

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the out or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

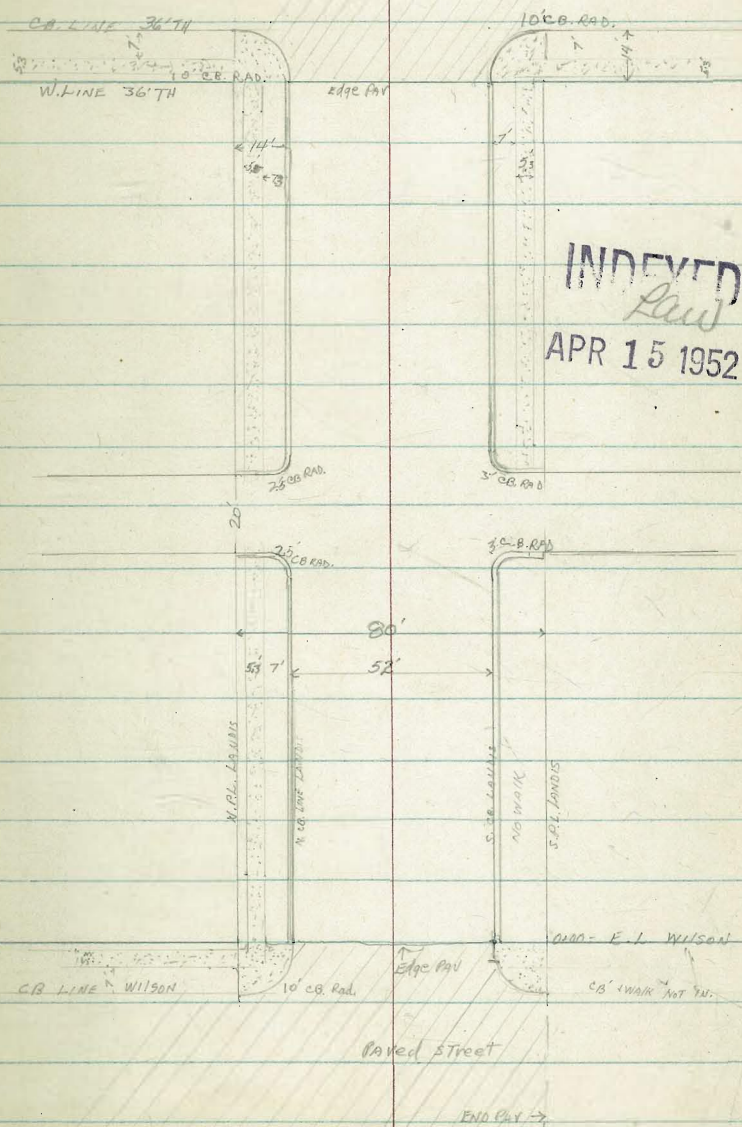
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Clark 4-11-52
Shephard W.O. 32058
Bruner
Bryson

X-SECT. LANDIS, WILSON TO 36TH
(NOT TO SCALE) Notes. Pg. 2



X-SECT. LANDIS: Wilson to 36'TH.

1+40.07 W.L. to Alley

334.9	333.91	333.60	332.5	332.7	333.1	332.5	332.9	333.25	332.70	333.0
50	70	28.5	28.5 EC	26		26	29 EC	29 EC	40 END	50
	TR.CB	TR.CB	GUT.				GUTT.	TR.CB	TR.CB	TR.CB
	VDIFT								+ DIVT	

1+37.57 = Alley BC LT. + 1+37.17 ON RT (see sketch)

333.59	332.7	333.10	332.5	332.25
26 TR.CB	26 B.C.G.		26 CB.C.G.	26 TR.CB

1+37 27.9R to Pole #P3575

1+0.0

333.94	333.53	332.8	333.0	332.5	333.07	332.2	332.7
38.3	26 TR.CB	26 G.		26 G.	26 TR.CB	40	50
B. WALK							

0+50

333.61	333.25	332.6	332.7	332.2	332.77	332.9	331.5
38.3	26 TR.CB	26 G.		26 G.	26 TR.CB	40	50
BK WALK							

0+32 27.7 RT. & P. Pole #P3557

0+00 E.L. Wilson Edge Pav.

333.30	333.04	332.28	332.50	331.91	332.44	332.45
38.3	26 TR.CB	26 G.		26 G.	26 TR.CB	39.3 BK WALK
BK WALK		Edge Pav.		Edge Pav.		

0-14 CB LINE Wilson

335.14	334.54	332.99	332.40	332.23	332.03	331.80	331.62	332.33	332.3
100 TR	100 G.	TR.CB 40	G 40	26 CR.L		26 CR.L	40 G	40 TR.CB	100
							#114 Pav.		

0-40 & Wilson (PAVED)

335.82	333.77	333.57	333.39	333.08	332.79	332.56	332.3	332.5
100	50	40	26 CR.L		26 CR.L	40 END	50	100
						Pav.		

335.25 D.M.T. - Ekv. Rod

335.25 = Elev. N.W. B/P 36'TH LANDIS

X-SECT LANDIS (CONT.)

3+14.14 N.C.B.L 36TH

336.36 335.16 334.97 334.65
 100 TPCB 40 90 T.CB 100 T.CB
 TPCA
 335.82 334.50 335.17 334.54 334.36 334.25 334.48 334.48 335.00 334.40 334.46
 100 G 40 G 36 TPCA 36 G 26 OR.PI 26 OR.PI 36 G 36 TPCA 40 G 100 G
 ON.PAV. ON.PAV.

3+00.14 W.LINE 36TH Beg. PAV 36TH

335.39 335.05 334.18 334.78 334.16 334.78 335.17
 38.3 WALK 26 TPCA 26 G PAV. 26 G 26 TPCA 38.3 WALK

2+50

334.88 334.65 333.9 334.70 333.5 334.25 334.46
 38.3 WALK 26 TPCA 26 G 26 G 26 TPCA 38.3 WALK

2+37

♀ 9' Drive RT

333.53 334.22
 26 Edge 33 WALK

2+00

334.45 334.27 333.4 333.8 333.0 333.70 333.69
 38.3 BR WALK 26 TPCA 26 G 26 G 26 TR CB 38.3 BK WALK

1+90

♀ 14' Drive LT

♀ 13.5' Drive RT

334.37 333.76 333.06 333.72
 38.3 Edge WALK 26 Edge WALK
 26 ♀ Lt

1+63.07 = Alley B.C.H.

333.30 332.7 333.49
 26 G 26 RC TPCA

1+62.5 = Alley B.C.H.

334.10 333.8 333.30
 26 TPCA 26 G

1+60.07 E.LINE 20' Alley

334.6 334.7 334.7 333.8 333.2 333.0 332.7 333.4 333.50 333.35 332.5
 50 40 28.5 EC 28.5 26 26 29.5 40 50
 END CB DIRT GUT TPCA TPCA

1+57

30.5 RT to ♀ Water meter

1+50

21 RT ♀ M.H.

332.73
 21 R.M.H.

X. Sect Landis (CONT)

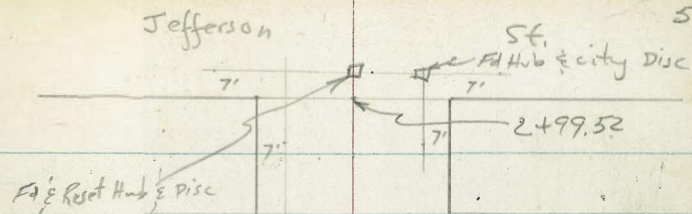
4

Check Direct w/ev Rod: 335.23 = 335.25 NW B.P. 36TH LANDIS

3740.14 E 36TH (Paved)

336.83	335.84	335.30	334.74	335	03	335.02	335.16	334.99	334.73
100	50	40	26			26	40	30	100

Roberts X-Section Arista St.
Cota
Pullen Moore to Jefferson
6-12-52
W.O. 32015



INDEXED

Law
JUN 16 1952

Reduced by
Lawrence
6-19-52

25' Arista 25'

0+00

Moore

St. Hub & Chisel crosses MA

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Lt

E

Rt 6

0+50

25.7	25.1	23.0	22.7	22.2	23.2	25.2
6.9	7.5	9.6	9.9	10.4	9.4	7.4
25	16	12		10	20	25

0+25

27.0	26.6	25.6	25.0	24.1	25.0	25.9	25.6
5.6	6.0	7.0	7.6	8.5	7.6	6.7	9.0
25	16	13		10	12	18	25

0+00

Property Line Moore

27.1	27.8	27.6	27.3	26.7	26.3	27.0	27.8	27.5
5.5	4.8	5.0	5.3	5.9	6.3	5.6	4.8	5.1
50	25	18	15		10	13	25	50

0-10

22.3	27.7	27.6	27.3	27.4	27.7	27.8
10.5	5.9	5.0	5.3	5.2	4.9	4.8
100	50	25		18	50	100

0-13

21.8	26.2	27.2	27.4	27.0	27.3	27.5
10.8	6.4	5.4	5.2	5.6	5.3	5.1
100	50	25		18	50	100

E Moore Street

22.1	26.0	27.93	27.6	27.6
10.5	6.6	4.68	5.0	5.0
100	50	114	50	100

T.P. 814 32.61 π 6.44 24.47

32.61 π

T.P. 203 30.91 7.40 28.88

BM 0.80 36.28 35.48 ^{SEBP} La Jolla & Arista

Cont'd From Page 6

Lt

E

R 7

1774 15' Lt begin 10' cb Inlet

15.14 14.32
5.14 5.96
15 15
cb Gott

1752 20² Lt to center P. Pole # JP3880

12.5 14.5 15.0 15.0 15.1 15.6 16.6
7.7 5.7 5.2 5.2 5.1 4.6 3.6
50 25 12 52 10 25 50

1748 18² Lt to center P. Pole # 3877

16.0 16.0 15.7 15.4 16.4
4.2 4.2 4.5 4.8 3.8
25 13 9 25

1700

21.0 20.5 19.0 19.0 17.7 17.2 16.7 17.2 17.6 19.4 19.9 19.9
+0.8 +0.3 1.2 1.2 2.5 3.0 3.5 3.0 2.6 0.8 0.3 0.3
35 28 25 16 13 9 11 17 20 25 35

T.P. 0.61 20.28π 12.94 19.67

20.28π

0775

23.6 24.0 22.9 20.3 19.9 19.5 19.7 22.1 22.7
9.0 8.6 9.7 12.3 12.7 13.1 12.9 10.5 9.9
25 20 15 12 10 15 20 25

0758 20² Lt to center P. Pole # R3870

32.61π
23.61

32.61π

Cont'd From Page 7

Lt

Rt

Rt

R

80

2+49 25³ Rt & 3' conc walk

17.90
2.38
25²
conc

18.46
1.82
36⁸
conc

2+34 25² Rt End one wall begin

17.1 16.7 17.58 17.79

31 3.5 2.70 2.51
25² Foot 25² 25²
SRD 25² Top Top
Foot west

2+24 25³ Rt & 25' conc walk

17.84
2.84
25²
conc

18.28
2.00
36⁸
conc

2+11 25⁴ Rt Begin conc BIK Ret. Wall

16.8 16.6 17.76

3.4 3.6 2.52
25⁴ 25⁴ 25⁴
SRD Foot Top

2+00

13.0 14.3 14.8 14.3 14.9 15.2 15.1 16.0 16.5 17.8

7.2 5.9 5.4 5.9 5.3 5.0 5.1 4.2 3.7 2.4
50 25 16 14 10 10 18 25 50

1785² 24⁶ Lt & 3' conc walk

13.21 13.90

7.07 6.38
40 24⁶
conc conc

1785 15' Lt End curb Inlet

15.17 14.33

8.11 8.75
15 15
Cb Gutt

9.00
11.28
INVERT
of
Inlet

20.28

20.28

Cont'd From Page 8

Lt

E

Rt 9

3+10 146 Lt to center Storm Drain MH

20.21
6.32
146
TOP
MH

3+08

13.2	18.4	19.7	20.6	22.1	22.8	24.0
13.3	8.1	6.8	5.9	4.4	3.7	2.5
100	50	25		25	50	100

2+99.50 { 25 ft End wall
Property Line Jefferson

17.6	18.3	19.0	19.5	20.1	19.9	19.3	19.8 ³	20.6
8.9	8.2	7.5	7.0	6.4	6.6	7.2	6.10	5.9
50	25	14		14	25 GPD	25 Foot	25 TOP	50

T.P. 7.34 26.53 X 1.09 19.19

26.53 X

2+98 17 1/2 Rt to center 5" Pepper Tree

16.1	16.6	15.8	16.8	17.0	17.2	18.0	18.5	18.97	19.20
4.1	3.6	4.1	3.4	3.2	3.0	2.2	1.7	1.31	1.08
25	17	15	10		11	18	25 conc	25 conc	36 ² conc

2+75 25 Rt E 2 Conc Walk

2+60.5 25 1/2 Rt End one wall begin another

17.7	17.6	18.0	18.9
2.5	2.6	2.2	1.5
25L GPD	25L Foot	25L West	25L East

2+50

13.9	15.2	15.6	15.0	15.6	15.7	16.0	16.4	17.4	18.4
6.3	5.0	4.6	5.2	4.6	4.5	4.2	3.8	2.8	1.8
50	25	17	14	9		10	15	25	36

20.28 X

20.28 X

check 0.80 35.47 = 35.48

T.P. 11.57 36.27 1.83 24.70

Q Jefferson Street

26.53 T

12.3	17.4	19.5	20.98	22.1	23.1
14.2	9.1	7.0	5.55	4.4	3.4
100	50	25	100	50	100

26.53 T

X-sec.

WINONA

8-6-52

Orange to 300' Nly.

W.O.#32031

INDEXED
Law

AUG 7 1952

C.H.S.
Begg
Oltman
Johns

denotes Pd. $\frac{1}{2}$ hub * Tack or disk

Ref. T.P. sheet 3664

F.B. $\frac{1672}{16}$

direct elev. rod used.

#7 B.M. = S.E. B.P. 49th + Orange

El. = 332.95. The hundred (which

is 3) is not shown in notes

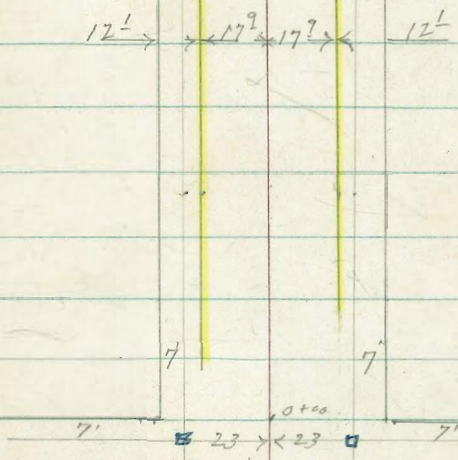
G = ground in gutter 19⁹' off \pm

cl. = top of cl. 17⁹' off \pm

Soil sample 10' N of Sta. 1400

APPROX.

N



\pm Orange = 0-40

Winnona

4

12

38.40
CL

1+2A 17⁹ = start 5' ch. to be refinished -

1+10 17⁹ Lt. = start A' ch. to be retopped

1+08 - 17⁹ Rt. = 6' ch. to be refinished

1+00

371.8
37.3 37.57 36.8 37.1 37.1 36.5 35.7 36.38 35.8 35.4
50 30 ch G 9 9 G ch 30 50

0+75

36.2 35.86 35.1 35.4 34.3 34.82 34.4
30 ch G G ch 30

0+59 = driveway on Lt.

36.30 35.48 34.33
40 30 17⁹
driv

0+42^A 17⁹ Rt. = start 3' ch. to be topped.

0+33 - 17⁹ Rt. = start conc. ch.

33.8 33.01 32.3 32.1 31.6 32.0 32.95 32.7
30 ch G 16 G ch 30

T.P. = 332.14

0+04^E 17⁹ Lt. = start conc. ch.

31.39 30.0
ch G

0+01

29.8 30.6 30.3 29.2 29.6 28.7 30.7 31.0 30.4
100 30 18 17 17 20 30 100

0+00 Cont.

B.W. = base of wall

T.W. = top " "

block wall.

30' RT. = South face 8' wide conc.

0+00 = N.Y. line orange

29.7 30.9 27.0 31.4
100 30 100 100
T.W. Ord T.W.
30.4 30.2 29.2 29.5 28.7 28.9 28.5 27.5
30 18 17 17 18 30 30
B.W.

0-40 = 4 orange

29.2 28.4 27.9 27.9 27.7 26.6 24.7
175 100 30 30 100 175

T.P. 331.39

Winona

2+10 - 17⁹ Rt. = start 5' of curb.
to be replaced.

broken out. Replace as driveway.
2+07 - 17⁹ Lt. = start 10² of curb

2+00

47.1 47.4 47.69 47.0 47.2 47.5 47.3 46.7 47.62 47.6 47.0
30 19 cl G 9 9 G cl 19 30

1+75

44.4 44.3 44.48 43.6 44.2 44.1 44.0 43.3 44.20 43.9 43.6
30 19 cl G 9 9 G cl 19 30

7. (T.P. = 344.30)
curb.
Note / should be replaced with standard
This drive is not in use. 15' long

1+62 17⁹ Lt. = \pm drive

43.55 43.24 42.47
30 24 17⁹

1+56³ 17⁹ Rt. = start 2' cl. to be replaced.

1+51

41.98
cl

1+50

41.1 41.2 41.4 41.4 41.2 40.3 41.13 40.6
30 cl G 9 9 G cl 30

1+46 - 17⁹ Lt. = \pm drive way

40.40 41.65 41.70 40.80
40 30 29 17⁹

1+25

37.4 37.54 38.6 38.9 37.0 38.8 37.9 38.4 37.9
30 cl G 9 9 G cl 30

T.P. 338.99

(Top)
zone

59.4 58.7 58.6 59.1
30 19 19 30

2+75 } cb. on left leans into roadway

58.64 57.7 57.9 57.9 57.7 57.8 58.60
cb. G 9 9 G cb
No good No good

2+51 - 25' RT = 20" diam acacia. (4 trunks from roots)

54.1 54.4 54.7 54.0 52.5
30 19 19 30 40

2+50

54.89 53.9 54.0 54.1 54.2 54.1 55.04
cb G 9 9 G cb
No good No good

2+46 { 17' RT = start curb to come out.
20' Lt = 8" acacia stump to come out.

2+38 17' RT = & driveway

54.60 17' cb
52.82 53.47 53.16 54.40
17 24 30 40

to preserve new curb to be built. This should come out so as

2+38 - 20' Lt = 14" diam acacia.

replaced.

2+31 - 17' Lt = start curb to be

T.P. 352.45

2+26 - 17' RT = start 4' cb to be

50.8 50.6 51.3 51.4
30 19 19 30

2+25

51.12 50.5 50.7 51.0 51.0 50.5 51.34
cb G 9 9 G cb

N117011A

15

±

EL in Bench book:

362.89 = N.W. B.P. Trojan + winona 362.91

Error 0.02

362.89

T.P. 366.74

T.P. 366.21

3+30

65.52	64.92	65.18	65.40	65.27	65.04	65.59
cb	G	9		9	G	cl

62.2
30

3+00 = { start oil + rock pavement

62.4	62.21	61.70	61.80	62.00	61.80	61.60	62.16
30	cb	G	9		9	G	cl

start good curb

2+93.9 17.9 Lt = end no good curb.

61.41
cb

2+91 - 17.9 Rt = driveway

60.90	60.22	
30	40	
60.45	60.97	61.17
172	218	263

also start good curb.
to come out.

TP358.84

2+83.5 17.9 Rt = end of N.G. curb

59.88
cb

Oliver St.
Lamont to Olney

C.H.S.
Beqq
oltman
Schelin

3-30-53
W.O.# 32050

- denotes Fd. Conc. Mon
- " " " Lat.
- ✕ " " cross in Conc.
- ✕ " " cut cross " "
- " " Nail or temp. point.
- Ⓢ " " Ctr. water meter box.

Soil sample #1 { 20' west of ϕ Noyes
30' North of ϕ Oliver

" " { ϕ Oliver
#2 250' East of Ely line Lamont

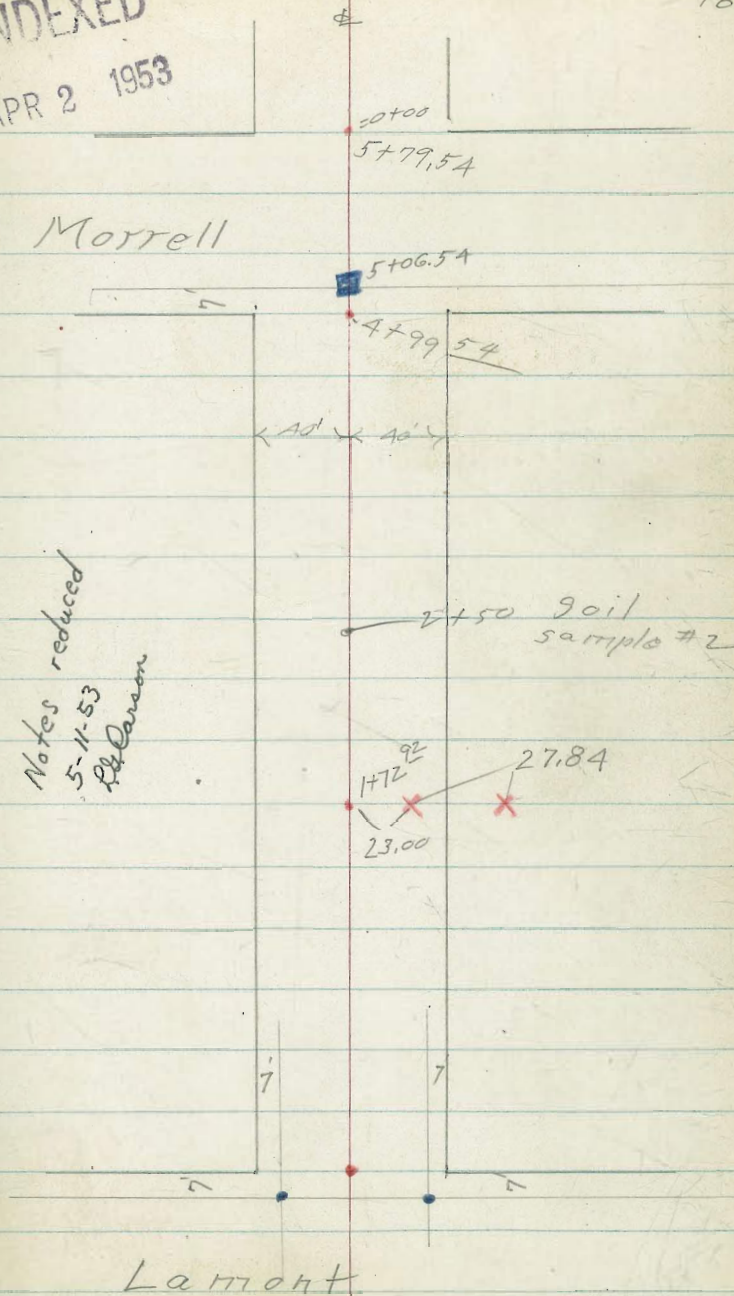
No soil sample taken from
marsh or loose fill (page 31-on)
this is regular bay mud +
street sweeping + sand.

INDEXED

APR 2 1953

16

Morrell



Cross on
drive →

10'

5+79.63

Noyes

soil sample #1

5+06.63

Cross
in
walk

10'

Levels page 26
and page 56

Reed

0+00

Morrell

5+06.54

7'

7'

Olney

EL. Man. =
-2.05

7'

5+06.45
1A20
4+99.45

1952 year nail
1 1/4" pole # A178

EL nail
= 4.39

7'

105.95

P.K. in pole # 2171
EL nail = 4.94

40' x 40'

set stub 1/4" x 1/2" C.H.S.

2+00

New levels
P-58

For
ditch see p. 61

0+00

5+79.63

Noyes

5+06.63

Oliver

T.P. 3.97 44.34 4.79 40.37
 0-10 - 20' RT } = E.C. 10' Rad. Cl. Rot.
 20' LT }
 on New Cold Lay

0-20 Cont.

2" ± thick
 = end good rock + oil

30' RT } = B.C. 10' Rad. Cl. Rot.
 30' LT }
 0-20 = Ely Cl. line Lamont

0-40 Cont.

0-40: ± Lamont (Rock + oil Pave.)

B.M.#2 4.79 45.16 5.74 40.37

B.M.#1 5.74 46.11 — 40.37

40.16	40.16	40.16	40.16	40.16	40.16	40.16	40.16
5.00	39.54	39.7	39.78	39.98	39.54	39.65	5.00
20	20	20	10	10	10	19.8	19.8
Cl.	get.	get.	Cl.	get.	get.	get.	Cl. E.C.
ETC.							
40.52	40.95	40.95	40.95	40.95	40.95	40.95	40.95
4.64	4.21	4.21	4.21	4.21	4.21	4.21	4.21
165	162	162	162	162	162	162	162
Pave.	Cl.	Cl.	Cl.	Cl.	Cl.	Cl.	Cl.
40.53	40.61	40.16	40.28	40.28	40.28	40.28	40.28
4.63	4.55	5.00	4.88	4.88	4.88	4.88	4.88
G	100	100	40	40	40	40	50
162	Cl.	G	Cl.	Cl.	G	Cl.	Cl.
39.74	40.21	39.74	39.65	40.04	39.69	39.62	40.19
5.42	4.95	5.42	5.51	5.12	5.47	5.54	4.97
40	30	30	20	20	20	30	30
G	Cl. B.C.	G	Pave	Pave.	G	Cl. B.C.	Cl. B.C.
40.54	41.38	40.96	40.96	40.96	40.96	40.96	40.96
4.62	3.78	4.20	4.20	4.20	4.20	4.20	4.20
50	165	100	100	100	100	100	100
40.54	40.46	40.37	40.08	40.08	40.08	40.08	40.08
4.62	4.70	4.79	5.08	5.08	5.38	5.40	5.50
50	40	30	30	30	30	40	50
			45.16	45.16	45.16	45.16	45.16

N.E. 7' LT. Oliver + Lamont

S.E. 7' LT. Reed + Lamont

0+45 - 22' Rt. = start 6' high Hedge
- 26' Rt. = 14" Diam Palm.

39.72
4.62
20
39.68
4.66
40
39.72
4.62
50

0+32 - 20' ^{8'}Rt. & 2' wide conc. walk.

0+24 - 27' Lt. = 14" diam poppo
start picket fence.

0+15 - 40' Lt. = end Hedge +

0+12 - 28' Lt. = 24" diam acaccia

0+10 40' Rt. = 5" Diam Tree.

{ 25' Rt. = 4" Diam. Aspen

0+04 { 22' Lt. = (W)

0+03 22' Lt. = (W)

0+02 22' Lt. = (W)

25' Rt. = 1" Diam Palm.

0+01 22' Lt. = (W)

40.4
3.9
40
40.44
3.90
35
walk
40.41
3.93
35
walk
40.34
40
40
40.35
40.02
39.79
39.65
39.76
4.7
39.73
39.85
40.21
40.39
3.99
30
walk
4.32
20
cl
20
gut.
10
on edge of
Cold Lay
4.13
10
gut.
4.13
20
cl
3.95
30
walk

30' Rt. = N.E. Cor. 5' wide conc. walk.

20' Rt. = end curb walk

30' Lt. = S.E. Cor. 5' wide conc. walk

20' Lt. = end curb

40' Lt. = start 4' high Hedge.

0+00 Ely Lino. La mant

0-01 - 21' Rt. = (W)

-0-03 21' Rt. = (W)

0-05 21' Rt. = (W)

0-06 22' Lt. = (W)

Oliver St.

¢

T.P. 3.80 42.32 5.82 38.52

1+43 34^E RT = ¢ 3' wide conc. walk

1+23-34^E RT = ¢ 2' wide conc. walk

1+16-40' Lt. = ¢ 2' wide Conc. walk

1+00 27' Lt. = 14" Diam pepper

0+90 27^E Lt. = 1" Diam pepper

0+82 30' RT = ¢ 3' wide Conc. walk
28' Lt. = 10' high shrub.

0+64 27' Lt. = 5' high shrub

0+60-19^E RT = ¢ 6' wide level conc. drive

0+55-22' RT = end hedge

0+50 28^E Lt. = 18" Diam Acacia

38.97
5.37 5.37 5.31
34^E 40 50

39.27 39.14 39.12
5.07 5.20 5.22
34^E 40 50

39.79 39.69
4.55 4.65
60 walk 40

39.8 39.1 39.2
4.15 5.12 5.1
40 15

38.8 39.3
5.15 5.10
15 40

39.22 39.20 39.17
5.12 5.14 5.17
30 40 46
walk

39.18 39.19 39.24
5.16 5.15 5.10
198 40 51
drive car floor

39.8 39.6 39.2
4.15 4.7 5.1
20 20 16 18 40

39.9 39.4 39.2
5.4 4.9 5.1
16 18 40

(40) Carbon

44.34

2+47			36.9	36.8	36.7	36.3	36.6	36.1	36.4	37.1
			5.4	5.5	5.6	6.0	5.7	6.2	5.9	5.2
			50	40	25	20		12	14	40
2+35	75' Lt. = \pm double bar	floor conc.			37.52					
					4.80					
					75					
					Floor					
2+27	40 ⁵ Lt. = end board fence			37.0	37.2		37.9	37.5	37.9	37.9
2+20				5.3	5.1	4.4	4.8	4.4	4.4	4.4
				40	20		12	15	40	40
1+90			37.5	38.2	38.5	38.6	38.2	38.4	38.7	
			4.8	4.1	3.8	3.7	4.1	3.9	3.6	
			40	30	15		15	17	40	
1+78				39.1	38.7	38.7	38.5	38.5	38.5	
				3.2	3.0	3.6	3.8	3.5	3.5	
				40	15		15	40		
1+77	41' Lt. = start board fence						38.54	38.99	39.04	
	40 ⁵ Lt. = end picket fence						3.78	3.33	3.28	
1+73	21 ² Rt. = \pm 3' wide conc. walk						21.9	40	50	
1+50			39.3	38.9	38.9	38.6	39.0			
			3.0	3.4	3.4	3.7	3.3			
			40	15		15	40			

42.32

Oliver

3+11 - 40' Lt. = \pm 8" wide conc. ^{walk} block

34.8
7.5 10.6 9.5
404 404 40
T.W. B.W. End

3+00

34.6 34.5 33.3 32.8 33.0 32.5 32.9 33.7 34.4
7.7 7.8 9.0 9.5 9.3 9.8 9.4 8.6 7.9
50 40 37 20 20 25 35 40 50

2+98 39⁵' Rt. = \pm 2⁵' wide conc. walk

34.21 34.40
8.11 7.92
39⁵' walk 50

2+90 - 40' Rt. = end conc. drive

34.55 35.28 35.57
7.77 7.04 6.75
40 55 68

2+86 40' Lt. = \pm 3' wide conc. walk

34.85 34.72
7.27 7.60
50 40
walk

2+80 40' Rt. = start conc. drive

35.22 35.72 35.57
7.10 6.60 6.75
40 55 68
on floor

2+55

35.12 35.6 36.1
7.2 6.7 6.2
40 20

35.8 36.3
6.5 6.0
20 40

42.82

22

Oliver

#

23

3+84 - 38² Rt. = ± 6" ^{wide} Conc block wall.

27.95
3.6
38
Grd
27.5
41
38²
B.W.
27.0
1.3
38²
T.W.

3+80 38⁵ Rt = end drive

3.15
38²
drive
1.27
68
Gar. floor

3+70 38⁵ Rt = start Conc. drive

28.62
2.48
38²
drive
29.23
1.27
68
Gar. floor

3+65 ?? Corron

2+65

25.1
25.7
26.8
26.2
27.1
60
5.4
4.3
4.9
4.0
50
40
25
20

27.7
3.4
2.5
20
40

31.10

T.P. 1.00 31.10 12.22 30.10

3+40 ?? Corron

2+40 38' Rt. = ± 6" wide Conc. wall.

30.8
11.5
38
Grd.
30.4
11.9
38
B.W.
32.6
9.7
38
T.W.

3+35 - 39⁴ Rt = end drive

31.28
11.04
394
32.87
7.45
56
Gar.

3+25 - 39⁴ Rt = start Conc. drive

30.0
30.4
31.1
30.6
30.9
12.3
11.9
11.2
11.7
11.4
50
40
25
20

30.8
31.58
31.7
32.87
11.5
10.74
10.6
7.45
20
394
drive
40
56
Gar.
Floor

42.32

Oliver

24

A+50 43⁷ Lt. = start conc. drive

20.05	19.25	18.8	18.0	18.8	19.1	21.1
11.05	11.85	12.3	13.1	12.3	12.0	10.0
55	432	40	30		15	40
on drive						on drive

A+34 38¹ Rt. = start conc. drive

21.95	22.70
9.25	8.40
382	61
	Bar, floor

A+29 45' Lt. = Φ 2⁵ wide conc. walk

21.12	20.36
9.98	10.74
55	45
walk	walk

A+27 38⁷ Rt. = Φ 2⁵ wide conc. walk

22.40	22.95
8.70	8.15
382	492
walk	

A+00 38⁴ Rt. = end drive

22.1	22.0	22.4	23.3	24.1	26.0	26.22	27.67
9.0	9.1	8.7	7.8	7.0	5.1	4.88	3.43
50	40	20		18	38	384	456
						Drive	Bar

3+95 - 44⁸ Lt. = Φ 3' wide conc. walk

22.32	22.20
8.78	8.90
548	448
walk	

3+90 - 38⁴ Rt. = start conc. drive

26.58	27.68
4.52	3.42
384	56
drive	Bar

31.10

Oliver

25

5+15

40 RT
39-RT
37 RT

} = (W)

5+11- 36 RT

= wly line Morrell

4+99⁵⁴ 40' RT = end conc. block wall.

4+99 20³ RT = 12" pole[#] 1999

4+80- 20' RT = dead man

4+75

4+73 40' RT = start conc. block wall

T.P. 1154 21.23 11141 19.69

4+59- 43 RT = end drive

4+51 38 RT = end conc. drive.

16.4
16.0
16.0
16.0
15.6
16.0

19.7 19.5 17.8 16.6 16.2 16.2 15.9 16.9 16.2 19.9
1.5 1.7 3.4 4.6 5.0 5.0 5.3 4.3 5.0 1.8
50 45 40 36 25 25 40 40 40 40
B.W. T.W.

19.7 19.7 17.0 17.2 17.7 19.5 20.0
1.5 1.5 4.2 4.0 3.5 1.7 1.2
50 40 32 40 20 40 50

19.3 18.8 19.69
1.9 2.4 1.54
40 40 40
B.W. T.W.

20.08
19.20
11.02 11.90
55 43 RT
on drive

20.96 22.65
10.14 8.45
38 RT 63
drive Bar.

31.10

F

Pole #2015

T.P. Nail 2.63 18.50 5.36 15.87

1+00 14' 19+ = 10" pole # 2015

0+90 51' Lt. = 3' wide Conc. walk

0+60

0+42 - 40.5' Lt. = 9' Conc. Dr

0+30

= 0+00

5+79.54 = Ely. Morrill

5+39.54 = Morrill (24 improved)

Note!
See page 56 for
new notes for yardage
south of E of Oliver
Taken 1-29-54

18.9	18.8	17.2	16.3	15.6	14.9	14.7	14.0	12.3	9.8
2.3	2.4	4.0	4.9	5.6	6.3	6.5	7.2	8.9	11.4
60	50	40	27	26		12	15	40	60
		19.17		18.67					
		2.06		2.56					
		614		514					
		walk							
19.5	18.9	17.0	16.1	15.4	14.6	14.0	12.9	11.2	10.8
1.7	2.3	4.2	5.1	5.8	6.6	7.2	8.3	10.0	10.4
60	50	40	27	26		12	15	40	60
	20.35		19.48	17.85					
	58.8		50	48.5					
	Floor of gar.								
	16.6	16.1	14.7	14.5		13.5	12.2	10.5	11.8
	4.6	5.1	6.5	6.7		7.7	9.0	10.7	9.4
	40	27	26			20	40	80	100
	18.0	16.4	15.1	14.7		14.5	14.7	14.2	
	3.2	4.8	6.1	6.5		6.7	6.5	7.0	
	50	40	25			20	40	50	
	21.2	16.4	15.7	15.4		15.4	15.6	18.4	
	4.0	4.8	5.5	5.8		5.8	5.6	2.8	
	115	40	20			20	40	140	

21.23

Oliver

27

2+34 40' Lt = 8' wide Conc. drive

15.40
3.10 4.66
60
Car.

2+16 40' Lt = 8' wide Conc. drive

16.08
2.42 4.09
60
Car.

2+00

14.7 14.1 13.1 13.4 13.3 13.1 12.0 10.3
3.8 4.4 5.4 5.1 5.2 5.4 6.5 8.2
40 30 29 20 15 40 100

1+97 40' Lt = 4' wide conc. walk

15.00
3.50 3.66
50 403

1+66 40' Lt = 8' wide Conc. drive

16.68
1.82 2.93
60
Car. drive

1+50

15.8 15.2 14.6 14.4 14.1 12.9
2.7 3.3 3.9 4.1 4.4 5.6
40 29 25 12 40

1+47 40' Lt = 4' wide Conc. walk

16.40
2.10 2.41
50 40
walk

18.50

Oliver

4+11 14' Lt. = 10" diam pole # 2065

4+02 38² Lt. = 3' wide Conc. walk

11.58
11.18
11.14
1.20 1.60 1.64
50 40 38²

4+00

11.7 11.1 11.0 9.2 8.6 8.4 9.4 8.5 7.7 5.5
1.1 1.7 1.8 3.6 4.2 4.4 3.4 4.3 5.1 7.3
50 40 37 24 12 13 20 40 100

3+77- 3.8⁸ Lt. = 2' wide Conc. walk

t.p. 330 12.78 9.08 9.42

3+50

12.16 11.94 11.92 12.78
0.62 0.84 0.80
50 40 38²
12.6 11.8 10.4 9.8 9.7 8.0
5.9 6.7 8.1 8.7 8.8 10.5
40 30 28 15 40

3+00

2+51- 15³ Lt. = 10" pole # 2051

13.8 12.8 12.2 11.3 11.0 10.6 9.5 7.6
4.7 5.7 6.3 7.2 7.5 7.9 9.0 10.9
60 40 29 28 15 40 100

2+50

13.5 12.0 12.0 11.7 11.0 10.3
5.0 6.5 6.5 6.8 7.5 8.2
40 25 15 25 40

2+45- 39² Lt. = 3' wide conc. walk

14.75 13.66
3.75 4.84
55 39²

18.50

oliver

B.M. 2.90 6.53 7.15 3.63

35' RT = dead man

5+11 14' RT = 10" pole # A198

4+99⁶³ = wly line Noyes

4+94- 41³ Lt. = 3' wide Conc. walk

4+54 41² Lt. = 3' wide Conc. walk

4+50 - 40' Lt. = 6" conc. wall

4+48- 40' Lt. = 2⁵' wide Conc. walk

4+23- 37⁸ Lt. = 3' wide Conc. walk

Noyes + oliver
chiseled square Nly. end N.W. cl. Ret

7.0	6.8	5.8	3.9	3.5	2.8	3.8	3.2	1.8
5.8	6.0	8.0	8.9	9.3	10.0	9.0	9.6	11.0
50	40	27	20		11	14	40	100

3.08	7.19
4.70	5.59
5.13	4.13

8.08	7.78	7.6	6.5	6.2	5.8	6.7	5.8
4.70	5.00	5.2	6.13	6.6	7.0	6.1	7.0
50	41 ²	40	20		15	16	40
walk							

8.9	7.9	8.4	6.9	6.5	6.2	6.8	5.8
3.9	4.9	4.4	5.9	6.3	6.6	6.0	7.0
40	40	40	20		15	16	40
T.W	B.W						

8.98	8.66
3.80	4.12
50	40

10.84	10.44	10.34
1.94	2.34	2.44
50	40	37 ⁸

12.78.

Oliver

30

40' Lt. = sly edge A.C. Pav.
 50' Lt. = B.C. curb.
 5+59⁶³ = Ely cl. line Noyes

3.81
2.72
100
cl

3.20
3.33
100
G

3.03
3.50
50
B.C.

2.39
4.14
50
G

2.45
4.08
40
E.P.

1.8
4.7
20

5.09
5.6

-0.5
7.0
5

-0.7
7.2
20

-1.0
7.5
40

40' Lt. = sly edge pave.
 5+39⁶³ = E Noyes

3.83
2.70
100

2.99
3.54
50

2.76
3.74
40
E.P.

2.2
4.3
20

1.7
4.8

1.1
5.4
20

0.3
6.2
40

-1.8
8.3
100

5+19³ Conf.

4.12
2.41
100
cl

3.49
3.04
100
G

3.58
2.95
50
cl

53' Lt. = approx E.C. cl. as built
 40' Lt. = sly edge A.C. Pav.
 5+14³ = wly cl. line Noyes

2.93
3.60
53
G

3.03
3.50
40
E.P.

2.8
3.7
20

2.4
4.1

2.2
4.3
20

1.6
4.9
40

5+17⁸ - 40³ Lt. = start existing cl.
 + A.C. Pav.

3.59
2.94
40³
cl

2.94
3.59
40³
G

5+12

3.6
2.9
40

3.2
3.3
36

2.8
3.7

2.5
4.0
10

3.8
2.7
13

3.5
3.0
37

2.6
3.9
40

2.3
4.2
50

6.53

oliver

Nail in Pole # 2119

T.P. 7.19 7.14 6.58 - 0.05

1+08 - 41' Lt. 2 8' wide conc. drive

5.48
1.05 4.62
75' 41'
Bar.

1+00 13⁵ Lt. = 10" diam pole # 2119

2.4 1.5 0.5 0.0 -1.0
4.1 5.0 6.0 6.5 7.5
50 40 20 1 M
7.7 7.9 8.0
20 40 60
M M M

0+58 40' Lt. 2 9' wide Conc. drive

4.41 2.10
2.12 4.43
71 40
Bar.
floor

0+35

1.8 1.4 1.0 -0.5 -1.1 -1.2
4.7 5.1 5.5 7.0 7.6 7.7
40 20 1 20 40
M M M

-0+00

5+79⁶³ = Ely. line Noyes

2.2 1.7 1.5 -0.8 -1.3 -1.5
4.3 4.8 5.0 7.3 7.8 8.0
40 20 5 20 40
M M M

5+61² = 40² Lt. 2 sly end existing
ob. + A.C. pave.

2.94 2.34
3.59 4.21
402 0
00 403
end

6.53

Oliver

2+83 - 3d RT = edge of slough

Notes { M. - denotes Marsh
S - denotes in slough

2+80 4d RT. = edge of Slough.

2+50

2+00

1+75

1+60 - 42" Lt. = 9' wide Conc. Drive

1+50

see new levels page 58

1.2	1.0	0.4	7	-0.9	-1.8	-2.0	-3.5	3.2
5.9	6.1	6.7	8.0	8.9	9.1	10.6	10.6	
50	40	37	M	15	30	32	40	
				M	M	S	S	

1.2	1.0	0.5	7	-0.9	-1.7	-2.1	-3.5	
5.9	6.1	6.7	8.0	8.8	9.2	10.6		
50	40	37	M	15	40	42		
				M	M	S		

1.7	1.3	0.4	-0.6	-1.2	-2.1	-2.2		
5.4	5.8	6.7	7.7	8.3	9.2	9.3		
45	40	36	17	M	20	40		
					M	M		

2.3	2.0	0.9	0.2	-0.9	-1.9	-2.0	-2.2	
4.8	5.1	6.2	6.9	8.0	9.0	9.1	9.3	
40	37	35	20	M	12	40	100	
					M	M	M	

2.7	2.2	1.1	0.5	-0.6	-1.3	-2.0		
4.4	4.9	6.0	6.6	7.7	8.4	9.1		
45	40	37	20		10	40		
					M	M		

6.48	2.51							
0.66	4.63							
74	42							
Gar								

2.2	1.8	1.1	0.3	-0.4	-1.6	-1.6		
4.9	5.3	6.0	6.8	7.5	8.7	8.7		
45	40	38	20		12	40		
					M	M		

7.14

4+02 - 13' Lt. = 10" pole #2171

3+90 - 54' Lt. = Φ 3' wide brick in

fill of street sweepings - sand - etc.
From here on F denotes loose

3+80

3+73 - 38³ Lt. = 12" pole #2160

3+56 50' Lt. = Φ 4' wide Conc. walk

3+30

3+11 45⁶ Lt. = Φ 4' wide Conc. walk

3+00

T.P. 7.16 7.16 7.14 0.00

4.14
3.102 3.56
64 54

2.7 2.6 2.1 - 2.4
4.5 4.6 5.1 9.6 9.8
40 30 10 M 40
F F M M

3.68 2.64
3.48 4.52
60 50

3.8 1.9 1.2 1.2 0.7
3.4 5.3 6.0 6.0 6.5 10.8 10.7 9.7 9.7
70 50 40 25 F S 18 20 40
10' 5'

2.67 1.66
4.49 5.50
55^E 45^E
walk

3.1 0.9 - 0.5 - 0.1 - 0.3 - 3.4 - 3.6 - 2.6
4.1 6.3 7.7 7.3 7.5 10.6 10.8 9.8
60 40 10 F 15 16 40 45
7.16 F S S

Oliver

5+79.45 = Ely Olney st.

-2.3	-2.4	-2.2
9.5	9.6	9.4
40	9	40
S		S

5+70

-1.8	-1.5	-1.6
9.0	8.7	8.8
40	M	40
M		M

5+44 14' RT = deadman

45' RT = deadman

5+13 14' RT = pole # 4178 12" diam

4+99.45 = wly line Olney

-1.9	-1.7	-1.7
9.1	8.9	8.9
40	M	40
M		M

4+50

-2.1	-2.0	-2.0
9.3	9.2	9.2
40	M	40
M		M

9+15

-3.3	-2.7	-2.3	-2.3	-2.1
10.5	9.9	9.5	9.5	9.3
50	40	20	M	40
M	M	M	M	M

9+05

-2.7	-2.7	-2.3	-2.4	-2.1
4.5	4.5	9.5	9.6	9.3
50	40	20	M	40
F	F	M		M

7.16

Oliver St

35

4.45 40.37 ✓

S.E. 7' LTT. Reed + Lamont

T.P.	6.00	44.82	0.40	38.82
T.P.	12.60	39.22	0.36	26.62
T.P.	11.10	26.98	0.11	15.88
T.P.	7.98	15.99	1.20	8.01
T.P.	9.24	9.21	7.19	-0.03

7.16

PACIFIC BEACH DRIVE

5-6-53

Lament to Morrell w.o. 32052

C.H.S.

Begg
Altman
Schelin

Ref. - T.P. sheet 1606

TP Book 20 - page 20

- Lentes Fd. Conc. Mon
- " Fd L+T
- " set Nail

B.L. = 23°^{08'} North of Sly line P.B. Dr.

see T.P. Book 20
p 20

Soil sample from

20' North of Sly line P.B. Dr.

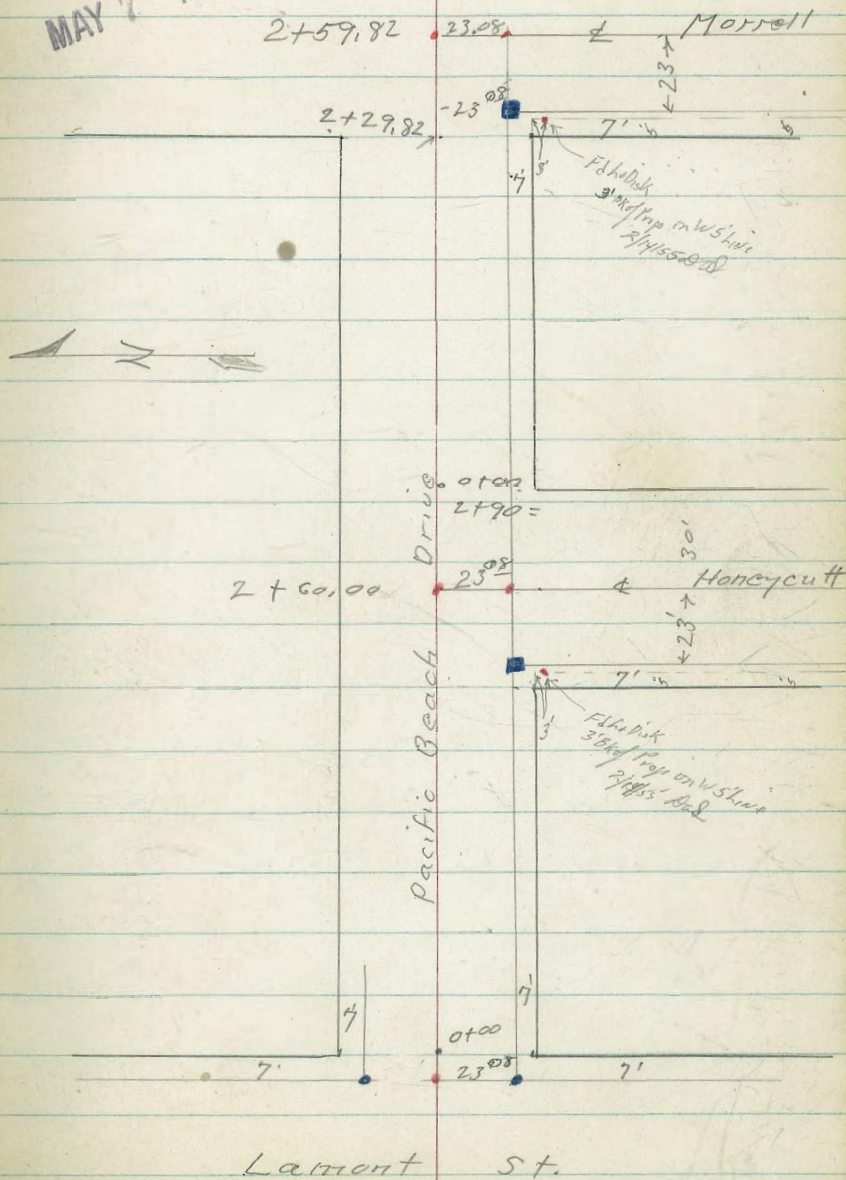
20' west of Wly. line Honeycutt.

INDEXED
JUN 25 1953

INDEXED
MAY 7 1953

B.L.

36



1+09 - 28' Rt. = end picket fence.

1+07 - 30' Lt. = start conc. slab.

1+00

T.P. 4.45 37.13 6.24 32.68

0+76 26' Lt. = 3' conc. walk

0+60

0+59 - 16' Rt. = 1 1/2" pole # 1913

0+53 30' Rt. = 4' diam pepper tree

30' Lt. = end chain link fence.

0+50 15' Rt. = start picket fence

0+30

0+13 30' Lt. = start picket fence.

34.23

2.90
30 2
slab

34.1

3.0
30

32.9

4.2
11

32.7

4.4

32.1

5.0
15

32.1

5.0
30

37.13

34.56

34.33

34.32

4.36

4.59

4.60

36

30

26'

on walk

33.9

5.0
30

33.6

5.3
20

33.0

5.9
13

32.7

6.2

32.4

6.5
13

32.9

6.0
15

32.6

6.3
30

34.5

34.3

33.9

33.2

33.0

4.4
40

4.6
30

5.0
18

5.7
12

5.9

33.0

5.9
15

32.4

6.5
30

32.3

6.6
40

38.92

T.P. 3,26 36.03 4,36 32.77

2+00

1+87 17' Lt. } = 6" diam tree
22' Rt }

1+82 - 17' Rt = 12" pole #19A

1+74 - { 30' Lt = start picket fence.

29' Rt = end picket fence

1+73 30' Rt = end picket fence.

1+65 - 15' Lt = 10" acacia

1+50

1+43 - 16' Lt = 5" Acacia

{ 31' Rt = 9 wide porch

1+32 - { 23' Rt = 3' Conc walk

1+26 22' Rt = (W)

{ 32' Lt = 3' Eucalyptus

16' Lt = 6" Eucalyptus

1+24 { 27' Rt = start picket fence

1+21 30' Lt = end slab.

34.2	34.1	33.4	32.9	32.5	32.2
2.9	3.0	3.7	4.2	4.6	4.9
30	15	13		14	30

34.1	33.9	33.2	32.8	32.4	32.1
3.0	3.2	3.9	4.3	4.7	5.0
30	13	11		15	30

32.23	32.22	32.22	32.2
4.90	4.91	4.91	4.9
23	30	31	32
walk	↑	porch	floor

34.57	34.31
2.56	2.82
40	30 ^e
slab.	

37.13

0+60 30' Lt. = start 4' high conc. wall

31.4
4.6
30
Ord

0+50

31.8
4.2
30
30.8
5.2
30.3
5.7
12
5.4
30
30.6

0+46 - 21' Lt. = (W)

33.35

32.23

32.2

31.5

31.0

0+20 31' Lt. = 8' conc. drive.

2.68
60
@ av.
Floor

3.80
31
drive

3.8
30

4.5

5.0
30

0+00 }
2+90 } = Ely Honeycutt

32.6
3.4
30

32.8
3.2
14

31.9
4.1
12

31.7
4.3

31.2
4.8
30

2+60 - 1' Rt. = sewer M.H.

33.5
2.5
40

33.3
2.7
30

32.1
3.9

32.2
3.8
Rim

11.7
24.3
1
I.E

31.6
4.4
30

2+37 - 30³' Lt. = end picket fence.

33.8
2.2
30

33.5
2.5
15

33.0
3.0
13

32.7
3.3

32.0
4.0
15

32.2
3.8
30

2+30 = wly. Honeycutt

2+05 - 23' Rt. = 1' diam tree

36.03

P. B. Dr.

B. L.

41

TIP. 2.61 29.36 9.28 26.75

1+69 25' RT. = end drive

1+56 25' RT. = start conc. drive

1+48 22' RT. = (W)

1+35 21' LT. = (W)

1+30- 18' RT. = lead man

1+20 30' Lt. ± 3' conc. walk

1+10- 30' Lt. = end 4' conc. wall

1+06 17' RT. = 10" pole # 1973

1+02- 21' RT. = (W)

1+00

0+98 30' Lt. = ± 3' walk thru wall.

33' RT. = ± door way to house

0+75- 25' RT. = ± 3' conc. walk

27.6	27.5	27.3	27.3	27.43	27.51
8.4	8.5	8.7	8.7	8.60	8.52
30	15	15	15	25 drive	30
				27.57	27.66
				27.46	27.37
				25 drive	30
					41- car floor

28.92	29.18	28.9	28.7	28.9	29.2	29.0
7.11	6.85	7.1	7.3	7.1	6.8	7.0
35	30	13		12	13	30
	walk					
29.9	6.1					
	30'					

30.5	30.4	29.6	29.4	29.4	29.5
5.5	5.6	6.4	6.6	6.6	6.5
40	30	20		12	30
30.38		30.33			
5.65	5.70				
40	30				
walk	walk				

30.45	30.47	30.9
5.58	5.56	5.1
25	30	33
		Floor

36.03

Roberts Survey For Street Lights & Walks
 Cota
 Moore
 Morales
 10-28-53
 W.O.#32144

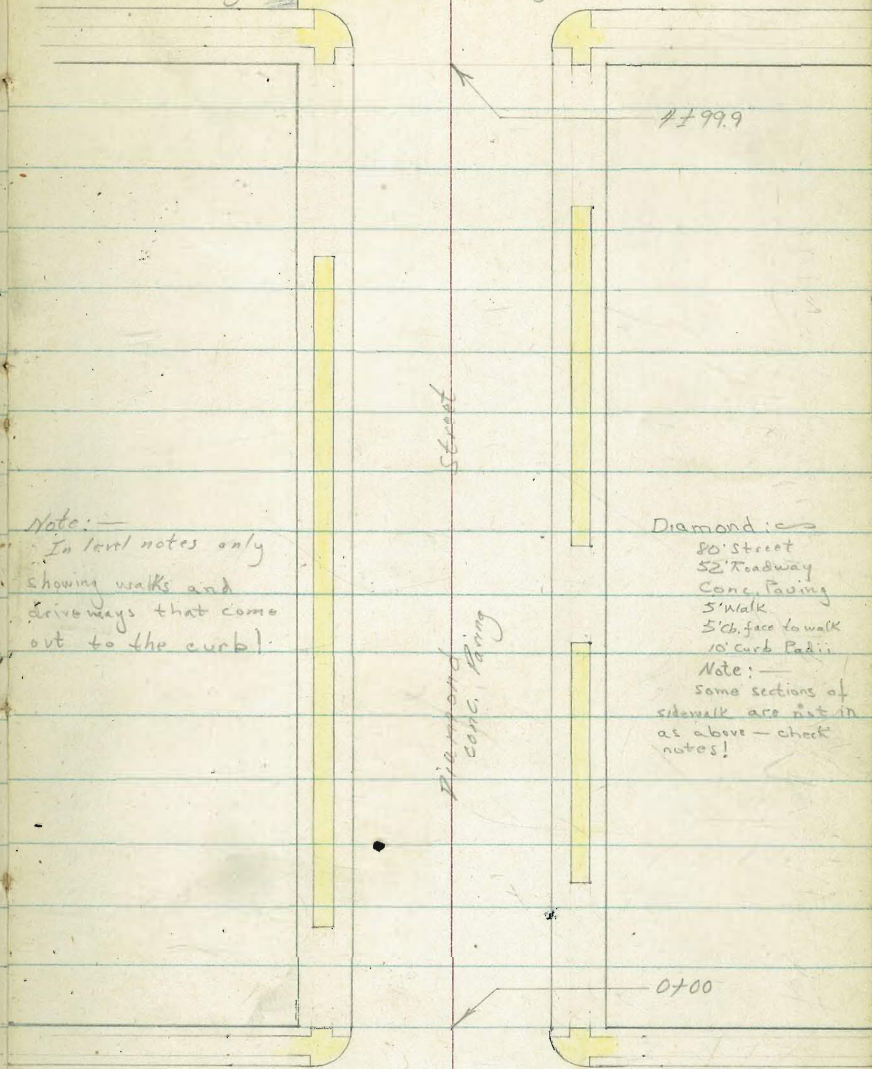
Diamond Street
 Mission Blvd to Cass

INDEXED
 JER
 OCT 29 1953

Bayard
 AC Paving

conc. Paving

street 43



Note: —
 In text notes only
 showing walks and
 driveways that come
 out to the curb!

Diamond is

80' Street
 52' Roadway
 Conc. Paving
 5' walk
 5' ch. face to walk
 10' curb Rad.:

Note: —
 Some sections of
 sidewalk are not in
 at above - check
 notes!

Mission
 Conc. Paving

Boulevard

Cass

Street

AC Paving

5000

Street

Diamond
conc. Paving

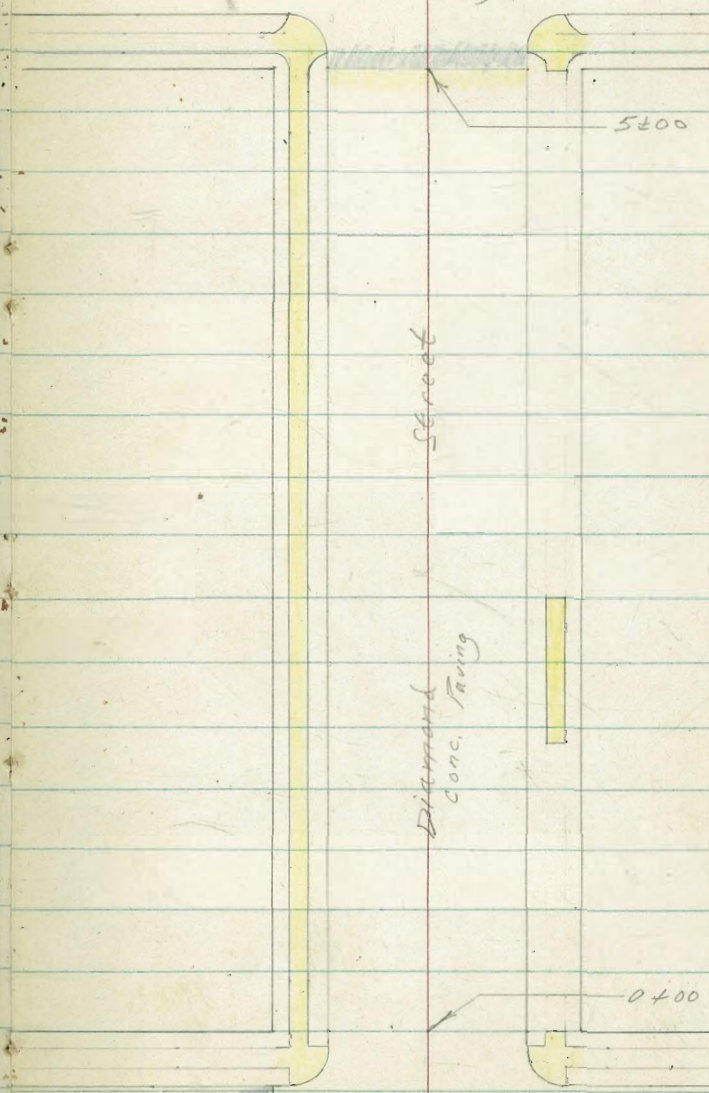
0400

Bayard

street

AC Paving

conc. Paving



1791.2 ✓ Q 3rd conc. walk on Left

1753.4 ✓ Q 2nd conc. walk on Left

1733.5 ✓ Q 2nd conc. walk on Left.

1726.6 ✓ Q 3rd conc. walk on right

1707.5 ✓ Q 10' ^{conc.} Drive on Right

0775 ✓ Begin walk on Right

31.73 31.84 31.90 32.0
26 30.4 35.4 40
cb walk

0752.9 ✓ Begin walk on Left

33.4 32.95 32.80 32.53
40 35.4 30.4 26
walk cb

0730

33.1 32.25
40 26
cb

31.27 31.4
26 40
cb

0700 { End of walk on Rt. and Lt.
Ely Line Mission Blvd.

32.7 32.29 32.23 32.01
40 36 31 26
walk cb

31.07 31.16 31.20 31.2
26 31 36 40
cb walk

BM

SWBP
30.92 Diamond & Mission

3+99.6 ✓ End walk on Left

36.8	36.60	36.50	36.38
40	<u>35.5</u>	<u>36.5</u>	26
	walk		cb

3+79.8 ✓ 10° conc. Drive on right

3+08.1 ✓ 14° conc. Drive on left

2+94.8 ✓ 10° conc. Drive on right

2+84.3 ✓ 3° conc. walk on left

2+53.7 ✓ 2° conc. walk on left

2+51.7 ✓ 3° conc. walk on right

2+50.2 ✓ Begin walk on Right

33.50	33.56	33.65	33.6
26	<u>30.5</u>	<u>35.5</u>	40
cb	walk		

2+27.1 ✓ 2° conc. walk on left

1+99.8 ✓ End of walk on Right

32.97	33.11	33.15	33.2
26	<u>30.5</u>	<u>35.5</u>	40
cb	walk		

1425 ✓ E 3° conc walk on left.

1407.4 ✓ E 13° conc Drive on left

0+75

37.34
26
cb

38.0
40

0+40.2 ✓ E of Garage on Rt, Drive not in, nor is
the curb broken for drive opening

0+00. { End of walk on Right
Ely line of Bayard

36.46 36.55 36.57 37.4 37.4
26 31 36 36 40
cb walk

4+99.9 { Begin walks both sides,
Wly line Bayard

37.7 37.54 37.47 37.47
40 36 31 26
cb walk

35.98 36.02 36.05 36.2
26 31 36 40
cb walk

4+50

37.7 36.89
40 26
cb

35.44 35.7
26 40
cb

4+24.3 ✓ End walk on Right

35.17 35.25 35.31 35.4
26 30 33 40
cb walk

4+23.3 ✓ E 2° conc walk on Right

3748.5 ✓ Q 2^o Conc walk on Right

3742.7 ✓ Q 12^E conc walk on Left

3706.5 ✓ Q 12^o conc walk on Left

3705.2 ✓ Q 11^o Conc Drive on Right

3700

40.35
26
cb

40.3
40

2791.2 ✓ Q 13^o Conc Drive on Left

2725 ✓ End of walk on Right

3933
26
cb

3946 3955
31 36
walk

39.4
40

1787.3 ✓ Q 3^o Conc walk on Right

1760.3 ✓ Q 14^o Conc Drive on Left

1750 ✓ Begin walk on Right

3834
26
cb

3843 3855
31 36
walk

38.7
40

Cont'd From Page 48

5700 } Begin walk on Right
wly Line Call

4470.2 ♀ 11° brick walk on Left

4459 ♀ 3° conc walk on Right

4432.8 ♀ 10° conc Drive on Right

4430.3 ♀ 24° Conc Drive on Left

4417.8 ♀ 10° conc drive on Right

4400

3490.9 ♀ 3° conc walk on Right

3451.2 ♀ 2° Conc walk on Right

L+

♀

R+ 49

42.99 43.04 43.09 43.1
26 31 36 40
cb walk

41.73 42.1
26 40
cb

Roberts
Moore
Marble
12-30-53
W.O. Wood

X-Section Block 308 Pacific Beach
Between Oliver & Pac. Bch. Dr.
From Marcell to Naves
(For Yards to be Dropped by Griffith Co.)

INDEXED
HER
DEC 31 1953

350

1435

See page 53
for No. Cross Sec.

4.7	5.6	10.1	11.0	10.3	7.9	5.2	5.0	2.1
125	100	44		8	40	70	94	125

1420

4.9	6.1	9.6	10.5	9.1	2.1	1.9	1.3	1.1
125	100	56	15		15	50	100	125

1400

5.4	7.3	9.0	9.9	8.7	6.6	1.2	
125	100	71	29	6		15	

Improved (Graded, you can see)

T.P.

1.6 17.67 A 9.25 16.06

17.67 A

0450

(Dwelling in SW part of block)
0450 to 1425

12.8	13.7	14.5	11.7	9.1	7.9	7.5	6.2	5.6
125	100	64	31		10	50	100	125

0400

East Line Marcell Street

11.2	11.3	8.9	8.7	6.8	5.7	4.4	3.5
125	100	68	50		50	100	125

BM

0.97 24.31 A

29.34 S.F. 7

Marcell & Pac. Bch. Dr.

24.31 A

4400

T.P.

2.61

8.20A

12.08

5.59

3450

3400

2460

2415

1483

17.67A

$$\begin{array}{r} 17.67 \\ 10.2 \\ \hline 7.5 \end{array}$$

7.6	18.4	4.4	4.6	5.4	3.3	5.1
0.6	1.8	3.4	4.6	5.4	3.3	3.1
125	100	50	50	50	100	125

8.20A

6.5	1.5	6.1	5.4	4.9	5.1	4.4
9.2	10.2	11.6	12.3	12.7	11.9	12.0
125	100	50	25	66	100	125

9.6	8.9	1.2	1.7	1.7	1.3	1.9
8.1	8.9	10.5	10.0	10.0	10.4	13.9
125	100	67	35	65	100	125

10.0	9.4	9.0	8.9	7.4	11.0	11.1
7.7	8.3	8.7	8.8	10.2	13.7	15.6
125	100	50	35	70	105	125

11.2	10.7	9.4	9.2	1.9	6.4	4.3
6.5	7.0	8.1	8.5	9.8	11.3	13.4
125	100	50	30	15	42	85

12.0	11.3	9.2	6.1	5.9	5.0	5.3
5.7	6.4	8.5	11.6	11.9	12.7	12.4
125	100	50	15	30	58	80

17.67A

check

3.25 23.34 = 23.34

T.P. 7.75 26.59 0.36 18.84

T.P. 11.53 19.20 0.53 7.67

5700 WEST LINE NOYES

2.9	2	0	1.6			
5.3	6.0	7.2	9.8	10.1	10.5	9.6
125	100	50		50	100	125

4750

5.7	4.6	3.2	1	0.2	0.3	1.9
2.5	3.6	5.0	7.1	8.0	7.9	6.3
125	100	50		50	100	125

8.20 ↑

11.8
8.20 ↑

Recross section of

Beqq
Schelin
pulleq

BIK 308-P. B.

1-29-54

See page 50

INDEXED
HER
FEB 3 1954

1/2

1+83

12.8 12.6 13.0 13.0 9.1 5.9 5.7
12.5 50 10 6 8 10

1+35

14.0 14.2 14.5 14.6
12.0 12.3 13.0 12.9 12.0 8.4 8.7
12.5 50 10 4 7 10

1+20

14.1 14.7 15.4 15.0 13.0 10.8 12.6
12.5 50 10 3 4 10

1+00

14.7 15.5 16.1 15.9 14.0 12.0 14.0
12.5 50 10 3 3 10

0+50

15.4 16.7 17.4 17.2 15.5 16.3
12.5 50 10 4 10

0+00 E line Morrell St

15.8 7.6 8.4 18.3 17.8 19.0
12.5 50 10 3 10

23.53

P.B Drive a Morrell

Note
Rods on pages 50-51 & 52
south of south line of
alley are unchanged
C.H.S. 1-29-54

5+00 W. Line Noyes

3.8	0.7	-1.0	-1.0	-1.2	-1.6
3.8	11.7	9.0	9.0	8.8	8.4
125	50	25	10		10

4+50

6.2	3.7	2.2	2.3	1.5
125	50	10		10

4+00

8.0	5.3	4.0	4.3	3.4	3.2
125	50	10	4		10

3+50

9.1	6.8	5.7	5.8	5.4	5.5
125	50	10	3		10

3+10

10.3	8.2	8.2	8.3	7.8	7.8
125	50	10	2		10

2+60

11.0	9.8	10.0	9.8	8.9	8.7
	50	10	3		10

2+15

12.2	11.4	11.6	11.7	8.6	7.4	6.8
125	50	10	5		2	10

5+40 $\frac{1}{2}$ Nojes

+1.2	-1.3	-1.4	-1.6	-1.7	-1.7
125	50	50	10	50	

Oliver

Cross Section from Morrell to
Noyes for change in yardage

1-29-54

C.H.S.

W.O.# 32052

Begg

Schelin

sketch P-17

Pullen

Note { Elevations north of \pm
are unchanged.
See page 26 for Elev.

Notes reduced
2-3-54
D. Cannon

1+00

14.9	14.7	13.8	14.6	14.7
4.6	4.8	5.7	4.9	4.8
	15	20	25	40

0+50

14.5	14.3	15.3	15.6
5.0	5.2	4.2	3.9
	15	22	40

0+00 = Ely line Morrell

14.8	14.7	15.9
4.7	4.8	3.6
	20	40

19.49

B.M.#1

3.62

19.49

15.87

T.P. - Nail in pole # 2015 (page 26)

Olivet

±

T.P. 0.35 9.76 10.08 9.81

4+00

8.6	8.3	9.3	8.7	8.0
10.9	11.2	10.2	10.8	11.5
	12	13	20	40

3+50

9.8	9.4	9.1	9.4	9.0
9.7	10.1	9.4	10.1	10.5
	12	13	20	40

3+00

11.1	10.7	10.9	10.1	10.2
8.4	8.8	8.6	9.4	9.3
	11	15	20	40

2+50

12.1	11.4	12.4	11.2	11.3
7.4	8.1	7.1	8.3	8.2
	12	14	17	40

2+00

13.3	13.3	12.6	12.6	12.8
6.2	6.2	6.9	6.9	6.7
	8	15	30	40

1+50

14.4	14.1	13.6	13.5	
5.1	5.4	5.9	6.0	
	15	25	40	

19.49

oliver

2+75

1.0	0.4	-0.9	-1.2	-1.0
4.0	4.6	5.9	6.2	6.0
40	36		20	40

2+50

1.5	1.2	0.3	-1.0	-1.1	-1.0
3.5	3.8	4.7	6.0	6.1	6.0
40	35	34		20	40

2+00

see page 61 for ditch on south.

set stub on $\frac{1}{2}$ (P-17)

2.4	2.0	0.9	-0.8	-2.2	-2.0
2.6	3.0	4.1	5.8	7.2	7.0
40	37	34		20	40

0+00 to 2+00 unchanged (page 31)

T.P. 5.73 4.97 5.43 - 0.76

0+00 = Ely line Noyes (sketch P-17)

1.04 4.67 — 3.63

4.97chisel \square Nly. and N.W. Ret. Noyes + OliverB.M. chisel \square
page 27

6.15 3.61 (3.63)

4+99 ⁶³ = Wly line Noyes

3.5	3.3	4.0	3.7
6.3	6.5	5.8	6.1
	13	14	40

4+50

6.4	6.1	7.1	6.1
3.4	3.7	2.7	3.7
	15	16	40

9.76

Oliver

3+90 83' Ltr = sly, face house

3+65

3+56 83' Ltr = sly face house

3+20

3+11- 83' Ltr = sly face house

3+11

T.P. 6.62 8.09 3.50 1.47

3+00

2+85

4.91

3.18

83
Floor Elev.

2.3

5.8
40

1.8

6.3
20

1.8

6.3

2.1

6.0
25

2.5

10.6
34

2.8

10.9
40

5.29

2.80

83
Floor Elev.

1.0

7.1
40

0.5

7.6
32

0.4

7.7

0.5

7.6
30

2.6

10.7
38

2.6

10.7
40

4.26

3.83

83
Floor level

8.09

0.8

4.2
40

0.0

5.0
20

0.4

5.4

1.0

6.0
30

3.1

8.1
36

3.1

8.1
40

0.6

4.4
40

0.9

5.9

1.0

6.0
35

3.3

8.3
40

4.97

Oliver

4

60

4+99⁴⁵ = wly Olney

-2.0	-1.9	-1.9	-1.9	-1.9
10.1	10.0	10.0	10.0	10.0
40	20		20	40

4+87

3.7	3.9	4.1	4.1	-1.9	-2.3
4.4	4.2	4.0	4.0	10.0	10.4
40	20		10	15	40

4+50

3.3	3.1	3.0	3.0	-2.0	-2.2
4.8	5.0	5.1	5.1	10.1	10.3
40	20		20	25	40

4+00

2.8	2.6	2.7	2.8	-2.4	-2.3
5.3	5.5	5.4	5.3	10.5	10.4
40	20		20	25	40

8.09

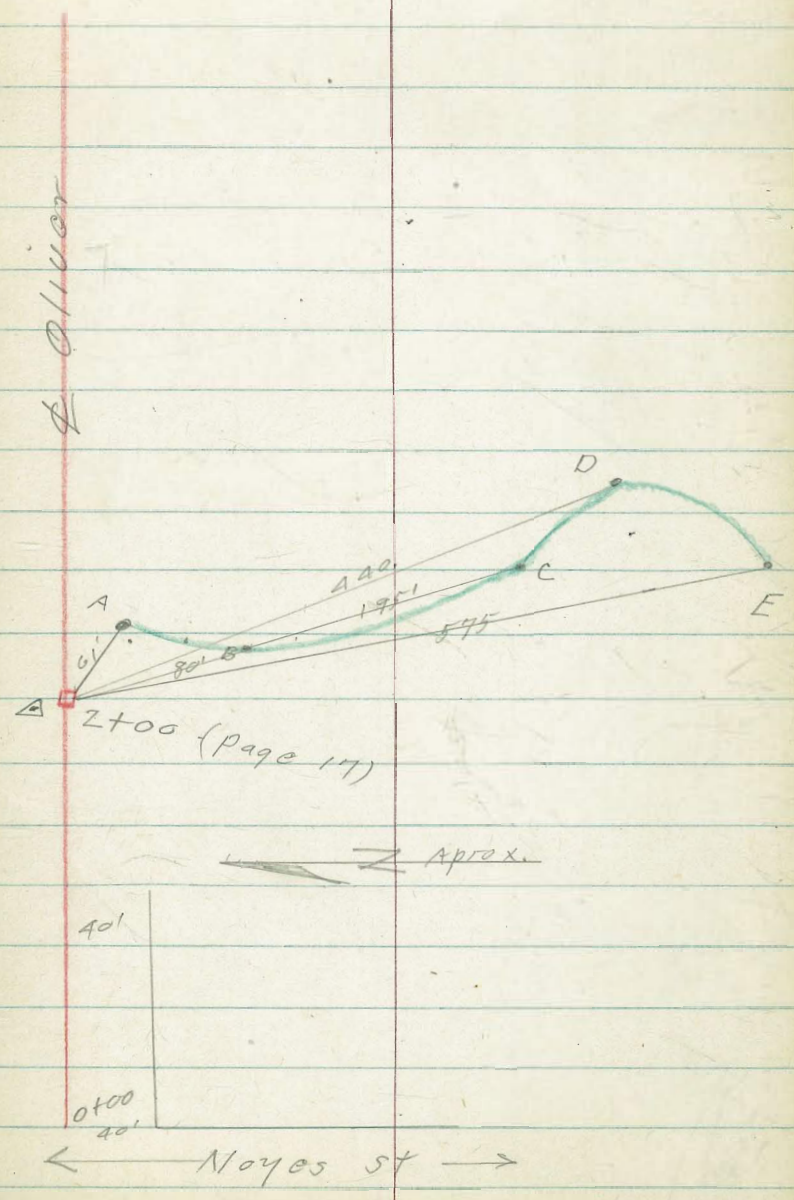
Line of ditch south
of Oliver Between Noyes
+ Olney.
2-1-54

← Olney St. →

Δ = 1/2 - sta. 2+00 page 17.
All angles turned off tang. to
East, which is ⊥ Oliver.
Green line = ± 15' ± 20" wide ditch

E	∠ 79° Rt.	575.00'
D	∠ 69° - 40' Rt.	440.00'
C	∠ 74° - 40' Rt.	275.00'
B	∠ 74° - 40' Rt.	80.00'
To point A	∠ 36° Rt.	Dist = 61.00'

Δ = 2+00 - Page 17.



Additional Notes Alley BIK 282

Also slq. 1/2 BIK 282 - Pac. Beach

C.H.S. 2-2-54
 Begg w.d. 32052
 Pullen
 Schelin

For sketch see $\frac{FB 1726}{40}$

stationing same as $\frac{FB 1726}{40}$

Note

see Loose Leaf C.A.
 7/1/57.

3+15

26.2	25.8	26.5	27.3	27.1	26.1	27.9
8.2	8.6	7.9	7.1	7.3	8.3	6.5
50	20	10		10	15	50

3+00

31.4	31.1	31.1
3.0	3.3	3.3
10		10

2+97 10' Lt. = end same

32.41	31.40
2.03	3.04
1A	10'
Car floor	apron

2+54 10' Lt. = start conc. apron
 to A car Cor.

32.48	32.36
1.96	2.08
1A	10'
Car floor	apron

T.P. 1.29 34.44 7.45 33.15

34.44

0.23 40.60 — 40.37

S.E. 7' L+T. Lamont & Reed

Continued on page 66

location of points A to D.
see page 63 for details of

A+42 { (see page 65)

A+23 21' Pt. = $\frac{1}{2}$ Sing. Barr
conc. floor. - no apron

20.0			
8.7			
D End			
21.7	20.2	22.41	19.4
7.0	8.5	6.33	9.3
C End. West of wall	C End. East south of wall	C Top of wall	C Base of wall
21.1	21.9	22.41	19.8
7.7	6.8	6.33	8.9
B North of wall End.	B. End west of wall	B Top of wall	B. Base of wall
23.0	23.19	20.5	21.1
5.7	5.55	8.2	7.6
A End to North + west	A Top of wall	A Base of wall	A End to East South east.

21
End. Floor

28.74

Alley BIK 282 P.B.

$4+994 \left\{ \begin{array}{l} 88' RT = N.E. Cor. \left\{ \begin{array}{l} 26' N+S \\ 49' E+W \end{array} \right\} \text{House} \\ 49' RT = N.E. Cor. \left\{ \begin{array}{l} 24' N+S \\ 32' E+W \end{array} \right\} \end{array} \right.$

T.P. 4.84 28.79 4.52 23.95

$4+72 \left\{ \begin{array}{l} 12' RT = N.W. Cor. \left\{ \begin{array}{l} 29' N+S \\ 27' E+W \end{array} \right\} \text{House} \end{array} \right.$

$4+69 \left\{ \begin{array}{l} 48' RT = N.W. Cor. \left\{ \begin{array}{l} 23' N+S \\ 32' E+W \end{array} \right\} \text{House} \end{array} \right.$

conc. drive to Morrell st.
Sing. Car. east front.

$4+65 \left\{ \begin{array}{l} 75' RT = \text{doorway of} \end{array} \right.$

T.P. 4.56 28.47 4.83 23.91

conc. floor

$4+50 \left\{ \begin{array}{l} 16' RT = \text{Sing. Car.} \end{array} \right.$

24.0	22.9	23.0	23.9	24.2	24.25
4.7	5.8	5.7	4.8	4.51	4.49
10	9.9		10	16	16 ²
Ord.	Base of wall				Floor
	Footing				
			<u>28.74</u>		

28.79

$\begin{array}{r} 20.6 \\ 8.2 \\ \hline 88 \\ \text{Floor Elev} \end{array}$

21.2	21.7	20.0
7.6	7.1	8.8
49	49	88
Ord	Floor Elev	Ord

$\begin{array}{r} 23.8 \\ 4.7 \\ \hline 12.8 \\ \text{Ord.} \end{array}$

4.10	24.37
12 ⁸	12 ⁸
	Floor level

$\begin{array}{r} 21.2 \\ 7.3 \\ \hline 48 \\ \text{Ord} \end{array}$

6.85	21.62
48 ⁵	
	Floor level

$\begin{array}{r} 21.37 \\ 7.10 \\ \hline 75 \\ \text{Floor} \end{array}$

28.47

INDEXED
SER
MAR 8 1954

Alley BIK 282 P.B
Ser #62 also KB 1726 p.40
Lt & House

0+40

0+31 E 10' Lt & 2⁵ cov walk end 6" wall

0+11 10' Lt Bk in grade cov wall 6"

0+02 5³ Lt & 12' gas valve

0+00 10' Lt Begn 3'icket fence
10' Lt Begn 6" cov wall

0+00 Fly Lamont ST end cb & AC par.

0-17 C6 EC. alley Returns

0-20 Fly C6 Live Lamont

BM 5⁹² 46²⁹

40³⁷ SF 7' at.
Needs lamont

Lt = Nly ♀ RT = Sly 68

6⁴ 39.82
2/63
Floor

40.2
39.9
39.8
40.2
40.6
6¹ 6⁴ 6⁵ 6¹ 5²
20 10 10 10 15

40.47
5⁸²
3/5

41.29 41.25 40.79 40.8 40.5 40.7 40.8
5⁰ 5⁰² 5⁸² 5⁶ 5⁸ 5⁶ 5¹⁴
20 10² 10² 10 10 10 20
top Footing

40.85
5⁴⁴
5²
1/11

40.59 41.29 41.85 40.74 40.96 41.05
5²⁰ 5⁰⁰ 5¹⁴ 5⁵⁵ 5³³ 5²¹
10² 10² 10² 10 10
Footing cb gut gut end

41.10 40.79 40.65 40.53 40.95
5¹⁹ 5⁸⁰ 5⁴⁴ 5⁶⁶ 5³⁴
10 10 10 10 10
gut gut gut end

40.89
40.42

41.15 40.71 41.07 40.72 40.89 40.54 40.44 40.97 40.82 40.93 40.65
5⁴² 5⁸⁷ 5¹⁴ 5⁵⁸ 5²² 5⁵⁷ 5⁴⁰ 5⁷⁵ 5⁸⁰ 5⁸² 5³⁷ 5⁸⁶ 5⁶⁴
65 65 35 35 13 13 10 10 13 13 63 63
gut cb gut cb gut gut gut gut gut cb

T 46²⁹

TP 3⁴⁰ 38⁷⁷ 10²² 35³⁷

2+00

1+50

1+42 20⁵ Lt E single garage con floor

1+31 10⁰ Lt end con paved area

1+29 12⁷ Rt E single garage con floor + apron

1+25

1+00 10⁵ Lt Begin con paved area

1+00 9³ Rt E 8" PP6/6 #A 1924

0+92 13² Rt E single garage con floor + apron

0+85 10⁰ Rt end 3' Picket Fence

0+80

Lt-Nly

Rt-Sly

69

34.6 35.2 35.3 35.1 35.8 36.0
11⁷ 11¹ 11⁰ 11² 10⁵ 10³
20 10 4 10 20

36.7 36.8 37.1 37.2 37.7
10⁶ 10⁵ 10² 10² 10⁶
10 10 10 10

36.54
9.35
20.5
Floor

37.79
8.50
10²
con

38.03 37.8 38.4 38.5 38.9 38.98 39.24
8²⁶ 8⁵ 7⁹ 7⁸ 7⁴ 6⁸ 6⁴
10¹ 10 6 10 20 20
con con con con con con con
12² 12² 12² 12² 12² 12²
apron apron apron apron apron apron
34.5 34.5
Floor Floor

37.54 38.56 38.9 39.3 39.3 39.9 40.2
7⁶⁵ 7³³ 7⁴ 7⁰ 7⁰ 6⁴ 6¹
20¹ 10² 10 7 10 20
con con con con con con con

20.05
6.24
13.2
apron
5.69
18.2
Floor

39.0 39.3 39.4 39.7 39.9
7³ 7⁰ 6⁸ 6⁶ 6⁴
20 10 10 10 20

T 4/6 29

Lt=Nly

Q

Rt=Sly

70

BM starting

5-25

410³⁶TP₂

707

46³¹

613

3864

3400

31.5

31.3

30.9

31.0

31.8

32.2

7³7⁵7²7⁸7⁴6⁶

15

10

10

12

20

32.42

31.38

6³⁵7³⁹

144

102

Floor

apron

32.41

31.93

31.9

32.0

32.3

32.19

6³⁶6⁵⁴6²6⁸6⁵5²

144

103

10

10

20

Floor

garage

2475

2467 62° Rt E double garage con Floor & apron

2454 10° Lt Begin 4 car garage con Floor & apron

2451 9° Rt E 12" P/Bk A1960

2450

32.47

32.34

6³⁰6⁴³

144

103

Floor

apron

43³⁸

34.38

6²6⁴³

apron

Floor

43³⁵

34.42

31.7

32.7

32.9

33.1

33.4

34.0

34.7

7¹6¹5⁹5⁷5⁴4⁸4¹

20

10

9

5

10

20

33.2

34.1

34.9

34.3

34.5

35.3

35.9

5⁶4²4⁴4⁵4³3⁵2⁹

20

10

9

5

10

20

2425

3877

PARADISE HILLS

SURVEY SEWAGE PUMP STATION SITE

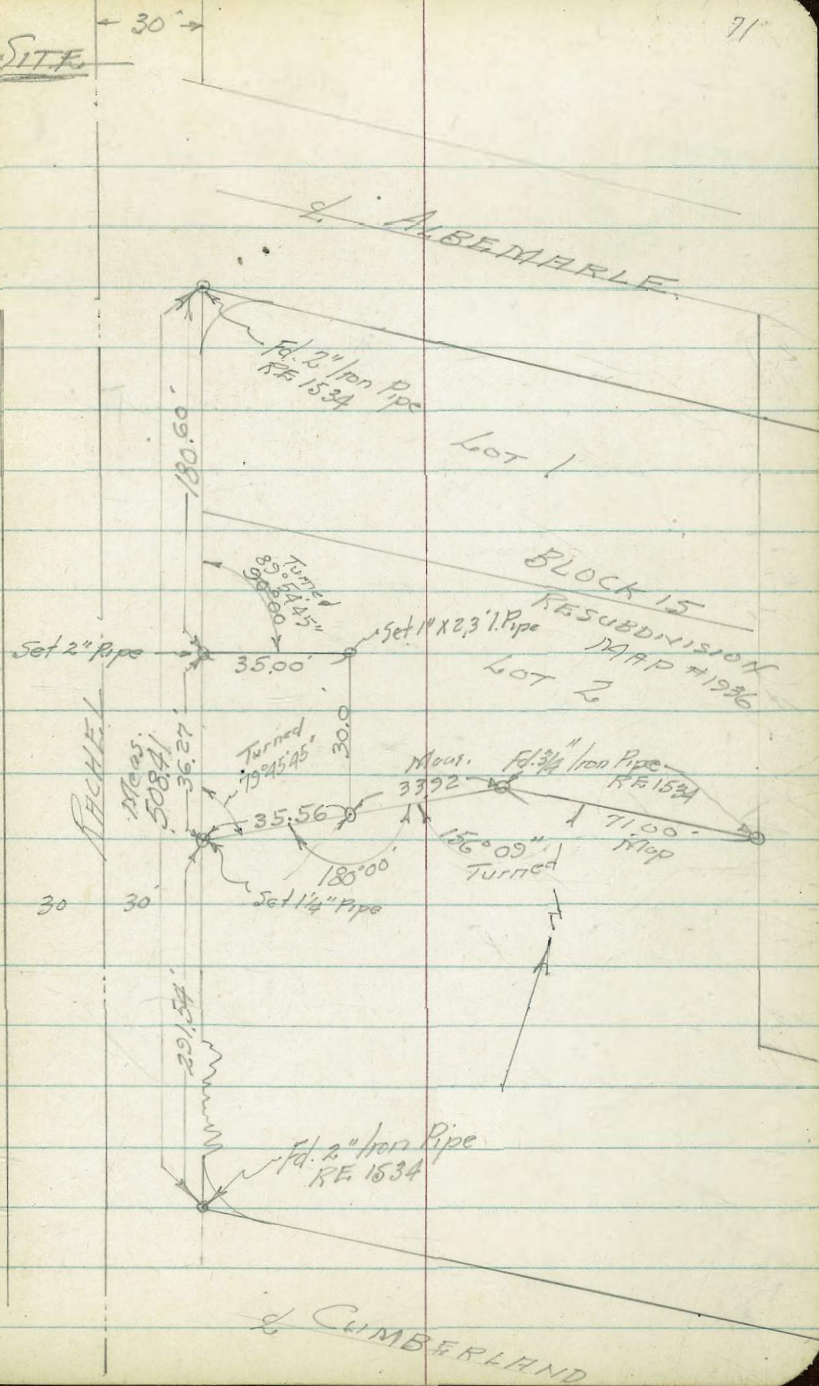
SITE

Walker
 Pope
 Dittman
 Blom
 8-25-54

IN LOT 2 of RESUBDIVISION
 Lots 1-12 Inc. PLAN 4094-B
 NO 20738

INDEXED
 HER
 AUG 31 1954

All pipes set with Cement
 And Copper Disc.



The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. A vertical red margin line is drawn on each page, creating a narrow left margin. The pages are otherwise blank, with no text or drawings. The number '76' is handwritten in the top right corner of the right page. The notebook is bound in the center, and the dark cover is visible at the edges.

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page is divided into three vertical columns by two red lines. The leftmost column is the widest, followed by a narrower middle column, and a narrow rightmost column. The pages are otherwise blank, with a few small dark spots and faint smudges. The notebook's dark cover is visible at the edges.

N. 441 362.89

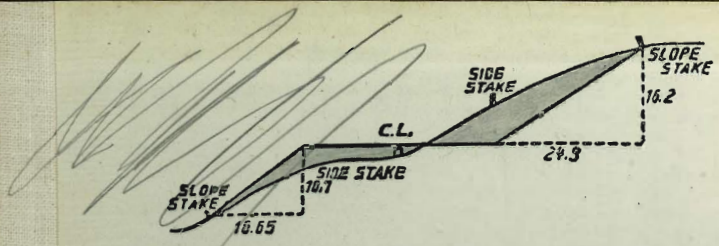
Mass 4407 SEBP

19.8
17.8

20.24
1128
900

26.53
406
22.47

614
610
44



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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