8.7 Ely Walk | 9.0 Top 15" Wall

0+80 = Nly Line A ST to Wly.

137.39 | 136.97
11.87 | 12.29
14.6 T.C. E.C. | 14.6 gut E.C.

14 7½ + A

0+71 - 14.6 LT = E.C. 5' Rad Return NWly cor

140.86 | 141.34 | 141.76 | 142.16
8.4.0 | 7.9.2 | 7.5 | 7.1
24.5 NWly edge Conc Walk | 33.3 SELy edge Walk | 40 | 50

19.6 LT = B.C. 5' Rad Ret NWly cor 14½ + A

135.63 | 135.02 | 137.45 | 136.73 | 136.94 | 137.66 | 137.74 | 138.37 | 138.5 | 140.66 | 139.86
13.6.3 | 14.2.4 | 11.8.1 | 12.5.3 | 12.3.2 | 11.6.0 | 11.5.2 | 10.8.9 | 10.7.6 | 8.6 | 9.4
40.0 T.C. | 40.0 gut | 19.6 T.C. B.C. | 19.6 gut BC | 14.6 | 3.7 gut | 3.7 T.C. | 8.7 ely of walk | 8.7 Top Wall | 10.0 gr at Ely of Wall

0+66 = Nly Curb Line A ST to Wly

0+57 - 32.0 RT = ℄ 20" Magnolia tree

149.26 T

X-Sec 14th ST — A ST to Russ Blvd

1+45 - 21 3 LT = Ely of frame House

11' opening in 15" wall for drive
Conc is in very poor condition

1+18 - 3 7 RT = ℄ 11' wide conc drive

Frame House.

1+14 - 20 0 LT = ℄ 5' wide Bay window in

Ely side Frame House

1+01 - 20 1 LT = ℄ 4 5 wide brick fire place in

1+00

LT = w/y Base Line RT = e/y.

142.26	141.70	141.54	141.06	141.94	141.96	142.56	142.63	144.76	144.56	144.76
7 0	7 7 6	7 7 2	8 2 0	7 3 2	7 3 0	6 7 0	6 6 3	4 5	4 7	2 5
20 Top Wall	19 6 W/y W/k	14 6 T.C.	14 6 9 OT		3 7 9 OT	3 7 T.C.	8 7 e/y W/k	9 0 Top Wall	10 0 9 OT	40

140.57	141.05	143.89
8 6 9	8 2 1	5 3 7
3 7 Lip of	8 7 Ark ind.	24 0 e/y edge 11' Conc drive

143.76	144.46
5 5	4 8
40	50

140.06	138.69	138.65	138.13	139.39	139.46	140.13	140.17	142.36	141.76
9 2	10 5 7	10 6 1	11 1 3	9 8 7	9 8 0	9 1 3	9 0 9	6 9	7 5
20 Top Wall	19 6 W/y of Walk	14 6 T.C.	14 6 9 OT		3 7 9 OT	3 7 T.C.	8 7 e/y Walk	9 0 Top Wall	10 0 9 OT E/y Wall

149.26 T

X-Sec 14[12] cont

27[5] RT = ℄ 10" acacia

17[0] RT = ℄ 8" acacia tree

4[4] RT = ℄ 8" Fire Hydrant

2[3] RT = ℄ 6" gate valve cover (water)

1+87 - 16[2] LT = ℄ deadman

1+85 - 16[5] LT = ℄ deadman

1+82 - 5[0] RT = ℄ 4" x 4" No Parking Sign

1+65 - 16[0] LT = ℄ 16" Power pole # P1322

1+58 - 5[2] RT = ℄ Meter has been Removed 1[5] x 2[8] Water Meter box

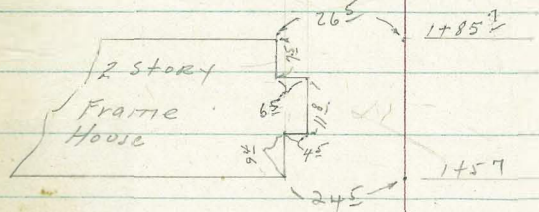
1+57 - 24[5] RT = SE℄ y Cor frame House - See Sketch

Walk behind steps is 6' wide
15" wall - See Sketch Page 58

1+53 - 8[7] RT = ℄ 7' Conc steps with opening in

1+46 - 21[3] LT = NE Cor Large 2 Story frame House

LT = Wly. Base Line RT = Ely 6[3]



149.26 π

X-Sec 14th ST – 'A' to Russ Blvd

LT = Wly | Base Line | RT = ely

14^6 LT = BC. 10' Radius Return Swly COR

2+00 ^{40} 3^7 RT = BC. 10' Radius Return – SELy COR

144.22	143.83		145.05	145.69			
5^{78}	6^{17}		4^{95}	4^{31}			
14^6 T.C. BC	14^6 GUT BC		3^7 GUT BC	3^7 T.C. BC			

1+95

144.30	144.35	144.37	143.91	144.85	144.92	145.52	145.49	143.00
5^7	5^{65}	5^{63}	6^{09}	5^{15}	5^{08}	4^{48}	4^{51}	7^0
20	19^6 Wly of Wlk	14^6 T.C.	14^6 GUT		3^7 GUT	3^7 T.C.	8^7 ELy Wlk	40

150.00 ⊼

TP2 5.89 150.00 5.15 144.11

Swly COR
ON L+T: Sly 12' Line Russ + Wly 2' Line 14^{th}

146.86	148.16
2^4	1^1
10 grat ELy Wall	40

Break in Curb + Sidewalk grades.
Sly edge Conc Paving Russ Blvd
Wall angles at 90° to Wly.
19^6 LT = Nly end 12" Conc Wall
8^7 RT = Nly end 15" Conc block wall
1+90 ^{40} = Sly Line Russ Blvd

145.06	144.55	144.46	144.03	144.7	144.74	145.34	145.30	147.26
4^2	4^{71}	4^{80}	5^{23}	4^{56}	4^{52}	3^{92}	3^{96}	2^0
20 Top Wall	19^6 Wly Wlk	14^6 T.C.	14^6 Conc GUT	CONC	3^7 GUT Conc	3^7 T.C.	8^7 ELy Walk	9^2 Top Wall

149.26 ⊼

X-sec 14th Cont

TP₃ - Starting BM. 12.52 (137.47) 137.48

2+10 40 = Sly Curb Line Russ Blvd

2+09 - { 24.5 LT = ℄ 16" Power pole # P1399 ; 40.0 RT = ℄ 12" Power pole # JP1405 }

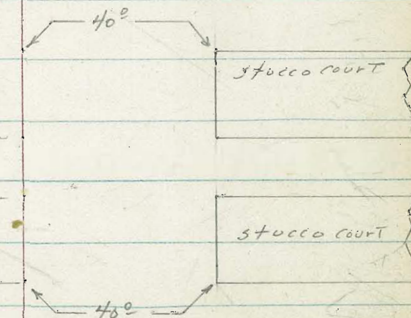
LT = Wly. Base Line RT = ely.

0+35.2

0+17.2

0+05.2

0-12.8



142.16	141.59	141.64	142.24
7.84	8.41	8.36	7.76
50 T.C.	50 90T	50 90T	50 T.C.

143.66	143.06	143.73	144.84	144.92	145.53	142.52	143.15	
6.34	6.94	6.27	5.16	5.08	4.47	7.48	6.85	
24.6 T.C. EC.	24.6 90T EC.	14.6		13.7 90T EC	13.7 T.C EC.	40 90T	40 T.C.	

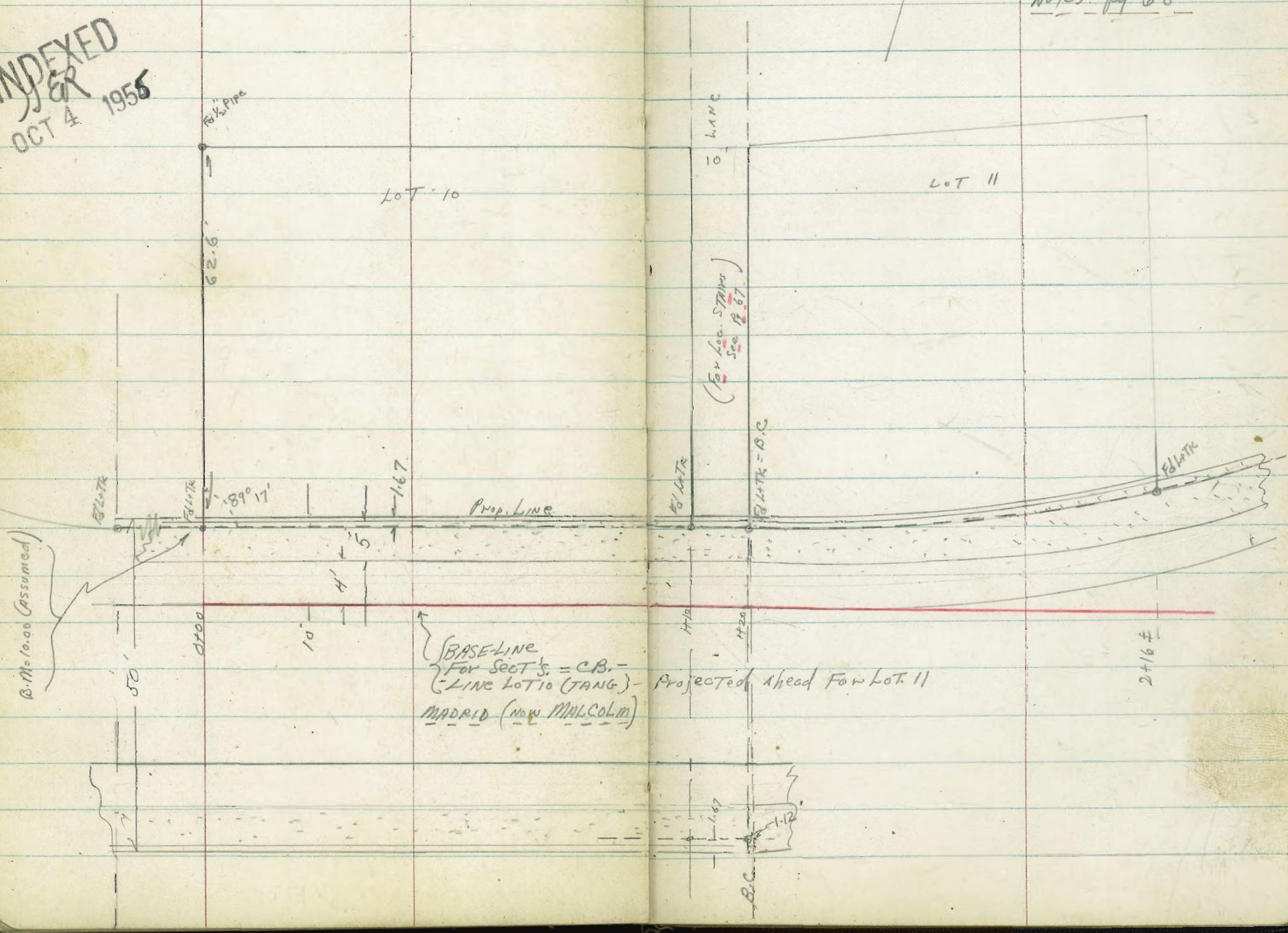
15 0.00 ⊼

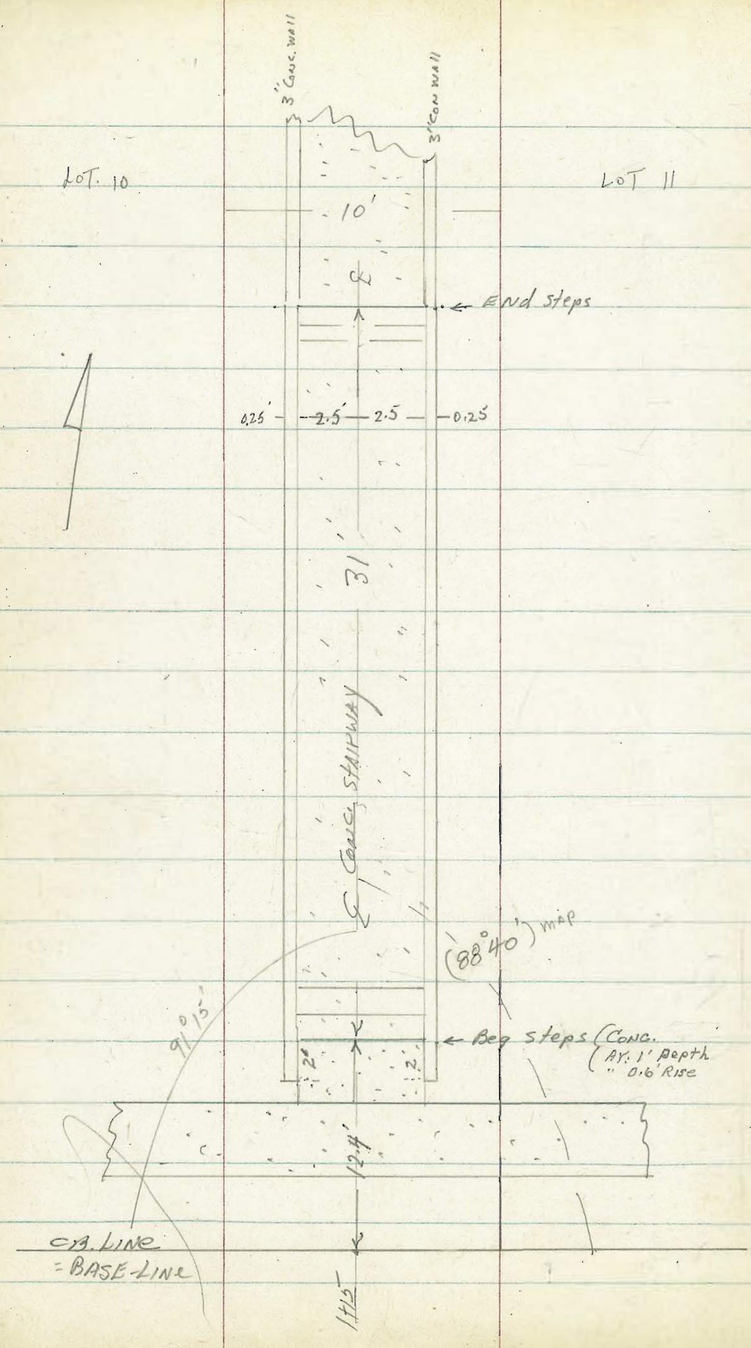
Clark
Garber
Bruner
Pullen
9-29-55
W.O. 19001

X-Sect. Lots 10 & 11 - Rolando
UNIT #3

Ref: Map #1965-3

Notes: Pg 68




LOT 10
LOT 11
3" Conc. wall
3" Con wall
10'
End steps
0.25
2.5
2.5
0.25
31'
Conc. STAIRWAY
(88°40') map
91°15'
Beg steps (Conc.
Av. 1' Depth
" 0.6' Rise
12.4'
C.B. LINE
= BASE-LINE
14.5'

0+75

0+65.5 ~ 40.5 Lt = ℄ 4" avocado Tree

0+58 ~ end wire fence & begin 5' board fence

0+51 ~ 44' Lt = ℄ 6" avocado tree

0+50

0+42 ~ 22.8 Lt. begin block wall fd. below fence

0+38 ~ 43.3 Lt. angle in block wall

0+25

0+20 ~ Angle in bloc wall ~ 50' from base line

0+05.5 ~ 60.4 Lt. begin 4' Hazard bloc wall

0+00 ~ 25' Lt begin 5' 2x4 post & chicken wire fence

0-03 - W'ly Top bank

0-02 - 24' Lt Southly of 4' cyclone fence.

0-16 = W'Ly toe EXIST. CUT-BANK

Note: ALL Elev's. Are Direct Readings From Assumed Elev. B.M - Not Philadelphia Rods

B.M. Dir. Elev. Rod. 10.00 = ASSUMED

BASE-LINE = N'ly C.B. Line Malcolm (68)

41.5 / 50 — 39.70 Top Wall 35 — 36.7 35 grd. — 34.8 21.5 Top Wall — 33.7 21.5 grd — 33.1 18 Top bank — 16.2 11 Toe bank — 16.2 10 — 16.19 9 edge — 15.97 — 15.35 gut

41.1 / 50 — 39.70 40.5 Top Wall — 36.8 grd. 40.5 — 34.10 Top wall 22 — 31.9 grd 22 — 31.3 17 Top bank — 14.3 11 Toe — 14.3 10 — 14.21 9 edge walk — 13.96 — 13.36 gut

33.66 Top Wall — 31.4 footing 22.8

39.55 Top Wall — 36.5 43.3 grd.

39.8 / 50 — 39.80 48 Top Wall — 36.1 48 grd. — 28.9 17 Top bank — 12.2 11 Toe — 12.2 10 prop. — 12.15 9 edge walk — 11.90 Top Cb — 11.37 gut.

39.80 Top Wall 50 — 35.9 grd. 50 — 35.10 footing 50

39.80 Top wall — 36.6 grd. 60.4

17.1 19 Brk — 10.5 10 P.Line — 10.00 9 Bk Walk — 9.70 — 9.12 gut.

35.6 60 Top bank — 33.1 50 Top bank — 27.4 21 Top bank — 10.2 10 Prop Line

10.8 56 — 11.4 50 — 11.2 18 — 8.9 10 P.Line — 8.60 9 Bk Edge Walk — 8.54 4 F.Edge Walk — 8.34 CP — 8.94 GUT.

Elev. 1+TCK. W'ly Line Lot 10 & N'ly 1.67' Line of MALCOLM

1+75

1+72 ~ 29.4 = ℄ 2" avocado tree

1+66 ~ 31 Lt. = ℄ 2" avocado tree

1+65 46.8 Lt. = ℄ 2" fruit tree

1+58 ~ 29.3 Lt = ℄ 3" avocado tree

1+54 ~ 30.3 Lt = ℄ 2" acacia tree

1+53 ~ 47' Lt = ℄ 3" apple tree

1+50

1+35 ~ 47' Lt = ℄ 6" fruit tree & 24' Lt = ℄ 2" tree

1+25 ~ 19.5 Lt. begin 5' cyclone fence & begin vertical bank.

1+21.5 ~ 13' Lt. angle in 5' cyclone fence

1+20.5 = B.C. and 2.5 Lt. = ℄ 1.5 x 1.5 St. light.

1+15.5 = ℄ 5' Stairway ~ cut is 10' wide ~ 2.5 on both sides from edge of conc. steps. Elevs. approx. same as pitch of stairs.

1+10 ~ 43' Lt. angle in board fence & end vertical bank for Stairway.

1+04 ~ 21.5 Lt. end block fd. & angle in fence

1+01 ~ 29.2 Lt. end Hazard blk. wall

1+00

0+98 ~ 36' Lt = ℄ 6" avocado tree

0+80 ~ 37.3 Lt = ℄ 6" avocado tree

Lt. | Base line

40.1 37.5 35.0 21.1 21.0 21.04 20.91 20.36 20.42
50 23 16 Top bank 12.7 Toe vert bank 11.7 prop 10.7 back walk 1.7 Top Cb. 1.7 gut on A.C. pave

41.0 38.0 35.6 21.1 21.0 21.01 20.88 20.25 20.27
50 22 14 Top vert bank 11.6 Toe 10 9.6 back walk .6 Top Cb. gut on A.C.

40.6 36.6 20.0 20.0 20.01 19.92 19.31
50 14 Top bank 11 Toe bank 10 prop 9 edge walk Top Cb. gut

39.94 39.33 19.71 19.46 19.25 18.62
50 43.4 Top of steps bottom of steps 12.5 begin steps 9 edge walk Top Cb. gut.

40.8 38.7 35.2 19.1 19.1 19.10 18.86 18.30
50 35 17 Top bank 11 Toe 10 prop 9 back edge walk Top Cb. gut.

36.40 35.2
Top fd. 21.5 grd.

39.80 36.8
Top Wall 29.2 grd

41.3 39.80 36.2 36.40 35.2 35.2 18.3 18.2 18.22 18.07 17.48
50 29.4 Top Wall 29.4 footing 21.5 Top Wall 21.5 grd. 17 Top bank 11 Toe bank 10 prop 9 edge walk Top Cb. gut

Lt.

Base line

38.1	36.4	34.0		19.2	19.2	19.18	19.19	18.68	18.82	
50	30	17		15.8	14.8	13.8	4.8	48	on	
		Top Bank		Toe bank	prop	back walk	Top Eb.	gut	A.C. pave	

2+16

2+14 cross 5' cyclone fence

2+13 - 21' Lt. Pt. angle in 5' cyclone fence

2+12 - 44' Lt. ℄ 2" pear Tree & 35' Lt. end eugina hedge

2+01 - 33.3 Lt. ℄ 3" Iron Pipe. conc. base

2+00

39.1	36.7	34.5		20.4	20.3	20.35	20.31	19.72	19.77	
50	27	17		14.3	13.3	12.3	Top	3.3	on	
		Top Vert. bank		Toe	prop.	back walk	Eb.	gut	A.C.	

1+88 - 47' Lt. ℄ 5" pear tree

1+81 - 30' Lt. begin 5' eugina hedge

Beg. Cross Sections of Nashville St.
From Midway to La Salle - See Sketch - P. 25 to 27

5-8-56 - F.O. W.O. 31971

			Lt.	℄	Rt.
0+66 - 17.2' Rt = ℄ P. pole # P539 ✓ walk					
0+59.5 - 14.8' Lt = end Dr. Sect. = Beg. old cb.			0.44 23.8 walk; 0.30 19.8; 0.25 Top; -0.01 14.8 gut		
0+50			1.03 50; 0.47 25; -0.02 14.5 gut. in Dr.; 0.71	-0.07 15.3 gut; 0.22 Top (Note these Minus Elev.?)	0.38 20.4; 0.46 24.4 walk; 0.5 25 By Bldg.
0+33 - 15.3' Rt = end good cb. - old Cb. Cont.					0.33 15.3 = Top cb.
0+23 = Beg. 4' walk -					0.36 20.2; 0.41 24.2 walk
0+15.2 - 17.1 Rt = ℄ F.H.					
0+06 - E.C. of Rt. = End "G" Type curbs = good curb Cont. on Rt.			0.87 25 on AC; 0.85 Top = E.C. end cb.; 0.34 15 gut; 0.41 13.8 Lip; 0.98	Lip Broken; 0.50 15 gut	0.99 Top = E.C.; 0.64 25 on A.C.
0+00 = NEly. Line Midway			1.65 50 on A.C.; 0.99 25; 0.99 Top; 0.43 15.8 gut; 0.51 14.6 Lip; 1.04	0.70 14.4 Lip; 0.59 15.8 gut; 1.15 Top	2.23 25 on A.C.; 2.33 25.5 on walk
NEly. Ret. 37.4 around - 4 - parts		Beg. P.C. on Midway	0.76 Lip; 0.65 gut; 1.31 Top 1/4; 0.71 Lip; 0.61 gut; 1.19 Top 1/2; 0.56	Lip; 0.45 gut; 1.04 Top 3/4	0.41 Lip; 0.34 gut; 0.85 Top E.C.
SEly. Ret. 31.3' around - 4 - parts.		Beg. P.C. on Midway - See Below = Lip	1.05; 1.01 gut 1/4; 1.64 Top; 0.98 Lip; 0.85 gut 1/2; 1.44 Top	0.75 Lip; 0.63 gut 3/4; 1.20 Top	0.59 Lip; 0.50 gut. E.C.; 0.99 Top
0-34 = NEly. curb Line Midway			1.54 Top; 0.94 80 gut; 1.46 Top = P.C.; 0.81 35 gut; 0.79 15; 1.11	1.00 15; 1.06 35 gut.; 1.71 Top = P.C.	1.34 80 gut.; 1.94 Top
B.M. = □ in Cor. of Conc. walk - N.E. Cor. Midway & Nashville	Check B.M. - P. 28 on Pipe.	2.33 0.19 = 0.13	P. 28	Actual Elev. Shown	

	Lt.				℄	Rt.				
2+90	1.4	0.6	0.24	0.08	-0.25	0.30	-0.16	0.04	0.20	0.5	1.7
	40	25	23.9 walk	Top	14.9 gut		15.2 gut	Top	24.2 walk	25	50
2+73.5 - ℄ 12' Conc. Dr. on Lt.	1.30		0.36	0.21	-0.30						
	41.2 floor gar.		25	20 walk	14.9 Dr.						
2+50 - 1.5 wly of ℄ of 20.4' Conc. Dr. on Rt.	1.3	0.5	0.33	0.14	-0.30	0.36	-0.15	0.14	0.31	1.53	
2+38.5 - 17.2' Rt. = ℄ P.pole # J.P. 575	40	25	23.8 walk	Top	14.8 gut		15.2 gut. in Dr.	20.3 walk	25 Dr	46.4 end Dr.	
2+33.4 = ℄ 12.5' Conc. Dr. on Lt.	1.41		0.44	0.29	-0.22						
	41.1 floor gar.		25 Dr.	19.8 Brk	14.8 Dr						
2+00	1.3	0.4	0.36	0.19	-0.20	0.38	-0.21	0.14	0.44	0.8	1.5
	50	25	23.8 walk	Top	14.7 gut		15.2 gut	Top	24.2 walk	25	50
1+93.5 - ℄ 12.5 Conc. Dr. on Lt.	1.30		0.41	0.26	-0.27						
	41.2 floor gar.		25 Dr.	19.8 Brk	14.8 Dr.						
1+63.88 = NEly. Line Jupiter	0.2		0.21	0.02	-0.33	0.40	-0.20	0.02	0.38	0.6	
	25		23.8 edge walk	Top	14.6 gut		15.2 gut	Top P.C.	24.2 walk edge	25	
1+38.88 = ℄ Jupiter = on MH. + Note: our Elev. are 0.06 Higher Than Allens			-0.10	-0.11		0.34	-0.17		-0.20		
			25	15		w. Cross	13.5 gut		25		
1+13.88 = SWly. Line Jupiter.	0.3		0.32	0.18	-0.25	0.61	-0.07	0.20	0.37	0.4	
1+13.5 - 17.1 Rt. - ℄ P.pole # JP 549 = BM. 0.72 = spike	25		23.8 walk	Top - P.C.	14.7 gut		15.3 gut	Top = P.C.	24.2 walk	25	
0+85	0.60	0.42	0.36	0.21	0.03	0.67	0.02	0.24	0.45	1.1	1.6
0+88 - 16.8' Rt. = ℄ Deadman	50 on A.C.	25	23.8 walk	Top	14.8 gut.		15.3 gut.	Top	24.3 walk	25	44.5 By House

Lt. | ℄ | Rt.

364
214
150

Top Hyd = 1.90 =

1.86 - P. 38 - Maybe wrong Cor. - No Hyd. on Westeren.

0.3 25 | -0.17 Top | -0.52 15.1 gut. | -0.36 | -0.51 15.2 gut. | -0.02 Top | 0.14 24 walk | Lt 25

++13.81 = NEly. Line La Salle

3+88.81 = ℄ on Sewer M.H.

0.52 25 | 0.43 15 | 0.29 on wly. Cross | -0.24 15 | -0.32 25

3+63.81 = Swly. line of La Salle

3+63.5 - 16.9 Rt. = ℄ P. pole. # P 599 = BM. 0.58 = spike

0.9 28 | 0.91 24.1 walk | 0.79 Top 1 | 0.29 15 gut. | 0.37 | -0.28 15.2 gut. - No cb. Here | 0.10 24 | 0.8 25

3+32.5 = ℄ 12' Conc. Dr. on Lt.

1.40 40 Dr. | 0.40 25 | 0.21 20 walk | -0.12 15 Dr.

3+17.5 = ℄ of 12' Conc. Dr. on Lt.

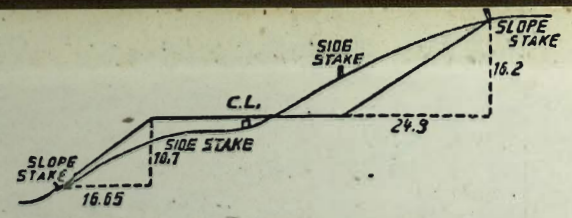
1.37 50 Dr. | 0.18 25 Dr. | -0.02 20 walk | -0.40 15 Dr. | 0.31 | -0.37 15.1 gut | -0.01 Top | 0.14 24 walk | 0.3 25 | 1.4 40

Cont. from P. 41

New Drives & Walks on La Salle - Nly. of Nashville

	Lt.	℄	Rt.
3+01 - 25' Rt. = ℄ 3' Conc. walk ✓			0.11 ✓ 25 walk 0.47 35 By House
2+87.5 - 24' Rt. = ℄ 3' Conc. walk ✓			-0.05 ✓ 24 walk 0.20 34.9 By House
2+61 - 24.8' Rt. = ℄ 3' Conc. walk ✓			0.07 ✓ 24.8 walk 0.48 35 walk By House
2+46.5 - 24.5' Rt. = ℄ 3' Conc. walk ✓			-0.02 ✓ 24.5 walk 0.40 34.9 By House
Set BM = spike in Pole Lt 2+44		- 0.33	
2+44 - 24.8' Rt. = ℄ P. pole # 631031-H ✓			
2+21.5 - 24.9 Rt. = ℄ 3' Conc. walk			0.14 ✓ 24.9 0.35 35.1 By House
2+06.5 - 24.9 Rt. = ℄ 3' Conc. walk ✓			-0.01 ✓ 24.9 walk 0.34 34.7 By House
1+81.5 - 24' Rt. = ℄ 3' Conc. walk ✓			-0.13 ✓ 24 walk 0.40 35 By House
1+67 - 24.8 Rt. = ℄ 3' Conc. walk ✓			-0.15 ✓ 24.8 walk 0.23 35 By House
1+64 - 25' Rt. = ℄ P. pole # 631030-H ✓			
1+59 - ℄ 8' Conc. Dr. on Lt. ✓	0.82 ✓ 40 Dr.	-0.32 ✓ 24.3 Brk	-0.56 ✓ 15.1 = Top cb + Dr.
1+41.5 - 24.1 Rt. = ℄ 3' Conc. walk ✓			-0.15 ✓ 24.1 walk 0.48 35.1 By House
1+36 - 24.1 Lt. = ℄ 2.5 Conc. walk ✓	0.64 33.6 By steps	-0.27 ✓ 24.1 walk	
1+26.5 - 24.9' Rt. = ℄ 3' Conc. walk ✓			-0.10 ✓ 24.9 walk 0.24 35 By House

Corr. Elev. shown.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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