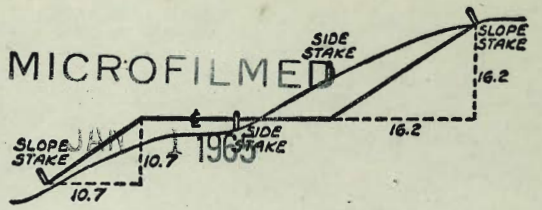
2215

SEWER

Kemper St. Sewer
V.O. 62289

TRANSFER BOOK



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

2215
Sewers

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

D. Smith
C. Allen
R. Taylor
R. Parks

Profile Murray Canyon Sewer

wo# 20789
3-13-52

					℄
+50					23.3 / 6 3
5+00					23.2 / 6 4
+50					23.1 / 6 5
T.P.	6 27	29 58	11 03	23 31	
4+00					23.1 / 11 2
+50					23.1 / 11 2
3+00					23.1 / 11 2
+50					23.1 / 11 2
2+00					23.0 / 11 3
1+54 Make Connection					22.6 / 11 7
		34.34 use		28 29 new rim SMH #30	
B.M.	6 05	32 73		26 68 Been moved? p 12 FB 877	

	℄
+50	25.0 / 4 6
10+00	25.1 / 4 5
+50	25.1 / 4 5
9+00	24.8 / 4 8
+50	24.6 / 5 0
8+00	24.4 / 5 2
+50	23.9 / 5 7
7+00	23.9 / 5 7
+50	23.7 / 5 9
6+00	23.4 / 6 2

I 29 58

14+28	36' Lt Ely edge 40' long 20' wide pond	9.2	6.7	21.6 / 5.2	5.9	5.9	
		36 water level	35		10	20	
14+00		4.3	5.3	22.0 / 5.5	6.0	6.3	
		20	10		10	20	
13+75		7.0	6.2	21.8 / 5.7	5.6	5.4	
		20	10		10	20	
13+50		3.4	3.2	21.0 / 3.5	3.6	4.2	
		20	10		10	20	
TP		2.45	2.40	24.20			
12+94.6	BS P.O.T. Hub BM. elv. 24.70	4.88	29.58	26.70 / 4.88			
+50				24.5 / 5.1			
12+00				24.5 / 5.4			
+50				24.7 / 4.9			
11+00				24.8 / 4.8			
			29.58				

				23.3			
16+00		4.8	4.6	4.2	3.9	3.0	
		20	10		10	20	
15+86		5.0	4.4	22.7 / 4.8	4.5	3.9	
		20	10		10	20	
15+84	Nly channel	10.9	10.7	16.8 / 10.1			
		20			10		
15+50	Sly S.D. River Channel	9.6	8.8	17.5 / 10.0			
		20	H2O level		20		
15+45		7.6	7.6	20.1 / 7.4	7.3	7.1	
		20	10		10	20	
15+25		3.2	2.8	23.5 / 2.0	1.3	2.2	
		20	10		10	20	
15+00		5.8	5.6	22.1 / 5.4	5.4	5.5	
		20	10		10	20	
14+60		6.3	5.7	22.2 / 5.3	5.8	6.0	
		20	10		10	20	
14+52		8.1	7.9	19.7 / 7.8	7.8	7.6	
		20	10		10	20	
				27.45			

	Lt	℄	Rt
17+30 bottom pond		15.3 13 4	
17+26 water edge pond 150' Lt. & 70' Rt ℄		14.3 9 4 water level	
17+20 Top pond (new)	2 1/10	26.0 2 2	2 5/10
17+00	2 8/10	25.7 3 0	3 3/10
16+65	3 9/10	25.1 3 6	3 3/10
16+55	7 6/10	21.4 7 3	8 4/10
16+44 ℄ Cr #2 (new)	9 5/10	19.8 8 9	8 2/10
16+30	7 8/15	21.8 6 9	6 5/15
16+20	3 9/10	25.6 3 1	2 6/10
BM 320	28 66	24 76 Hub 22+82 13	

	℄
7+50	24.6 4 1
21+00	24.9 3 8
+50	24.4 4 1
20+00	24.0 4 2
+50	23.4 5 3
19+00	23.6 5 1
+50	23.9 4 8
18+00	24.4 4 3
17+55	24.6 4 1 4 2/10
17+50 bot pond	15.3 13 4
TP 28 66	

			℄	
+50			11.2	25.7
25+00			11.4	25.5
+50			11.6	25.3
24+00			11.7	25.2
+50			11.6	25.3
23+00			11.5	25.6
	12.10	36.86	24.26	
22+82.13 L.Rt elv. 24.76 ± Hub FB 18 77-18			3.91 on Hub	
+50			3.6	25.1
			3.5	25.2
22+00				
			⊼ 28.66	

	℄	
+60 AC	1.7	35.2
+30 Begin AC Drive	1.4	35.5
28+00	1.3	35.6
+ 70 end AC Begin grass area Parking	1.6	35.3
+50 AC	1.2	35.7
27+00 AC	2.2	34.8
+70 Begin Ac parking area	2.0	34.9
+60 AC	8.9	28.0
+50	10.0	26.9
26+00	10.9	26.0
⊼ 36.86		

		34.3
450		63
		34.2
30400		64
		34.1
30460		65
		33.5
30445		81
		32.4
30440		82
		33.5
29438		71
TP on Hub	5 45	40 56
29422 44 Pot Hub elv. 35 11		176 Hub
		35.2
29412 N edge Road		12
		34.4
30475 AC gut		25
		36.86

		5
TP	5 70	46 20
		0 06
35+54 76 Lt At elv 40 50 1677-25		0 06
		39.8
35400		08
		38.4
30450		20
		39.3
34400		13
		38.00
30450		26
		36.3
33406		43
		35.1
30450		55
		34.1
32400		59
		34.9
30450		57
		34.3
31400		63
T	40 56	

38+00		47.8 2 9		
+75		46.9 3 8		
37+50		46.1 4 6		
TP	5 19	50 20	0 69	45 51
37+00		44.3 1 9		
+80		42.5 3 7		
+55		39.9 6 3		
+27		39.7 6 5		
+17		40.7 5 5		
36+00		41.0 5 2		
		4 6 20		

40+50	+1° 13	44.1 6 6	5 7 10	
40+00	+1° 14	44.3 6 4	6 6 10	
+75		44.0 6 7		
+60		49.8 0 9		
+40		48.8 1 9		
39+00		46.4 4 3		
+90		46.2 4 5		
+65		42.4 8 3		
+55		41.1 9 6		
+45		42.9 7 8		
38+23		47.7 3 0		
		5 6 20		

44+00			46.7 5 6		
+50			45.9 6 4		
43+00			45.1 7 2		
+50			44.5 7 8		
TP	8 63	52 31	7 02	43 68	
42+00			43.8 6 9		
41+70			43.5 7 2		
41+35		+2 3 10	43.1 7 6	7 8 10	
41+20		+1 6 5	47.1 3 6	7 7 6	
41+05		11 0 10	+0 8 3	50.5 0 2	7 4 11
40+85		+0 8 6	48.6 2 1	5 8 4	
		T 50	70		

				53.3	
+50			4 8 7	N 9	12 5 10
				53.3	
48+00			5 6 7	N 9	12 6 10
TP	13 17	6 5 23		0 25	52 06
+50				52.0 0 3	
47+00				51.1 1 2	
+50				50.3 2 0	
46+00				48.6 3 2	
45+52 40		3°31'15" LRT		48.3 4 0	
45+00				47.7 4 6	
44+50				47.1 5 2	
T				52 31	

℄

+50 — 66.5 — 10 4

+16 Begin Bottom wash — 65.1 — 11 8

+07 — 70.1 — 6 8

51+00 — 69.9 — 7 0

+50 — 67.8 — 9 1

50+00 — 65.7 — 11 2

TP 12^{27} 76^{90} 0^{60} 64^{63} — 10 ft off guard rail end, Nail in post

Lt Bridge Culverts washed out

$49+38^{43}$ ∠ Lt 6°39′15″ — 1 0 — 64.2

+15 — 53.9 — 11 3

49+00 — 53.9 — 11 3

⊼ 65^{23}

89^{16} ℄ 6^{72}

elv. 82^{44}

$54+19^{91}$ ∠ Lt 23°28′ — 6^{72} Hub

+80 — 81.6 — 7 7

+73 — 83.1 — 6 2

TP 12^{55} 89^{26} 0^{19} 76^{71}

+64 — 75.4 — 1 5

+58 end Bottom wash — 73.2 — 3 7

+50 — 71.2 — 5 7

53+00 — 71.7 — 5 2

+50 — 68.4 — 8 5

52+00 — 67.4 — 9 5

⊼ 76^{90}

	8	
	80.8	
+ 28	8 4	
	81.2	
58+00	8 0	
	78.8	
1+50	10 4	
	78.8	
57+00	10 4	
	78.3	
150	10 2	
	78.0	
56+00	10 0	
	77.7	
+50	9 5	
	77.9	
55+00 Begin Bottom wash	9 3	
	84.3	
+80	4 9	
	83.9	
54 + 50	5 3	
	89 16	

	8	9
	86.7	
+40	4 2	
	90.9	
+18	0 0	
	89.2	
60+00	1 2	
TP 5 28 90 90		-3 54 85 62
	84.4	
59+70 44 10° 02' 15" L. Rt	4 8	
	85.1	
+40	4 1	
	82.4	
+36 End Bottom wash	0 8	
	82.2	
59+00	7 0	
	84.6	
+94	4 6	
	84.7	
+53	4 5	
	87.4	
58+40	1 8	
	89 16	

		90.5
+90		1.5
		89.2
+62	(Begin rock + rubble piles 3' high + rocky fill)	2.8
		86.5
+50		5.5
TP	5.17 92.03	4.04 86.86
		86.1
63+00		4.8
		86.4
+50		4.5
		85.6
62+00		5.3
		85.7
+50		5.2
		85.4
61+00		5.5
		85.4
60+65		5.5
	π 90	90

		90.3
+37		1.2
		89.0
+10		8.4
		88.7
66+00		8.7
		88.3
+50		9.1
TP	9.74 97.37	4.40 87.63
		88.8
+35		3.2
		88.1
+06		3.9
		89.9
65+00		2.1
		89.1
+50		2.9
		90.2
64+00		1.8
		92.03

		93.7	9 7
+50			
		94.8	8 6
70+00			
		95.1	8 3
+50			
TP	8 52 10 3 35	2 54	94 83
		94.7	2 7
69+00			
		93.9	3 5
+50			
		94.6	2 8
68+00			
		94.0	3 4
+50			
		93.0	4 4
67+00			
		91.5	5 2
66+50			
		97	37

		99.4	6 0
+50			
		103.4	2 0
+40			
		102.7	2 7
73+00			
TP 427	105 40		2 22 101 13
72+53 89 Lt	15°53'30"		101.13 2 22 on Hub New
+40 end rock and rubble fill			103.4 0 0
72+00			100.6 2 8
+68	11 7 10		98.1 5 3
+50	10 8 10 Tie record		98.0 5 4
71+00			96.8 6 6
			103 35

	102.3	
1+15	3	
	101.3	
77+00	4	
	100.6	
1+10	4 8	
	100.1	
76+00	5 3	
	99.7	
1 50	5 7	
	99.2	
75+00	6 2	
	98.9	
1+60	6 5	
	97.5	
1+50	7 9	
	97.3	
74+00	8 1	
	96.7	
73+80 E. channel	8 7	
	π 105 40	

TP	79 23	122 39	114.5	0 39 114 46
			0 4	
1+50				
			113.3	
80+00			1 6	
			112.4	
1+50			2 5	
			110.1	
79+00			4 8	
			108.1	
1+50			6 8	
			105.1	
78+00			9 8	
			104.4	
1+52			10 5	
			104.7	
1+62			10 2	
elv. 105 04		80°42'45"		
77+52 55	Lt		9 79	on Hub
			104.4	
77+20			10 5	
TP	13 28	π 114 85	3 83	101 57

elv 117.41

83+20.57 Lt 8°53' 4.93 on Hub

+15	5.2	117.2
83+00	4.2	116.2
+95 E wash creek	8.2	113.7
+92	6.2	115.7
+85	5.4	117.0
+50	5.2	117.2
82+00	5.2	116.7
+82	4.8	117.6
+50	5.0	117.4
81+00	6.6	115.8

122.39

TP	8.67	134.91
+50	0.8	126.1
87+00	1.9	125.0
+50	3.6	123.3
86+00	4.6	122.3
+50	5.9	121.0
85+00	6.5	120.4
+50	6.7	120.2
84+00	7.8	119.1
83+50	8.7	118.2

TP 9.43 × 126.89 4.93 117.46

92+00		134.7	
TP	13 06	146 49	148 133 43
1+50		131.5	
91+00		130.8	
1+75 Cross Creek			
1+50		130.2	
90+00		130.1	
1+50		130.0	
89+00		129.3	
1+50		128.5	
88+00		126.8	
			134 21

95+50 L.Rt 0° 16' 30" Changed Here			N 147.5
TP	12 38	158 23	0 14 146 35
95+00			145.9
1+50			142.3
94+00			140.2
1+50			138.6
1+35			137.8
1+25 crosses end creek			135.4
93+00			135.2
92+50			135.2
			146 49

	Lt	℄	
99+00		158.8 8.5	
	12.3 9°	158.3 9.0	
98+92 LT = approx :35	4' Creek Bank		
	Lt 21°33' Pt. changed Here		
98+90 .87			
TP	9.64 167.28	109 157.64	
+50	14.8 2.5	156.2 2.5	
	18 17 creek creek bank		
98+00		156.1 3.0	
+50		154.7 4.0	
97+00		153.2 5.5	
+50		151.5 7.2	
96+00		149.1 9.6	
	T 158.23		

		℄	
102+00		164.1 3.2	
+64		163.2 4.1	
+59 channel		161.0 6.3	
+50		162.3 5.0	
101+00		161.8 5.5	
+80		161.0 6.3	
+68 channel		159.4 7.9	
+50 channel		159.8 7.5	
100+00 Begin creek		159.5 7.8	
99+50		159.4 7.9	
	T 167.28		

+50		12 1	167.7	109+00		11 5	180.6
+33		14 9	166.4	TP	12 29	192 4	0 41 180 02
TP	13 35	180 43	0 20 167 08	+56		0 1	180.3
105+00		1 1	166.2	108+00		1 5	178.9
+50		2 0	165.3	+87		2 5	177.9
104+00		1 8	165.5	+68		4 9	175.5
+75 chained		2 1	165.2	+50		5 5	174.9
+50		2 0	165.3	107+00		8 2	172.2
103+00		2 5	164.8	+50		10 1	169.7
102+50		2 8	164.5	106+00		12 1	168.3
	T 167 28					180 43	

	2	189.2
+50	2 9	
		188.0
112+00	4 1	
		186.4
+50	5 3	
		186.1
111+00	6 0	
		185.4
+50	6 7	
		183.8
110+00	8 3	
		183.3
+60	8 8	
		181.4
+50	10 1	
		180.0
+35 channell	12 1	
		181.8
109+15	10 3	
	↑ 192 11	

	2	200.8
+50	3 8	
		200.4
+25	4 2	
		197.0
116+00	7 6	
		196.0
+50	8 6	
		195.4
115+00	9 2	
		194.2
+50	10 4	
		192.9
114+00	11 7	
TP . 13 10 204 56		0 65 191 46
		191.3
+50	0 8	
		190.4
113+00	1 5	
	↑ 192 11	

TP 12 27 222 53 ℄ 277 210 26

28° 21' 15" changed Herz 15

120+49 06 L.L. 277 on Hub

elv. 210 16

	208.6	
120+00	4 4	
	207.6	
+50	5 4	
	206.5	
119+00	6 5	
	204.6	
+50	8 4	
TP 9 41 213 03	0 94 203 62	
	203.3	
118+00	1 3	
	202.4	
+66	2 3	
	201.4	
+50 channel	3 2	
	202.0	
117+00	2 6	

℄ 204 56

℄

	218.2
+40	4 3
	217.6
124+00	4 9
	215.9
+50	6 6
	214.7
123+00	7 8
	214.3
+50	8 2
	213.9
+40	8 6
	212.2
122+00	10 3
	211.7
+75	10 8
	211.2
+50	11 3
	210.4
121+00	12 1

℄ 222 53

			E	233.2
+50			10	9
TP	12 39	244 12	0 53	231 73
				227.6
+42			4	2
				226.5
127+00			5	8
				225.1
+50			7	2
				222.7
126+00			9	6
TP	9 93	232 26	0 20	222 33
				221.5
+50			1	0
				220.2
125+00			2	3
				219.1
124+60			3	4
		T 222 53		

			E	240.6
131+00			3	5
				239.7
+50			4	4
				239.2
130+00 creek Bank			4	9
				236.2
+90 creek			7	9
				235.1
+67 creek			9	0
				238.3
+64 creek Bank			5	8
				237.9
+50			6	2
				236.2
129+00			7	9
				234.9
+50			9	2
				233.7
128+00			10	4
		T 244 12		

		246.2
+39 - creek		9.6
		246.2
+18 creek		9.0
		248.2
134+00		7.0
133+94.50 L.Lt 6°04'30"		7.13
		Hub
		246.7
+56		8.5
		244.5
133+00		10.7
		244.0
+50		11.2
TP	12.32 255.20 1.24	242.88
		243.0
132+00		11.4
		241.5
131+50		2.6
	↑ 244.12	

		20
TP	10.85 263.80	2.25 252.25
		253.8
137+00		1.4
		252.6
+50		2.6
		251.4
+25		3.8
		249.4
+15 ℄ creek		5.8
		252.5
+09		2.7
		252.1
136+00		3.1
		251.7
+50		3.5
135+00		
		248.8
+75		6.4
		247.2
134+50		8.0
	↑ 255.20	

TP	6^{35}	267^{81} 2^{34}	261^{46}
140+00			261.4 2^{4}
+50			260.1 3^{7}
139+00			258.5 3^{3}
+50			256.6 4^{2}
+15			256.0 7^{8}
138+00			254.4 9^{4}
+95 ℄ creek			252.6 11^{2}
+80			255.6 8^{2}
137+50			255.2 8^{6}
		263^{80}	

143+00			265.3 9^{5}
+73 creek edge			265.4 9^{7}
+46			266.1 9^{0}
142+00			265.4 9^{7}
141+50			263.8 11^{3}
TP	11^{69}	275^{06}	4^{44} 263^{37}
141+36.14 Lt	elv. 263.33	12°26'15"	4^{44} Aug
141+00			262.9 4^{9}
140+50			261.9 5^{9}
			267^{81}

+12	4	271.1
145+00	4	270.9
+92	4	270.5
+89 E creek	6	268.9
+82	4	270.8
+50	5	270.1
144+00	6	268.8
+50	8	267.1
+43	9	266.1
143+35 creek edge	10	264.9

T 275.06

+50	9	275.4
+16	10	274.2
+11	12	272.0
+09	10	273.8
146+00	10	274.4
TP	11.10	284.95 1.51 273.53
+70	1	273.6
+40	2	272.7
+25	4	270.6
145+16	5	269.8

275.06

	8	
722 E creek	10 3	279.7
149+00	8 3	281.7
782	7 0	283.0
750	7 3	282.7
TP 7 12	289 97	18° 282 85
elv. 282 64		
148+30 26 Lt	9° 55' 30" Rt	18°
	Aug	
148+00	3 9	280.8
770	7 0	277.7
756	7 5	277.2
147+00	8 5	276.2
	T 284 65	

	8	
0+50 26	4 6	285.4
0+25	6 4	283.6
MH 0+00 = 148+30 26	7 1	282.9
wherry extension		
149+98 65	7 5	282.5
750	8 5	281.5
149+40	8 6	281.4
	T 289 97	

Clark
Shephard
Bruner
Bryson

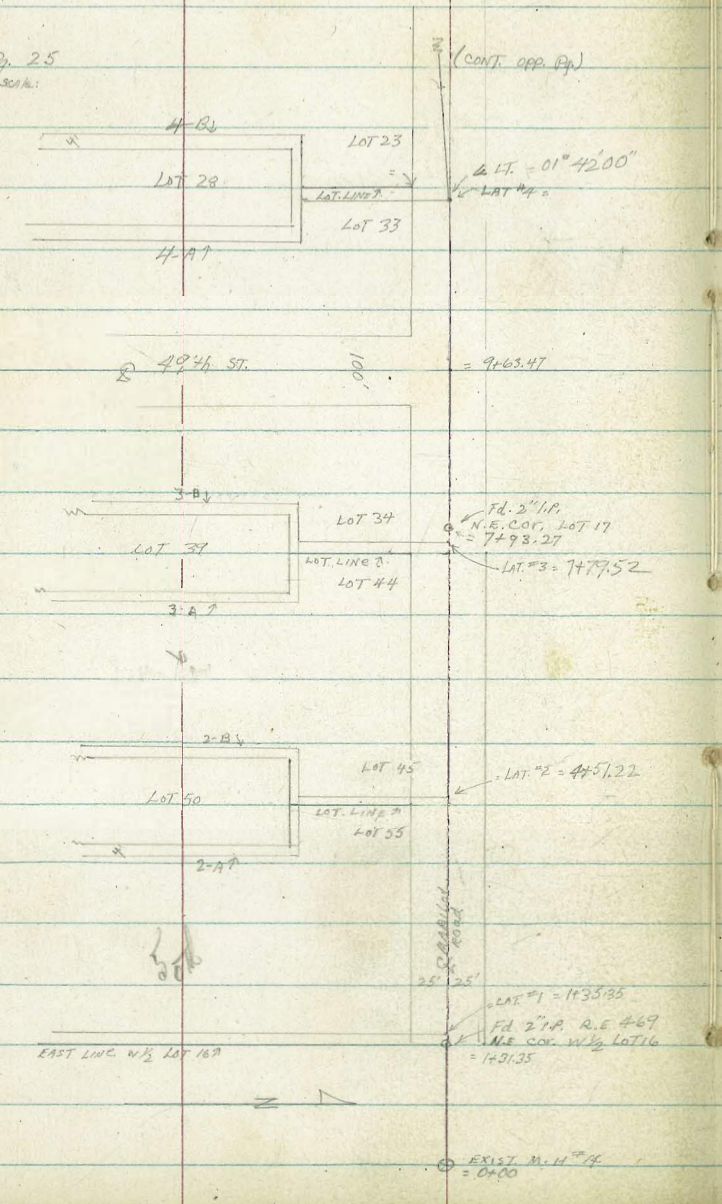
724-52
W.O. 32021

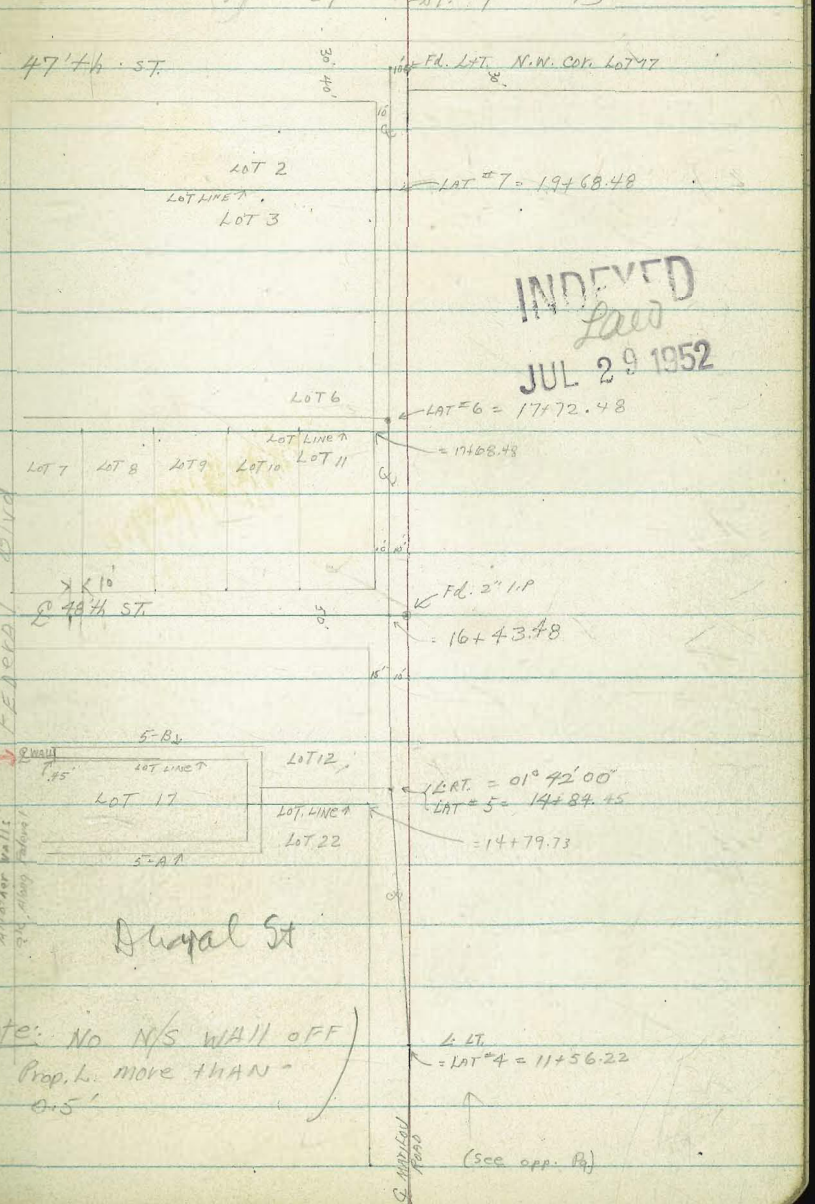
Lines & Profiles, Sewer, AS per
IMIG PARK NO. 2 (MARILOU Rd.)
Dwg's 1795-D & 1796-D etc.

Note: Profile: MARILOU Rd Page 25

LAT. #1	Page 32	LAT #5	Page 39
LAT. #2	" 34	LAT #6	" 41
LAT. #3	" 35	LAT. #7	" 43
LAT #4	" 37		

NOTES. Pg. 25
Sketch not to scale:





LINE + Profiles, SEWER, AS per DWG's 1795-D & 1796-D; IRVING PARK NO. 2 (MARILOU Rd etc.)

MARILOU RD.

24.10' LT Deadman
3.6' LT Deadman

1+34.5

(1+35.35) opp. LAT #1 (See Page 32)

1+31.35 = T.B.M on 2" I.P. 12.84 210.35

1+25

1+00

0+50

0+12 10' RT END C.B. INlet.

18' RT + 16' INLET & DRAIN.

0+00 = EXIST. M.H #14 (℄ MARILOU Rd)

Note: MARILOU Rd. Is Sectioned For 1500' due to Extremely Rough Terrain

	1.07	(223.19)	11.48	(222.10)
T.P.	3.94	(233.60)	0.29	(229.66)
B.M.	5.03.	(229.95)		(224.92)

N/E. B.P. Federal & 49th

LT.	℄	RT.
	211.1	
209.6	212.1	214.5 214.6 216.1 218.4
13.6 25	11.1	8.7 8.6 7.1 5.0 5 21 25 30
209.4	212.1	214.4 214.7 216.1 218.0
13.8 25	11.1	8.8 8.5 7.1 5.2 5 21 25 30
209.2	211.5	214.1 214.4 216.1 217.5
14.0 25	11.7	9.1 8.8 7.1 5.7 5 21 25 30
		211.40 212.25 11.79 10.94 C 16 TP. CP
210.8	212.8	204.90 211.37 212 214.7
12.4 25	10.4 Rim ℄	18.29 Flo. LINE ℄ 11.82 11.00 8.5 18 18' 25 C TP. CP
	(223.19)	

Note:

MARLOU Road

4+50

4+51.22 = OPP. LAT #2 (See Page 34)

4+47.32 LOT LINE 45/55 T&M: Spike Pole #273720 1.68 ⟨229.75⟩

4+00

3+50

3+00

T.P. 8.40 ⟨231.43⟩ 0.16 ⟨223.03⟩

2+50

2+00

1+54 24" LTG Pole #273703

1+42

⟨223.19⟩

LT. ℄ RT.

229.0 227.7 224.4 220.9
2.4 3.7 10.0 10.5
25 12 25

227.3 226.3 221.1 220.3
4.1 5.1 10.3 11.1
25 10 25

225.1 225.1 220.1 219.8
5.9 6.3 11.3 11.6
25 15 25

223.4 223.7 217.8 217.6 219.5
8.0 7.7 13.6 13.8 11.9
25 15 25 30
PL PL

⟨231.43⟩

224.2 224.3 217.4 216.4 216.2 219.1
+1.0 +1.1 6.0 6.8 7.0 4.1
25 12 5 25 30
PL

223.6 223.6 214.3 215.2 218.7
+0.4 +0.4 8.9 8.0 4.5
25 17 25 30
PL

222.9 221.0 221.5 214.7 216.3 218.3
0.3 11.2 8.7 8.5 6.9 4.9
25 5 22 25 30
PL

⟨223.19⟩

MARILOU Rd

8+00

7+79.52 = opp. Lt. #3 (see Pg. 35)

7+50

T.B.M. 3.25 ⟨236.92⟩ 2.53 ⟨233.67⟩ - chisel "L.P."

7+00

6+50

6+00

5+50

5+00

T.P. 6.45 ⟨236.20⟩ 1.68 ⟨229.75⟩

⟨231.43⟩

Lt.	℄	Rt.
234.3	234.2	234.4
2.6	2.7	2.5
25		25
233.6	233.7	233.4 / 234.4 / 228.2
3.3	3.2	3.5 / 2.5 / 8.7
25		5 / 6 / 25
	⟨236.92⟩	
233.7	232.9	233.3 / 224.9
2.5	3.3	2.9 / 11.3
25		7 / 25
232.9	233.2	232.2 / 224.9
3.3	3.0	4.0 / 11.9
25		7 / 25
231.4	232.6 / 231.5	224.3 / 223.6
4.8	3.6	4.7 / 11.9 / 12.6
25		7 / 21 / 25
231.2	230.7 / 223.5	222.4
5.0	5.5	12.7 / 13.8
25		16 / 25
230.1	229.0 / 222.1	222.0
6.1	7.2	14.1 / 14.2
25 PL		12 / 25 PL
	⟨236.20⟩	

MARILOU Rd.

			LT.	℄	RT.
T.B.M. (1452.22) ON LFT.	SPIKE IN Pole P273714	3.76		233.16	
1+48.22	℄ LT. opp. LOT #4 (See Page 36) 1° 42' 00"			LOT LINE -40' = EASEMENT LINE	
1+00			232.1 / 4.8 / 25	230.7 / 6.2	227.6 / 9.3 / 10 — 226.9 / 10.0 / 25
			232.5 / 4.4 / 25	231.[illegible] / 5.[illegible]	227.9 / 9.0 / 25
10+50			232.5 / 4.4 / 25	231.9 / 5.0 — 231.8 / 5.1 / 3	230.1 / 6.8 / 25
10+00			231.1 / 5.8 / 25	231.5 / 5.4	231.9 / 5.0 / 25
9+96.56	W. Edge PAV. 49th			231.52 / 5.40	
9+63.47	℄ 49th ST.		231.56 / 5.36 / 25	231.84 / 5.08	232.16 / 4.76 / 25
9+20.48	E. Edge PAV. 49th			230.92 / 5.95	
9+00			233.0 / 3.9 / 25	232.3 / 4.6	232.7 / 4.2 / 25
8+50			234.0 / 2.9 / 25	233.8 / 3.1	234.1 / 2.8 / 25
				236.92	

(236.9±)

				LT.				RT.	
15+00				232.4		231.9	230.4	226.1	
				4.0		4.5	6.0	8.3	
				15			5	10	
								P.L	
14+84.45	(1.RT opp LAT #5, (See page 39)			232.4		231.7	230.8	228.1	225.1
	(142' 00")			4.10		4.7	5.6	8.3	11.3
				15			5	10	18
				P.L				P.L. RT.	Toe
T.B.M (14+80 LT)	3.27	⟨236.43⟩	3.76	⟨233.16⟩	SPIKE IN Pole #P:273-711	⟨236.43⟩			
14+50				232.7		232.0	231.4	224.0	223.1
				4.2		4.9	5.5	12.9	13.8
				15 P.L Approx		5		17	P.L
14+00				232.3		231.8	228.2	224.7	223.5
				4.6		5.1	8.7	12.2	13.4
				16		6		8	34
				P.L					P.L Approx
13+50				232.1		231.7	228.4	225.1	224.5
				4.8		5.2	8.5	11.8	12.4
				18		6		12	32
				P.L Approx					P.L Approx
(+15.97)	(℄ Dual St)			231.3		231.4	228.5	225.7	225.0
13+00				5.6		5.5	8.4	11.2	11.9
				20		6		9	30
				P.L					P.L
12+50				232.1		231.0	227.9	225.7	225.4
				4.8		5.9	9.0	11.2	11.5
				22		8		7	28
				P.L					P.L
12+00				232.1		231.4	229.0	227.0	226.1
				4.8		5.5	7.9	9.9	10.8
				24 Approx		6		5	24
				P.L					P.L Approx
		⟨236.92⟩				⟨236.92⟩			

MARILOU. Rd + Alley

T.B.M. (17+68.48) ON LEFT. 2.82 (233.61) NAIL IN P/o # P273708

17+72.48 opp Lt 6 (See Page 41)

17+50

17+00

16+61.48 ± W.C.B. Line 48 Lt

16+43.48 ± E 48 Lt

16+25.48 E.C.B. Line 48 Lt

16+00

15+50

(236.43)

	Lt.	℄	Rt.
	231.0	232.6	232.2
	3.4	3.8	4.2
	10.		10
	232.2	231.8	231.3
	4.2	4.6	5.1
	10		10
	P.L		P.L
	230.29	230.3	230.2
	5.94	6.1	6.2
	10		10
	P.L		
TP. C.B. END			
	230.45	230.3	230.4
	5.98	6.1	6.0
	10		10
	Edge Pav		
	230.36	230.3	230.3
	6.07	6.1	6.1
	15		10
TP. END CB			P.L
	231.8	230.9	230.4
	4.6	5.5	6.0
	15		10
	P.L		P.L
	232.5	231.0	229.0
	3.9	5.4	7.4
	15		10
	P.L		P.L

(236.43)

MARILOU Rd. + ALLEY

Check: 9.50 ⟨228.05⟩ = 228.05 = LT & Federal #4744

T.P. 3.94 ⟨237.55⟩ 2.82 ⟨233.61⟩

20+00

19+68.48 opp. LAT. #7 (see page 43)

19+50

19+00

18+50

18+00

⟨236.43⟩

LT. & RT.

232.3	232.4	237.5
4.1	4.0	2.9
10	10	10
232.4	232.4	233.4
4.0	4.2	3.0
10	10	10
232.4	232.3	234.0
4.0	4.1	2.4
10	10	10
232.9	232.5	233.0
3.5	3.9	3.4
10	10	10
232.8	232.5	233.2
3.6	3.9	3.2
10	10	10
232.8	232.3	232.2
3.6	4.1	4.2
10 P.L.	10	10 P.L.

⟨236.43⟩

LAT. #1

See sketch Pg 24.

1+75

1+50

1+25

1+00

0+75

0+50

0+25 - S.L. MARILOU Rd.

0+03

0+00 = STA. 1+35.35 on ℄ MARILOU Rd

Def. L to LT. OFF MARILOU = 89°57'18"

T.B.M. 12.67 ⟨223.02⟩ ⟨210.35⟩ Elev. 2' I.P. (see Pg 25)

℄

218.0
5.0

218.0
5.0

215.3
2.7

11.4
11.6
10
Toe

216.6
6.4

221.6
1.4
10
TP

216.3
6.7

216.3
6.7

210.0
13.0
10
Toe

216.3
6.7

223.1
10.1
10
TP BENCH

210.3
12.7

11.7
11.3

⟨223.02⟩

Check: 12.64 (210.38) 210.35

2+50

2+25

2+00

(223.07)

216.4
6.9
6 Toe

218.1
4.9

220.1
2.9
5 Top

217.8
5.2

215.8
7.2
8 Toe

218.5
4.5

220.9
2.1
6 Top

(223.02)

check 5.30 229.75 = 229.75 Spike IN Pole

LAT. # 2 +2-A +2-B

See sketch Pg 24

Note: { ℄ 8" WALL Bet. LOTS 45-55 = LOT LINE = thus added for purposes of STATIONING 4' WAS to ℄ sta. OF MARILOU Rd opp LOT. LINE to obtain STA. OF LAT. # 2 = EASEMENT LINE

2+28.5 = FC. WALL LOTS 48/49 etc.

2+00

1+77 = FC WALL LOTS 47/48 53/52

1+50

1+22 = 4' BK. WALL between LOTS 46/47 54/53 = 90° ∠ IN LAT # 2. See sketch 2A = LINE to WEST, 2B = LINE to EAST.

1+00

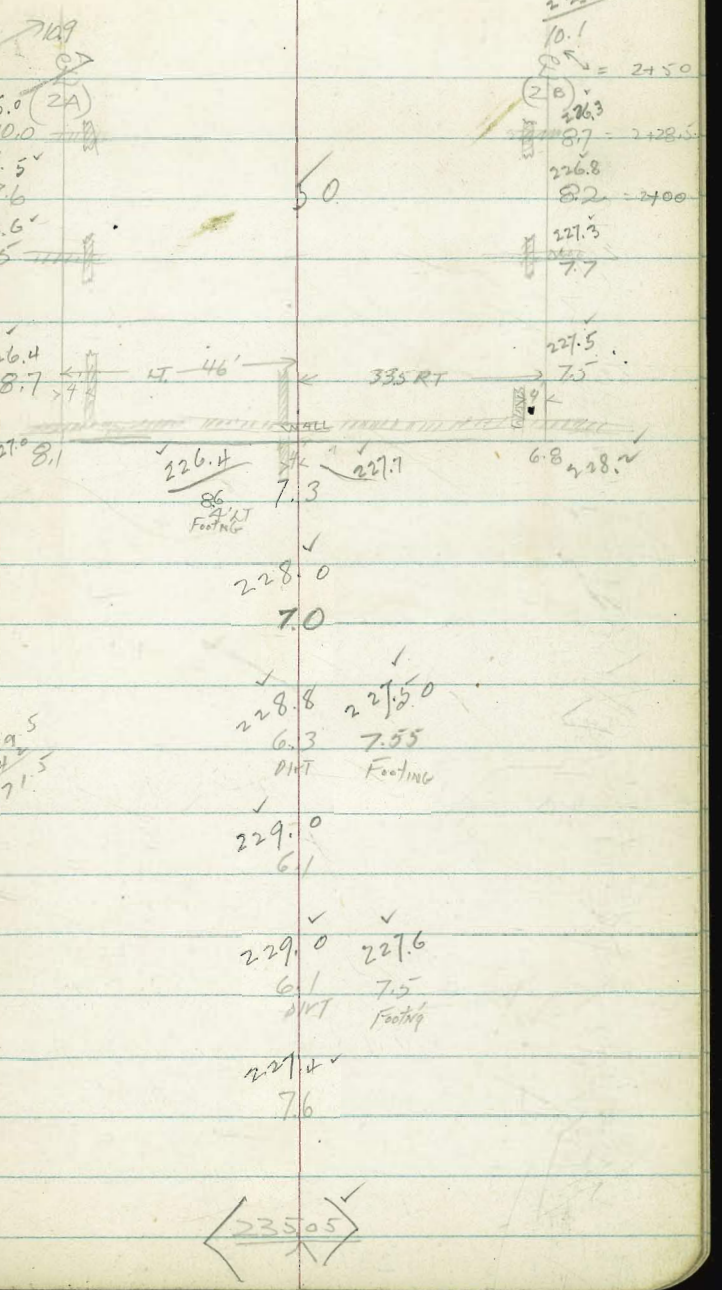
0+749 = FC 8" WALL bet. LOT 45/46

0+50

0+24.6 = FC 8" WALL ALONG S.P.L. MARILOU Rd
0+23.5 = 4' LT ℄ Pole
WALLS av. 4.5' high

0+00 = 4+51.22 ℄ MARILOU Rd (Pg 26)
DEF ∠ to LT OFF " "
= 89° 55' 17"

5.30 ⟨235.05⟩ ⟨229.75⟩ = SPIKE IN Pole (Pg 26)



LAT #3

Sketch Pg 24

Note: ℄ 8" x 4.5 WALL bet. LOTS 34/44 = 0.40' ⇐ OF
Prop. Line: THUS STA. OF LAT #3 = LOT
LINE + 4.8' = 7+79.52 ℄ MARILOU

1+77 = FC. WALL bet. LOTS $\frac{36}{37}$ & $\frac{42}{41}$

1+50

1+22 = 4' BK WALL bet. LOTS $\frac{35}{36}$ $\frac{43}{42}$ = 90 ∠ IN LAT 3
3A to EAST
3B to WEST

1+00

0+75 = FC 8" WALL bet. LOTS $\frac{34}{35}$ $\frac{44}{43}$

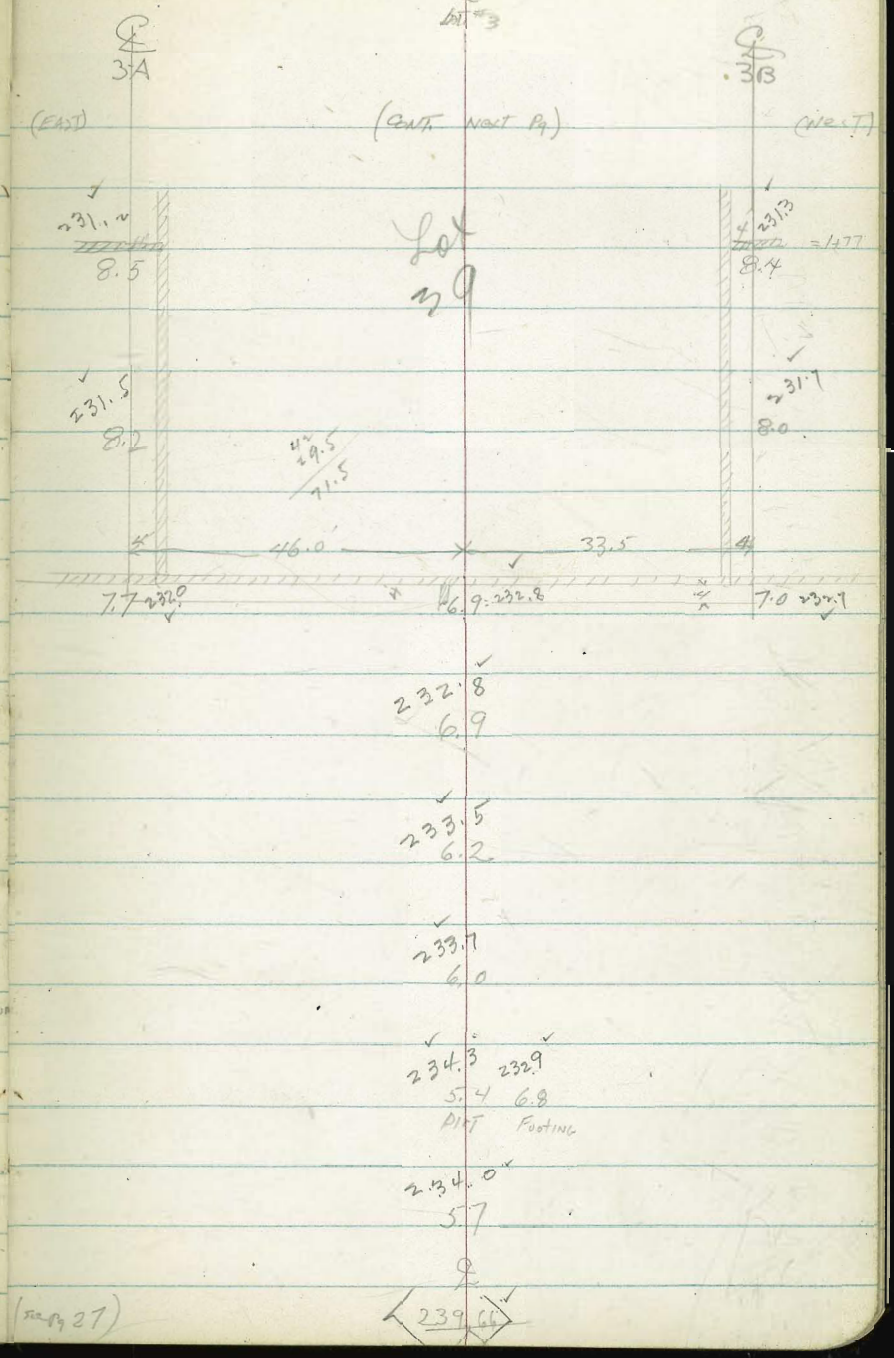
0+50

Note: VARIOUS SMALL SHRUBS TOO NUMEROUS TO MENTION WE WITHIN THE 4' EASEMENT.

0+25 = FC. 8" WALL ≤ LINE MARILOU
0+24 = 4' LT ℄ POLE
WALLS AV. 4.0' high

0+00 = STA. 7+79.52 ON ℄ MARILOU Rd
= DEF ∠ TO LT = 89° 55' 17" OFF ℄ MARILOU

T.B.M. 5.99 (239.66) (233.67 over 2" I.P. (see Pg 27)



check: 5.99 / 233.67 / 233.67 = ELEV. 2" I.P

2+50

2+28.50 - FC wall betw lots 37/38 + 41/40

2+00

<239.66>

℄ 3-A

℄ 3-B

EAST

WEST

4'

228.5
11.2

229.8
9.7

4'

229.0
10.7

4'
9.6 = 230.1

= 2+28.5

46.

33.5'

230.2
9.5

230.5
9.2

<239.66>

LAT. #4 etc.

Note: ℄ Wall bet. LOTS 23/33 = Prop. L

1+77 = Fc. Wall bet. LOTS 25/26 + 31/30

1+50

1+27 (on 4-B) 3' Lt ℄ = ℄ Pole # 5146514

1+22 = 4' Bk Wall bet. LOTS 24/25 + 32/31 = 90° Lpt in LINE OF LAT #4
4A to EAST
4B to West

1+00

Note: Various Flowers + Shrubs Fall within 4' EASEMENT.

0+75 = Fc. Wall bet. LOTS

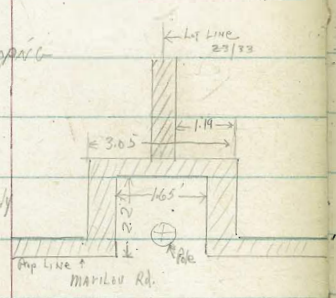
0+69 3.1 Lt to Fc. End 6" Conc. Cap

0+50.

0+27 3.1 Lt to Beg 6" Conc. Cap on ℄

0+25 = Fc. Wall on S.L. MARILOU

0+25 4' Rt ℄ Pole set in Alcove of Walls this sta

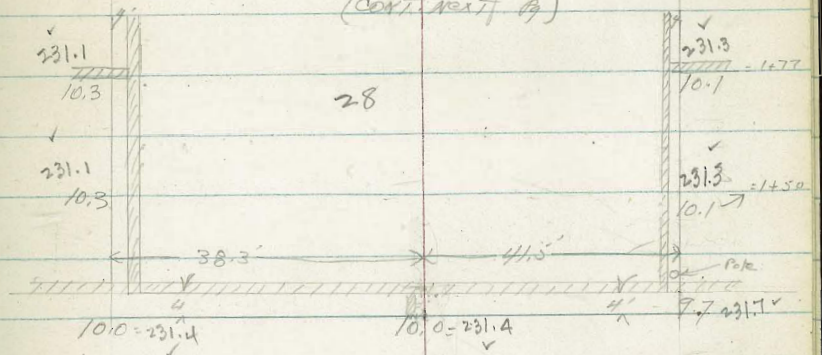


0+00 STA. 1+48.22 ℄ MARILOU Rd.
DEF ∠ to LT. = 89° 53' 16" OFF ℄ MARILOU

8.27 ⟨241.43⟩ ⟨233.16⟩ = elev Spike in Pole (see Pg 28)

℄ (EAST) 4-A

(CONT. NEXT Pg)



℄ 4-B (West)

28

231.7
9.7

232.2
9.2

Mag Lot to Lot Line
176.44
- 3
149.44
to Lot Line

232.2 232.21
9.2 9.22
3.1 3.1
DIRT TP.

8.8 8.84
DIRT. 3.1
TP. Cadena

232.2 230.8
9.2 10.6
DIRT Footing

231.0
10.4

⟨241.43⟩

Check: 8.26 ⟨233.17⟩ = 233.16 = Elev. SPIKE IN Pole

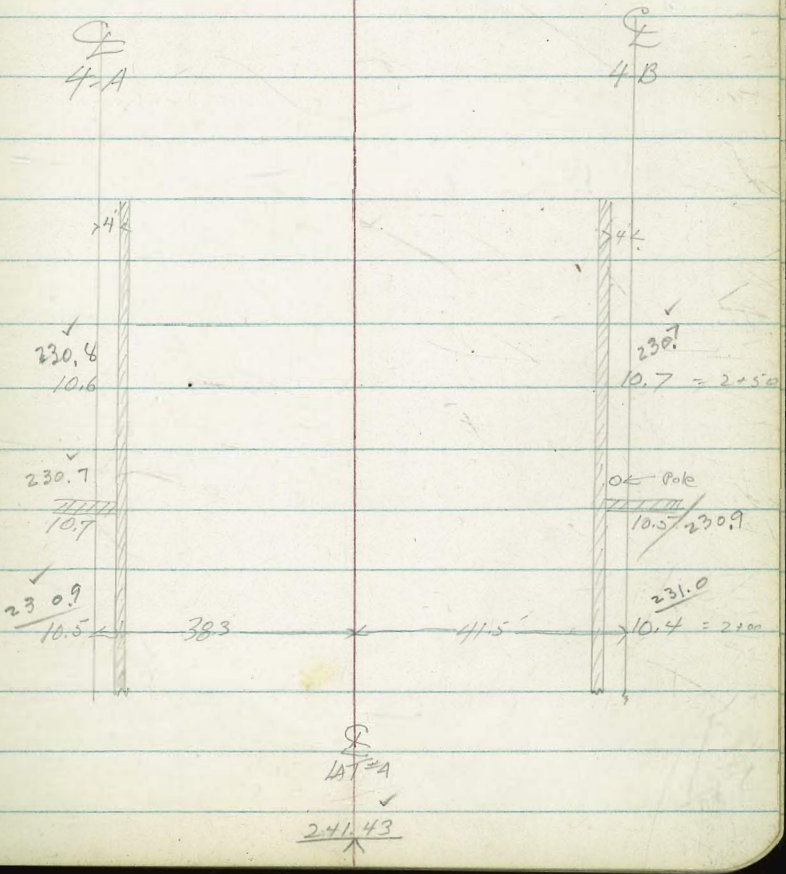
2+50

2+29 (ON 4-B) 3' LT ℄ to ℄ Pole # 5146488

2+28 = Fc. Wall bet. LOTS $\frac{26}{27} \times \frac{30}{29}$

2+00

⟨241.43⟩



LAT. #5

Note: ℄ 8"x4.0 WALL = Prop. Line bet. LOTS 12 & 22
Sketch Pg 24.

1+40

1+12 = Fc. 8" WALL bet. LOTS 13/14 & 21/20 = 90°∠ in LAT. #5
AV. Height WALLS = 4.0
5-A to EAST
5-B to WEST

0+90

0+65.6 = Fc Picket Fence LOTS 12/13 & 22/21

0+40

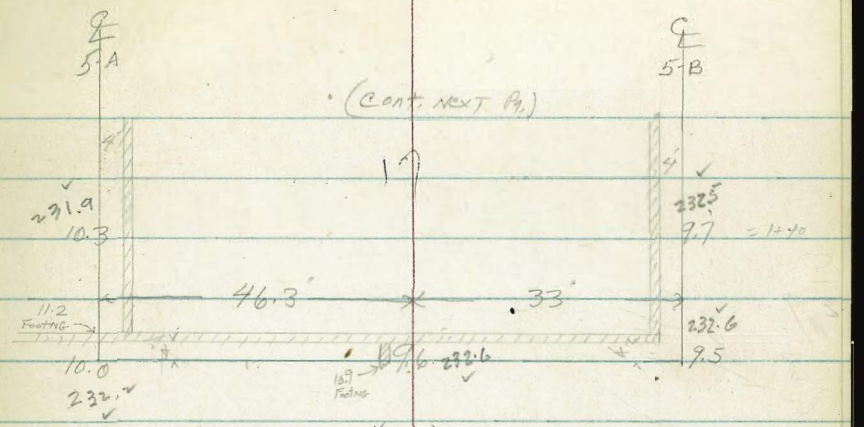
0+15 S.L. Alley Fc 4' Board Fence S.L. Alley

0+13.5 ⅋ LT = ℄ Pole

0+00 = 14"84.45 ℄ MARILOU

Note: Shrubs & Flowers Fall within 4' EASEMENT.

8.99 ⟨242.15⟩ ✓ ⟨233.16⟩ ✓ = Spike IN Pole (Pg 29)



232.4
9.7

232.7
9.7

232.5
9.6

232.3
9.8

231.7
10.4

℄ LAT #5

242.15

Check: 8.98 ⟨233.17⟩ = 233.16 = elev SPIKE IN Pole

2+30

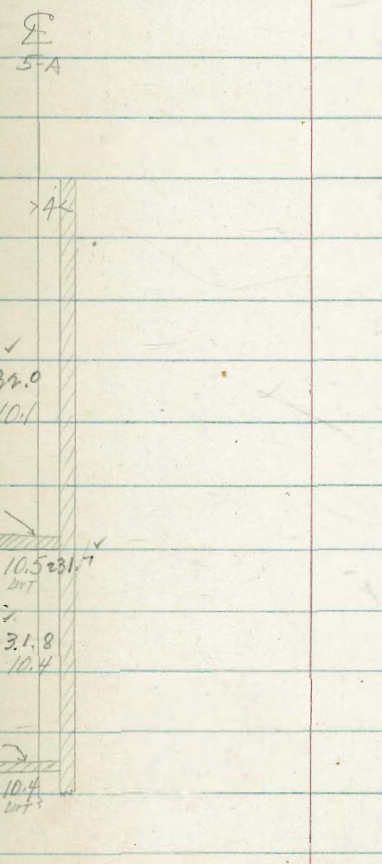
2+19 = Fc. 8" WALL (ON 5-B) bet. Lots 15+16

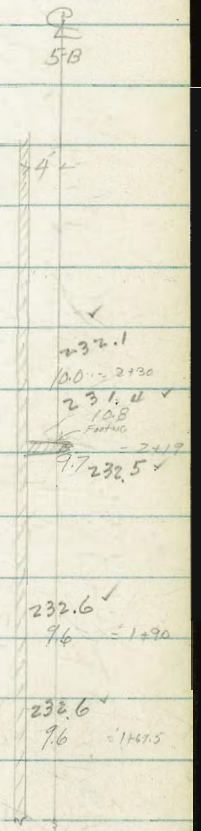
2+11.5 = Fc. 8" WALL (ON 5-A) Not on LOT LINE

1+90

1+67.5 = Fc 8" WALL (5-A ONLY) bet. LOTS 20/19

⟨242.15⟩





⟨242.15⟩

LAT #6

Note: West Face of N&S WALL bet LOTS 6 & 11 IS 0.10 EAST OF LOT LINE

	LT.	℄	RT.
1+75			
1+65	3.5 LT ℄ Pole # P273709		
1+50			
1+25			
1+00			
0+75			
0+50			
0+25			
0+10	4' LT Fc. WALL		
0+09	4.5 LT ℄ Pole P273708		
0+00 = STA. 17+72.48 ℄ Alley DEF to LEFT = 89°53'16"			

(Cont. Next Pg.)

233.4
5.1

233.4
5.1

233.4
5.1

233.5
5.0

233.7
4.8

232.5 (6.0 ℄ Footing) 233.5 (5.0 ℄ Bott) 233.5
5.0

233.0
5.5

232.8
5.7

232.6
5.9

4.85 (238.46) 233.61 = Spike

238.46

N Pole (See Pg 30)

Check: 4.85 ⟨233.61⟩ = NAIL

In Pole

2450

2425

2400

⟨238.46⟩

233.0
5.5

232.4 (6.3, 4 FOOTING)
233.3 (5.2, 4 DIRT)
233.2
5.3

233.3
5.2

⟨238.46⟩

LOT #7

= LOT LINE BETWEEN 2/3

check: 4.85 = ⟨233.61⟩ = NAIL Pole

1+25			231.9 ✓ 6.6
1+00			232.2 ✓ 6.3
0+75			232.3 ✓ 6.2
0+50			232.4 ✓ 6.1
0+25			232.5 ✓ 6.0
0+10 S.L. Alley			232.5 ✓ 6.0
0+00 = ℄ Alley STA	19+68.48 (See Pg. 31) Def. Lt. 89°53'16" OFF ℄ Alley		232.2 ✓ 6.3
4.85	⟨238.46⟩ ✓	233.61 ✓ = NAIL Pole	(See Pg 30) ⟨238.46⟩ ✓

Clark
Shephard
Bruner
Bryson
8-19-52
WO. 32021

Loc. Sewer IMig Pk #2
N of N. Line Federal Blvd

Notes: Page 45

Ref: Dwg. #1795-D
#1796-D

Not to scale:

(See opp. pg.)

E. Line N½ Lot 16

EXIST. M.H. 19+69.94

67° 51'

℄ 24" corrug. Steel Pipe

19+16.10

11.45'

Def. ∠ Rt. = 3° 44' 45"

H. Wall = 7.5' Long.

Set stub & Tack 18+36.98

Fd. L.Y.C.T. ℄ 36' Con. Pav. Strip Fed. Blvd.

50'

2'

N. Line Federal

Fd. Nail in Conc.

3'

E. L.

Duval St.

50'

W. Line

Set Nail 6+52.40

Fd. Nail in Conc.

50th St.

50'

Set Nail 16+84.66

Fd. Nail in Conc.

E. L.

48th St.

50'

W. Line

Set Nail 3+25

Fd. Nail in Conc. Walk

N. Line Federal

Set Stub & Tack 0+00

Fd. I.P.

℄ E'ly Line Lot 2

E. Line

Mary Lou

50'

W. Line

Set Nail 13+57.23

Fd. Nail in Conc.

N. Line Federal

2'

Fd. Nail in Conc.

E. Line

49th St.

100'

W. Line

Set Nail 3' Bk. P.L. 10+04.79

50'

2'

3'

Fd. Nail in Conc. Walk

3'

(See Preced. Page)

Loc. SEWER. IMIG PK. #2
N. of N Line Fed Blvd.

		LT.	℄	RT.
2+10	Beg. LAWN		232.1 ✓	
2+00			3.7	
1+98.30	7.4' RT. Beg 5'60 Conc. WALK & CB.		232.3 ✓	230.69 ✓
1+50			4.1	5.75 7.4 BK WALK
1+00			231.8 ✓ 4.6	
0+50			231.3 ✓ 5.1	
0+04			230.4 ✓ 5.7	
0+00	=E. Line Lot 2 End Asphalt		230.1 ✓ 6.3	
0-01.5	2' RT. 5" Steel Sign Pole			
0-37	, Asphalt 53. LT. ℄ 42'+24 Service St. Bldg.	230.30 ✓ 6.14 53 Conc. Floor	229.79 ✓ 6.65	
B.M.	8.39 (236.44 ✓)	(228.05) ℄ Lt. Fed. & 47'th		(236.44 ✓)

		LT.	℄	RT.
			230.9	231.49
			5.95	5.38
			Gutt.	TP CB
3+43	TP CB at Return (E. CB)			
		232.40	232.10	231.25
		4.47	4.77	5.62
3+25	℄ 48.4h	100	50	
		(AC. PAV.)		
			231.75	231.25
			5.12	5.62
3+04.83	TP. CB. Ret (W. CB.)		TP CB	Gutt
	(3' LT to ℄ Stop Sign Post.			
	BK Edge WALK at Return		231.84	
2+98.2	ENS LAWN		5.03	
			232.1	
2+50			4.2	
			232.60	
2+41.9	ENS WALK.		4.27	
		232.86	232.59	232.46 231.98
	(2.9' RT. to Step.) 5' LT. to Steps to house	4.01	4.28	4.41 4.89
2+39	Edge 2.9' WALK	5	Conc.	2.9 2.9
				TP. Gutt. Step
2+20	4.5' RT & 8" Palm			
T.P. 5.40	⟨236.87⟩ 4.97 ⟨231.47⟩			⟨236.87⟩

4+04.5 — 4.5' LT & 1" Rosebush
2.5' RT & 1" Rosebush

T.P. 4.48 ⟨235.69⟩ ✓ 5.66 ⟨231.21⟩ ✓

4+03.2 — Edge WALK

4+00.30 — Edge WALK

3+98 — 4.5' LT & 1" Rosebush
2.5' RT & 1" Rosebush

3+82 — 3' LT & 1" Magnolia

3+76 — 3.5' RT & 2" Palm

3+59 — 3' LT & 1.5" Pine tree

3+51.7 = { 2' hedge along BK WALK
BK. WALK at Ret WALL
Beg. LAWN

⟨236.87⟩ ✓

⟨235.69⟩ ✓

231.63 ✓
5.24

231.57 ✓
5.30
Edge
WALK

231.64 ✓
5.23

⟨236.87⟩ ✓

		LT.	℄	RT.
5+48	4.5 RT ℄ 1' Palm			
5+24	℄ 4' high hedge			
5+21	4.5' RT ℄ 1' Palm			
5+00			231.4 ✓	
4+89	4.5 RT. ℄ 1' Palm		43	
4+79	℄ Geranium Bed			
4+78	E. Edge Drive		231.57 ✓	
4+60	W. Edge Cone Drive		412	
4+58	℄ Geranium Bed		231.60 ✓	
4+56	℄ 4' High hedge		409	
4+54	5' RT. 12" Palm			
4+50			231.4 ✓	
4+30	5' Rt. ℄ 12" Palm		43	
4+22	4' Lt ℄ 1" Magnolia			
	〈235.69〉 ✓		〈235.69〉 ✓	

		LT.	℄	RT.
			230.1 ✓	
7+00			5.0	
6+79.11	BK. WALK Beg. LAWN		229.88 ✓ 5.21 CONC.	229.9 ✓ 5.2 LAWN
6+72.46	CB at Ret. (E. Ret.)		229.35 ✓ 5.74 OUTT.	229.79 ✓ 5.30 TP. CB.
6+52.40	℄ DUVAL	230.11 4.98 100	229.9 ✓ 5.17 50 (A.C. PAV.)	229.84 ✓ 5.65
T.P. 5.02	⟨235.09⟩ ✓	5.62	⟨230.07⟩ ✓	⟨235.09⟩ ✓ 229.99 ✓ 5.10 TREE
6+32.21	CB.			229.53 ✓ 6.16 OUTT.
6+25.43	BK edge WALK At Return (W. Ret.) END LAWN		230.09 ✓ 5.60	
6+01	4' RTE 1' PALM			
6+00			230.9 ✓ 4.8	
5+76.3	E. Edge Walk		230.81 ✓ 4.38	
5+73.3	W. Edge WALK		230.85 ✓ 4.34	
5+50			231.1 ✓ 4.1	
	⟨235.69⟩ ✓		⟨235.69⟩ ✓	

8+50	4.5' RT ℄ 8" Palm			
8+20				
8+16	4.5' RT. ℄ 10" Palm			
8+04	3' LT 1" Rosebush 1' RT 1" Rosebush			
T.P.	3.52 ⟨232.10⟩	6.51	⟨228.58⟩	
8+02	E. edge Drive			
8+00				
7+87	W. edge Drive (conc)			
7+63	℄ 2' Hedge			
7+62	4.4' RT. ℄ 10" Palm			
7+57	4' RT ℄ 1' Palm			
7+50				
7+38.7	E. edge WALK			
7+35.7	W. edge WALK			
7+03	4.2' RT ℄ 1' Palm			
	⟨235.09⟩			

LT.	℄	RT.
	229.4	
	2.7	
230.1	229.6	228.40
2.0	2.5	3.70
4		7.40
Brow slope		BK WALK Toe slope
	⟨232.10⟩	
	229.64	
	5.45	
	229.65	
	5.44	
	229.77	
	5.32	∴ Lawn Flush with Drive
	230.2	
	4.9	
	230.14	
	4.95	Flush with Lawn
	230.16	
	4.93	
	⟨235.09⟩	

		LT.	℄	RT.
10+04.79	℄ 49'th	228.6 3.48 100	227.36 4.74 50 (A.C PAV)	225.17 6.38 3' BK Prop.
9+62.73	CB at W. Ret.	226.56	5.54 TOCB	6.08 CUTT
9+56.02	BK. WALK at W. Ret. END LAWN		226.61 5.49	
9+50			227.22 4.9	
9+47.	END Slope LAWN	229.8 2.3 4	227.8 4.3	226.7 5.4 6 BK WALK Toe Slope
9+32.5	4.3 RT. ℄ 1' Palm	229.8 2.3 4 Brow	229.0 3.1	227.30 4.80 7.4 BK WALK toe Slope
9+00				
8+99.	2.5' RT 2" Fir			
8+97.8	E. Edge Steps:	229.75 2.35 1.4	228.72 3.38	227.74 4.36 1.4
8+93.8	Lawn Flush with Steps W. Edge Steps (4) Line passes thru middle 2nd Step)	229.75 2.35 1.4 LT= WALK AT TP. 4th step	228.73 3.37	227.71 4.39 1.4 RT= WALK At bottom of 1st step
8+92	2' RT ℄ 2" Fir			
8+75	4.5' RT. ℄ 8" Palm			
8+53 ℄ 2' Hedge				
	232.10		232.10	

					LT.	℄	RT.
11+59		3.0 RT. ℄ 10" Palm			227.7	225.7	224.3
11+50					2.6	4.6	6.0
					7		3.5
					Brow		toe
11+34		3.5 RT 10" Palm				225.3	
11+10						5.0	
T.P.	5.85	(230.26)	7.69	(224.41)		(230.26)	
		Check	7.20	224.90 = 224.92 =	N/E B.P Fed. 449th		
11+06.10		E, edge steps			229.05	225.1	224.65
					3.05	7.00	7.45
					10		W/ALK
		(Depth 1' - Rise .04' each step)					
11+02.10		W edge 10 steps (Line passes on top edge Bottom Step.)			229.05	225.1	224.68
					3.05	7.00	7.42
					10		Walk Bot
					TP 10th Step		1st Step
11+00					228.3	225.4	224.8
					3.8	6.7	7.3
					7		2.5
					Brow		Toe
10+81		3' RT ℄ 10" Palm					
10+63		Beg. Slope LAWN			228.5	225.6	225.3
		Beg. LAWN			3.6	6.5	6.8
					Brow	225.41	2.5 Toe Slope
10+54.62		BK. WALK E. Ret.				6.69	225.4
							6.7
						224.86 Conc.	225.46 LAWN
10+47.57		CB. E Ret.				7.24	6.64
						C.O.T.T.	T.A.C.B.
		(232.10)				(232.10)	

		LT.	℄	RT.
13+00		227.0 ✓	224.8 ✓	221.9 ✓
		3.3	5.5	8.4
		5 Brow		6.4 Toe + BK WALK
12+80			224.2 ✓	
			6.1	
12+77.8	E. Edge Steps + WALL			
	(Line Passes 0.30' BK. Top 1st Step)			
12+73.4	W. edge 13 Conc. Steps & 3' Brick Ret. WALLS (Depth 1.2' - Rise 0.50' each step)	228.7 ✓	225.45 ✓ 222.87 ✓	222.37 ✓
		1.55	4.81 7.39	7.89
		13.8 Top 13th Step	TRwall TP. 1st Step	0.30 WALK + Bottom 1st Step
12+70			224.6 ✓	
			5.7	
12+52	3.0 RT. ℄ 8" Palm			
12+50			225.2 ✓	
			5.1	
12+27	3.0' RT. ℄ 1' Palm			
12+00		225.7 ✓	225.0 ✓	223.22 ✓
		4.6	5.3	7.04
		3 Brow		6.4 BK WALK Toe Slope
11+93	3.5' RT ℄ 1' Palm			
			224.48 ✓	
11+76.4	E. Edge Drive		5.78	5.8 LAWN
			224.40 ✓	
11+65.7	Brk		5.86	
			224.69 ✓	
11+62.7	W. edge Conc Drive		5.57	
11+60	℄ 3' Hedge			
	⟨230.26⟩ ✓			⟨230.26⟩ ✓

				LT.			℄			RT.	
	(Line passes 0.76 LT. of TP edge 1ST Step)										
14+35.30	Conc. Wedge 11 steps & Brick Ret. Walls. Depth 4.2' - Rise 0.45'	2x5'		225.68 1.82 11.6 TP. 17th step			222.51 4.99 TP. WALL		220.82 6.68 TP. 1ST step	220.39 ZW 0.7 WALK	
14+33							222.1 5.4 LAWN				
14+05	3.0' RT. ℄ 10" Palm										
14+00							223.0 4.5				
13+94				226.0 1.5 8 Brow. Slope			222. 5.1 LAWN		220.76 6.74 BK WALK Toe slope		
13+85.05	BK WALK. E Ret Beg. LAWN						221.20 6.30 Conc.		221.3 6.2 LAWN		
13+77.92	CB at E. Ret.						220.89 6.61 GUTT		221.00 6.08 TP. CB		
13+57.23	℄ MARY-LOU			227.25 0.25 100	224.54 2.96 50 (A.C. PAV.)		221.33 6.17	(2' BK Prop)			
13+36.40	CB. At. W. Ret.						221.88 5.62 TP CB		221.39 6.11 GUTT.		
13+29.75	BK edge WALK W. Ret. end LAWN.						221.81 5.69 Conc.				
13+23				226.5 1.0 5 Brow			223.5 4.0		221.66 5.84 BK WALK Toe Slope		
13+05	3.5' RT ℄ 10" Palm										
T.P.	5.89	⟨227.50⟩	8.65	⟨221.61⟩			⟨227.50⟩				

		LT.	℄	RT.
	(LINE Passes 0.10' BK (LT.) TP. edge 1ST STEP)			
16+08.63	W. edge 8 Steps + 2.5' Brick Ret. WALLS Depth 1.2 - Rise 0.5 each step	222.30 ✓ 5.20 8.20 TP. 8th Step	220.66 ✓ 6.84 Top WALL 219.82 ✓ 7.7 LAWN	218.9 ✓ 8.58 TP. 1ST Step
16+07				218.34 ✓ 9.16 0.10 WALK
16+00		222.3 ✓ 5.2 4 Brow	220.3 ✓ 7.2	217.80 ✓ 9.70 6.4 Toe
15+59	℄ 5' Hedge			
15+50		221.8 ✓ 5.7 4 Brow	220.2 ✓ 7.3	218.5 ✓ 9.00 6.4 Toe
15+25		221.0 ✓ 6.5 4 Brow	220.3 ✓ 7.2	218.74 ✓ 8.76 6.4 Toe BK WALK
15+04.7	E. Edge Drive		219.82 ✓ 7.68 Conc.	
15+00			219.9 ✓ 7.60 Conc.	
14+90.85	W. Edge Conc. Drive		220.0 ✓ 7.50 Conc	Flush - LAWN
14+89	℄ 4.5' Hedge			
14+80		224.0 ✓ 3.5 5 Brow	222.4 ✓ 5.1	219.41 ✓ 8.09 6.4 Toe BK WALK
14+50			223.0 ✓ 4.5	
14+42			222.0 ✓ 5.5 LAWN	
14+39.70	E. Edge Steps + WALL			
	⟨227.50⟩ ✓		⟨227.50⟩ ✓	

17+50	END LAWN - Beg. Ice-plant				
17+20	Beg. Slope ~~Lawn~~ Ice-Plant Rt.				
17+12.21	BK WALK. E. Ret. Beg. LAWN (DIAC.)				
17+05.40	= CB. At. E. Ret				
16+84.66	= ℄ 50th St				
16+63.99	CB at W. Ret.				
16+56.95	BK. WALK at W. Ret. END LAWN				
16+50	END Slope LAWN				
T.P.	4.88	⟨222.40⟩	9.98	⟨217.52⟩	
16+14					
16+13.08	E. Edge Steps & WALL				
		⟨227.50⟩			

Lt.	℄	Rt.
	218.5	
	3.9	
220.7	218.3	216.25
1.7	4.1	6.15
5		6.4
Brow		Toe Cove
	216.66	216.7
	5.74	5.7
		LAWN
	216.12	216.72
	6.28	5.68
	GUTT.	TP. CB.
220.50	218.90	216.68
1.90	3.50	5.72
10.0	.50	
	(A.C. PAV)	
	217.22	216.66
	5.18	5.74
	TP CB	GUTT.
	217.33	
	5.17	
	CONC	
221.9	218.9	217.18
0.50	3.5	5.22
5		4.2
Brow		TOE
		BK. WALK.
	⟨222.40⟩	
	219.8	
	7.7	
	LAWN	
	⟨227.50⟩	

		LT.	℄	RT.
18+71.5	BRK.	214.6 ✓ 7.8 5	214.9 ✓ 7.5	214.4 ✓ 8.0 5
18+44.5	BRK.	215.9 ✓ 6.5 5	215.5 ✓ 6.9	215.2 ✓ 7.2 5
18+36.98	2" DK. N. Line Fed. & E. Line W½ Lot 16 ∠ RT. Def. = 03° 44' 45" to ℄ M.H.	219.4 ✓ 3.0 4 Brow	217.7 ✓ 4.7	214.86 ✓ 7.54 6.4 BK WALK ✓Toe
18+00		220.0 ✓ 2.4 4 Brow	218.4 ✓ 4.0	215.60 ✓ 7.20 6.4 BK WALK Toe
17+70			217.9 ✓ 4.5	
17+67			217.1 ✓ 5.3	
17+65.5	E. edge Steps & Wall			
17+61	(Line Passes 0.5' (LT) BK. Top Edge 1st. step) W. Edge 10 Steps & 2.5' Brick Ret. Walls Depth 1.1 – Rise 0.45'	220.5 ✓ 1.90 10:10 TP. 10th Step	218.17 ✓ 4.23 TP. Wall 219.2 ✓ 5.2	216.20 ✓ 6.20 TP. 1ST Step 215.78 ✓ 6.62 0.5 WALK
17+60.				
	⟨222.40⟩ ✓		⟨222.40⟩ ✓	

				Lt.	℄	Rt.
	Check	2.71	210.38 = 210.35 = 2" ✓	I.P. N.E. Corn. W½ Lot 16		
						208.87 ✓
19+69.94	℄ Exist. M.H.					4.22
						T.P. m.h. (impossible to get Flow-line)
19+62	Edge cut at m.h.				209.8 ✓	
					5.3	
19+50				207.4 ✓	207.9 ✓	207.8 ✓
				5.7	5.2	5.3
				5		6
						toe Fill Fed. Blvd
19+16.10	℄ Sewer & ℄ 24" Corrug. Pipe			206.6 ✓	208.48 ✓	205.7 ✓
	See sketch Pg. 44.			6.5	4.61	7.35
					11.45 T.P. H.W. Wall	Flo. Line
					∠67° 51' Rt.	24" Pipe
					(Deflect.)	
19+00				209.3	208.6 ✓	209.2 ✓
				3.8	4.5	3.9
				5		5
18+74	Brk				210.09 ✓	
					3.0	
T.P.	1.89	(213.09) ✓	11.20 (211.20) ✓			(213.09) ✓

D. Smith
C Allen
R Taylor
R. Parks

Proposed Sewer

Ref. FB 2012
67
Drawing D-1064 Public Housing Add.
U.S. Gov.

Midway & Kemper St.

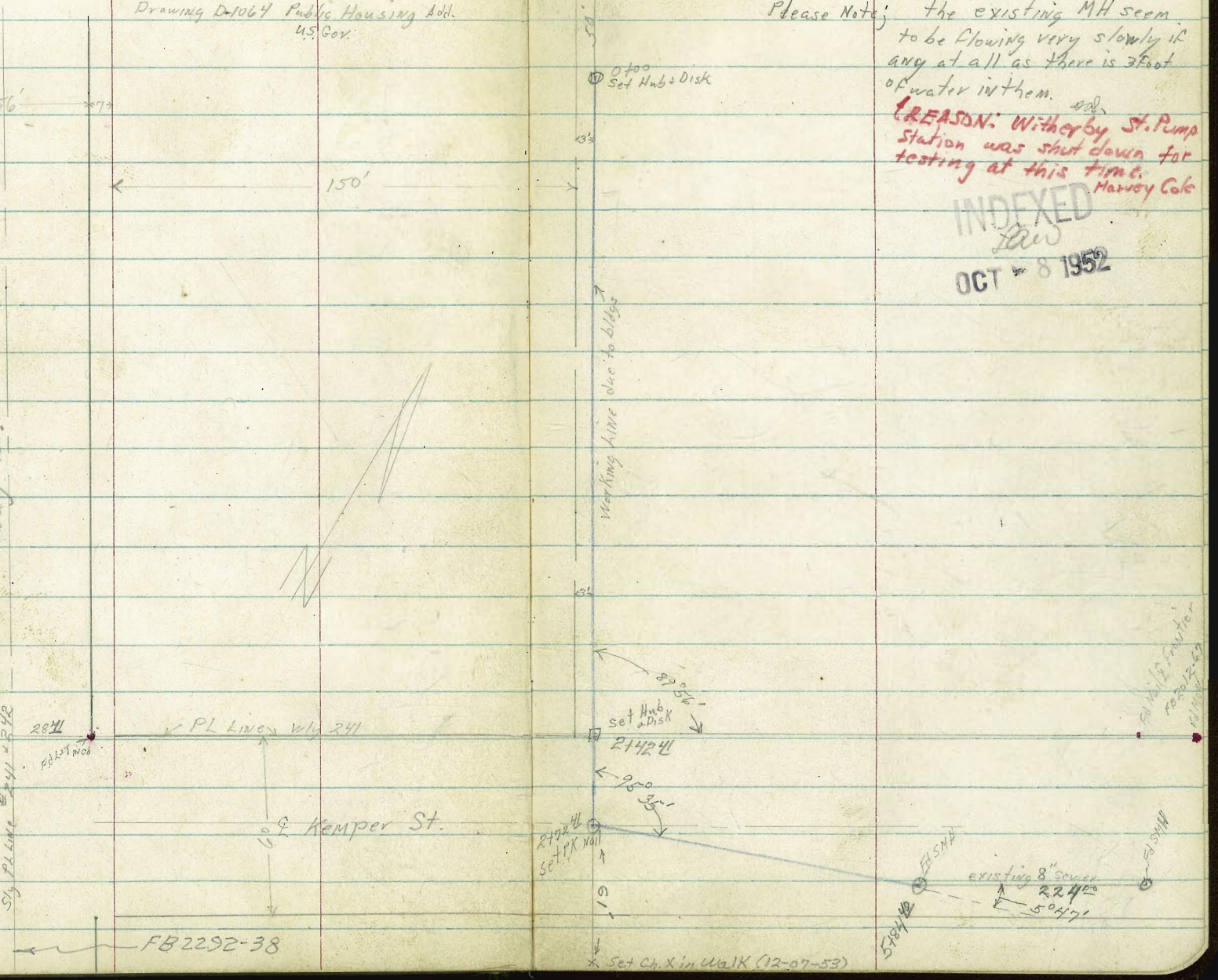
WO # 62289
10-7-52

59

Please Note; the existing MH seem to be flowing very slowly if any at all as there is 3 Foot of water in them.

REASON: Witherby St. Pump Station was shut down for testing at this time. Harvey Cole

INDEXED
OCT 8 1952



	Lt	℄ working line	Rt
1+00		2.7 4.6 10	2.6 4.7 2.1 5.2 3 2.3 5.0 10
0+79 11.5 Rt NE cor Bldg			2.75 4.50 11.5 Floor
0+51 65.5 NE cor bldg	Reduced & Plotted 10/91 H. III. 1/5		2.25 5.00 65.5 Floor 3.80 3.45 111 Floor
0+50		2.3 5.0 10 1.5 5.8 3 1.2 6.1 1.8 6.5 10	
0+10 2.5 Rt SE cor Fence			
0+00 31.5 Rt House 2.2 Rt Fence		2.1 5.2 10 1.75 5.50 Hub 1.85 5.4 3 1.65 5.6 10 2.02 5.23 31.5 Floor	
TP 2	5.75	7.25	4.73 1.50
TP 1	5.19	6.23	8.86 1.04
BM	3.09	9.20	6.81 RP. NW traffic Midway Dr + set From Headwall of culvert

	Lt	℄ working line	Rt
2+42.41 Hub int P.I. & base line	2.8 4.5 10	4.87 Hub	2.7 4.6 3/4 2.6 4.7 3 2.6 4.7 10
2+00	2.8 4.5 10	2.7 4.6 3 2.7 4.6 10	2.7 4.6
1+80 29 Rt end con apron			2.75 4.50 29 apron
1+65 3.9 Rt SE cor lean to			2.66 4.59 3.0 Floor
2.8 Rt NE cor Shed Lean to.			
1+53 1.5 Rt SE cor Bldg			
1+50	2.6 4.7 10	2.5 4.8 2.3 5.0 15 90	
1+25 1.5 Rt NE cor Bldg			2.48 4.77 1.5 Floor
Island W Point Loma Blvd.			7.25

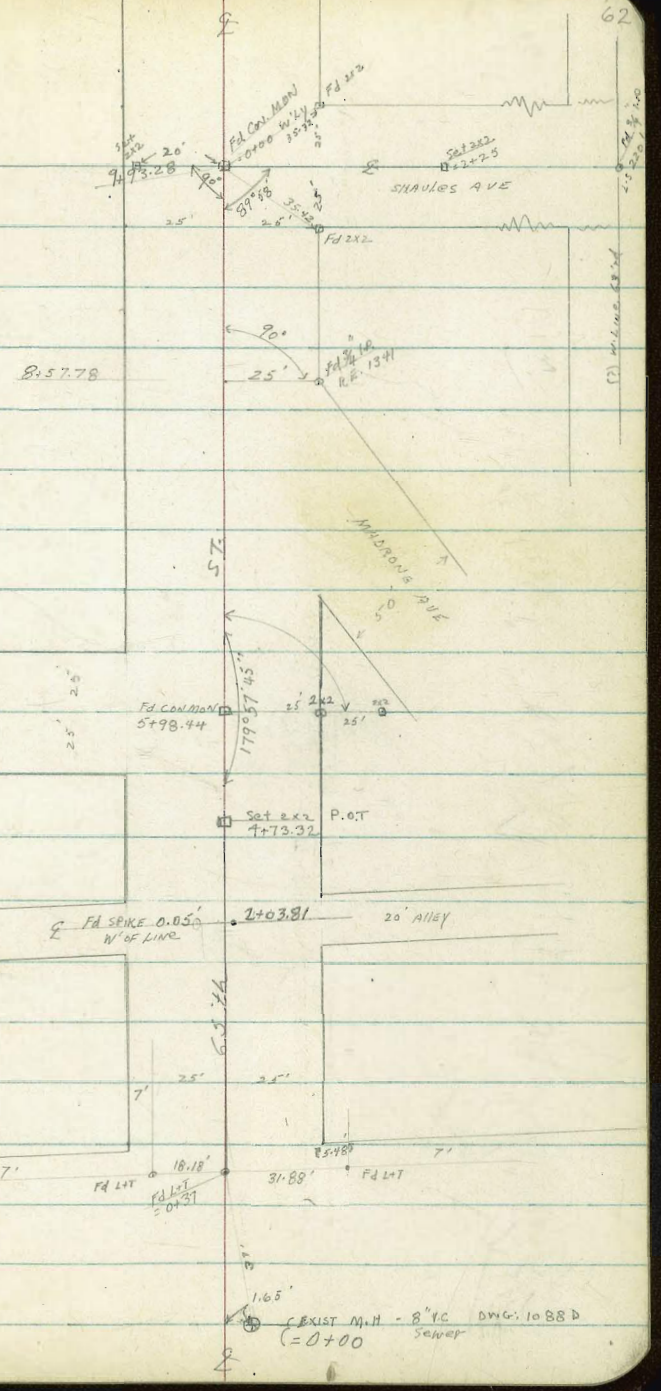
	Lt.	℄ working Line	Rt
4+50		2.11 2.24 2.51 5-61 5-48 5-21 10 5 edge AC. 85	
4+00		2.72 2.09 2.50 5-50 5-63 5-22 10 10	
3+50		2.06 2.04 2.06 5-66 5-68 5-66 10 10	
3+00		2.3 2.02 1.97 5-4 5-70 5-75 10 10	
2+72.41	℄ Kemper St L. taken on split	2.13 1.91 1.90 1.83 5-59 5-81 5-82 5-89 10 3 10	
2+66	℄ crosses Nly AC edge	2.15 2.10 2.08 2.07 5-57 5-62 5-64 5-65 10 3 10	
TP3	5-34	7-72	4-87 2-38

	℄ working Line	(Lt. Pt)
Starting BM	2.96	6.82
TP6 4.76	9.78 1.12	5.02
TP5 5.05	6.14 5.45	1.09
TP4 4.53	6.54 5.71	2.01
8+08.40 ℄ SMH existing	-1.68 3.15 9-40 4-57 1℄ rim	
5+84.40 ℄ SMH L. existing	-2.85 2.71 10-57 5-01 1℄ rim CON 45 has wood cover.	
5+50	2.36 2.67 2.7 2.9 5-36 5-65 5-0 4-8 10 15 5 edge AC. 10	
5+36 ℄ crosses Sly edge AC.	2.65 5-08	
5+00	2.28 2.51 2.59 2.8 5-44 5-21 5-13 4-8 10 43 5 edge AC. 10	
	T 7-72	

Clark
Shephard
Bruner
O'Neil
5-8-53
W.O. 62328

PROPOSED SEWER 6"ø
IMPERIAL to SHAWLES - 4 W.Ly 225'

DATA: F.B. 1660-48



Proposed Sewer 65'4L (Cont)

1+93.71	N'Ly Line Alley				
1+50					
T.P.	11.55	242.15	0.13	230.60	
1+00		Ground to LT & RT Bk of Prop Higher than ℄			
0+90		15' LT END CB 25' LT END Store Bldg			
0+44	Blk	(25'Ly Store Bldg Store on RT connected to Imp. sewer) 5'Ly Line Imp. END A-C Beg Asph. Pav. CB on LT No CB on RT.			
0+30		5'Ly CB Line Imp			
0+23 = ℄ Imp.					
0+00 = ℄ Exist. MH 44' N'Ly 5'Ly Line Imperial & 1.65' W'Ly of N'Ly Projection of ℄ 65'4L					
B.M.		7.09	230.73	223.64 S.E. TP. F. Hyd. Imp. 46 5'4L	

Notes reduced by Carson 5-12-53

LT. (E'Ly) ℄ RT. (W'Ly)

240.3	240.69	240.55	241.11	240.25	240.5	241.0
1.5 50 Dirt	1.76 25	1.60 15' Pav	1.04	1.90 15 Edge Pav	1.7 25	1.2 50

235.35
6.80
242.15
228.67
2.06

226.92	227.50	224.17
3.81 25 Floor	3.23 15 TP CB	9.56

221.7 221.25

9.0 25 Floor	9.48 15 TP CB

220.71
10.02
220.91
9.82
A-C Pav
214.75
16.98
Flow Line
220.60
10.13
Rim

230.73

Proposed Sewer - 65'th (cont)

3+00				
T.P.	12.35	277.03	0.20	264.68
2+62	33.5 Lt ℄ House			
2+50				
T.P.	12.16	264.88	0.83	252.72
2+20	Brk			
2+13.91	℄ly Line Alley			
2+10	Brk			
2+06	End Pav.			
2+03.81	℄ Alley			
T.P.	12.30	253.55	0.90	241.25

Lt.	℄	Rt.
	271.5	
	5.5	
259.58	277.03	
5.30 33.5 Fl.		
	257.9	
	7.0	
	264.88	
247.4	248.1	249.8
6.2 25	5.5	3.8 25
243.9	245.9	246.0
9.1 25	7.7	7.6 25
	243.6	
	10.0	
	242.9	
	10.70	
239.1	242.53	244.46
14.5 100	11.02	9.09 25
241.5		247.1
12.1 50		6.5 50
241.9		248.7
11.7 25		4.9 100
	253.55	

Prop. Sewer 65+46 (Cont.)

5+98.44 = Con. MH ℄ Madrone to E&W			6.02	330.09
T.P. 5+50	12.35	336.11	0.16	323.76
5+00				
4+73.32 2x2 P.O.T.			9.60	314.32
T.P. 4+50	12.29	323.92	0.42	311.63
T.P. 4+00	11.88	312.05	0.50	300.17
T.P. 3+50	11.80	300.67	0.20	288.87
T.P. 3+30	12.26	289.07	0.22	276.81
@ LT ℄ House				

309.1 316.2 324.0 LT. ℄ 330.1 337.9 RT

220 / 75 — 19.7 / 50 — 12.1 / 25 — 6.0 DIFF — + 1.8 / 25

Uniform slope — Uniform slope

336.11 — 326.1 — + 2.2

299.5 307.2 313.9 319.2 323.9

24.4 / 75 — 16.7 / 50 — 10.0 / 25 — 4.7 — 0.0 / 25

Uniform slope — ground rises

323.92 — 308.6 — 3.5

288.5 291.2 312.05 299.9

12.2 / 50 — 9.5 / 25 — 4.3 — 296.4 — 0.8 / 25

ground drops uniformly — ground Rises

300.67 — 285.0 — 4.1

272.37 289.07 279.5

4.66 FLOOR 6.1 — +2.5

Prop. Sewer 65'4h (Cont)

8+50				
T.P.	12.34	383.98	0.59	371.64
8+00				
T.P.	11.92	372.23	0.02	360.31
7+50				
T.P.	12.15	360.33	0.09	348.18
7+00				
T.P.	12.28	348.27	0.12	335.99
6+50				

LT. ℄ RT.

380.0

4.0

383.98

346.2 355.9 363.3 370.4 378.1 379.2

26.0/75 16.3/50 7.0/25 1.9 +5.9/25 +7.0/30

UNIFORM slope

Brk Shoulder = elev. EXIST (Ground Rises Wkly)

372.23

357.5

2.8

360.33

323.8 330.3 337.0 344.2 350.7

24.5/75 18/50 11.3/25 4.1 +2.4/25

UNIFORM slope

Ground Rises

348.27

335.1

1.0

336.11

Prop. SEWER 65'+L (CONT)
SHAULES W'Ly & 65'+L

0+25 = W'Ly Line 65'+L

0+05 = Edge Broken o.l.-pav.

0+00 = W'Ly ON SHAULES Common ℄ 65'+L

12+43.28 = Beyond CREST VERT. CURVE

11+33.28 = CREST Vert. Curve

Note: Profile shots ahead on ℄ 65'+L to show EXIST GRADE 65'+L beyond CREST OF VERT. CURVE

9+93.28	= Com. Msn ℄ SHAULES ∠ 65'+L	6.65	388.99	
9+50				
T.P.	11.93	395.64	0.27	383.71
9+00				
8+80	Beg Broken o.l.-pave			
8+61	BRK = Berm EXIST GRADE MADRONE			

LT. ℄ RT.

392.9 | 394.3 | 390.7
2.7 | H 3 | 4.9
25 | 389.6 | 25
Ground Rises | 6.0

390.7
4.9
395.9
+0.3

380.0 | 383.0 | 386.8 | 389.5 | 389.4
15.6 | 12.6 | 8.8 | 6.1 | 6.2
75 | 50 | 2.5 | 18 | o.l. PAV
Uniform Slope | BRK | BRK | Berm

387.0
8.6
o.l. PAV

395.64

364.7 | 372.7 | 379.9 | 385.0 | 384.4 | 384.2 | 387.5
19.3 | 11.3 | 5.1 | +1.0 | +0.4 | +0.20 | +3.5
75 | 50 | 25 | 6.0 | o.l. PAV | 18 Toc | 24 Shoulder
Uniform Slope | BRK | | Berm | | | | ground-Rises

383.5 | 382.8 | 382.0
0.5 | 1.2 | 2.0
o.l. PAV | | 7
o.l. PAV; MADRONE

383.98

PROP. SEWER 6542 (cont.)
(SHAVLES)

T.P.	0.14	407.21	10.77	407.07.
3+50	Past Crest V. Curve			
4+00 =	Crest Vert. Curve			
	Note: ∫ Profile Cont. over Crest Vert. Curve (on ℄ Shavles, etc			
2+25				
2+00				
T.P.	11.74	417.84	0.53	406.10
1+50				
1+12	℄ house, 82' LT			
1+00				
T.P.	11.42	406.63	0.43	395.21
0+50				

LT. ℄ RT.

406.5
11.3
424.2
+6.4
409.5
8.3
403.3
14.5
7%
UNIFORM slope
407.0
10.8
417.84
402.5
4.1
402.8
3.8
2%
Level
398.9
7.7
8%
floor
398.2
8.4
406.63
396.6
+1.0
5%
394.0
1.6
393.6
2.0
5%
~~383.98~~ 395.64 (Carson)

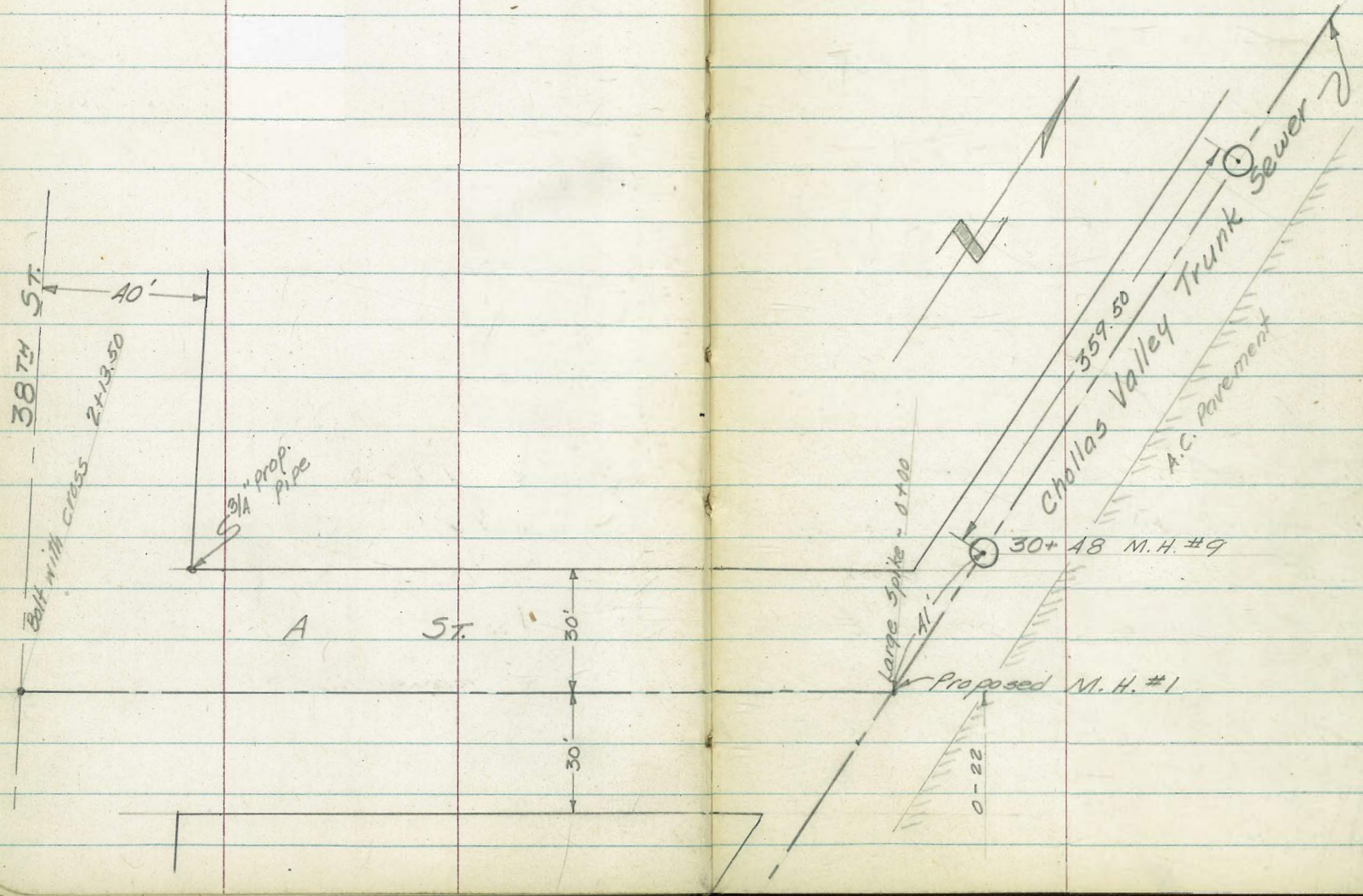
65th - Sewer (Cont.)

CHK:			8.06	223.61 = 223.64 =	S.E. TP. Fire Hyd. 65th x IMPERIAL
T.P.	0.07	231.67	10.96	231.60	
T.P.	0.02	242.56	12.22	242.54	
T.P.	0.24	254.76	12.10	254.52	
T.P.	0.14	266.62	12.12	266.48	
T.P.	0.33	278.60	11.26	278.27	
T.P.	0.30	289.53	12.19	289.23	
T.P.	0.28	301.42	11.94	301.14	
T.P.	0.22	313.08	12.27	312.86	
T.P.	0.45	325.13	12.15	324.68	
CHK: MON E 65th x E MADRONE ELY)			6.76	330.07 - 330.09 (See Pg 65)	
T.P.	0.36	336.83	12.28	336.47	
T.P.	0.35	348.75	12.08	348.40	
T.P.	0.10	360.48	12.15	360.38	
T.P.	0.16	372.53	12.21	372.37	
T.P.	0.71	384.58	12.03	383.87	
CHK: ON CON. MON E 65th x SHAVLES			6.91	388.99	
T.P.	0.70	395.90	12.01	395.20	

Hatch
Whipple
Ferguson
1-5-51
W.O. 62368

Recheck & Profile for Sewer
A St. ~ Chollas Valley Trunk Sewer
213.50 West to E of 38th St.

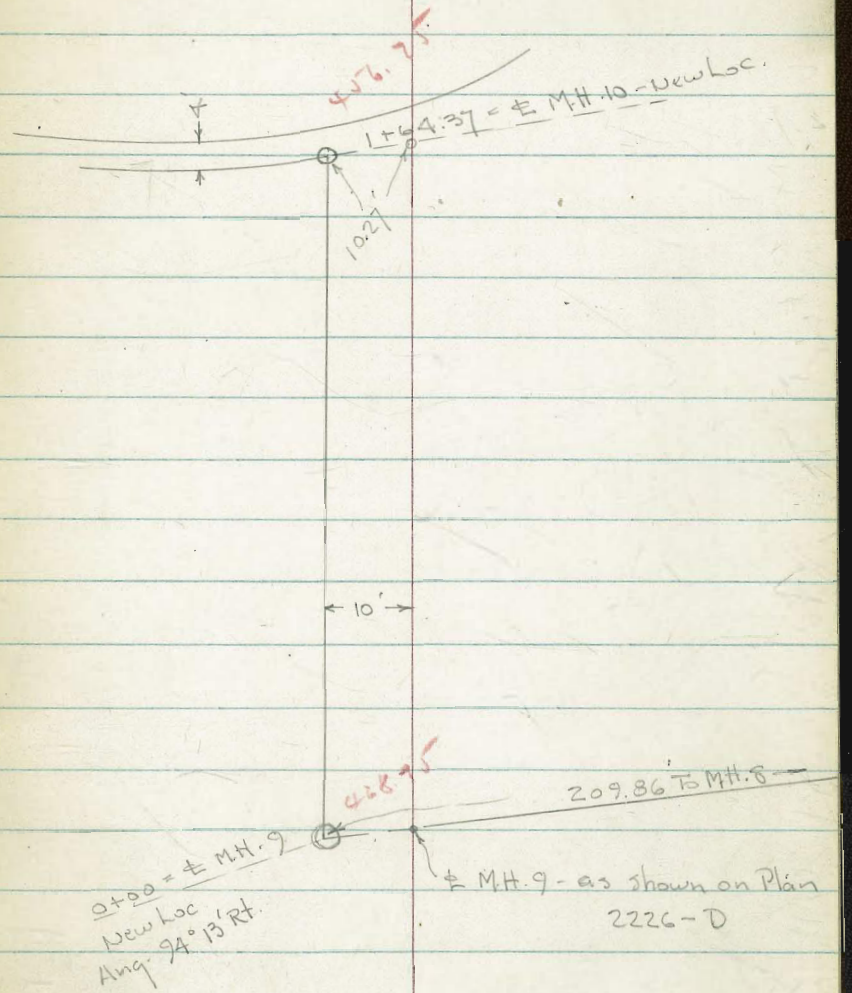
Plan: 5202-B



Recheck Sewer Profile A St.

			℄
Error due to differences in benches (see below)		2+13.50	71.8
City datum	75.35	2+00	71.6
Plan 5202-B	82.50		
R.E. 4191	81.52	1+95	74.1
		1+50	74.2
		1+00	74.4
		0+50	74.2
B.M. = N.W. B.P. on Bridge - Home & Federal	75.35		
City Bench book calls same B.P.		0+05	73.8
75.35, which was used in all notes			
Same B.M. used by privite Engineer		0+00	74.4
# 4191 called elevation	81.52		
From Plan 5202-B =	82.50	0-10	76.2
N.W. Cor. HOME AVE & FEDERAL			
B.M. = Brass plug west side of bridge		0-22	76.23
		Actual Elevs.	edge pave

210' South of M.H. #9 (PIPE EXPOSED) Rod Taken on Top. -1.42 for I.E. or 17."	67.36 Top of 16" Sewer pipe	65.94 I.E
Manhole ~ 30+48 M.H. #9	75.72 Top Ring	68.62 Flow
Manhole ~ 359.5 North of 30+48 M.H. #9 (See drawing)	81.23 Top M.H. ring	73.92 Flow
B.M. = 75.35	Actual	Elev. Shown


4W6.7'
1+64.37 = ± MH.10 - New Loc.
10.27'
10'
4W8.7'
209.86 To MH.8
0+00 = ± MH.9
New Loc
Ang. 94° 13' Rt.
± MH.9 - as shown on Plan
2226-D

Levels along ℄ of New Loc. of Sewer
10' N. from New M.H. 9 to New M.H. 10
See Sketch- P. 73
W.O. 21075 - 2-4-54 - 7.0.

	Lt.	℄	Rt.	
1+23 = edge of A.C. Dr.		62.49		
1+19		62.3		
0+95		56.0		
0+75		52.2		
0+46 = Est. ℄ of small wash		47.0		44.5 = Est. grade of Fl. of wash.
0+25		42.1		
0+00 = New ℄ M.H. 9		35.8		

Note: area has been graded for ditcher.

Actual Elev. Shown.

	Lt	℄	Rt.
old Loc. on Curve.			
1+64.37 = New. M.H. 10 - 10.27 ahead of		64.7 -	
1+60.3 = q.t.		63.60 q.t	64.02 - Top
1+58.3 = edge Conc.		63.68	
1+48.4 = ℄ Pave		63.92	
1+38.3 = edge Conc. Pave		64.03	

INDEXED
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(76)

TIES TO EXISTING SEWER KEMPER &
FRONTIER STS. W.O. 20006
Ref FB. 1679
Ref PHA Map E-706

HOLYOKE ST.

50'

50'

(Contd Pg. 77)

1-28-55
Stampel
Hoffman
Shipman
Sherwood
Elmore

DRIVE
509.14'

ANN ARBOR

90°

90° 00' 30"

M. 106.64'

Set P.K.

E. FRONTIER 286.93'

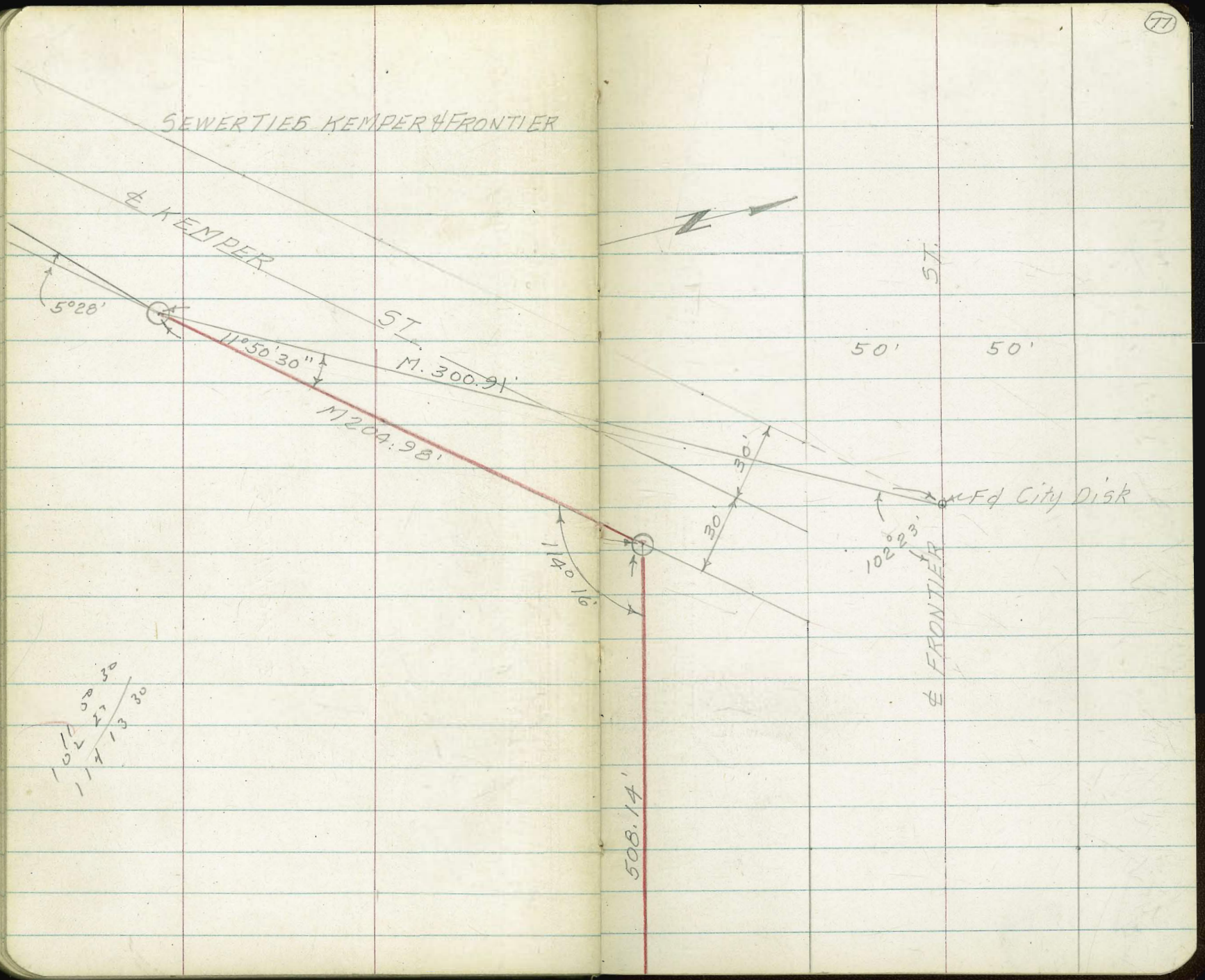
FORDHAM

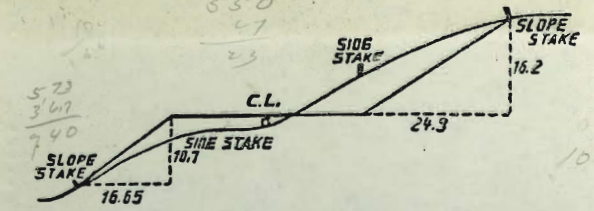
ST

1679-18
65° 53'

Fd City Disk

180° 65° 53' / 114 07


SEWER TIES KEMPER & FRONTIER
℄ KEMPER
ST.
5°28'
11°50'30"
M. 300.91'
M 209.98'
140 16'
508.14'
30'
30'
50'
50'
ST.
Fd City Disk
102°23'
℄ FRONTIER



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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