

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Borrow Pit
Elev 5.00 @ 74+0

+0.50 Grade

IMPROVED TABLES
AND
INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

Overpass 22057
Grading & Paving 22067

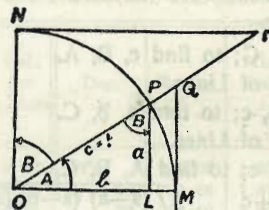


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \text{cos } B = LP \\ \text{cos } A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \\ \text{covers } A &= \frac{OP-LP}{OP} = OP-LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1-\text{Cos } A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1+\text{Cos } A}{2}} \\ \sin 2 A &= 2 \sin A \cos A & \cos 2 A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2 ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2} (A+B)}{\tan \frac{1}{2} (A-B)} \end{aligned}$$

TABLE IX

MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C o'	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.73
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE X

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XI

INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL.

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XII

MINUTES IN DECIMALS OF A DEGREE.

0'30''	.00833	10'30''	.17500	20'30''	.34167	30'30''	.50833	40'30''	.67500	50'30''	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE														
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46	
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68	
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90	
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14	
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39	
35°	.11	.22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66	
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94	
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21	
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48	
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77	
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07	
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39	
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72	
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09	
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46	
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89	
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32	
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83	
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34	
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60	
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22	

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE														
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020	
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083	
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135	
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188	
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264	
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341	
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445	
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550	
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700	
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851	
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01	
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17	
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39	
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62	
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91	
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20	
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58	
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96	
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96	
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32	

Morena Blvd. Linda Vista Road
Camino Del Rio + Taylor St.
 Sketches And Reference Points: 1-6
Morena Blvd North Approach C" Line Allg. Grade 7 31-36
 " " *B Line* 8 45-47
 " " *D Line* 9 37-39
Morena Blvd + Linda Vista Rd "H" Line 12-13 42-45
Morena Blvd + Camino Del Rio South End Inner Loop 14-15 46-49
 " " " " " " " " " " South West Inner Loop 16-17 50-53
Morena Blvd Over Pass to Taylor St. E Line 18 50-54
Morena Blvd South Approach W Center Cam 19 55-58
Storm Drain Napa St Linda Vista Road + Morena 20 31-33
Morena Blvd Storm Drain 27-30 23
 South West Inner Loop Storm Drain 34-35 23
Morena Blvd "G" Line 36 24
Morena Blvd And C" Line 0-25 to 140 25-36
Linda Vista Road 2+0 to 7+5.385 40-42
Napa St 47-48
Sherman St 49-50

Bench Level 10-11

Morena Blvd Linda Vista Road
Camino Del Rio + Taylor

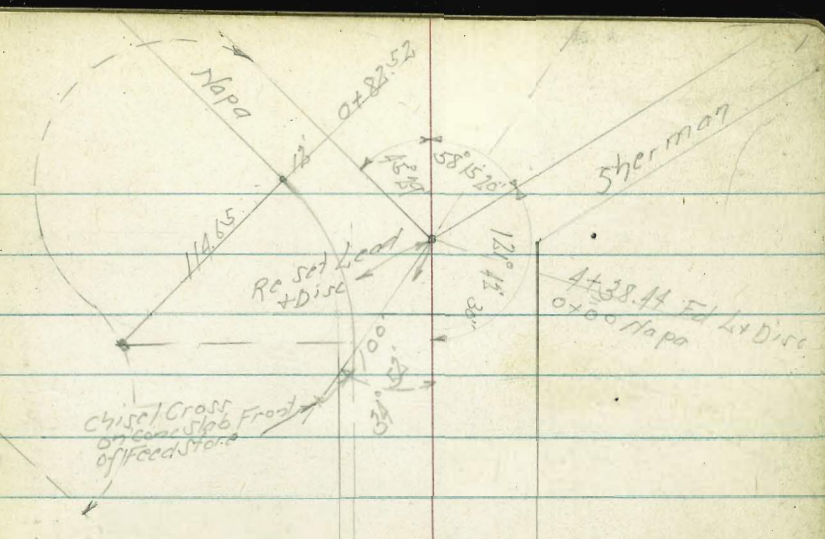
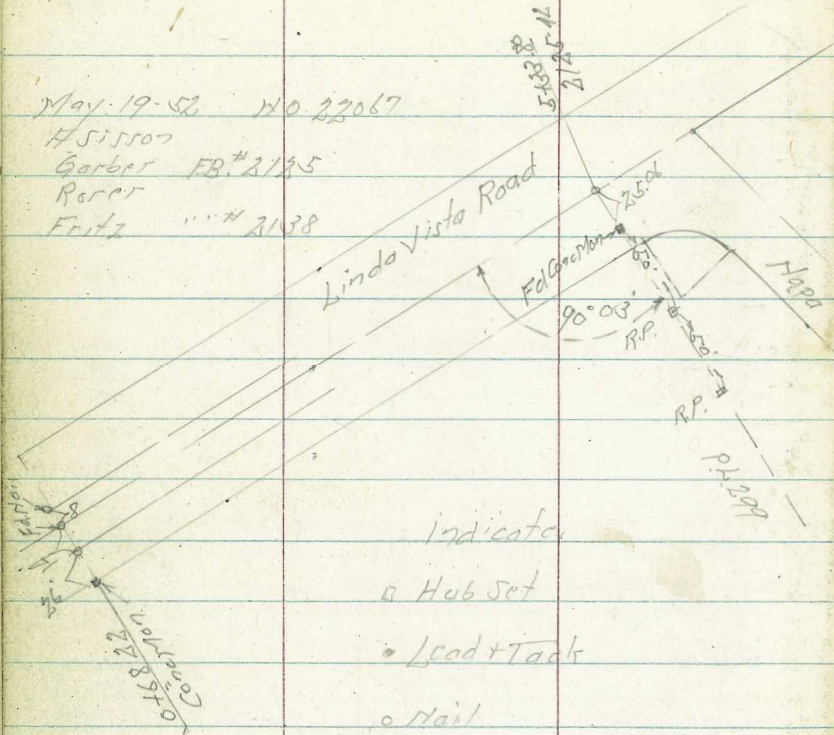
May 19-52 NO 22067

H. Sisson

Garber FB# 2125

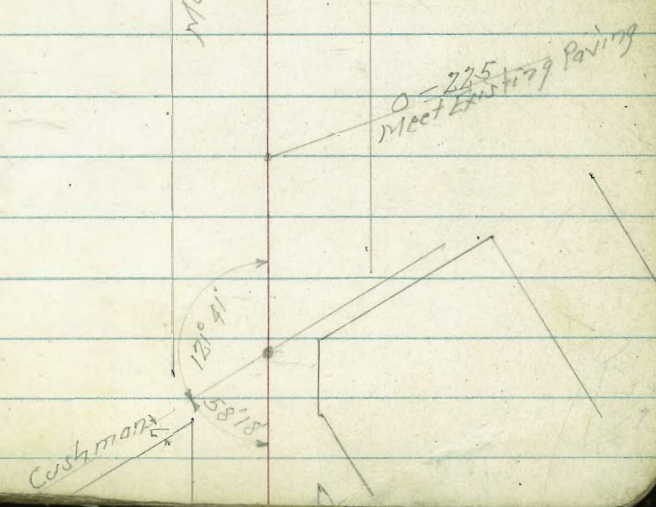
Rorer

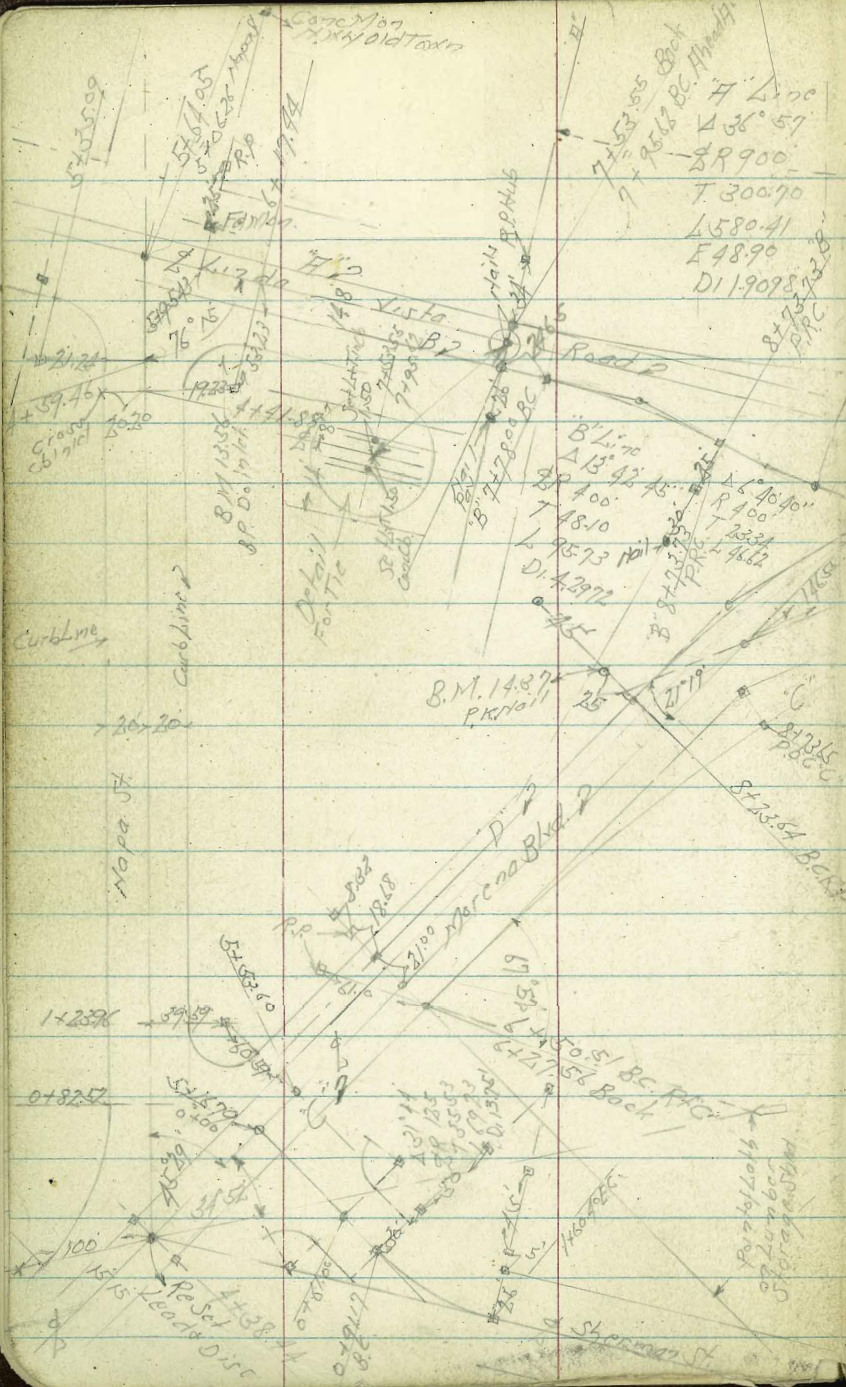
Fritz FB# 2138



BM 14.11
2.53
21.57

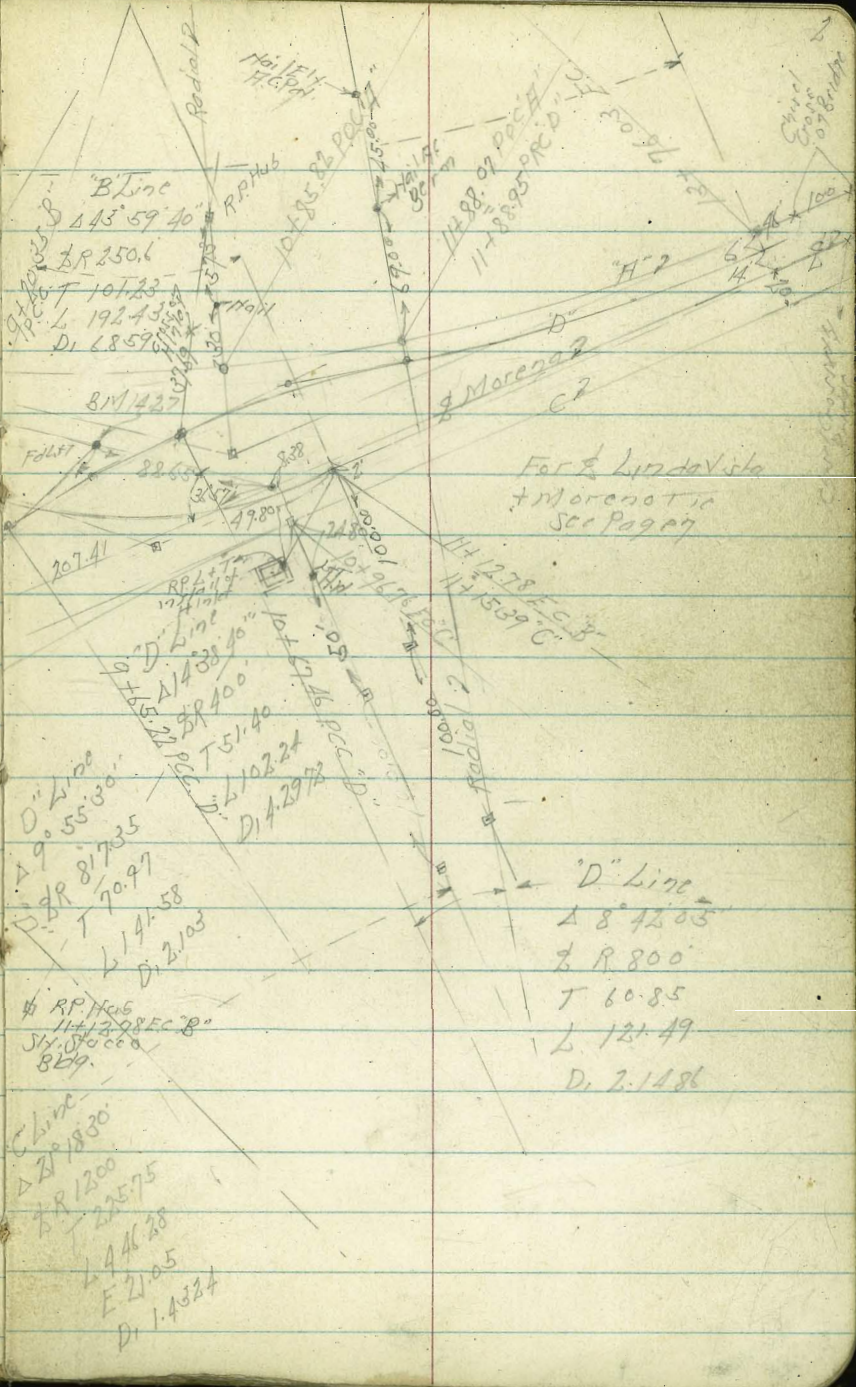
Conc. Pad
16.11
16.17
5.47
1.22
0.11





F Line
 $\Delta 38^{\circ} 59'$
 BR 900
 T 300.70
 L 580.41
 E 48.90
 D 1.9098

B Line
 $\Delta 13^{\circ} 42' 45''$
 T 48.10
 L 25.73
 D 1.4297



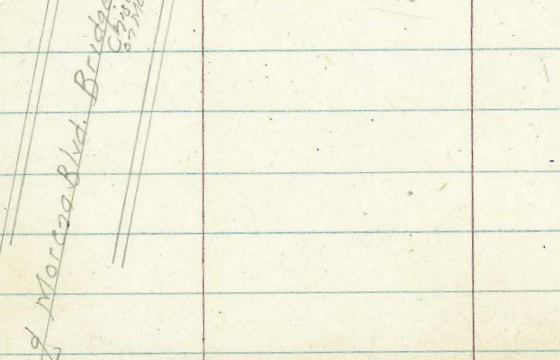
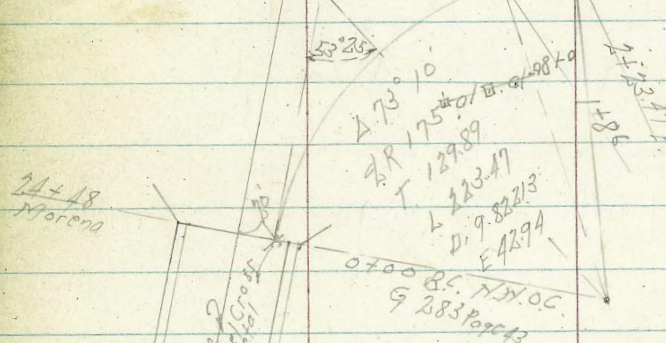
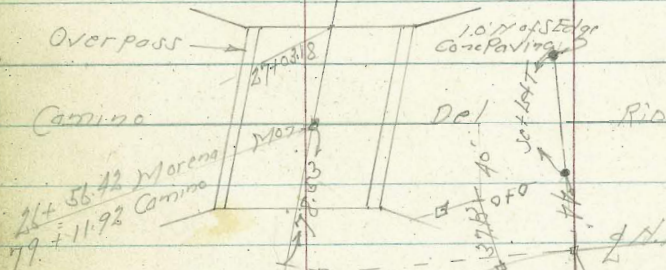
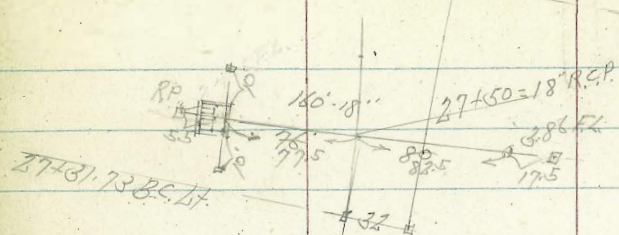
B Line
 $\Delta 43^{\circ} 59' 40''$
 BR 250.6
 T 107.23
 L 192.43
 D 1.8590

D Line
 $\Delta 43^{\circ} 40'$
 BR 400
 T 51.40
 L 102.24
 D 1.4297

D Line
 $\Delta 8^{\circ} 42' 05''$
 BR 800
 T 60.85
 L 121.49
 D 2.1486

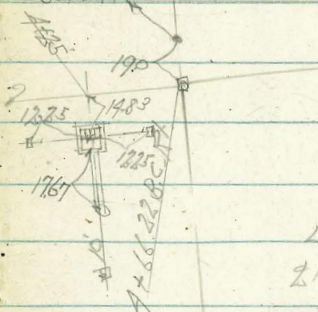
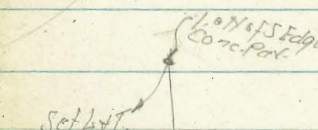
C Line
 $\Delta 18^{\circ} 30'$
 BR 1200
 L 225.75
 E 21.05
 D 1.4324

Morena Blvd. - Camino Del Rio And
North West Outer Connection



7229.91 Camino
7947.85 C. S. N. L.

Survey Loop

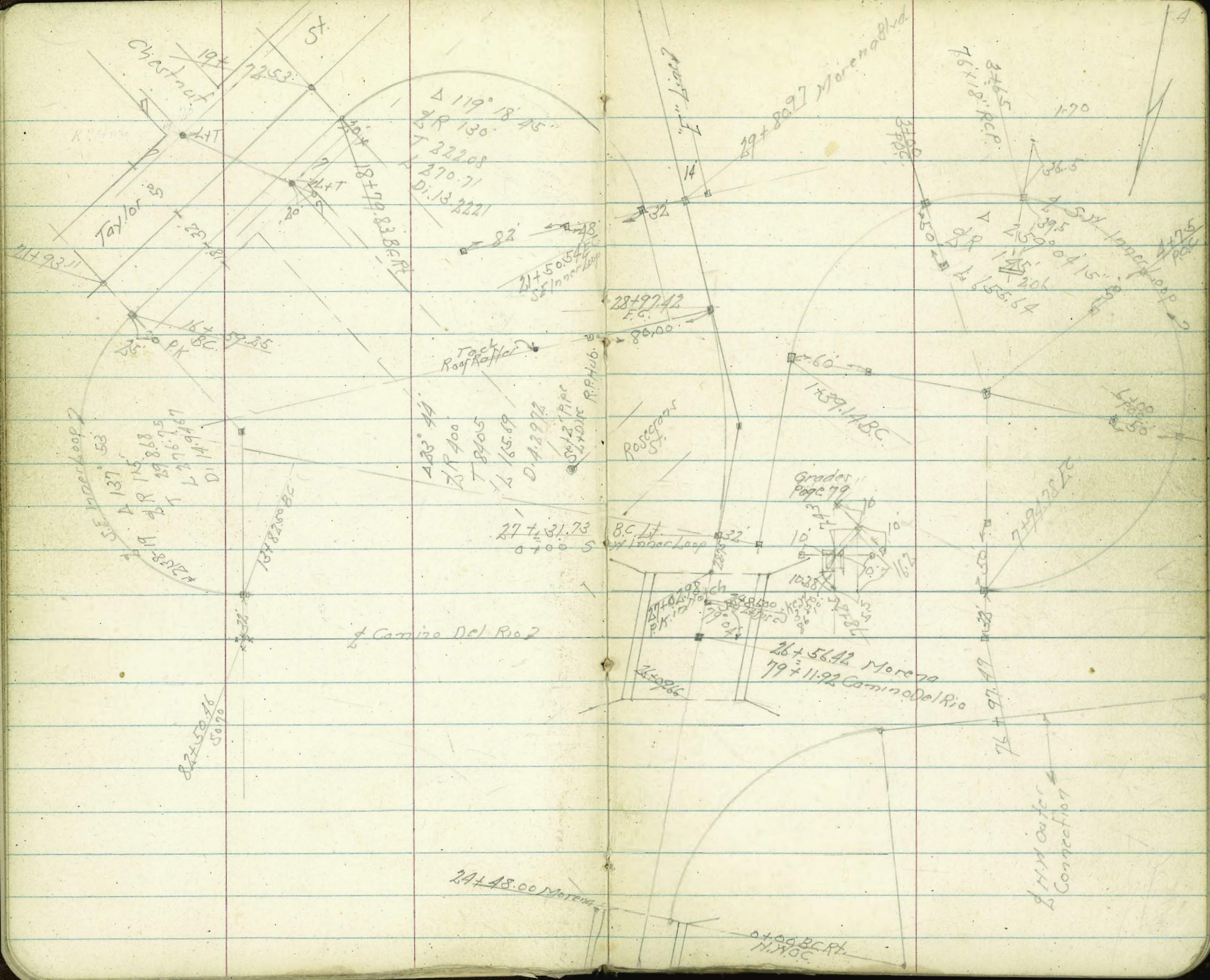


$\Delta 5^{\circ} 54'$
2R 2000
T 100.07
L 205.95
D1 0.85943

6+72.7 FC

7+25.85
N.W.C.

72497.51 FC R2000
Camino Del Rio



19+72.53
 Chestnut

$\Delta 119^{\circ} 18' 45''$
 BR 130
 T 222.08
 L 270.71
 D. 13.2221

29+80.97 Morera

3465
 76x18" RCP

SE Loop
 $\Delta 137^{\circ} 53'$
 BR 115.88
 T 29.75
 L 17.91
 D. 11.11

43° 45'
 BR 400
 T 18.05
 L 165.69
 D. 13.2972

28+97.42
 F.C.
 86.00

Grades
 Page 79

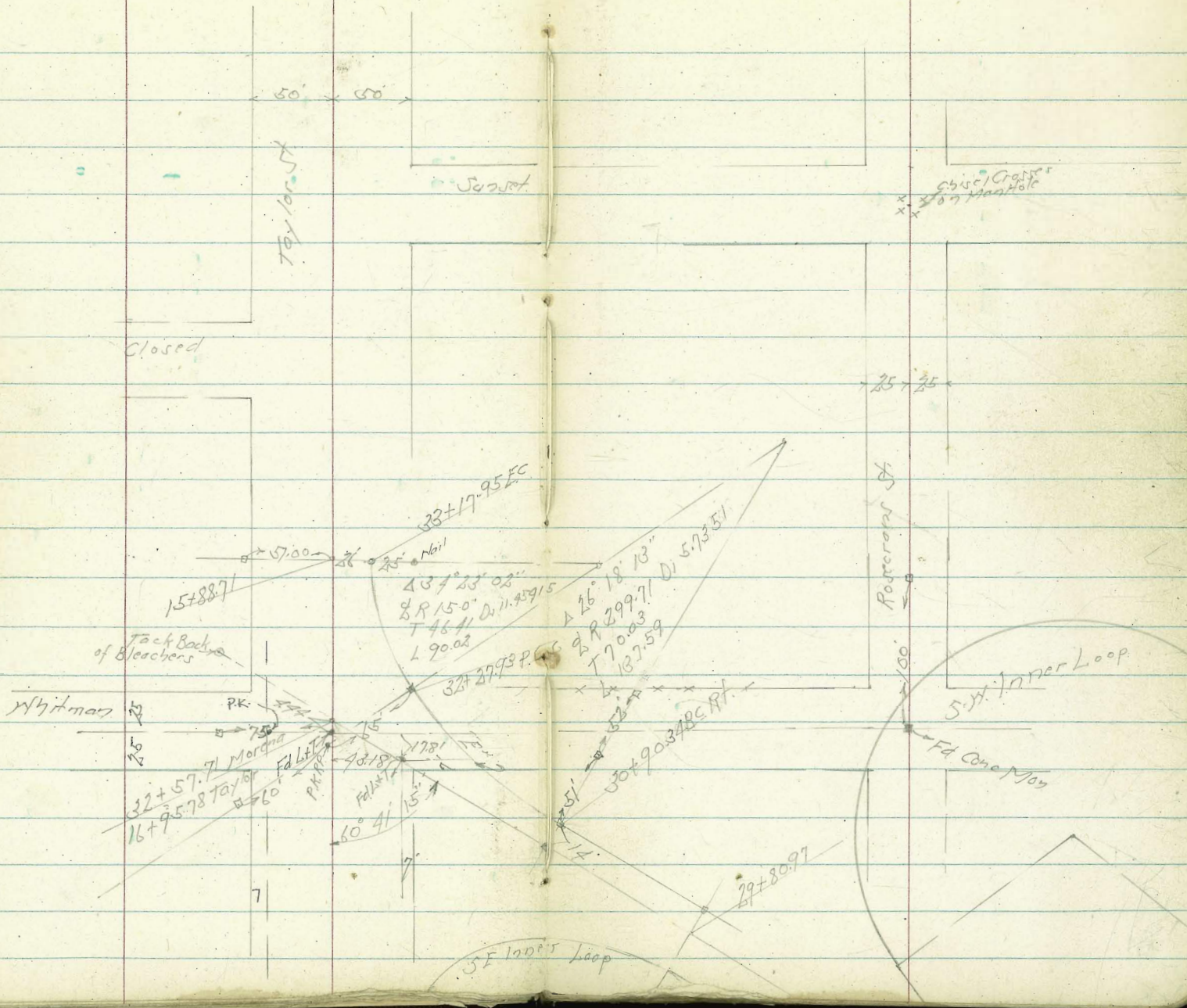
Camino Del Rio

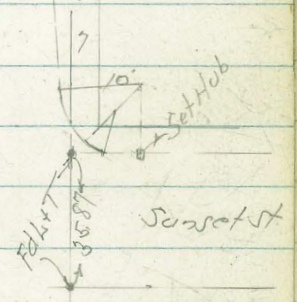
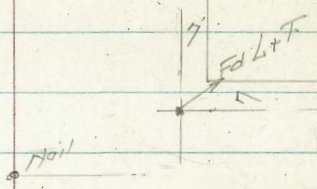
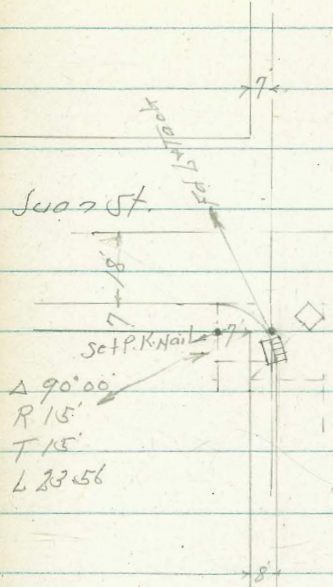
26+56.42 Morera
 79+11.92 Camino Del Rio

Hwy Outer
 Connection

27+48.00

0+00 B.C.R.
 H.M.C.

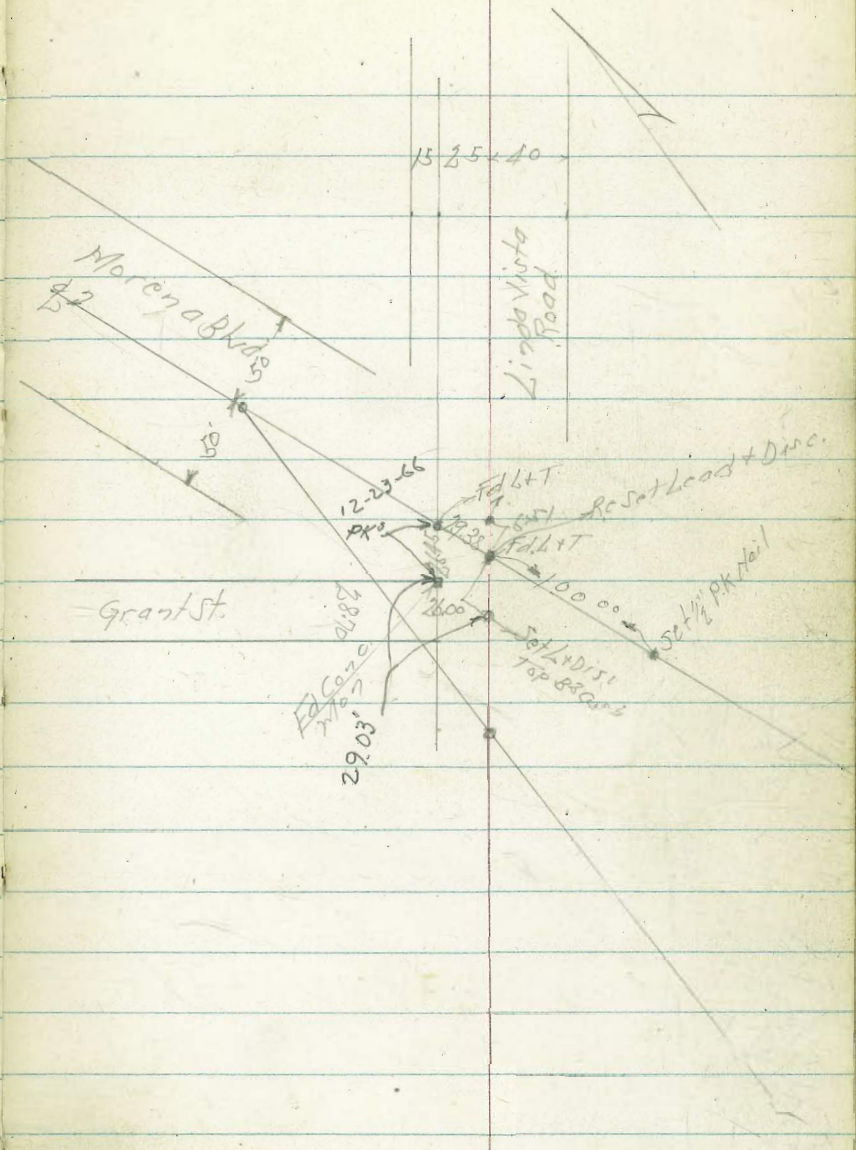




Alignment Morena Blvd North Approach
"C" Line

+96.79 E.C.	10° 39.25'	
+83.80	10° 20.64'	
+75	10° 08.04' LHT	
+50	9° 32.23' LHT	
+25	8° 56.42' LHT	
10+0	8° 20.61' LHT	Δ 21° 18' 30"
+75	7° 44.80' LHT	2 R 1200'
+50	7° 08.99' LHT	T 223.75
+25	6° 33.18' LHT	L 146.28
9+0	5° 57.67' LHT	E 21.05
+75	5° 19.62' LHT	D 1.4324
+50	4° 45.75' LHT	
+25	4° 09.94' LHT	
8+0	3° 34.13' LHT	
+75	2° 58.32' LHT	
+50	2° 22.51' LHT	
+25 1.50	1° 46.70' LHT	
7+0	1° 10.89' LHT	
+75	0° 35.08' LHT	

6+50.51.5 B.C.P.A.
6+27.56.7



Alignment - Moreno Blvd + Linda Vista Road
"B" Line

+12.78	EC	21° 59.83'	
11+0		20° 32.18' ✓	Δ 43° 59' 20"
+82.08 = 1' Road		18° 27.41'	
+75		17° 40.71' ✓	∠ R 250.6'
+50.		14° 49.24' ✓	T 101.23
+25		11° 57.77' ✓	L 192.43
+08	11 = Signal	10° 01.17'	
10+0		9° 06.30'	D1 6.859
+75	Rt. Signal	6° 14.83' ✗	
+6480		5° 04.87'	
+50.11 = CHANT		3° 24.12' ✓	
+20.35	PCC	3° 20.35' ✓	
+13		2° 48.95'	Δ 6° 40' 40"
9+0		1° 52.89' ✗	∠ R 400' L 46.62
+73.78	PRC	6° 51.37' ✓	T 23.34 D1 4.2972
+50		5° 09.40' ✗	Δ 13° 42' 45"
+25		3° 21.97' ✗	∠ R 100'
			T 18.10
8+0		1° 34.54' ✗	L 95.73
			D1 4.2972
7+78.00	B.C. RT Linda Vista		

Alignment Moreno Blvd + Linda Vista
"D" Line

+88.95	P.R.C.	4° 21.05"	Δ 8° 42' 05"
+75		3° 50.98" ✓	LR 800
+50		2° 57.21" ✓	T 60.85
+25		2° 03.51" ✓	L 121.49
11+0		1° 09.83" ✓	DI 2.1486
+75		0° 46.20" ✓	
+67.46	P.C.C.	7° 19.33"	
+50		6° 04.14" ✓	Δ 14° 38' 40"
+49.07		6° 00.14"	
+25		4° 16.71" ✓	LR 400
+11.67		3° 19.46"	
10+0		2° 29.28"	T 51.40
+75			L 102.24
			DI 4.29.72
+65.77	P.C.C.	1° 57.75"	
+52.76		1° 42.50"	
+38	Rt. Signal	1° 25.70" ✓	Δ 9° 55' 30"
+50			
+25		3° 33.15" ✓	LR 817.35
+20	Lt. Dispute	3° 22.64" ✓	
9+0	45.970	2° 40.58" ✓	T 70.97
+75		1° 48.00" ✓	L 141.58
+50		0° 55.43" ✓	DI 2.103
8+23.64	B.C.R.		

Bench Marks Morena Blvd + Linda Vista

Morena Blvd.

BM	4.70	18.97	14.27	LTT P.I. 2 Linda Vista Rd + Morena Blvd #2125-26.
BM		4.60	14.27	P.K. Hill 20' 41" 8' 23' 29" D
TP	5.25	19.145	5.075	12.895
BM		5.025	14.11	Chisel X 100' R.P. for Sherman & Korman Sylvia Conroy's Food Store
TP	6.235	23.705	1.675	17.47
				M.H. Rim 235' 1' 50" 17.44 2125-30
BM	5.895	26.400	3.20	20.505
				57' Rim Sherman Morena Cushman
TP	2.21		5.30	21.10
BM		8.18	16.13	16.19
				Sylvia Proprietor M762 Morena & Dorcas 16.19
BM	5.56	19.83	14.27	2 LTT Linda Vista + Morena
				Nov. 10-62
BM		1.99	14.84	10' 47.5" R. Crown Top 4 in let.

May 27-62

F. S. Johnson
Garber
Rorer
Fritz

Linda Vista Road

10

BM	5.77	20.04	14.27	LTT 2 Linda Vista Rd + Morena
TP	9.98	26.33	3.69	16.35
BM		3.98	22.35	B.P. Mt. Car. Bridge Top Ving Wall
BM	4.01	18.28	14.27	LTT 2 Linda Vista + Morena
	6.115	19.255	5.04	13.24
				P.K. Hill Rt. Linda Vista Road + Hapo
BM		1.055	18.30	2 Hill 21' Linda Vista
TP	5.30	18.54	6.115	13.24
BM	Start	4.26	14.28	LTT 2 Linda Vista + Morena 14.27
BM	4.315	18.585	14.27	LTT 2 Linda Vista + Morena
BM		5.025	13.56	S.W.P. Doris Hapo Linda Vista

Bench Levels Morano Blvd
Camino Del Rio + Taylor St.

BM	3.76	23.83	20.07	Six BP in walk of Bridge Morano + Taylor St.
	3.49	14.65	11.67	12.16
BM	4.10	11.895	6.855	7.795 SE BP check out Taylor (9.82) Rec
B.M.	4.905	11.16	5.64	6.255 Check H 3' off Taylor S. 1/4 Highway
	4.36	10.21	5.31	5.85
BM			5.56	4.65 1.6304 SE BP Jewett St + Taylor 4.61 #21388
B.M.	3.435	23.505	20.07	Six BP in walk of Bridge Morano + Taylor
TP	11.22	32.79	1.935	21.570
B.M.			5.25	27.54 BP E cb. Morano 35 South of Overpass
BM	0.92	28.46		27.54 7.600
Cons/BM			0.17	28.29 28.47 28.35 Page 60
	3.28	20.18	11.56	16.90
	3.505	15.065	8.62	11.56
BM	6.59	17.02	4.635	10.430 27 Moos Under Overpass (10.54)
BM Starting	7.09	22.21	1.90	15.12 Six BP walk of Bridge Morano + Taylor
			2.14	20.07

BM	3.96	10.21		Check H SE of Taylor 6.25 S. 1/4 Highway
BM	Set	2.92	7.29	Six BP end North moor + Taylor
				Feb. 13. 58 F.P. 5500
				Morano + Taylor St. Bridge C.I. G.I. Station
				Cut off for removal of old Bridge
BM	1.62	20.70		BP out used as 20.07 2.07 29.08
	1.52	19.43	12.79	17.91
			11.50	7.93 Water level under Hwy Bridge
				used as 8.00 Cut off.
				Rod 11.43 8.92 63.00 and Piers + Hacks that

Alignment Moreno Blvd + Linda Vista Road
"A" Line

+50	11° 16.81' ✓	
+25	10° 29.06' ✓	
11+0	9° 41.32' ✓	
+85.82 P.O.C. Mid. Point	9° 14.24' ✓	Δ 36° 57'
+75 - opp'd 17' lot on lot	8° 53.57' ✓	Δ R 900'
+50	8° 05.82' ✓	T 300.70'
+46.46 = 1' Rot RT	7° 59.06' ✓	
+25	7° 18.08' ✓	L 580.41'
10+0	6° 30.33' ✓	F 4890'
+75	5° 42.59' ✓	D. 1.9098
+50 x	4° 54.84' ✓	
+25	4° 07.10' ✓	
9+0	3° 19.35' ✓	
+75	2° 31.61' ✓	
+50	1° 43.86' ✓	
+25	0° 56.12' ✓	
8+0	0° 08.37' ✓	

7+95.62 B.C. of A Road
7+53.55 Back

"H"

18

+76.03 FC	18° 28' 50" X
+50	17° 38' 77" ^W 10
+25	16° 51' 03" ^W 10
13+0	16° 02' 28" ^W 10
+75	15° 15' 54" ^W 10
+63 = P.B. 02 FT.	14° 52' 62" ^W 10
+50	14° 27' 79" ^W 10
+25	13° 40' 05" ^W 11
12+0	12° 52' 30" ^W 11
11+8807 P.O.C. P.R.C. "D."	12° 29' 50"
11+75	12° 04' 55" X

Alignment South East Inner Loop
 Moreno Blvd Camino Del Rio + Taylor St.

+59.25 FC	18° 56.5' ✓	
+42.77	14° 50.20' ✓	
+12.22	59° 59.26' ✓	∧ 127° 53'
16+0	51° 10.93' ✗	∠ R 115°
+72.71	47° 22.86' ✓	T 298.68
+60: S.A. + P.B.	41° 13.07'	
+350	41° 42.60' ✗	L 276.75
+25	35° 29.90' ✗	D. 14.9469
15+0	29° 16.24' ✗	
+95 P.O.C.	28° 01.51'	
+79.99	24° 17.39' ✗	
C 2995		
+55	16° 48.90' ✗	
C 1501		
+34.99	13° 04.70' ✗	
+101/2 S.L. 078'	5° 51.04'	
14+0 05.83	5° 48.71' ✗	
C 23131		
13+82.50		B.C. Rt.

South East Inner Loop

+50.54 F.C. C 22.79	59° 39.37'	
+23.23	53° 38.27' ✓✓	
+12.20	51° 12.42' ✓✓	
21+0	48° 31.11' ✓✓	Δ 119° 18' 45"
+75	43° 00.56' ✓✓	∠ R 130°
+50	37° 30' ✓✓	T 222.08
+35	34° 11.67' ✓	
+25 P.O.C.	31° 59.45' ✓✓	L 270.71
20+0	26° 28.90' ✓✓	D: 13.2221
+75	20° 58.25' ✓✓	
+50 50% 99700	15° 27.80' ✓✓	
+38.04	12° 47.65' ✓✓	
+25	9° 57.24' ✓✓	
+07.14	6° 01.08' ✓✓	
19+00	4° 26.69' ✓✓	
C 22.15		
18+79.83 B.C. Rt		

Alignment South West Inner Loop.
Morena Blvd + Camino Del Rio

5+0	71° 17.74' LH	
+75 P.O.C.	66° 21.38' LH	
+50	61° 25.03' LH	
+25	56° 28.67' LH	Δ 259° 04' 15"
4+0	51° 32.31' LH	1/2 Δ 129° 32' 07 1/2"
+75	46° 35.96' LH	9 R. 145°
+65 = C.V.	44° 37.41'	
+50	41° 39.60' LH	L 655.64
+25	36° 42.24' LH	D 1185.43
3+0 P.O.C.	31° 46.88' LH	
+75	26° 50.53' LH	
+50 = Light on RT	21° 54.17' LH	
+40 = PB on RT	19° 55.62'	
+25	16° 57.81' LH	
C 2497		
2+0	12° 01.45' LH	
+75	7° 05.10' LH	
+66.92	5° 29.57' LH	
+50	2° 08.74' LH	
C = 10.85		
1+39.14 B.C.		

0+00 = 27+31.73 B.C. Morena Blvd.

South West Inner Loop

+94.78	F.C.	129°	22.12	✓
+75		125°	37.66	✓
+72.90		125°	12.78	
+50		120°	41.32	✓
+25		115°	44.96	✓
7.40		110°	48.60	✓
+75		105°	52.24	✓
+50		100°	55.89	✓
+25		95°	59.53	✓
6.40	P.O.C.	91°	02.17	✓
+75		86°	06.81	✓
+50		81°	10.46	✓
5.25		76°	14.10	✓

Alignment Morcna Blvd
Over Pass to Taylor St.

E Line Morcna Blvd + Taylor St.

18

+97.42	FC	11° 52' ✓	
+75		10° 15.66' ✓	Δ 23° 44'
+50		8° 28.22' ✓	Σ R 400'
+25		6° 40.80' ✓	T 84.05'
28+0		1° 53.37' ✓	L 165.19
+75		3° 05.94' ✓	Di 4.2972
+50 = 18" RCP		1° 18.51' ✓	
27+31.73	BCR†		

+17.95	FC	17° 11.52' ✓	Δ 31° 23' 02"
33+0		13° 15.85' ✓	Σ R 150.00
+75		8° 59.38' ✓	T 46.41
+50.73		4° 21.26' ✓	L 90.02
+50		4° 12.90' ✓	Di 11.45915
+27.93	PCC	13° 09.10' ✓	
32+0		10° 28.91' ✓	Δ 26° 18' 12"
+75		8° 05.55' ✓	Σ R 300'
+50		5° 42.16' ✓	T 70.10
+25		3° 18.78' ✓	L 137.73
31+0		0° 55.46' ✓	Di 5.72958
30+90.34	BCR†		

Alignment North West Outer Connection
 Morena Blvd. South Approach

+23.47 E.C.	36° 35'	
+10 Light	34° 22.69	
2+0	32° 44.47 ^{III}	
+86 = Culvert 18'	30° 26.94 [✓]	
+75 P.O.C.	28° 38.90 ^{III}	Δ 73° 10'
+50	24° 33.34 ^{III}	Δ R 175'
+25	20° 27.79 ^{III}	T 129.89
+11.74 Mid Point	18° 17.5°	
1+0	16° 22.23 ^{III}	L 123.97
+85 Light	13° 54.89	
+75	12° 16.67 ^{III}	DI 9.82212
+50	8° 11.11 ^{III}	F 42.94
+25	4° 05.57 ^{III}	

C 24.97
 0+0.0 B.C.Rt = Opp
 24+48 Morena Blvd.

+72.17 E.C.	2° 57' [✓]	
+50	2° 37.95 ⁺	
+25	2° 16.46 [✓]	Δ 5° 51'
6+0	1° 54.98 ^W	Δ R 2000 T 103.07
+75	1° 33.49 ^W	L 205.95
+50	1° 12' ⁺	D.O. 85913
+28.81 [✓]	0° 53.79 [✓]	
+25	0° 50.52 [✓]	
5+0 [✓]	0° 29.04 ⁺	
+83.81 [✓]	0° 15.12 [✓]	
+75	0° 07.55 [✓]	

4+66.22 B.C.Rt

BM 465 1428
L+T
Morong +
Linda Vista
1427

+97 = Outlet 7.25
11.68
5.07
c6.66

+39.3 = H Carb Inlet +39.68
Grate Top 13.84 14.67
5.09 4.26
5.07 5.07
c6.62 F0.81
7.45 11.48
5.07
c6.41

+79 7.53
11.40
5.05
c6.25

+85.7 = H Inlet #3 North Side Edge
Grate Top 14.00 14.83
4.93 4.10
4.56 4.56
c6.37 F0.46
8.44 10.49
4.56
c6.93

5+01 7.62
11.31
4.98
c6.33

+60 8.31
10.62
4.87
c6.65

+81 7.70
11.23
4.63
c6.60

+90 8.70
10.65
4.83
c6.70

1-20
+61 Souths
+79.5 North inside of
cleanout box.
TOP 15.85
3.09
4.60
F1.52
F0.54
7.79 11.14
4.60
c6.54
10.54

+70 8.10
10.83
4.60
c6.23

4+28 7.90
11.03
4.63
c6.38
10.5

0+0 - Clean out
= 1+12.5%
TOP 15.94
8.00 10.93
4.52
c6.41

Grades Storm Drain Morcena Blvd May 29-52
27+50

Sketch Page 3
2 Rad 2 Ground

Restake June 9-52
7.46
6.87
60.85

+77.5 = R.P.				
+60 = outlet	6.8	7.3	3.86 6.30	10.33 c3.72
+40.5	6.3	7.8	3.96 6.34	10.13 8.84 c3.77
1+20	6.3	7.8	4.07 6.37	10.92 10.96 c3.56
1+00.5	5.1	9.0	4.17 6.41	9.91 5.67 c4.53 10.50
+80	5.5	8.6	4.27 6.45	9.82 5.73 c4.07 10.50
+60	5.5	8.6	4.37 6.49	9.72 5.80 c3.72 10.50
+40	5.6	8.5	4.48 6.52	9.66 5.96 c3.66 10.50
+20	6.3	7.8	4.58 6.56	9.51 6.05 c3.89 10.50
0+0 = inlet	7.71 6.91	7.0 5.91	4.68 6.60	9.41 7.00 c2.71 10 South
0 - 07 = R.P.	7.18 7.08 6.18 7.07	8.18 7.08 c1.18 Grate	7.16 6.55	
BM 7.18	14.09		6.91	07 R 145 H 6 5.12
3.91	13.76	4.16	9.85	
BM 3.47	14.01		10.54	BM not Morcena Camino

Storm Drain South West Inner Loop
3+65 76'-18"
Sketch Page 4

23
June 4-52
FD 5507
Garber
Rort
Fritz

					2 Rad	2 Ground Elev.
+76 = outlet	4.8	6.6	1.70	9.19 4.86 c4.59		
+57 = outlet	4.8	6.6	1.79	9.60 4.87 c4.73		
+38	4.6	6.8	1.88	9.51 4.64 c4.84		
+19	4.8	6.6	1.97	9.43 4.83 c4.89		
0+00 = inlet	4.7	6.7	2.06	9.33 4.71 c4.56 10 East		
BM 4.98	11.39		6.91	07 R 145 H 6 5.12 Bp 61		

Storm Drain + H Curb Inlet
Outer Conn.

July 10-52
175.500
Garber
Rorer

Sketch Page 3 80' 18" R.C.P.

Storm Drain + H Curb Inlet
4+25 North West Outer Connection
Sketch Page 3
18' 18" R.C.P.

June 24
176.52
7.00.000

18.62 X B Ford Page 57

"H" Inlet

tapcs 1.62
17.00 7.99

17.87
10.00
8.87

Grate

16.08

2.54
9.99
12.53
10.00

Bottom Box

6.23

13.07
9.49
3.58
10.00

16' H of H Inside Box
Outlet

5.75

13.07
8.32
4.75
10.00
11.29

+80 = NW 1/4 outlet

7.00 $\frac{13.60}{1.80}$
c 11.80

$\frac{13.60}{1.80}$
11.80

+60

7.28 $\frac{13.22}{0.02}$
c 12.20

$\frac{13.22}{0.02}$
12.20

+40

7.75 $\frac{12.85}{1.85}$
c 11.00
10

$\frac{12.85}{1.85}$
11.00
20

+20

8.13 $\frac{13.47}{5.19}$
c 6.67
105

0+0 = Inlet

8.50 $\frac{13.10}{9.69}$
c 2.51
105

BM 5283-49 10.06

20.60X

10.54 Corners of Storm

Lt. East

F. Simon
R. Porter
D. Simpson
off-man

Rt. West

Sta	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	E	E.P.	Shdr. Hinge	Toe	R.P.
BM	3.39		23.90 T		20.51						
-200	Finish & Grader				15	19.60 12		19.37 8 Ex. 1	15		Soil Cuts 24.36 T
BM	14.11 7.30 21.41 T										
-1456	Sub Grader		266	5.2 5.2 FO.2 26.3	18.73 20	16.52 FO.6 13.3	19.32 13.35	19.30 10.7	19.31 FO.7	46.50 FO.4 15'	19.26 15'
-125	2 IR		OK		18.63 25'	23.2 25.7	19.20 19.18 14	5.06 5.25 FO.19 2.82 2.81 FO.18	19.20 19.30 12	5.18 2.25 5.13	19.03 15'
-1400			302	5.5 5.1 FO.6 26.4	18.39 25.50	5.0 6.1 FO.4 14.5	18.94 14.50	19.06 2.44 2.42 2.81 FO.18	19.36 1.05 18.94 13.54	5.0 5.2 FO.4 13'	18.74 17'
-1475				5.8 out	18.16 26'	5.2	19.23 5.06 18.71 15'	19.33 2 18.83 2.17 2.84 FO.18	5.65 2.5 5.9	18.46 19'	5.5 out
-0+50			249	6.0 8.1 FO.7 39.7	17.92 26.5'	5.4 8.1 FO.7 7.5	18.47 15.5	18.59 2.91 3.84 FO.18	19.09 3.06 18.47 15'	5.4 5.2 FO.2 15'	18.17 21'

on R.M. 2111
Morena
Cushman
Page 10

Soil Cuts
24.36 T

27 M.H.
Concrete

Morena Blvd.

2390A

Sta	Slope Super	R.P.	Toe	Shdr. Hinge	F.P.	φ	F.P.	Shdr. Hinge	Toe	R.P.
-0+25	Finis Grader 21.41 T		out	17.70 27'	18.87 18.25 16.33 3.50	0.0	18.87 18.25 16 16	17.70 27' 24.5		20.357 28.7 17.78 6.58 24.36
0+00	Sub. Grader cont 21.50 T	3.93	6.4' 11.2' 1.53 35.5	17.48 27.5'	5.9 11.2 F.58 26.5		18.65.06 G. 3P 18.03 16.5 3.27 3.78	18.15 18.03 17'	17.48 28'	6.4 5.7 20.7 28.7
0+25				17.25 28'	17.80 17.92 17.57 3.95		17.92 17.80 18' F.0.13 F.0.07	17.25 29'		8 Island road BM 14.11 7.21 21.33
0+50		4.37	6.9' 7.6' F.0.7 29.6	17.02 28.5'	6.3 7.6 F.L.2 17.5		2.28 2.5 3.03 3.92 17.57 17.5 4.18	17.69 17.57 19'	17.02 30'	6.9 6.5 20.6
0+60 = ICLR cont							3.20 3.20 F.0.56 18.17 4.70 ICLR 3.40	18.11 18.11 3.40		
0+75				16.80 29'	5.02 3.82 F.0.53 17.35 18.15 3.5 3.75		18.00.02 0.30 17.97 7.50 F.0.70 17.35 20'	16.80 31'		
TP		3.21	20.82	6.39 17.51			3.40 3.5 3.21			

Sta	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	#	E.P.	Shdr. Hinge	Toe	R.P.
			20.82			17.77	cl	17.74	cl		
1+00			4.84 4.2 F0.3 30.0	16.57 29.50'	3.7 1.6 F0.9 18.5	17.12 18.50'	1724 4.26 4.27 4.0	17.12 20.75'	3.7 3.1 C0.6 20.75	16.57 31.75'	4.3 C1.3 33.0
	Finish on										
	21.41										
	Subgrade on										
	21.56										
1+25				16.34 30'		16.89 19'	17.01 4.6 4.49 4.50 4.0	16.89 21'	3.8 3.16 3.16 3.25 3.2	16.34 32'	Soil G R1.19 20.25
	21.32	Island									
		Curv									
1+50			5.30 4.7 2.8 F0.1 33.7	16.11 30.50'	4.0 4.8 F2.6 19.5	16.66 19.50'	16.78 4.72 4.73 4.0	16.66 21'	4.0 4.0 3.9 3.9 3.2 C0.8 31.0	16.11 32'	1.7 3.4 C1.3 33.3
1+75				15.88 31'		16.43 20.50'	16.55 4.95 4.94 4.0	16.43 21'	4.3 4.7 F0.49 3.9 3.9 3.9	15.88 32'	
1+82.5											
2+00			5.76 5.2 5.2 6.0 31.5	15.65 31.5'	4.6 5.2 F0.6 30.5	16.20 20.50'	16.32 5.18 5.16 4.0	16.20 21'	4.5 4.3 C0.3 31.0	15.65 32'	5.2 4.3 C0.9 33.9

Morena Blvd.

20.82T

Sta.	Slope Super	R.P.	Toe	Slidr. Hinge
2+25	3' 50 1st Finish 21.41T		5.4. 5.2 0.0 32.0	598 15.43 32' 48 5.2 F0.6 21.0
2+50	Island Cr 21.32T		5.7. 7.0 F1.6 37.2	424 15.17 34.86' 5.1 7.0 F2.2 23.86
2+75				14.91 37.71'
3+00	494 BM 14.11 4.87 18.90		6.2. 6.7 F0.5 71.4	676 14.65 40.57' 5.6. 6.7 F1.4 29.57
3+30	18.70 12.37 4.33 4.47 F0.4 3' East		6.5. 6.5 0.0 77.0	704 14.37 44' 5.9 6.6 F0.6 33.0

E.P.	E	E.P.	Slidr. Hinge	Toe	R.P.
166.02 7-24 1/2 15.98	4.77 5.23 F0.51 16.10	436 2.7 1.8 15.98	15.43 32'	5.1. 4.5 0.0 32.9	pt. 381.0 20.35T
211.558 5.89	5.40 5.95 F0.05	21' 21.0			
1537.02 7	4.95 5.17 F0.69	410 4.8 5.1 F0.5 21.0	15.20 32'	5.6. 5.0 0.0 32.0	
1514 7	5.18 5.03 F0.91	482 4.8 5.08	14.97 32'		
1591 7	5.41 5.72 F0.71	506 5.3 5.5 F0.2 21.0	14.74 32'	6.1. 10.7 F0.6 38.9	
1566 7	5.11 5.02 F0.68	535 5.5 5.8 F0.3 21.0	14.49 32'	6.3. 12.1 F0.8 40.7	

Morena Blvd.

Lt. East.

Rt. W

20.82T

Sta.	Slope Super Finish	R.P.	Toe	Shdr. Hinge	E	E.P.	φ	E.P.	Shdr. Hinge	Toe	R.P.
3+50	Sub Grade cut 21.550X		7.6 6.6 6.0 44.0	14.25 44'	6.0 6.6 Fo. 6.0 33.0	14.80 33' 6.70 6.88 6.95 6.97	15.04 6.71 6.88 Fo. 1.2	14.92 21' 5.48 5.78	14.37 32'	6.5 12.6 Fo. 6.1 41.2	✓
TP	4.01	18.12	6.72	14.11 14.10	Chisel Cone Start Feed Start 14.11 Page 10						Soil/Cracks at Ticks BM 14.11 x Feed Start 18.93T
3+75				14.14 44'		14.69 33' 6.81 7.02	14.93 6.57 6.65 Fo. 0.8	14.81 21'	14.26 32'		
4+06.05			4.1 4.4 Fo. 0.2 44.5	14.05 44'	3.5 4.4 Fo. 0.7 33	14.60 33' 6.92 7.15	14.84 6.66 6.74 Fo. 0.8	14.72 21'	14.17 33'	4.82 4.9 Fo. 0.5 41.9	Nov 21. 52 Soil/Cracks at Ticks BM 14.11 x Feed Start 18.93T
4+25		For 41951 BM 14.11 6.56 19.61									14.11 18.99T
+28 - 8' CB Rad.						14.83 43.4 4.34 Fo. 1.0	14.71 21'		14.31 35.06'		
+35 - 1' 30" R.						6.00					
4+50						14.60 33' 6.83 Fo. 1.5	14.84 6.73 6.88 Fo. 1.5	14.72 21'	14.30 39.08'		
+75						14.90	6.57 Fo. 3.0				

Morena Blvd

Lt = F

Rt. W

30

18.12

Sta. Slope Super R.P. Toe Shdr. Hinge

E.P. ϵ E.P.

Shdr. Hinge Toe R.P.

4+81.88 = BC on Pt

44.69 14.93 14.69
33' out 33'

Gut E11 (4.71)
43.10'

15.39T
Page 47
2.1
5.1
F3.0
4.5
12.5 in from
20' Road

Soil Cr.
18.93T

5+00

14.76 15.00 14.76
33' 4.07
4.25
F0.28

5+25

14.89 15.13 14.89
33' 3.94
4.41
F0.47

BM 14.84
19.21T

5+50.54 = BC on Lt.
= R2 on Rt.

18.54T
Page 27
3.9
3.2
1 F1.9
48.8
Gut E11 (4.61)
44.23

15.01 15.25 14.97
33' 3.82
4.27
F0.27

394
534
F1.70 15.77
5
15.75.06 F1.38
9 43.6
4.5 3.95 36.
5.84
14.56 436
30 4.61
18.48T

+54.79 = BC on Pt.

14.95
33

Gut E11 (4.56)
43.68' F1.1
45.4
Set from
S. Morena

+75

15.38 14.94
33'

3.2
4.7
F1.5
33
1.25 1.88
4.37 37.45
3.81 15.90.25
53.2 F1.57.5
40.45
Gut E11 (4.65)
40.45
15.88.06
9
4.22
1.14
3.83
3.88
F1.55

Morena Blvd. & "C" Line

Rt. 111

31

18.12

Sta.	Slope	Super	R.P.	Toe	E.P.	Slide Hinge	E.P.	±	E.P.	Slide Hinge	E.P.	Toe	R.P.
6+00			18.547	4.1 6.1 F1.0 45.3	3.6 5.1 F1.5 37.6	14.43 14	149.3 346	15.50	15.22 21'	6.1 36.45'	4.2 3.7 2.5 F1.6 21	3.4 4.5 F1.1 38.2	Island 19.71X
6+27.56	Morena	back			C5 16.14	14.85	1540	15.64	15.27 21'	14.72 32'	4.2 2.9 2.5 F1.6 21.0	3.2 4.5 F1.1 33.7	Island BM 14.11 4.27 18.7
6+50.51	B.C.	"C" Line Ahead	05		3.59 5.45 F1.87	44'	47.2	33'	2.53 5.45 F1.95	16.18 9	16.16 9	4.2 2.9 2.5 F1.6 21.0	BM 14.11 4.27 18.7
7+50	"C"					14.27 44'	47.2	33'	5.45 F1.95	16.18 9	16.16 9	4.2 2.9 2.5 F1.6 21.0	BM 14.11 4.27 18.7
6+75	"C"	Line	0325			16.26 24.2 5.52 F2.06		15.76 6'	15.31 6'	14.90 17'			BM 14.11 4.27 18.7
7+00		.046			3.34 5.52 F2.25	16.39	15.89	6'	15.34 6'	14.88 17'	2.8 4.5 F1.7 8	3.2 4.5 F1.3 19.0	BM 14.11 4.27 18.7
TP	462		18.34	4.40	13.72								
7+25		.052			3.34 5.52 F2.25	16.49	15.99	6'	15.36 6'	14.78 17'			

"C" Line

18.34T

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	E	E.P.	Shdr. Hinge	F.P.	Toe	R.P.	
7+50		.057			3.16. Curb 4.91 F1.75	16.57	16	.07 6'	14.94 14	14.77 17'	3.0. 4.8 F1.8 6	3.6. 4.8 F1.2 18.8	18.48T
7+75		.059			3.11. 4.58 F1.47	16.62	16	.12 6'	14.94 14	14.76 17'			19.73T
8+00		.06			3.16. 4.48 F1.28	16.63	16	.13 6'	14.94 14	14.75 17'	3.0. 4.4 F1.5 6	3.6. 4.4 F1.8 18.2	20.32T
8+25		.06			3.12. 4.46 F1.34	16.61	16	.11 6'	14.91 14	14.73 17'			
8+50		.06			3.16. 4.34 F1.18	16.57	16	.07 6'	14.87 14	14.69 17'	3.0. 4.6 F1.6 6	3.7. 4.6 F1.6 18.4	

"C" Line

18.24

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	¢	E.P.	Shdr. Hinge	E.P.	Toe	R.P.
B+75		06			338. Carb 2.27 F1.04 16.48	15.98 6'		15.26 6'	14.78 5.54 14 5.79	14.60 17'		18.48 3.99 14.49 2.15 18.61
9+00		06			336. 1.45 F1.09 16.37	15.87 6'		15.15 6'	14.67 5.45 14 5.70	14.49 17'	3.2. 10.5. F1.3 6	19.23 Soil/Grd. 20.32 6.15 14.17 8.66 20.83
9+25		06			3.49. 1.42 F0.97 16.24	15.74 6'		15.02 6'	14.54 14 5.78 6.03	14.36 17'		
9+50		06			3.61. 1.24 F0.92 16.12	15.67 6'		14.90 6'	14.43 14 3.98 6.15	14.24 17'	3.4. 5.8 F1.1 6	4.1. 5.8 F1.7 19.6.
9+75		06			3.74. 1.25 F0.99 15.99	15.49 6'		14.77 6'	14.29 14 6.84 6.78	14.11 17'		

"C" Line

1834

Sta.	Slope	Super	R.P.	Toe	Slidr. Hinge	E.P.	Φ	E.P.	Slidr. Hinge	E.P.	Toe	R.P.
10+00		06			387 488 F1.01	15.86	15.36 8		14.64 6'	13.98 17'	4.4 4.4 F0.7 6'	18.64T
10+25					398 508 F1.09	15.74	15.24 6		14.04 6'	13.86 17'	19.73 Sail Crct 20.88T	
10+50		059			412 509 F0.87	15.61	15.11 6'		14.40 6'	13.75 17'	26 4.6 6.0 17'	
10+75 = 1/2 lot on RT		052			419 516 F0.97 04	15.54	15.04 6'		14.41 6'	13.83 17'		
+83.80 = 1/4 on RT					414 536 F1.22	15.59						
10+96.76 E.C.		05					15.10 6'		14.59 6'	14.04 17'	3.8 4.7 F0.7 6'	4.3 4.7 F0.4 17.6
B.M	8.77	2204	407	14.27	Lt. P.I. Linda Vasta 7/1/07		14.27 Plan					

"C" Line

55

23.04

23.017

Sta.	Slope	Super	R.P.	Toe	Shldr. Hinge	E.P.	E	E.P.	Shldr. Hinge	F.P.	Toe	R.P.
11+25					curb	15.53 29.51'		14.96' 6'	14.41 17'			18.647
11+50						15.83 28.24'		15.38 6'	14.83 17'	38' 7.7 1.6 F39 5	8.2 1.6 F39 38.1	
11+75						16.24 26.96'		15.89 6'	15.34 17'		0.1	
12+00						16.78 25.68'		16.46' 6'	15.91 17'	6.6 1.6 F8.0 6	7.1 1.6 F7.5 38.2	
12+25						17.44 24.40'		17.14' 6'	16.59 17'			

"C" Line

23.04

Sta.	Slope	Super	R.P.	Toe	Curv	Slidr. Hinge	E.P.	¢	E.P.	Slidr. Hinge	Toe	R.P.
12+50			BM 22.25 66 23.01		18.74	4.27 5.36 F1.29	18.24 23.12'	2.88 2.25 2.73	17.95 6'	17.40 17' 17.93	5.5 14.5 F9.4 30.4	18.61 17.32 BM 17.32 19.35
7.60		R/S	5.2									0.91 3.34 F2.12 18.5
12+75					19.56	3.45 4.88 F1.43	19.06 21.84'	2.05 2.25 2.30	18.78 6'	18.23 17'		
13+00					20.33	2.78 4.13 F1.35	19.83 20.56'	1.25 1.33	19.56 6'	19.01 17'	4.0 12.8 F8.8 30.2	S.C. at 12.9 20.87 0.81 20.22 5.60 2.562 2.323 BM 22.37 11.88 22.35
13+25					21.03	1.99 3.21 F1.23	20.53 19.28'	0.55 2.25 2.20	20.28 6'	19.73 17'		
13+50					21.16	1.35 2.28 F1.38	21.16 18'	4.28 4.7	20.92 6'	20.37 17'	2.1 10.1 F8.0 38.1	
13+76.27					22.29	0.72 1.88 F1.10	21.79 18'	4.07 4.25 4.33	21.55 6'	21.00 17'		
14+00					22.80		22.30 18'	3.56 2.25 3.8	22.06 6'	21.51 17'	1.0 19.9 F8.9 37.6	1.5 9.7 F8.1 37.6
7.25					23.18		22.68					
BM					0.67	22.37	N.E. BP Cor. at Wing Ho of Bridge 22.35 P10					N.E. BP Cor. Wing Ho of Bridge

"D" Line

1951X

Sta.	Slope	Super	R.P.	Toe	EP	Shdr. Hinge	E.C.	±	E.C.	Shdr. Hinge	Curb	Toe	Hinge
8+75				41 52 F1.1 247	36 52 F1.6 72	15.38 23'	15.93 12'	4.19 4.35 4.74 4.72 12	16.12 12'	3.93 4.74 F1.27 12	16.62 12	3.99 4.26 F1.37	19.05X S.C. on St 20.13X
9+00				42 58 F1.1 254	36 58 F2.2 72	15.34 23'	15.89 12'	4.23 4.35 4.78 4.78 12	15.99 12'	3.06 4.85 F1.52 12	16.49 12	3.33 4.33 F1.29	
9+25				42 52 F1.2 243	37 54 F1.7 72	15.27 23'	15.82 12'	4.30 4.35 4.54 4.54 12	15.87 12'	3.18 4.62 F1.24 12	16.37 12	3.34 4.57 F1.23	
9+50									15.74 12.55'	3.31 4.70 F1.39 12.55	16.24 12.55	3.47 4.82 F1.15	
9+64.29 = A 02 Pt									15.64 14'	3.41 4.81 F1.20 14	16.14 14'	3.57 4.72 F1.16	
9+74.31 = A 02 St.					3.34 3.99 F0.65	Curb 16.11 14'	15.61 14'						
10+00			17.45X		3.99 4.16 F0.47 14 C6.225	15.96 14'	15.46 14'						BM 14.27 6.79 21.06X
10+12.67						04'			15.45 12'	3.49	15.96	5.69 6.92 F1.84	
10+25					3.69 5.03 F1.34	15.76 14.78	15.26 14.78		15.35 12'	3.60	15.85	5.21 7.71 F2.50	

"D" Line

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	E	E.P.	Shdr. Hinge	Curb	Toe	R.P.
10+49.07 =	18 on lt				Curb 15.61 17	15.11 17'						BM 14.84 x top H 14.10 10+754 8.07 23.93
10+50		BM 14.84	x on top H 14.10 10+754					15.23 12'		15.73 12'	5.23 7.17 F1.81 12	
10+75	✓							15.16 12'		15.66	5.40 8.81 F1.71	7.27 7.95 F0.18
10+93			4.70 stake	15.09	18 15.73 5. F0.15	4.61 4.86 F0.05						
11+00								15.22 12'		15.78	5.34 6.70 F1.08	7.25 7.85 F0.14
11+25								15.41 12'		15.91	5.15 6.70 F1.08	7.02 7.51 F0.47
11+50								15.71		16.21	4.85 5.89 F0.74	6.72 7.58 F0.56
11+75								16.15 12'		16.65	4.41 5.22 F0.73	6.28 6.89 F0.61

Linda Vista Road Lt. East

Rt. West

Sta.	Slope Super	R.P.	Toe	F.P.	Slidr. Hinge	E.P.	±	F.P.	Slidr. Hinge	F.P.	Toe	R.P.
		17.39										
6+25	Soil Cr. 17.90 4.27 13.63 4.88 18.51				12.89 37'	510 527 F117 12.44 26'	14.28 14.19	509 527 F118 13.45 26'	12.90 37'	5.65 25 570		
6+50			4.3 4.1 Co.3 37.2	3.8 4.1 Fo.3 26	12.99 37'	496 500 519 F119 13.54 26'	14.28 14.30	498 512 F121 13.56 26'	513.01 37'	3.7 4.6 Fo.9 26	4.3 4.6 Fo.3 37.5	out 12.84 14.1 17.28
6+75					13.14 37'	421 F122 13.69 26'	14.43 14.45	483 F124 13.71 26'	13.16 37'			
7+00			4.0 3.8 Co.3 37.2	3.4 3.8 Fo.4 26	13.30 37'	495 F126 13.85 26'	14.43 14.46	489 F129 13.92 26'	13.37 37'	5.1 5.4 4.5 Fo.1 26	3.9 4.5 Fo.6 37.9	out
7+25					13.52 37'	488 F131 13.87 26'	14.86 14.89	489 F130 14.15 26'	570 37'	4.25 5.2		
7+53.55 Back			4.0 4.0 Co.3 37.1	3.4 4.0 Fo.6 26	13.34 37'	491 F133 13.89 26'	15.11 15.16	483 F137 14.41 26'	13.86 37'	3.9 3.7 Fo.8 26	3.4 3.7 Fo.3 37.5	
7+95.6 A' Ahead												
TP	6.09	19.38	4.00	13.29								
8+25					13.42 28.52	494 F139 13.97 17.52	15.11 15.16	483 F137 14.87 6'	15.27 37'	4.08 3.76 F1.68		14.84 4.61 19.45
8+50			5.1 5.7 Fo.7 37.7	5.0 5.7 Fo.7 78	13.84 27.37	493 F141 14.39 16.37	15.11 15.16	388 F145 15.07 6'	15.57 8'	4.31 5.61 Fo.12		14.84 4.66 19.70
8+75		out			13.87 25.54	409 F147 14.42 14.54		373 F149 15.22 6'	15.22 6'	3.73 3.73 Fo.76	F1.16	

"A" Line

Lt = F

Rt = W

43

19.38

Sta.	Slope	Super	R.P.	Toe	EP	Slidr. Hinge	EP	E	EP	Slidr. Hinge	EP	Toe	R.P.
9+00				5.3. 5.8 F0.5 23.9	4.8. 6.8 F1.0 12.06	14.06 23.06	14.61 12.06		15.33 6'		14.05 5.50 F1.15 6'	15.83 6'	3.62 2.92 F1.25 19.45
9+25	3M	14.84	X TOP H 10+754			14.23 20.76	14.72 9.76		15.40 6'			15.90 6'	3.55 4.73 F1.12
9+50	6.8	out		5.1. 5.9 F0.8 20.2	4.5. 6.9 F1.4 8	14.31 19.02	14.86 8.02		15.42 6'		3.91 5.42 F1.50 6'	3.83 4.92 F1.42 6'	X TOP H 10+754 14.84 6.39 21.73
9+75						14.34 17.81	14.89 6.81		15.41 6.01			3.51 3.43 F1.91 6.01	1.59 6.01
10+00				5.1. 5.7 F0.6 18.0	4.5. 6.7 F1.2 8.4	14.32 17.14	14.87 6.14		15.35 6.72	cb in	4.03 5.29 F1.26 6.72	4.17 15.85 6.72	3.60 5.22 F1.62
10+25	14 HCB	50'		4.2. 5.7 F1.2 23.8 Hbd	4.6. 5.4 F0.2 17.3 8k	14.21 17' BK	15.19 22' AHD	14.76 6'	15.32 8.55		10.6 5.02 F0.96 8.55	4.18 5.18 F1.01 8.55	3.63 3.88 5.45 F1.45
10+46.46			Rio of Rt.						15.07 11'			15.57 11'	15.61 5.84 5.84 F1.20
10+50				3.9. 5.4 F1.5 24.3	5.2. 5.4 F0.2 14	15.46 22'	14.23 14'		15.07		4.31 out		
10+75			11.76 of Lt.			15.00 22'	14.17 14'		15.05 6'				

"A" Line

1938

Sta.	Slope	Super	R.P.	Toe	E.P.	Shdr. Hinge	E.P.	Carb φ	E.P.	Shdr. Hinge	Carb	Toe	R.P.
11+00				4.3. 5.2 F09 337.	5.2. 5.2 0.0 14.	15.06 22'	14.23 14'	5.10 5.8 5.878 14.90 6.53 7.39 F0.86 382	15.11 6'				21.45
11+25 TP	6.54		20.81	5.11	14.27	15.24 22'	14.41 14'	5.08 6.35 7.50 F1.03 5.08 F0.28	15.29 6'				22.92
11+50				5.3. 10.2 F1.9 294.	6.2. 10.3 F4.0 14	15.49 22'	14.66 14'	15.33 6.10 6.26 F0.16 4.9 49.02	15.54 6'				
11+75						15.98 22'	15.15 14'	15.82 5.41 6.06 F0.45	16.03 6'				Carb graph. 21.06
12+00				4.3. 11.8 F7.2 32.8.	5.1. 11.5 F6.4 14.	16.53 22'	15.70 14'	16.37 5.06 5.20 F0.61	16.70 18'		17.20 18	23.1 5.25 F0.13	
12+25						17.21 22'	16.38 14'	17.05 4.88 4.89 F0.42	17.38 18'		17.88 18	2.8 1.6 F1.22	5.05 5.72 F0.87
12+50				2.8. 11.4 F8.1 349.	3.6. 11.4 F7.8 14.	18.02 22'	17.19 14'	17.86 3.57 3.94 F0.32	18.19 18'		18.69 18	2.37 3.70 F1.23	4.24 4.44 F0.20
12+75						18.85 22'	18.02 14'	18.49 3.74 3.07 F0.33	19.02 18'		19.52 18	1.54 2.1 F1.34	3.41 3.81 F0.40
13+00				1.7. 6.3 F5.2 30.	2.0. 6.5 F4.5 14	19.63 22'	18.20 14'	19.47 1.96 2.22 F0.33	19.80 18'		20.30 18	0.76 2.10 F1.34	3.63 3.97 F0.41

"A" Line

20.81

Sta.	Slope Super	R.P.	Toe	E.P.	Shdr. Hinge	E.P.	Carb	†	E.P.	Shdr. Hinge	Carb	Toe	R.P.	
13+25					20.35 22'	19.52 14'	20.19	1.24 1.27 F023	20.57 18'		21.02	0.54 1.26 F1.76	1.91 2.28 F0.37	21.06 T 1.20 1.28 5.26
13+50			-0.3 5.2 F5.6 29.4	+0.6 5.2 F4.7 13'	21.07 21'	20.24 13'	20.91	0.53 0.79 F0.27	21.16 18'		21.66	4.13 F0.76 F0.77	1.27 1.23 2.58 3.27 3.11 2.23 5.80 1.1 8.10	
13+76.03	F.C.				21.90 18'	21.07 10"	20.74	4.14 1.57 F0.43	21.79 18'		22.29	3.53 F1.70	0.64 1.73 F1.08	
14+00			-2.0 4.7 F6.7 25.1	-1.1 5.8 F5.8 7	22.77 15'	21.94 7'	22.61	3.22 1.05 F0.78 3.55 23.27 2.61	22.30 18'		22.80		21.23 T 0.77 2.06 5.24 2.58 2.37 BP.22 1.13 2.38	
7+78 B.C.					19.51 Bt Ford Page 38									
8+00					3.70 5.51 F1.81	15.58 12		4.46 1.73 F0.78	14.64 12'	14.09 23'		4.9 5.9 F1.0 12.	5.4 5.9 F0.5 23.8.	2/land 19.28
8+25			Change		3.50 5.58 F1.98	15.78 12		4.20 1.25 F0.85	15.10 12'	14.65 21'		4.3 5.3 F1.3 12	4.9 5.7 F0.8 22.2	
8+50					3.34 4.89 F1.55	15.94 12.cb		3.80 1.05 F0.75	15.30 12'	14.85 21'		4.2 5.8 F1.6 12	4.7 5.7 F1.7 22.7	
8+73.73 P.C.					3.23 4.86 F1.63	16.05 13		3.66 1.25 F0.75	15.44 12'	14.99 21'		4.1 5.0 F1.3 12	4.5 5.9 F1.9 23.1	

"B" Line

19.5T

Sta	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	±	E.P.	Shdr. Hinge	Toe	R.P.	
9+00	✓				^{3.15} 4.77 F1.52	15.63 12'		^{3.54} 3.79	15.56 12'	15.11 21'	^{4.0} 2.0 F1.0 12'	^{4.1} 1.6 F1.6 234
+13												3 1/2 19.10T
9+25					^{3.13} 4.64 F1.51	15.65 12'		^{3.54} 3.78	15.59 12'	15.14 21'		
9+50.11		△ Curb			^{3.55} 4.70 F1.65	15.61 12'						
9+64.80								15.64 14'		16.14 14'		15.1000 19.7T
9+75								15.57 12.87'		16.07	^{3.64} 2.05 F0.91	
					Curb							
10+00.09				21.06T	15.96	15.46 14'		15.45 12'		15.95	^{3.76} 5.02 F1.33	
10+25					^{5.22} 6.95 F1.73	15.34 12.06'		15.33 12'		15.82	^{3.88} 4.87 F0.99	
10+50					^{3.34} 6.75 F1.41	15.22 12'		15.21 12'		15.71	^{4.00} 4.99 F0.99	
10+75					^{5.38} 6.84 F1.46	15.18 12'		15.12 12'		15.62	^{4.09} 5.12 F1.03	
10+82.08								15.09		15.59	^{4.11} 5.54 F1.43	

"B" Line

June 12-52

H. Sisson
Garber
Rorer
Fritz

47

Sta.	Slope Super	R.P.	Toe	E.P.	Slidr. Hinge	E.P.	¢	E.P.	Slidr. Hinge	E.P.	Toe	R.P.
11+00					Curb 5.74 15.82 12.1097	15.32						
11+10		17.68		14.11	14.11							
N.F. Return	Mid. Point	3.8		3.2	13.89	14.44						
	R103.65											
	Curb Grade	F2.2 3.6										
0+82.52	EC on R103.65	4.13 2.99 14.57	3.1	3.5	14.58	14.23	14.51					
					23'	12'						
S.F. Return	Mid. Point				14.54	14.11	14.44	14.09	14.43			
	R116.59				24.24	12'		12'				
1+23.96	EC on R116.59	4.18 3.07 14.46	3.1	3.6	14.54	14.09	14.32	14.29	14.88			
					26	12		12	26			
1+25					14.52	14.07	14.34	14.29	14.34			
					26'	12'		12'	26'			
1+50		4.35 3.20 14.39	3.3	3.7	14.41	13.98	14.24	14.18	14.75			
					26'	12'		12'	26'			
+75					13	13.89	14.04	14.07	14.34			
2+00		4.54 3.29 14.12	3.4	3.9	14.24	13.80	14.04	13.96	14.52			
					26'	12'		12'	26'			
+25						12.71	14.04	13.85	14.04			

Rt = Souths
Curb Gr
Scot 2.52
Curb Staln.
RM 14.11
18.52
18.647

13.56
2.08
17.647

3.88
4.87
14.76
2.99

4.01
4.86
14.63
F0.85

14.10
1.24
5.12
F0.88

Napa Street

Lt. North

Rt. South

Cont. Station
18.64T 48.

17.68

Sta.	Slope Super	R.P. Curb Grade	Toe	E.P.	Shdr. Hinge	E.P.	E	E.P.	Shdr. Hinge	E.P.	Toe	R.P. Curb Grade
2+50		^{4.69} 5.32 F0.73 13.95.	3.6. F2.4 296.	4.1. 5.6 F1.9 12	14.07 26'	13.62 12'	13.84	13.74 12'	14.29 26'	3.9. 5.0 F2.1 12	3.2. F2.6 299.	4.4. 5.35 F0.88
2+75	5.44	17.72	6.00	11.65		13.53 ^{4.11} 4.35		12.67	14.05 26'			17.64T
3+00	5.94	17.12	6.00	11.88		13.44 ^{4.10} 4.35	13.64	13.52 12'	14.06 26'	3.6. 5.3 F1.7 12	3.1. 5.5 F2.2 293.	4.70 5.62 F0.72
3+25						13.35 ^{4.39} 4.57		13.41	14.23 26'			
3+50		^{5.03} 5.62 F0.59 13.61.	3.1. F4.2 323	3.9. 7.6 F3.7 12	13.73 26'	13.25 12'	13.44	13.31 12'	13.83 26'	3.8. 5.2 F1.4 12	3.3. 5.2 F1.9 289.	4.25 5.63 F0.70
4+75	For Check		3.86	13.26	P.R. Nail P.L. Under Nails +4.00 13.24	13.16 12'		13.20	14.1. 4.35 26'			
4+00		^{5.20} 5.78 F0.78 13.44.	3.6. 3.7 F5.1 33.7	4.1. 8.7 F4.6 12	13.56 26'	13.07 12'	13.24	13.09 12'	13.60 26'	4.0. 5.1 F1.1 12	3.5. 5.1 F1.6 284.	5.6. 5.62 F0.52
4+25					13.47 26'	13.01 12'	13.14	13.01 12'	13.51 26'			
4+41.88	BC on Rt	^{5.35} 5.20 0.27 13.29 = Top in bl.	4.6 6.0 F0.5	4.1 2.6 F0.5 1.1	13.56 23'	12.00 12'	13.00	13.00	13.45 26'	4.1. 5.8 F0.7 12	3.7. 4.8 F1.1 297.	5.9. 5.69 F0.38
4+59.46	BC on Lt				12.56 23'	12.00 12'	13.15					
4+75	Return Midpoint				13.16	13.21						

Sherman St.

B.M. 228 16.39
 Sta. Slope Super RP. Toe
 Lt. South
 Chicago
 100' RP. 2x
 50' RP. 1x
 1.78 x 2.97 Pro
 Slide Hinge

Willy Line Morena 0+50	SM 11.11 Above 3.52 17.64x	2.2 3.9 F.O. 8 12 = NSB in From Radius	476 136 47	14.21 21.30'	14.53	14.10 21.30'	182 25 5.07	2.3 5.5 F. 32 18 From 20' R	Soil On 18.92x
0+61 = 80' R. 1st	x	26 70 F. 4.4 37.6	5.13 25 5.38	13.79 21'	14.23	4.76 25 5.81	13.79 21'	5.13 2.6 2.4 F. 2.7 25.1	5.9 6.9 F. 2.1 24.1
0+78.40	out	5.86 6.11	13.06 21'	13.60	5.39 out	13.06 21'	5.86 25 6.11		
0+91.17 80' 1st		3.8 8.8 F. 5.0 28.5	6.37 26 6.63	12.55 21'	13.09	5.90 25 6.15	12.55 21'	6.37 25 6.62	5.1 7.4 F. 2.0 24.0
1+14.24	5° 17.23' →	4.7 7.8 F. 3.1 25.7	7.21 26 7.46 8.24 F. 0.78 120' INC	11.71 21'	12.25	6.74 25 6.99	11.71 21'	7.21 25 7.46	4.7 8.7 F. 1.0 27.0 814 14.11 4.88 18.99
1+37.32	10° 34.10' →	5.4 7.5 F. 2.1 24.2	7.23 25 8.18	10.99 21'	11.53	7.46 25 7.71	10.99 21'	7.23 25 8.18	5.4 8.7 F. 2.0 25.5
1+60.40 E.C.	15° 35.2'	5.4 6.9 F. 1.5 25.3	8.52 25 8.77	10.40 10.95 23'	10.94	8.04 25 8.29	10.95 23'	8.52 25 8.77	5.4 8.5 F. 1.1 27.7
1+78.40	out		10.48 23'	10.27	10.48 23'				
1+98.40		6.4 8.8 F. 0.4 23.6	10.02 23'	9.81	10.02 23'			6.4 8.5 F. 2.1 26.2	
TP	3.81	13.52	6.88	9.51					

Rt = North
 June 9 - 52
 45' 10" on
 Garber
 Part
 F. 1.2

E.P.	£	E.P.	Slide Hinge	Toe	R.P.
14.21	14.53	14.10			
13.79	14.23	13.79			
13.06	13.60	13.06			
12.55	13.09	12.55			
11.71	12.25	11.71			
10.99	11.53	10.99			
10.95	10.94	10.95			
10.48	10.27	10.48			
10.02	9.81	10.02			

Sherman St.

12.32

Sta.	Slope	Super	R.P.	Toe	Slide Hinge	E.P.	φ	E.P.	Slide Hinge	Toe	R.P.
2+18.40		out			9.62 23'		9.41		9.62 23'		
2+38.40					9.30 23'		9.09		9.30 23'	4.0 5.6 F 1.6 35.4	
52.91											
2+90.81					8.54 23'		8.33		8.54 23'	4.8 4.8 0.0 3.8	

Morena Blvd.

10' Carb

Sta.	Slope	Super	R.P.	Toe	Slide Hinge	E.P.	φ	E.P.	Slide Hinge	Toe	R.P.
24+18 = 51' Bridge											
24+25					29.47 37'		28.87		28.63 26'		
25+00					29.57 39'		28.99		28.75 26'		
25+25					29.69 41'		29.12		28.88 26'		
25+50					29.79 43'		29.23		28.99 26'		

2917 - Enites
 29.45
 29.37-06
 29.49-05
 29.62-04
 29.72-04

2917-54
 50.8
 32.62

R.P.C.B.
 Morena Blvd.
 10.54
 5.27
 13.81
 35.2
 12.28
 7.76
 20.04

2 Mo. -
 10.54
 5.27
 13.81
 35.2
 12.28
 7.76
 20.04

Morena Blvd.

10.047

Sta	Slope	Super	R.P.	Toe	F.P.	Slide Hinge	E.P.	±	E.P.	Slide Hinge	Toe	R.P.
25+75			8.6 8.2 +0.2 82.6	-9.8 8.6 F18.4 72.6	-9.0 8.6 F17.6 36	29.85 29.87 45'	29.94 29.97 36'	29.83 29.32	29.80 29.18 26'	29.33 41'		
26+00						29.83 47'	28.98 36'	29.66 29.30 29.60	29.24 29.06 26'	28.16 44'		
27+00						28.74 45'	27.93 41' 38'	28.65 28.63	28.35 28.35	28.47 28.47		
27+31.73	49.5	11.86	4.2 4.2 86.1	-16.0 4.2 F18.3 76.1	-15.2 2.06 F19.3 38.8	27.81 45.80'	27.00 38.80'	27.66 2.21	28.26 38'	28.44 49'		
27+50	26.70	out				27.22 46.50'	27.26 39.50'	27.72 26.6	27.72 26'			
27+75	35.95	17.849		-14.5 14 F18.9 75.4	-13.7 24 F18.1 40'	26.40 46.97'	25.59 39.91'	27.07 26.57	27.19 26'			
28+00	25.17		4.6 4.7 84.5	-13.7 4.6 F18.3 74.5	-13.9 4.6 F17.5 40'	25.58 47'	24.77 40'	26.35 25.85 4.02	26.53 26'			
28+25	24.33	out				24.73 47'	23.92 40'	25.53 25.03	25.73 26'			
28+50	23.45		4.5 4.4 86	-12.0 4.5 F17.5 71.8	-11.8 4.5 F15.7 40'	23.86 47'	23.05 40'	24.13 24.13	24.93 30.26'	25.19 37'		

Co. Grade
28.35
1.81
30.16X

27.56
20.1
27.55
27.54

Morena Blvd.

Sta.	Slope	Super	R.P.	Toe	E.P.	Slidr. Hinge	F.	P	¢	E.P.	Slidr. Hinge	EP	Toe	Hinge
			11.86											
28+75	22.53	26	out			22.96	22.84	17	23.15	23.83	24.11		cb Grade 30.16	29.87
						47'	40'			28.15'	37'		12.86 17.30 17.63 17.93	
28+97.42 EC	21.18	26		-1.04	-9.1	22.21	22.09	40	22.20	22.77	22.96	-10.9°	-1.1	17 SW 12
				4.6 4.6 0.0	7.66 7.66 7.66	47'	40'		7.82	28.42	37'			
29+23	20.62	26	out			21.47	21.02	33	21.01	21.40	21.87	-10.0	-9.5	PI. Slope 1+95 SW 12
						47'	40'			32.25	37'		58.6	
29+41	19.83	26		-8.5	-7.7	20.36	20.22	35	20.14	20.49	20.52	-8.6	-8.7	50
				4.7 4.7 0.2	7.5 7.5 7.5	47'	40'		9.73	35.33	38.5'	9.35	13.1	29 29 29
29+50.60	out							out	19.66	19.96		out		W. Edge 17.15 16.85 16.80 12.96 29.56
29+66	18.63	26				18.79	18.79	63	18.89	19.02	19.02	out		
TP	4.04		11.01			4.89	6.97							
29+73.60	out								19.01	18.51	18.20	out		
											49'			
29+80.97	21.50	26		-6.1	-5.0	17.98	17.98	89	18.15	18.15	17.71	-6.3	-5.9	49
				4.6 4.6 0.0	7.6 7.6 7.6	47.4	49.4			38'	49'	38	10.8	5.3 5.3 5.3
30+00	20.10								17.69	17.04	16.54	-6.0	-5.5	4.5
									2.91	38'	49'	38	6.4	7.1

Marena Blvd.

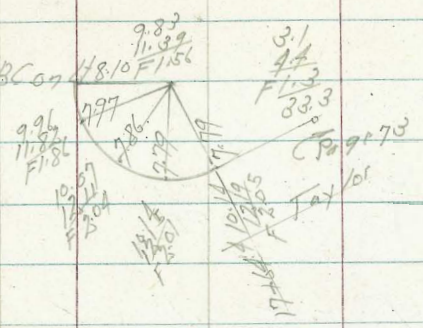
11.01

Sta.	Slope	Super	R.P.	Toe	Slidr. Hinge	E.P.	E	F.P.	Slidr. Hinge	F.P.	Toe	R.P.
30+21.17	20.10T 8.61 11.49 2.24 13.93T				158° 258 F1.00.	16.33 15.85 28'	16.63-cb 16.13 16.30-cb F1.31-cb				17.93T	W. Edge 17.45 4.65 TP16.80
30+25					out	15.66 28'	15.94 1.29 16.44-cb out 3.05	15.65 38'	15.10 49'		out	
30+50				-4.1 4.1 F0.82 70.3	curb 302 3.67 F0.65.	14.91 14.41 28'	15.19 14.69 5.41 3.27-cb F0.88.	14.34 38' 3.16 33%	13.80 49'	6.36-0.3 4.9 F0.77 38	-3.8 3.2 -7.3 39.8	4.4 10.3 89.8
30+75					4.27 5.15 F0.85.	13.66 13.16 28'	13.94 13.44 3.22 F0.94-cb	13.08 38'	12.53 49'		out	
31+00	490			-1.8 1.8 F0.87	-1.2 3.2 F1.1 34.6	curb 532 6.37 12.58 28' F0.88.	8.19 12.41 11.91 28'	12.19 12.19 7.91	11.83 38'	11.28 49'	2.65-0.5 5.0 F0.55 38"	10.1 5.0 F0.49 56.4
31+25	5-12		11-38		6.26 6.30 F1.1 8.17	6.26 6.30 F1.1 8.17	8.02 11.16 10.66 28'	11.44-cb 10.94 6.42-cb 7.77	10.58 38'	10.03 49'		
31+50				4.71	6.30 +1.3 4.8 F2.7 (32)	6.30 6.30 F1.1 8.17	9.02 10.19 10.66 28'	10.19 9.69 4.21	9.47 26'	5.58 2.5 3.8		7.27 5.76 12.05T
31+60					8.52 9.50 F0.98.	9.41 8.91 28.29'	9.69 9.19 8.75 F0.91-cb	9.03 26'		out		
31+78.47					5.86 9.36 10.65 F1.90	5.86 9.36 10.65 F1.90	8.57 8.07 29.57	8.87 8.37 5.55 9.06-cb 10.21 F1.15.	8.33 26'	1.72 6.5 4.93		

Moreno Blvd.

11638

Sta	Slope	Super	R.P.	Toe	Side Hinge	E.P.	E	E.P.	Side Hinge	E.P.	Toe	R.P.		
31+90.91	= CB	BC on	48.10	F156	8.27 ^{cb}	7.60						17.93 ^T 10.17 ^{CP} BM 7.77 ^{CP} SF 8P Chapin Taylor		
32+00							8.14 ^{cb}			5.37 ^T 2.5 ^T 5.63 ^T		12.05 ^T		
32+10.27	= CB	BC				7.93 ^{cb}						7.29 ^{CP} 16.16 ^T 17.45 ^T		
30+90	= BC									12.33 ^T 2.4 ^T 5.37 ^T				
31+00					12.67 ^T	12.19 ^T				23.28 ^{out}				
32+40										6.99 ^T				
31+25					11.41 ^T	10.94 ^T				1.68 ^T 2.7 ^T 6.7 ^T	10.76 ^T	21.77 ^{out}		
31+50					18.19 ^T	7.26 ^T				7.92 ^T 8.7 ^T	9.55 ^T	9.11 ^T 18.47 ^T 17.06 ^T	482 ^T 1.8 ^T 4.9 ^T F 3.1 ^T 18.5 ^T 2.3 ^T 2.9 ^T F 2.6 ^T 33.6 ^T	
31+75	BM	6.27	on a whitman & Taylor P 99.11	6.25	8.83 ^T	9.13 ^T				9.92 ^T 9.37 ^T	8.43 ^T	8.11 ^T 16.06 ^T 17.85 ^T	24 ^T	
32+00					8.18 ^T	9.26 ^T				9.98 ^T 10.23 ^T	7.47 ^T	7.44 ^T 14.57 ^T 16.04 ^T	7.44 ^T 17.57 ^T F 0.9 ^T 7.6 ^T F 0.9 ^T 7.9 ^T	
32+27.73	= PCC				7.68 ^T	3.03 ^T					6.80 ^T	6.65 ^T 14 ^T	7.41 ^T 17 ^T 6.52 ^T 4.7 ^T 5.6 ^T F 0.9 ^T 7.4 ^T	4.2 ^T F 1.5 ^T 1.9 ^T



"E" Line

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	±	E.P.	Shdr. Hinge	E.P.	Toe	R.P.
			11.38									
32+50.73	Right				7.25 12' 0"	3.16 2.56 12.75 F0.29 12.75 H.C.		6.20 14'	6.99 20'	5.3 5.3 F0.14 14	1.1 1.1 F0.9 21.4	17.45
32+75			6.25 3.96 10.21X	4.5 10.1 Shiphitman	3.66 3.89 F0.23 H.C.	6.55 12'		5.85 14'	6.64 20'			
33+00					3.82 3.89 F0.07 H.C.	6.39 12'	6.18	5.49 14'	6.28 20'			
33+17.95 EC	10.81		21.35	10.54	3.88 3.91 20.08 + Marc + Camino + Marcos	6.33 72	6.10	5.63 14'	6.42 20'			8 P. EC Marcos 35 So. Overpass BM 27.54 5.00 32.54
BM	N. W.	Outer	Connection		0.7 M.H.P. on 8 ft. bridge 40 overpass 9283-49							
BM	0.24		23.56	23.32								
0+00	0.24			2'				28.42 8'	28.07 15'		2.81 out	
0+25			For high 28.28 25 120 155 3.2	on overpass				40.5 28.49 8'	27.94 19'	3.94		
0+50			Finish Grades 27.54 B.P. EC Marcos 4.34 31.88X	35 So. Overpass				41.0 28.44 8'	27.89 19'	3.78 4.5 F1.23 8	6.5 4.2 F1.07 35.1 31.4 30.4	
0+75		0.364			3.51 1.61	3.15 28.73 6'	0.51 1.59	4.22 28.22 8'	27.67 19'	4.31		
+85									27.49	For high 30.1		
1+00		0.75			4.00 2.25 4.25	3.34 28.54 6'	4.22 5.09	4.22 27.75 8'	27.20 19'	4.22 F1.03 8	6.4 3.2 F1.23 8	3.6 2.6 F1.23 33.6 32.9

N.W. Outer Connection Lt.S.

Rt-N

36

Sta.	Slope	Super	R.P.	Toe	E.P.	Slide Hinge	E.P.	±	E.P.	Slide Hinge	E.P.	Toe	R.P.	
			23.56											
			31.35 X #2											
1+25	.075		For Light 32.55 X		28.55 11.27'	11.27' 4.4'	28.32 8.27'	5.16 5.89	27.10 8'	26.28 19'	5.60			
1+50			Finish Grade 31.88 X 11.20 27.8' Sub 20.28 27.8' 19.2'		27.91 11'	5.26 5.27	27.50 6'	6.19 5.71	26.35 8'	25.45 19'	6.13 -2.8 5.37 5.87 5.8	5.6 -1.9 5.7 5.7 29.7	-1.1 -3.7 -3.7 30.7	
1+75		Sub Grade	32.65 X 10.08 21.28 22.70 X		26.99 11'	7.39 6	26.60 6'	7.04 7.29	25.50 8'	24.64 19'	7.24 -1.9 6.5	2.7 out 6.8 2.7	8.74 10.5 5.2 16.34 -2.5 4.3 6.8 29.2	
2+10.12			For Light		25.88 11'	7.39 6	25.54 6'	7.95 8.29	24.59 8'	23.84 19'	8.04 -3.3 7.3 7.3	-0.3 6.8 2.7	16.34 -2.5 4.3 6.8 29.2	
2+10					24.72 11'	7.16 6	24.45 6'	8.80 9.05	23.74 7.12'	23.14 18.12'	8.73 -0.8 7.3 7.2	-2.4 7.0 7.2	7.04 6.0 3.7 3.7	
2+23.47 E.C.			-8.4 3.5 F13.7	7.3 F13.9 31.9	-0.9 12.7 F13.6 6	7.16 6	24.45 6'	8.80 9.05	23.74 7.12'	23.14 18.12'	8.73 -0.8 7.3 7.2	-2.4 7.0 7.2	7.04 6.0 3.7 3.7	
2+53.40			-6.8 5.2 F13.3 29.3	4.0 F13.0 29.0	7.0 F13.8 6	8.79 6	23.09 11'	9.58 9.83	22.96 6'	22.64 17'	9.79 +0.9 5.6 5.6	+1.5 6.3 6.3	-0.7 4.8 3.5 3.5	
TP	6.84		18.62	11.78	11.78									
2+75					21.93 11'	10.62 10.92	21.87 6'	10.88 11.07	21.72 6'	21.17 17'				
3+00			-4.2 4.8 F13.5 24.5	-1.9 7.1 F13.0 24.5	-4.3 8.0 F13.1 6	11.33 6	20.55 11'	11.33 2.35 2.3	20.65 6'	20.53 17'	11.33 11.90	19.98 17'	1.9 10.8 5.9 5.9 7.4 7.4 25.7	+1.4 5.6 4.5 3.8
3+25					19.26 11'	11.33 6	19.51 6'	11.33 11.33	19.39 6'	18.84 17'				

N.W. Outer Connection

R.T.N

18.62

Sta.	Slope Super	R.P.	Toe	E.P.	Shdr. Hinge	E.P.	¢	E.P.	Shdr. Hinge	E.P.	Toe	R.P.
	Sub Grade	21.35T #2										
3+50	22.76T	-20.37 F57 196	-2.7 F50 Rao	3.8 F57 6	-22 F52 6	4.39 18.57 6'	436 18.45 6'	17.90 17'	4.85 F53 6	22 F56 6	+0.7 F58 276	-16 F58 30.2
5	#3											
+75	BM 10.54	2.53 18.07T				196 53 17.80	308 53 17.68		3.9 F56 6		5.5 F56 306	
4+00	Finish Grade	21.65T	-2.7 F52 758	1.6 F52 6	-0.9 F52 6	4.1 F52 6	5.5 17.25 6'	5.8 17.13 6'	6.07 16.58 17'	1.5 F52 6	-0.8 F52 30.1	-2.3 F52 29.8
+25		20.87 12.66 32.47T				5.82 16.93	5.25 16.81					
4+50	on Grate	21.19T 2.84 16.05	+2.0 F54 716	1.8 F54 6		6.05 16.60 6'	6.03 16.73 6'	6.13 16.18 17'	6.13 16.18 17'	1.91 F54 6	2.4 F54 35.1	1.9 F54 27.5
+75						5.22 17.02	5.26 16.90 6'					
+83.81				1.91 9.55	5.84 curb 6.34 F570	17.85	17.18					
5+00				1.1 out	5.53 curb 6.25 F570	18.16	17.49 6'	5.88 17.37 6'	5.78 16.87 16'	1.3 F570 6	1.8 F570 16.1	1.3 F570 30.0
7+28.81	fly Co of R.H. to fly Co of L.H.				curb 18.75 18.83		18.28	18.15 8	18.82 curb 18.1			
5+50		11.89	28.71	7.80	16.82		19.04 6'	18.81 8'	19.60 14'	30.5 -0.7 99 F570 8	9.1 16.3	7.5 F570 30.5

Camino Del Rio

18.34

59

Sta	Slope	Super	R.P.	Toe	EP	Shldr. Hinge	E.P.	φ	E.P.	Shldr. Hinge	Toe	R.P.
72+27.5	0°	42.97		-14.1 3.5 F 17.6 6.59 0.4	-13.3 3.5 F 16.8 33.5	32.42 39.50	105 31.63 33.50 33.25		32.30-d 31.94 32.6 14.6 F 6.64			
72+52.5			Finish Grader 33.177 4.73 289	out		266 30.81 44.38	30.02 38.38 38.72		38-69-c6 38.40 5.30 5.68 F 6.30			
72+77.5	EC	28.84	on 2 Hub 72+77.5 R.P.	-10.9 F 19.2 40'	-10.6 F 19.9 40'	426 29.21 46'	28.42 40'		27-07-c6 28.88 6.22 6.82 0.0			
73+00				-11.1 9.5 F 20.6 76.9	-10.4 9.5 F 19.9 70'	27.83 46'	27.04 40'		27-71-c6 F 0.10			
73+25						26.35 46'	25.56 40'		out			

38.21
12.37
15.94
28.34
18.19
17.15
14.18
29.33
28.23
29.33
27.56
28.73

41
289
289

28.71

12.77

S.W. Inner Loop

Lt. East

 June 3-52
 H.S. Brown
 Harbor
 Road
 E.P. 15
 O. S. Brown
 Denote
 Grade 3
 Back of EP

Rt. West

10

Sta.	Slope	Super	R.P.	Toe	E.P.	Shldr. Hinge	E.P.	Φ	E.P.	Shldr. Hinge	E.P.	Toe	R.P.	
B.M.		5.69	15.63		10.54	2 Moog Cambridge + Macanob								
0+00	13.11	0.16					28.07 6'		28.26 6'	28.43 17'		003-12.6. 82 F208. 6'	-128. 82 82 5.0 485. 585.	
						Finis 5 Gr. BP B.M. 27.54 0.92 28.46X								
						Sept. 18 52 Finis 5 Graders on w/er part								
0+50		0083				B.M. 28.47 1.40 29.87X 2.19 20.68 on Feb 177 20' 8" 210 22.75X	27.00 6'		27.10 6'	27.19 17'		127-11.5. 81 F196. 6'	-116. 81 F197 46.6 58.6'	
+75									26.30	26.17			3.7 for 5h.	
1+00		024					25.71 6'		25.42 6'	25.15 17'			4.72 381 -9.8. 82 F180. 6'	-9.5. 82 F187 43.6 53.6
1+07.92		0291					25.63 11'	25.48 6'	25.13 6'	24.81 17'				
1+39.14 B.C.		05					3.60 24.26 11'	24.78 24.61 6'	23.92 7.58'	23.36 18.58			6.51 510 -8.3. 83 F177. 7.72 F167. 22.6	-7.7 83 F160 22.6 56.6
1+66.92		069					5.63 4.22 24.24 11'	24.10 23.89 6'	22.64 22.85 9'	22.09 20'			6.37 7.2. 82 F156. 9'	-6.5 84 F142 42.4 8.4 82 7.2 527
TP		295	11.70	7.88	7.75			23.38	23.41					
2+00		092					-11.8. 4.2 F163 35.8. 8'	-11.4. 4.2 F161. 8'	23.53 11'	23.07 6'			-100. 47 9.19 7.78 9'	-9.0 47 F157 40.6 42 526

S.W. Inner Loop

11.27

6.91 on Rad. Hds P 61 Denoter
 2278x
 11.58x
 Grade 3
 Back of F.P. 82

Sta	slope	Super	R.P.	Toe	F.P.	Slidr. Hinge	E.P.	±	E.P.	Slidr. Hinge	F.P.	Toe	R.P.
4+50		22.45T 10.81 11.64 3.73 15.37	0.12 5.1 5.2 2.0 40.1	-7.5 5.2 F12.7 30.1	-6.9 5.2 F12.1 8	18.81 11'	18.57 18.21 6'		11.05 16.41 9'	786-5.1 15.09 20'	-3.8 4.8 F8.6 32.9	18 out	
4+75		21.38T 0.12	5.0 4.9 40.1 39.2	-7.1 5.0 F13.1 29.2	-6.5 5.0 F13.5 8	18.35 11'	18.11 17.75 6'		15.59 15.95 9'	6.75 14.63 20'	out		
5+00		0.12	4.9 4.9 0.6 38.3	-6.6 4.5 F11.5 28.3	-6.0 4.9 F10.9 6	17.89 11'	17.65 17.29 6'		15.13 15.49 9'	2.28-4.2 14.17 20'	-3.9 2.5 F7.4 31.1	4.5 out 4.1	
5+25		0.12	4.9 4.8 40.1 37.7	-6.2 4.2 F11.1 27.7	-5.6 4.9 F10.5 6	17.43 11'	17.19 16.83 6'		14.67 15.03 9'	7.62 13.71 20'	out		
5+50		0.12	4.8 4.8 10.2 31.8	-5.7 4.8 F10.5 26.8	-5.1 4.8 F9.9 6	16.96 11'	16.72 16.36 6'		14.20 14.56 9'	9.21-5.3 13.24 20'	-3.0 4.8 F6.8 30.2	4.8 out 4.0	
5+75		0.12	R.P. number 4.8 40.1 26.6	-5.3 4.8 F10.1 26.6	-4.7 4.8 F9.5 6	16.50 11'	16.26 15.90 6'		13.74 14.10 9'	8.60 12.78 20'	out		
6+00		0.12	4.7 4.8 40.1 35.3	-4.8 4.5 F9.5 25.3	-4.2 4.5 F8.9 6	16.04 11'	15.80 15.44 6'		13.28 13.64 9'	10.13-3.4 12.32 20'	-1.6 4.8 F5.9 28.9	4.8 out 3.8	
6+25		0.12 out	5.1 4.7 40.1 35	-3.9 4.1 F9.2 25	-3.3 4.1 F8.2 6	15.58 11'	15.34 14.98 6'		12.82 13.18 9'	9.52 11.86 20'	out		
6+50		0.12	4.3 4.2 40.1 32.2	-3.9 4.2 F8.7 23.2	-3.3 4.2 F7.3 6	15.12 11'	14.88 14.52 6'		12.32 12.72 9'	9.98 11.40 20'	-1.0-1.5 F6.1 9	-0.1 4.8 F5.1 26.3	4.8 out 3.8

S.W. Inner Loop

11.68T

Denotes
Grade of
Back of F.R.

63

11.27

Sta.	Slope Super	R.P.	Toe	E.P.	Shldr. Hinge	E.P.	Φ	E.P.	Shldr. Hinge	E.P.	Toe	R.P.
6+75	15.87X 4.28 70.5 0.17	3.6 4.2 6.6 3.5	-3.4 3.6 F7.0 3.5	-2.8 3.6 6	6.7 14.64 11	14.41 14.06 6'		11.96 12.31 9'	4.34 11.83 20'		10.35 out	
7+00	21.28T 9.84 0.107 11.15 3.45 14.99T	3.6 2.3 out 0.7 Fill	-3.1 2.3 F5.9 2.1	-2.3 2.3 F4.6 8	7.03 14.35 13'	13.92 13.60 6'		11.68 12.00 9'	4.04 10.83 20'	0.7 -0.3 4.3 F4.2 F4.6 9	+0.9 +2.3 F3.4 F3.4 2.5 2.5 5.6	2.3 2.3 3.0 3.0 3.0 3.0
7+25	0.092	16.40	3.63	7.64	13.88 14'	13.42 13.14 6'		11.48 11.76 9'	10.75 20'	10.63	out	
7+50	0.75					12.90 12.68 6'		11.33 11.55 9'	4.27 10.72 20'	4.65 4.9 2.5 F4.9 F4.9 9	5.7 7.0 F3.5 F3.5 2.5 2.5	4.5 4.6 4.1 3.0
7+72.90	06					12.44 12.26 6'		11.18 11.36 9'	4.29 10.90 20'	4.9 5.0 8.0 F3.0 9	5.7 8.0 F2.3 2.3 2.5	8.0 8.0 8.0 8.0
7+94.78	EC. 0.08					11.99 11.85 6'		11.03 11.17 7.97'	4.27 10.62 18.97'	5.3 8.7 F3.7 7.97	5.8 F3.1 2.7 3.7	8.9 8.9 8.0 3.7
76+97.47	Camino											
Camino Del Rio												
Finish Grade												
77+37.16	BM 10.13								10.82 38'	10.27 49'		
77+55										(Gut El.) 10.29 49'	3.47	

For Light
BM 10.54
2.85
5.29X

Mon &
Morana
Camino Del Rio
10.54

BM 10.13
3.33
13.76

Camino Del Rio

Sta	Slope	Super	R.P.	Toe	Slide Hinge	E.P.	±	E.P.	Slide Hinge	Toe	R.P.
77+75		13.76%					92.5 42.5	10.49	(Gut El.) 38'		
		2.68							46.58'		
		11.08									
78+00		16.85%					92.5 45.0	10.25	(Gut El.) 38'		367
									44.28		
78+25							442 437	10.08	(Gut El.) 38'		407 959 on Gate Hinge
									42.76'		
78+50				14.50%			440 428	10.01	(Gut El.) 38'		Carb top
				4.07	Conc Mon under				42.06'		
	±60 =	M4 C6 on Rt		10.43	over pass					18.63	313 on top
		"H Type"	3M								
78+75							452 425	9.98			10.65
								39'			
79+00							440 425	10.03			10.70
								39'			3.06 on top
79+25				BM 10.43	Mon under		440 425	10.10			10.77
				4.34	over pass			39'			2.99 on top
				14.70							
79+50							440 425	10.24			10.91
								39'			3.85 out
	±60 =	Fly H Carb on Rt									
79+75							490 425	10.50	Gut El. 38'		3.78 1.62 Fa. 84
									42.52'		2.67

Camino Del Rio

Sta	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	φ	E.P.	Shdr. Hinge	F.P.	Toe	R.P.
80+00	1/2 Start		18.68									
			10.54									
			16.85									
80+25			Nov. 15-53									
			Rx 20.07									
80+50			1.12									
			21.19									
			9.97									
			11.32									
			3.28									
			14.50									
80+75												
81+00												
81+25												
81+50												
81+75												
82+00												

2 Mon
Camino
Morano

Nov. 15-53
R.P. 54 Bridge

8.1
10.9
F3.8
48.5
19.9
-0.2
58.5

(Gut El)
10.73
48.03'

593 7.2
out 11.2
F4.0
38

7.8
11.2
F3.4
54.1
11.2
+0.1
64.1

500 6.3
out 11.0
F4.7
38

6.8
11.0
F4.2
55.3
11.0
-0.2
65.3

404 5.3
11.2
F5.7
38

5.9
11.2
F5.3
57.0
out Under Trailer

308 1.4
11.2
F6.8
38

1.9
11.2
F6.3
58.5
out Under Trailer

Camino Del Rio

Lt. North

SE 1/4 June 2-52

pt. South

66

Sta	Slope	Super	R.P.	Toe	Slidr. Hinge	E.P.	¢	E.P.	Slidr. Hinge	TOO	R.P.
			16.857								
82+11.17								14.53 38'	13.98 49'	out	21.19 X
81+25								14.93 25'	14.72 38.32'	14.18 49.32'	
82+50.46								4.45 4.7	15.41 25'	15.02 40.58'	14.47 51.58'
12+28.5° B.C.P.											
S.E. Inner Loop											
B.M.	7.20		1774		10.57						
14+25.83						15.80 6'		15.07 10"	14.52 21"	6.27 10.0 F7.2 16	3.2 10.0 F6.9 3.73
710 S.L. B.M.	7.80										9.41
14+34.99	180.24					16.10 16.24 11"		14.86 10'	14.09 21"	7.2 3.2 F2.2 10	3.2 5.2 F1.5 3.3
14+50	2.2				0.9	16.16 9.33'		14.59 10'	13.68 21"	7.0 3.2 5.3 F2.1 10	4.1 5.3 F1.2 2.3
14+79.99						15.71 8'		13.82 10'	12.67 21"	8.4 3.3 3.9 4.4 5.1 F2.2 10	5.1 5.1 F0.3 3.8 2.9
15+00						15.21 8'		13.16 10'	11.91 21"	9.8 4.6 5.3 F0.7 10	5.8 5.3 C0.5 2.5
15+25						14.38 8'		12.30 10'	11.41 20.70	(Gut El.) 9.8 5.4 5.2 C0.2 10	6.3 5.2 C1.7 2.8

S Mon. Moreno Camino Del Rio

6.27 2.7
10.0
F7.2
40.58 EP
3.38
Foot buck

9.41
6.82
F2.57
14.43
22.55 L.M.

S.E.P.P.
2.7
3.4
B.M. 7.80
11.67
19.47

0661
31.29T 17.74T
S.E. Inner Loop H. MEY

Rt. 554

67

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	ϕ	E.P.	Shdr. Hinge	E.P.	Toe	R.P.
			17.10T									
15+50		7/6 10.42	1413.	13.76	3.3 3.3 F1.6 F1.7	13.46	12.65	11.55	(Gut. El.) 11.04	10.25 9.1 F2.2 10	6.7 9.1 F2.4 2.4	6.5 F2.0 10.38 For P.B. aw
+60 - S.L. H. P.P.P.			13.76	13.76	7.53 8.87	13.09	12.36	11.32	10.91	10.91 10.35 For B.P.		
15+72.71		8.01 8.88 F0.87	12.28	12.28	9.5 9.2 F2.5 1.8	12.61	12.00	11.00	(Gut. El.) 10.76	10.53 8.1 F2.3 10	7.5 8.4 F2.3 10	6.3 F2.1 F2.1 1.89
16+00		8.68 10.19 F1.51	12.61	12.61	5.5 5.2 F2.0 1.0	11.94	10.70	10.70	(Gut. El.) 10.63	10.55 9.1 F2.1 10	7.1 9.1 F2.0 1.79	6.5
16+33.37	R.I.	9.14 10.58 F1.44	Taylor 12.15	12.10	9.19 10.58 F1.39	11.43	10.52	10.52	(Gut. El.) 10.51	10.78 7.2 F2.3 10	7.2 9.5 F2.2 1.7	
JP	6.79	15.03	9.50	8.24								
16+42.77												
16+59.15	FC											
BM				7.17	7.86							

SERP
Chartnut + Taylor
780

Self Grav.
19.47A

S.E. Inner Loop

Sta.	Slope	Super	R.P.	Toe	Shdr. Hinge	E.P.	φ	δ	E.P.	Shdr. Hinge	Toe	R.P.
BM		4.30	12.10	7.80	SE BP Chartnut + Taylor							
18+79.83 B.C.						7.65	5.90 5.45	7.86 7.88	7.19	4.72	4.9 4.4	4.4 4.4
					Curb Street	6'	F0.53	F0.51	10.41'	16.41	Co.5 10.4	F0.5 16.9
19+07.14						7.68	4.97 5.29	4.25 4.25	7.89 7.22	4.69	4.9 4.6	4.1 4.6
						6'	F0.32	F0.31	12'	19'	Co.3 13	F0.5 19.8
+30												
19+25						7.70	4.20 4.88	7.91 7.24	8.05		out	
						6'	F0.26	F0.24	12'	19'		
19+38.04 - R. 2nd						7.79	8.29 5.85	7.93 7.26	8.07		4.9 4.9	4.9 4.9
						11'	F1.85	F0.9	12'	19'	Co.0 13	F0.9 20.4
19+50						7.84	8.31 5.80	7.95 7.28	8.09		out	
						9.62'	F1.85	F0.7	12'	19'		
19+75						8.23	8.73 5.41	8.07 7.61	8.21		4.7 5.2	5.8 5.8
						8.10'	F1.60	F0.53	12'	19'	F1.1 13	F1.9 21.9
20+00						9.04	9.57 4.10	8.48 7.81	8.62		4.3 5.2	5.5 5.2
						8'	F0.90	F0.7	12'	19'	F1.0 12	F1.8 21.7
20+25						10.27	10.77 3.87	9.32 8.64	9.45		5.5 5.4	5.7 5.4
						8'	F0.66	F0.4	12'	19'	F1.9 12	F2.7 23.1
20+50						11.84	12.34 2.80	10.58 9.91	10.72		2.2 3.5	1.4 5.5
						8'	F0.93	F0.7	12'	19'	F3.3 13	F4.1 25.2
TP	4.82	11.67	5.25	6.85	SE BP Chartnut + Taylor							

S. E. Inner Loop

11.87

69

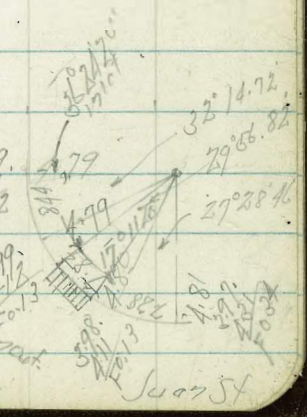
Sta.	Slope	Super	R.P.	Toe	Shldr. Hinge	E.P.	±	E.P.	Shldr. Hinge	E.P.	Toe	R.P.
		20.107										
20+75				14.14X 0.87 12.37 12.85	-1.8 F2.6 799 HP	13.97 66 13.44 8'	0.28 0.017 FO.86	12.31 6.82	7.65 0.0 4.7 12	-0.8 4.7 F5.5 27.5		
21+00				28.93X 1.02 24.90 4.93 29.82X 1.47	-3.4 4.8 8.2-EP 30.3	5.08 15.52 15.07 8'	10.40 0.113 FO.90	14.28 11.64 13.61 12'	11.64 0.73 14.42 19'	5.8 -1.9 4.8 F6.7 12	-2.8 4.8 F7.6 30.4	
21+12.20	-30	21.17		3.5 on Over-Pass		16.32 15.87 8'	9.60 10.58 FO.98			out		
21+23.23					-4.7 out	375 16.35 6'		15.98 15.31 12'	2.94 2.79 0.15 16.17 19'	3.98 -3.6 4.9 F9.9 12	-1.5 4.2 F8.8 32.2	
21+50.54	E.C.		Page 52			17.89 6		17.84 17.17 10.41'	8.08 3.1 F0.13 17.98 17.41'	2.12		
								12.37 11.70 -0.6				

Taylor St. Carb Grades

West Side
Staked
Sept 10-52
A.S. 5500

Rt. East

		Lt. West				Carb	
12+0		5.22	5.07 194 Co. 17 x 0.716			5.25	353. 372 Fo. 20 ✓
+75		5.15	-			5.18	
+50		5.08	5.21 5.05 0.016			5.11	367. 426 Fo. 59
+25		5.01	-			5.04	-
11+0		4.94	5.35 5.42 Fo. 07 x 0.016			4.97	381. 397 Fo. 16 ✓
+75		4.86	5.43 5.26 Co. 17			4.91	387. 415 Fo. 58
+43 = Brk on East		4.77	out			4.82	396. 430 Fo. 34 ✓
+35 = Cb FC on West		4.75	5.56 on	H Inlet BM 4.63 5.62 10.94			
+33 = Cb FC on East							
BM West side 5.66	10.29	4.63		Top	4.79 5.51 5.42 Co. 09 5	3.99 4.61 Fo. 62	32' 14.72 29' 66.82 27' 28.16
10+0 = Juan				Grate	3.96 5.53 5.42 Co. 09 5	4.79 4.99 Fo. 16	
Fast side BM 4.15	8.78	4.63	SE RP Juan x Taylor	Dot Bar	0.50 9.80 5.42 0.138 5' Back Carb FCC	3.99 4.79 Fo. 13 4.30 5.17 5.37	Juan St



Taylor St.

14+0

+90 = RR road

+85.15 = C&FC
07 H&T

+75

+50

+25

+15.15 = C&BL
07 H&T

13+0

+75

+60 on East

12+2.25

$\Delta 44^\circ 25' 37''$
R20'
T 8.17
L 15.41
D 18.5911

$\Delta 40^\circ 34' 23''$
R10'
T 4.20
L 7.95

Sunset St.

$\Delta 45^\circ 34' 23''$
R10'
T 4.20
L 7.95
D 117.887

$\Delta 42^\circ 22' 57''$
R20'
T 7.75
L 14.81
D 18.5911

10.29 W
8.78 E

West Cb

5.79

1.50
5.02
F0.84

5.75

5.54

5.55

5.75

5.55

5.75

5.55

5.55

5.55

5.55

5.55

5.55

5.55

5.55

5.55

5.50

5.43

5.36

5.29

4.79
4.99
F0.19

4.93
5.16
F0.19

2 Curb 211.29

6.67
4.64
5.27
6.65
F0.63

4.64
5.27
6.65
F0.63

TP

Clean out Grad
SEBP
BM 4.63
5.81
10.41

Rt = East

Curb

Gut.

5.79

out

5.72

5.66

4.81
4.93
5.51

5.59

4.79
1.91
5.53

5.58

out

5.51

5.52

5.45

out 5.39

5.32

4.77
4.72
F0.15

4.90
5.00
F0.16

4.22

3.26
3.22
60.04

3.39
3.58
F0.19

8.78

Taylor St.

		West Curb	Gut		2 Curb	Rt. East	Curb	
32+75		4.18 4.18 0.0	1.52	5.85	+25	7.23 4.66 4.64 FO.58	6.41	
C Stake line 22.14								
33+0		4.34 4.58 FO.24	1.36	5.69	16+0	7.17 4.12 4.79 FO.67	6.34	4.33 4.37 0.01
C Stake line 15.90								
33+17.95	Def. Page 18							
+88.71	FC E Line		6.30	4.40 4.84 FO.44 ✓				
	B.M. 7.29 West Side 4.00 Taylor 11.29 Whitman							
+75			6.26		7.11	4.18 4.80 FO.62	6.27	
+50			6.20	4.50 4.88 FO.18 ✓	7.04	4.25 4.85 FO.60	6.20	4.36 4.34 0.10
+25		0.0269	6.13		6.98	4.31 4.90 FO.59	6.13	0.0272
15+0			6.06	4.64 4.66 FO.01 ✓	6.93	4.37 5.01 FO.14	6.07	4.49 4.76 0.23
+75			5.99		6.85	4.44 5.08 FO.64	6.00	
+50			5.93	4.77 5.08 FO.31 ✓	6.79	4.50 5.26 FO.66	5.93	4.63 4.84 FO.21
14+25			5.86		6.73	4.56 5.17 FO.61	5.86	
TP West Side 5.45	10.70	5.09	5.25					
	10.29				10.56			

Taylor St.

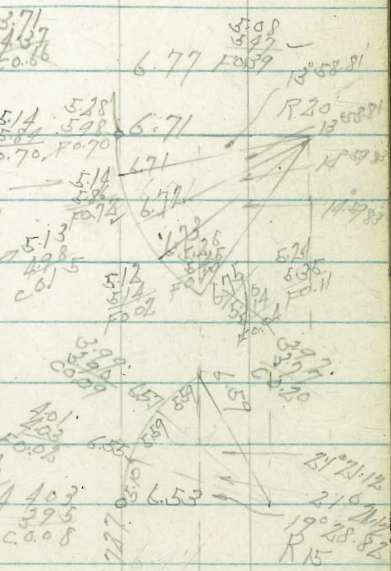
Lt = West

Sept 9. 52
H.S. 5509
Rover
Perki 21

73

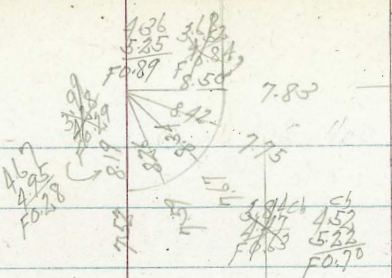
	Curb	Gutter	Rt = East	Curb
+75	103 8.03 F200 8.15	7.65	8.06 11.29 Curb 7.98	331 378 F0.67 7.25
+50	BM 7.80 4.88 12 18T 8.05	7.56	7.90	339 4.06 F0.67 7.15
+25	4.20 6.32 F2.15 7.98	7.48	7.82	347 4.12 F0.65 7.06
18+0	7.90	7.40	7.74	355 4.19 F0.64 6.96
+75	7.82	7.32	7.66	363 4.28 F0.65 6.86
+146 = Cb E.C. 0711	Page 54	7.29		
+50			7.58	371 4.37 F0.66 6.77
+35 = Cb E.C. RL			7.55	5.14 5.18 5.84 F0.70 F0.70 6.71
17+00.25 = Whitman			7.68	5.13 4.95 5.27 5.20 F0.66 F0.63 6.71
BM For check	4.46	6.24	17+00.21	5.12 5.17 F0.62 6.53
+70.22 = Cb B.C.P.1			7.25	397 4.46 F0.64 6.53
32+27.73 = P.C. 'E'	3.38 3.01 F7.63	7.32	7.32	4.03 3.95 C0.08 6.53
C. Stake Line 19.55				
32+50	3.83 3.86 F1.43	6.87	6.20	4.09 3.95 C0.14 6.47

B.M. 6.26
Chisolm
35 ft Taylor
50 ft Whitman
11.85T



2.34 L.L.
Taylor
54 Whitman
6.25 P.11

Taylor

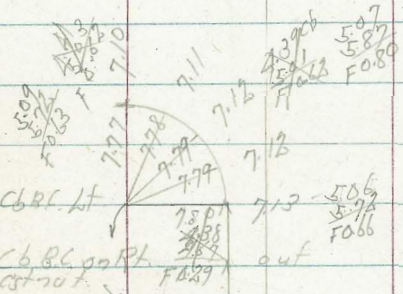


Cont 77
20+75.14
4 1/2 8.33

East

74

Chartnut



463
7.82

1/2 Curb

Curb

For Chartnut
SFPP
7.80 Chartnut
5.06 Taylor
12.86 T

7.80
4.6 T
13.4 5T

+25.14 - Curb Lt

486
5.78 7.57
F0.32

+25.14

8.45

284
3.03
F0.51

106
40.80 on C

+15.14 - Curb on Rt
Chartnut

out

7.79

20+10.48

5.05
3.21
F0.41
7.81 C
7.14 C
4.17
3.39
F0.39

7.14 C

485
5.29
F0.45
7.60

20+0

8.37

292
3.61
F0.19

7.73

413
4.39
F0.38
3.48

+72.53 = 1.8 + 79.83 SF 11

5.00
3.25
F0.55
7.86 C
7.32 5.11

7.19 C

480
7.65
3.6 F0.54

+75

8.29

300
3.70
F0.73

7.64

+50

8.21

5.08
3.80
F0.72

7.54

4.31
4.35
Curb

+25

8.13

5.16
3.80
F0.64

7.44

+11.09 0.7 V 1 R
Page 18

8.29 F1.86
7.79

19+0

393
8.18
F0.25
8.25
7.75

8.05

5.74
3.80
F0.64

7.35

4.50
4.77
00.06

Curb Gutter

11.85

Curb

0.00000

Taylor St.

Curb Gutter

+41.60 = Exist Curb -2.50	13° 17.75	18.43	18.43
+25	11° 13.81 ✓	17.78	
24+0	8° 07.12 ✓	16.83	16.22 - Pav
Δ26° 35' 36" R2320.25 +			
+75	15° 00.55 ✓	15.83	
L 106.86 D. 7.4652			
+50	15° 53.92 ✓	14.83	
+34.74 RC Lt		14.22	13.55
+25		14.03	13.36
23+0		13.53	12.86
+75		13.03	12.36
+50		12.53	11.86
22+31.22 = EG 19		12.15	11.48
BM	122 21.29	20.07	8° 54' 8"

Chestnut St. Grader
Taylor St to Rosecrans St.

Nov. 18. 52
H. J. Wilson
Garber

Roger
Kelley

		Curb	Gutter	Z	Gutter	Curb	
3+0 = S.E. Rosecrans	$\frac{4.39}{4.84}$ F0.25 18'	7.27	$\frac{6.60}{15}$	7.00	$\frac{6.60}{15}$	7.27	$\frac{4.39}{4.84}$ F0.25 18'
750	$\frac{4.50}{4.25}$ E0.25	7.36	6.69	7.12	6.76	7.43	$\frac{4.13}{4.23}$ E0.
2+0	$\frac{4.41}{4.54}$ F0.12	7.44	6.77	7.24	6.91	7.58	$\frac{4.38}{4.58}$ F0.50
750	$\frac{4.34}{4.63}$ F0.29	7.52	6.85	7.36	7.06	7.73	$\frac{4.12}{4.82}$ F0.69
1+0	$\frac{4.26}{4.73}$ F0.47	7.60	6.93	7.47	7.21	7.88	$\frac{3.98}{4.52}$ F0.59
750	$\frac{4.17}{4.45}$ F0.38 18'	7.69	7.02	7.59	7.37	8.04	$\frac{3.82}{4.57}$ F0.85 18'
0+0 = N.W. Taylor		7.77	$\frac{4.76}{4.70}$ 15'	7.71	$\frac{4.34}{7.52}$ 15'	8.19	
BM 406	11.86		7.80				STOP Chestnut St

E0.00

Taylor St.

Corb Gutter

+25

23+0

+75

+50

22+31.22 = RI on Mat.

21+93.11
16+59.25 FCSEIL

+65.25 B.C. Pav Edg

+50

+25

21+0

20+751d

Str Page 75

↓

2.57
4.41
F1.84

10.29 9.62

2.86
2.68
F1.88

10.00 9.33

3.24
2.68
F1.32

9.50 8.83

3.24
3.27
F1.41

9.00 8.33

12.86T

8+ Ford. Page 74

10.70
26
1.75
2.25
FO.60

10.13
26
2.32
2.87
FO.55

9.83
26
2.62
3.16
FO.54

9.33
26
3.13
3.67
FO.45

8.83
26
3.62
4.02
FO.40

4.12
4.41
FO.29
8.23
26

12.45 T
1.47
10.98
Coff

Camino Del Rio

78

				Out.	Curb
+80.26	FndCb on South				19.40 Exist
+71.51	FndCb on S				out
+10				18.52	18.50
					19.27 2.03 3.18 F1.16
84+0				17.92	17.90
					18.57 2.17 2.91 F1.19
+16.43				17.27	17.25
					17.92 2.37 3.27 F0.60
+150				16.92	17.693
				54.124	17.60 3.69 2.77 F1.68
+25				16.53	16.43
					17.10 4.19 3.44 F1.25
+06.43	R10291			16.23	16.13
				54.124	16.80 4.19 3.57 F1.08
83+0					16.10.5.514
					16.77.5.514 4.52 5.57 F1.05
82+41.76					
BM	1.22	21.27	20.07	SW BP W of Bridge Moros & Taylor	

Storm Drain + H¹ Inlet
78 + 25 Camino Del Rio

Sketch Page 4

8' x 18"

June 20 52
H.S. Wagon
Garber
Rorer
Fritz

Restake

Aug. 28 52
H.S. Wagon
Garber
Rorer
Chipman

79

B.M. 4.71 15.25

10.54

1/2 Mon
Camino Del
Rio
+ 1000'

B.M. 10.54
3.85
14.19

Top Curb

3.46
4.63
11.17
10' East

10.73

4.58
5.76
10.34
10'

Grate

4.29
4.63
10.94
10'

9.90

5.35
5.76
11.11
10'

Bottom Box

6.87
4.63
11.50
10' E

7.32

7.99
10.66
13.65
10'

Outlet 18" Pipe

7.19
5.64
12.83
10' W

7.00

8.25
4.79
13.04
10' W
10' W
10' W

Sta Levels North West Outer Camp +

Caminos Del Rio Barron Pit
St. N

Oct. 14. 52

B

F. Simon
Garber
Rorer
Kelley

B.M.	75+50	120 42	59 25	40 0.0
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Top C.

	75+0	105 31 30 4	96 20	
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Grat

Bottom	+50	114 30 30 5	90 18	
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outlet

	74+0	101 29 5.2	73 17	
--	------	------------------	----------	--

	+50	96 32 5.2	71 19	
--	-----	-----------------	----------	--

	73+0	105 39	66 21	
--	------	-----------	----------	--

	72+50	73 31	45 24	
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B.M.	753	1807	1054	May 2 Caminos Del Rio + Murcillo
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