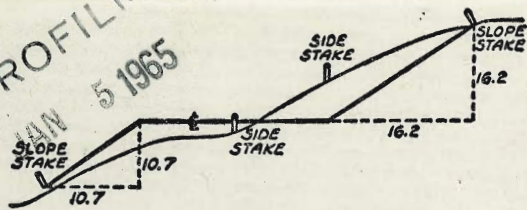


MICROFILMED
5 1965



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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54	X- Sec Franklin Ave - Evans to 28th
60	X- Sec Alley Bk 113, Pacific Beach See also FB 1810-13
66-	Re- x- sec Alley Bk 6, Ocean Beach

x-Sect. Franklin Ave.
from Dewey to Evans

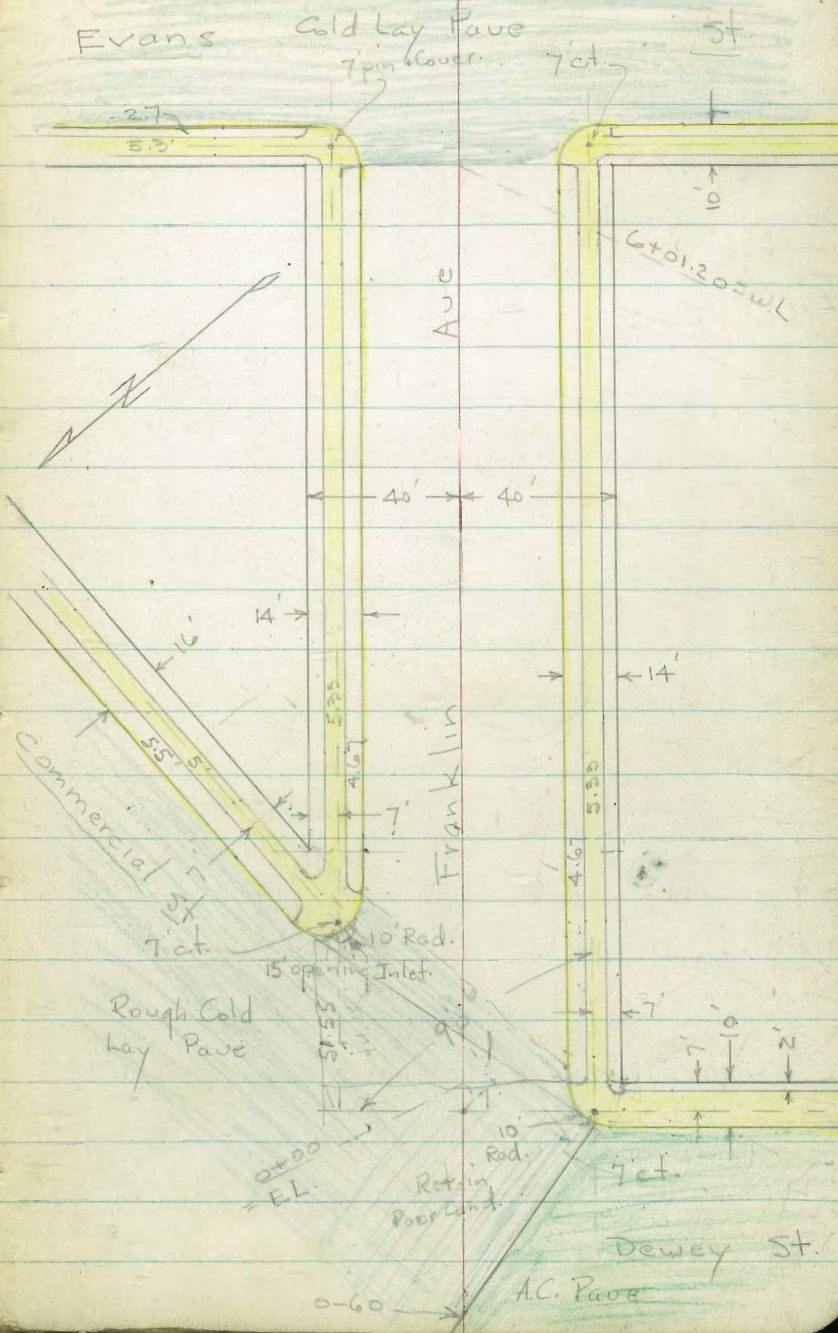
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1-7-53

7.0.

w.o. 32195

INDEXED
Leads
JAN 7 1953



X-Sect. Franklin Ave - See Sketch P. 1

15' opening "G" Inlet.

0+40.7 = opp. Most. Wly. of 10' Rad. Ret. on Lt. 59.5
50

59.95 58.93 55.74 58.97 59.9 60.3 60.4 60.1 60.96
TOP 34.1 I.E. of 30.5 15 15 26.1 60.96
cb. edge of Box edge of
of grate grate
got. Top

0+25 = 59.9 59.3 60.0 59.8 60.60
50 26 got. Top

0+00 = 90° to Prop. Cor. on Rt.

60.16 59.8 59.6 59.7 59.7 59.3 59.92
47.2 35 15 15 26.2 Top
S. Rail got.

0-10 = E. cb. of Dewey.

60.1 60.10 59.6 59.5 59.14 59.88 60.53 61.43
50 39 15 33.4 Top 60
S. Rail edge of cb got Top
ht.

0-30
Rough oil pave on Commercial

60.54 59.9 59.9 59.97 59.5 59.29 59.07 59.67
Top 71.6 45 22.1 20.3 31 50
got. S. Rail edge of got.

0-60 = ϕ and edge of A.C. pave

60.17 59.4 59.7 59.69 59.70 59.20 58.84 59.39
Top 46.3 25 2.7 30 50 70
got. S. Rail ϕ got.

Very Muddy - if more data needed will get later.

0-90.5 = edge of A.C. pave at N. cb. of Commercial

59.93 59.08 59.4 59.39 58.94 57.96 58.90
Top 21 27.1 50 72.6 Top
got. S. Rail on SE
can of grate cb

+ 26th
0-96 = opp. P.C. of N.E. Ret. Commercial

59.90 58.87 59.40 59.31 59.04 57.98 58.86
Top 16.6 32.2 50 72.4 Top
cb. got. - end of opening of Inlet S. Rail got. = edge of inlet

+ Franklin
Top of F.H. - S.F. Dewey 62.19

B.M. = N.W. B.P. - 26th + Imperial 63.92

Actual Elev. Shown.

133 Lt. ♀ Rt. 3
117

4+00 = Brk. in curbs.

67.99 67.2 67.7 68.4 68.7 68.8 69.99
Top 26.1 15 15 26.1 26.1 26.1
gut. gut. Top

3+50

66.72 66.1 66.9 67.5 67.9 67.9 68.66
Top 26.2 15 15 26.1 26.1 26.1
gut. gut. Top

3+06 = E of 12' Conc. Dr. on Lt.

65.75 65.17
29.8 26.1
walk Dr.

3+00

65.50 65.0 65.9 66.5 66.9 66.6 67.43
Top 26 15 15 26.1 26.1 26.1
gut. gut. Top

2+50

64.32 63.4 64.6 65.2 65.6 65.1 66.16
Top 25.9 15 15 26.1 26.1 26.1
gut. gut. Top

2+00

63.15 62.5 63.4 64.1 64.4 64.2 64.99
Top 26 15 15 26.1 26.1 26.1
gut. gut. Top

1+50

62.04 61.5 62.4 62.9 63.2 63.0 63.67
Top 26.1 15 15 26.2 26.2 26.2
gut. gut. Top

1+00

60.82 60.2 61.1 61.8 61.9 61.6 62.44
Top 26 15 15 26.1 26.1 26.1
gut. gut. Top

0+64 = Brk. in cb. on Lt.

59.92
26
Top cb.

0+50 = opp. P.C. of. Ret.

59.2 59.99 59.92 59.4 60.1 60.5 60.7 60.4 61.20
gut. 49.6 Top 26.2 15 15 26.1 26.1 26.1
Top P.C. gut. Top

Franklin

Lt.

Rt.

4

Evans + Franklin
Set B.M. on S.W. 7th ct.

71.03

11

6+11.20 = WESTLY CURB LINE OF EVANS

Returns = Level

Cold Lay Pav. (Badly Broken)

6+01.20 = WESTLY LINE of EVANS = edge of

69.66	69.03	69.95	69.35	69.71	70.22	70.59	70.66	70.63	70.67	71.00	71.79	72.53
Top	gut.	Top	gut.	26	13		13	26	40	Top	60	Top

69.97	69.45	70.01	70.13	70.46	70.13	70.99
Top	26.1 gut.	13	on C.L.	13	26.2 gut.	Top = P.C.

5+50

69.42	68.9	69.5	70.0	70.3	70.3	70.73
Top	26.1 gut.	15		15	26.2 gut.	Top

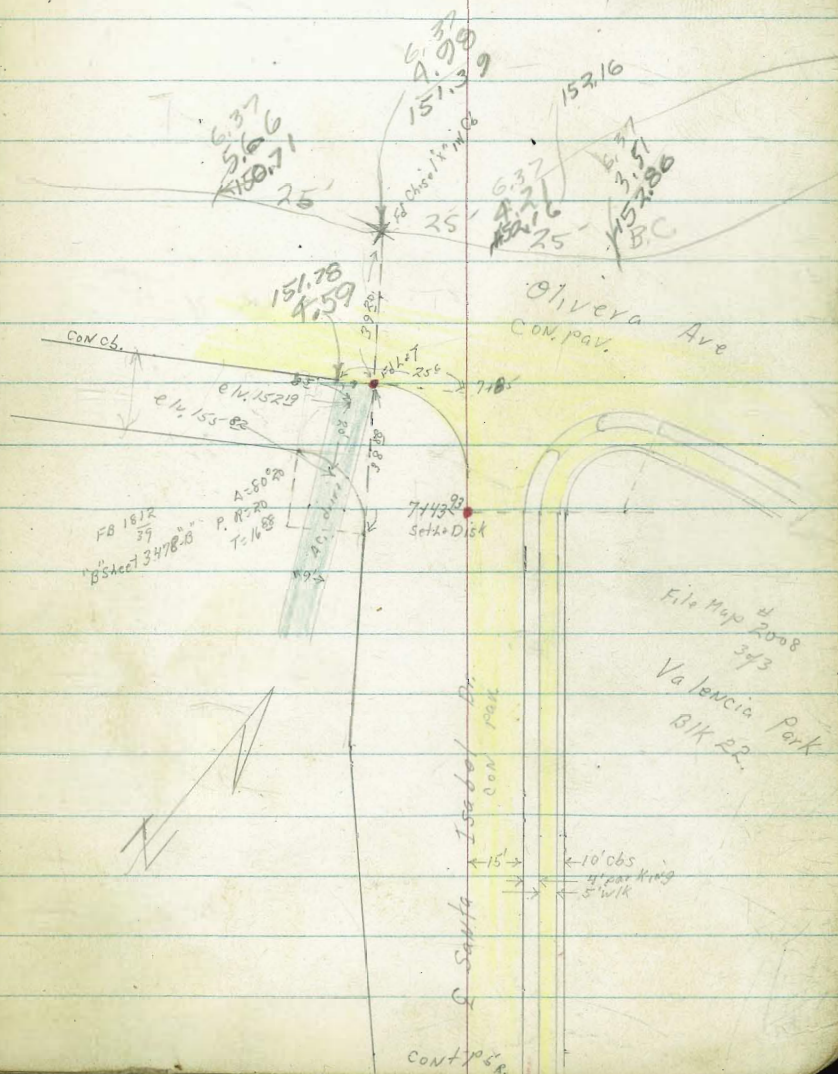
5+00

68.93	68.4	69.1	69.7	70.1	70.0	70.17
Top	26.1 gut.	15		15	26.2 gut.	Top

4+50

68.43	67.8	68.5	69.2	69.4	69.4	70.21
Top	26 gut.	15		15	26.2 gut.	Top

151.78
 4.59
 156.37



Took soil at 15.64 7443²³ Prop BC Olivera St

D. Smith
R. Taylor
J. Schelin

"X" Sec Santa Isabel DA Encina to Olivera D

W 0 4
32250 7

lt. Wly

0725 End AC, on Wly

IND
Law
JUL 7 1953

199.8 199.5 199.4 199.33 199.05 198.71 199.33 199.46
63 76 75 75 803 837 725 762
50 25 15 135 AC 15 gut 15 cb 29 w/k

0718 csa gut Type 'G' end 15' wly

200.2 200.4 200.23 199.79 199.6 199.16 199.67 199.82
58 62 685 729 742 792 741 726
50 25 15 15 15 15 29
cb end gut cb w/k

0713 15' RT & 15' drive

199.70 199.83 200.50
738 725 658
gut 15 15 19

0700 Ely Prop & CB KC,

201.7 201.17 201.04 200.60 201.21 201.38
54 591 604 648 587 570
25 15 15 15 24
gut cb w/k

0-16⁸ cb line Wly taken on cb line extended

201.13 201.68 202.70 202.24 202.18 202.25 202.24 202.03
493 540 438 484 490 483 484 505
99 99 49 49 25 15 15
cb gut cb gut

0-19²⁹ cb line Ely taken on cb line ext.

202.38 202.51 202.57 202.29 202.66 202.24 202.09 201.18
470 454 457 479 442 384 229 250
25 15 105 375 275 875 870
gut cb gut cb

TP₂ 6⁸⁴ 207⁰⁸ 0²⁴ 200²⁴ K

End of top
rvt. 0418 27.

TP₁ 12²⁶ 200⁴⁸ 0¹⁶ 187⁵²

BM 4²⁸ 187⁶⁸

183⁴⁰ NWBP
San Bernardo +
San Jacinto

207⁰⁸

NWly Return
Santa Isabel & Encina

30' C6 Rad L=51° 5 parts 10² ea

BC, ENCINA

702.70
438
ob
702.50.9ut
458
702.02
506

1/3

702.13
425
701.65
542

2/5

701.65
543
701.70
588

3/5

701.05
603
700.61
647

4/5

700.23
686
ob
199.79
729
944

Santa Isabel
End EC.

π HI = 207°8

NEly Return
Santa Isabel & Encina

25' C6 Rad L=36° 4 parts 9° ea

BC, ENCINA

202.24
284
ob
202.66
442
9ut

1/4

202.81
427
202.20
488

1/2

202.30
478
201.63
545

3/4

201.75
533
201.12
596

Santa Isabel
EC. = 0 + 00

201.21
587
ob
200.60
648
944

π HI = 207°8

1+55 27° Lt & dead man

1+54 19° Lt & 10" Power Pole 372414

c=24²⁰

1+50 3° 18.895'

c=20²⁵

1+29 24 BC 0° 00' Rt.

1404 25° Lt 8' road drive

1700

TP₃ 0²⁰ 19489 12³⁹

0+75

0+50

$\Delta = 45^{\circ} 15' 15''$

RR = 175

T = 7294

L = 138²¹

d = 9.82213 per foot

NOV 19
401 1/2
562109H
@ 1420

19469

LT-W/ly

rt = Ely

9

1956	192.9	190.7	190.2	189.19	188.64	189.23	189.20
70 ²	2 ⁰	4 ²	4 ²	5 ²⁰	6 ²⁵	5 ⁶⁶	5 ⁶⁹
50	25	15	12		34	26	24
					34	26	24

1959	193.7	191.9	191.4	190.67	190.03	190.62	190.64
71 ⁰	1 ³	3 ⁰	3 ⁵	4 ²²	4 ⁸⁶	4 ²⁷	4 ²⁰
50	25	15	13		15	15	24
					34	26	24

19529
70²⁰ 0²⁰
135° drive

196.2	194.6	193.9	193.10	192.58	192.23	193.12
71 ³	0 ³	10	129	231	166	177
50	25	15		15	15	24
				34	26	24

19489

197.5	196.3	195.3	195.11	194.79	195.13	195.78
96	10 ⁸	11 ⁸	11 ⁹⁷	12 ³⁹	11 ⁶⁵	11 ⁶⁰
50	25	15		15	15	24
				34	26	24

199.4	197.9	197.2	197.15	196.94	197.54	197.70
72	9 ³	9 ²	9 ⁹³	10 ¹⁴	9 ⁵⁴	9 ³⁸
50	25	15	15	15	15	24
			34	34	26	24

T 20708

2191²⁰ At 06 BC

2167²⁵ 22° 37.63 EC

2157²⁵ 25° Lt My con drive
c=179⁵

2150²⁵ 19° 41.107'

2140²⁵ 27° Lt Sly con drive
c=242⁸

2125²⁵ 15° 35.554'

2100²⁵ 11° 30.001'

1795²⁵ 46° Lt E 8' con driveway

1775²⁵ 22° Lt E dead man
7° 24.448'

1760²⁵ 27° Lt E dead man

LT = W14

188.0	187.6	183.9	183.7	183.4	183.50	183.05	183.47	183.47
62	73	112	112	115	1139	1184	1142	1142
50	40	28	25	15		15	16	24
						94	06	24

RT = E14

189.24	187.24	187.9	184.7	184.3	184.04	183.53	183.93	184.20
565	73	70	103	106	1085	1136	1026	1069
353	253	28	25	15		15	16	24
drive	drive					94	06	24

189.53	187.97	190.8	187.5	186.5	184.63	184.20	184.62	184.75
536	692	41	74	92	1026	1069	1020	1014
378	278	50	25	12		15	16	24
drive	drive					94	06	24

194.3	193.3	190.0	187.7	186.8	185.69	185.15	185.64	185.83
05	16	42	52	81	920	924	935	900
50	33	31	25	15		15	16	24
						94	06	24

194.8	193.9	192.4	190.5	189.9	188.1	186.69	186.25	186.63	186.80
02	10	25	44	50	68	820	864	826	809
50	41	40	25	20	16		15	15	24
							94	06	24

194.74	194.13
05	026
573	465
drive	drive

194.4	191.7	189.6	189.0	187.13	187.19	187.75	187.79
02	32	53	52	716	720	714	710
50	25	19	15		15	15	24
					94	06	24

7194⁸⁹

SEly Return San Onofre + Santa Isabel

25' cb Rad L=39 4 parts 9²⁵ ca

BC Santa Isabel

222 183.06
sat 20 183.48
cb

1/4

222 182.89
242 183.36

1/2

222 182.81
230 183.93

3/4

222 182.83
239 183.59

P.P., San Onofre

222 182.81
sat 23 183.46
cb

π HJ 185²⁸

NEly Return San Onofre + Santa Isabel

25' Rad L=39 4 parts 4²⁵ ca

BC Santa Isabel

179.34 179.69
6⁴⁴ 6⁰⁹
sat cb

1/4

180.21 180.37
5⁵⁷ 5¹¹

1/2

begin good cb
↓

180.58 181.23
5²⁰ 4⁵⁵

3/4

181.13 181.63
4⁶⁵ 4¹⁵

PCC, San Onofre

181.55 182.13
4²³ 3⁶⁵
sat cb

π HI 185²⁸

c=25°

5750 18° 24.12

5730 RT E 13° drive

5725 9° 58.57

c=24°

5700 1° 33.021

c=45°

4795 1/4 BC Lt 0° 00'

4775

4765 RT E 16° cov drive

4760 30° Lt E 11° AC drive

4750 RT begin good cb

773 153 174³⁹ 12⁹² 172⁸⁶

LT = W/Ly RT = E/Ly 13

175.69	168.2	166.4	165.0	164.2	164.45	163.96	164.506	164.58
713	62	80	94	102	94	1043	989	981
50	25	18	17	11	15	15	24	15
					Sut	cb	W/K	W/K

175.7	168.7	165.7	165.83	165.10	165.93	165.05	165.14	165.56
713	52	82	856	899	876	939	935	883
50	25	13	15	15	15	15	15	15
			Sut	cb	cb	W/K	W/K	W/K

177.3	170.4	168.1	167.24	166.81	167.39	167.52
722	40	63	715	758	700	687
50	25	12	15	15	15	24
			Sut	cb	W/K	W/K

177.6	170.8	168.4	167.60	167.07	167.70	167.88
732	36	60	679	732	660	659
50	25	12	15	15	15	24
			Sut	cb	W/K	W/K

178.0	172.5	170.9	170.1	169.39	168.70	169.22	169.60
736	12	35	43	500	569	517	429
50	25	15	10	15	15	24	15
				Sut	cb	W/K	W/K

176.39	174.39	169.58	169.68	170.25
720	000	481	421	414
403	302	153	150	19
drive		Sut	L/A	W/K

177.4	174.3	172.7	171.76	171.35	171.69	171.89
730	01	12	263	304	220	250
50	25	15	15	15	25	15
			Sut	cb	W/K	W/K

174.39

LT = Wly

♀

RT = Ely

14

7443²³ CL BCRT

160.0	158.9	158.7	155.1	154.68	154.37	154.95	155.08
12	30	32	68	722	753	625	682
50	25	22	15	15	15	24	24
				9ut	06	WIK	

7700

166.7	165.9	160.5	157.2	156.81	156.37	156.78	157.05
448	440	14	47	509	553	512	485
50	30	25	12	15	15	24	24
				9ut	06	WIK	

6750 RT & 10° broken cby

165.0	165.9	166.1	159.8	159.05	159.00	159.57
440	440	448	21	24	220	253
50	25	20	6	15	15	24
				9ut	06	WIK

TR₆ 0° 161²⁰ 12⁴⁹ 161²⁰

π 161²⁰

6700

175.49	168.9	167.2	166.5	162.8	162.1	161.95	161.48	162.04
+12	522	78	72	116	123	1244	1221	1236
50	25	22	15	9	7	15	15	24
						9ut	drive	WIK

5497 RT & 11° drive

161.61	161.75	162.16
1228	1264	1223
15	15	19
9ut	210	WIK

5488 172 LT & 8° empty P. 178075

5485 183 LT & 12 Power P. 178075

5475²² EC, 26° 55.25'

176.2	169.3	167.5	163.6	163.0	163.25	162.71	163.24	163.35
+12	51	62	108	114	114	1168	115	1104
50	25	17	12	9	15	15	24	24
					9ut	06	WIK	

π 174³⁹

5460 18° LT & deadwood

SEly Return
Olivera + Santa Isabel

25' CB Rad L = 56^s 5 parts 11^s ea.

BC, Santa Isabel	154.37 7 ³	154.95 6 ²
	9 ⁴	0 ⁶
1/5	153.97 7 ⁹	154.55 7 ³
2/5	153.64 8 ²	154.22 7 ⁶
3/5	153.63 8 ²	154.26 7 ⁶
4/5	153.85 8 ⁰	154.51 7 ³
PCC, Olivera	154.09 7 ⁸	154.69 7 ²
	9 ⁴	0 ⁸

BM starting	1 ⁴	183 ⁴⁷
TP ₂	8 ¹⁴ 184 ²⁰	0 ⁶ 176 ⁷⁶
TP ₇	13 ²⁹ 177 ³²	0 ⁰ 164 ⁰⁸
TP ₆	12 ³¹ 164 ¹¹	10 ¹⁰ 151 ⁸⁰

SWBP cb end
Olivera
Santa Isabel

8105 E Olivera taken along

147.89	151.11	151.42	151.85	152.41	152.85	154.34	156.29
12 ⁰¹	10 ²⁹	10 ⁴⁸	10 ⁰⁵	9 ⁴⁹	9 ⁰⁵	7 ⁵⁶	5 ⁶¹
7 ⁵	2 ⁵	1 ⁵	1 ⁵	1 ⁵	2 ⁵	5 ⁷	10 ⁷

7485 Sly CB line Olivera taken along

150.28	147.68	151.78	151.10	151.52	152.09	152.64	153.03	154.09	154.69	156.18	156.87
11 ⁶²	12 ²²	10 ¹⁵	10 ⁵⁰	10 ²⁸	9 ⁰⁹	9 ²⁶	8 ⁸⁷	7 ⁸¹	7 ³	5 ²²	5 ⁰³
7 ⁵²	7 ⁵	2 ⁵	2 ⁵	1 ⁵	1 ⁵	2 ⁵	2 ⁵	5 ⁶	5 ⁶	10 ⁸	10 ⁸
0 ¹	5 ⁴	0 ⁴	3 ⁴	1 ⁵	1 ⁵	1 ⁵	2 ⁵	0 ⁶	0 ⁶	5 ⁴	0 ⁶

Note: AC, driveway on Lt in sketch p. 6.
elv. also + distances

7465

154.8	154.4	153.5	153.38	153.61	153.63	154.22
7 ¹	7 ¹	8 ⁴	8 ⁵²	8 ²⁹	8 ²⁷	4 ⁶⁸
5 ⁰	2 ⁵	1 ⁵	1 ⁵	2 ⁴	2 ⁴	5 ⁶

T 161²⁰

R150

TP₂

63

97³⁶

124

90⁷³

R225

R107 20° RT & 10° drive

R105 20° LT & 8° drive

R100

1157 20° RT & 10° drive

1150

1109 20° LT & 9° drive

1100

0169 20° RT & 10° drive

91⁰⁶ Lt-Nly
 6³⁰ 90⁵⁵ 90³⁵ 90⁷ 90⁹ 90² 90² 91³³
 20 20 20 20 20 20 20
 w/k out out out out out out out

90⁵⁵ 90⁷² 90³ 90³ 90⁴ 90⁵ 90⁵ 91² 91²²
 14 124 12 12 16 15 14 022 068
 20 20 20 20 20 20 20 20 20
 w/k out out out out out out out out

90⁶² 90⁵³ 89⁹² 90²⁷ 91¹⁵ 91¹⁶
 13 14 20 12 0 0
 20 20 20 20 20 20
 w/k w/k out out out out

90⁵⁷ 90⁴⁵ 89⁵⁷ 89⁹² 90⁰ 90⁵ 89²² 90⁴ 91⁰⁵
 14 15 23 20 19 19 20 13 0
 20 20 20 20 20 20 20 20
 w/k out out out out out out out

89⁴ 89⁴⁰ 89⁵ 88² 88² 88² 89⁰ 89¹¹ 90⁰⁵
 23 25 34 31 31 31 30 21 19
 20 20 20 20 20 20 20 20 20
 w/k out out out out out out out out

337 348 412 375 375 375 375 388 389
 20 20 20 20 20 20 20 20 20
 w/k w/k out out out out out out out

88²⁵ 88¹¹ 87⁵ 87⁵ 87⁵ 87⁵ 87⁵ 88⁵ 89⁰⁸
 36 53 45 43 44 44 44 342 389
 20 20 20 20 20 20 20 20 20
 w/k out out out out out out out out

80²² 80¹¹ 80¹¹ 80¹¹ 80¹¹ 80¹¹ 80¹¹ 80¹¹ 80¹¹
 50 43 43 43 43 43 43 43 43
 20 20 20 20 20 20 20 20 20
 w/k out out out out out out out out

76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶ 76¹⁶
 20 20 20 20 20 20 20 20 20
 w/k w/k w/k w/k w/k w/k w/k w/k

5250

5125

5100

4750

4700

3792 20° RT & 12° drive

3750

3744 20° RT & drive opening

3700

19

6 ⁰⁵ 275 w/k	91 ³¹	6 ¹² 20 20 cut	91 ¹⁵	6 ¹⁹ 20 20 cut	91 ⁰⁵	6 ¹⁶ 10 10 cut	90 ⁰⁸	6 ¹⁵ 10 10 cut	90 ⁰²	6 ¹⁷ 20 20 cut	90 ⁰⁷	5 ¹⁸ 20 20 cut	91 ¹¹	5 ²⁰ 275 w/k	91 ⁰⁶
5 ⁴⁹ 275 w/k	91 ⁰⁷	5 ³⁸ 20 20 cut	91 ⁰⁴	6 ³³ 20 20 cut	91 ⁰⁰	6 ² 10 10 cut	91 ⁰³	5 ²⁹ 10 10 cut	91 ⁰⁵	5 ²⁹ 10 10 cut	91 ⁰⁴	5 ²¹ 20 20 cut	92 ⁰⁵	5 ⁰⁴ 275 w/k	92 ⁰⁰
5 ¹⁵ 275 w/k	92 ⁰⁸	5 ³⁵ 20 20 cut	92 ⁰¹	6 ⁰ 20 20 cut	91 ¹⁴	5 ² 10 10 cut	91 ⁰⁷	5 ⁰⁵ 10 10 cut	91 ⁰⁹	5 ⁰⁵ 10 10 cut	91 ⁰⁵	4 ⁵⁸ 20 20 cut	92 ⁰⁴	4 ⁶³ 275 w/k	92 ⁰²
5 ³⁰ 275 w/k	92 ⁰⁵	5 ⁴⁰ 20 20 cut	91 ¹⁵	5 ² 20 20 cut	91 ⁰⁵	5 ¹⁵ 10 10 cut	91 ⁰²	5 ⁴ 10 10 cut	92 ⁰⁰	5 ² 10 10 cut	92 ⁰²	4 ²⁵ 20 20 cut	92 ⁰¹	4 ⁵² 275 w/k	92 ⁰⁴
5 ³⁷ 275 w/k	91 ²²	5 ³⁸ 20 20 cut	91 ²⁸	6 ⁰ 20 20 cut	91 ¹⁴	5 ⁶ 10 10 cut	91 ⁰⁸	5 ⁵ 10 10 cut	91 ⁰⁷	5 ⁴ 10 10 cut	92 ⁰⁰	5 ⁶ 20 20 cut	92 ⁰⁰	4 ⁵³ 275 w/k	92 ⁰³
5 ¹⁸ 275 w/k	91 ⁴³	6 ⁴ 20 20 cut	91 ⁰⁰	6 ⁰ 10 10 cut	91 ¹⁴	5 ¹⁸ 20 20 cut	91 ⁰⁷	5 ² 10 10 cut	91 ⁰⁷	5 ¹⁸ 20 20 cut	91 ¹⁴	5 ⁰⁸ 225 w/k	91 ⁰⁵	5 ¹⁴ 275 w/k	92 ⁰²
5 ²⁷ 275 w/k	91 ³⁷	6 ¹⁷ 20 20 cut	91 ¹⁹	6 ⁶ 20 20 cut	90 ⁰⁸	6 ¹³ 10 10 cut	91 ⁰⁰	6 ¹ 10 10 cut	91 ⁰³	6 ¹ 10 10 cut	91 ²²	5 ⁰⁸ 225 w/k	91 ⁰⁵	5 ¹⁴ 275 w/k	92 ⁰²
5 ²⁹ 275 w/k	91 ³⁷	6 ¹⁷ 20 20 cut	91 ¹⁹	6 ⁶ 20 20 cut	90 ⁰⁸	6 ¹³ 10 10 cut	91 ⁰⁰	6 ¹ 10 10 cut	91 ⁰³	6 ¹ 10 10 cut	91 ²²	5 ⁰⁸ 225 w/k	91 ⁰⁵	5 ¹⁴ 275 w/k	92 ⁰²

1791 20° Lt & 12° drive

1775

1750

1743 20° Lt & 10° drive

1725

TP4

385

907R

67R

8687

1700

0789 20° Lt & 10° drive

0756 20° Mt & 12° drive

0750

8622
438
275
w/k

8621
458
225
w/k

8558
506
20
w/k

8642
423
270
w/k

8619
453
20
06

8571
50
20
gut

858
42
10

857
50

858
53
10

847
60
20
gut

8511
56
20
06

8534
538
275
w/k

8641
41
275
w/k

8623
439
20
06

8597
48
20
gut

861
46
10

860
42
10

858
51
10

850
52
20
gut

8510
532
20
06

852
509
275
w/k

9072
385
275
w/k

8644
408
20
06

861
46
20
gut

862
44
10

862
45
10

858
48
10

858
53
20
gut

858
484
20
06

858
539
275
w/k

8732
620
275
w/k

8712
647
20
06

865
71
20
gut

862
70
10

865
70

864
72
10

858
72
20
gut

861
708
20
06

8724
625
275
w/k

8742
610
275
w/k

8740
619
225
w/k

8657
708
20
w/k

663
20
w/k

525
225
w/k

584
275
w/k

8823
526
275
w/k

8717
662
20
06

871
65
20
gut

874
610
10

878
62
10

872
63
10

871
65
20
gut

872
526
20
06

8727
520
275
w/k

9359

4400

3490 20° Lt & 14° drive

3460 20° Lt & 20° drive

3450

3409 20° Lt & 11° drive

3400

2455 20° Lt & 9° drive

2450

2405 20° Lt & 11° drive

2400

Lt = Nly

858	848	842	844	842	832	835	837	845
551	583	64	63	64	68	72	62	667
275 wlk	20 cb	20 put	10		10	20 put	20 cb	275 wlk

858	858	848						
543	557	632						
275 wlk	20 wlk	20 wlk						

858	858	848	848	848	848	842	835	848
551	552	613	60	61	64	41	647	633
275 wlk	20 put	20 put	10		10	20 put	20 cb	275 wlk

858	858	848	848	848	848	842	835	848
508	520	580						
275 wlk	20 wlk	20 wlk						

858	858	848	848	848	848	842	835	848
506	526	58	58	60	63	62	622	609
275 wlk	20 cb	20 put	10		10	20 put	20 cb	275 wlk

483	481	525						
275 wlk	20 wlk	20 wlk						
860	860	857	851	852	851	847	847	848

860	860	857	851	852	851	847	847	848
472	520	56	55	56	60	66	524	528
275 wlk	20 wlk	20 put	10		10	20 put	20 wlk	275 wlk

860	860	857	851	852	851	847	847	848
450	467	52	510	52	56	63	524	560
275 wlk	20 wlk	20 put	10		10	20 put	20 wlk	275 wlk

79072

5450

82 ³¹	82 ³¹	82 ³¹	82 ³¹	82 ³¹	82 ³¹	82 ³¹	82 ³¹
0 ²³	0 ⁵⁷	0 ¹⁶	0 ¹⁰	0 ²⁰	0 ²⁰	0 ¹²⁰	0 ¹⁴⁰
275 w/k	20 c6	20 gut	10 100	20	20	20 gut	275 w/k

5425

82 ²⁷	82 ²⁷	81 ⁹	81 ⁵	81 ⁵	81 ⁵	81 ⁵	81 ⁵
40 ⁶⁹	40 ⁴⁹	0 ⁶	0 ²	0 ²	0 ⁸	1 ²⁰	0 ¹³
275 w/k	20 c6	20 gut	10	10	10	20 gut	275 w/k

775 0¹⁸ 82³⁸ 862 82¹⁰

5412 20° RT & 12° drive

5408 20° LTR 10° drive

82 ²⁸	82 ²⁸	82 ²⁸	82 ²⁸	82 ²⁸
800	826	800		
20 w/k	20 w/k	20 w/k		

5400

83 ²⁵	83 ²⁵	83 ²⁵	83 ²⁵	83 ²⁵	83 ²⁵	83 ²⁵	83 ²⁵
6 ⁸²	7 ⁰²	7 ⁶	7 ²	8 ⁰	8 ³	8 ⁰	7 ²²
275 w/k	20 c6	20 gut	10	10	10	20 gut	275 w/k

4475

84 ²⁷	84 ²⁷	83 ²⁷	83 ²⁷	83 ²⁷	83 ²⁷	83 ²⁷	83 ²⁷
6 ¹⁵	6 ¹¹	7 ³	7 ³	7 ⁴	7 ²	7 ²	7 ³⁵
275 w/k	20 c6	20 gut	10	10	10	20 gut	275 w/k

4450

84 ²¹	84 ²¹	83 ²¹	83 ²¹	83 ²¹	83 ²¹	83 ²¹	83 ²¹
5 ⁸¹	6 ⁰⁵	6 ⁹	6 ⁸	6 ⁹	7 ⁰	7 ⁵	7 ¹⁰
275 w/k	20 c6	20 gut	10	10	10	20 gut	275 w/k

4440 20° Lt. & W° drive

84 ²¹	84 ²¹	84 ²¹	84 ²¹	84 ²¹	84 ²¹	84 ²¹	84 ²¹
5 ⁷⁶	5 ⁸⁷	6 ¹⁵⁸					
275 w/k	20 c6	20 gut					

4425

85 ⁰⁴	84 ²⁰	84 ²⁰	84 ²⁰	84 ²⁰	84 ²⁰	83 ²⁰	83 ²⁰
5 ⁶⁸	5 ⁹⁸	6 ⁵	6 ⁵	6 ⁶	6 ⁹	7 ⁵	6 ²⁸
275 w/k	20 c6	20 gut	10	10	10	20 gut	275 w/k

BM starting 112 91⁸⁸
 TP8 7⁹² 93⁰⁰ 10⁶⁷ 86⁰¹
 TP7 6⁶² 96⁶⁸ 0² 90⁰⁶
 TP6 8⁶⁴ 90²⁸ 0¹⁴ 82¹⁴

6+83⁴⁵ & 40th st

6+55 right & 12th P.P. # 60066

6+53⁴⁵ Wly 40th st also P.L. line

6+10

5+80

74 ⁵	73 ¹	73 ²	73 ²	74 ²	74 ⁴	74 ²	74 ⁸	75 ¹	75 ⁴	77 ²				
$\frac{78}{80}$	$\frac{92}{50}$	$\frac{91}{30}$	$\frac{86}{20}$	$\frac{80}{10}$	72	$\frac{74}{10}$	$\frac{75}{20}$	$\frac{73}{30}$	$\frac{69}{50}$	$\frac{45}{80}$				
78 ⁵	77 ⁵	76 ¹	76 ¹⁴	76 ¹⁰	76 ⁰	76 ²	76 ¹	76 ²	76 ⁵	74 ²	74 ²	75 ⁰⁴	76 ⁵	77 ²
38 ⁸⁰	48 ⁶⁰	52 ³⁰	6 ²⁷⁵	6 ²²⁵	6 ²⁰	6 ²⁰	6 ²⁰	6 ²⁰	5 ²	7 ³⁶	7 ³⁰	7 ²²	5 ¹	5 ¹
wik	wik	wik	wik	cut	cut	cut	cut	cut	cut	cut	cut	cut	wik	wik
78 ⁵²	78 ⁴²	77 ⁵	77 ²	77 ²	77 ²	77 ²	77 ²	77 ²	77 ⁴⁴	77 ⁵⁵	43 ⁸⁰			
369	3 ⁸⁵	4 ⁸	4 ⁶	4 ⁸	5 ¹	5 ¹	4 ⁸⁴	4 ⁷³						
275	20	20	10	10	10	10	20	20	273					
wik	cut	cut	cut	cut	cut	cut	cut	cut	wik					
80 ¹⁵	79 ²⁸	79 ²	78 ²	78 ²	78 ²	78 ²	77 ²	79 ¹	79 ¹	79 ¹²				
212	230	33	31	36	40	45	329	314						
273	20	20	10	10	10	10	20	20	273					
wik	cut	cut	cut	cut	cut	cut	cut	cut	wik					

82⁸⁰

"X" Section Bear St.
Kurtz to California

LT-Wly
 6L 31.8
 6 31.6
 6 31.4
 6 31.1
 7 31.8
 6 31.6
 6 31.6
 6 31.5
 6 31.7
 26

0+25
 0+14 40' Lt & 10' door to storage Bldg cow floor
 0+07 35' At outlet (5) 2" drain pipes
 0+01 40' At Begin 9 high board fence
 0+00 Nly line Kurtz

6.31.90
 402
 Elev

21.3
 66 31.4
 72 30.7
 78 30.1
 84 29.4
 86 29.3
 74 29.5
 11 24.8
 76 30.0
 35 27.03
 70 27.03
 72 31.2
 40

28.0
 97 28.2
 96 28.3
 9 28.6
 10 28.9
 8 29.1
 9 28.7
 8 29.2
 12 25.4
 8 29.7
 8 29.7
 40

0-10
 0-25 28' At to 12' wide wood plank bridge over ditch

0-37' E Kurtz St ESMH

NOTES REDUCED BY
 ACUMM 1-8-54

27.5
 104 27.7
 102 27.1
 102 27.1
 10 26.9
 10 27.8
 96 28.3
 10 25.1
 86 29.3
 82 27.2
 92 28.6
 40 20 28 28 38 38 40 50

25.7
 12 26.5
 12 25.8
 12 25.5
 102 27.0
 10 27.2
 10 27.1
 116 26.3
 12 25.8
 14 23.4
 12 25.7
 12 25.6
 40 27 20 10 6 12 15 29 31 34 40

0-75 Sly line Kurtz
 0-123' 32' At & 24" ACP under RR.

TP ₂ BM	218	379.1	806	35.73	on Mon & Chalmers 25' Sly line California
TP ₁	432	432.9	122	39.47	
BM	128	51.66	4928		SEBP Chalmers + Kettner

171.50
 20.42
 327
 10
 24.800
 37.5
 T.M
 Hubert

37.91

"X" Sec California St

Lt = Sly

2

Rt = Nly

28

0+50

35.3	39.37	37.7	39.9	39.6	40.7	41.7	42.7	43.0
104	1034	110	98	94	80	70	60	52
370	252	257	12	13	22	30	375	

0+48 36° Rt Begin 2° con walk 11 to line

36°
WIK

0+37 382 Rt 2 20' con driveway

570
382
drive

552
382
drive

0+25

37.5	37.42	36.7	34.1	38.8	40.2	42.0	42.9
112	1129	120	106	92	85	67	58
375	252	257	12	13	28	375	

1190
257
cb end

0+05 252 Lt end cb

0+04 273 Lt 28" pole #3652

0+00 NWly ⁰⁰⁶ Bean St @ 90° to California St

36.7	37.0	36.4	37.4	38.3	39.4	41.2	42.4
120	112	123	113	104	93	75	63
375	27	26	12	10	22	375	

TP4

1190

7871

916

3681

end cb on Lt
0402 25117

487

0-2679 E int. Bean + California @ 90° to California

36.0	35.5	36.6	37.2	37.9	38.4	38.6	40.3	41.9
100	102	94	80	79	76	74	52	44
375	31	19	10	146	21	5	19	375

0-702 Ely Live Bean St taken on line of.

34.5	35.1	35.1	37.4	39.2	41.2
115	109	105	86	68	48
395	20	10	19	395	

4597

Lt = Sly

Rt = Nly

29

1783⁰⁶ Lt Prop Lt. or Sly

65	69	62	63	61	57	59	48
42.2	42.52	41.8	42	42.4	43.0	43.4	43.9
375	255	255	12	12	12	25	375
	26	94					

1775

62	63	68	64	61	59	54	49
42.0	42.38	41.9	42.3	42.6	42.8	43.3	43.4
375	255	255	13	13	13	22	375
	26	94					

1757 24^s Lt & 18" cov drain pipe layed in gutter

72	72	80	70	62	61	56	51	42
41.5	41.5	40.7	41.7	42.0	42.4	43.1	43.6	43.2
375	253	255	13	12	12	25	30	375
	26	94						

1750

1725

72	78	82	77	72	64	60	53	49
40.8	40.8	40.0	41.0	41.5	42.3	42.7	43.4	43.2
375	252	252	14	12	15	25	32	375
	26	94						

1724 42^s Rt & 18" P Pole # 1637

1707 31^s Rt & 2^s Wlk L to line

82	81	93	81	78	62	62	55	52
40.0	39.9	39.4	40.3	40.9	41.8	42.5	43.2	43.4
375	251	253	13	14	14	23	30	352
	26	94						Wlk

1700 35^s Rt. evl 2^s cov walk // to line

0775

95	96	102	91	85	76	66	58	56
39.2	39.11	39.5	39.6	40.2	41.1	42.1	42.9	43.1
375	251	252	15	11	11	23	30	375
	26	94						

T 4871

TP 948. 38⁸⁶

2120⁰⁸ Fly Prop Emory St

697	701	762	702	681	659	682	624
375	306	305	15	15	31	31	31
	R	9ut			9ut	06	
41.37	41.30	40.72	41.32	41.53	41.75	41.52	42.10

1480⁰⁶ E Emory St

609	623	634	630	601	561	537
575	255	12	6	15	30	375
41.05	41.61	41.82	42.02	42.33	42.73	42.97

1440⁰⁴ Fly Prop Emory St

657	659	709	620	587	554	506	470
365	255	235	12	15	30	375	
AK	06	2ut					
41.77	41.75	41.26	42.04	42.17	42.80	43.28	43.55

48 34

"X" Sec Kurtz St
Bear to Emory

1+25

1+00

Note: due to box cars cant
take rail shots on Lt. looks like
straight grade to where picket up.

392^{ft} SE cor another Warehouse

0+92 37^{ft} SW cor Warehouse

0+75

0+50

0+25

TP,

727

34⁸⁹

9⁸⁹

27⁶²

34⁸⁹

0+02 28" L x 12" Pole 1651

373^{ft} RT SE cor Warehouse Bldg.

0+00 Wly Bear St. 279^{ft} RT E Rail Road siding Begin ex rails

BM

138

374

3523

2 Hor Chalmers
1/2 25' L x 1" dia
10.26

374

Lt-Sly

8 ² 26.5	8 ² 26.7	7 ² 27.2	7 ² 27.1	7 ⁰ 27.9	6 ² 28.01	6 ² 28.05	7 ⁰ 27.9	6 ² 28.2
37 ⁵	30	15	15	15	25 ² 54 ¹	30 ⁵ 14 ¹	31	37 ⁵

8 ² 26.4	8 ² 26.7	7 ² 27.3	7 ² 27.8	7 ⁰ 27.9	6 ² 28.1	6 ² 28.05	6 ² 28.11	6 ² 28.1
37 ⁵	30	15	15	15	25 ² 54 ¹	30 ⁵ 14 ¹	30 ⁵ 14 ¹	37 ²

8 ² 26.4	8 ² 26.6	7 ² 27.3	7 ² 27.7	6 ² 28.2	6 ² 28.05	6 ² 28.14	6 ² 28.2
37 ⁵	30	15	15	23 ² 54 ¹	30 ⁵ 14 ¹	30 ⁵ 14 ¹	37 ²

8 ² 26.1	8 ² 26.5	7 ² 27.2	7 ² 27.4	7 ⁰ 27.9	6 ² 28.1	6 ² 28.15	6 ² 28.15	6 ² 28.10
37 ⁵	30	15	15	15	23 ² 54 ¹	30 ⁵ 14 ¹	30 ⁵ 14 ¹	37 ²

11 ² 27.7	10 ² 27.1	9 ² 27.5	9 ² 27.9	9 ² 28.02	9 ² 28.05	8 ² 28.3
37 ⁵	15	15	15	25 ² 54 ¹ Sly rail	30 ⁵ 14 ¹ My rail	37 ⁵

TP₃ 7²¹ 33²¹ 7²⁹ 25³⁰

2150

2125

2100

1483 27³ L+E dead man

1475

TP₂ 5⁵² 32⁵⁹ 7⁸² 27⁰⁷

1455 1⁵ A+E 6" clay pipe drain outlet

1450 27⁵ L+E 10" P Pole # 1675

1443 10² RT SW cor Warehouse

1442 37² RT begin 3' high cor block wall with 5' Cy clone fence on top

Lt. Sly

RT-N14

34

22.0	22.2	22.4	22.5	22.5	22.0	22.3	25.3	25.1	26.8	27.3	27.6
20 ⁶	10 ⁴	9 ²⁸	9 ⁷⁸	10 ¹	10 ⁶	10 ³	7 ³	6 ⁸	5 ³	5 ³	5 ⁰
37 ²	36	28 ⁹	23 ²	18	17	15	8	15	15	21	37 ⁵
		5 ⁴	14 ¹⁶								

22.75	22.13	22.5	22.1	25.5	25.1	26.4	27.3	27.3	27.3	27.5	27.5
9 ⁵⁴	10 ³	10 ¹	10 ⁵	7 ¹	7 ⁰	6 ²	5 ³	5 ³	5 ³	5 ⁰	5 ⁰
39 ³	37 ⁵	38 ¹	31	22	16	18	18	24	24	37 ⁵	37 ⁵
14 ¹	10 ¹¹										

22.6	23.5	24.9	25.4	25.4	26.5	27.0	27.0	27.5	27.5	27.9	27.9
10 ⁰	9 ¹	7 ³	7 ³	6 ⁸	6 ¹	5 ⁶	5 ⁶	5 ⁰	5 ⁰	4 ²	4 ²
4 ²	37 ⁵	35	31	15	15	5	20	20	20	37 ⁵	37 ⁵

25.6	26.1	26.4	26.5	27.0	27.5	27.6	27.6	27.6	27.6	27.6	27.6
7 ⁰	6 ⁵	6 ²	6 ¹	5 ⁶	5 ¹	5 ⁰	4 ⁸	4 ⁸	4 ⁸	4 ⁸	4 ⁸
37 ⁵	30	13	3	13	13	24	37 ⁵	37 ⁵	37 ⁵	37 ⁵	37 ⁵

32⁵⁹

26.1	26.7	27.3	27.3	27.3	27.3	27.3	27.3	27.3	27.3	27.3	27.3
8 ²	8 ²	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵	7 ⁵
37 ⁵	15	15	15	15	15	15	15	15	15	15	15

26.41	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6
8 ⁸	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³	7 ³
15	15	15	15	15	15	15	15	15	15	15	15

34⁸⁹

Lt = Sly

♀ Mt = Nly

3+78¹⁸ Wly Emory St

90	90	82	121	112	106	103	94	96	96
372	20	7	5	115	165	23	262	375	375
			SyR	SyR	M/R	SyR	M/R		

3+38¹⁸ ♀ Emory st
4Z Lt & SMH

86	98	123	110	1103	1113	102	106	82	72	72	72
375	15	10	6	42	116	10	14	14	26	312	375
				M/R	Hul	SyR	M/R	M/R	M/R	M/R	M/R

3+35 I ♀ crosses Sly Rail

3+27 28° Lt & deadman

3+25 36° Lt & 14" Pole gave

3+20 ♀ crosses Wly Rail

2+98¹⁸ Ely Emory

38' Mt cell cov block wall with Expt ext'n

5° below

86	92	125	114	1038	1038	106	81	66	64	629	58	68	372
375	29	24	19	123	78	7	21	262	375	375	375	375	375
				SyR	M/R			SyR	M/R	M/R	SyR	M/R	SyR

2+75

82	120	126	102	1038	1033	110	80	73	60	546	580	510	510
43	375	35	29	223	172	10	3	11	20	263	318	375	375
				SyR	M/R					SyR	M/R		

33²¹

"X" Sec Emory St

1752 40° Lt Nly drive entrance AC,

1750 27° RT E dead man

1722 40° Lt Sly drive entrance AC,

1700

0475

0478 40° Lt Begin 8" con retaining wall

0430 40° Lt E 73' drive to parking area oil

0410

TP4 108° 42° 05 196 31° 25

0400 Nly Kurtz St

Station	Angle	Dist	Lat	Long	Remarks
1752	40° Lt	36.61	39.145		AC, drive
1750	27° RT E	36.61	39.145		dead man
1722	40° Lt Sly	36.61	39.145		drive entrance AC,
1700		33.16	33.5		
0475		32.4	32.11		
0478	40° Lt	27.84	31.4		Begin 8" con retaining wall
0430	40° Lt E	30.4	30.8		73' drive to parking area oil
0410		30.4	30.8		
TP4	108° 42° 05	23.6	24.1		
0400	Nly Kurtz St	23.6	24.1		

↑ 3321

Lt = Wly

2

At = Ely

37

BM Starting

404

49⁸⁰

49⁷⁸

TP7

543

5384

219

4841

TP6

11⁷⁵

50⁶⁰

7⁸⁰

38⁸⁵

5113032

2707²⁰ SCLive Hancock to West

40.31	39.86	41.28	40.69	41.34	40.74	40.93	41.36	41.49	41.52	41.06	41.61
6 ³¹	6 ²⁹	5 ³²	5 ²⁸	5 ³¹	5 ²⁷	5 ²⁸	5 ²⁹	5 ¹⁶	5 ¹³	5 ²⁹	5 ²⁴
87	87	40	40	36	36	26	13	13	13	27 ²³	27 ²³
86	9ut	9ut	9ut	86	9ut	9ut	9ut	9ut	9ut	9ut	9ut
				41.27	40.71					41.09	41.64
				5 ³⁸	5 ²⁴					5 ⁵⁶	5 ²⁶
				86	9ut					9ut	86

Mid Pt SE Ret

mid Pt SW Ret

2700²⁰ sly Hancock St edge road pav.

41.4	41.3	40.59	41.21	41.40	41.36	40.92	41.59	41.69
5 ²⁹	5 ³⁹	6 ⁰⁶	5 ³⁹	5 ²⁵	5 ²⁹	5 ²³	5 ²⁶	4 ⁹⁶
40	26	26	12	12	12	26	26	40
wk	26	9ut	9ut	9ut	9ut	9ut	9ut	wk

1496 27⁵ Lt E 12" Tel Pole # 416736 H

TP5

654

4665

124

4041

1475

1457

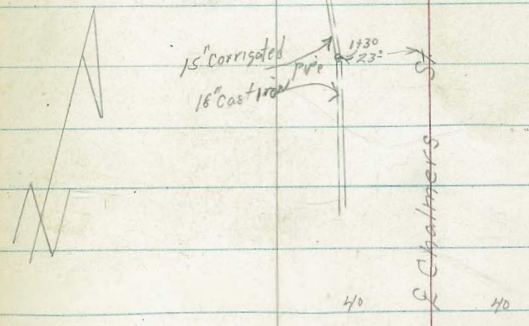
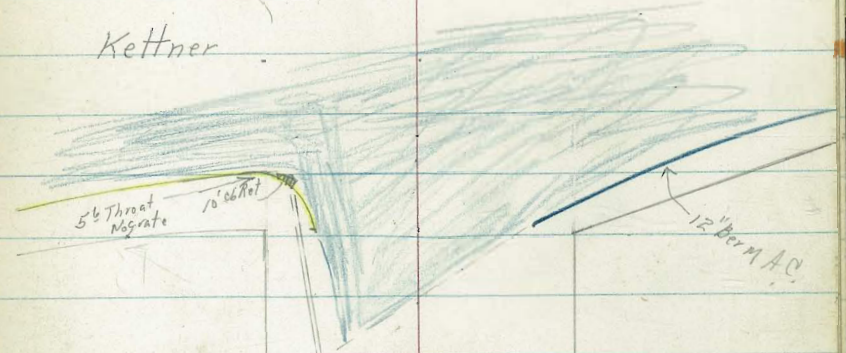
28³ At E deadman

38.5	37.6	35.3	38.9	37.6	39.4	39.2	39.4	40.1
36	48	38	32	36	22	22	23	20
40	30	26	13	13	13	24	27	40

4205

FD 717 LAT ← 33' → FD 717 LAT

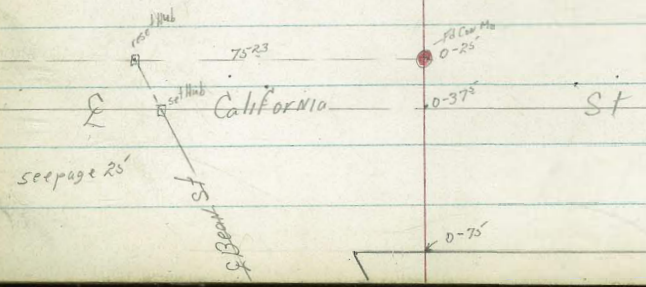
Kettner



E. Chalmers

40 40

0+00



X. Soc Chalmers

Lt. Wly

Rt. Fly

39

0+50

43.2	41.9	40.6	39.2	39.2	41.3	41.2	40.2	40.2	40.4	39.1	39.6	39.6	39.3
72	92	112	124	124	103	104	112	114	112	124	120	120	122
20	25	21	20	17	15	10	8	13	29	32	38	40	

TP1

1151

57³⁹

2⁸⁰

40⁰⁸

0+25

42.5	41.6	40.2	39.9	39.5	39.7	38.4	38.6	38.5	38.5	37.6	38.4	38.4	38.0
04	13	22	23	31	32	42	43	44	44	53	45	45	42
40	27	22	19	16	9	6	11	20	29	31	37	40	

0+01 40² Lt SE cor Warehouse Bldg

43.5	40.8	40.2	40.2	40.2	40.2	40.2	37.5	37.0	35.6	36.6	36.2	34.3	
41.5	40.8	35.4	35.3	35.2	35.2	35.0	37.0	37.0	35.6	36.6	36.2	34.3	
14	24	44	76	72	42	42	53	54	52	72	63	62	86
40	25	20	19	17	14	8	7	18	30	31	40	100	

0+00 Nly California St

0-23

38.9	38.4	37.4	34.2	34.0	33.5	33.7	36.4	36.6	35.6	33.7	33.4	31.6
43	45	55	82	82	64	72	65	63	73	92	95	113
40	23	21	18	16	14	8	5	20	35	40	100	

0-375 E California St also on SMH

38.1	37.2	33.1	32.9	34.2	33.5	33.5	35.2	35.2	31.3	33.5	33.1	31.0
48	52	98	100	87	73	73	65	65	76	94	98	112
40	25	19	16	15	11	6	13	13	30	40	100	

0-434 1/2 Lt to E inlet 24" cast iron pipe

10 ¹⁵	16 ⁵	10	30.2	30.5	33.8	33.6	33.3	31.1	33.6	33.6	31.3	
72	84	91	93	96	112	93	93	93	96	112	116	116
40	20	11	18	18	40	100						

18² Rt to NW cor Laundry Bldg

0-75 sly line California St.

30.2	30.5	33.8	33.6	33.3	31.1	33.6	33.6	31.3
72	84	91	93	96	112	93	93	93
40	20	11	18	18	40	100		

B.M.

715

42⁸⁸

35⁷³

p 26
SMH
Chalmers
28 W Calif

42⁸⁸

Lt=Wly

RT=Ely.

40

49.0F
3.51 437
26 26
2 gal

1475 26° Lt evb cb Return + inlet throat

47.1 47.44 47.46 47.54 47.64 47.52 47.7
45 45 43 405 385 403 32
40 23 13 17 30 40
edge 12 15

1465 Begin AC paving over old RR tracks

1460 32° RT & 16" PPole # JR1905

1450

47.0 47.0 47.3 47.3 47.2 47.3 46.0 46.3
46 46 43 43 44 43 55 53
40 32 20 13 8 32 34 40

1430 23° Lt & 15" corrugated pipe Nly
18" cast iron pipe sly runs into oil drums
somewhere underground, before open ditch

78.5 73.74 45.10
18" 18" 15"
23°

1426 27 1/2° Lt & 14" PPole # 1906

1425

45.7 45.8 45.2 44.9 45.9 45.9 44.2 44.8 45.1
52 58 64 62 52 52 74 68 65
40 33 17 12 10 28 31 40

1400 38° Lt & 12' door con floor + apron

0499 36° RT & 8" tel Pole # 473047 H

0484 23° Lt & 10" Anchor Pole # gone

0475

46.0F 45.46 45.1 43.9 43.4 44.3 43.8 42.4 42.9 42.1 42.2
55 63 65 72 82 73 78 93 82 88 94
Floor apron 36 16 10 15 29 31 36 40

0469 23° Lt & dead end

0468 39° RT & 10" Pepper tree

44.6 43.5 42.5 41.6 42.0 42.0 41.5 40.8 40.8
70 81 91 100 96 96 104 108 108
40 24 14 0 11 20 29 40

T 51.59

Opal St.

Fanuel to Gresham

3-17-54

W.O. 32335

Schmormeyer

Boyer

T.P. sheet # 1780

Schelin

" 1781

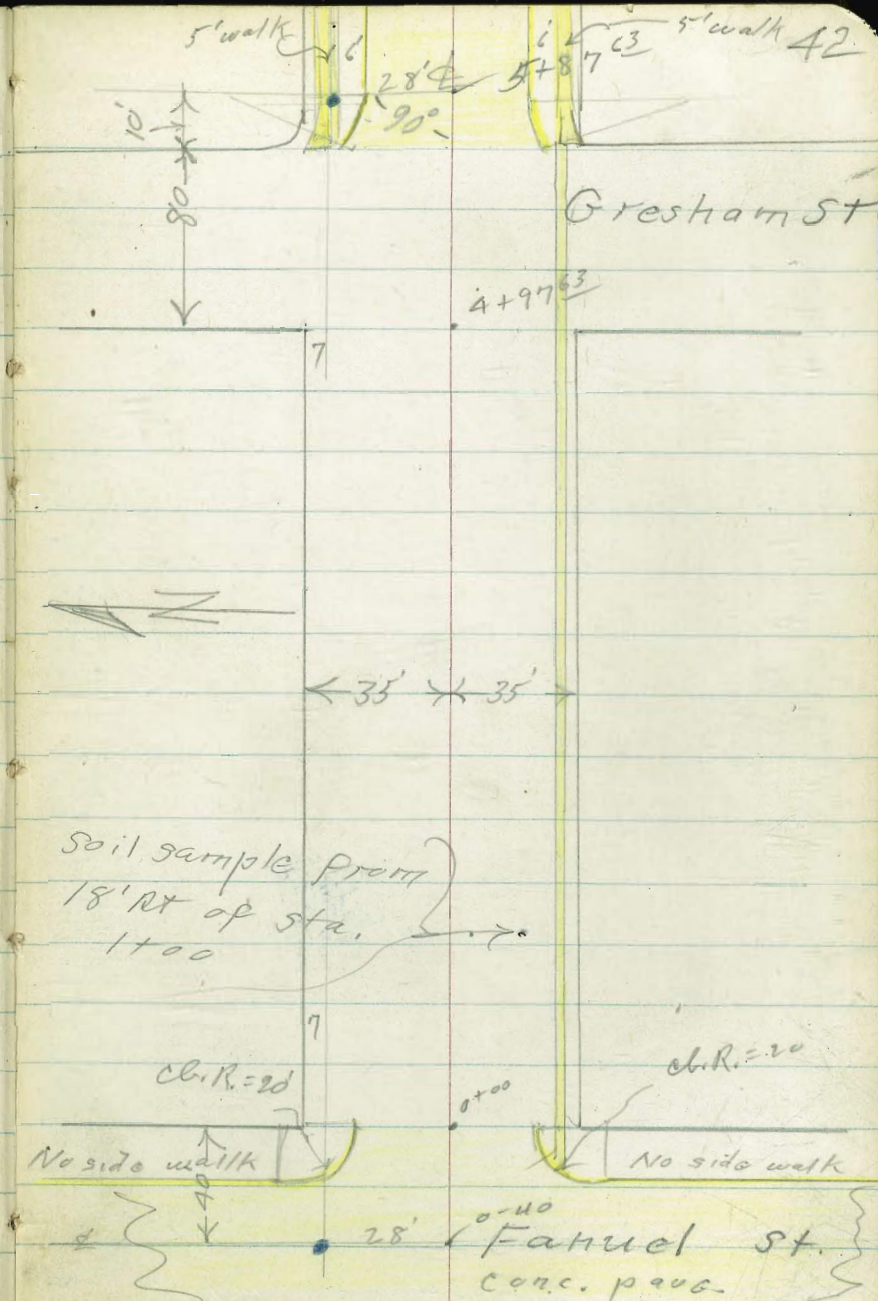
Pullen

Map # 1263

w denotes on conc. walk

W.M. in water meter box

INDEXED
Law
MAR 19 1954



Opal

Notes reduced 4/9/54
rereduced 4/13/54
Change of 6.21' in the
Original B.M.
D.D.S.

151.19
3.98
28
w
151.7
4.0
35
43

0+25

153.6 153.3 151.8 151.8 151.5 150.9 151.7 151.74
1.6 1.9 3.4 3.4 3.7 4.3 3.5 3.93
35 28 18 15 20 21 25
w

0+22 - 15' Lt. = W.M.

153.1
2.1
35
149.94
5.23
28
w
149.5
5.7
35

35° Lt. = start fence

20' Rt } end cl. = E.C. 20' Rad
20' Lt }
0+00 = Ely line Fanuel
= end conc. pave.

152.1 151.50 150.86 150.74 148.94 149.45 149.94
3.1 3.67 4.31 4.93 6.23 5.72 5.23
30 20 20 20 20 20 25
cl c cl w

0-12 - 25' Rt = start Nly edge walk
0-15 - 28' Rt = start Sly edge conc. walk

152.34 151.84
2.83 3.35
cl c
85 85
146.33 146.86
8.84 8.31
85 85
c cl

20' Rt }
40' Lt } = B.C. 20' Rad. cl.

0-20 = Ely cl. Fanuel

150.99 150.47 149.84 149.79 148.59 147.97 148.55
4.18 4.75 5.33 5.88 6.58 7.20 6.62
40 40 20 20 20 40 40
cl c c B.C. B.C.
cl c

0-40 = Ely Fanuel

151.77 150.17 149.09 148.03 146.25
3.40 5.00 6.08 7.14 8.92
85 35 35 85
155.17

B.M.#2 5.24 155.17 11.41 149.93

Lt. Nly. 7' Opal & Ely Fanuel

B.M.#1 0.06 161.34 - 161.28

Top. S.E. Hydt. Tourmaline & Fanuel

Opal

0+87 - 31' Lt. = end fence.

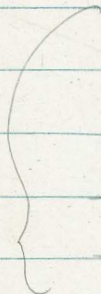
0+77 24' Rt. = W.M.

0+75 - 22' Lt. = W.M.

T.P. 9.13 162.30 1.2.00 153.17

30⁵ Lt. = start

0+54 - 28' Rt. = 3' N. + S. walk



35' Lt. = end fence.

0+50 } 30⁵ Lt. = start fence

0+41 35' Lt. = 8⁵ wide conc. ^{car port}

0+28 - 23' Rt. = W.M.

4

162.30

151.97	151.67	151.43
3.25	3.50	3.74
28	35	45
W	W	W

151.78	151.8
3.39	3.4
28	35
W	

153.9	153.6	152.5	152.7	152.5	151.8	152.4	151.84
1.3	1.6	2.7	2.5	2.7	3.4	2.8	3.33
35	30	18		15	20	21	25
							W

154.17	153.89
1.00	1.28
55	35

155.17

Opal

45

1+35 - 30' Lt. = Φ 8' conc. drive

157.66	156.31	155.98
4120	5155	5188
78	35	302
Cor. floor		

1+29 - 23' RT. = W.M.

1+17 { 28' RT. = Φ 3' conc. walk
22' Lt. = W.M.

153.81	153.71	153.56
8.05	8.14	8.30
28	35	45
w	w	w

161.86

T.P. 7.98 161.86 8.42 153.88

1+14 35' Lt. = Φ 3' conc. walk

155.95	155.50
6.35	6.80
45	35
w	w

153.30	153.19	153.5
9.00	9.01	8.8
25	28	35
w	w	

1+00

155.0	153.7	154.3	154.3	153.9	157.9	153.4
7.3	8.6	8.0	8.0	8.14	9.4	8.9
35	18		8	15	20	21

0+92 35' Lt. = Φ 8' conc. drive

155.98	155.07
6.32	7.23
55	35
Cor. floor	

162.30

opal.

2+11 - 22' Lt = W.M.

2400

1+81 { 28' Rt = 3' conc. walk,
26' Lt = 8' wide conc. drive

1+80 23' Rt = W.M.

1+58 - 22' Lt = W.M.

1+73 - 30' Lt = 4' wide 6' high hedge

1+75 - 35' Lt = start fence

1+1

1750

4

46

156.58
5.28 5.23 5.1
25 28 35
w w

158.4 158.7 157.4 157.3 157.6 157.6 157.7 156.9
3.5 3.7 4.5 4.6 4.3 4.3 4.7 5.7 5.0
35 27 22 18 8 15 20 21

159.13 157.83 157.50 157.04 155.95 155.78 155.58
2.73 4.03 4.36 4.82 5.91 6.08 6.28
75 35 30 28 35 45
on conc. drive w w w

155.2
6.7
35

155.7 155.00 154.98 155.3
6.7 6.86 6.88 6.6
21 25 28 29
w w

157.1 156.8 155.5 155.9 155.9 155.5 154.5
4.8 5.1 6.4 6.0 6.0 6.4 7.4
35 28 18 8 15 20

161.86

Opal
 T.P. 5.55 165.97 1.49 160.37

2+84

2+81-23' RT. = W.M.

2+50 } 22' Lt. = W.M.
 28' RT. = 3' conc. walk

2+39 36' Lt. = end drive

2+31-23' RT. = W.M.

2+30 36' Lt. = start conc. drive

2+25-36' Lt. = end fence

47

158.52
 3.34 158.9
 28 31.0
 w 29 31.4
 35

161.1 160.1 160.1 159.2 158.0 158.9 158.56
 0.8 1.8 1.8 2.7 3.9 3.0 3.30
 35 18 15 20 21 25
 w

157.85 157.04 157.63 157.73
 4.01 4.02 4.23 4.63
 25 28 35 45
 w w

159.9 159.7 159.7 159.3 159.0 158.6 157.7 158.1
 2.0 2.2 2.7 2.6 2.9 3.3 4.2 3.8
 35 25 18 7 15 20 21

160.76 159.96
 1.10 1.90
 67 36
 Gar. floor

160.76 159.66
 1.10 2.20
 67 36
 Gar. floor

161.86

opal

3+34 37 Lt. = 8' wide conc. drive

163.33
2.80 4.13
70 37
Gar. floor

3+25 34' Lt. = end fence

3+19 28' Rx. = 3' wide walk

158.78
7.35 7.72 8.16
28 35 45
w w w

158.71
7.42 7.11 7.6
28 29 35
w w w

3+00 } 22' Lt. = w. m.

161.3 160.6 160.3 159.2 158.5 159.2 158.73
4.8 5.5 5.8 6.9 7.6 6.9 7.40
35 18 15 20 21 25
w w w

166.13

B.M.#3 7.55 166.13 7.34 158.58

2+92 34' Lt. = start v high tail fence

Set. B.M. chisel in walk 25' Rx Sta. 1+83

2+86 36³ Lt. = 9' wide conc. drive

162.18 161.17
3.74 4.75
65 362
Gar. floor

165.92

Opal.

±

49

4+25 35⁵ Lt. = start fence

159.47	159.40	159.6	159.3
6.66	6.73	6.5	6.8
25 ²	28 ²	29	35
w	w		

4+00 } 22 Lt. = W.M.

167.4	161.7	161.2	160.8	160.1	159.0	159.7
3.7	4.4	4.9	5.3	6.0	7.1	6.4
35	18		8	15	20	21

3+82 28' Rt. = ± 3' conc. walk

159.31	158.95	158.47
6.82	7.18	7.66
28 ²	35	45

3+80 37' Lt. = ± 8' conc. drive

166.13	162.43
0.00	3.70
107	37
Gar. floor	

3+77 23' Rt. = w.m

3+55 23 Rt. = W.M.

3+50 22' Lt. = W.M.

159.03	158.97	159.1	158.8
7.10	7.16	7.0	7.3
25 ²	28	29	35
w	w		

161.9	161.1	160.3	159.7	158.7	159.2
4.2	5.0	5.8	6.4	7.4	6.9
35	18		15	20	21

166.13

Opal

A+82 22' Lt. = W.M.

A+79 22' Rt. = W.M.

A+75 35² Lt. = end fence

A+69 on walk

A+65 35 Lt. = \pm 8' conc. drive

22' Lt. = W.M.

A+60 25² Rt. = start dip in walk

3 T.P. A.61 166.73 A.01 167.12

3 A+47 28² Rt. = \pm 3' walk

A+27 22' Rt. = W.M.

50

160.27
6.46 6.48
252 282
w w

159.90
6.83 6.85
252 282

164.80 163.43
1.93 3.33
68 35
Gar. floor

160.13 160.03 160.3 159.9
6.60 6.70 6.4 6.8
252 282 29 35
w w

163.1 162.2 161.7 161.3 160.7 159.6 160.4
3.6 4.5 5.0 5.4 6.0 7.1 6.3
35 20 8 15 20 21

166.73

159.98 157.63 158.53
6.15 6.50 7.60
282 35 45

166.13

Opal

5+42 - 22' RT. = W.M.

5+37⁶³ } Φ Grosham

5+16 - 28⁹ RT. = Φ 3' walk

4+97⁶³ } = wly Grosham

Φ

51

	160.48		
6.25		160.41	
26		6.0	160.7
w		30	160.5
		w	35

	166.6						
0.1		167.6		161.7		161.4	
125		4.1		5.0		5.8	
		3.5		8		15	
		1.7				160.9	
		18				6.5	160.7
						20	160.8
						21	

	160.38		
6.35		160.08	
289		7.10	159.63
		35	45

	160.38		
6.35		160.30	
252		6.43	160.4
w		w	35
		282	35
		w	35

	163.5						
3.2		162.6		161.7		161.6	
36		4.1		5.0		5.1	
		35		18		8	
						161.3	
						6.0	160.7
						13	159.8
						20	160.5
						21	

166.73

Opal

B.M.#4
FR 4.65 166.13 5.25 161.48

6+37⁶

5+87⁶ { 20' RT } = E.C. 20' Rad Ref.
 { 20' Lt } = cl.

35' Lt = N. w. cor. walk to east
26' Lt = S.W. cor. walk to east
21' Lt = start curb.
34' RT = S.W. cor. walk to east
26' RT = end 3' walk from west
 east
26' RT = N.W. cor. walk to
22' RT = start curb
 = start conc. pave.

5+77⁶³ = Ely line Groshean

Set B.M. on Lt. 28' Lt. of Sta, 5+87⁶³

161.03 160.37 160.78 159.41 160.03
5.70 6.36 6.45 7.32 6.70
20 20 20 20 20
cl c c c cl

161.8 161.49 160.38 160.2
4.8 5.24 6.35 6.5
35 31 31 35
Nly. edge Nly. edge
walk walk

161.46 161.37 160.71 160.62 159.63 160.13 160.31
5.27 5.36 6.02 6.11 7.10 6.60 6.42
26 20 20 20 20 20 26
slg. cl c c cl Nly. edge
walk

160.71 160.18 160.26 160.3
4.6 6.52 6.55 6.47 6.4
35 26 29 34 35
Grd Both Both
walks walks to
east

161.61 161.54 161.5 159.43 160.08 160.1
5.12 5.19 5.2 7.30 6.65 6.6
35 26 22 c 22 22
w w c cl Grd

161.46 160.91 160.9 160.70 161.4 159.8
5.27 5.82 5.8 6.03 5.3 6.9
21⁶ 21⁶ Grd & Pave. 15 21
cl c Grd Grd

166.73

Opal St.

53

check B.M.#1

0.08 155.07

T.P. 11.44 155.15 7.44 143.71

T.P. 3.35 151.15 12.12 147.80

159.92

B.M.#1 - Page A3 = orig B.M. ^(161.78) EL = 155.07
149.93
B.M.#2 - Page A3 (EL = 143.72)

X Sect. Franklin Ave. Evans To 28th St.

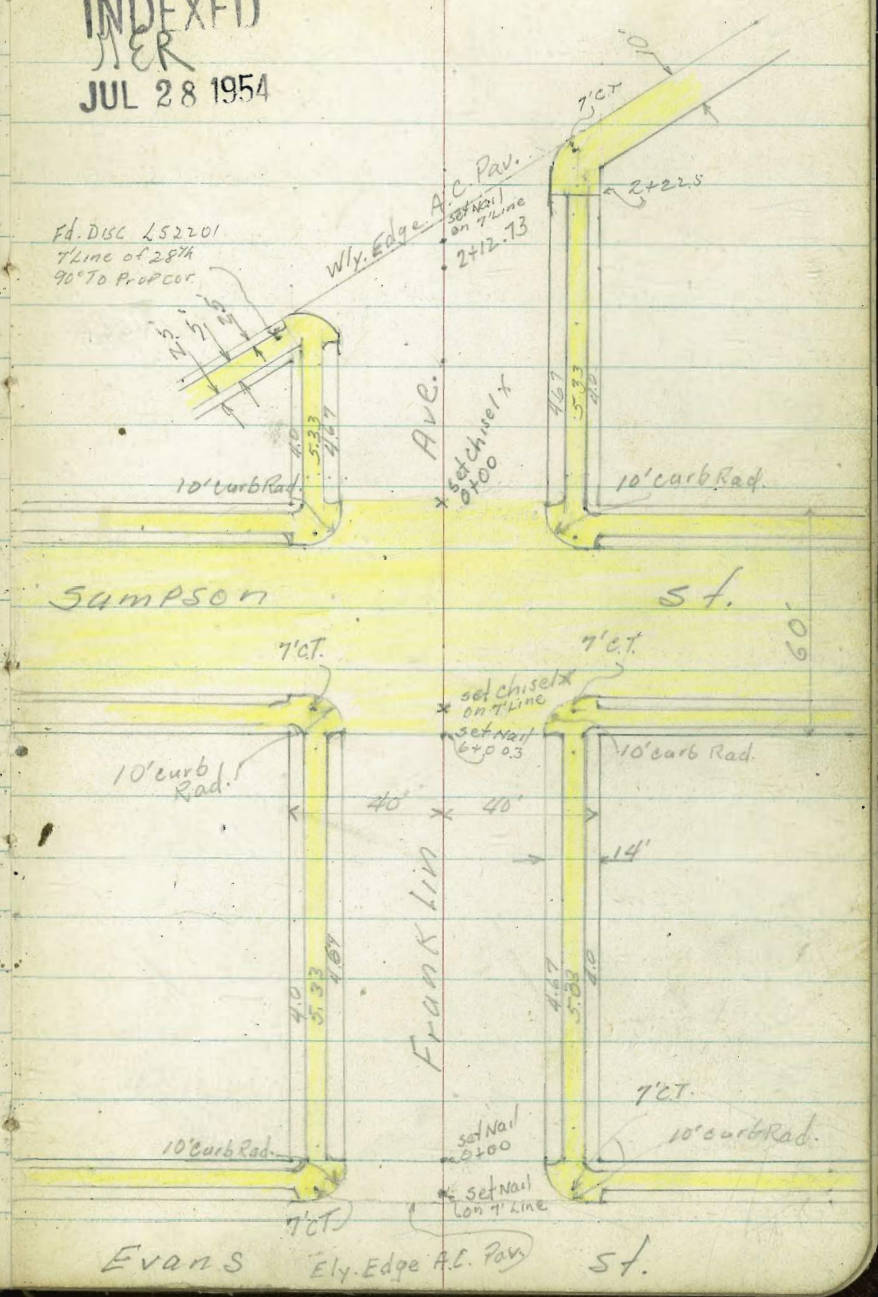
7-24-54 W.O. 32380

Pope
Parks
Olson
Map # 379

Note - Existing curbs & sidewalks
are in rather poor condition

INDEXED
MER
JUL 28 1954

Fd. Disc 452201
7' Line of 28th
90° To Prop Cor.



X sect. Franklin Ave. 28th St. To Evans St. Lt. & Rt.

(Sketch Page 54)

0+58 = East Edge Ribbon Drive 26' Right

73.08 73.83 73.87 75.69 75.83
 26 30 30 47 57
 LIP Edge Back
 walk walk

0+52 = West Edge Ribbon Drive 26' Right

72.49 73.40 73.60 75.71 75.99
 26 30 30 47 57
 LIP Edge Back
 sidewalk walk

T.P. 72.28

0+50

71.95 71.3 72.1 72.6 72.7 72.5 73.20
 26 26 13 13 26
 TOP Gut TOP
 curb

0+00 East Line Evans

70.89 70.3 70.9 71.4 71.4 71.1 72.02
 26 26 13 13 26 26
 TOP Gut Gut TOP curb
 curb

Curb Return South Side

71.36 71.95 71.2 71.93 71.2 72.02
 B.C. B.C. Mid Pt. Mid Pt. E.C. E.C. = 0+00
 Gut. Top Ground TOP Ground TOP
 AC curb curb curb curb curb

Curb Return North Side

70.40 70.91 70.3 70.92 70.4 70.89
 B.C. B.C. Mid Pt. Mid Pt. E.C. E.C. = 0+00
 Gut. Top Ground TOP curb Ground TOP curb
 AC curb curb curb curb curb

0-10 cont.

70.30 69.50 75.25 75.85
 90 90 90 90
 TOP Gut Gut TOP
 curb curb curb curb

0-10 = Ely. Curb Line Evans St. Also Ely. Edge AC paving

70.89 70.37 70.45 70.94 71.18 71.25 71.12 71.41 71.94
 40 40 26 13 13 26 40 40
 TOP Gut Gut Gut TOP curb
 curb

0-30 = E Evans

69.65 70.16 70.36 70.59 70.82 70.89 70.93 71.32 71.98
 90 40 26 13 13 26 40 90

BM = S.W. T.C. Evans & Franklin 71.03

See Page 4

Actual Elev. Shown

L- E R-

5+00

8042	80.0	80.7	81.2	81.5	81.3	81.82
TOP	26	13		13	26	26
Curb					Gut.	TOP
						Curb

4+96 TO 5+00 Curb is Broken out on Left side st.

4+50

7970	79.2	79.9	80.5	80.8	80.7	81.26
TOP	26	13		13	26	26
Curb	Gut.				Gut.	TOP
						curb

4+00

7888	78.5	79.1	79.7	80.1	80.0	80.64
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

3+50

7810	77.8	78.4	78.9	79.2	79.1	80.12
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

TR

79.01

3+00

7717	76.8	77.4	78.0	78.2	78.3	78.87
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

2+50

7625	75.8	76.3	76.8	77.1	77.1	77.79
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

2+00

7506	74.7	75.4	75.7	76.0	76.0	76.68
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

1+50

74.22	73.6	74.2	74.8	75.0	74.9	75.48
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

1+00

73.03	72.3	73.3	73.7	73.9	73.7	74.42
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

L. & R.

TP - NE 7 c.T. Franklin & Sampson 82.05

0-10 cont.

80.33	79.68	83.06	83.74	84.32
90	90	40	90	90
TOP	Gut.	TOP	Gut.	TOP
Curb		Curb		Curb

0-10 Ely. Curb line Sampson

81.96	81.25	81.42	81.66	81.92	82.09	82.23	82.56
40	40	26	13		13	26	40
TOP	Gut.						Gut.
Curb							

0-30 = & Sampson

80.08	81.52	81.75	81.96	82.10	82.32	82.64	83.03	84.22
90	40	26	13		13	26	40	90

0-50 cont.

80.22	69.66	83.72	84.32
90	90	90	90
TOP	Gut.	Gut.	TOP
Curb		Curb	Curb

0-50 Wly. Curb line sampson

81.97	81.27	81.45	81.65	81.83	82.01	82.20	82.43	83.01
40	40	26	13		13	26	40	40
TOP	Gut.						Gut.	TOP
Curb							Curb	Curb

Curb Return South side

82.37	82.98	82.30	82.97	82.36	82.98
BC	BC	Mid Pt.	Mid Pt.	EC	EC
Gut.	TOP	Gut.	TOP	Gut.	TOP
	Curb		Curb		Curb

Curb Return North side

81.36	81.95	81.38	81.97	81.32	81.99
BC	BC	Mid Pt.	Mid Pt.	EC	EC
Gutter	TOP	Gut.	TOP	Gut.	TOP
	Curb		Curb		Curb

5497 to 6400 = Curb broken out on R. side St.

64003 west line sampson St. & Wly. Edge Conc. Paving

81.96	81.36	81.78	82.08	82.17	82.23	82.36	82.98
TOP	26	13		89	13	26	26
Curb	Gut.			TOP		Gut.	TOP
				water			Curb
				Valve			

TP

82.06

5150

81.18	80.7	81.4	81.9	82.1	81.9	82.43
26	26	13		13	26	26
TOP	Gut.				Gut.	TOP
Curb						Curb

2+12.73 = wly. line 28th st

83.0

83.0

83.3 83.89

13

26
Gut. TOP
curb

1+79 = 90° To Prop. cor. on left

82.9/82.3 82.7

83.0

83.2

83.2

83.72

26
TOP
Curb26
Gut

13

13

26

26

TP: 7' C.T. S.Wly. 28th Franklin 84.26Gut. TOP
Curb

1450

82.78

82.4

82.8

83.7

83.2

82.9

83.60

26
TOP
Curb26
Gut

13

13

26

26

1+48.8 = 4 Conc. Drain under side walk 2' wide 4.5' deep

Flowline = 82.93

Gut.

TOP
Curb

1400

82.43

82.1

82.7

83.1

83.1

82.8

83.17

26
TOP
Curb26
Gut

13

13

26

26

0+50

82.24

81.7

82.4

82.8

82.8

82.6

83.20

26
TOP
Curb26
Gut

13

13

26

26

0+41 TO 0+49 Curb Broken out on left

Gut. TOP
Curb

0+40 TO 0+47 Curb Broken out on Right

0400

81.93

81.32

81.75

82.19

82.34

82.42

83.12

26
TOP
Curb26
Gut

13

13

26

26

North East Curb Return

81.32

82.00

81.37

81.88

81.34

81.91

BC
GutBC
TOP
CurbMid pt.
Gut.Mid pt.
TOP
CurbEC
Gut.EC
TOP
Curb

South East Curb Return

82.46

83.03

82.38

83.01

82.42

83.13

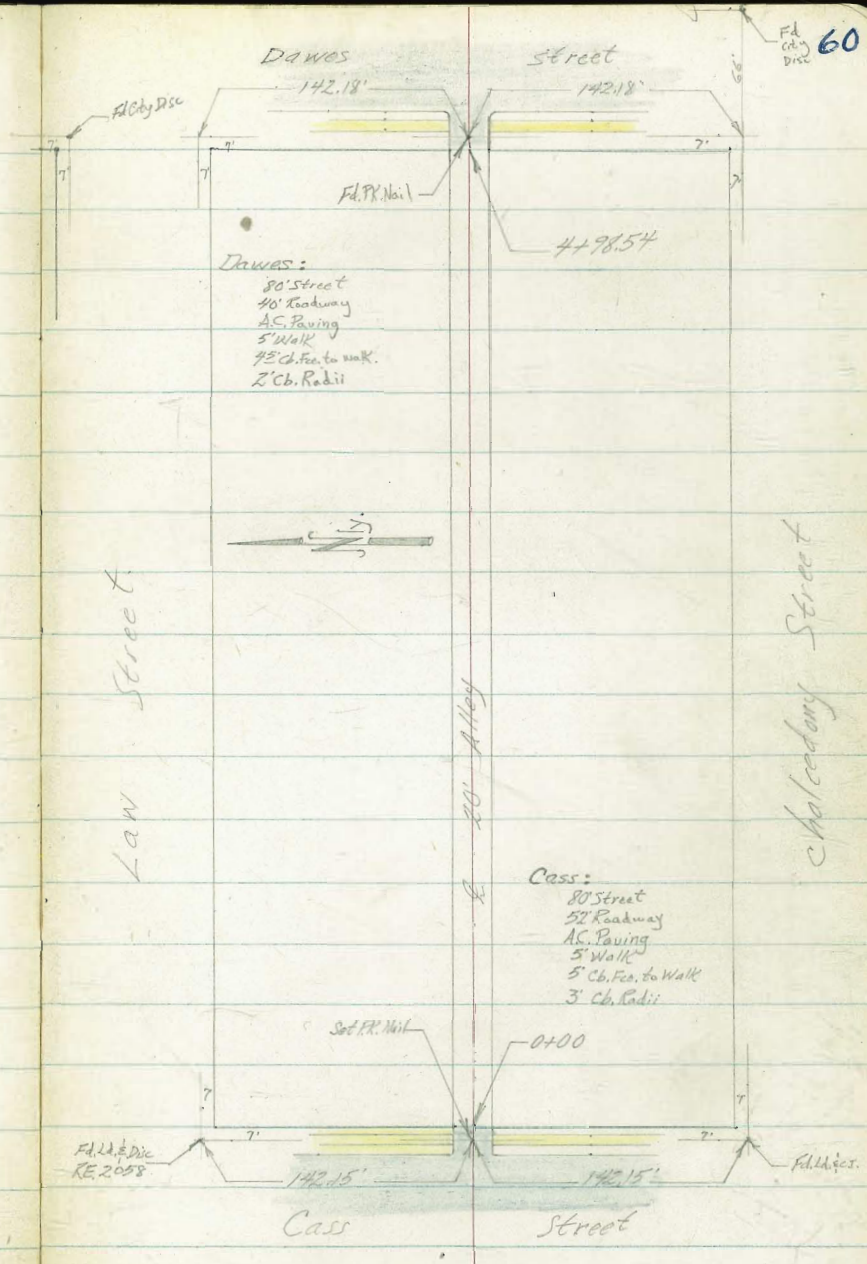
BC
Gut.BC
TOP
CurbMid pt.
Gut.Mid pt.
TOP
CurbEC
Gut.EC
TOP
Curb

Roberts
Cota
Bunker
O'Neil
12-10-54
WA# 52447

X-Section Alley B/K 113, Pac. Bch.

Map 1042

INDEXED
MER
DEC 14 1954



0+37 9² Lt begin opening in garage

66.09
2.78
92
conc
Floor

0+32.5 9⁹ Lt End opening in

66.11
2.76
92
conc
Floor

0+15 10 Lt begin opening in garage

Entrance
doorway

66.09
2.78
10
conc
Floor

65.2
3.7

65.2
10

64.5
4.4
15

0+01 10 Lt begin GARAGE

0+00 East Line of Cass

64.52
4.35
92
cb

64.36
4.51
92
cut

63.93
4.94
102
cut

63.93
4.94
102
cut

64.11
4.76
102
cb

East Curb-Line Cass 0-14

65.19
3.68
50
cb

64.53
4.34
50
cut

64.45
4.42
13
cb

63.80
5.07
13
cut

63.52
5.35

63.27
5.60
13
cut

63.95
4.92
13
cb

62.47
2.40
50
cut

63.12
5.75
50
cb

Q Cass Street 0-10

65.04
3.13
50

64.02
4.85

63.12
5.75
50

BM

932 68.87

SW 71 C.T.

59.55 Cass & Chalcedony

68.87

1+25

9^L Rt begin wooden fence.T.P. 613 73.55 π 145 67.4273.55 π

1+00

9^o Rt + center Pole #PA101067.3
16
2567.3
16
1067.0
1967.9
2.0
1066.7
2.2
25

0+99.5

9^E Lt End Conc Apron67.42
145
195
conc67.43
144
95
conc

0+81

9^L Lt End GARAGE; begin conc. apronto other
entrances.66.53
2.34
148
conc
Near
Edge
Entrance66.97
1.90
96
conc

0+77

9^o Rt. to deadman

0+54.8

9^L Lt End opening in garage66.16
271
93
conc
floor

0+50

66.2
27
98
dirt66.2
2766.0
2.9
1065.4
3.5
2568.87 π 68.87 π

3+00

10² Rt End board fence68.9
4.6
2068.8
4.8
1068.5
5.168.6
5.0
1068.6
5.0
20

2+77

10² Rt & 4 conc. walk68.5
5.1
10
4RD68.09
5.46
10²
CONC67.79
5.76
20²
CONC

2+70

10² Rt begin board fence68.8
4.8
2068.5
5.1
1068.2
5.468.2
5.4
1068.0
5.6
12

2+49.5

9² Rt to center P.Pole # PA1050

2+32

13⁸ Rt & Single Garage68.03
5.52
13⁸
CONC
Floor

2+00

10² Rt to wooden fence68.7
5.2
2068.2
5.4
1068.0
5.668.0
5.6
1067.8
5.8
20

1+50

68.2
5.4
2567.9
5.7
1067.6
6.067.7
5.9
1067.2
6.4
20

73.55 T

73.55 T

T.P. 489 77.18 ∇ 126 72.29

4+00 { 92 Rt to center P. Pole # PA1080*
 98 Rt End wire fence & conc. base

4+92 98 Rt ^{begin} wire fence on conc. base.

11.6	11.1	11.4	11.3
2.0	2.2	2.2	2.3
20	10	10	20

3+72 12" Rt End apron $\frac{1}{2}$ garage

70.77	71.01
278	254
12" conc	15" Floor

3+77 12" Rt begin conc apron 2nd garage

70.70	71.01
285	254
12 conc	15" Floor

3+75 98 Rt End board fence

3+50

70.0	69.8	69.6	69.6	69.4
3.6	3.8	4.0	4.0	4.2
20	10	10	10	20

3+24 98 Rt begin board fence.

3+08 20" Rt @ Single garage

68.96
459
20" conc
Floor

73.55 ∇ 73.55 ∇

check 7.78 69.40 = 69.38 SEE BP chalcidony & Dawes

5+38.54 Q Dawes 73.07 4.11 5.01 72.17 71.16 6.02 5.0

5+18.54 West Curb Line of Dawes 72.88 72.32 72.25 71.85 71.70 71.42 71.93 70.76 71.34
 4.32 4.84 4.93 5.33 5.48 5.76 5.25 6.42 5.84
 4.5 4.5 12 12 12 12 12 4.5 4.5
 cb cut cb cut cut cut cut cb cut cb

4+98.54 (10³ Rt End Conc. base West Line Dawes Street) 72.49 72.15 72.16 71.87 72.18 71.9 73.0
 4.89 5.03 5.02 5.31 5.00 5.3 4.2
 10 10 10 10 10 10
 cb cut cut cb cut cut top

4+92^E 10³ Rt End board fence

4+85 13 Lt to garage opening to East 73.21 3.97 1.3 Floor conc.

4+50 72.6 72.5 72.0 72.4 72.3
 4.6 4.7 5.2 4.8 4.9
 15 10 10 10 15

4+49 10³ Rt begin board fence on conc. base 72.1 71.9 72.4
 5.1 5.8 4.8
 10³ GRD 10³ Foot 10³ Top
 Conc. Conc. Conc.

77.18x

77.18x

Re-x-sec Alley BIK 6, Ocean Beach
 Sec FB 1810 - 13 for sketch +
 add'l information
 2/1/55 - C. Allen, D. Sisson, C. Powell

TBM. 0.99 197.45 - 8.77 196.46

0+04 - 10° RT = opens to SELY Guizot ST
 Conc Drive - 2 car garage

NWly end alley curbs
 0+00 - NWly line Guizot + edge conc pave

0-10 - 10° LT + 10° RT = Curb Ret B.C.s 2' Rad

Conc Alley Apron
 0-12 = NWly Curb line Guizot ST

TP, 0.56 205.23 - 13.34 204.67

BM - 0.03 218.01 217.98

INDEXED
 FEB 16 1955

20' Alley RT: NELY. 66

197.45 T

Lat. 2 Alley BIK 6 + NWly 7' Line Guizot ST

Notes reduced,
 Reynolds 2/23/55

197.23

800
 10 2
 Floor

197.45	197.03	196.53	196.60	196.68
728	820	820	863	855
10° T.C.	10° 9UT	10° 9UT	10° T.C.	10° T.C.

197.91	196.80	196.26	196.67
792	843	897	856
10° T.C. BC	10° 9UT BC	10° 9UT BC	10° T.C. BC

198.64	198.14	197.38	196.91	196.77	196.40	196.09	196.05	196.54	193.94	196.85
659	709	785	832	846	883	914	918	868	1129	1066
50 T.C.	50 9UT	12° T.C. EC	12° 9UT EC	10	10	10	12° 9UT EC	12° T.C. EC	30 9UT	50 T.C.

205.23 T

SWly BP - Guizot + Del Monte Ave

0+74- 10² RT = end Conc Drive

19556	19567
189	178
102	131
Drive	Floor

0+60- 10⁵ RT = begin Conc drive 2 car garage

19566	19573
179	172
105	131
Drive	Floor
	Conc

10² LT = begin 8" tile wall - 6' high
0+50- 10² LT = end 6' high picket fence

1955	1966	1966	1962	1962	1963	1955
2 ²	02	02	13	3	2	2 ²
10 ²	10	8.5	8	10	25	
Foot						
Wall						

0+27- 10² LT = begin 6' high picket fence

0+26- 10² LT = end Conc drive

19837	19784
+092	+039
20 ²	10 ²
ON	Drive
Drive	

0+25

19780	1973	1970	1970	1967
+035	02	05	05	08
10 ²	10 ²	10	25	
Drive	ground			

0+24- 10² RT = car frame garage

19945	19793
+200	+048
37 ²	10 ²
90 ² floor	Conc
	Drive

0+18- 10² RT = begin Conc drive

19745

195.08 π

TP 1.17 195.08 3.54 193.91

Spike in power pole # JPA 4520 - 8° LT Sta 1725

10° RT = begin conc block wall (4' high)
1+50 10° RT = end picket fence

1924	1919	1919	1915	1915	1916	1919	1921	1921	1921	1921	1921	1921	1921
5 ¹	5 ⁶	5 ⁶	6 ⁰	6 ⁰	5 ⁹	5 ⁶	5 ⁴	5 ⁴	6 ²	6 ⁷	7 ⁰	7 ⁰	7 ⁰
25	10	7.6			6	6 ²	10	10 ²	10 ²	10 ²	10 ²	10 ²	25
									9 ⁴	Foot	Foot		

10° LT = begin picket fence - 4' high
8° LT = 10" power pole # JPA 4520
1+25 10° LT = end 8" Tile wall 6' high

1928	1937	1937	1932	1927	1926	1926	1929	1929
4 ²	3 ⁸	3 ⁸	4 ²	4 ⁸	4 ⁹	4 ⁹	4 ⁶	4 ⁶
10 ²	10 ²	10	6 ⁵	6		7	7 ⁵	10
Foot	9 ⁴							

1+00 - 10° RT = begin 4' picket fence

1950	1947	1943	1939	1938	1938	1938	1933
2 ⁵	2 ⁸	3 ¹	3 ⁶	3 ⁷	3 ⁷	3 ⁷	4 ²
25	10	6 ⁵	6		8	10	25

0+95 - 10° LT = 2⁵ opening in wall
2⁵ wide conc walk

19467
278
10°
walk

0+75

1956	1954	1950	1950	1950	1953
1 ⁹	2 ¹	2 ⁵	2 ⁵	2 ⁵	2 ³
10	7 ⁵	7		8	10

197.45 π

X-Sec Alley BIK 6 cont

2+49-10⁵ RT = Car single garage (see below)

Opens to Sly-

Garage Parallel to Alley + Has Conc Foundation

2+29-10² RT = Car single garage - DIRT Floor

2+25

2+19-30⁰ RT = 1 single garage - DIRT Floor

2+00-10² RT =

Wall is 5' high
end conc block wall.

1+94-13⁹ LT = 1

Conc Floor
Single garage

1+75-10¹ RT = 1 gateway thru block wall.

1+63-10⁵ LT = end picket fence

LT = SWly

RT = NELY

69

188.4

6⁷

10²
DIRT Floor

187.6	187.6	187.3	187.4	187.4	188.3
7 ⁵	7 ⁵	7 ⁸	7 ⁷	7 ⁵	6 ⁸
10	7	6		8	10

188.7

6⁴

30⁰
DIRT Floor

189.5

5⁶

25

189.3

5⁸

10

189.0

6¹

189.7

5⁹

7

189.9

5²

8

189.8

5³

10

189.8

5³

10²

189.8

6¹

10²

189.8

6¹

10²

9' at FOOT
Wall

190.1

5⁰⁰

13⁹

Conc
Floor

190.7

4⁴

10

190.4

4⁷

190.8

4³

10

190.89

4¹⁹

10¹

Top base
of wall

195.08 T

X-sec Alley BIK 6 cont

3+23-12² RT= Conc Apron + floor
end 2 car garage.

3+06-12³ RT= begin double garage
Conc Floor + Apron

T.P. 3.52 185.73 12.87 182.21

3+00 = Sewer Manhole
10⁵ LT = begin low conc block Retaining Wall

2+75

2+64-27⁵ RT= double garage - Conc
Floor + Apron

2+50⁵ - 7⁵ LT = 2 10" concrete pile # JPA 4538

2+50

LT = SWLY

RT = NELY

70

182.95
27⁸
12⁰
Conc
Apron

184.36
137
19¹
Conc
Floor

183.37

184.43

236

130

12³
Conc
Apron

19¹
gar
Floor

185.73 X

182.54	181.0	182.6	182.6	182.4	183.01	183.0	183.9	184.6
12 ⁵	14 ¹	12 ⁵	12 ⁵	12 ⁷	12 ⁰⁷	12 ¹	11 ²	10 ⁵
25	10 ⁵	10 ⁵	10	7	R. 177 SMTH.	7	10	25
Top Foot Wall	10 ⁵	10 ⁵	10	7				
	grat	grat						
	Wall	Wall						

184.2	184.4	184.7	184.3	184.6	184.9
10 ⁹	10 ⁷	11 ⁰	10 ⁸	10 ⁵	10 ³
10	7	6		8	10

18646	187.36
862	772
275	480
Conc Apron	Conc Floor

185.6	186.2	186.2	185.7	185.8	186.0	186.8	187.0
9 ⁵	8 ⁹	8 ⁹	9 ⁴	9 ³	9 ¹	8 ³	8 ¹
25	10	7	6		8	10	25

195.08 X

10^3 LT = begin Conc block wall
 $3+77-12^3$ LT = end 2 car garage Conc block + Apron

	177.68	177.76	176.9	180.6	178.2
80 ⁵	797	88	51	75	
20 ²	12 ³	10 ³	10 ³	10 ³	
Conc Floor	Apron	Foot	Top Wall	9 ² at Wall	

3+75

	178.0	178.5	177.8	180.1
7 ²	7 ²	6 ²	5 ⁶	
10		6	10	

and begin 2 car garage - Conc Apron + Floor
 $3+61-12^3$ LT = end Conc block wall

	177.71	178.46	177.8	180.68	178.6
80 ²	723	72	505	71	
20 ²	12 ³	12 ³	12 ³	12 ³	
Floor	Apron	Foot	Top Wall	9 ² at Wall	

178.1
 7⁶
 10⁴
 Foot

8^2 LT = 2 10" power pole # PA4560
 12^1 LT = begin Conc block wall } To
 $3+50-10^4$ LT = end Conc block wall } Show 5' in Wall

	178.6	180.49	180.0	180.0	179.8	179.5	179.7	180.2	181.1	181.4
7 ¹	5 ²⁴	5 ⁷	5 ⁷	5 ²	6 ²	6 ⁰	5 ⁵	4 ⁶	4 ³	
11 ⁰	10 ⁴	10 ⁴	10 ⁰	7	6		7	10	25	
7 ^{at} Top Wall	7 ^{at} Top Wall	7 ^{at} Top Wall								

$3+39-10^0$ RT = begin 6' high board fence on Top of Conc Retaining Wall - Retaining Wall -

	181.0	181.1	180.8	181.0	181.4	182.4	181.5	183.0
4 ⁷	4 ⁶	4 ²	4 ²	4 ³	3 ³	4 ²	2 ⁷	
10	8	7		8	10 ⁰	10 ⁰	10 ⁰	
					9 ² at Wall	Foot	Top Wall	

$3+25-10^0$ RT = begin Low Conc

185.73 X

Alley BIK 6 cont

LT = SWLY

RT = NELY

72

175.55 π

TP - 2.19 175.55 12.37 173.36

Nail in picket fence - 11⁵ LT station 4+49

4+55. 20⁵ LT = Conc floor & single garage

172.75
12⁹⁸
20⁵
conc
floor

4+50

173.2 172.9 172.9 173.4
12⁵ 12⁸ 12⁸ 12³
10 10 10 25

4+25

175.4 175.0 175.2 176.4
10³ 10⁷ 10⁵ 9³
10 7 10

4+00-10² LT = end conc block wall

175.6 180.5 176.7 177.3 177.3 176.7 177.0 177.5 179.0 180.2
10¹ 5² 9⁰ 8⁴ 8⁴ 9⁰ 8⁷ 8² 6⁷ 5⁵
25 10² 10² 10² 10⁰ 7 8 8 10 25
Top wall Foot 9-9T wall

3+99-10⁰ + 6' high conc block wall - RT = end Conc Retaining Wall

179.0 178.6 180.7
6⁷ 7¹ 5⁰
10⁰ 10⁰ 10⁰
9² Foot Top wall

185.73 π

5+25-10⁴ LT = end 4⁵ high Tile Wall

168.7	168.6	168.6	168.3	167.7	167.7	167.5	168.2	168.2
6 ⁹	7 ⁰	7 ⁰	7 ³	7 ²	7 ²	8 ¹	7 ⁴	7 ⁴
10 ⁴	10 ⁴	10	8	7		7	10	25
Foot	grat	Wall						

Floor + Apron
5+20-22³ RT = end 2 car garage. Conc

169.25	169.40
6 ³⁰	6 ¹⁵
22 ³	24 ³
Apron	Floor

Conc Apron + Floor
5+01-22³ RT = begin 2 car garage -

169.22	169.39
6 ³³	6 ¹⁶
22 ³	24 ³
Apron	Floor

5+00

170.1	170.3	169.5	169.2	169.2
5 ⁵	5 ³	6 ¹	6 ⁴	6 ⁴
25	10		10	25

4+75

171.4	171.7	171.1	170.7	170.3
4 ³	3 ⁹	4 ⁵	4 ⁹	5 ³
25	10		10	25

4+73.10² LT = begin 4⁵ high Tile wall

170.7	172.0
4 ⁹	3 ⁶
10 ⁷	10 ³
Foot	grat
	Wall

175.55 RT

X-sec Alley BIK 6 cont

5497

LT = SWLY

RT = NELY

154.5	155.4	154.8	154.7	160.8	156.7	154.7
8 ²	7 ³	7 ²	8 ⁰	12 ²	6 ⁰	8 ⁰
10	7		6	7	10	25

Sec 3 Ketch FB 1810-13
Conc steps

5491 - 11¹ LT = Near corner of 3' wide

156.56
6¹₃
11¹
Conc steps

5490

157.9	158.3	157.4	156.7	156.4	162.0	162.4	158.1
4 ⁸	4 ⁴	5 ³	6 ⁰	6 ³	0 ⁷	0 ³	4 ⁶
15	10	7		5	7	10	25

5482 - 10⁸ LT = NELY end of lateral conc

block wall.

161.3	163.4	162.0
1 ⁴	+0 ⁷	0 ⁷
10 ⁸	10 ⁸	10 ⁸
Foot	Top	Foot
	Wall	Wall

TP 0.43 162.69 13.29 162.26

162.69 π

5470

163.9	163.7	163.1	161.9	161.3	161.1	164.8	165.1	165.5
11 ⁷	11 ⁹	12 ⁵	13 ⁷	14 ³	14 ⁵	10 ⁸	10 ⁵	10 ²
25	10	8	7		6	7	10	25

5450

165.1	165.3	165.2	165.1	166.5	166.5	166.6
10 ⁵	10 ³	10 ⁴	10 ⁵	9 ¹	9 ¹	9 ⁰
25	10		7	9	10	25

5426 - 8⁸ LT = ϕ 12" power pole # PA 4590

175.55

X-sec Alley BIK 6 cont

LT = SWly

RT = NEly
Alley

75

See FB 1810 for sections on curbs

↓ Froode ST - No change

Levels checked into levels in

FB 1810 -

15332
 151.59 ?
 937
 11 1/2
 edge 3' wide
 Conc steps

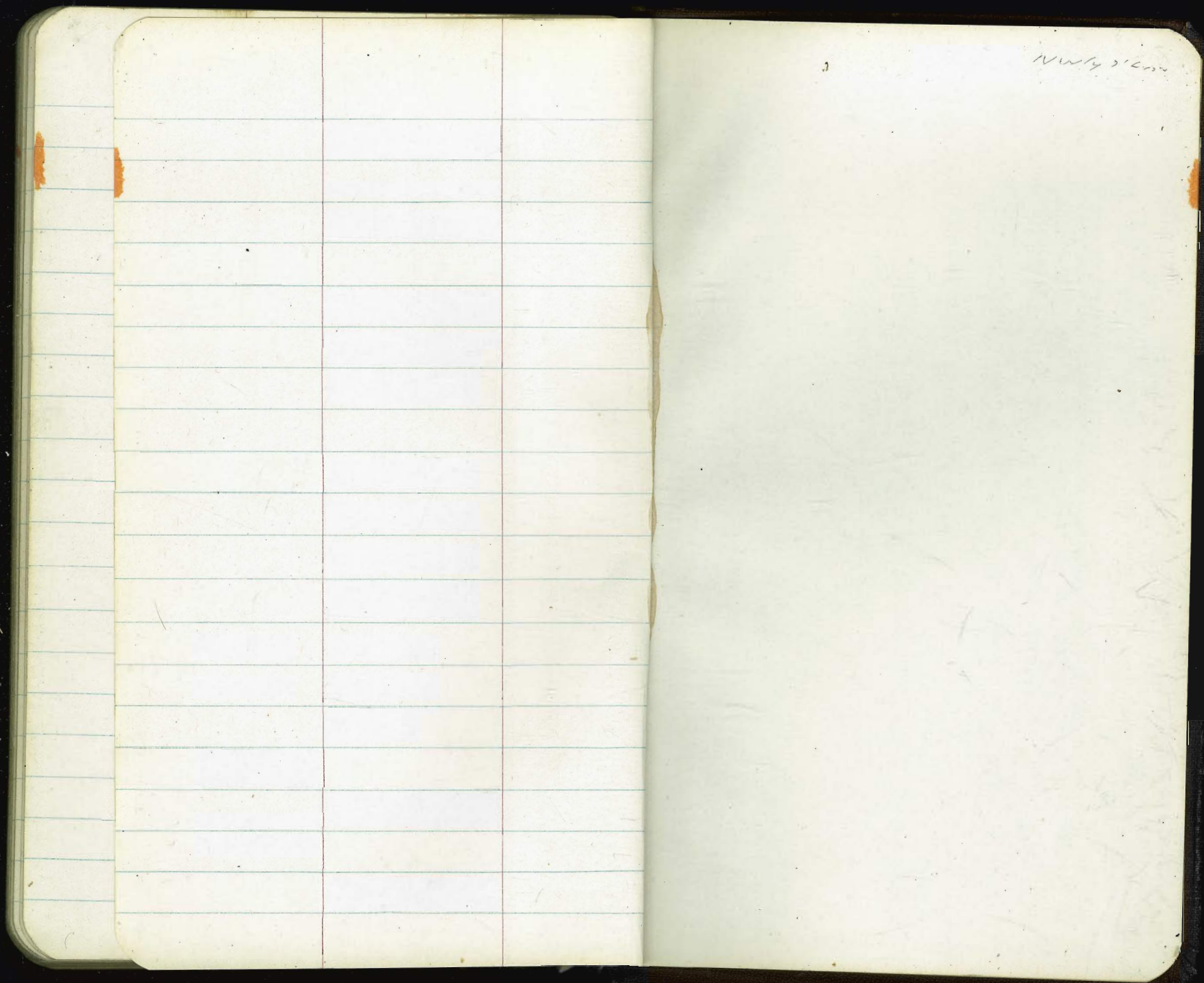
152.52 152.77
 10'7 9'92
 9'9 9'9
 9'07 7'02

A.C. is covered with dirt

ST 9923 = SEly line of Froode = edge A.C. Pav

153.24	152.86	153.5	154.3	154.3	152.46	154.3	154.9	154.7
945	983	92	84	84	1023	84	78	80
102	102	10	8	DIRT	2	6	7	92
Topcb	907	DIRT			A.C.	DIRT	DIRT	DIRT
								DIRT over curb

162.69 T



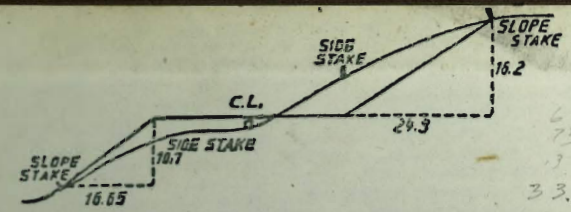
11/14/2000

83 21
 51 03
 83 19
 134 24
 48 95

20090

Dawson & Caldwell
 SEBP - 69.34

30
 13
 27



60
 72
 32
 33.54

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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