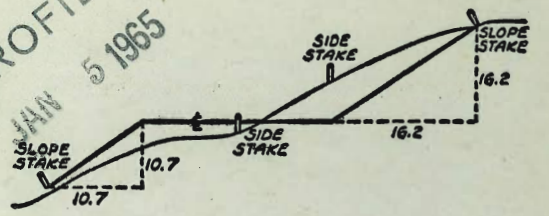
2269

SEWER



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

-Index-

Sewer - Prelim Blk 149 - Choates Add. 1-6.

Prelim Sewers - Swan's Add. 7-32.

Realign Sewer " " 34-42

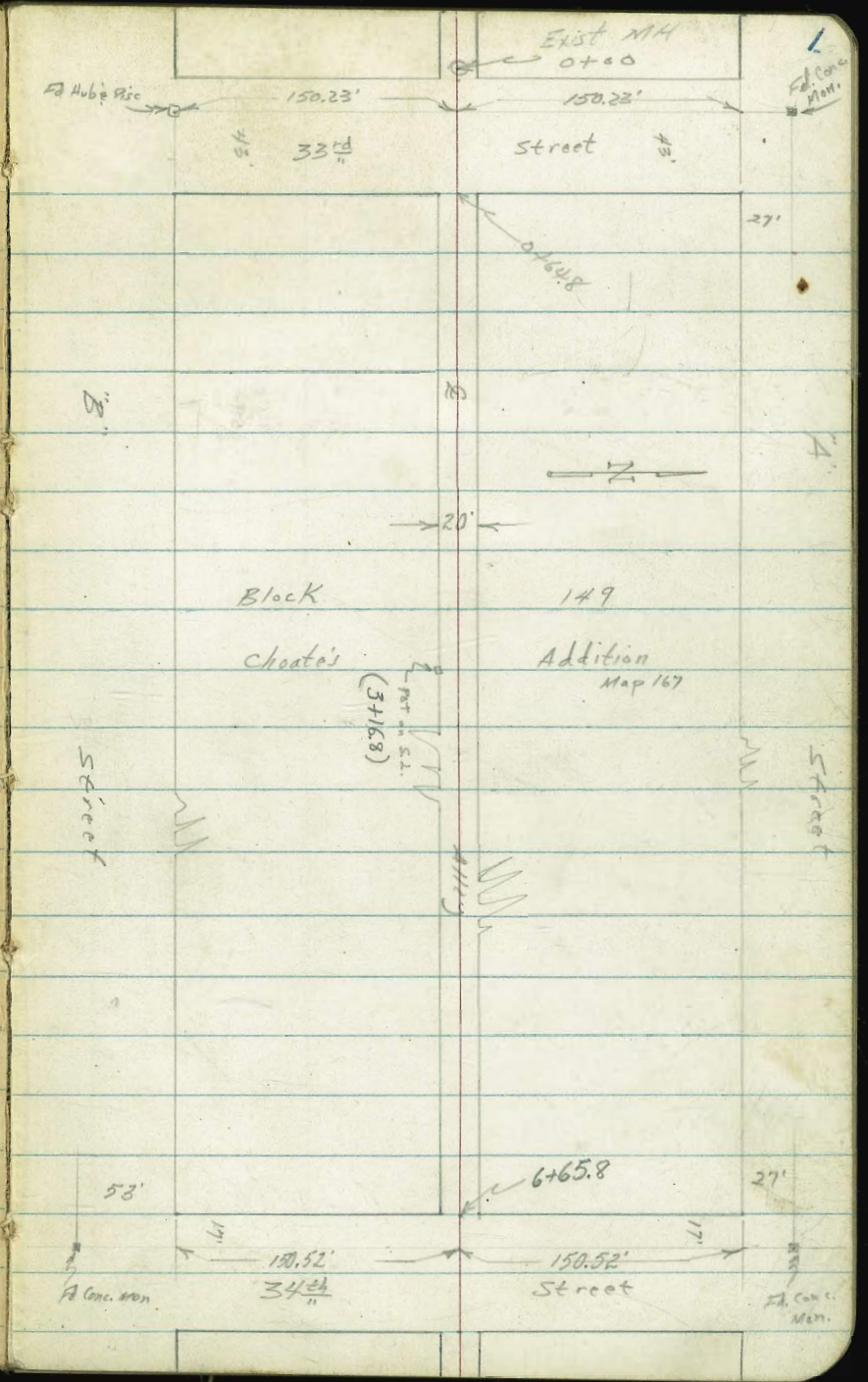
Re-x-sec Alley Blk 20 Swan's add - 65

Roberts
Cota
Pollen
Chipman
8-19-52
W.O. #62258

Prelim. Sewer Survey Blk 149
Cheates Addition

T.P. 104

INDEXED
Sadie
AUG 21 1952



Contd From Page 1

0+50				
T.P.	12.27	152.68 ℄	0.98	140.41
0+40				
0+26				
0+20				
0+00	Exist M.H.			
T.P.	0.84	141.39 ℄	11.73	140.55
T.P.	0.39	152.28	13.06	151.89
BM	2.52	164.95		162.43 N.E. Mon. 33 cm ℄ "A"

℄

134.7		141.7
18.0		10.8
Bot. Ditch		GRD.
	152.68	
132.6		141.7
8.8		0.7
Bot. Ditch		GRD.
131.2		135.7
10.2		8.7
Bot. Ditch		GRD.
130.8		130.8
10.6		10.6
Bot. Ditch		GRD.
133.24	133.3	131.4
8.15	14.0 ℄	9.0
℄M	INVERT	GRD
	141.39	

Doubtful as to BM (Could only find Conc. Mon. shown on pg. 1.)

Cont'd From Page 2

2+10				
T.P.	12.78	175.84 ⊼	0.32	163.06
1+90				
1+67				
T.P.	11.42	163.38 ⊼	0.72	151.96
1+07	End of Diggings.			
0+85				
		152.68 ⊼		

℄

166.5 — 9.3 — 175.84 ⊼

162.3 — 1.1 — 159.6 — 3.8 — 163.38 ⊼

141.1 — 11.6 Bot. Ditch — 153.5 — 0.2 GRD

1380 — 14.7 Bot. Ditch — 149.3 — 3.4 GRD. — 152.68 ⊼

Contd From Page 3

4+62				
4+22				
3+65				
3+36				
2+60				
T.P.	11.83	186.82 ℄	0.85	174.99
2+40				
		175.84 ℄		

				184.6
2+22				
				183.8
3+00				
				183.5
3+33				
				182.2
4+66				
				176.4
10+4				
		186.82 ℄		
				177.6
3+2				
		175.84 ℄		

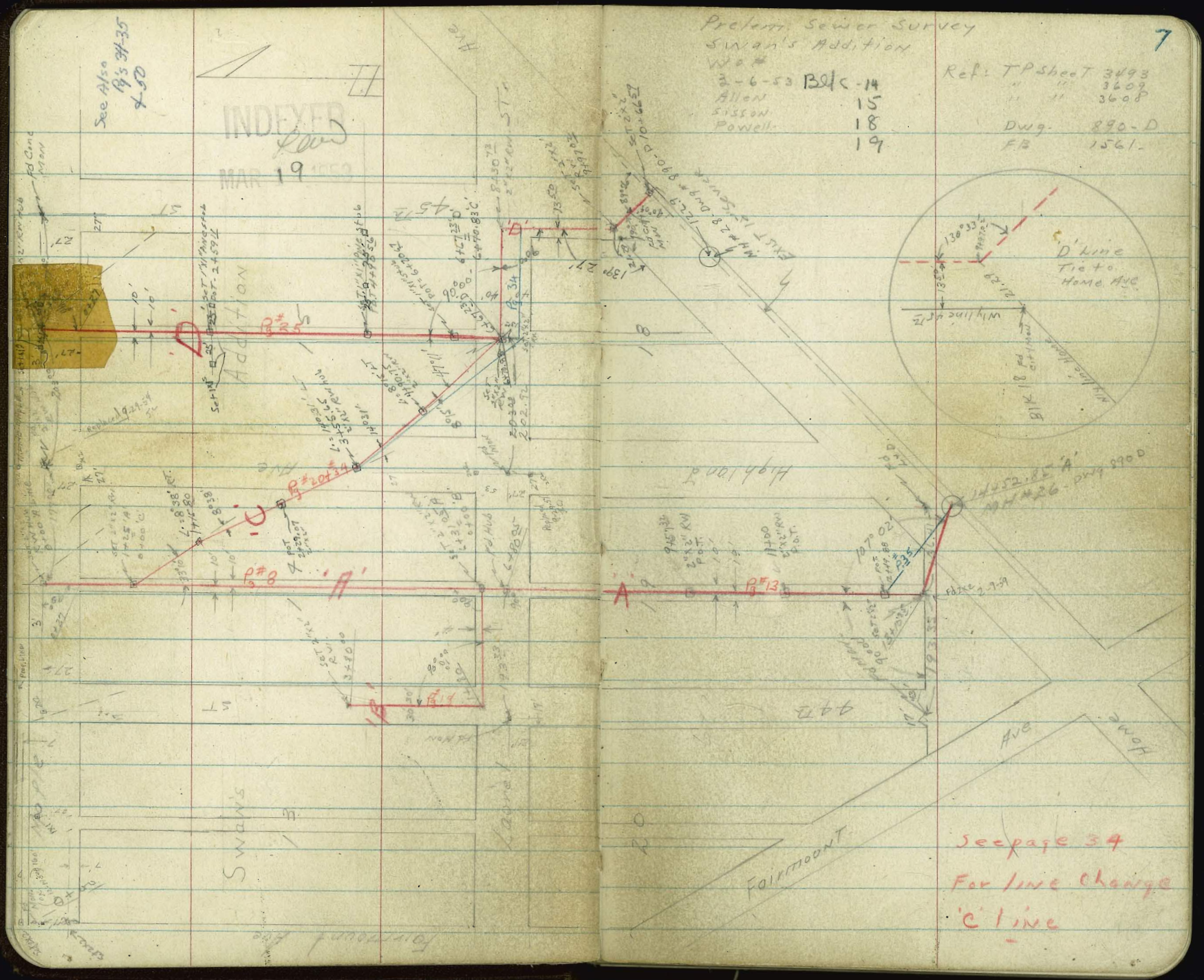
Contd From Page 4

					E
					3.18
7+15					8.5
					0.38
6+75					7.8
					4.68
6+35					3.4
					8.28
6+00					2.0
					0.28
5+55					2.2
T.P.	3.36	189.63 T	0.35	186.47	189.83 T
					0.38
5+12					0.2
		186.82 T			186.82 T

Contd From Page 5

T.P.			13.04	162.39 = 162.43	?? on this bench!
T.P.	0.38	175.43	12.97	175.05	
T.P.	1.45	188.02	3.26	186.57	
8+00					
		189.83 ℄			189.83 ℄

173.7
16.1


Preliminary Sewer Survey
Swan's Addition
W.O.#
2-6-53 BS# C-14
Allen 15
Sisson 18
Powell 19
Ref: TP Sheet 3493
" " 3609
" " 3608
Dwg- 890-D
FB 1561
7
See Also
P's 34-35
& 50
INDEXED
MAR 19
D' Line
Tie to
Home Ave
Swan's
Addition
Fairmount
Ave
Seepage 34
For line change
'C' line

Levels. Sewers Swan's Add.
See page 7 for sketch.
'A' Line in alleys Blks 14 and 19-

0+45				
0+25				
TP4	0.11	240.75	11.91	240.64
0+00 A = ℄ Alley Blk 14 and 27' North of South line Maple				
0-13 = ℄ Alley and ℄ Maple				
TP3	0.03	252.55	13.17	252.52
TP2	0.29	265.69	13.03	265.40
TP1	0.49	278.43x	12.51	277.94
	10.28	290.45		

N.W. BP. Fairmount & Maple
280.17

'A' Line

Lt = Ely — ℄ — Rt = Wly

240.7
0 1
10

231.7
9 1

246.7
14 1
11
Bottom Creek

240.3
0 1
10

235.3
5 1

227.8
13 0
23
Bottom Creek

240.75 T

252.5
0 1
25

245.21
7 3/4
on hub

232.1
20 5
33
Bottom of Creek

247.9
4 2

252.55

1+50

1+25 'A' = 0+00 'C' Line - L. = 33°10' LT

Nail in anchor pole 11' RT 1+25

TP5 6.36 233.93 13.18 227.57

1+27 - 9° Rt = ℄ Anchor pole

1+00

0+75

0+50

A Line

LT = Elv ℄ Rt = Elv

217.8	222.9		229.4	234.6
16 1/2	10 0		4 1/2	+0 2
12			10	20
Bottom Creek				
226.7	223.8	221.77	223.4	228.7
7 0	10 1/2	12 1/2 16	10 1/2	+0 1/2
20	10	on Hub Bottom Creek Gr = 12 1/2	10	20

233.93 ℄

233.7	224.8	222.8	
7 1/2	16 0	18 0	
10		4	
		Bottom Creek	
237.8	227.8	224.6	227.2
3 0	13 0	16 1/2	13 1/2
10		12	20
		Bottom Creek	
	232.6	226.3	
	8 1/2	14 1/2	
		12 0	
		Bottom creek	

240.75 ℄

					Lt. Ely	℄ Line	Rt. Wly
1	TP7	9.72	255.05	0.30	245.33	255.05 x	
						231.1 / 14.5 / 10	233.2 / 11.4	237.8 / 7.8 / 10
1+	2+18						
						236.6 / 14.0 / 10	235.9 / 9.7	239.7 / 5.9 / 10	243.9 / 1.7 / 20
No. 11							
TL	2+00						
1							
1	TP6	11.75	245.63	0.05	233.88	245.63 x	
						222.2 / 11.1 / 20	226.6 / 7.3	231.9 / 2.0 / 10
0	1+80						
							224.3 / 9.6
0	1+65						
						233.93 x	

4+00				
TP8	11.86	265.61	1.30	253.75
3+50				
3+03 - 9.5 rt-k 10" Power pole #2557				
3+00				
2+75				
2+50				

4+00

Lt=e/y

253.1 — 12.5 / 10

254.7 — 10 — 9

Rt=w/y

256.3 — 9.3 / 10

264.3 — 1.3 / 5.0

TP8 265.61

3+50

249.1 — 6.0 / 10

257.3 — 3 — 8

253.5 — 1.6 / 10

3+00

242.8 — 12.3 / 10

246.9 — 8.2

250.9 — 4.2 / 10

253.4 — 1.7 / 20

2+75

240.1 — 15.0 / 10

242.9 — 11.2

247.9 — 7.2 / 10

251.5 — 3.6 / 20

2+50

238.5 — 16.6 / 10

241.6 — 13.5

244.6 — 10.5 / 10

248.8 — 6.3 / 20

255.05

6+00

5+50

5+30

5+16 · 9.5 Rt = ℄ Deadman

TP9	6.04	271.50	0.15	265.46

5+25 - 9.5 Rt = ℄ Power Pole # 2519

5+00

4+50

4+26 - 9.5 Rt ℄ 16" power pole # 2523

LT = ℄

258.3	263.5			
13.2	7.9	7.0		
50	10			
261.8	263.7			
9.7	7.8			
10				
258.1	260.6	262.7		
13.4	10.9	8.8		
25	10			
256.4	257.8	261.4		
9.2	5.5	4.2		
25	10			
253.8	256.2	258.4		
11.8	9.4	7.2		
25	10			

271.50 ℄

RT = WLy

268.5	265.3	268.8		
7.0	6.2	2.7		
10	10	50		
263.7	265.4			
7.8	6.1			
10				
262.7	264.5	265.4		
8.8	7.0	2.1		
10	10	50		
261.4	263.6	268.3		
4.2	2.0	2.7		
10	10	35		
258.4	260.4	265.0		
7.2	5.2	0.6		
10	10	35		

265.61 ℄

Station					LT = Ely				℄ A			Rt = Wly	
8+50							250.3 / 9^{7} / 10		250.6 / 9^{4}	251.2 / 8^{8} / 10			
8+00						254.5 / 5^{5} / 50	257.4 / 2^{6} / 10		257.2 / 2^{8}	257.2 / 2^{8} / 10	255.7 / 4^{3} / 40	252.8 / 7^{2} / 65	
TP10	1.65	259.99	13.16	258.34					259.99 ⊼				
7+50						260.0 / 11^{5} / 50	260.0 / 11^{5} / 10		259.7 / 11^{8}	259.6 / 11^{9} / 10	258.6 / 12^{9} / 50		
7+00					255.7 / 15^{8} / 100	260.1 / 11^{4} / 70	261.7 / 9^{8} / 50	262.2 / 9^{3} / 10	262.3 / 9^{2}	262.1 / 9^{4} / 10	262.5 / 9^{0} / 50	261.7 / 9^{8} / 85 Top Canyon	
$6+80^{05}$ ℄ Alley + 27' North of South line Laurel						255.5 / 16^{0} / 100	261.4 / 10^{1} / 50		261.4 / 10^{1}	253.7 / 7^{8} / 50		262.5 / 9^{0} / 85 Top of Canyon	
$6+31^{05}$ 'A' = 0+00 'B' Line ∠ = 90°00' LT						259.2 / 12^{3} / 50	263.9 / 7^{6} / 10		264.34 / 7^{16} on hub		265.0 / 6^{5} / 10		

271.50

TP12	0.75	227.78	12.83	227.03
10+50				
10+00				
ON POT 9457.32				
TP11	1.05	239.86	8.64	238.81
9+50				
9+00				
TP11	0.64	247.45	-13.18	246.81

LT = c/y. ℄ 'A' Rt = w/y

227.78 T

226.1 — 13 8 — 20 — ON Steep Slope

227.8 — 12 1 — 10 — 1→25.1

229.2 — 10 7 — 17

230.3 — 9 6 — 10

232.4 — 7 5 — 37 — Top Canyon

232.6 — 12 1 — 50

232.8 — 7 1 — 10 — 1.5:1

234.3 — 5 6 —

235.4 — 4 5 — 10

232.3 — 2 6 — 40 — Top Canyon

239.86 T

236.7 — 10 8 — 50

238.9 — 8 6 — 10

239.8 — 7 1 —

240.0 — 7 5 — 10

240.0 — 7 5 — 5.0 — Top Canyon

242.7 — 4 8 — 50

244.5 — 3 0 — 10

244.8 — 2 7 —

245.2 — 2 3 — 10

243.5 — 4 0 — 50 — Top Canyon

239.8 — 7 1 — 70

247.45

259.99 T

12+49.88	Set 1½" x 14" lath w/Nail P.O.T			
TP,5	1.15	192.32	13.12	191.17
12+00				
TP,14	1.90	204.29	13.10	202.39
11+50				
TP,13	0.93	215.49	13.22	214.56
11+00 - Set 2"x2" RW, Hub P.O.T.				

LT = Cly

℄ Rt = Wty

NEW LINE CONT. on Pg 43

189.24

30.8

ON P.O.T.
Gr. Same

192.32 +

194.6	196.6	198.8	201.0	202.0	204.1
9.7	7.7	2.5	3.3	2.3	0.2
20	10		3	10	20

204.29

201.3	207.3	209.7	211.7	215.3	216.0
14.2	8.2	5.8	3.8	0.2	+0.5
35	10		10	29	40

215.49

214.5	218.8	220.99	222.5	225.3
13.3	9.0	6.79	5.3	2.5
30	10	Hub Gr. Same	10	41 Top Canyon

227.78 +

TP_8	2.20	159.95	12.92	157.75
3+25				
13+10 35 L.	Section taken on split at angle. 72°58' Left - Set 2" x 2" R.W.			
TP_7	1.55	170.67	12.46	169.12
TP_6	1.90	181.58	12.64	179.68
12+80				
12+50 - Break in ℄ grade				

℄ P.

LT = ℄

RT = W℄

159.95 ±

162.6 — 8 1/10 — N℄

158.4 — 12 3 — 165.82 — 4 85 on Hub or same

157.6 — 16 1/10 — S℄ — 165.8 — 4 9/10

164.4 — 6 1/10

170.67 ±

181.58 ±

174.5 — 17 8/10 — 2.0 x 10

178.5 — 13 8 — 181.5 — 10 8/10

184.4 — 7 9/10 — 2.4 x 8 — 186.8 on steep slope

187.2 — 3 1/10 — 189.2 — 0 7/10 — + 2 1/20 — 184.4

192.32

B.M. B.P. Ely Cor. Box Culvert - Fairmount Ely of Home 148.05 (FB 1561) 38

TP 11.90

14+52.85 = SMH #26 Dwg 890 D.

14+32.8 Ely edge H.C. P.T. Home Ave

14+05.4 = Wly edge A.C. p.t. Home ave.

13+95: Top Roadway Fill - Home Ave

13+83: Toe Roadway Fill - Home Ave

13+50 = Ely toe of East + West slope

Lt = N ℄	℄	Rt = S ℄
	150.62	141.91
	9.33 Rim	18.04 IE
150.83	150.38	150.05
9.12 40 AC	9.57	9.90 40 AC
150.86	150.37	150.18
9.09 40 A.C.	9.58 A.C.	9.85 40 A.C.
150.0	150.6	150.6
9.0 40 Top Fill	9.4	9.4 40 Top Fill
	147.0 Inv.	
146.4	146.0	146.0
13.6 40	14.0	14.0 40 Toe Slope

159.95

Levels 'B' Line Swan's Addition

See sketch Page 7.

Lt = S/y

℄ 'B'

Rt = N/y.

1+80 - L. Rt = 90°.00' Section taken 90° to back line

	274.2	258.3	263.28			
	26 2	17 1	12 20 8			
	#9 ℄ Laurel.	25	Hub Gr Stone			
1+40	260.2	263.9	266.5	266.9	272.6	
	25 2	11 5	8 9	8 15	2 8	
	#9 ℄ Laurel	17		4	50	
1+00		260.4	267.6	267.9	272.3	
		15 10	7 8	7 5	3 1	
		#9 ℄ Laurel		4	50	
0+50		263.6	267.0	267.1	268.7	
		11 8	8 4	8 1.3	6 7	
		#9 ℄ Laurel.		4 Prop	50	
			264.4			
			11 0			

0+00 'B' line = 6+31.05 'A' line

Hub 6+31.05 'A' line Page 13

BM =	11.03	275.37	264.34
			275.37

TP3 - Start BM -			12.08	264.34 ✓
TP2 -	2.95	276.42	12.65	273.47
3+80 - 57° LT = ℄ Stucco house (Next Lot North Approx same elev)				
3+40				
3+00 - 45° Rt = doorway Stucco House				
TP1	10.91	286.12	0.16	275.21
2+50				
2+00				
1+84 - Nly line Laurel				

LT = Wly

Rt = ely -

284.08 / 2 04 / 57° / Floor

282.3 / 3 00 / 30

281.02 / 5 10 / Hub Gr same / 30

280.5 / 5 6 / 30

279.9 / 6 N

279.3 / 6 00 / 30

277.3 / 14 8 / 95 / Top Canyon

277.1 / 9° / 50

278.1 / 8° / 30

277.8 / 8 W

277.9 / 8 2 / 30

280.97 / 6 05 / 45° / Floor

286.12

270.3 / 4 1 / 30

273.5 / 9

275.1 / 0 13 / 30

257.6 / 10 R / 30 / Prop.

266.2 / 7 2

269.2 / 6 2 / 30 / Prop

257.2 / 16 2 / 30 / Top Canyon Prop

263.8 / 11 6

266.4 / 8 6 / 30 / Prop

275.37

Levels for 'C' Line Swans Add.
See sketch page 7.

LT = EH

℄ 'C'

Ref - W14

20

1+10 - Bottom creek			211.0	1 7/10	
				Bottom creek	
1+00		210.6	213.1	10 3/10	213.8
		12 8/10			9 5/10
		6			
		Bottom creek			
0+80		212.7	216.9	6 5/10	219.6
		9 7/10			3 8/10
		Bottom creek			
0+67			214.5	8 2/10	
				Bottom creek	
0+50		219.9	216.8	6 6/10	216.2
		3 5/10			4 2/10
				Bottom creek	
0+00 'C' Line = 1+25.00 'A' Line	L = 33° 10' Lt.	224.0	221.7	1 7/10	
		+0 6/10		Bottom creek	
BM. 1.67	223.44	Hub 1+25 'A' Line			
		221.77 Page 9			223.44 Σ

2+30				
2+00				
1+78				
TP,	0.87	211.01	13.30	210.14
1+50				
1+15 80 L.	8°38' rt			

Lt: Elv

Rt: Elv

201.9	200.0	212.0	
9 1/ 11	3 0	+1 0 / 10	
Bottom Creek			
204.5	205.4	211.5	
6 5/ 2	5 6/	+0 5/ 10	
Bottom Creek			
209.9	205.6	211.5	
1 1/ 7	5 4/	+0 5/ 10	
	Bottom Creek		
	211.01 T		
214.9	213.4	206.4	
8 5/ 10	10 0	17 0 / 8	
		Bottom Creek	
215.4	212.6	214.0	
8 0/ 10	10 80/	13 4/ 11	
	Hub Gr Same	Bottom Creek	
	223.44 T		

CHG TO C_1 LINE Pg 36

3+55.65 Δ: (14°31) · LT (on spl, T)

3+30

TP_2 1.16 199.30 12.87 198.14

3+00

2+85

2+50

LT

0.88	194.0	195.25	198.6
1 3	5 3	4 05	+0 3
10	3 Bottom Creek	Hub Gr. Sauge	10
1.84	195.4	197.4	202.4
0 9	3 9	1 9	+3 1
10	3 Bottom Creek		10

199.30

	197.7	201.0	205.9
	13 3	10 0	5 1
	4 Bottom Creek		10
	197.9	200.5	206.8
	13 1	10 5	4 2
	6 Bottom		10
1998	206.2		210.7
11 2	4 8		0 3
12			10
Bottom Creek			

211.01 x

					Lt	℄	Rt
5+50 - Creek bears sly of Pre. Sewer line					187.0 2 2 10	183.9 5 3 Bottom Creek	184.7 4 5 10
TP_3	3.12	189.21	13.21	186.09		189.21 ±	
5+20					188.2 11 1 10	184.0 13 3 Bottom Creek	189.2 10 1 10
4+90 75 L. 8°15' LT (on split)					191.2 8 1 10	188.42 10 88 ON Hub Gr. Same	186.4 12 9 4 Bottom Creek 187.7 11 6 10
4+50					185.3 4 0 10	188 9 5 Bottom Creek	183.7 5 6 10
4+00					185.7 3 6 10	181.3 8 5 Bottom Creek	182.3 2 10 10
						199.30 ±	

'C' Line should be Moved 20' South to fit creek bottom better.

6+70 $\frac{83}{}$ 'C' = 6+67 $\frac{23}{}$ 'D'

6+35

6+00

5+75

Lt	& 'C'	Rt.
	182.70	
	6 $\frac{5}{}$ Hub Gr. Same	11 $\frac{6}{}$ 19 Bottom Creek
188.2	184.0	179.8
1 $\frac{0}{}$ 10	5 $\frac{2}{}$	9 $\frac{4}{}$ 17 Bottom Creek
182.7	184.9	182.0
1 $\frac{5}{}$ 10	4 $\frac{10}{}$	7 $\frac{2}{}$ 14 Bottom Creek
188.2	185.2	182.8
1 $\frac{0}{}$ 10	4 $\frac{0}{}$	6 $\frac{4}{}$ 10 Bottom Creek

189.21 $\frac{T}{L}$

Levels for 'D' Line Swans Add. Lt=ely. Rt. Wly. 25

See Sketch Page 7.

0+50						
0+27 - Sly line Maple ST						
0+00 - ℄ Alley Sly 27' Line Maple						
0-13 = ℄ Alley + ℄ Maple.						
	3.46	281.13	-5.95	Hub 0+00 'D' Line 277.67		
TP2	13.05	283.62	0.02	270.57		
TP1	12.83	270.59	0.08	257.76		
				0+00 'A' on Hub Page 8		
BM.	12.63	257.84		245.21		

278.0 / 3 1 / 10

278.3 / 2 8

278.6 / 2 4 / 10

276.9 / 4 2 / 25

278.1 / 3 0

279.2 / 1 9 / 25

276.6 / 4 5 / 25

277.7 / 3 4

279.1 / 2 0 / 25

275.8 / 5 3 / 25

277.4 / 3 1

279.7 / 1 2 / 25

281.13 ±

Lt = e'ly ℄ 'D' Rt = w'ly

T.P.	0.48	268.50	13.11	268.02

2+59.9 = 1"X1" pine stub – P.O.T.

2+50

2+00

1+50

1+00

268.50

		272.2	271.9	269.7	
		8 9/50	9 2/10	11 4/50	
272.0	274.9	275.5	275.7	275.6	274.8
8 1/50	6 2/25	5 5/10	5 4/	5 5/10	6 3/40
274.6	276.1	277.8	277.9	277.6	278.1
6 2/50	5 0/32 Brk	3 3/10	3 4/	3 4/10	3 1/50
277.1		278.0	278.2	278.4	278.6
4 0/50		2 1/10	2 9/	2 7/10	2 5/50

281.13 ℄

TP_3	0.88	242.99	13.10	242.11
4+50				
4+00				
TP_2	0.01	255.21	13.30	255.20
3+50				
3+00				

Lt=ely

242.99 ℄

244.5	243.8	243.1	242.5	237.9
10 7/50	11 4/10	12 1/	12 7/10	17 3/40

251.1	251.0	250.6	250.8	248.6
4 1/40	4 2/10	4 4/	4 4/10	6 6/40

255.21 ℄

255.8	257.9	257.7	257.4	255.6
12 7/40	10 6/10	10 8/	11 1/10	12 9/40

265.9	265.7	265.8
2 6/10	2 8/	2 7/10

268.50 ℄

Rt=wly

6+00				
5+85				
TP5	0.23	217.21	13.08	216.98
5+50				
TP4	0.37	230.06	13.30	229.69
5+00				
4+90	56	P.O.T. 1"x1" Pine stub		

Lt = ely

℄

Rt = wly

208.3 — 208.8 — 205.5 — 203.0

8 9/10 — 11 1 — 14 2/10

211.5 — 211.0 — 208.9

5 7/10 — 6 2/10 — 8 3/10

217.21 ℸ

223.8 — 221.6 — 219.5 — 219.5 — 215.4

6 3/40 — 8 5/10 — 10 6/10 — 10 6/10 — 14 5/40

Rim Canyon.

230.06 ℸ

236.3 — 234.7 — 234.2 — 232.7 — 228.9

6 7/50 — 8 3/10 — 8 8/10 — 10 3/10 — 14 2/40

Top Canyon

242.99 ℸ

1+39.23 = P.O.T. 1"X1" Pine Stub

7+00

CHG TO 'C' LINE Pg 34 (D Line)

6+67 $^{23}_{-}$ 'D' = 6+70 $^{83}_{-}$ 'C' Line L. 90°00' RT

TP7	2.54	194.42	12.79	191.88

6+30-

6+20 $^{67}_{-}$ - P.O.T. 1"X1" Pine Stub

TP6	0.22	204.67	12.76	204.45

LT = c/y ℄ Rt = w/y-

189.7 4^{7}_{10} N/y

186.7 7^{7}_{-}

183.9 10^{5}_{10} S/y

177.4 17^{0}_{32} S/y Bottom Creek

182.72

11.70 Hub Grsonne

194.42

193.8 10^{9}_{10}

184.5 10^{2}_{-}

182.4 12^{3}_{10}

204.67

217.21 T

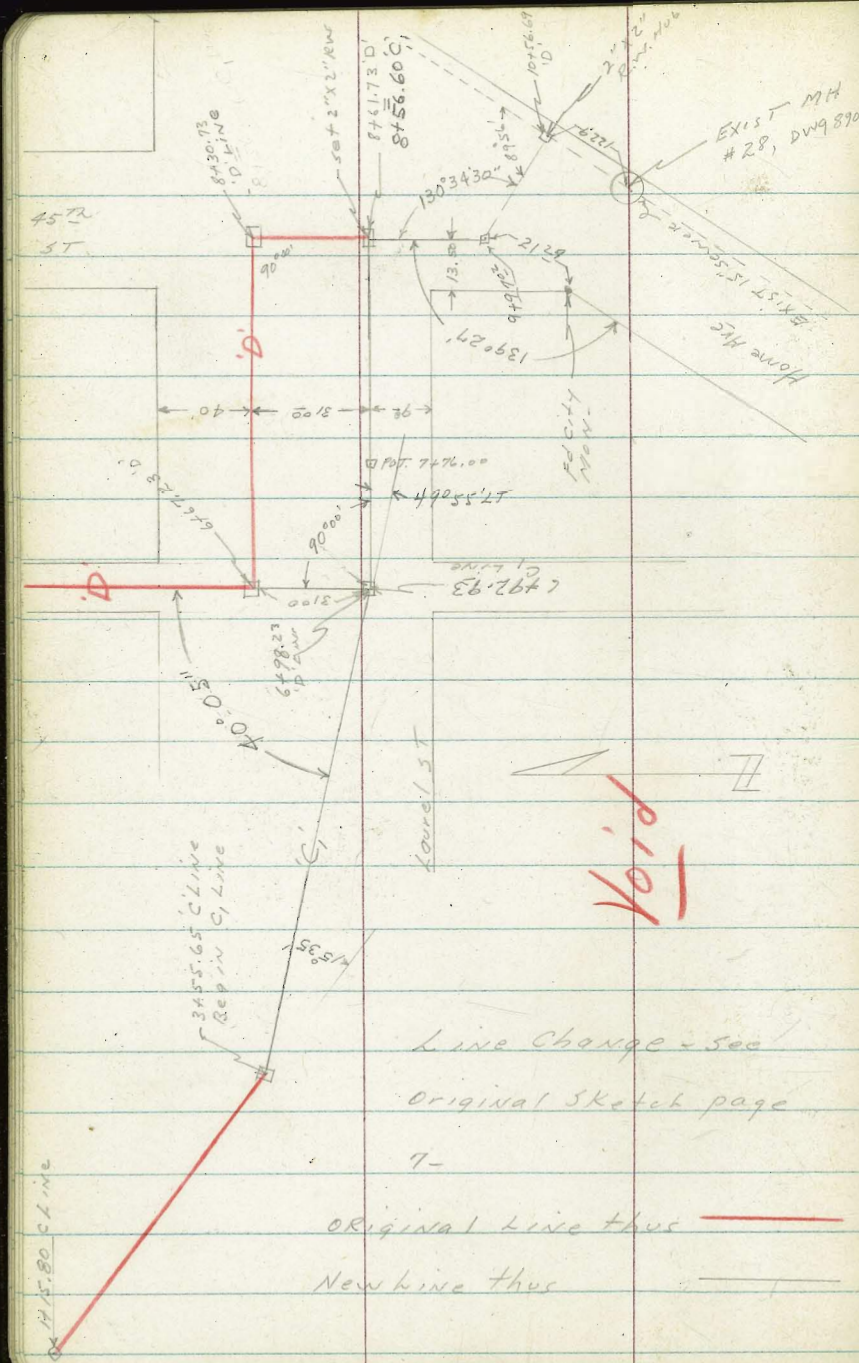
	8+50				
	TP9	1.95	170.81	13.36	168.86
6	8+30.73 - L: 90°00' Rt. (on split)				
7	TP8	0.69	182.22	12.89	181.53
6	7+70				
6	7+40				

Hub L: 8+30.73

	LT	℄	RT
	163.4 / 7 4 / 10 E14	166.3 / 4 5	167.8 / 3 0 / 10 W14
		170.81 ±	
	168.3 / 13 9 / 10 N14	168.86 / 13.36 Hub Gr. same	169.1 / 13 6 / 10 S14
		182.22	
	184.8 / 9 6 / 10	182.6 / 11 8	180.9 / 13 5 / 10
	181.9 / 2 5 / 10 N14	180.6 / 7 8	182.8 / 11 6 / 10 S14
		194.42 ±	

			LT	℄	RT
				D	
9+97.0 R-L	150°33' LT	ON SPLIT	16.38 7 0 10 EH	162.55 8 26 Hub	163.1 7 7 Sp.	161.5 9 3 10 WH
9+78				166.4 4 4		
9+66				166.1 4 7		
9+65				164.5 6 3		
9+50			162.2 8 6 40 EH	164.2 6 6		166.7 4 1 40 WH.
9+00			164.0 6 8 40 EH	166.2 4 6		168.9 2 0 50 WH
				170.81		

					LT	℄ 'D'	RT
				BP Culvert See page 17			
TP 12. BM.			6.80	148.04			
TP 11		2.72	154.84	8.86	152.12		
TP 10		1.37	160.98	11.20	159.61		
10+69	-	3' Rt = ℄ 10" power pole # 584610H					
		Manhole Sealed					
		122.9 Rt = ℄ SMH # 28 - DWG 890-D.					
10+66.59		Intersection Prelim line + EXIST 15" Sew.				155.51	155.56
						11 3.0 H06	11 2.5 122.9 Rim Manhole Sealed
					161.52	160.99	160.43
10+48		= Ely edge A.C. Pave Home Ave			9 2.9 40 NW	9 8.2	10 3.8 40 SW
					161.28	160.63	160.11
10+R4		= WH edge A.C. Pave - Home Ave			9 5.3 40 NW	10 1.8	10 7.0 40 SW
10+10					161.6	161.1	161.6
					9 2.5 25 NW	9 1.1	9 2.5 25 SW
						170.81 +	



Line Change - Sewer Line in Swans Addition - WO # 32292 4-30-53 Allen, D. Sisson, C. Powell - Angle point at 4+90.75 'C' line eliminated by change -

See Page 7-

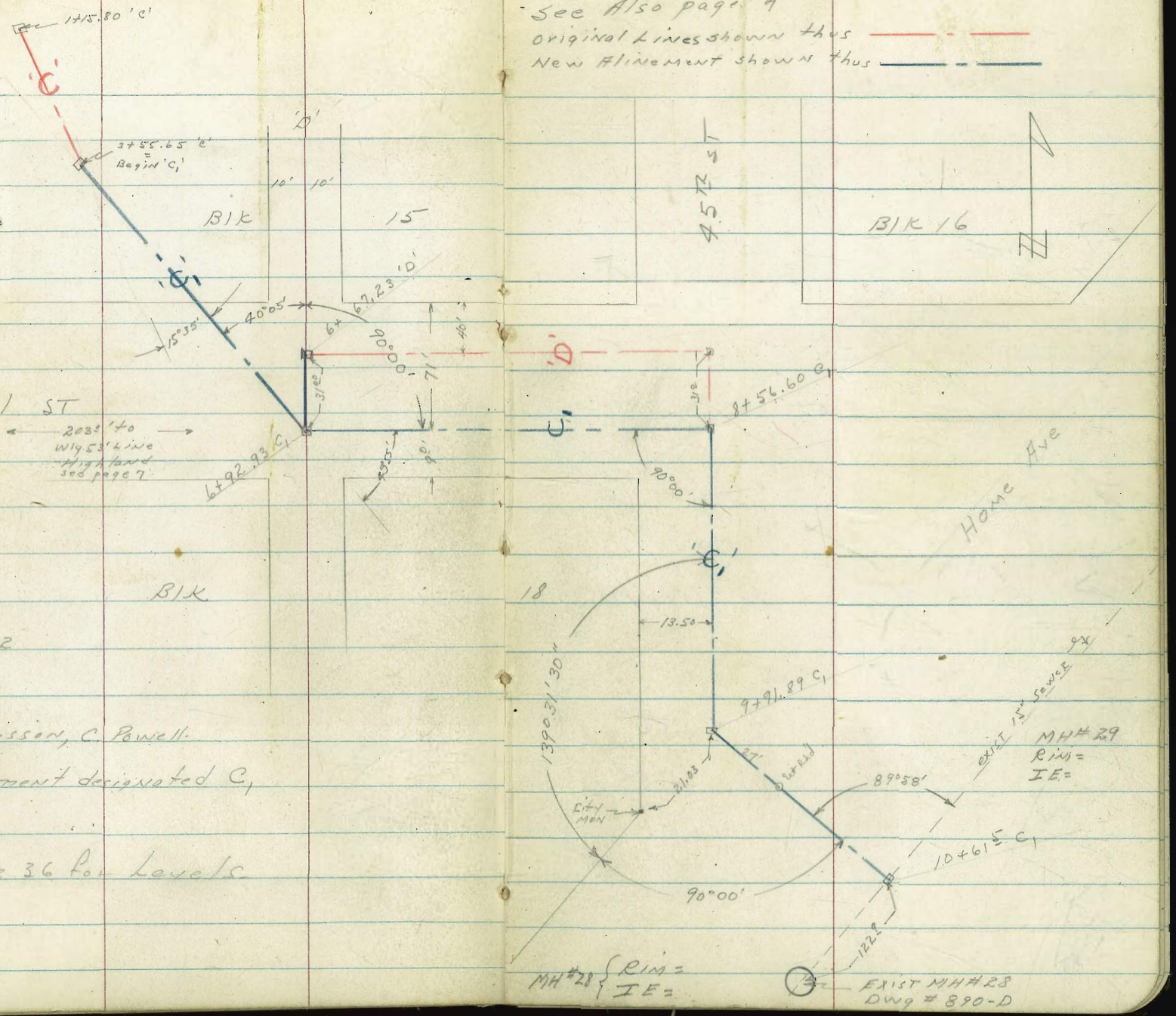
Line Change

'C' Line Swans Addition

See Also page 9

original Lines shown thus ——— · ———

New Alinement shown thus ——— - - ———



INDEXED

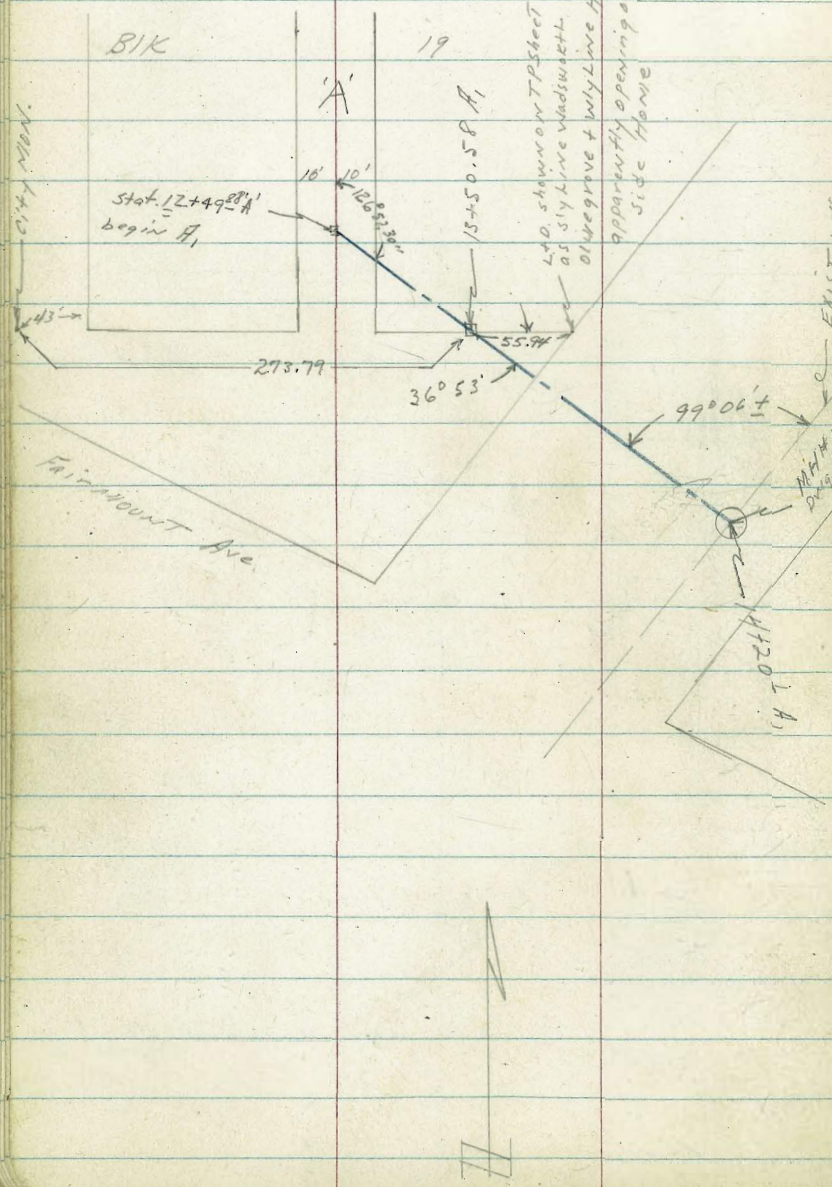
W.O. #32292

4-30-58.

C. Allen, D. Sisson, C. Powell.

New alinement designated C_1

See page 36 for Level



Line Change on 'A' Line - Blk 19, Swan's Add.

W.O. # 32292-

4-30-53

C. Allen, D. Sisson, C. Powell-

Changed Line designated A1

New Alinement shown thus ——·——

See page 7-

Levels page 43.

Profile - Line change - C Line.
See sketch page 7 & 34.
New alignment designated C_1

3+55.65 C Line = begin C_1 Line Stationing Carried Through -

	LT = Ely	℄ C_1	Rt = Wly
	188.3		187.1
4+90	8^{0}		9^{1}
			9^{0} BOTTOM creek
	194.2	188.5	194.1
4+50	2^{6}	7^{3}	2^{7}
	10	BOTTOM creek	10
	192.8	192.5	197.8
4+00	1^{0}	5^{5} 3^{9}	$+1^{0}$
	10	2 BOTTOM creek	10
	198.1	193.6	199.6
3+80	$+1^{3}$	3^{2}	$+2^{8}$
	10	BOTTOM creek	10
	201.3	195.3	201.3
	$+4^{5}$	2^{7} 1^{5}	$+4^{5}$
	10	3 BOTTOM creek	10

196.75

L. = 15°35' Left + ONSPLIT
3+55.65 ℄ = begin C_1 line

BM 1.50 196.75 195.25

ON Hub L. 3+55.65 page 22

6+50				
6+00				
TP	4.16	188.51	12.40	184.35
5+50				
5+25				
5+00				

LT = E'ly ℄ Rt = W'ly

C1

4.18	4.24	4.17	4.27	4.23
7 1/10	7 1	9 8 Creek Bottom	8 8/10	6 1/2 15
3.50	5.27	6.18	6.22	4.81
3 5/10	5 8	6 8 Creek Bottom	6 5/10	4 1/2 15

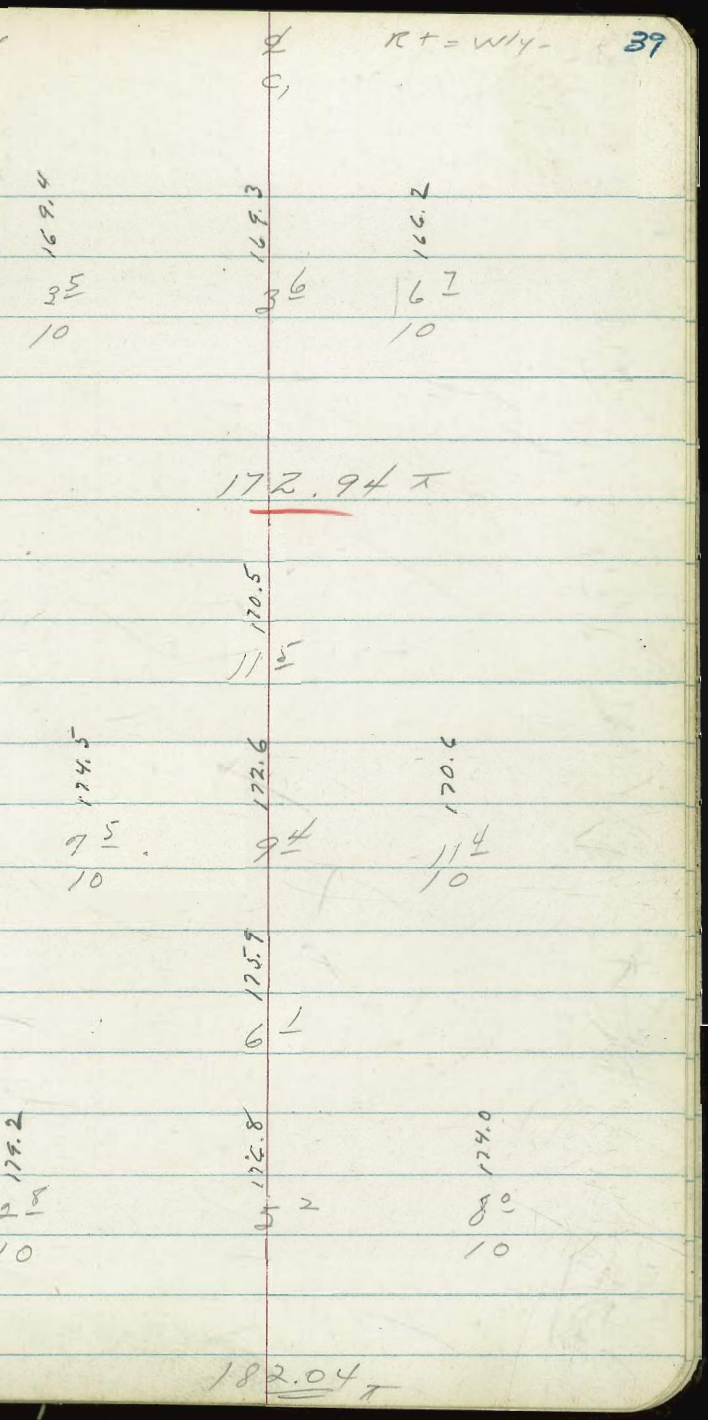
188.51 ✕

6.58	6.41		6.24	
11 2/10	12 7 Bottom Creek		10 6/10	
8.82	7.55		9.82	
9 1/10	11 3 Bottom Creek		8 2/10	
6.00	5.27	5.78	6.01	
5 9/10	8 9	10 3 7 0 Bottom	6 7/15	

196.75 ✕

				Lt ely	℄	Rt ely
					℄	
7+50				178.0 3 0 / 10	174.9 7 1	173.2 8 8 / 10
7+25				178.1 3 9 / 10	175.8 6 2	175.4 6 6 / 10
7+18					172.7 4 3	
7+00				178.9 3 1 / 10	172.0 5 0	175.3 6 7 / 10 Creek BOTTOM	176.7 5 4 / 20
TP_2	6.23	182.04	12.70	on Hub 6+92.93 C_1 175.81		182.04 ℸ
6+92.93 = C_1 ℄ ahead 49°55' Lt deflection – ON split				185.5 10 0 / 10	175.7 12 8 / 10 Bottom Creek	178.1 10 4 / 10
						188.51 ℸ

8+20				
TI_3	3.49	172.94	12.59	169.45
8+05				
8+00				
7+75				
7+64				



9+76

9+70

9+58

9+50

9+44

9+00

ON SPLIT

8+56.60 ℄ L. 90° = 8+61.73 D line.

Stations Carried ahead on ℄ Line

Without regard to 'D' Line

Lt ℄ Rt

40

9+00 — 16.4 — 5

9+44 — 16.3 — 6

9+50 — 16.2 — 7

9+58 — 16.1 — 8

9+76 — 16.0 — 9

16.3 9° 10

16.6 8 2

16.7 7 2 10

16.5 9 3 10

16.6 8 3

16.9 6 0 10

16.3 9 3 10

16.4 7 5

16.3 7 6 10

17 R. 94

	Lt	℄	Rt
10+31 ℄ A.C. Paving Home Ave	162.77 10 1/7 100 ℄ Ac	161.07 11 8/7	159.42 13 5/7 100 ℄ Ac
10+19 ± Wly edge A.C. Paving Home Ave	162.24 10 7/0 100 Ac	160.58 12 3/5 Ac	159.02 13 9/2 100 Ac
10+13.		160.3 12 1/6	
10+00	164.5 8 4/ 10	162.3 10 6/	160.8 12 1/ 10
9+91 89/ ± ℄ 90° to Wly line Home Ave ON SPILT	163.8 9 1/ 10	162.2 10 7/	161.5 11 4/ 10
9+84		164.6 8 3/	
		172.94	

Rim = 163.66
MH #29 IE = 154.83
where is this m.H ? clark

Rim = 159.54
MH #28 I.E. = 149.40

160.59±
Check - Wly edge A.C. Pave page 32 = 160.63

10+61 5 Intersection ℄, Line ℄ exist 15" Sewer

10+43 5 = Ely edge A.C. Paving

LT ℄ RT

15-9.5-1

13 4/3 ± ON hub or same

162.37 — 10 5/7 — 100 AC

160.97 — 11 9/7 — AC

159.42 — 13 5/7 — 100 AC

172.94 π

Line Change 'A' Line
Swan's Add. - see page 7+35
New line designated A_1

TP_3	2.42	154.72	13.21	152.30	154.72 ±
TP_2	0.34	165.51	12.92	165.17	167.1 / 166.7 / 166.2 — 11.0/10 — 11.4 — 11.9/10
12+93 - Top steep slope					
TP_1	0.01	178.09	13.00	178.08	178.09 ±
12+75					175.6 / 175.6 / 174.6 — 15.3/10 — 15.5 — 16.3/10
12+49.88 'A' line = Begin A_1 line	$\angle$ = 53°07'30" LT			6M SPLIT	192.1 / 189.3 / 191.1 — 4.9/10 — 1.8 — 0.0/10
					191.08 ±
BM.	1.84	191.08		189.24	on POT 12+49.88 page 15.

LT = N'ly — A_1 — RT = S'ly

14+01 $\frac{8}{}$ = Ely edge AC. Home Ave

13+89.8 ℄ AC. Home Ave

13+77 $\frac{8}{}$ = Wly edge AC. Pave Home Ave

13+70 = top fill embankement Home Ave

13+58 - Toe fill for Home Ave

13+50 - IN. bottom channel

13+25 = toe slope

LT = Sly - ℄ - Rt = Sly

									150.00
									4 7 2 / 50
		151.28		150.46					
		3 4 4 / 50		4.24					
			151.06		150.83		150.84		
			3 6 6 / 10		3 7 9		3 8 8 / 10		
					150.67			150.41	
		151.37							
		3 3 5 / 50 Ac			4.13 Ac			4 5 8 / 50 Ac	
			150.4		150.4			150.1	
			4 3 / 10		4 3			4 6 / 10	
		146.7			146.7			146.8	
		8 0 / 10			9 0			7 9 / 10	
		146.5			146.4			146.3	
		8 2 / 10			8 3			8 4 / 10	
		146.5			146.2			146.7	
		8 2 / 10			8 5			9 0 / 10	

154.72

#5

FB 1561 - 38

BM- 6.69 148.03 (148.05) BP - Ely Cor. Box Culvert Fairmount Ely of Home

150.66 Rim 4.06 12.81 I.E. 141.91

14+20 = M.H. # 26 - Dwg 890-D

154.72 ±

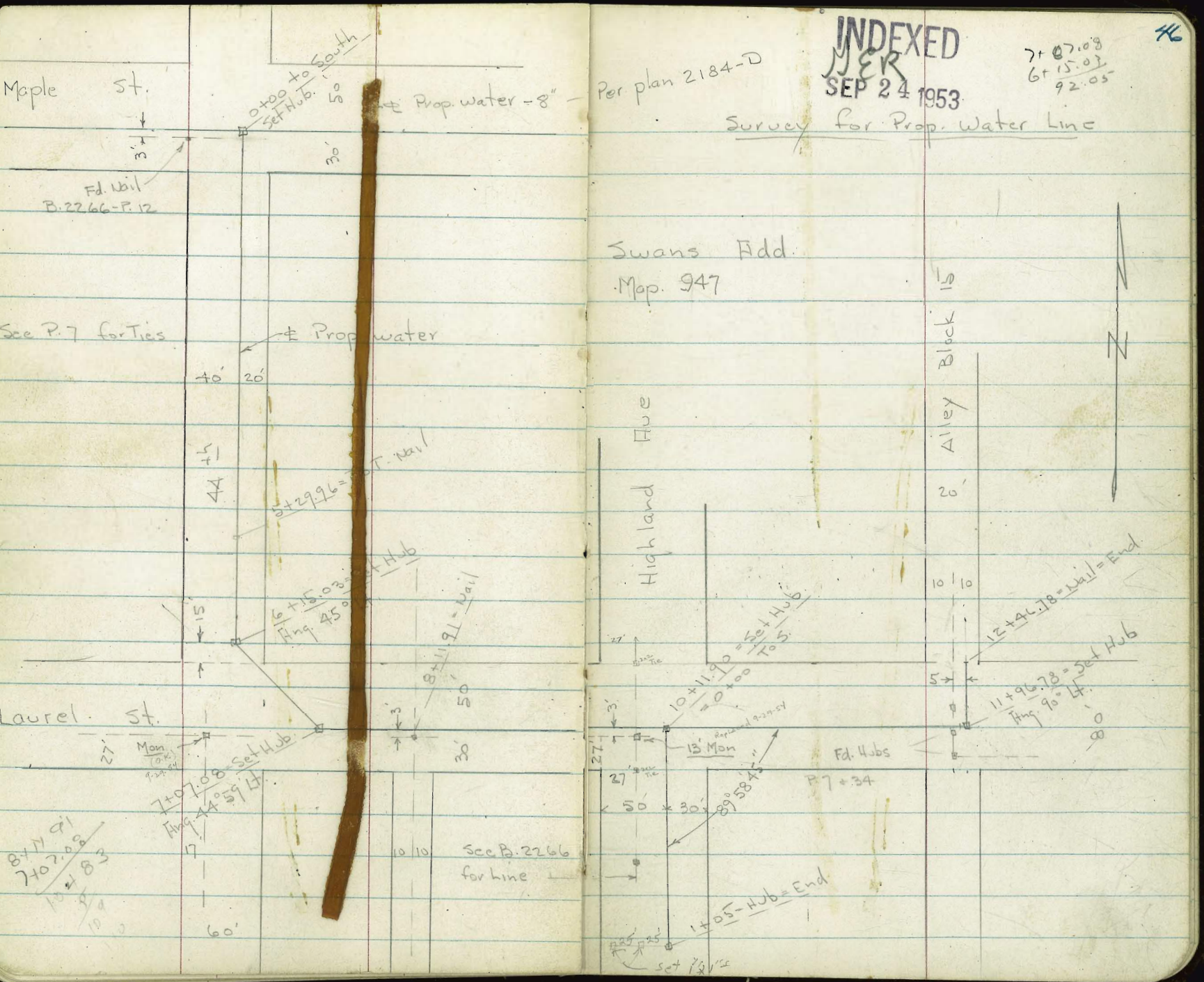
INDEXED
MER
SEP 24 1953

7+87.09
6+15.03
92.05

116

Per plan 2184-D

Survey for Prop. Water Line



Beg Levels along ℄ of Prop. Water Line in 44th - Maple to Laurel & E. To Alley in Block 15 - See Sketch - P. 46

Contours.

6 + 65 - Move over more if Needed - showing

6 + 15.03 = Ang. P.t. - Sect. 90° To foward Tan.

5 + 80

5 + 50

5 + 00

4 + 50

4 + 00

3 + 50

3 + 00

2 + 50

2 + 00

1 + 50

1 + 00

0 + 50

= 10' S. of ℄ of Maple

0 + 00 = ℄ of Water Line Shown on Plan 2184-D + Maple

Set B.M. = Spike in S.W. Pole - 44th — 286.80 ↔ Set Chis NE corn of Conc. Walk #4395 Maple Elev = 287.13

B.M. = N.W. B.P. Fairmount + Maple — 280.17

Lt.	℄	Rt.
67.7 / 25	64.9	61.7 / 10
70.6 / 20	67.08 = on Hub.	65.4 / 10
	72.4	
	75.3	
	78.5	
	80.3	
	80.8	
	80.3	
78.0 / 10	79.0	80.8 / 10 = edge
	77.0	
72.9 / 10	74.8	77.5 / 10 = edge
	74.0	
74.3 / 10	75.6	78.1 / 8 = edge of Rd.
	77.1	
	76.95 = on Hub.	
	200' Sq. Not Noted.	

Actual Elev. Shown

		Lt.	℄	Rt.
check Hub. - 6+70.83 - 8.29	182.70			
11+46.78 = end - at N.L. of Laurel			96.9	
11+21.78			88.4	
11+96.78 = Ang. Pt.			181.60 = on Hub.	
11+63 = ℄ Wash			78.8	
11+30			190.7	
10+90			203.0	
10+75			14.5	
10+45			24.9	
10+11.90 = 0+00 on line to South			34.81 = on Hub.	
Set B.M. on 13" Mon - Highland	240.68			
9+80			43.3	
9+50			48.9	
9+00			56.4	
8+70			60.6	
8+30			63.1	
7+80		64.7 30	63.3	62.9 10
7+35		67.0 40	63.6	62.6 10
7+07.08 = Ang Pt. - outs: 90° to back Tang		66.8 50	65.2 25 / 57.5	52.3 10 = in wash

Beg. Levels along ℄ of 105' Stub.
S. of Sta. 10+11.90 on Laurel St. -See P. 48

	Lt.	℄	Rt.
1+05 = End = Hub.		39.58 = on Hub.	
0+70		39.8	
0+35		38.4	
0+00 = Sta. 10+11.90		234.81	

D.Smith
J.ROHER
R.Taylor
B.Fish

INDEXED
NOV 4 - 1953

Sewer SWANS Addition

WO# 32292
11-2-53

50

Added Notes
Cont. p 7

(316.70 tie Sheet)

Laurel St

Cont p 46

Fd Cov Mon

166.65

11+38.60

Clark 7-2954

Set Hub POT. 10+80.1'

Set Nail

20'

BLK 2 Swans Add #947

St

43'

Ave

27'

Set 3x3 8-17-54 - Clark

Olive St

37+15

19+27

Set Hub

Fd Cov Mon

Fd Cov Mon

43'

17'

3'

14'

20'

Fd Nail

Nail-P.Pole

P.Pole-Nail

Fairmount Ave

BLK

20 Swans Add #947

Fd ½ Pipe RE 15.34 Lot 35

3+25 End

10'

10'

17'

Hillyard St

BLK B 13 Swans Second Add #956

Highland Ave

Fd ½ Pipe RE 15.34 Lot 31

existing SMH Dwg 6900-4

12"

existing 8" sewer

Set 2+41.01 POT, Hub

Set 0+63.79 POT, Hub

Maple St

Fd Hub 0+00 "A"

Cont p 7

27'

53'

Alley Blk 20 Swans

Lt = W/y

Rt = Ely

		211.84 8.3 10	210.34 9.8 10	209.84 10.3 10
0+92				
0+88		209.04 11.2 10	208.34 11.8 10	207.74 12.4 10
TP5	12.80	220.14	209.84 0.01	207.34
0+50		206.05 13 10	205.25 21 10	204.15 32 10
0+25		204.15 33 10	202.95 45 10	202.25 51 10
0+00		192.85 14.50 19 10	200.31 7.04 rim	
TP4	13.16	207.35	0.57	194.19
TP3	13.22	194.76	0.62	181.54
TP2	13.16	182.16	0.51	169.00
TP1	12.80	169.51	0.34	156.71
BM	9.00	157.05		148.05

BP. Ely Box Co. Fairview

Alley Blk 20 Swans

Lt = W/y

Rt = Ely

TP8	12.71	25.93 245.52	244.82 02 10	244.02 1.7 10
2+50				
2+25		241.62 3.2 10	240.92 4.8 10	240.32 5.4 10
2+00		237.72 8.0 10	237.02 8.7 10	236.32 9.4 10
TP7	13.22	245.72		0.13 232.50
1+75		231.03 1.6 10	230.13 2.5 10	228.83 3.8 10
1+50		225.23 7.4 10	224.03 8.6 10	223.03 9.6 10
TP6	12.70	232.63		0.21 219.93
1+20		216.24 3.9 10	215.84 4.3 10	214.44 5.7 10

A 220.14

Lt=Wly | ℄ Alley Blk 20 Swans | Rt=Ely

				263.29 ✓ P18	
BM		263.31 3.81		263.31 Hub 1480 "B"	
TP9	10.20	267.12	0.51	256.42 ✓	
3+25		253.83 4.1 10	253.73 4.2 10	253.73 4.2 10	
3+00		253.03 4.2 10	252.93 5.0 10	253.13 4.8 10	
2+75		249.93 8.0 10	248.63 9.3 10	247.53 10.4 10	
		T. 257.23			

Lt=Wly | ℄ Alley Blk Swans 2nd Add | Rt=Ely

1+50		271.4 11.4 20	272.6 10.2 10	273.3 9.5 10	275.0 7.8 10	275.1 7.7 20
TP2		12.84	282.81 ✓		10.18 269.87 ✓	
1+00		264.0 6.1 20	265.2 ✓ 4.9 10	266.3 3.8 10	268.0 2.1 10	269.2 ✓ 0.9 20
0+66		253.7 16.4 15	258.9 11.2 10	261.3 8.8 10	262.7 7.4 10	263.8 6.3 20
0+57.92 LT ℄ 12" PB/L # 439342H						
0+50		253.4 16.2 10	258.4 11.6 20	259.7 10.4 10	260.2 9.9 10	
TP1		12.31	270.05 ✓		0.47 257.74 ✓	
0+25		249.0 9.2 10	253.2 ✓ 5.0 10	256.0 2.2 10		
0+00			245.2 ✓ 13.0			
BM		13.00	258.21 ✓			245.21 P8 on Hub 0+00.84 "A"

Alley Blk B
Swans 2nd Add

Lt = Wly
Rt = Ely

3+28 9° Lt ℄ dead man

3+00

285.3 285.6 286.0 286.4 286.7
6 7 6 5 5
20 10 10 20

2+75

284.0 285.0 285.5 285.9 286.2
8 7 6 6 5
20 10 10 20

2+69 9° Lt 18" Pepper tree

2+50

282.3 283.0 283.9 284.4 284.9
9 9 8 7 7
20 10 10 20

2+39 10° Lt 4" Pepper tree

2+25

280.0 281.3 282.2 283.0 284.0
12 10 9 9 8
20 10 10 20

TP3 9.38 292.04 0.15 282.66

2+02 8° Lt ℄ 12" PI Pk "PA2629

2+00

276.8 277.9 279.2 280.0 281.9
6 4 3 2 0
20 10 10 20

1+81 7° Lt ℄ dead man

282.81

Lt = Wly
Alley Blk B
Swans 2nd Add
Rt = Ely

6+00 10° Lt Begin 8" conc wall

292.1 292.6 292.5 291.9 291.8 291.7 291.7
+0.2 +0.62 +0.5 0.1 0.2 0.3 0.3
Footing 10.3 Top 10 10 7 10 20

6+00

5+53 9° Lt 18" PBL PA2761

5+53 10° Lt End 4' cyclone fence

291.5 291.4 291.9 291.7 290.6 290.5
0.5 0.6 1.1 1.3 1.9 1.5
20 10 7 10 20

5+50

290.3 290.5 290.0 289.9 289.4 289.3
1.2 1.5 2.0 2.1 2.6 2.2
20 10 7 10 20

5+00

288.7 289.0 288.4 288.3 288.0 287.4
3.3 3.0 3.6 3.7 4.0 4.6
20 10 7 10 20

4+50

4+29 10° Lt Begin 4' Cyclone fence

286.0 286.0 285.8 285.5 284.3
6.6 6.0 6.2 6.5 7.7
20 10 10 20

4+00

3+54 10° Lt ℄ 18" P Pk "PA2693

284.7 285.3 285.1 284.9 285.0
7.3 6.7 6.9 7.1 7.0
20 10 10 20

3+50

292.04

Lt-Lwly — Alley B/W B — Rt-Ely — Swan's 2nd Add

6+00 — 294.0 (13) 293.4 (4.2) 293.3 (5.0) 293.4 (4.2) 292.1 (6.2) — (15) (10) (10) (20)

7+72 9.3 Rt end 3' Picket fence

7+66 8.2 Lt E 14' P Pole # PA2825

7+63 9.2 Lt E 16" P Pole # PA2825

7+60 — 295.9 (2.4) 295.8 (2.5) 294.2 (4.1) 293.3 (5.0) 293.2 (5.1) 293.2 (5.1) 292.6 (5.7) 292.6 (5.7) — (20) (14) (10) (6) (10) (11) (14)

9.2 Rt Begin 3' Picket Fence

7+13.6 M/y Olive — 294.1 (4.2) 293.3 (5.0) 293.1 (5.2) 292.9 (5.4) 292.3 (6.0) — (20) (10) (5) (10) (20)

6+83.6 C Olive — 293.7 (4.6) 293.3 (5.0) 292.8 (5.5) 292.2 (6.1) 291.6 (6.7) 291.0 (7.3) — (20) (10) (10) (20) (30)

Lt end 8" conc wall

6+53.6 S/y Olive — 293.1 (5.2) 293.1 (5.2) 293.4 (4.9) 293.1 (5.2) 292.2 (5.9) 292.0 (6.3) 291.9 (6.4) 291.5 (6.8) — (20) (10.3) (10.3) (10) (10) (20) (30) — Existing Top

6+25 — 293.0 (5.3) 293.3 (6.0) 292.1 (6.2) 292.0 (6.3) 291.9 (6.4) — (15) (10) (10) (10) (20)

TP 4 — 7.23 — 298.34 — 0.93 — 291.11

Lt-Lwly — Alley B/W 2 — Rt-Ely — Swan's

10+42 — 282.3 (5.2) 282.6 (4.7) 282.5 (4.8) 284 (6.2) 279.1 (8.2) — (20) (10) (10) (20)

TP 5 — ~~282.3~~ 1.88 — 287.27 — 12.95 — 285.39 — Pot Hub 10+00

10+00 — 290.2 (8.1) 287.7 (10.6) 286.8 (11.5) 284.5 (13.8) 285.4 (12.95) Hub 3d 286.1 (12.2) 285.8 (12.5) 283.8 (14.5) — (20) (10) (7) (4) (9) (10) (17)

9+63 9.2 Lt E 18" P Pole # PA2905

9+54 10° Rt and Lt Conc wall — 289.4 (8.2) 288.8 (9.5) 289.0 (9.3) — (10) (10) (10) Top Existing 96

9+50 — 293.4 (4.2) 291.3 (7.0) 289.2 (9.1) 289.2 (9.1) 289.2 (9.1) 290.1 (8.2) — (18) (10) (7) (9) (10) (14)

9+27 15' Rt Lt E House — 294.0 (7.32) 15.5 Flow

9+05 10' Rt Begin 6" conc wall — 290.80 (7.54) 290.2 (8.1) 290.3 (7.8) — Top Existing 3d

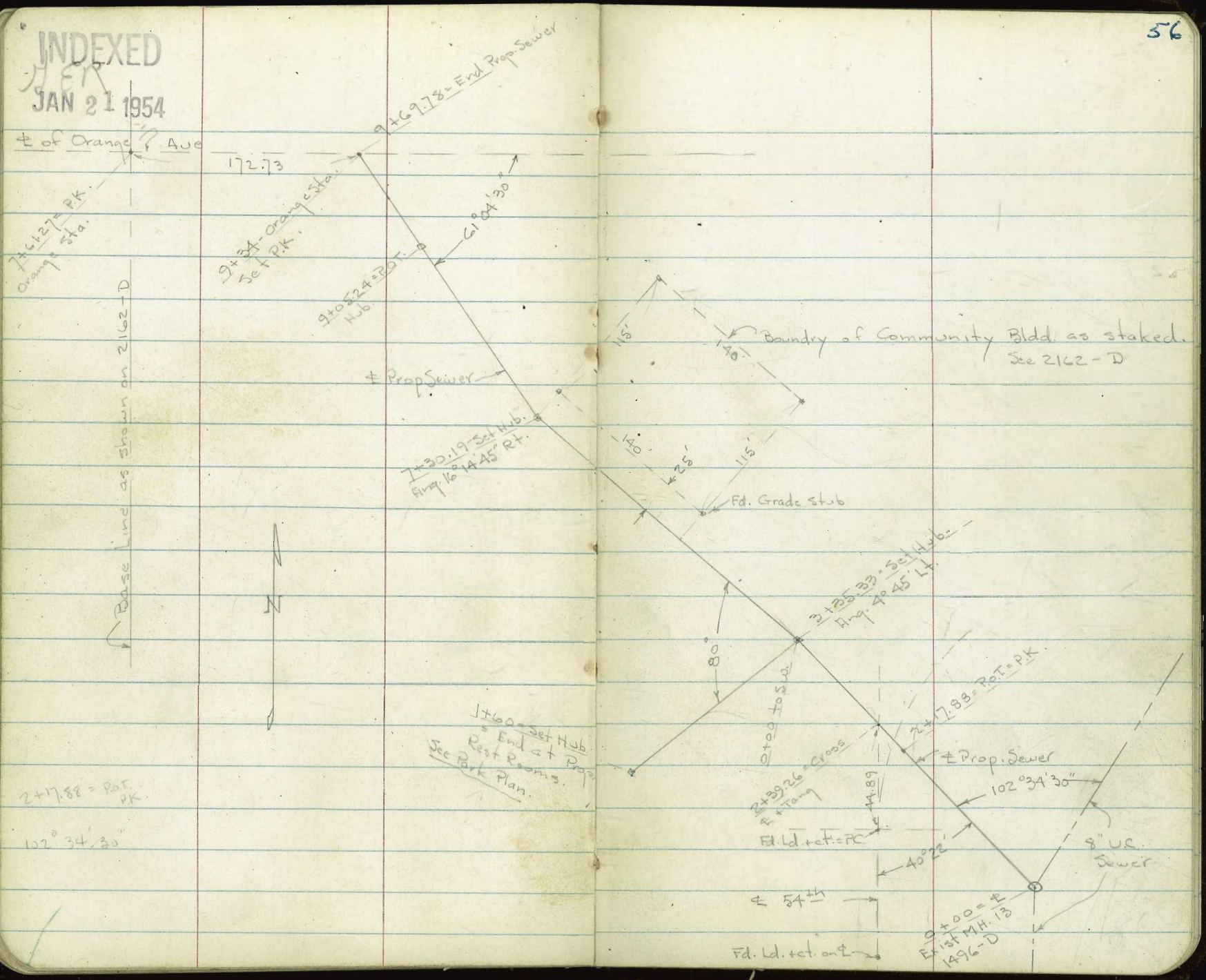
9+00 — 294.0 (4.3) 294.5 (6.3) 292.0 (6.3) 290.8 (7.5) — (15) (10) (10)

8+98 10.2 Rt E double garage conc floor + apron — 290.88 (7.45) 290.99 (7.35) — 102 apron 15 Flow

8+50 — 293.6 (4.7) 293.3 (5.0) 293.3 (5.0) 293.2 (5.1) 292.2 (6.1) — (15) (10) (10) (10) (20)

π 298.34

		12 Wig	Alley 1812 Swans	Alley
BM start p52			14 42	245 23 (245 21)
TP9	0 98	259 65	12 34	259 57
TP8	0 01	271 91	13 28	271 80
TP9	0 75	285 18	13 07	284 43
TP6	11 07	297 50	0 84	286 43
11+38 6 end			274.0 13 3 10	272.3 15 0	271.3 16 0 10
11+20			276.5 10 8 10	274.1 13 3	271.7 15 6 10
11+00			277.1 10 3 10	273.6 13 2	269.9 17 4 10
10+85			276.0 11 3 10	272.8 14 5	269.3 18 0 10
			TP 287 29		



Levels along ℄ of Prop. Sewer to E.S.D.

Park - 54th & Orange - See sketch - P. 56

W.O. 21087 -- 1-19-54- 7.0.

T.P.	12.62	370.98	0.59	358.36
1+00				
0+73.5 - 10' Rt. = ℄ 20" Vit.				
0+65				
0+60.5 - 7.5' Rt. = ℄ 8" Vit.				
0+58 - 11' Rt. = ℄ 10" Vit.				
0+52 - 1.5' Lt. = ℄ 8" Vit.				
0+40				
0+00 = ℄ Exist. MH				
T.P.	0.59	358.95	13.14	358.36
Set B.M. - on P.C. Ld. + ct.			2.24	369.26
T.P.	50.3	371.50	2.10	366.47 = Hub - 3+ 35.53
T.P.	4.67	368.87	13.22	363.90
B.M.	4.30	377.12		372.82 = Spike in Pole 9+65' on Orange

Lt.	℄	Rt.
	370.98	
53.6	58.8	52.1
5.3	6.1	6.8
10		10
44.7	44.0	44.4
11.2	11.9	11.5
10		10
45.8	45.2	44.4
13.1	12.7	11.5
10		10
	48.99	41.76
	9.96	17.19
	W. Rim	I.E.
	358.95	

2+80 - 7.5' Rt. = ℄ W.M. + Gate

2+76.5 - 7' Lt. = ℄ 24" Cypress

2+73.7 = N. edge of 6" Conc. wall - 5' Long.

2+60 - 8.5' Lt. = Near Cor. of 6" Conc. wall - 5' Long

T.P. 4.99 374.25 1.72 369.26 = on P.C. c.t.

2+46 = edge Conc. Pave

2+20.2 = edge Conc. Pave

2+16 = edge A.C.

2+00

1+92 - 13' Lt. = ℄ 8" Olive

1+85

1+40

Lt. ℄ Rt.

73.0 2.3 25

71.59 2.66 4.2 end of wall

71.58 2.67 8.5 = Top wall

71.63 2.62 Top wall + ground

71.62 2.63 0.5 = end wall

71.0 3.3 25

374.25

73.0 +2.0 25

70.7 0.3 11

70.34 0.64 edge Conc.

69.29 1.69 36.5

69.69 1.29 29 edge Conc. Pave

69.32 1.66

69.1 1.9 25

69.14 1.84

68.94 2.14 19 edge Conc.

68.9 2.1

65.1 5.9 15

63.3 6.7 25

68.28 2.73 33.1 edge Conc. Pave

68.25 2.5 15

67.8 8.3 25

66.48 6.2

59.3 11.7

60.4 10.6 15

58.2 12.8 15

370.98

6+50

6+00

5+50

5+00

4+50

Beg. flat graded area

3+97 = Toe of Slope

T.P 2.18 363.36 13.07 361.18

3+75 = Top Bank

3+35.33 = Ang. Pt. + 0+00 for Sta. to W.

3+05.5 - 6.3' Lt. = ℄ 4" Olive

3+02 - 4' Rt. = ℄ 3" Olive

3+00

Lt.	℄	Rt.
	55.2	
	8.2	
55.1	55.0	
8.3	7.8	
32		
Top Bank	56.0	
	7.4	
	56.5	
	6.9	
	56.8	
	6.6	
62.9	56.8	56.7 63.3
0.5	6.6	6.7 0.1
21	15	Toe 18 = Top
Top	Toe	363.36

64.2

	10.3	10.0	9.6
	25		25
66.6		66.7	67.7
7.8		7.78	7.1
25		on H.b.	25
		Sect. 90° to Back Tang.	
70.8		69.2	69.1
3.5		5.1	5.2
25			25

374.25

starting
check B.M. - 2.30 372.83 ✓

9+69.75 = end at ℄ of Orange - Sta. 9+34

9+61 = edge A.C. pave
9+51.5 - 2.8' Lt. = ℄ P. pole # None
9+23.5 = Line of graded curb.

9+00 = Top of Bank as Built
T.P. 11.94 375.13 0.17 363.19

8+67 = Toe slope

8+00

7+30.19 = Ang Pt.

7+00

Lt	℄	Rt
	372.82	
	11.0 / 4.0 on P.K.	
	10.86 / 4.27	
11.4 / 3.7 Top Dirt gut.		10.8 / 4.3
	11.8 / 3.3	
	375.13	
	55.1 / 8.3	
54.6 / 8.8		55.0 / 8.4 / 18 = Cor. of Toe of Slope
54.81 / 8.55 on Hub		
55.1 / 8.7	54.8 / 8.6	
28 = Top	363.36	

Beg. Levels on Stub to w. from
sta. 3+35.33 - See Sketch - P 56 - Notes. P. 59

1+85 - for profile

1+60 - end

1+00

0+50

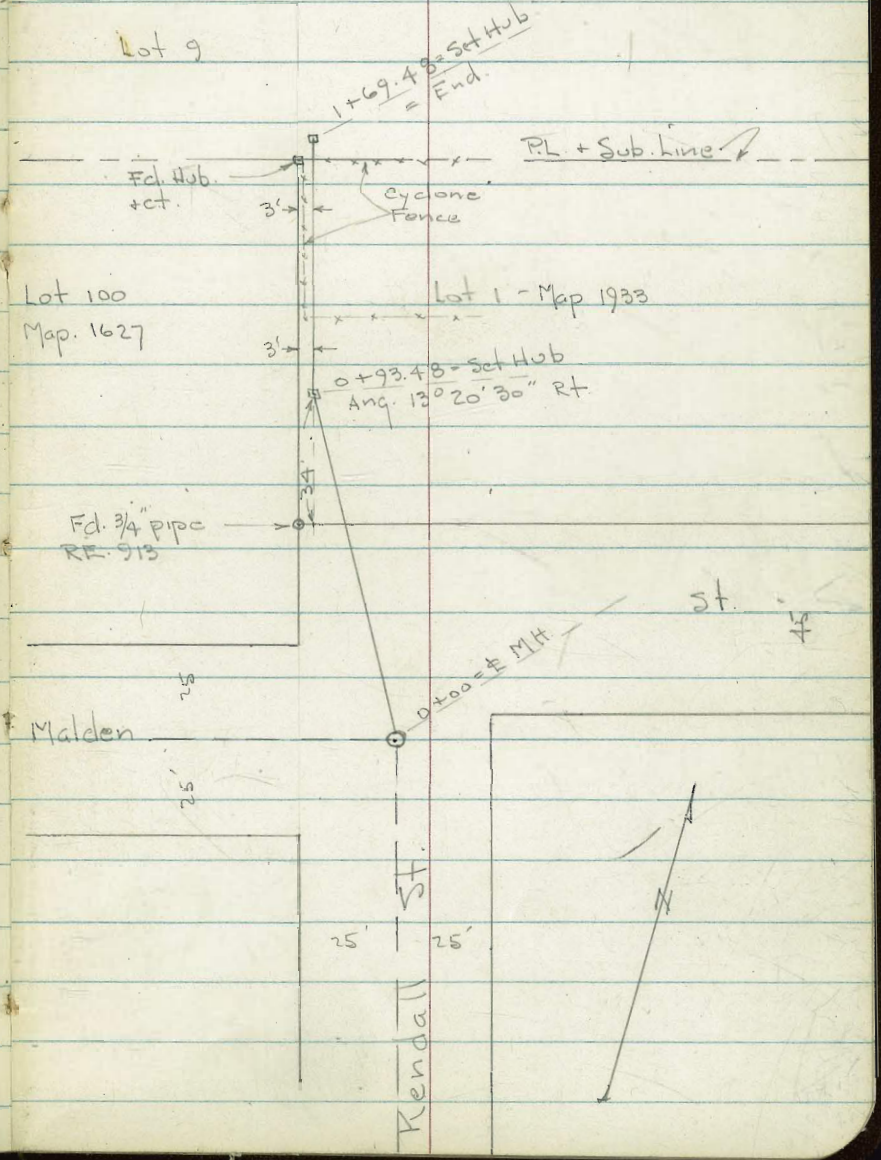
0+00 = 3+35.33 on Main Line

B.M. = Hub. 370 370.17 366.47 - 3+35.33 P. 59

Lt.	℄	Rt.
	64.0	
	6.2	
66.3	64.39	62.8
3.9	5.79	7.4
25	on Hub.	25
67.0	64.43	62.9
3.2	5.8	7.3
25		25
67.8	65.6	63.8
2.4	4.6	6.4
20		25
edge of shrub planting	66.47	
	3.70	
	Hub.	
	370.17	

Survey for Prop. Sewer - from M.H.
in Malden & Kendall To Lot 9 - Soledad Terr.
W.O. 62422 - 2-28-55 7.0.

Owner of Lot 100 Does not want Line in
Their prop. - Kept all R.O.W. in Lot 1.



X-Sect. along ℄ of Prop. Sewer –

See sketch – P. 62

	Lt.	℄	Rt.
1+08 – 5.6' Lt. = end walk & 8.2' Lt. = end Conc. wall for Conc. Slab. to House	35.62 8.2 Conc. slab.	35.06. 5.6 = Cor. of walk	
0+93.48 = Ang Pt. – outs. Normal to Foward Tang.	33.60 8.3 By House	33.51 5.8 walk	33.25 on Hub. 33.3 10
0+77.5 – 7' Lt. = ℄ 48" Euc.			
0+75	29.84 13.1 By House walk	29.82 10.5 walk	29.4 10.5 gr. 30.0 30.4 10
0+70 – 9.5' Lt. = ℄ 36" Euc.			
0+60	27.07 25 Conc. Dr	27.28 14.2 Conc.	26.8 26.9 27.1 10
0+57 – 12.8' Rt. = Wly. of Rough Rock & Conc. wall House – Jains' Dr.			
0+57 – 14.9' Lt. = Beg. Ely. of 30" Conc. walk along			
0+49 – 14' Lt. = ℄ 24" Euc.			
0+45.5 – 15.1' Lt. = Cor. Conc. Dr. – (cured sect.)			
0+35	23.47 17.6 Conc. Dr.	22.9 10	22.8 23.2 10
0+30 – 18.8' Lt. = Cor. Conc. Drive			
0+27 – 19' Lt. = ℄ 40" Euc. Tree			
0+00 = ℄ of Exist Sewer M.H. – channel & stub. to North – & Exist. 4" Lat. High to N.		17.60 W. Rim 09.80 I.E. of M.H.	14.60 I.E. 4" To N.
Malden & Kendall Set. B.M. – spike in S.E. Pole	221.76		
B.M. = S.W. 7' Mon. Kendall & Collingwood.	197.32		

200' fig. Not Noted

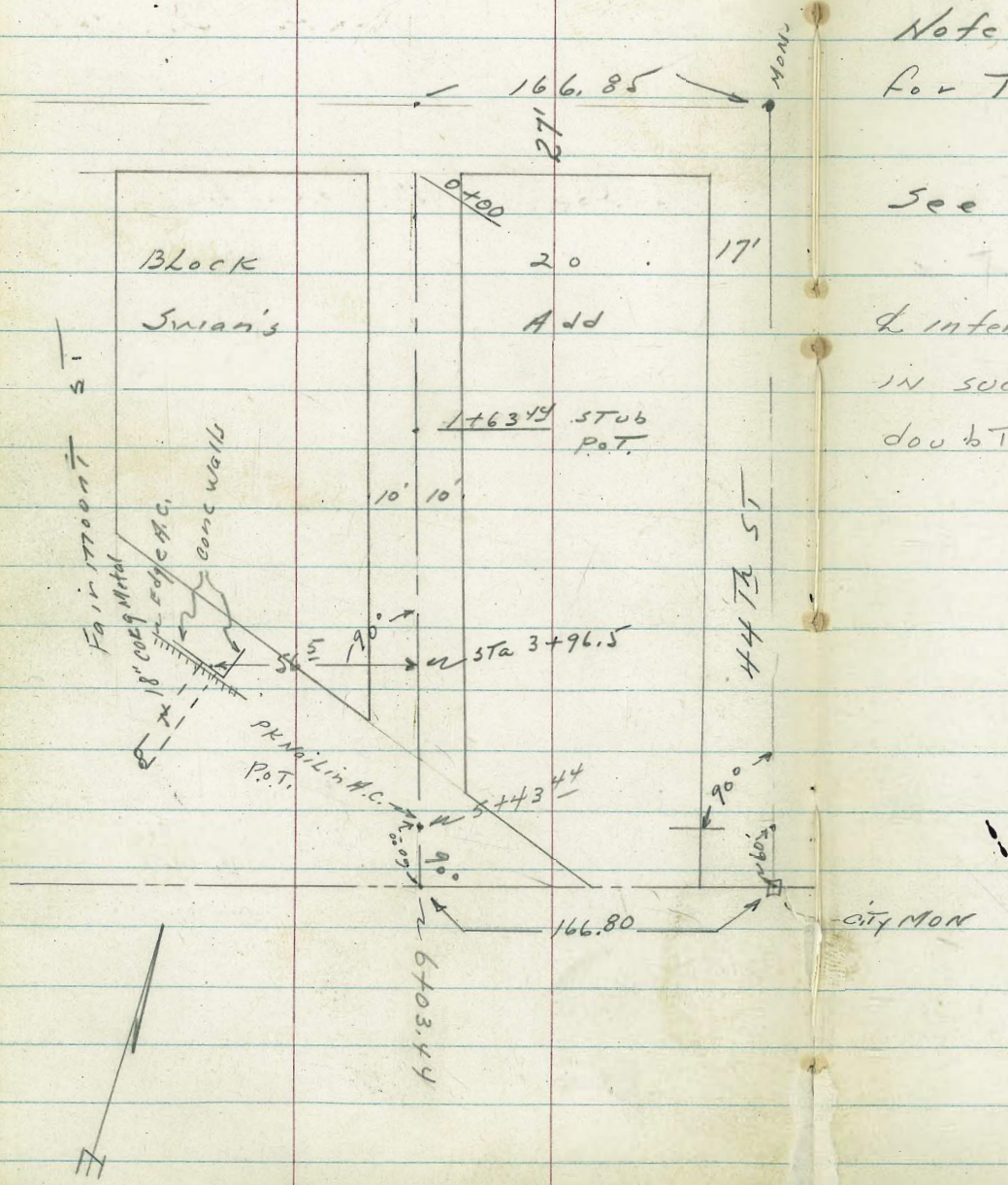
	Lt.	℄	Rt.
1+69.48 = End.			
1+64.1 - Cross fence - 2.5' Lt. = Cor.			
1+61.5 - 5.3' Rt. = ℄ Deadman			
1+50			
1+44 - 5.7 Rt. = ℄ P. pole # P. 4588			
1+30			
1+27.2 - Cross Cyclone fence - 2.5' Lt. = Cor. under const.			
1+23.5 = Toe of Rock wall - loose No Conc			
	49.2 (10)	50.03 on H.b	51.4 (10)
	43.3 (15) Beg Lawn	44.9 (7)	44.7 — 46.0 (10)
	38.0 (15)	38.2 (10) Lawn	40.2 (6) 40.0 — 40.0 (10)
	37.7 (15)	37.8 (7) Beg. Lawn	37.9 (5) 36.8 — 36.3 (10)
1+10	37.3 (15)	37.2 (8 = Beg. Lawn)	36.0 — 35.8 (10)

Re-X-sec Alley Block 20, Swain's Add. See page 50 for Ties @ N'ly end of Block

Note! No information furnished for Tie to Fairmount Ave

See Page 66 for Levels.

& intersection Laurel + alley Block 20 in such deep canyon very little doubt of any use.



Levels Alley Block 20
Swans Addition - See
sketch Page 65 -
See also Page 50

0+84 = Top Fill

0+50 - ON Fill - 7° RT = Top Fill

0+25 - ON Fill - 8° RT = Top Fill
16½ RT = ℄ P.P. # 4378
16° RT = Top Fill
0+00 = Sly Line Laurel - Poorly Compacted Fill

Fill slopes to Canyon on Same Grade

ON Fill Poorly Compacted
0 - 40 = ℄ Laurel ST

TP2	3.32	264.12	9.79	260.80
TP1	2.22	270.59	12.56	268.37
B.M.	0.76	28093		280.17

LT = Ely ℄ RT = Wly

20' Alley

12 25 1.6 / 10
6 16 25 27.5
7 7 25 27.4 / 10
7 5 25 27.6 / 25

16 1 24 47.0 / 10
10 0 5 4 25 47.7 / 7
6 0 25 48.1 / 10
5 0 25 48.3 / 25

15 7 24 48.4 / 10
9 5 25 54.6
3 0 26 0.3 / 00
3 0 26 0.3 / 10
4 5 25 57.6 / 15
4 5 25 57.6 / 25

22 3 23 1.8 / 10
14 2 25 6.5
7 0 25 7.1 / 10
3 6 26 0.5 / 16

Top Fill

31 0 23 3.1 / 10
25 4 23 8.7
18 3 24 5.8 / 10

264.12 T

Laurel ST

Nail in PP # 4375 S Wly Cor. Alley Blk 20 +

NW BP Maple & Fair mount Ave

Alley Blk 20 cont

2+25

TP 0.59 252.52 12.19 251.93

2+00 37° LT = Top Fill

1+75

1+50 - 44° LT = Top Fill

1+25 - 30° LT = Top Fill

1+00

LT = EM & Alley PT = W/S

246.1 6 4 10

246.7 8

247.5 9 10 10

252.52

ON STUB P.O.T. at 1+63.44

246.8 17 3 37° Top Fill

249.1 15 0 10

249.6 14 5

249.9 14 2 8

251.3 12 8 10

252.3 11 8 25

251.1 13 0 10

251.7 12 4

252.1 12 0 7

253.7 10 4 10

254.1 10 0 25

251.1 13 10 44 Top Fill

252.8 12 3 10

252.1 12 0

252.4 11 7 5

254.0 10 6 6

254.3 9 8 10

254.5 9 6 25

252.5 11 6 30 Top Fill

252.6 11 5 10

251.9 11 2

253.3 10 8 3

255.1 9 10 6

257.1 9 0 10

249.5 14 6 20

252.7 11 4 10

257.9 7 2 3 Top Fill

256.7 7 4

255.9 8 2 10

256.1 8 0 25

264.12

Alley Blk 20 cont

3+50				
TP	0.35	227.59	12.89	227.24
3+25				
3+00				
TP	0.61	240.13	13.00	239.52
2+75				
2+50				

LT = Cly ℄ RT = Wtr

220.9 221.7 222.9 223.4 223.7 225.9 224.4 224.4

227.59 ℄

228.6 228.5 229.1

233.8 234.5 234.3 234.9 235.2 237.1 236.3 237.2

240.13 ℄

239.2 239.2 242.0 241.2 241.3

241.9 242.7 243.0 243.5 245.0 246.1

252.52 ℄

Alley Blk 20 cont.

4+75 -13° RT = Nly edge A.C. Pave

4+50 -26° RT = Nly edge A.C. Fairmount

4+25

4+00

3+96.5 56.5 RT = 18" CORG drain under Fairmount

TP 0.36 214.76 13.19 214.40

3+75

LT = ely

Alley

RT = wly

200.8 14° 20

202.0 12° 10

205.1 11 1

203.7 11 1/10

202.71 12.5 13° edge A.C.

202.4 12.4/20

203.9 10.9/10

204.8 10

205.5 9.3/10

205.8 8.9 26° edge A.C.

206.5 8.3/10

207.4 7.4/8

207.2 7 1/2

208.2 6.6/10

209.6 2.5 - 1.2 / 20

210.0 4.8/10

211.4 3 4/10

211.7 BM 1.1/10

212.12 2.16/20

212.67 2.09/56.5 Top Head Wall

209.78 4.98/56.4 I.E. 18" CORG Pipe

214.76 ✱

215.5 12.1/10

217.6 10.0/8

217.2 10.4

217.6 10.0/10

227.59 T

Alley Blk 20 cont

LT = Ely. & RT = Wly

			(148.03)	
		5.80	147.98	BP. Ely of Box Culvert Fairmount & Ely of Home - FB 1561-38
TP	1.40	153.78	12.19	152.38
TP	0.25	164.57	13.08	164.32
TP	0.25	177.40	13.02	177.15
TP	0.32	190.17	13.04	189.85
			el of PK.	
Side Shot		7.45	195.44	ON P.K. Nail in A.C. at 5+43.44
5+30 5 ± = ℄		A.C. Paving	Fairmont	7 5/5 (195.34) 18 2 N'ly of A.C.; 6 6/4 (196.25) 10 A.C.; 6 0/0 (196.89) A.C.; 5 5/0 (197.31) 10 A.C.
5+17 5	10°	LT = N'ly edge	A.C. Pave	5 5/20 (197.4); 4 9/14 (198.0); 5 6/10 (197.26) N'ly edge A.C.; 4 7/2 A.C. (198.17); 4 0/8 10 A.C. (198.81)
4+98.4 =		N'ly edge A.C.	Pave Fairmount	4 1/20 (198.5); 2 9/10 (200.0); 2 3/3 (200.6); 3 0/7 A.C. (199.82); 2 2/4 10 A.C. (200.65)
TP	0.64	202.89	12.51	202.25

202.89 ℄

214.76 ℄

2527 Bar 8' Top of Ground below Street