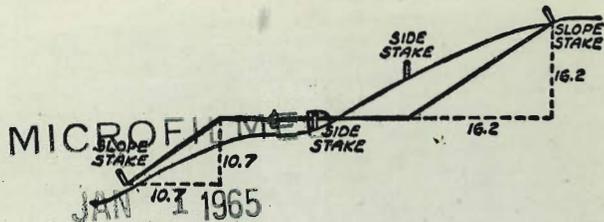


2212

STORM DRAIN

BASE BOOK



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.887	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

Pgs

Drain Survey - Lot 20 La Playa Highlands 1-5
 4020 Goldfinch - elevations gutters 6
 Drain Survey - BIK 23 Fairwood Add 7
 DRAIN - 54th & TROTAN 12
 BIK 2 Nordica Hgts } Drain
 Cottonwood St. } 42
 DRAIN: 52nd to 54th, 54 TROTAN 78

D. Smith
C. Allen
P. Taylor
R. Parks

Proposed Storm Drain
W. Li. Lot 20 La Playa Highw Sands
Tavara Pl Southerly

W0#20965 1

4-4-52

Fd + Disk on AP
C-4 Steps

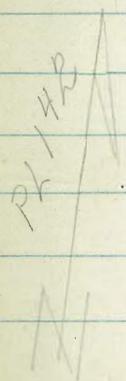
Mon out
Fa 2-2050

INDEXED

Law

APR 8 1952

Mon out for
under Mr Hazar's
Flower garden



Pr 130

Sub line 0+91⁸⁵ 0+91¹²
Tavara Pl.

68°39'

Mon knocked
over
Necet 4-4-52

0+63³⁰

Fd Mon

0+10³⁹

+ + + Cyclone Fence
Cor

0+00

Pr 128

Lt-West

Q

Rt-East

2

0458

 $\frac{242^3}{10}$ 241^3 $\frac{259^3}{10}$

0450

 $\frac{248^2}{10}$ 246^3 $\frac{245^6}{10}$

0440

 $\frac{250^2}{10}$ 251^0 $\frac{250^5}{10}$

0427

 $\frac{260^4}{10}$ 262^3 $\frac{259^3}{10}$

0410

 $\frac{269^2}{10}$ 269^2 $\frac{269^2}{10}$ 0400 ^{3'lt} NE Fence Cor $\frac{280^3}{10}$ 279^3 $\frac{275^0}{10}$

0-20

 $\frac{285^2}{10}$ $\frac{285^0}{3}$ 283^0 $\frac{229^1}{10}$

BM.

212

21

NWBP
La Crescenta Dr
Tavara Pl

Lt = West 2

Rt = East 3

0791¹³ C6 line taken along

222⁶³ 222⁰⁸ 221¹⁶ 221⁶⁵ 219²⁸ 220⁴⁹
8 8 sut. 06 10 10
06 sut sut 06

0789

218³ 222^L 220⁴
10 10

0772

234^L 233⁸ 232²
10 10

TP ₁₈	0 ⁶⁵	162 ²⁵ ✓	1 ⁴⁵	161 ⁶⁰ ✓ overnight	
TP ₁₇	0 ⁶⁹	163 ⁰⁵ ✓	12 ⁴⁶	162 ³⁶ ✓	
TP ₁₆	0 ²⁸	174 ⁸² ✓	12 ⁶⁰	174 ⁵⁴ ✓	
TP ₁₅	0 ²²	187 ¹⁴ ✓	12 ⁸¹	186 ⁹² ✓	
TP ₁₄	0 ³⁶	199 ²² ✓	13 ³⁶	199 ³⁷ ✓	
BM TP ₁₃	0 ⁵²	212 ²³	11 ⁰⁴	212 ²¹ ✓	NWBP La Crescentia Dr Tarrara Pl
TP ₁₂	12 ²³	223 ²⁵ ✓	0 ²³	210 ⁵² ✓	
TP ₁₁	12 ⁶⁹	210 ⁷⁵ ✓	0 ²³	198 ⁰⁶ ✓	
TP ₁₀	12 ⁷²	198 ²⁹ ✓	0 ³³	185 ⁵⁷ ✓	
TP ₉	13 ²⁴	185 ²⁰ ✓	0 ²⁹	172 ⁶⁶ ✓	
TP ₈	13 ¹³	172 ⁹⁵ ✓	0 ⁰⁷	159 ⁸² ✓	
TP ₇	13 ³¹	159 ⁸⁹ ✓	0 ³⁴	146 ⁵⁸ ✓	
BM			10 ³⁸	136 ⁵⁴ ✓	✓ R chisel ok replaced with SW cor B.P. 136 ⁵² San Geronimo + La Crescentia Dr coming down
TP ₆	12 ²¹	146 ⁹² ✓	0 ¹⁷	134 ⁷¹ ✓	
TP ₅	13 ²⁰	134 ⁸⁸ ✓	0 ¹⁸	121 ⁶⁸ ✓	
BM			3 ²⁶	117 ⁹⁰ ✓	✓ chisel ok replaced with NE cor B.P. coming down Kellogg San Geronimo 117 ⁸⁹
TP ₄	12 ²⁸	121 ⁸⁶ ✓	0 ³⁴	109 ⁰⁸ ✓	
TP ₃	13 ³¹	109 ⁴² ✓	0 ²⁰	96 ¹¹ ✓	
TP ₂	13 ²⁶	96 ³¹ ✓	0 ³¹	83 ⁰⁵ ✓	
BM			2 ¹⁶	81 ²⁰ ✓	✓ chisel ok replaced with SW cor Kellogg + San Fernando 81 ¹⁸ coming down
TP ₁	12 ³⁶	83 ³⁶ ✓	0 ²⁰	71 ⁰⁰ ✓	
BM	11 ⁵⁵	71 ²⁰ ✓		59 ⁶⁵ ✓	SWBP Kellogg San Elijo

BM starting 7⁵⁸ 59⁰⁴ ✓ ✓
 SWBP
 San ELISO
 Kello99

TP₂₆ 2⁴⁷ 67²² ✓ 11⁶⁶ 64⁵⁵ ✓

TP₂₅ 0²¹ 76²¹ ✓ 13³⁵ 76⁰⁰ ✓

TP₂₄ 0²¹ 89³⁵ ✓ 12²⁷ 89¹⁴ ✓

TP₂₃ 0¹⁹ 102¹¹ ✓ 13²⁵ 102⁰¹ ✓

TP₂₂ 0⁷⁴ 115²⁶ ✓ 12⁰⁸ 114⁵² ✓

8⁷² 117⁰⁸ ✓ NEBP
 Kello99
 San Boronio

TP₂₁ 0⁵¹ 126⁶⁰ ✓ 12⁶⁸ 126⁰⁹ ✓

2¹⁸ 136⁵⁹ ✓ SWBP
 San Boronio

La Crescentia Dr

TP₂₀ 1¹⁶ 138²⁷ ✓ 12⁷⁵ 137⁶¹ ✓

TP₁₉ 0⁵⁶ 150³⁶ ✓ 12⁴⁵ 149⁸⁰ ✓

4020 Goldfinch
Yard & gutter elevations

C.H.S.
Begg
oltman
Johns

5-14-52
W.I.O. 20006

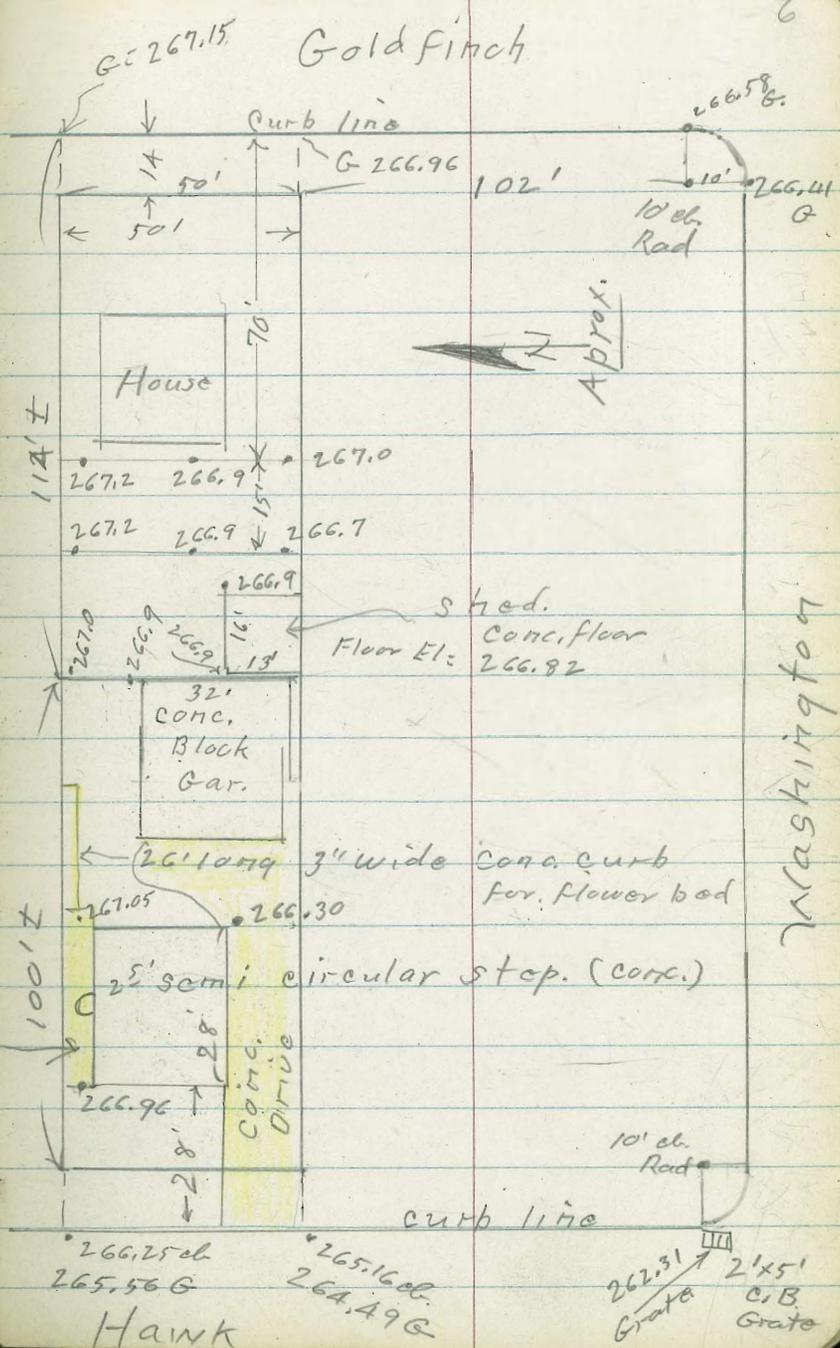
No map given
No tie points u
No Ref. u

2" or 3" of conc. added to
shed floor & a little fill
in yard and the yard
will drain thru yard
to west.

INDEXED

MAY 15 1952

Conc.
walk
5' x 32'



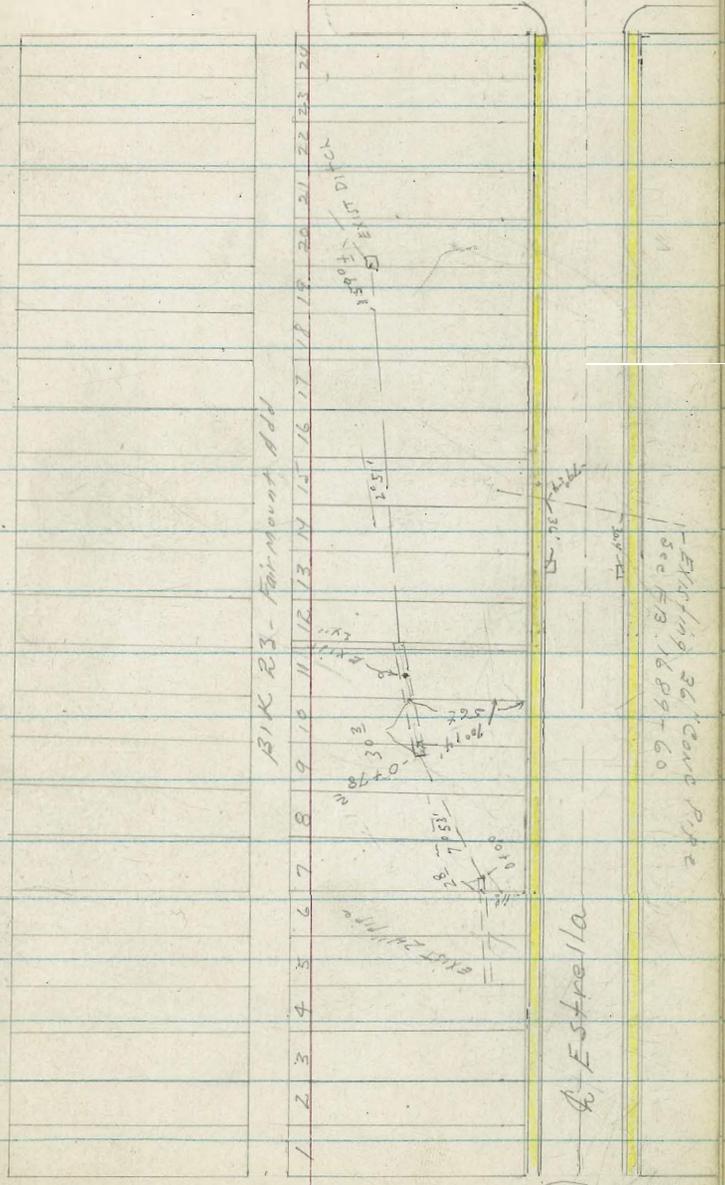
Hawk

Washington

Survey for storm drain in BIK R3,
Fairmont Addition
See P.B. 1689 - Page 60 for ties and
elevations on drain under Estrella
St between Polk + University

Allen	Ref - FB 1689-60
Parks T	T.P. 1460
Taylor	6782-L
Perkins	6783-AL

INDEXED
NOV 17 1952



Polk

EXISTING 36" CONC PIPE
See FB 1689-60

Storm Drain BIK 23 - Fairmont
See sketch Page 4.

Lt: Ely-

☒

Rt: Wly

8

1+10 - 8² Lt & Clump 16" Evc. Trees

0+88

310 I
5'
10

310 I
5' 11"

310 H
5'
10

0+78² Nly end exist 24" pipe

308 S
8'
10

305 S
10' 14"

310 R
5'
10

0+40

310 S
5'
10

306 S
9'

307 S
8'
10
Toe bank

0+00 = End exist. 24" pipe in lot 7, BIK 23

314 S
2'
10
Toe Bank

306 R
9' 77"

315 S
0'
10

TP₂ 1.99 315.99' 3.99 314.00'

315.99'

TP₁ 0.17 317.99' 11.36 317.82'

BM- 3.00 329.68'

SW BP. Estrella
326.68' ONLY

Lt = ELY

2

Rt = Wly.

9

1791 - 23° Rt NE Cor Apt house

304.85
20.3
23°
Floor

End of Apron

1789 - 3' Rt = 2 1/2" wide Conc Apron

301.96
45.2
3°
Apron

TP3 2.98 306.48 12.49 303.50

309.3

309.2

306.48

303.2

303.2

1750

6.7
20

12.0
4
Toe

12.2
ON CONC
Apron

12.3
10

12.8
14
Toe Slope

See FB 1689-20

1734 3/4 Begin 2 1/2" Wide N+S Conc Apron

305.1

304.63

306.1

1734 3/4 5/4 end exist 24" pipe

6.9
10

11.30
1.5

9.9
10

310.8

305.5

310.0

1722

5.2
10

6.1

6.0
10

315.99

2+50

2+100 $\frac{45}{10}$ Lt = SW COR house

2+116 - 11° Lt = NW COR house

2+116 - 73° Rt = end 36" F.W. Pipe UNDER Estrella

2+112 - 29° Lt S.E. COR APT house

2+00

Lt = ELY

300 Z

56

10

302 Z

39

45

302 Z

39

11°
LOWER
FLUX

301 Z

46

10
Ditch

305 Z

15

10

300 Z

58

10

301 Z

46

10
Ditch

302 Z

38

10
pitch

Rt = WLY

10

300 Z

52

10

303 Z

34

30

300 Z

59

10
pitch

300 Z

62

54
pitch

301 Z

50

25
Gr
House

300 Z

61

73
IF

306.48

LT = ELY

RT = W14

Start B.M.	2.02	326.69	(326.68)
12.09	328.71	1.54	316.62
TP4 12.61	318.16	0.93	305.55

3+29- Bottom Ditch to Alley

296.2	297.2	297.2
9.5	9.2	8.8
10' Ditch		10' Ditch

3+24 Top bank ditch to Alley

298.2	298.8	298.8
6.8	6.7	8.9
10		7.2 Bottom Ditch

3+17- 3 4E 10" pole # PA4025

3+00

299.5	300.5	300.7	298.2	300.8
5.0	6.0	5.8	8.5	5.2
		7' Top Ditch	12' Bottom Ditch	16' Top Ditch

306.48

SURVEY - OPEN DRAIN
54TH & TROJAN

Clark
Shepherd
Bruner
Proceq
W.O. 210.71
1-19-53

DATA: MAP # 2447-2
Sketch - Tie sheets 3661-B
3671-A

Sketch Not to Scale

Notes: Pg 13

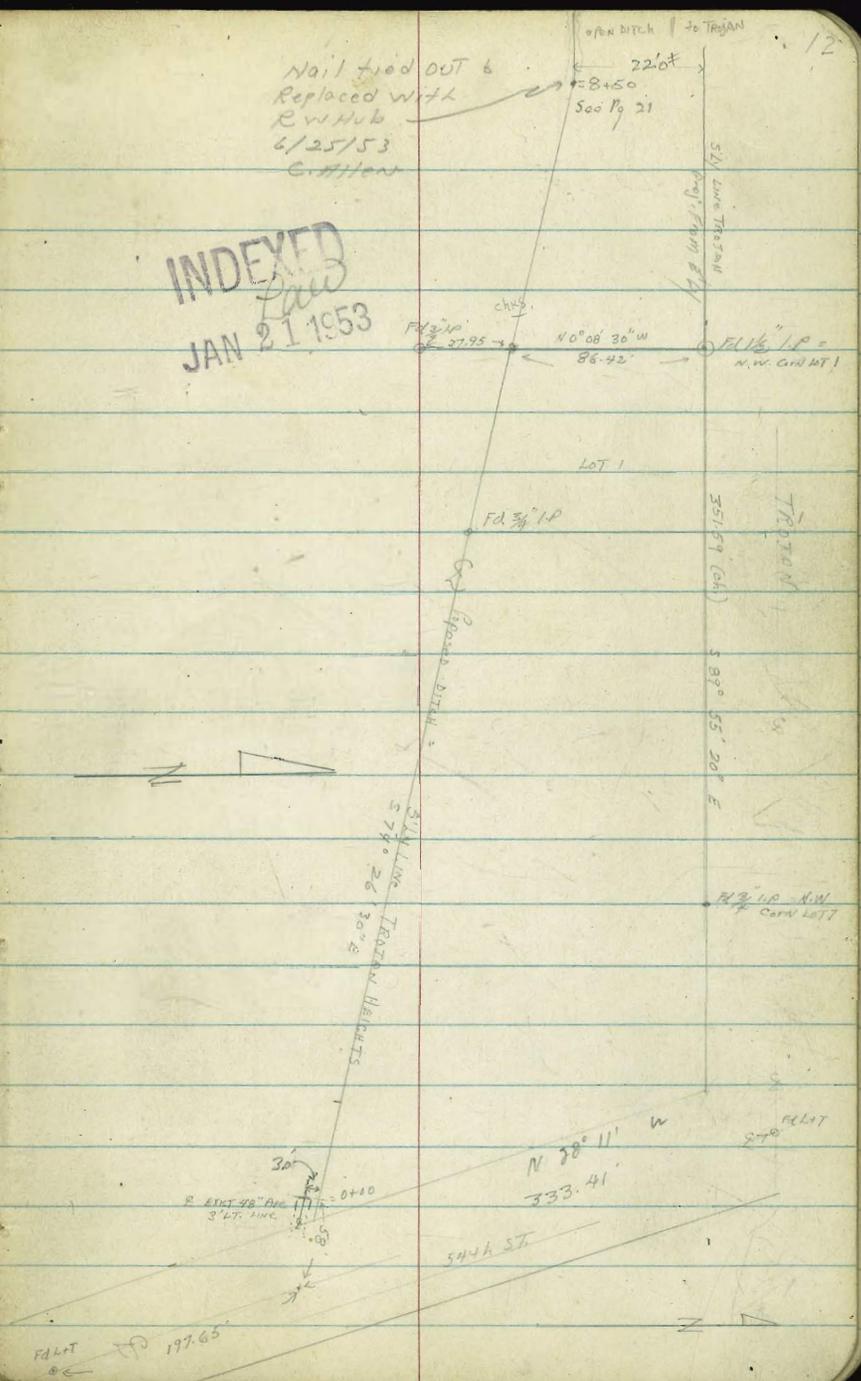
INDEXED
JAN 21 1953

Nail tied OUT &
Replaced with
R.V. Hub
6/25/53
C. MILLER

OPEN DITCH to Trojan

22' 0" ±
84.50
See Pg 21

12



NOTE: SEE Page 16 For Level Check with B.M.

DRAIN - 54th to TROJAN

LT. S RT

2+75 End Picket Fence on line ✓

REMOVED BY
R. BARBER
1-29-53

2+50

2+25 9' RT Beg 5' Picket Fence ✓

2+04 4.7 RT E. M.H.

2+00

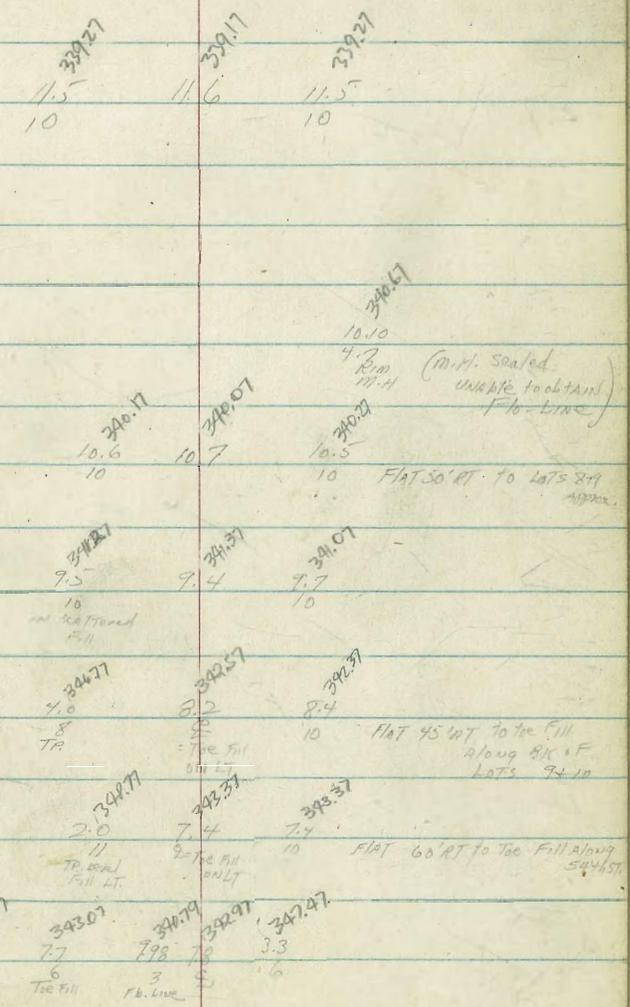
1+50

1+35 END Solid Fill ON LT Beg scattered fill

1+00

0+50

0+00 Beg Barbed wire Fence along S'ly line
Trojan HTS.



CORRECTED E.L. IS

340.79

100.00 = Assumed Elev

FLO LINE EXIST 18" PIPE
AT 0+00

9.98

350.77

B.M (No available bench)

107.98

350.77

109.98

LT. E RT.

DRAIN - (CONT.)

5750

395.07
7.0
10
334.67
7.4
3
Top BK
332.67
9.4
E =
Toe
Ditch
338.77
6.3
10
Top
BK

5700

337.61
4.4
6
Top
334.87
7.2
4
Toe
339.77
7.5
5
BK
339.07
5.0
10
335.97
6.1
10

4484

42' RT E Sw. M.H. ✓

336.74
5.33
4.2
R.M.
M.H.
(M.H. Sealed)

4470

Bag open ditch (EXIST)

337.61
4.4
8
Top
335.97
6.1
5
Toe
335.37
6.7
5
Top BK
336.07
6.0
10
336.97
5.6
10

4450

2.5' RT end Picket Fence ✓
with 30'3rd wire fence

336.74
5.9
10
336.07
6.0
10
336.27
5.8
10

4400

2.5' RT Bag 3' Picket Fence ✓

336.97
5.1
10
337.07
5.0
10
336.27
5.3
10

3450

334.97
7.1
10
337.27
7.8
10
331.77
4.9
10

3400

339.67
3.5
10
339.07
4.0
10
338.27
3.8
10
Flat 55' RT to toe Lot 101

T.P.

2.50 342.07 ✓
701.28 11.20

339.57 ✓
98.78

342.07
701.28 ✓

LT. E. RT.

DRAW (CONT.)

8+00

329.05
6.8
10
322.85
7.0
321.35
7.5
10

7+50

330.45
5.4
10
330.15
5.7
327.95
5.9
10

7+30

open ditch meanders to RT + spreads out - dissipates, etc

7+00

330.85
5.0
10
330.95
4.9
330.45
5.4
9
320.25
5.1
12
TOP BK

6+50

331.95
3.9
10
331.45
4.4
330.75
5.1
7
331.35
4.5
13
TOP

T.P.

335.85 ✓
4.54 95.06 10.76
331.31 ✓
90.52

335.85
95.06

6+05

0.50' LT of 3' Tree

6+00

333.97
0.6
10
332.77
9.3
331.77
10.9
9
335.97
6.6
20
TOP BK

5+85

Open ditch meanders to RT

331.77
10.3
E

342.07
101.28

LT E RT.

DRAIN (CONT)

(1-26-53)

Tie in with B.M.

CHK. 3.42 351.67 = 351.67

Elev F. Line ex. Pipe 14.30 340.79

B.M. 3.42 355.09 351.67 = Elev of LT. E 54' 1/4 x Trojan, F.B. 1846-59

chk: 5.32 100.01 = 100.00 (see pg 15)

T.P. 11.87 105.33 1.60 93.46

9+50

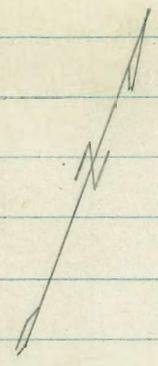
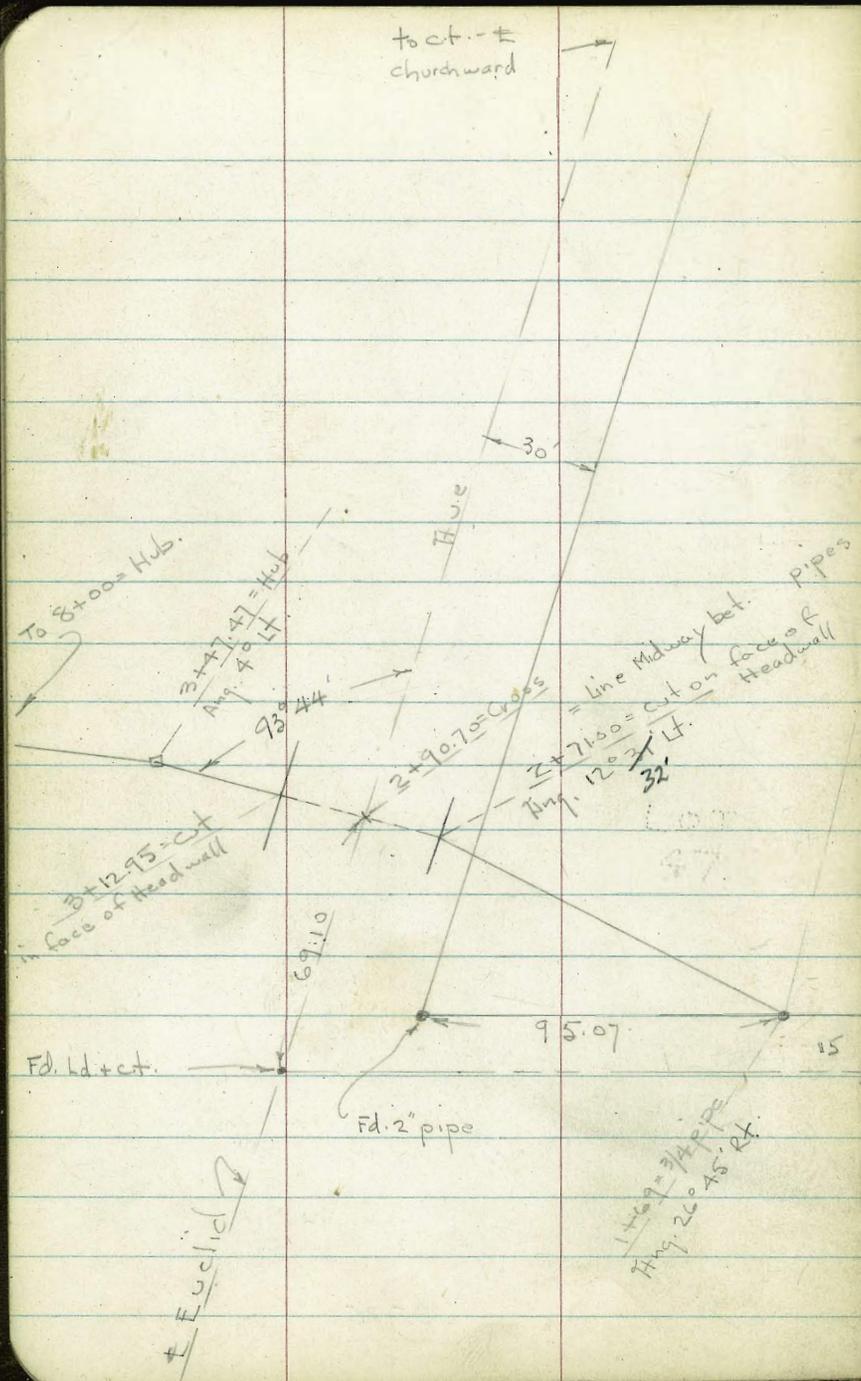
8+50

L. LT. P.M.T. with open ditch // to
S'ly Line Trojan (approx 22' south
on S'ly Line Trojan
projected from E.

328.25
7.6
10
329.75
9.1
F.L. Line
EXIST. Ditch
329.75
8.7
6.1
10
F.L. Line
EXIST

335.85
95.08

to ct. - t churchward



Euclid Manor
Map. 2752

LOT
48

± 42" P.C. pipe

Fd. 2" pipes

9.20

91.38

Sub. Line
± of Prop. Drain

0+00 = cut on
face of headwall
± 0 4 1/2" pipe

well 4.5' Long.
± along face

Req. Levels along \pm of Prop. Drain E. +

W. of Euclid at Sly. Bndry. of Euclid Manor.

7504 2-11-53 7.0

W.O. 21085

1+30

11.5 12.1 11.6 11.9
18 10
 \pm wash 13 = Toe

0+90

12.2 13.3 14.2
29
 \pm wash 11 = Toe

0+42

14.1 14.2 15.0 15.2 20.5
30 10 5 15
 \pm wash

0+32 = \pm Large Mound of Dirt

14.9 20.2 17.7 20.5
12 6 12

0+20

15.0 15.9 21.0
30 15
 \pm wash = Present waterway

0+04.8 = end of Head wall

15.9 19.10 17.5 21.5
10 Top wall Dirt 10
 \pm wash

\pm along sub. line

0+00 = \pm of 42" pipe + 9.5' Headwall - normal to

19.05 14.00
Top wall I.E. of outlet
at cut. of 42" pipe

Set. B.M. \square in East Head wall - \pm N. pipe 111.85

B.M. - S.W. B.P. Trinidad way + Euclid 121.17

Actual Elev. Shown.

Lt E Rt 18

INDEXED
FEB 17 1953

3+47.47 = Ang. Pt. - Sect. on split

3+20 = in pool at outlet.

48" pipes - End of Walls Covered.

3+12.95 = face of Head - Midway bet. \pm 's of 2-

3+10

8" along Euclid

3+03.5-7' \pm = \pm Sewer MH

3+00.8 = edge Conc.

2+90.7 = \pm Euclid

2+80.9 = edge Conc. pauc

2+75

End. of Walls Covered -

of 2-48" Cor. Iron pipes - 5' apart

2+71.00 = face of Headwall at Midway bet. \pm 's

2+20

1+69 = Ang. pt. - Sect. on split

Lt. \pm Rt. 19

08.8 14.7 14.6 10.6 10.01 09.7 11.6
45 34 25 15 on Hub. \pm 16 43 = Toe
 \pm old wash \pm wash
= present waterway

09.0 10.7 08.5 10.4
25 10 20
 \pm Side wash Sand Levee

Now Blocked 05.71 11.68 08.6 05.84
2.5 2.5
I.E. of Top wall ground. I.E. of
48" 48"

14.7

14.75 10.16
7 7 = I.E.

= Top N. Rim. 14.68

14.72

14.62

14.6

06.51 11.83 10.0 06.53
2.5 2.5
I.E. of Top wall ground. I.E. of
48" 48" pipe

11.3 10.7 11.6 10.4 12.2
30 18 10 25 = Toe
 \pm wash

11.8 11.8 10.9 11.6 11.7 10.9 11.8
30 10 4 12 15 25 = Toe
 \pm wash

8+90 - 16 Rt. = € Wash at Ang. Sharp Lt Thru Leves

00.1
16 = € wash

8+00 = End = Hub.

00.8	01.4	12.5	05.51	02.6	16.3
100	50	28	on Hub	8	42 = Top
	Toe	Top		€ wash	

7+50

13.6	04.3	16.5
33 = Top	2	32 = Top
	€ wash	

7+00

14.0	05.1	12.6	13.7
40	€ wash	16	40
Top			

6+50

14.2	05.7	05.7	09.5	10.4
43	6	€ wash	5	38 = Toe
Top				

6+00

03.6	04.8	14.5	06.6	07.9	09.3
100	65	46	7		32 = Toe
		Top	€ wash		

5+50 = € Wash

14.3	08.8	08.4	10.1
47	24		30 = Toe
Top			

5+00

04.5	06.0	14.8	09.4	09.6	08.7	09.8	10.9
115	62	49	35	5	2		25 Toe
€ old wash					€ wash		

4+50

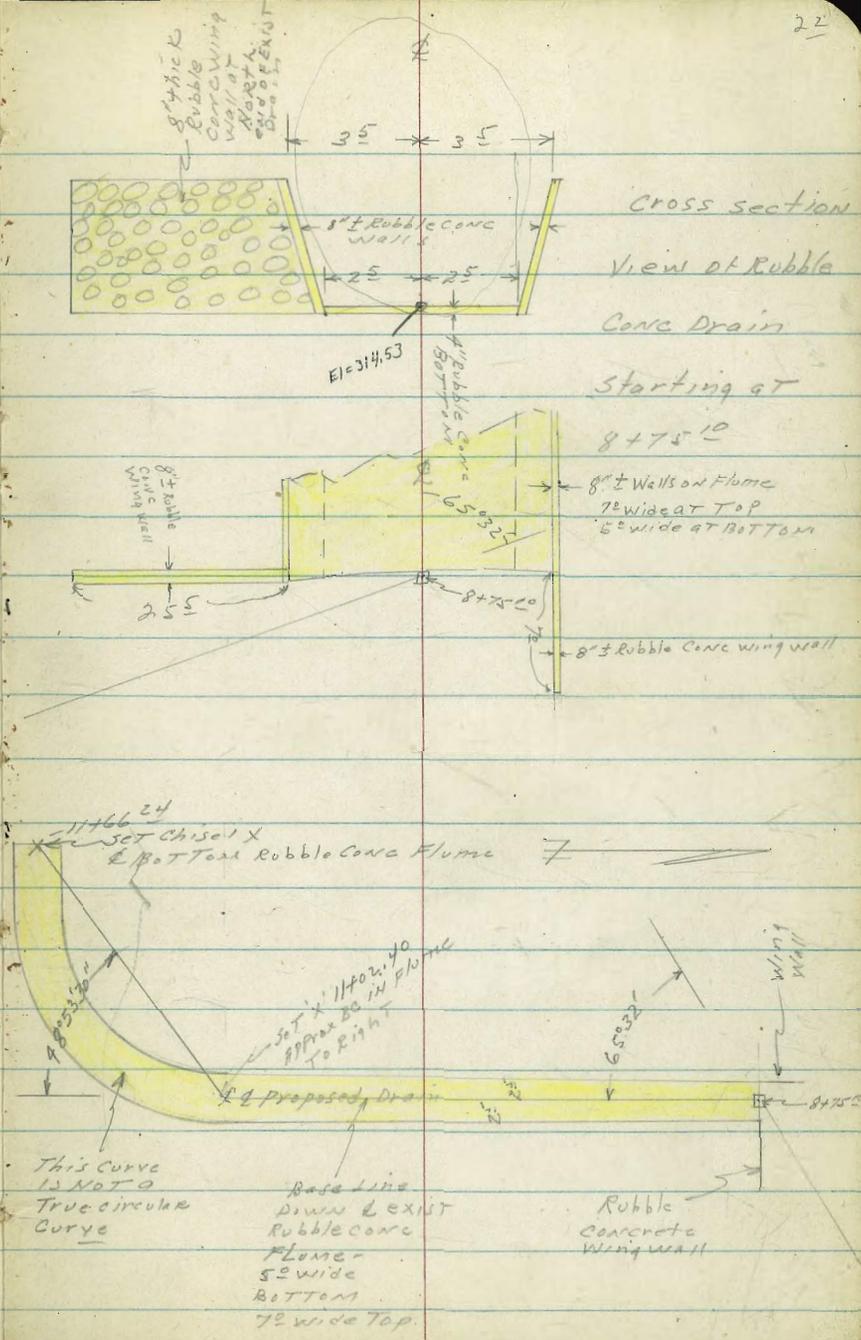
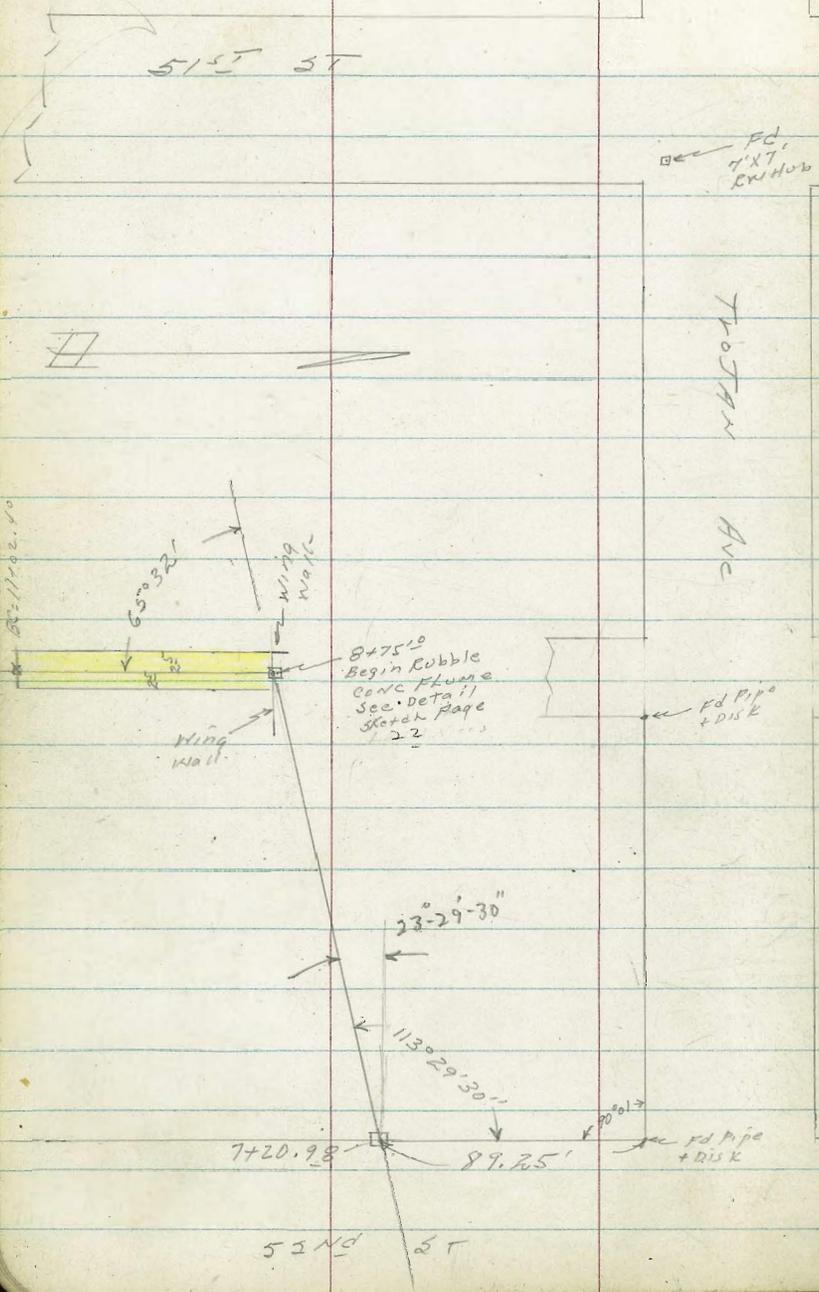
14.4	09.5	09.7	09.0	10.8	10.5
40	27		5	10	25
Top			€ wash		Toe

4+00

14.3	09.8	10.1	09.6	11.2
32	18		16	35
€ Top of Leves			€ wash	Toe

12733

22



8475'0
Begin Rubble
Cone Flume
See Detail
Sketch Page
22

11466 24
SET Chisel X
& POT Test Rubble Cone Flume

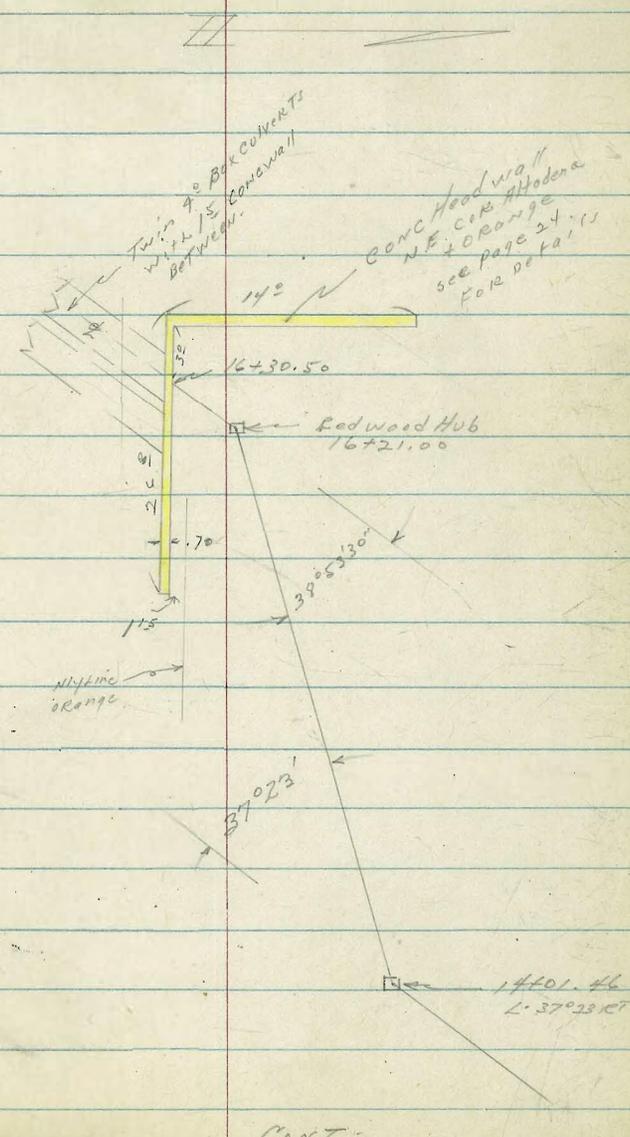
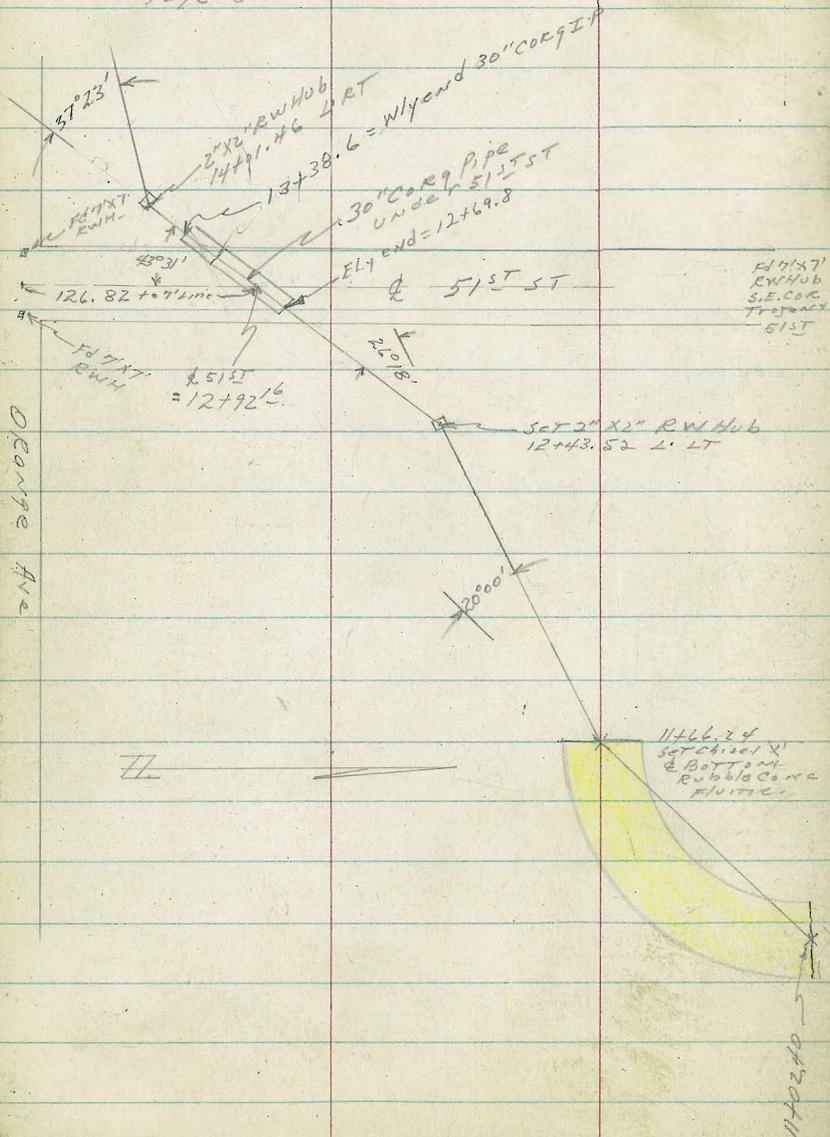
This Curve
is NOT a
True circular
Curve

Base line
Draw & EXIST
Rubble cone
Flume -
5' wide
Bottom
7' wide Top.

Rubble
Concrete
Wing wall

Drain Survey, 544 Trojan to
Altadena - CONT from
Page 22

Cont Page 23.



Nly Line Orange

10' CB RT'S ALL CORNERS.

DRAINAGE

Ave

15' cbs

36" RCP
CONCRETE
PROVIDE HEADWALL

35" CONC
GUTTER

54' end Box Culvert
= 17+34.5 ±

71°
at 90°

33" CONC
GUTTER

34x24
grate on
14" throat
Type 6

55' 90°

40'
15" CONC
WALL

Altadena a 3' ±

Two 40"
Box culverts
under intersect.

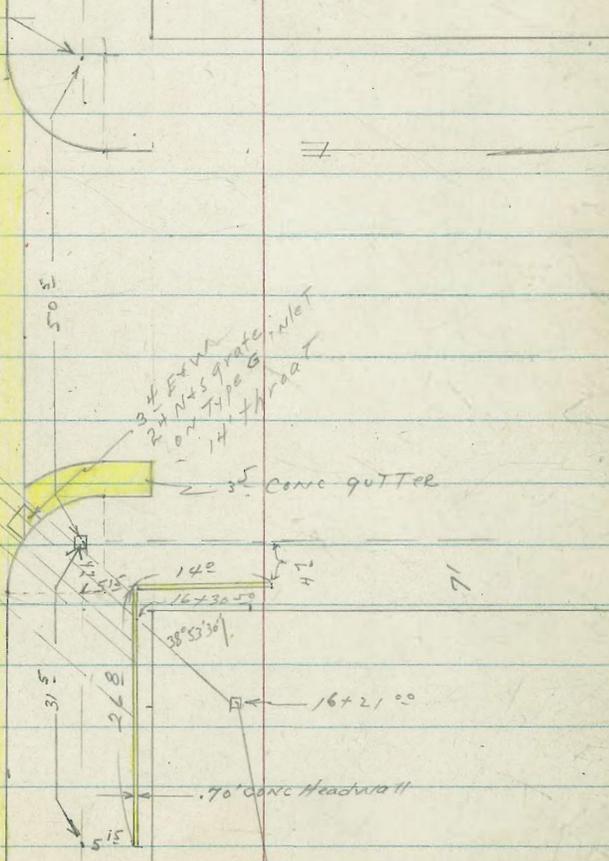
34" EX W
2x 14" x 5" grate, inlet
on 14" throat

35" CONC GUTTER

12' cbs

Ely Line
Altadena

54'
Line Orange



Nly Line Orange Ave

Levels for Proposed Drain
 from 54^B + Trojan to Altadena
 and Orange - See sketches pages 21, 22, 23
 24

LT = 514

RT = N14 25

TP₃ 4.57 332.30 9.58 327.73[✓]

2+00 - 2⁵ LT = Barb wire Fence

1+50

1+00 - 3⁰ LT = Barb wire fence

0+50 = ♀ Ditch - 3⁰ LT = Barb wire fence

0+00 = 8+50 Page 12. 3⁰ LT = Barb wire fence

TP₂ 8.87 337.31[✓] 12.30 328.44[✓]

TP₁ 0.71 341.74[✓] 12.94 341.03[✓]

BM 230 353.97[✓] 351.67[✓]

332.30 x
 325.2
 324.1
 322
 320.9
 11 6 13⁰ 12⁴ 8³
 3
 BOTTOM DITCH BANK TOP FILL TROJAN

327.2
 326.5
 325.5
 326.3
 321.9
 10 7 11 8 11 0 7 4
 5 3 6 20
 TOP FILL TROJAN

328.8
 327.0
 326.2
 327.1
 321.2
 9 3 10 3 11 1 10 2 6 1
 5 3 6 22
 TOP FILL TROJAN

329.2
 328.1
 326.2
 327.5
 322.0
 8 1 9 2 11 1 9 8 5 3
 5 5 3 19
 TOP FILL TROJAN

329.8
 327.3
 327.25
 327.2
 7 2 9 6 10.06 4 1
 5 3 3 22
 ON hub ground same TOP FILL TROJAN

337.31 x

LT of 54^B + Trojan - FB 1846 - 59

5+22.67- L. 23°26'30" LT. Section on Bisector

5+00 - 4° LT= Barbwire Fence

4+50

4+00- 3° LT= Barbwire fence

3+50

3+00 2 1/2° LT= Barbwire Fence

2+50 - 2 1/2° LT= Barbwire Fence (3-5. Stron. B)

3229	9 1/2	9 1/2	10 1/2	9 1/2	8 7/8	8 1/2	9 1/2
75	54	52	50	ON Hub ground same	11	17	
Top Hill					Top Slope	Top Fill Trojan	
3242	3229	3221	3227	3232	3238	3250	
8 1/2	9 1/2	10 1/2	9 1/2	9 0	8 1/2	7 3/8	
75	50	40	37		10	15	
					Top Fill	Top Fill Trojan	
3242	3230	3232	3222	3232	3240	3257	
8 1/2	9 3/8	9 0	10 1/2	8 9/8	8 3/8	6 1/8	
75	50	36	26	22	8	13 1/2	
					Top Fill	Top Fill Trojan	
	3248		3238		3235	3247	
	7 1/2		8 1/2		8 8/8	8 1/2	
	75		50		3	6	
					Bottom Bank	Top Fill Trojan	
			3242		3244	3244	
			8 10		7 9/8	8 1/2	
			50		3	4	
					Bank	Bottom Bank	
			3250		3247	3246	
			7 1/2		7 6	8 1/2	
			50		3	6	
					Bottom Creek	Bank	
			3259		3242	3245	
			6 1/4		6 9/8	8 1/2	
			50		Bank	3 1/2 Bottom Creek	
					6	21	
					Bank	Top Fill Trojan	

332.30 x

6+42

6+40

6+30

6+13

6+11

6+00 - 29° Pt - Barb Wire Fence

5+50 - 6° Pt - Barb wire Fence

TP4 - 3.41

326.92

8.79

323.51

LT = 5.14

RT = 1.14

22

320.2

319.2

319.2

319.5

321.4

322.2

322.3

326.92

322.30

6°

0

7°

1

15

4.9

100

326.92

322.30

321.4

321.2

319.2

48

56

72

50

25

22

320.2

321.2

66

57

28

39-

322.5

323.2

321.8

321.5

37

51

54

60

47

27

4.4

43

Top Fill

323.3

322.3

322.2

36

46

46

75

60

25

322.3

324.0

324.8

219

21

25

Top Fill

30°

Top Fill

Top Fill

Hob L 5+22.67

322.30

LT=514

RT=N14 28

316 10 0

318 2

317

318 2

318 2

317 2

318 2

318 2

7+78

7+73

7+50

7+20.98 intersects Wly Line 52Nd

7+00

320 6	8 2	8 2	9 6	8 6	8 6
20		20	23	28-50	
320 2	321 5	320 5	317 8	320 6	319 8
39	5 4	6 3	9 1	6 3	7 0
25		16	22	28	30

6+98-14^S LT intersects Sewer Manhole
Flows From North turns to Wly toward Alley

308
Rim

14.08
I.E.

6+62 intersects N+S Barb wire Fence

322 2

321 1

319 4

320 2

321 5

6+50

47
50

58

75
15

67
28

59
40

326.92 7

Section taken 90° to Forward Tangent
See sketcher Page 22.

Drainage ditch in good condition

8+75¹⁰ L. 65° 32' LT also begin rubble conc

Manhole sealed

8+65- 5² RT = 4 Sewer Manhole

NECOR.

8+49- 12⁴ LT = Nly Face 8" Rubble conc wing wall

TP5 0.23 318.76¹ 8.39 318.53¹

8+00

7+87-

7+8.4

LT = S14

R to Nly

29

317.3	316.88	314.51	314.51	316.28	318.02	316.8
15	180	425	423	422	069	210
10	31 TOP Wall	25	ON CONC FLOOR	25	35 TOP Wall	100

317.44
132
Rim

318.8	318.4	318.3	315.8	316.2	316.2	316.5	316.8
40	04	03	32	21	25	28	24
35	130 ground Slyside	128 TOP Wall	122 ground Nlyside		25	35 BOTTOM CREEK	50

318.76¹

ON top Cobble stone wing wall Ely of Drain

319.3	318.4	316.3	316	317.8	317.2	316.8	317.2
76	87	106	103	91	93	1010	96
25	13	12	8	7		15	50

317.5
9
100

316.5
10
103

326.92¹

10+75

10+50

CANYON RIM ON FLY gets progressively steeper

TP6 8.82 321.48[✓] 6.10 312.66[↓]

Wood stringers
10+05' 8' Wide Wooden Bridge across channel

10+50

9+50

9+00

LT = FLY

Rt = WLY.

30

317.1	315.5	312.56	312.56	312.48	315.15	321.2
44	600	892	912	920	633	03
10	35 TOP	25	25	25	35 TOP	10
318.2	317.6	315.25	312.61	312.75	315.48	316.0
33	39	623	887	888	600	51
10	6	35 TOP Wall	25	25	35 TOP Wall	10

321.48 [✓] ↓

317.1	315.41	312.86	312.83	312.82	317.03	315.2
11	325	590	593	596	173	29
10	35 TOP Wall	25	25	25	35 TOP Wall	10
316.5	316.15	315.25	315.21	312.7	318.14	316.2
22	261	551	555	559	060	216
10	35 TOP Wall	25	25	25	35 TOP Wall	10
316.2	316.9	315.8	315.8	315.29	318.09	316.5
21	183	493	495	497	066	213
10	35 TOP Wall	25	25	25	35 TOP Wall	10

318.76[✓]

11450 - 7° LT = $\frac{1}{2}$ Flume

11440 - 11° LT = $\frac{1}{2}$ Flume

11430 - 14° LT = $\frac{1}{2}$ Flume

11420 - 13° LT = $\frac{1}{2}$ Flume

11410 - 7° LT = $\frac{1}{2}$ Flume

11407 - Top Rubble Core Flume wall.

11405 $\frac{1}{2}$ intersects Wly Wall Flume

OR diameter from long chord

Location of Flume shown from

Not a true circular curve -

Roughly B.C. of Flume - The curve is

11402.40 C. 48° 53' 30" RT

323.6	314.28	311.47	314.48	316.8	316.2	314.6	313.4	312.9
+2.1	7.20	9.99	7.00	4.7	5.3	6.9	8.1	8.5
25	18.1	14.6	10	8		25	20	100
	Top Wall	Flume	Top Wall					

315.4
6.30
Top Wall Flume
312.26
9.22
Bottom Flume

316.5	315.08	312.20	312.27	312.16	314.85	322.7
5.0	6.34	9.18	9.41	9.32	6.63	+1.4
10	3.5	2.5		2.5	3.5	10.0
	TOP WALL				TOP WALL	

321.48

LT = S14

Rt = N14

32

1243 ⁵² L. 26°18' LT - Sect taken Tangent 90° to Back

3142	3100	3106	3104	3108	3121	3122
12	23	48	50	50	31	32
10	5	2		2	4	10

TP7 4.71 315.35 10.84 310.64

315.35 x

12400

3154	3143	3105	3107	3108	3191	3124
61	72	106	108	107	74	89
10	3	15		4	55	50

also begin clearly defined Drainage Ditch
Sect 90° to Forward Tangent
11466.24 - L. 2.0°00' Rt = end Rubble Conc Flume

3175	3152	3114	3117	3112	31420	3140
40	753	1034	1031	1027	710	75
10	35 TOP WALL	25		25	35 TOP WALL	10

11461 - BOTTOM Flume at N14 Wall

31121
1027

11458 - intersects N14 Wall & Rubble Conc Flume

31445
703

321.48 x

LT=514

Et=Nly

33

TPg 2.88 314.32 8.47 311.44

ON Hub L. 14+01.46

13+50

3114	3103	3086	3102	3110
8 ⁵	9 ⁶	11 ³	9 ⁷	8 ⁹
10	5		3	10

13+38⁶ = s.wly end 30" corg iron pipe under ^{51ST}

3152	3112	3072B	3114	3114	3137
4 ⁷	8 ⁷	12 ⁶³	8 ⁸	8 ³	6 ²
10	3	IE	5	10	25

13+30.11³ Et = L 12" pepper tree

13+22

3160	3150	3145
3 ¹	4 ³	5 ⁴
10		10

Section taken along L 51ST
12+92⁶ L intersects L 51ST ST

3155	3148	3122	3142
0 ¹²	5 ⁵	6 ¹⁶	5 ⁶
50		50 LOW POINT	100

TPg 5.51 319.91 0.95 31440

319.91 ✓

Under 51ST ST
12+69⁸ = ely end begin 30" corg iron pipe

3140	3122	30900	3118	3132
1 ³	2 ¹	0 ³⁵	2 ¹⁵	2 ¹
10	4	IE	20	10

315.35 ✓

16400

15465 & crosses creek

15450

TP₁₀

15400

14450

Sect taken 90° to Back Tangent
14401.46 to 37°23' Ct.

LT=514 - et=1/4 - 34

312.2	307.7	307.8	308.3	305.2	305.5
54	97	10	93	124	91
13	5	10	119	130	18
Top slope	Toe slope ORANGE		Toe slope ORANGE	BOTTOM creek	

312.8	307.8	306.2	305.8	307.8	308.0	307.5	308.0
48	98	114	118	98	96	101	96
19	12	10	9	5	10	10	25
Top slope ORANGE			BOTTOM creek				

9.20 317.62 5.90 308.42

308.9	307.7	307.8	308.0	317.62	308.6	310.7
54	66	65	53	54	57	35
11	9	5	3	25	25	20
Top slope ORANGE						

14473- & intersects & creek

310.5	308.2	308.2	308.5	308.5	309.5
34	46	3	50	58	48
25	2	3	3	6	10
Toe slope to orange ST			& creek		

314.32

TP₁₂ (328.87)^{0.04}
 0.32 328.91 ✓

TP₁₁ 11.96 329.23 ✓ 0.35 317.27 ✓

17+34.5 = IE S Wly end Wly 4x4 Box
 CULVERT

This INLET drops into Fly 4x4 Box
 17+15 ± Face Curb over INLET S.W. COR

(Below INLET Drops into Wly Box) A HADENAY DRAINAGE
 16+45.6 = Curb Face over INLET NE COR

Wly Box of two 13 boxes
 16+30.50 - INVERT 4'x4' Box CULVERT

Section taken 90° to Back Tangent
 16+21.00 L. 38°53'30" LT

16+06 - 9' LT = NE COR Wing Wall.

LT = S1Y NY = RT - .35
 Top Nly end Return NW COR S1ST Orange FB 2021-71

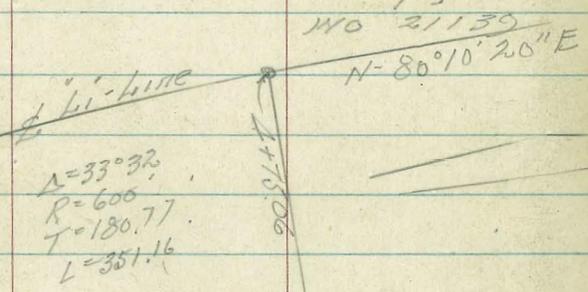
304.52
 13.10
 1E
 311.44
 6.18
 7.26
 Top Cb Top grate
 311.82
 5.13
 6.19
 Top curb Top grate
 305.91
 12.21
 1E

REMOVED BY LOCKHEAD
 7-14-53

	312.25	305.2	307.0	307.2	305.2	309.2
	5.37	12.4	10.6	10.4	12.4	8.2
	7.0	7.0	9	9	12	2.5
	TOP Wing Wall	grat Wall			BOTTOM creek	
312	312.24	312				
5.4	5.38	8.9				
10.2	9.2	9.2				
ground S1Y side	Top Wall	ground NY side				
						317.62 x

LOCATION EXISTING CULVERTS AND INLETS, ALSO PROPOSED EXTENSIONS OF DRAINS TORREY PINES RD. AND VIRGINIA WAY

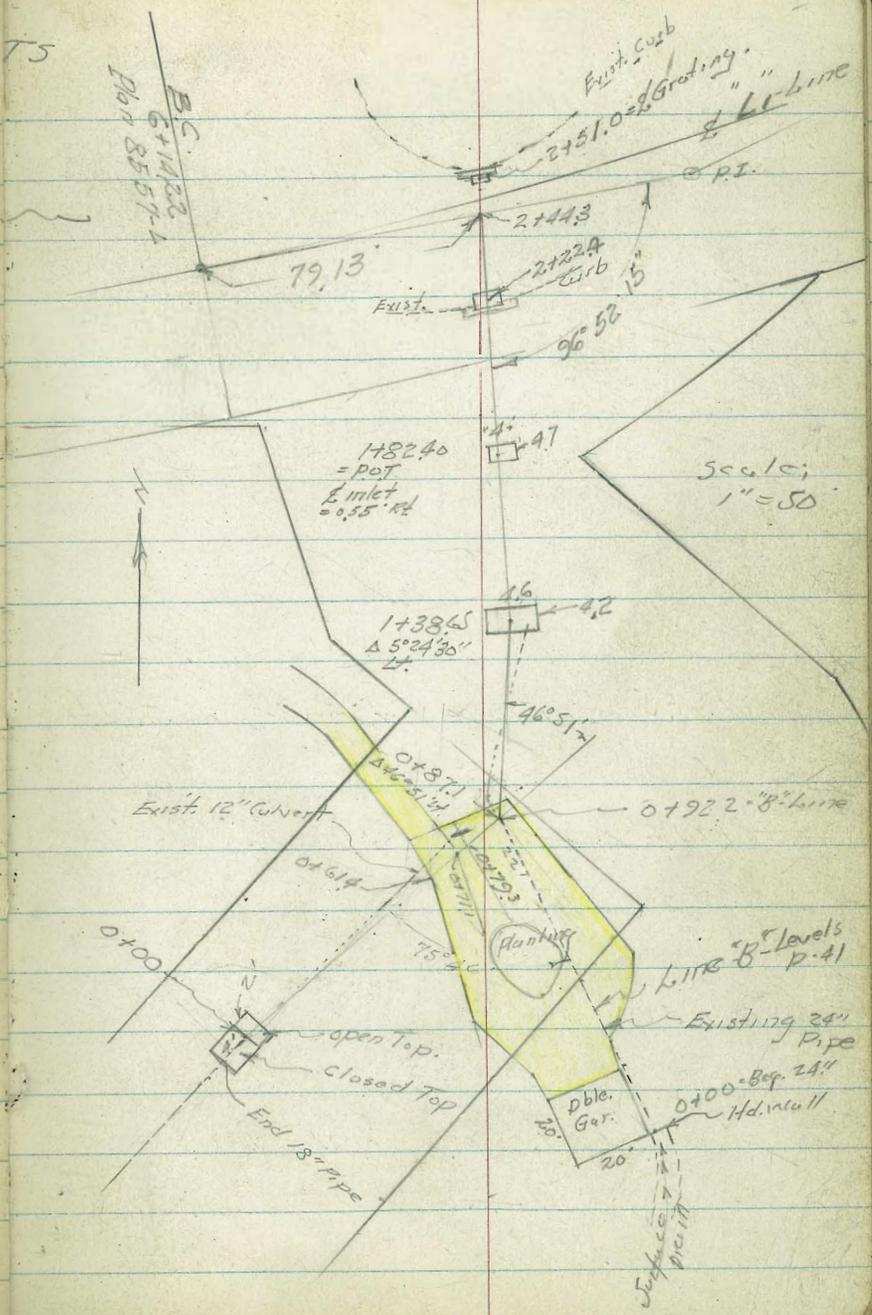
Mulker
Pope
Pullen
Olson
9-22-53



Levels P-37

INDEXED
SER
SEP 24 1953

See Also the Notes on Page 46



LEVELS FOR CULVERTS
AS PER LOCATION P 36

0+614 = 1st Conc. Pav. = Diag. Sec on Pav

TP 2.06 127.32 127.7 125.2.6

0+50

0+38

TP 12.5 138.03 133.1 136.78

0+285 = opp Cor Hot House 5.5'lt

0+146 = opp. Cor. Hot House 8.9'lt

0+00

12.31 150.09 0.02 136.78

12.78 136.80 0.19 123.82

10.42 124.01 113.59

121.61	120.34	120.41	120.75
571	698	691	6.57
15	82	101	8
Pav.	Pav.	Pav.	Conc. Pav
	Brk	127.32	

124.6
13.4

133.7

4.3

138.03

137.9

12.2

12.0

8.1

146.46

146.24

1.63

3.85

Add wall

0

Invert

150.09

B.M.
S.W. B.P. TORREY RD And CORST BLYD.

F.B. 3094
60

1706 \pm = 16" Fire Tree 61' Rt

0+98.6

0+92

0+87.1 = Δ Lt, 46° 51'

0+87.1 Sec. Rt Δ to Buck Turn

0+83 = opp End 12" Conc. Pipe

0+79.3 = ^{Diag Sec} Low Pt in Pav = Valley

0+71.1 = Bk in Pav

114.90 118.8 115.64

12.42 8.5 11.58

1.2
on Top
8" 24" Pipe

116.34

10.98

6.5
on Top
Sewer
Pipe

119.49 119.63

7.83 7.69

2.4
Edge
Pav

116.05

11.27

1.0
invert

118.74 118.66 118.78 120.32 120.75

8.58 8.66 8.54 7.00 6.57

4.6 2 1.5 2.1
Edge Pav 4" x 4" Grating Bk Edge Pav

120.37 119.56 119.82 120.87

6.95 7.76 7.50 6.45

1.0 5 1.86
Bk Pav Pav

127.32

TR 747 116.91 1330 109.44

P.O.T.
1+824 = cleanout

7' Lt.
= 10" Euc. Tree

105.68 109.43 110.6
1706 1331 121
Bottom Box Grating Ground

1+57

110.5
12.4

1+53 = 1/2 30" Euc. Tree 5' Lt.

1+50

112.5
10.2

1+38.65 Δ 50 24' 30" Lt.

109.36 114.04 109.42
1333 8.70 1332
Bottom Grating 1.8 = 1/2 24"
Conc. Box Inlet

1+30

117.4
53
122.74

TR 552 122.74 1010 117.22

1+29 = 1/2 18" Euc. Tree 2.5' Lt.
127.32

chk. Starting BM 333 ⁰⁰¹
 113.59
 113.58

2+51 = 2 Grating

2+35

2+21.3 = 1/2 Exst. Curb kerne = 2 Inlet

2+19.8 = 2 Stand Pipe

2+00

1+99 = 16" Exc. Tree 5' RT

110.05 108.88 100.10
 686 8.03 16.81
 cb. Grating 0
 Bottom
 Conc. Box

111.00
 591
 Pav.

111.52 110.92 107.68
 539 599 923
 0 0 0 = Bottom
 Conc. Box
 103.03 Grating
 1388
 111.9 Invert
 50

116.91

LINE "B"
Culvert

Lt

£

FF.

41

0+92.2

119.63

769.

0+82

120.13

119.70

120.44

120.77

7.19

7.62

6.88

6.55

15.7
Pav.

8
Pav.
Yurley

7
Edge Pav.

0+70

120.86

120.73

121.15

121.70

6.46

6.59

6.17

5.62

16.4

8.8
Pav.
Low H.

10.4

Edge Pav.

0+44.5

123.04

122.44

122.44

122.55

4.28

4.88

4.88

4.77

30
Edge

10
Pav.

Pav.

12.5
Pav.
Edge

10

0+27.7

123.60

123.32

123.32

3.72

4.00

4.00

2.2

Edge
Pav.

11
Pav.

Conc. Pav.

0+20

0.67 ft = Cur. Garage.

0+00-

1.4 ft.
= Cur. Garage

122.19

126.54

5.13

0.78

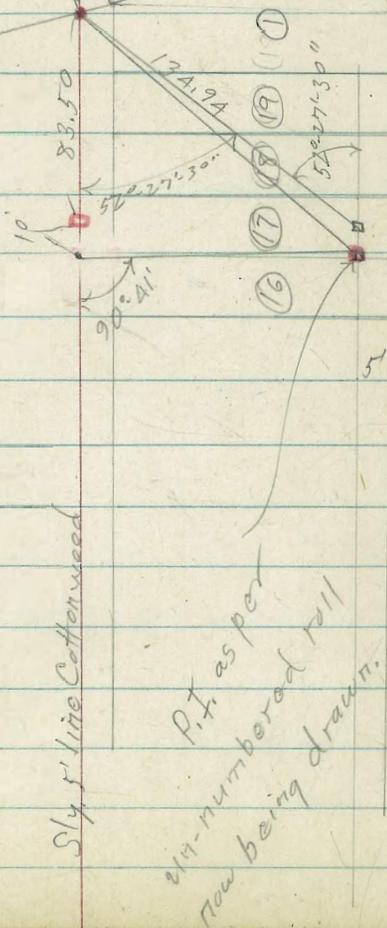
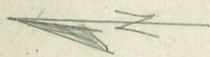
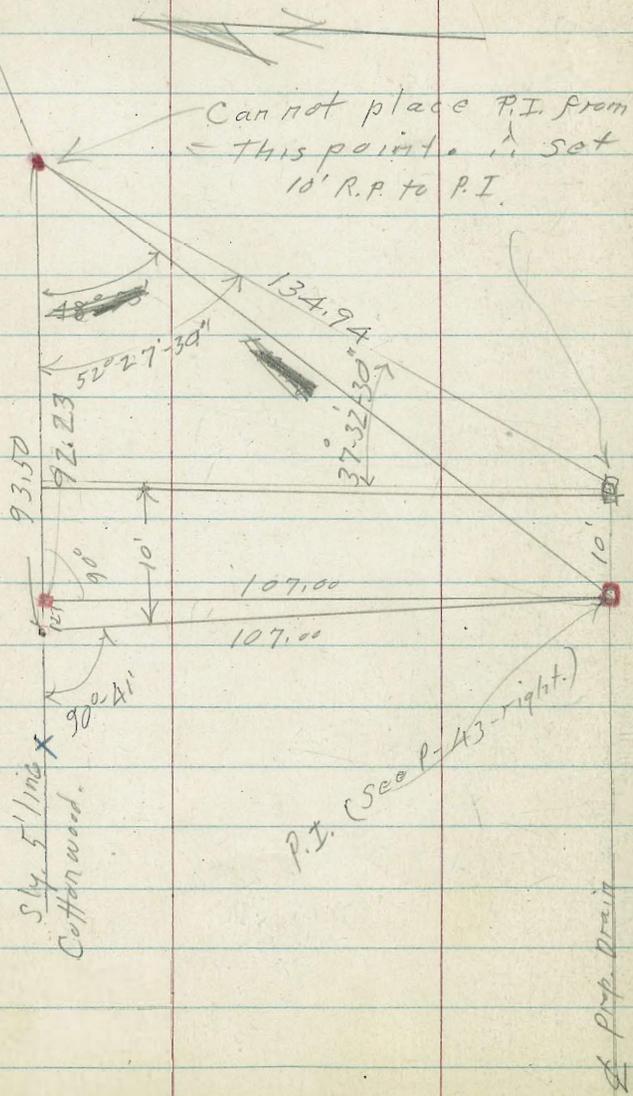
0
17" set
24" Pipe

Top Hd Wall

127.32

T = P 38

Detail for setting of P.I. shown on page 42



± stakes on proposed
Location of drain thru
Blk 2 Nordica Hqts
and in Cottonwood street.

Lath only on stations listed
excepting where noted
otherwise

0 + 66.06 = E.C.

0 + 60

0 + 50

0 + 40

0 + 30

0 + 20

0 + 10

0 + 00 = B.C. Lt. - Page 42

0 - 25

0 - 50 } on ± (on Tang. from west)

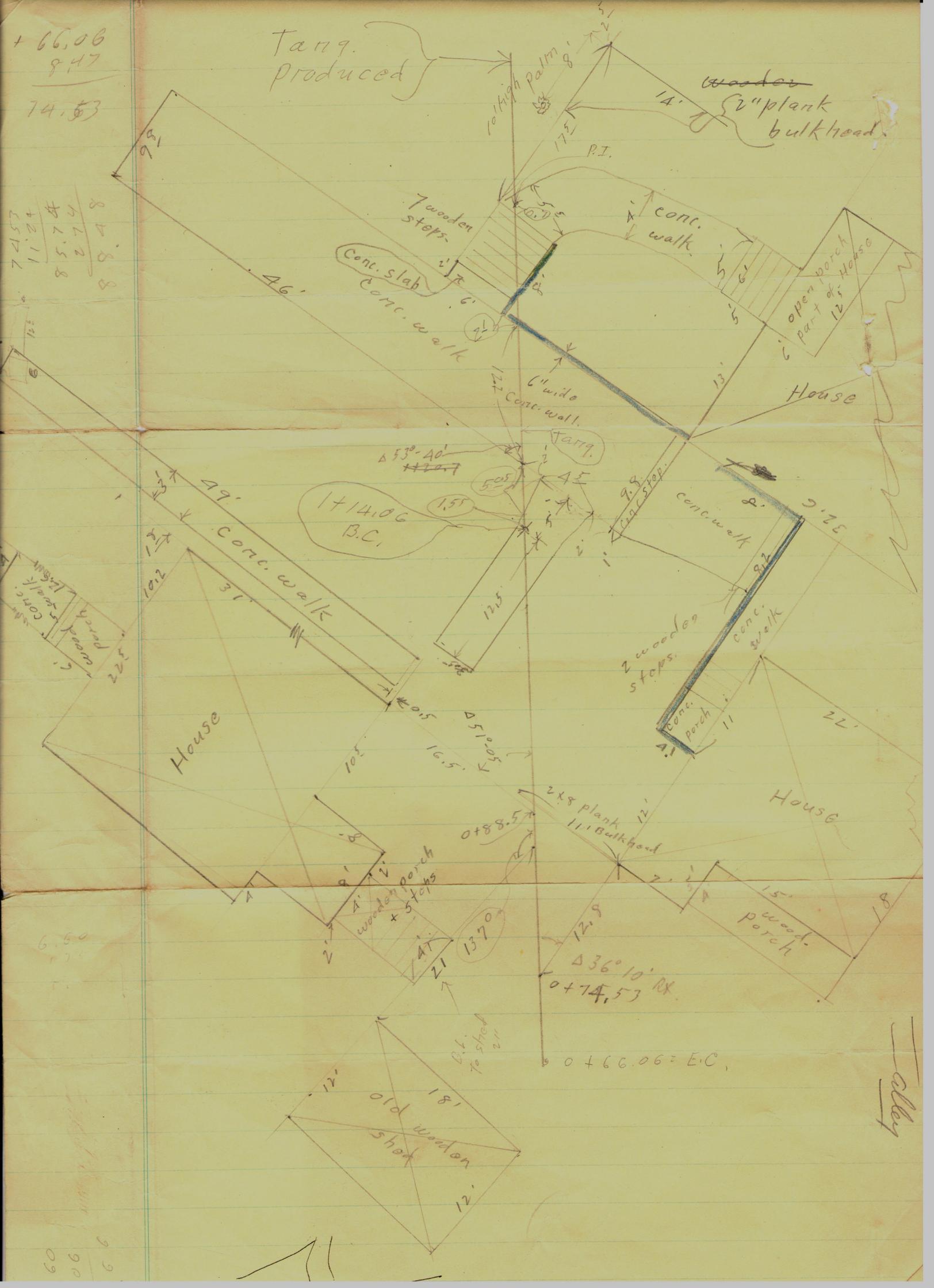
0 - 75

+ 66.06
8.47

Tang.
Produced

74.53

7.2153
11.24
85.74
2.70
88.48



wooden
2" plank
bulkhead

open porch
part of House

House

1+14.06
B.C.

House

House

wooden porch
+ 5 steps

wood.
porch

old wooden
shed

$\Delta 36^\circ 10'$ rx
0+74.53

0+66.06 = E.C.

alley

60
90
99

$$2 + 33.41 = \angle Pt. - \Delta 19^\circ 42' RT.$$

$$2 + 13.00$$

$$1 + 93.0$$

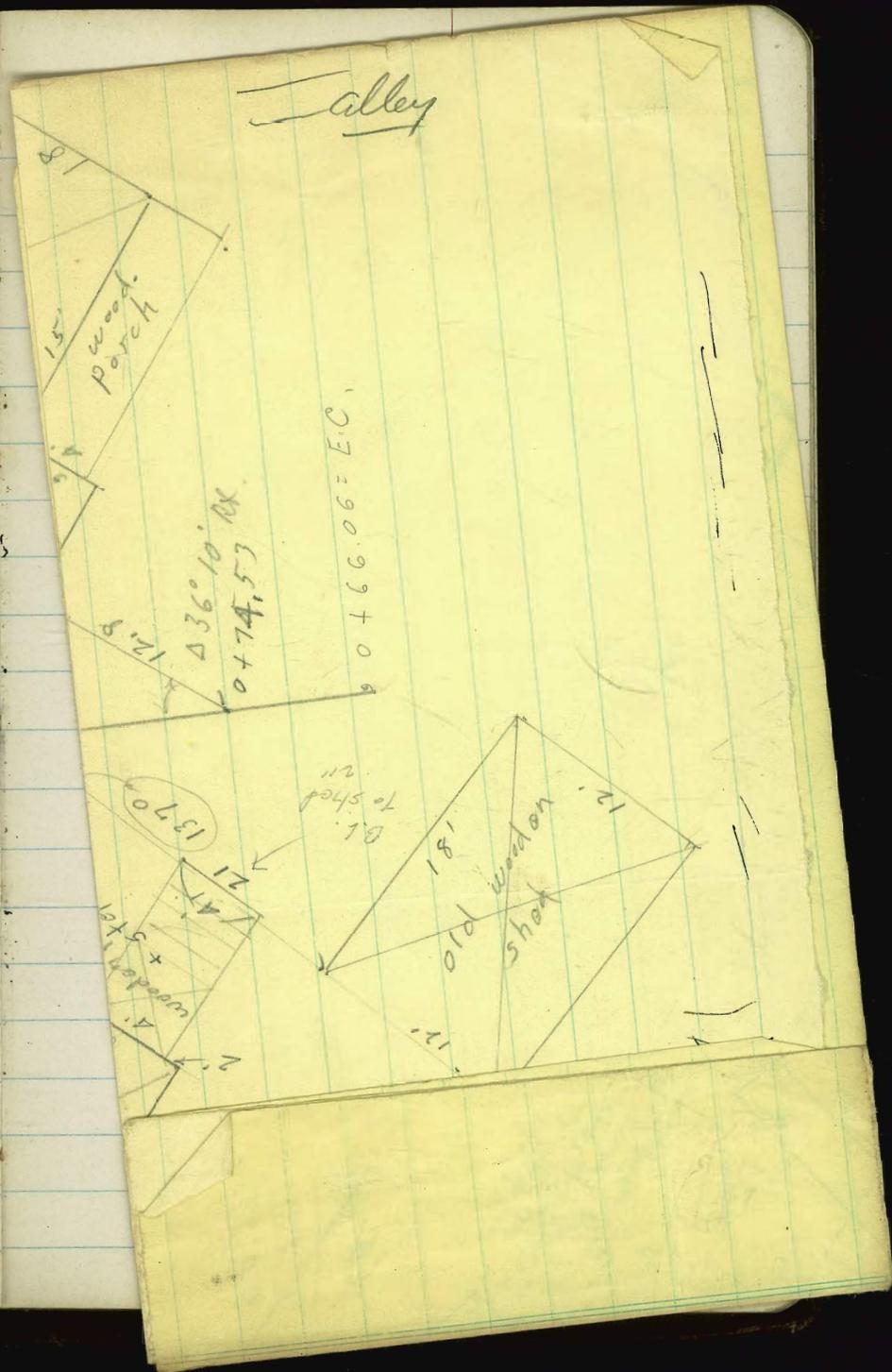
$$1 + 72.70 = E.C. = Nail + lath$$

$$1 + 53.16$$

$$1 + 33.61$$

$$1 + 140.6 = B.C. Lt. = Cross on walk.$$

$$0 + 90$$

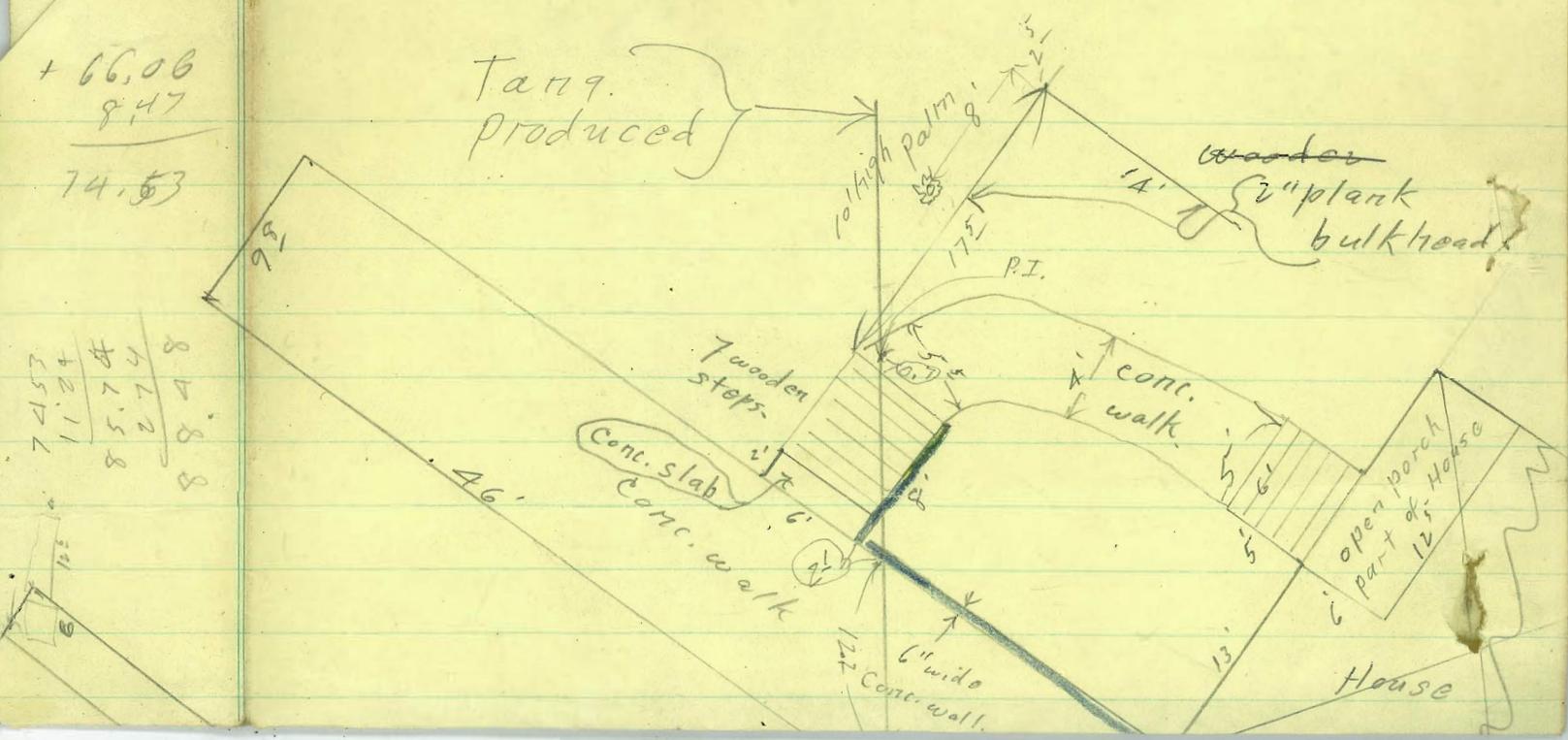


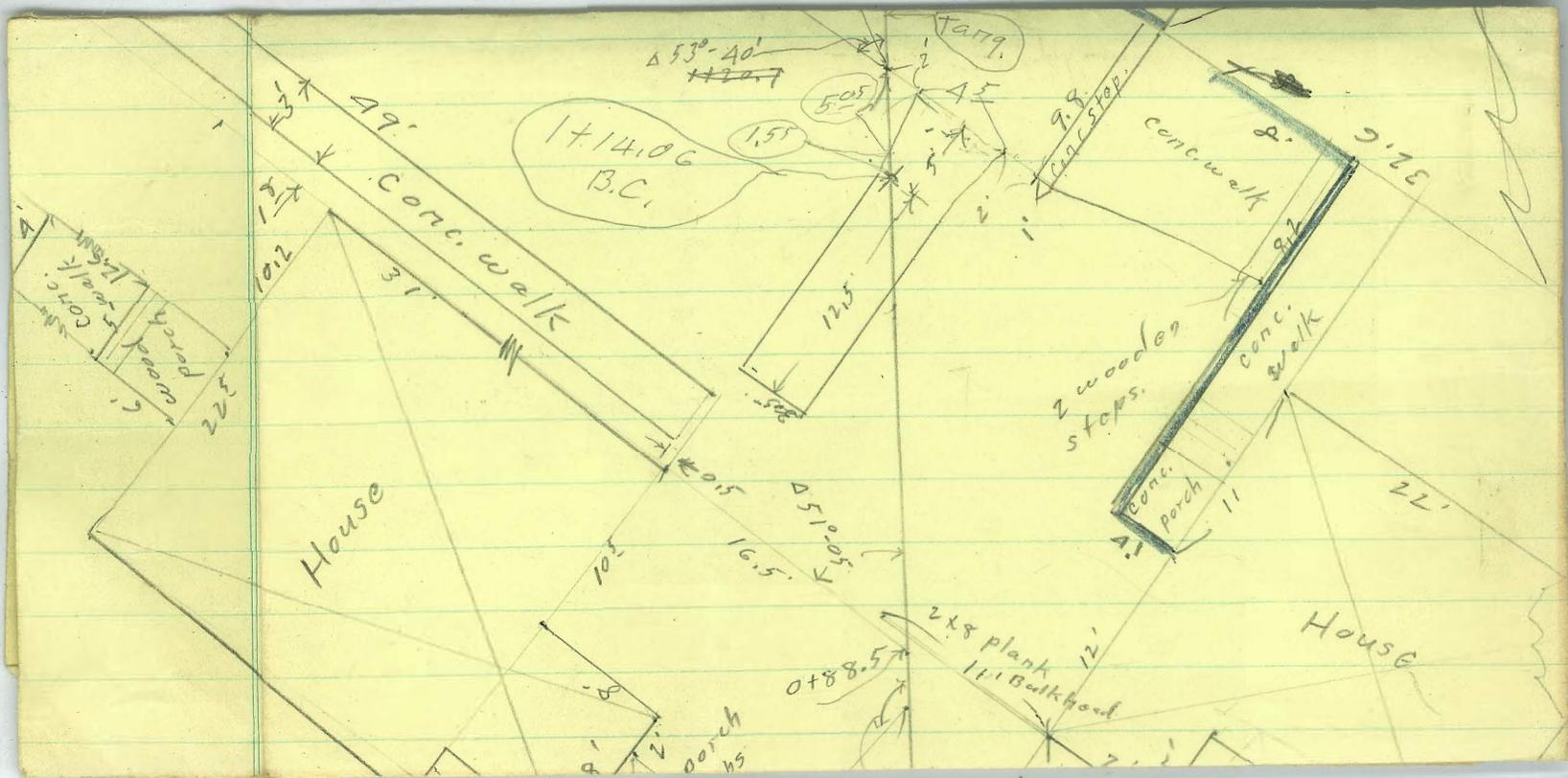
+ 66.06
 8.47

74.53

74.53
 11.24
 85.74
 2.74
 88.48

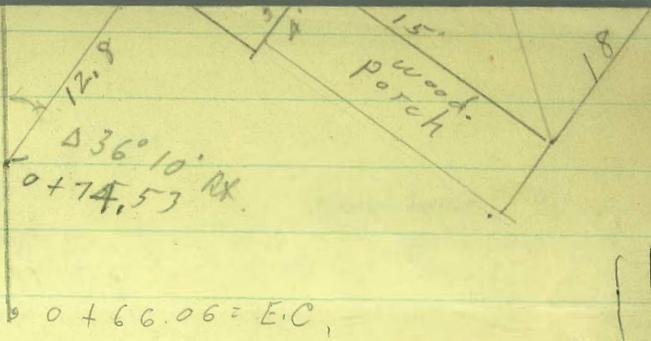
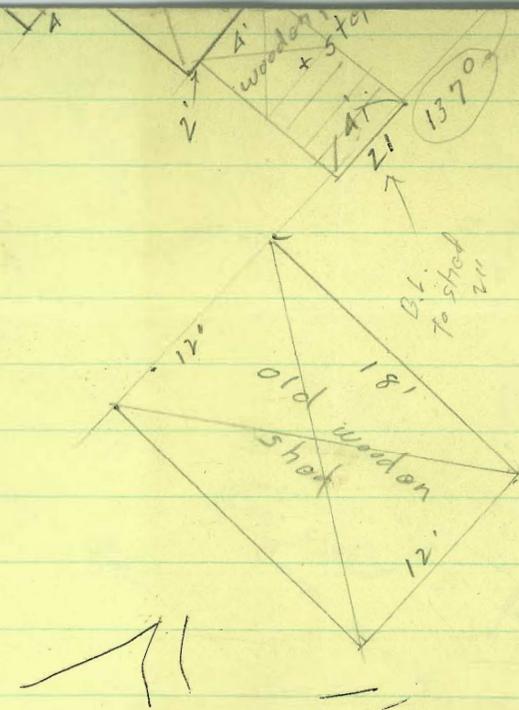
Tan 9.
 produced





6.60
172

6.60
141.06
20.66



st. wall.

D. Smith
 J. Rorer
 R. Taylor
 B. Fish

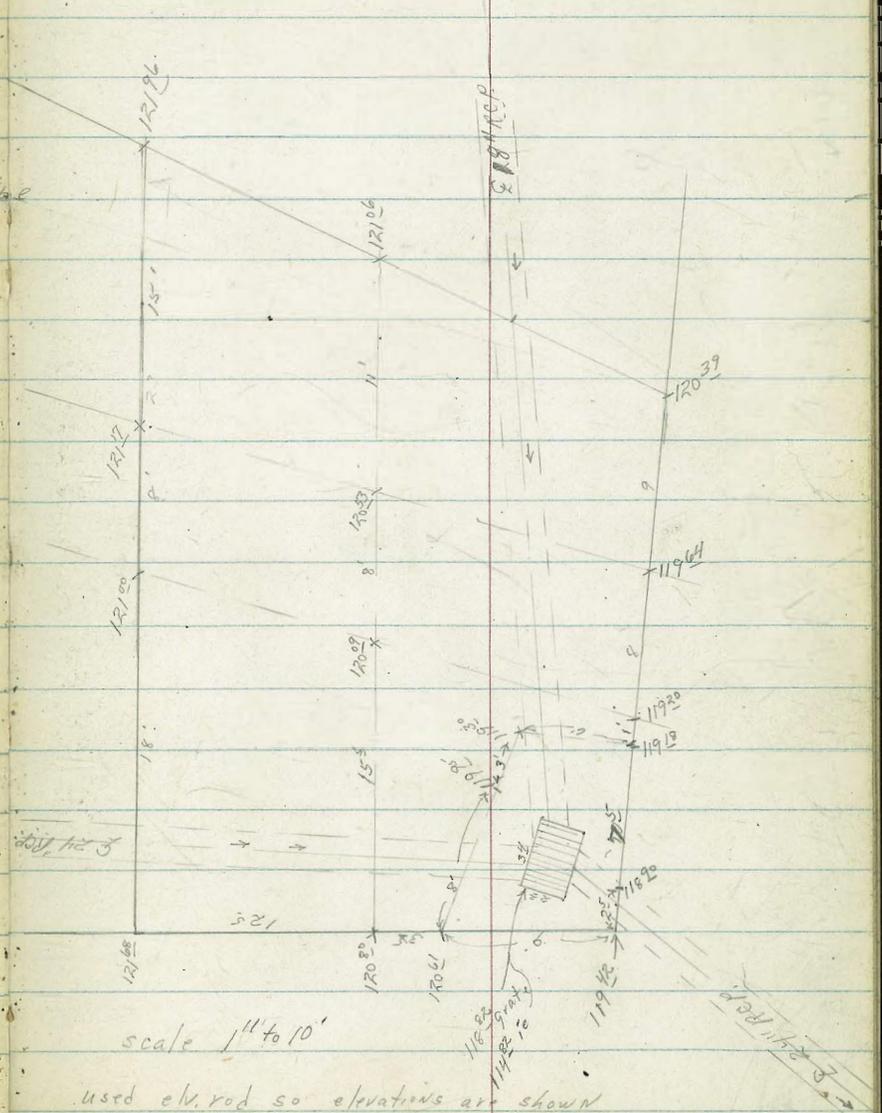
Check Plan 5099-B As Built near 1575 Torrey Rd.

Wot 21139 46
 4/22/54

Connection #1 pipes Flow lines & 18" don't match by 2" and collar top isn't large enough to cover top of down grade pipe
 seal

Refer Back to Page 36

gauge



BM 11359 SE BR Torrey Aves Rd + Coast Blvd.

Clark
Shepherd
Bruner
8-23-64
W.O. 21148

REF MAP # 2527

Elev's (Elev.) - 5546 + HARDY
EXIST. (Pav.) - CR'S + CUTTS
Proposed CROSS-DRAIN - ELY 5546 + HARDY

chk.

439.98 = 439.98 (see B.M.)

INDEXED
SER
AUG 24 1954

439.93
607.43678

CR A: 76°25'25"
CR R: 42.64
CR L: 67.14
CR L divided 4 pts (R.O.S. incl)

INLET W.P. = 15.4
GATE 35 wide

55.7A ST Q

HARDY

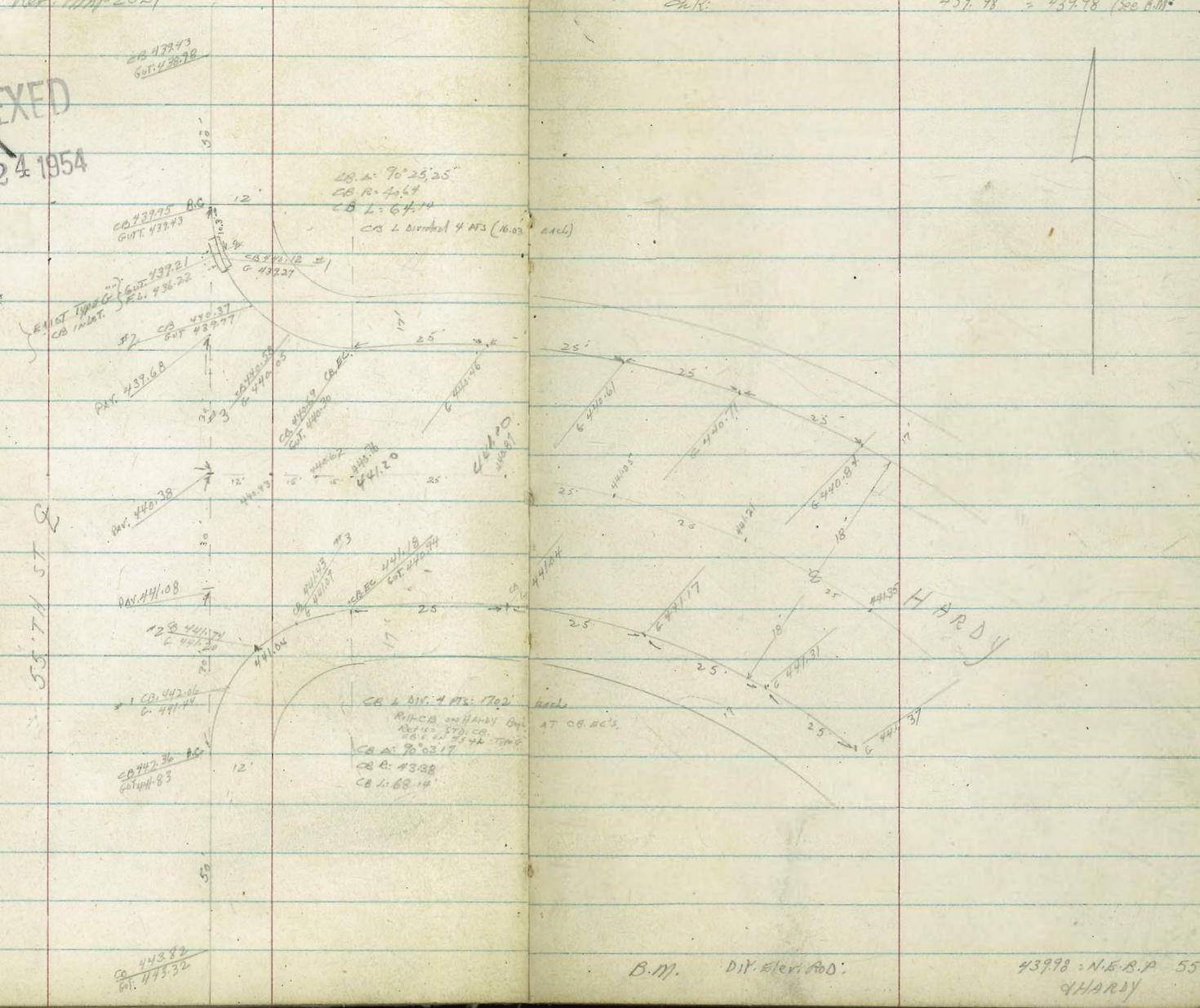
12'

CR 443.82
607.44532

CR L Div. 4 Pts: 1702
R/O CR on HARDY Gwy.
R.O. = 570.00
CR L = 5546 + TRNG
CR A: 76°03'17"
CR R: 43.38
CR L: 69.14

B.M. DIX. Elev. Rod.

439.98 - N.E.R.P. 5546
HARDY

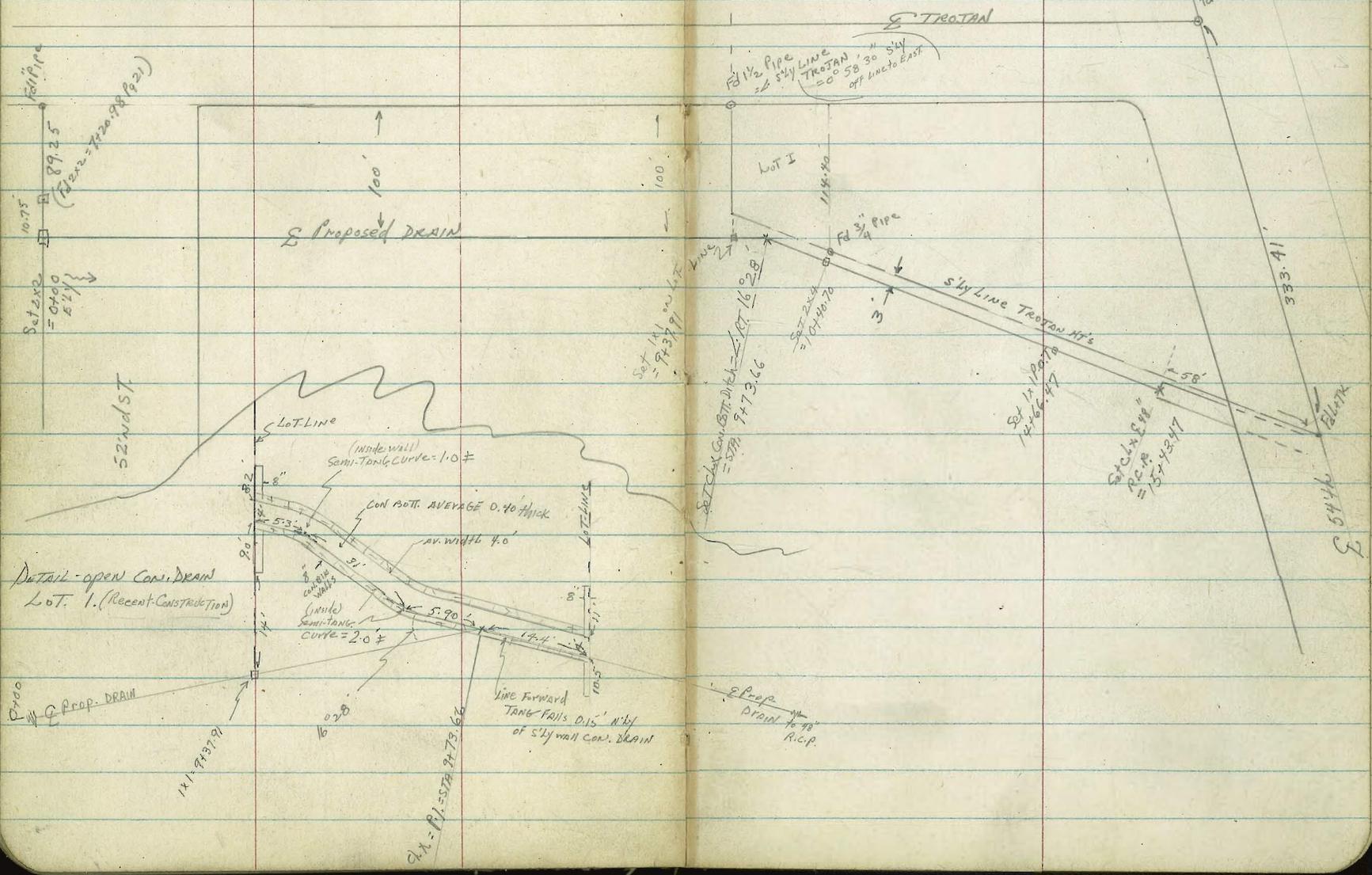


Clark
GAMBER
BRUNER
O'NEIL
12-15-55
W.O. 21071

Proposed DRAIN: 52'nd to
54th; Sly of TROTAN

Ref: Pg. 12-21
map 2447-2

INDEXED
DEC 19 1956
48



Detail - open con. drain
Lot I. (Recent Construction)

Prop. DRAIN

Prop. Drain to 78' R.C.P.

S TROTAN

Fd 1/2 Pipe Sly
LINE TROTAN
= 0° 58' 30" Sly
OFF LINE TO EAST

Lot I

Fd 3/4 Pipe

Sly Line Trotan H's

333.41'

54th St

Proposed DRAIN

52nd St

Lot Line

(wide wall)
Semi-Tang Curve = 1.0'

CON BOT. AVERAGE 0.40 THICK

av. width 4.0'

(wide)
Semi-Tang
Curve = 2.0'

Line Forward
TANG POINTS 0.15' N'W
of Sly wall con. drain

141.913791

C.M. = P1-574 7473.66

Set 1/4 on Lot
= 943.79

Set 1/4 on Lot
= 574 7473.66

Set 2 1/4
= 10740.70

Set 1 1/2 Point
= 4166.47

Set 1 1/2 Point
= 57473.47

1075
Set 1/2 Pipe
= 89.25
(P1-574-72098.92)

Set 1/2
= 0400
511

100'

100'

14.80

58'

8 Prop

DRAIN to 78' R.C.P.

Proposed DRAIN 52nd to 54th

3+00

2+50

2+00

1+50

1+00

0+55

cross N+S Barbed-wire Fence

0+50

0+00

0+30

7.5 LT & M.H

0-50

B.M.

4.23

327.74

323.51 = 2 x 2

(5722.67 Pg 21)

LT (N4) $\frac{323.6}{25}$ 1.9 325.8 RT (S4) 79
 $\frac{331.9}{25}$ +4.2

$\frac{323.0}{25}$ 1.6 326.1 327.7
 $\frac{322.6}{25}$ +5.0

$\frac{322.6}{25}$ 3.0 324.7 327.7
 $\frac{321.3}{25}$ +3.6

$\frac{322.3}{25}$ 3.1 324.6 327.7
 $\frac{321.3}{25}$ +3.0

$\frac{321.3}{25}$ 5.1 322.6 327.9
 $\frac{321.3}{25}$ +0.2

$\frac{322.7}{25}$ 5.5 322.7 324.5
 $\frac{322.7}{25}$ 5.0 3.2

$\frac{319.7}{25}$ 8.0 320.3 321.9
 $\frac{320.7}{25}$ 7.4 5.8

$\frac{318.14}{25}$ 3.87 317.9 318.1
 7.5 RIM 7.8 9.6

327.74
 $\frac{327.74}{1}$

52nd - TROTAN - CONT.)

LT. Σ RT 50

6+50

~~3.7~~
25
329.0 ✓

2.8
25
329.9 ✓

0.7
25
322.0 ✓

6+00

~~4.8~~
25
327.9 ✓

~~4.8~~
25
328.6 ✓

2.1
25
330.6 ✓

5+78

4.4 RT Σ 18" Pepper Tree ✓

5+50

~~5.3~~
25
322.4 ✓

5.1
25
327.6 ✓

3.4
25
329.3 ✓

5+00

4+84 7' LT Σ 36" Pepper Tree ✓

4+83 Cross NIS Barbed-wire fence ✓

4+50

~~5.9~~
25
326.8 ✓

4.8
25
327.9 ✓

3.7
25
329.0 ✓

4+20

3.6 LT Σ 18" Pepper Tree ✓

~~6.7~~
25
326.0 ✓

5.5
25
327.2 ✓

3.7
25
329.0 ✓

T.P. 5.70 332.72 0.72 327.02

7+00

325.04
2.7
25
324.4 ✓

332.72
1.3
25
326.4 ✓

329.9
+2.2
25
327.9 ✓

3+50

324.4
3.3
25
324.4 ✓

1.3
25
326.4 ✓

329.9
+4.0
25
327.9 ✓

327.74

52nd - TROJAN - Cont.

9+38 (9137.91) 25' LT = E 4' Con. DRAIN (sect. along Lot-Line)
(See Sketch)

9+32 BRK

9+00

8+50

T.P. 9.33 340.21 1.84 330.88

8+00

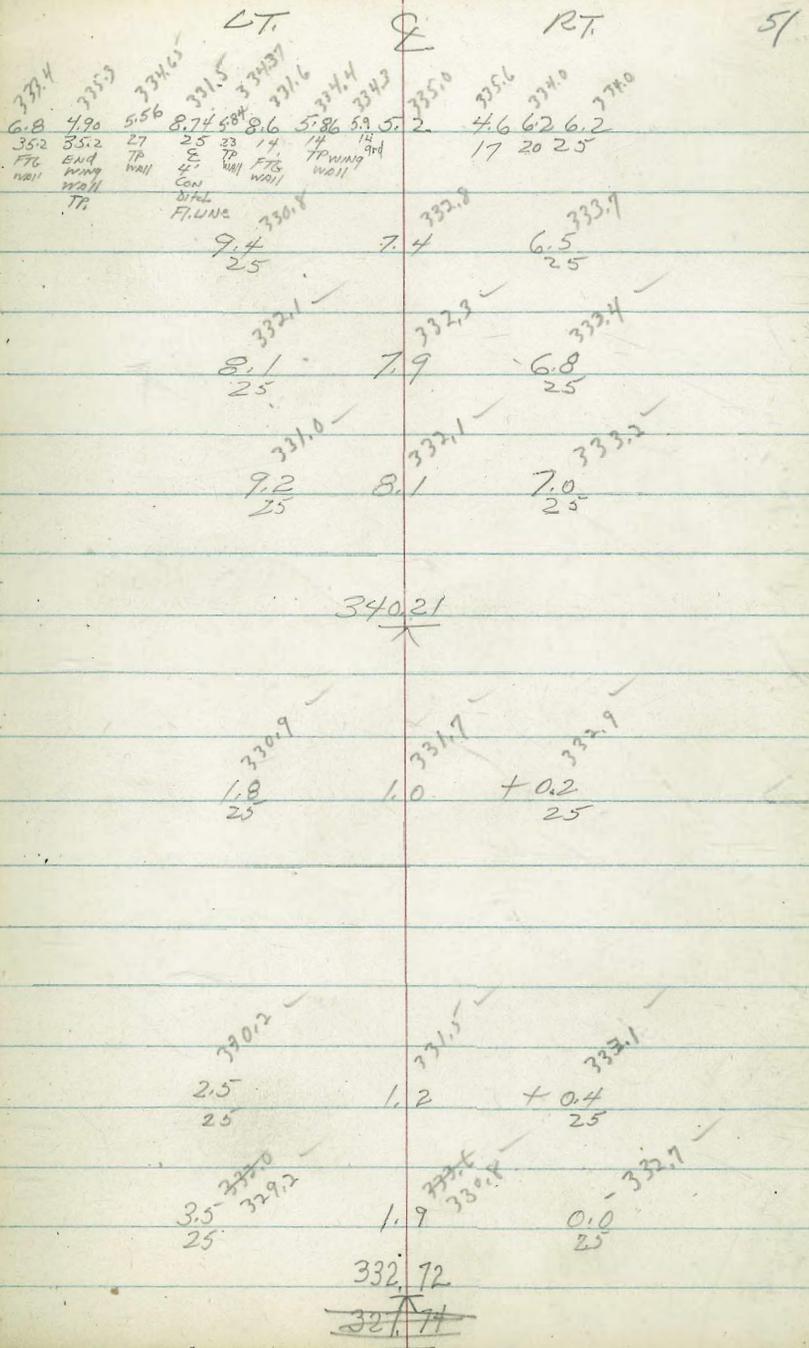
7+91 15' LT E 18" Pepper Tree ✓

7+64.5 Cross N/S Barbed Wire Fence ✓

7+50

7+11 3.1 E 12" Pepper Tree ✓

7+00



450

10145

10126

10117

10100 (profile - here-on)

9188 1.85 LT ⊙ CON. DRAIN (sect. along lat-line)
(see sketch)

9173.66 = LRT 16° 28

Note: (inside line wall)
Falls 0.15' SLY of line

9150

9139.5 12' LT ⊙ 36" Cypress

3351.1
5.1

3327.7
7.5

3327.7
6.5

3356.6
4.6

3343.3
5.9

3332.2	3351.94	336.02	332.07	332.24	332.77	335.98	335.10	332.8	335.7
70	4.27	4.19	7.41	7.37	7.34	4.23	4.81	6.4	4.5
FTC	14.9	3.9	3.85	1.85	2	0.15	10.65	FTC	20
WALL	TP	TP	Bot	Bot	Bot	TP	TP	TP	9d
END WALL	WALL	WALL	DRAIN	DRAIN	DRAIN	WALL	END WALL		
336.2	335.4	335.29	332.11	332.43	332.45	334.97	335.2	335.9	
4.0	4.8	4.62	7.80	7.78	7.76	5.24	4.4	4.3	
15	5	4	2	2	2	20	20	25	
9rd	TP	TP	Bot	Bot	Bot	TP			
	WALL	WALL	DRAIN	DRAIN	DRAIN	WALL			
						(Flush 9rd)			
331.95	334.78	334.12	335.10	335.6	336.1				
8.26	5.43	6.0	5.2	4.6	4.1				
16.24	14.24	14	15	15	25				
E	TP	9rd							
CON	WALL								
DRAIN									
FLINE									

340.21

52nd - TROJAN - (CONT.)

FT.

Σ

RT.

53

+50

2.6

3454

+16

6.

3419

14+00

5.

3429

+60

4.6

3434

+50

Beq area loose } Fill (see also pg 13)
& scattered

7.2

3448

13+00

8.5

3395

12+50

9.3

3389

T.P.

9.24

347.95

1.50

338.71

347.95

12+00

8.3

3379

+50

2.9

3373

11+00

4.3

3359

340.21

52nd - TROJAN - 54th (CONT.)

LT.

E

RT.

54

Re checked
Had the
12-20-21

CHK:

14.89 340.77 = 340.79 = F.L. EXIST.
48" Pipe
(#13)

15+43.47 = 2 EXIST Pipe

+10

340.77 ✓
14.89
F.L. Linc 48" Pipe (see Pg 13)

15+00

343.2 ✓
12.5

14+94

346.1 ✓
9.6

T.P. 9.62 355.66 1.91 346.04

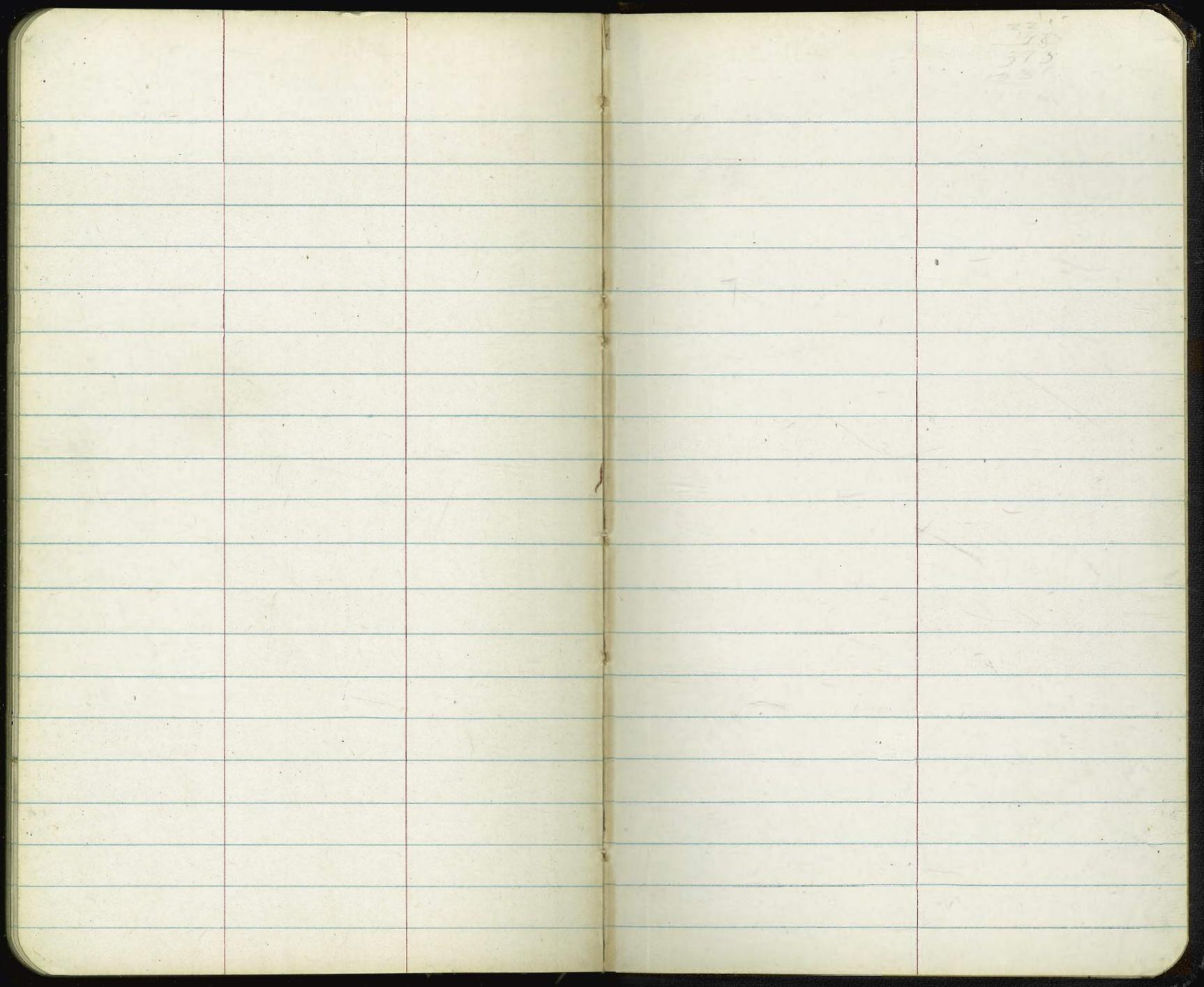
348.5 ✓
7.2

14+60

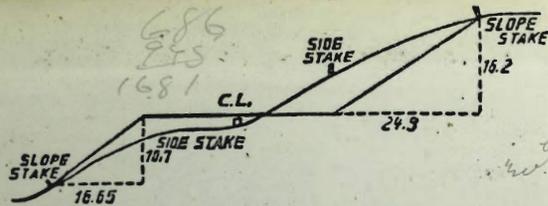
355.66

347.7 ✓
0.3

347.95



33
34
35
36



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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