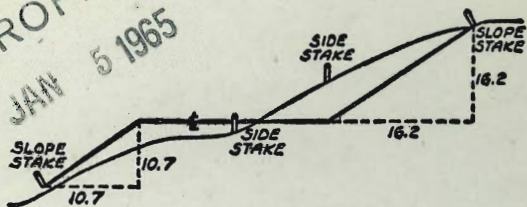


MICROFILMED
 JAN 5 1965



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	34	47	58	69	79	81	92	1.04	1.29	1.42	1.54	1.66
40°	13	26	40	53	67	80	93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	34	51	68	85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	57	76	95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	63	84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	69	93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	27	56	83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	61	91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	36	72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Index

Proposed Sewer Connection Alvarado

Filtration Plant 1-5

Sewer alignment Wing St 8

Check Profiles: 33rd ST SEWER ORANGE to EI CATON 11

INSPIRATION DRIVE - MUIRLANDS SEWERS 13

Proposed Sewer from Alvarado
Filtration Plant to existing
Sewer

Wo# 60015
2-11-53

Ret: City of La Mesa
Drawing - Plan +
Profile of Improvements
of Rasonia
Sheet # 3.

INDEXED

FEB 13 1953

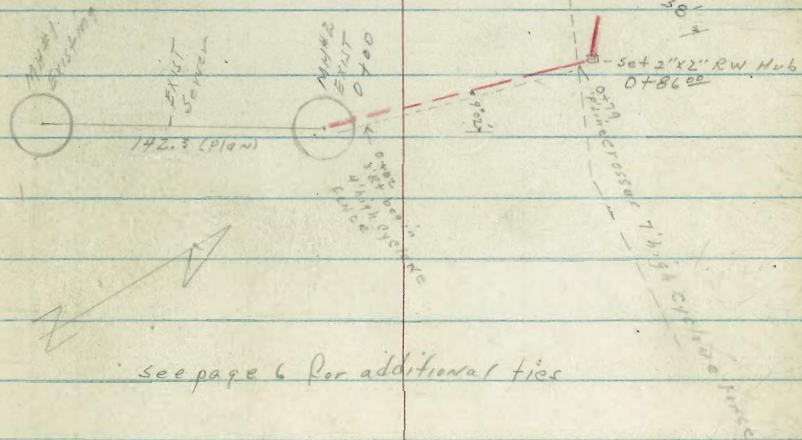
Allen
Sisson
Powell
Schelin

Reduced + Plotted
2-20-53
H. Mills

All elevations

are U.S.C.G.S. datum.

Notes reduced to City Datum
9.01' above U.S.C.G.S.
all El. in Green are City Datum
7' high cyclone fence along
Westerly boundary of Plant
Grounds shown as 1' east of
West bdy.



0+50

0+25

0+06

0+05 - open lateral ditch

0+02 - 3' ht. begin 4' high cyclonic fence

0+00 - Existing Manhole #2

BM. 9.84 541.66

Sp. Ka. in pole # 562923
SE cor Colorado + Oregon.
531.82

USCGS Datum -

LT

526.1
6¹/₂
5

525.6
7¹/₂
5

525.6
7¹/₂

522.7
10⁰

522.07
10⁵⁸
15 Rim. Ground

532.65 City datum
541.66 use CGS datum.

ct.

525.4
7³/₄

525.3
7¹/₂

525.2
7⁵/₈
5

525.3
7¹/₂
5

525.4
7³/₄

ct.

LT

E

RT

0+89- 11° Rt = E dead Man

T.P.

10.74 546.22 6.18

or RW hub 0+86

535.48

537.21

546.22

526.7

6°

5

90° to back line

526.47

6 18

ON

hub

526.3

6 4

5

90° to back line

0+86- L. 84° 38' Lt. set 2"x2" RW.

525.3

7 4

10°

ON Drain

525.1

7 6

824.5

7 9

10°

ON Drain

0+81- E crosses 4' wide black top drain Parallel to
fence - rubble conc. curb forms West side of Drain

0+79- 4° Lt = E High Voltage Junction box

0+79- 3° Rt = end 4' high cyclone fence

7' cyclone fence is 1' back of property line

0+79- E crosses 7' cyclone fence w/ rubble conc
base

0+76- 2° Lt = E 8' power pole #(?)

525.6

7 1

5

525.6

7 1

532.65

541.66 x

525.4

7 3

5

0+75

1492⁵ - $\frac{1}{2}$ intersects 6" Curb around parking Area

1487 - 0⁵ Lt = $\frac{1}{2}$ 3" Eve tree

1475 - 11¹ Lt = $\frac{1}{2}$ 7' cyclone fence

1471 - 3³ Rt = SW car parking area

1450 - 10² Lt = $\frac{1}{2}$ 7' cyclone fence

1449 - 4¹ Rt = $\frac{1}{2}$ 1' tree

1425 - 9⁶ Lt = $\frac{1}{2}$ 7' cyclone fence

1400 - 7⁵ Lt = $\frac{1}{2}$ 7' cyclone fence

Lt

Rt

Rt

7

532.1

532.49

Rt

7

Gr

Gr

Black Top

528.7

528.0

528.6

532.5

532.5

532.67

532.25

8⁵

9²

8⁶

4²

4²

4¹

4⁹

11¹
Top Drain

9²
Drain

7²
Top Drain

2⁶
Gr

2⁶
Top Cb

10²
Black Top

532.3

532.70

532.20

4²

4⁵

5⁰

3²
Gr

3²
Cb

3²
Parking Surface

527.2

526.9

527.6

530.1

531.4

531.9

10²
Top Drain

8²
Drain

6²
Top Drain

5²
3

5³
10

527.0

526.2

526.9

528.8

528.9

10²

11⁰

10³

8⁴

7³

9⁵
Top Drain

7²
Drain

5⁰
Top Drain

10

526.2

525.6

526.3

522.4

528.5

11⁰

11⁶

10²

9⁸

8⁷

7⁵
Top Drain

5⁵
Drain

4¹
Top Drain

10

537.21

546.22

LT

⊥

et

USCGS Datum

TP₃ - Start. BM. 9.94 531.83

TP₂ 3.09 541.77 7.54 538.68

R+26^L = Existing Man hole - 8" Sanitary Sewer
from Filtration Plant

R+23- 9^o Lt = ⊥ 10" power pole # 277145

R+00- 13^o Lt = ⊥ 7' high cyclone fence

522.7	528.9	529.5	532.3	532.37	531.84	531.99
75	8 ³	72	42	484	537	522
13 ^o	11	9 ²	4	1.4	Black Top	10 ^o
Top	R	Top Drain		Top Cb		Black Top

537.21
546.22

525.84

531.53

1187
I.E.

568
Rim
⊥

H.I. 5.56
 00 1.62
7.18
 541.50
534.32

HAND LEVEL

GUTTER EL

3.00

525.12
527.92 GUT. EL
 530.92 = H.I.

TOP COND. AT FENCE

5.1

525.82 EL

TOP " " NORTH SIDE

5.1

525.82 EL

H.I.

5.63

527.92 GUT EL
5.63
 533.55 = H.I.

20' SO. M.H. IN DITCH

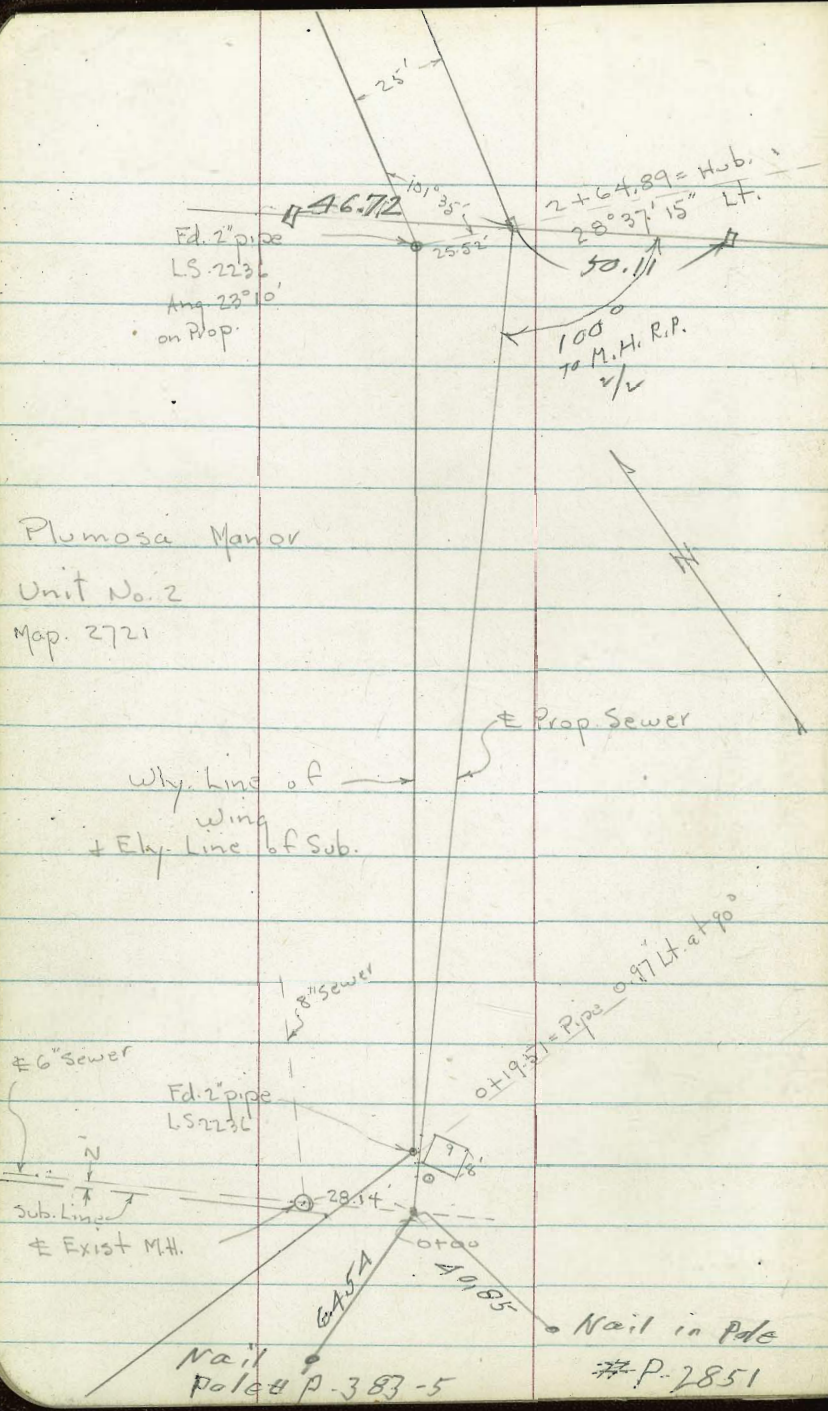
1.4

532.15 = EL

3' R FROM DITCH UP 1.7'

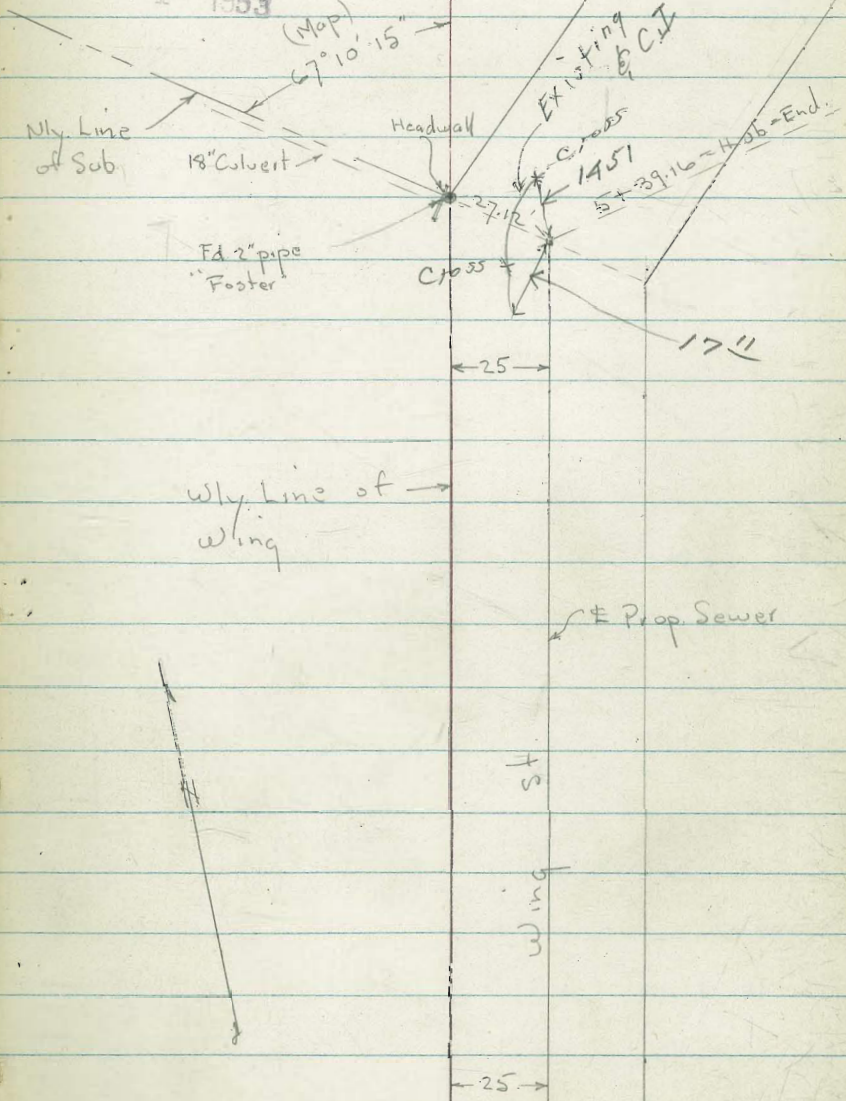
533.85 EL

Plumosa Manor
Unit No. 2
Map. 2721



INDEXED

JUN 1 1953



Begin Levels along \pm of Prop. Sewer
in Wing st. - See sketch P 8

#7058

W.O. 21117 - 5-29-53 - 7.0.

1+00

46.7 41.4 41.3 41.8
25 8 25

0+50

47.7 43.5 43.4 44.0
25 4 25

0+20 - 3' Rt. = Cor. Conc. Tank

48.3 45.2 44.9 45.0 45.70
30 13 9' 3
Top
Cor.

Conc. tank - 8' N+S. - 9' E+W. - pump House on top.

0+12.2 - 0.7' Rt. = Cor. of Conc. top to Exposed

45.2 45.67 45.68
0.7' = Top at Cor.
Conc.

0+09 - 3.3' Rt. = \pm MH. to tank (underground)

46.52 = Top - Rim

Note: Looks like a tap & line ahead is thru tank

0+0.0 - outs. to Lt. are along Sewer line

45.39 49.65 47.4 46.1 45.65 45.4
I.E. TOP 28.14 20 on Hub. 20
at of Rim ground at 90°
2

#P. 2851

Set B.M. in Pole opp. Pump House

48.82

B.M. = S.E. B.P. - Homer + Chatsworth

83.63

Actual Elev. Shown.

Lt. \pm Rt.
INDEXED
JUN 1 1953

Sect. B.M. - N.E. Cor. of Headwall = 0 37.15

5+39.16 = \pm on Sub. line prod. = End
outs. on Sub. line

5+33 = \pm Exist Wash from Drain on Lt.

5+00

4+50

4+00

3+50

3+00

2+64.89 = Ang. Pt. - Sect. on split

2+50

2+00

1+53 - 15' H. = \pm Guy Pole

1+50

Lt.

\pm

Rt.

37.15

Top of
Wall

33.1

27.12
gr. in
wash

35.9

20

34.14 = on Hub.

32.7

32.4

25

37.3

25

32.8

31.5

25

36.7

25

33.0

32.1

25

36.2

25

33.9

33.8

25

36.7

25

34.8

34.8

25

36.8

25

36.3

36.0

25

37.60

25.52 =
on pipe

37.20

on Hub.

38.4

25

38.3

25

37.9

38.5

25

42.5

25

40.2

15

39.5

39.4

25

46.3

25

40.8

40.7

25

Clark
Shepherd
Brumer
ONEIL

7-15-53.
20910-W.O

CHECK PROFILES - 33rd St. SEWER
ORANGE TO EL CATON

Elev's 5' offset
w/ly &
GRADE BOOK
EXIST. (7-15-53)
EXIST. & (7-15-53)
shots along & #2145-60 (7-15-53)

Elev's
& Sewer

Elev's 5' offset

Elev's
& Sewer

STA.	GRADE BOOK	EXIST. (7-15-53)	EXIST. & (7-15-53)	shots along & #2145-60 (7-15-53)	STA.	GRADE BOOK	EXIST. (7-15-53)	EXIST. & (7-15-53)	shots along & #2145-60 (7-15-53)
17+52				369.48 M.M.H.	17+10	371.47	371.47	371.45	
17+35	369.11	369.08	369.28		17+00			371.24 371.28 371.27	
17+00	368.59	368.58	368.84	368.47	18+75	371.11	371.08	371.08	
From 17+00 on shots taken Along & as shown #2145-60 As further elev. (shots taken only at same station #2145)		to 368.47			18+79.8 - & BRANSON PL.			370.49 370.61 370.70 5 5 5	
16+65	368.28	368.27	368.42		18+40	370.51	370.47	370.58	
16+30	367.75	367.74	367.95		18+38			370.45 &	
15+95	367.35	367.35	367.62		18+05	369.97	369.95	370.09	
15+60	366.92	366.92	367.12 M.M.H.		18+00			369.68 369.95 370.07 5 5 5	
Note: stations with red dot = CONST. STA. others are STA's on side As shown #2145-60					17+70	369.53	369.46	369.62	
15+24.30 (ahead) (= 15+36.30 BACK) (see notes) M.H. 33rd VORONGE	366.20	366.20	366.59 M.M.H.						
B.M. Dir. Elev. Rod.			366.76 2145-60	N.W. B.P. ORANGE + 33rd					

STA.	Elev's 5' offset		EXIST. 7-15-53	Shots along E 2145-60 7-15-53
	GRADE Book	EXIST. (7-15-53)		
21+00				372.83 5 372.71 5 372.76
20+85	373.66	373.54	373.48	
20+50	373.13	372.98	373.06	
20+15 m.H. #7	372.58	372.51	372.58 RIM M.H.	372.58 5 372.41 5 372.42 5 372.56
20+00				
19+92.3				372.30 5 372.39 4 RIM M.H.
19+80	372.29	372.24	372.16	
19+45	371.87	371.82	371.74	
19+25				371.59 5 371.60 5 371.58

STA.	Elev's 5' offset		EXIST. (7-15-53)	Shots along 2145 -60 7-15-53
	GRADE Book	EXIST. (7-15-53)		
CHK:				366.76 = 366.76 (See B.M.)
22+58.68 = M.H. 8	374.82	374.81	374.98	
22+25	375.19	375.17	375.17	
21+90	374.79	374.78	374.79	
21+71.2 = 5' by CR LINE ELEVATION				374.44 374.49 374.52 5 5 5
21+60				374.51 374.54 374.48 5 5 5 M.H. M.H. M.H.
21+55	374.60	374.55	374.55	
21+20	374.21	374.12	374.03	

Proposed Sewer in Inspiration Drive
The Meirlands and La Jolla Highlands

C. Allen, D. Sisson, C. Powell

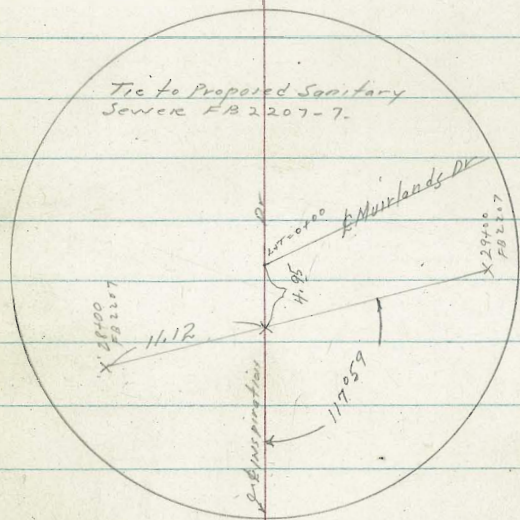
Ref. opening sheet Inspiration Dr

File Maps 2024, 2546.

See Also FB2207-7

Wd# 21075

7-22-53



sty line The Meirlands

NECOR
2" T 11= 8172.06

Inspiration Drive

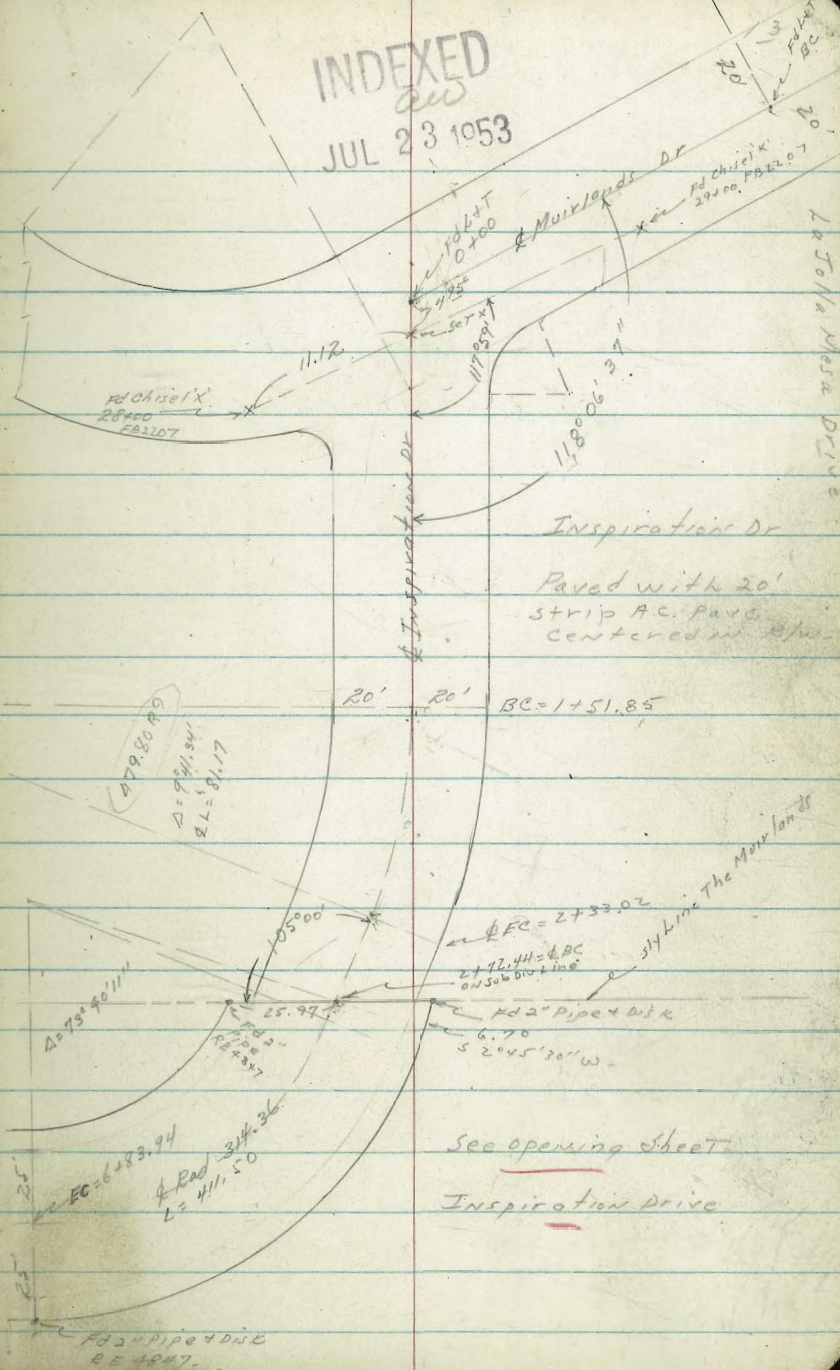
FD 2" PIPE
RE 4847

11

10

INDEXED
RW

JUL 23 1953



See opening sheet

Inspiration Drive

Levels for Proposed Sewer
in Inspiration Drive - Muirlands
See sketch page 13

0+53³⁸ - 20' LT = Prop EC on West

0+50 - 73⁵ LT = Stucco House

0+27.24 - 20' LT = Prop EC

0+11¹ = Styedge Portland Concrete +
Begin AC Pav

0+04⁹⁵ intersection with Plm Sewer Muirlands Dr

0+00 = intersection Inspiration Drive.
Muirlands Dr +

BM. 4.13 524.78 520.65

LT = Ely

et = wly 14

521.77	520.53	520.58	
301	4 ²⁵	20	
735 Floor elev.	10 Elyedge Ac.	520.50	520.15
		28	4 ⁶³
			10 Wlyedge Ac.
		519.93	
		85	
	519.82	519.60	519.31
	4 ⁹⁶	18	5 ⁴⁷
	25		25
		519.55	
		23	
		519.50	
		20	

Notes Reduced
7-23-53
R. Larson

524.78 x

Plm Sewer Line Muirlands Dr

See FB

2+33° = EC

2+15- 28° LT = Large Stucco House

1+75 ON CURVE

T.P, 11.48 535.86 0.40 524.38

Parallel to ϕ
1+68 \approx 10' LT = NW COR 6' CURVE WALK

1+51.85 = BC LEFT

1+00 - 10' LT + 10' RT = edges AC, Pave

LT = e1y

ϕ returnly

15

	528.72		528.91	529.58
	7.14		6.95	1.28
	10' edge AC + walk			10' edge AC
529.36	527.88		527.96	527.66
6.50	7.98		7.91	8.20
28° Floor House	10' Edge AC No curb			10' edge AC
	525.68		525.68	
			10.18	

535.86 x

	524.23		524.37	524.09
	0.55		0.41	0.69
	10' edge AC			10' edge AC
521.84	521.84		521.80	521.38
2.94			2.98	3.40
10' edge pave				10' edge AC

524.78 x

Levels for proposed Sanitary
Sewer in & Inspiration Drive
La Jolla Moorlands & La Jolla Highlands

3+50

3+25

3+15-70³ LT = & Large Front House

3+02 6° RT = & 3' in dia gas co MH.

3+00

2+96- 4° RT = & 2⁵/₈ in dia Telephone co MH.

and the Wylhine La Jolla Highlands

2+72⁴/₄ BC RT + Intersection & Inspiration Dr
Parallel to line - No. curb:

2+69- 10° LT = SW CURB 6' CONC WALK

LT = E14

532.41

3⁴/₄
10°
edge AC

530.85

5⁰/₁
70²
Floor

531.20

4⁶/₆
10
W edge
AC

532.57

531.69

531.76

531.40

530.63

535.86 x

RT = W11.15 26

532.15

3⁷/₁
10°
edge AC

531.35

4⁵/₁
6°
RM

531.12

4⁷/₄
10
W edge
AC

531.31

4⁵/₂
4°
Rim

524.4

11⁵/₅
6°
BOTTOM
BOX

524.31

11⁵/₅
4°
BOTTOM
BOX

5400

4475

TP₂ 2.19 535.37 248 533.18

4450

4425

4400

out taken Radial. tod
3475-100° NT = d Fronte House

50.
LT = 017

532.96
241
95
edge
AC

533.19
267
100
edge
AC

533.03
283
edge
AC

526.31

955
100°
Floor

d

532.97

240

533.16

221

535.37 T

533.20
266

533.16

270

533.02

284

532.86

210

535.86

RTW 14 77

532.48

289

105
edge AC

532.69

317
100
edge
AC

532.61

325

10
Nowly edge
AC

LT = 50 E17

6+25-79⁵ Rt = ϕ Brick + Frame House

6+04 5⁸ Rt = ϕ 3' dia Gas Co M.H.

6+00

5+98- 4⁰ Rt = ϕ 2⁵ dia telephone Manhole

5+75

5+50

5+25

530.84

507

530.81

456
10⁰
edge AC

530.91

446

531.62

375

532.27

310
95
edge
AC

532.23

374

532.70

267

535.37

Rt = Newly 18

535.34

003

795
Floor House

530.67

470

5⁸⁰
Rim

530.59

478
10
edge AC

530.90

447

4⁰
Rim

531.67

370
105
edge AC

521.7

137

5⁸⁰
BOTTOM
Box

523.37

120

4⁰
BOTTOM
Box

Levels Proposed Sanitary Sewer
in & Inspiration Drive Muirlands &
La Jolla Highlands

- 8400

FP₃ 2.44 524.49 13.32 522.05

7450

we cant do rock Pak this fellow
7420 - 188° LT = & Stucco House

7400 - 61° RT of Conc Block House

6483^{9d} = E.C.

6450

LT = 514

521.53

10
edge
AC

524.47

10 90
10°
edge AC

501.2

34²
188°
Floor

527.12

825
10°
edge
AC

529.17

620
10
edge
AC

521.76

524.49 π

524.91

10 46

527.52

785

528.31

16

529.47

590

535.37 π

RT = 514 19

521.35

10
edge AC

524.49

10 88
10
edge AC

527.28

807
10
edge AC

529.23

614
10
edge
AC

531.10

427
6/8
Floor

LT = 514

Rt = N14 - 20

(527.45)

TP₂ BM.

3.34 527.44

IN Previous Survey - House is on rt corner station 7400
SW Cor. Lower Brick step. House left of station 9400

TP₄

8.73

530.78 2.44

522.05

La Jolla Highlands

7 9+25-98° LT = ϕ Frame house on Lot 11.

511.04

13 1/2

980
Floor

515.18

931

100
edge
PC

515.52

997

524.49

920

10
edge AC

7 9+00-

house

7 8+90-103° Rt = ϕ Long rambling Stucco

530.48

321

1030
Floor

RE 9847.

8+78.06-25° LT = NE COR Lot # 11 - Fd pipe + disk

527.81

588

50
Rim

511.2

13 1/2

50
Bottom
Box

7 8+52.56 Rt = ϕ 3' dia Gas Co MH.

6 8+50

511.61

12 88

950
Floor

528.16

553

41
Rim

511.4

13 1/2

41
Bottom
Box

6 8+47.4' Rt = ϕ 3' dia Telephone MH.

8+30-95° LT = ϕ Frame + Stucco House

524.49 x

106' Lt. + Pick up pt.
from E St.

36' from prop. line
of Lot North

			10.8
			.2
5.5			10.3
5.4			10.4
		5.3 5.2	5.2
5.5	5.5	0.0	0.0
		3.4	
	5.5		
5.5	H.1 π	0.0	

Cont. bottom
Rt. 29

Alley

10' x 21462

10' →

15
pt 2145

10' x 18405

10' →



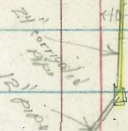
Cont. pg 25
L. Bottom

24

10' →

92
x 24445

1204 St

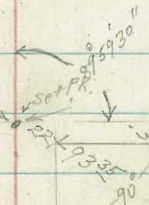


98
x 23427

Ave

Adams

SE.
676 Edge wall
Adams
To F.I.D.T 15686



SW Corner
Adams
11522 To F.I.D.T 676

Cont from pg 23

Cont from top
L. B.

"X" Sec Sewer Copeland Ave
 Monroe - 42nd St
 Lt-Wly

Lt-Wly E RT-Ely 26

Notes reduced 5-24-54

1+25
 1+50
 0+75
 0+50
 0+25
 0+00
 BM

Copeland Ave
 15° At to ob line Ely
 25° At to ob line Wly

364.54	364.39	364.24
6 ³³	6 ⁴⁸	6 ⁶³
5	5	5
364.69	364.56	364.42
6 ¹⁸	6 ³¹	6 ⁴⁵
5	5	5
364.83	364.75	364.60
6 ⁰⁴	6 ¹²	6 ²⁷
5	5	5
365.03	364.93	364.79
5 ⁸⁴	5 ⁹⁴	6 ⁰⁸
5	5	5
365.13	364.98	364.85
5 ⁷⁴	5 ⁸⁹	6 ⁰²
5	5	5
364.99	364.87	364.74
5 ⁸⁸	6 ⁰⁰	6 ¹³
5	5	5

2+75
 2+50
 2+25
 2+00
 1+75
 1+65
 1+50

Flows N+S
 1+65 7⁵ Lt & SMH

347.24
 364.24
 23⁶³ 6⁶³
 7⁸ 7⁸
 1e 111

363.42	363.27	363.09
7 ⁴⁵	7 ⁶⁰	7 ⁷⁸
5	5	5
363.60	363.47	363.32
7 ²⁷	7 ⁴⁰	7 ⁵⁵
5	5	5
363.79	363.67	363.55
7 ⁰⁸	7 ²⁰	7 ³⁴
5	5	5
363.96	363.83	363.69
6 ²⁸	7 ⁰⁴	7 ¹⁸
5	5	5
364.14	364.00	363.83
6 ²³	6 ³⁷	7 ⁰⁴
5	5	5
364.33	364.20	364.06
6 ⁵⁴	6 ⁶⁷	6 ⁸¹
5	5	5

6⁴⁰ x 370⁸⁷

364⁴⁷ N.W.B.P.
 Monroze Copeland.

x 370⁸⁷

Lt = Wly

Rt = Ely

Lt = Sly

Rt = Nly

27

4450

361.71
6²²
5361.43
6⁴⁹
5361.19
6⁷³
5

362.29

362.18

362.07

4425

5⁶³
55⁷⁴
55⁸⁵
5T₁6³⁴ T 367.929²⁹
362.45

362.37

361.58
362.21

4400

8⁴²
58⁵³
58⁶⁶
5

362.63

362.53

362.38

3775

8²⁴
58³⁴
58⁴⁹
5

362.81

362.71

362.56

3450

8⁰⁶
58¹⁶
58³¹
5

362.96

362.87

362.74

3425

7²¹
58³⁰
58⁴³
5

363.16

363.04

362.90

3400

7²¹
57³³
57⁴⁷
5

T 370.87

6400

363.93
3²²
54⁰³
54¹³
5

363.77

363.36

363.24

5775

4⁵¹
54⁵⁶
54⁶⁸
5

362.93

362.90

362.79

5450

4⁷⁹
55⁰²
55¹³
5

362.95

362.91

362.36

5425

5⁴⁷
55⁵¹
55⁵⁶
515° 41' 0" S 40° E
28° 41' 0" N 42° E
Morroco

5100 36° RT & SMH

361.91

361.86

361.80

4485 45° RT & SMH

6⁰¹
56⁰⁶
56¹²
5

361.50

361.29

360.98

4475

on split

L. Pt 89° 58' 30"

6⁴²
106⁶³
106⁹⁴
10361.80
36° 11' 10"353.37
36° 10'361.48
6⁴⁴
11m347.69
4⁵
1220²³
6"
10
370.87

Lt = Sty

365.23
5 18
365.13
5 13
365.11
5 15

7+55

TP₂

419 T 370²⁶

366.52
140
94
114

366.46
185
194
10

366.02

7+35 9° Lt E SMH

140
94
114

366.59
366.46
366.19

7+29²⁹ L. Pt 90° 12' 30"

133
10
146
10
173
10

7+00

365.92
118
199
115

365.44
248
249
268

6+75

364.94
298
297
308

364.46
346
364.43
349
364.34
358

6+50

6+25

T 367⁹²

Lt = Wly

Pt = Fly 28

9+00

364.57
5 69
364.30
5 96
364.05
5 221
364.99
5 527
364
49
24 26

8+97 10° Lt E SMH

348.39
247
350.35
192
10
10
10
119

364.80
5 46
364.73
5 53
364.55
5 71
364.26
5 13
364.63
5 13

8+75

365.00
5 16
364.73
5 33
364.95
5 181
364.79
5 117

8+50

365.21
5 58
364.85
5 31
364.65
5 61
365.02
5 24

8+25

365.43
5 58
365.22
5 04
364.87
5 39
365.30
5 42

8+00

365.56
4 20
365.39
4 87
365.09
5 17
365.44
4 77

7+75

5° Pt to Fly 06
25° Pt to Fly 06
42° Rd St.

T 370²⁶

	Lt=Why	\$	Rt=Ely
10+75	7 ¹⁵	363.11	7 ¹⁵ 362.46
	5		5 362.54
			5 362.65
			5 362.19
10+50	6 ⁹³	363.33	7 ²⁰ 363.06
	5		5 362.80
			5 363.19
			5 363.19
10+25	6 ⁷¹	363.55	7 ¹⁹ 363.07
	5		5 363.19
			5 363.19
			5 363.19
10+00	6 ⁴⁷	363.79	6 ⁶⁸ 363.58
	5		5 363.33
			5 363.75
			5 363.57
9+75	6 ³⁰	363.96	6 ⁵² 363.74
	5		5 363.55
			5 363.57
			5 363.57
9+50	6 ¹²	364.14	6 ³⁵ 363.91
	5		5 363.70
			5 364.05
			5 363.91
9+25	5 ²⁹	364.32	6 ¹⁷ 364.09
	5		5 363.86
			5 363.91
			5 363.91

370²⁶

	Lt=Why	\$	Rt=Ely
12+80	4 ³⁴	361.83	4 ⁶⁴ 361.63
	5		5 361.36
			5 361.61
			5 362.03
12+25	4 ²⁰	362.07	4 ²¹ 361.96
	5		5 361.61
			5 362.03
			5 362.03
12+00	8 ²¹	362.25	8 ²⁷ 361.99
	5		5 361.74
			5 362.19
			5 362.19
11+75	7 ⁸⁴	362.42	8 ¹² 362.14
	5		5 361.91
			5 362.00
			5 362.00
11+50	7 ⁶⁵	362.61	7 ²¹ 362.35
	5		5 362.12
			5 362.53
			5 362.53
11+25	7 ⁵²	362.74	7 ⁷⁶ 362.50
	5		5 362.28
			5 362.67
			5 362.67
11+00	7 ³³	362.93	7 ⁵⁵ 362.71
	5		5 362.83
			5 362.89
			5 362.89

370²⁶

on Five Hpd
N.E. cor
42nd St
7/27

Lt. Why

360.69
5⁵⁸
5
360.40
5⁸⁷
5
360.10
6¹³
5
360.46
5⁸¹
5
194⁰⁶

14125

360.79
5⁴⁸
5
360.54
5⁷³
5
360.21
6⁰⁶
5
360.62
5⁶⁵
5

14750

360.98
5²⁹
5
360.71
5⁵⁶
5
360.38
5⁸⁹
5
360.79
5⁴⁸
5
194⁰⁶

10 4375

361.15
5¹²
5
360.84
5⁴³
5
360.50
5⁷⁷
5
360.92
5³⁵
5
194⁰⁶

10 13750

361.32
4²⁰
5
361.02
5²³
5
360.73
5⁵⁴
5
361.14
5¹³
5
194⁰⁶

97 13725

361.51
4⁷⁶
5
361.24
5⁰³
5
360.92
5³⁵
5
361.23
4²⁴
5
194⁰⁶

97 13700

361.70
4⁵⁷
5
361.43
4⁸⁴
5
361.14
5²³
5
361.50
4¹⁷
5
194⁰⁶

97 12775

366.27

Lt. Why

RT-ELY

15775

361.53
4²⁴
5
361.43
4⁵⁴
5
361.55
4¹⁸
5
361.6
4²
5

15750

361.23
5⁰⁴
5
361.19
5²⁸
5
361.4
4¹⁹
5
361.9
4⁴
5

15725

360.70
5³⁷
5
360.89
5³⁹
5
361.1
5²
5
361.4
4²
5

15700

360.26
5¹⁵
5
360.22
5⁵³
5
361.0
5¹⁰
5
361.0
5¹
5

14785 1374 26 water gate

14775

360.66
5⁶¹
5
360.99
5²⁸
5
360.48
5⁷⁹
5

14754 105 Lt RSMH

349.17
17¹⁰
105
Why
349.23
17⁰⁴
105
Why
349.06
17²¹
105
Why
361.46
4²¹
105
Why

1474959

361.24
5²³
5
361.08
5²⁴
5
360.85
5¹²
5

366.27

17725

Lt-Wly RT-Ely

362.58
362.55
362.4
362.36
362.4
362.7

362.40
362.36
362.4
362.7

362.18
362.15
362.7
362.4

362.09
362.08
362.2
362.4

362.03
362.05
362.39
362.03
361.90
361.99
362.10
362.40

361.77
361.66
361.7
361.8
361.92
362.27

361.77
361.66
361.7
361.8

366.27

17700

16775

16750

16731 E crosses Nly edge con apron to garage

16725

16712 E crosses sly con apron to garage

16700

TP4

Lt-Wly

368.39
363.03
363.27
363.47

18750

18725

18705 105 Lt-Sly

18700

17775 0° RT Nly edge con apron

17755 0° RT Sly edge con apron to garage

17750

362.99
363.03
363.27
363.47
362.95
362.91
363.1
363.4
363.11
349.77
363.02
362.90
362.77
362.80
362.77
362.80
362.87
363.20

366.27

20425

Lt-Wly 363.24
5¹⁵ 5²⁰ 5¹ 4⁸
3
pool
Ac. edge

Rt-Wly 363.19
363.3
363.6

20400

363.46
4⁷³ 5⁰² 4² 4⁸
5
2
pool
Ac. edge

363.5
363.8

19775

363.57
4⁸² 4²⁰ 4⁴ 4⁵
5
3
pool
Ac. edge

363.99
364.0
363.9

19750

363.53
4⁸⁶ 4⁹⁸ 4² 4⁸
5
3
pool
Ac. edge

363.41
363.5
363.6

19725

363.38
5⁰¹ 5¹² 4⁹ 4²
5
3
pool
Ac. edge

363.27
363.5
363.7

19700

363.26
5¹³ 5¹⁸ 5⁰ 4²
5
3
pool
Ac. edge

363.21
363.4
363.7

18475

363.16
5²³ 5²⁹ 5² 5¹
5
3
pool
Ac. edge

363.10
363.2
363.4

368.39

Lt-Wly

Rt-Wly

21753 2⁵ Lt & water valve

361.07
7²² 7³³
5
9²
Ac. edge

361.94
361.04
361.30

21745 & crosses Wly cov apron

361.46
6²³ 7³ 7⁰¹
5
9²
Ac. edge

361.26
361.38
361.54

21728 & crosses Sly cov apron to garage

361.84
6⁵⁵
5

362.02
6³⁹
5

21717 02 At 2' cov walk

362.09
6³⁰ 6⁴⁷
5
Ac. edge

361.92
362.5
362.44

21700

362.11
6²⁸ 6²
5
Ac. edge

362.18
362.44

20795 & crosses Wly cov apron

362.67
5⁷⁸ 5⁸³ 5⁷⁴
5
0²
Ac. edge

362.56
362.62

362.65
5⁷⁴
5

362.91
5⁴⁸
6

20772 & crosses Sly cov apron to garage

363.01
5³⁸ 5⁴⁹ 5³ 4⁸
5
3
pool
Ac. edge

362.90
363.1
363.6

20750

368.39

22+75

Lt=Wly ♀ 356.78
11.61 11.78 11.62
5- 5- 5-

22+50

357.68
10.71 10.24 10.60
5- 5- 5-

22+34 ♀ crosses Sly AC parking Area

358.07 358.11 357.79
10.32 10.28 9.28
05- 5- 5-

22+25

358.57 358.45 358.39 358.9
9.82 9.24 10.0 9.5
5- 5- 5- 5-

22+100

359.49 359.32 359.3 359.5
8.20 9.07 8.7 8.7
5- 5- 5- 5-

21+75

360.27 360.10 360.59
8.38 8.29 7.8
5- 5- 5-

21+71 2⁵ LI & 6" water valve

350.37 350.27 361.19
18.02 18.12 7.20
10- 10- 10-
wly N+S rim

21+62 10" LI & SMH

18.02 18.12 7.20
10- 10- 10-
wly N+S rim

X 368.39

Lt=Wly ♀

RT=Ely 33
352.23
16.16
5-
re inlet

23+58 5" RT of a 5" cl opening inlet 24 corrugated runs Nly see sketch p 24

23+53 5" H to ed

23+50

354.86 354.66 354.70
13.53 13.73 13.69
5- 5- 5-

23+37 17" LI & 3'x3' gas vault

23+27 9" LI & SMH

352.21 350.44 355.70
17.63 17.20 17.29
9.8 9.8 9.8
10- 10- 10-
wly N+S rim

23+25

355.62 355.61 355.63
12.77 12.28 12.26
5- 5- 5-

23+100

355.65 355.66 355.70
12.74 12.73 12.69
A.C. A.C. A.C.
2091 2091 2091

22+88 ♀ crosses Nly AC parking Area begin paving (AC) Adams Ave.

356.02 355.99
12.37 12.30
5- 5-

T 368.39

25+00

LT=Wly 359.24
95 92
5 8
RT=Elly 359.18
92 359.2

24493 50 ft end cl walk

359.46
99.93 10
5 10
359.21 95 92
5 8
359.4 95 92
5 8
359.41 95 92
5 8

24475

358.02
10.23 10.26
5 5
357.53 11.27 10.66
5 5
357.32 357.73

24450

350.75
17.49 17.45 10.67
92 92 92
10 10 11
N+S N+Y

24444 5 93 LT E SMH

357.07 356.87 356.81 356.69 357.12
11.32 11 11.52 11.58 11.20 11.27
5 5 5 5 5

24425

356.18 356.05 355.78 356.33
12.21 12.34 12.41 12.06
5 5 5 5

24400

355.59 355.40 355.10 355.68
12.20 12.29 13.29 12.27
5 5 5 5

23475

368.39

LT=Wly RT=Elly 34

26425

360.01 359.88 360.12
351 364 34
5 10 5

26400

360.35 360.24 360.3
317 328 32
5 10 5

25475

360.44 360.42 360.5
308 310 310
5 10 5
360.34 360.34 360.13 360.25
315 328 339 327
5 12 5

25454 12 ft Wly cov apron to garage

359.98 360.17
354 338
10 5

25439 10 ft Sly cov apron to garage

360.04 359.94 359.81 359.83
378 358 371 369
5 14 5

25433 14 ft Wly edge cov apron to garage

359.47 359.60
405 392
12 5

25413 18 ft Sly edge cov apron to garage

TPs 459 363.52 946 358.23

Lt. Wly
356.45
707
5
356.48
734
5
356.49
703
15
356.42
710
5

27777 1st RT sly cont apron to garage

356.15
677
5
356.17
678
25
356.71
678
5
356.75
677
5

27451 2nd RT Nly AC apron

3rd RT sly
27730 crosses AC apron to garage

357.10
672
3
357.12
670
5
357.22
630
5
357.16
636
5
357.3
630
5

27425

27400

357.93
539
5
357.97
555
5
358.4
551
5

26775

358.76
476
5
358.70
482
AC
359.3
472
5

26450

359.42
470
5
359.38
474
AC
359.8
37
5
350.60
1262
93
111

26437 9th Lt ESMH

π 363 ⁵²

Lt. Wly
357.56
526
5
357.56
524
5
357.47
628
5

29425

29420 2nd Lt E 6" watergate

29400

357.20
632
3
357.25
627
10
357.3
670
5

28775

356.90
662
5
356.67
625
5
356.71
621
10
357.1
64
4
357.6
652
5
356.96
656
4
356.71
621
5

28455 E crosses Nly AC apron

28438 E crosses sly AC apron to garage

28425

356.56
696
5
356.66
598
5
356.49
703
5
356.52
718
AC
356.7
619
5

28400

356.31
721
5
356.42
710
AC
356.9
66
5
356.51
721
15
356.54
5198

27794 1st RT Nly cont apron

π 363 ⁵²

25

Lt = Nly

357.98 Rt = Sly
544

30+75

358.45
507

30+50

357.42
510

30+25

357.29
513

30+00

357.13
539

29+75

357.63
519

29+54

357.40
12^R 5.65
9^L 11M
1e 92

29+46 5/1 94 Lt & SMH

on dia

29+46 5/1 91 Lt & 91 53

357.92
357.80
5⁶⁰ 5¹² 5⁸⁸
10 10

357.64

7363⁵²

Lt = Nly

Rt = Sly

36

SE 6' 1/2' Bond Dr
+ Adams Ave

BM

338 357⁴⁹

4005
357⁴⁴

TP

069 360⁸⁷

334 360¹⁸

30+9/16 & SMH

end line

346.13
16²⁹ 5¹¹
same 1e rim

363⁵²

X Sec Madison Ave Line

42nd to Van Dyke
Lt-Nly Rt-Sly

1425

359.46
344
5

359.38
349
5

359.23
364
5

1400

359.73
344
5

359.64
323
5

359.44
343
5

0725

359.98
289
5

359.86
320
5

359.70
317
5

0750

360.20
267
5

360.00
287
5

359.88
299
5

0425

360.44
213
5

360.32
255
5

360.09
278
5

0400 Ely

1444959 125

361.08
179
5

361.03
184
5

360.90
192
5

184 + 362.87

361.03

2. PK Nail
1444959
P.30 - 0400

Lt-Nly

Rt-Sly

37

2487 5° Lt ESMH

350.02

1285

552

same

58

58

10

111

2475

357.56

531

357.47

510

357.29

558

2450

357.92

475

357.80

507

357.60

527

2425

358.23

464

358.12

475

357.90

497

2400

358.56

531

358.45

442

358.21

466

1475

358.79

418

358.74

413

358.54

433

1450 1 1/2" at 6" watergate

359.12

325

359.07

320

358.93

314

362.87

Lt=Nly Rt=Sl4

4750

354.50
8.37
5
354.43
8.44
5
354.28
8.59
5

4725

355.05
7.82
5
355.00
7.87
5
354.85
8.02
5

4700

355.66
7.21
5
355.60
7.27
5
355.45
7.42
5

3775

355.20
6.67
5
355.12
6.75
5
355.98
6.89
5

3750

355.56
6.24
5
355.51
6.31
5
355.39
6.48
5

3725

355.25
5.82
5
355.18
5.89
5
355.75
6.12
5

3700

357.19
5.68
5
357.15
5.72
5
356.95
5.92
5

T 362 87

Lt=Nly

6700

350.96
11.21
5
350.71
11.26
5
350.80
12.07
5

5775

351.78
11.09
5
351.73
11.14
5
351.62
11.25
5

5750

352.30
10.57
5
352.24
10.63
5
352.14
10.78
5

5725

352.77
10.00
5
352.70
10.17
5
352.62
10.25
5

5700

353.29
9.58
5
353.22
9.65
5
353.06
9.81
5

4788 5° RT 8" water gate

353.72
353.54

4786 5° Lt 8" MH

12.15 9.33

5.2 Sept 12 5.0 11.4

4775

353.60
8.97
5
353.74
9.04
5
353.74
9.13
5

T 362 87

Lt-Nly ♀ Rt-Sly

see sketch p923
SMH on Van Dyke

340.26
 13¹³ 367
 11192 11192
 12 12
 346.34
 346.22
 344.46
 8⁹³ 1400
 378 378
 12 12
 339.39
 SMH
 sly k-to
 cany

7+21³⁰ end int Nas existing sewer

7+00

346.94
 6⁴⁵
 346.85
 5⁵⁴
 346.67
 6⁷²

6+75

349.05
 5³⁴
 347.99
 5⁴⁰
 347.79
 5⁶⁰

6+50

349.04
 4³⁵
 348.99
 4⁴⁰
 348.88
 4⁵¹

BM starting

1²⁸ 361⁰⁴ p37
 ✓ 102
 ✓

TP1

3³¹ π 353³⁹
 12⁷⁹ 350⁰⁵

6+25

350.04
 12⁸³
 349.96
 12⁹¹
 349.87
 13¹⁸

TP2 9⁰⁹ 362³²

0¹⁶ 353²³

π 362⁸⁷

X Sec Sewer Hilldale Rd
 Marlborough to Fly
 Lt = Nly Rt = Sly

Lt = Nly Rt = Sly

40

5	1700	358.05 686 88 26	357.58 733 55 9ut	357.96 695 5	358.16 675 5
	0775	358.88 603 82 26	358.12 679 82 9ut	358.54 677 4	358.72 679 5
7	0750	359.46 540 133 26 9ut	359.51 540 5	359.51 540 5	359.53 538 5
6	0725	359.74 517 5	359.71 520 5	359.69 522 5	
6	0700 int.	359.86 505 5	359.87 504 5	359.86 505 5	
7	SMHs	355.65 926 1423 10	360.67 1424 1423 10	362.82 209 1430 rim	355.30 961 1430 16
6	BM,	521 	36421 	35920	

Note Didnt clear cb by 5' as it looks on ground like
 intersected would be under a water line. *ed*

1778²⁵ SMH.
 end

1750

1725

		342.24 2267 10 rim	356.52 839
		356.18 723 43 26	356.39 852 43 9ut
		357.46 745 32 26	356.59 832 3
		356.97 794 32 9ut	357.17 774 5
			356.69 822 3
			357.45 746 5

36421

VWBP
 New & Ret
 Hilldale Rd
 Marlborough

D. Smith
J. Rorer
R. Taylor

X. Sec. Monroe Ave

INDEXED
JER
JUN 4 1954

Vista St

25'

Monroe Ave

HT
21/13

Copeland to Van Dyke
for Sewer change.

Wot 21242 41
6/3/54

SMHering
E Van Dyke 140 90

25'

to Vista St

HT

21/13

HT
21/13

could not find any
HT
21/13
25'
is visible.

B.M.

024

362.03

361.29

4475.24
PK
1927

0400

5.10

360.99

0.90

361.13

0.81

361.22

0425

5.19

360.09

1.73

360.30

5.16

360.42

0450

5.23

359.10

2.72

359.31

5.10

359.43

0475

5.88

358.15

5.70

358.33

5.57

358.46

1400

4.81

357.22

4.64

357.39

4.54

357.49

1425

5.81

356.22

5.64

356.39

5.55

356.48

1450

7.81

354.16

6.67

355.36

6.55

355.48

Notes reduced 6-4-54
B. Larson

Lt-Nly

Rt-Sly

Lt-Nly

Rt-Sly

42

1475

7.83

354.20

7.63

354.40

7.51

354.52

2100

8.53

353.50

8.38

353.65

8.31

353.72

2125

9.24

352.99

8.23

353.10

8.09

353.19

2150

9.43

352.60

9.31

352.62

9.16

352.57

2175

6.38

358.81

9.60

352.43

2175

25' R' 10' throat
32' x 24' gate

6.34

352.25

6.62

352.19

6.68

352.13

2400

6.18

352.63

6.16

352.65

6.20

352.61

2175

7.55

351.26

12.03

346.78

2150

Flows only

2135

42' x 18' SMH

8.56

353.47

12.25

349.28

Flows from N take

Lt=Mly

Rt=Sly

Lt=Mly

£

Rt=Sly

43

4759 5⁶ Lt & 2⁵ 12⁵ gas vault

353.34

547

5⁵

353.35

546

5⁵

353.35

546

5⁵

353.26

555

5⁵

353.12

549

5⁵

352.69

552

5⁵

352.80

601

5⁵

353.43

538

5⁵

353.46

530

5⁵

353.35

546

5⁵

353.22

559

5⁵

353.05

576

5⁵

352.86

598

5⁵

352.85

596

5⁵

353.47

534

5⁵

353.51

530

5⁵

353.38

548

5⁵

353.23

558

5⁵

353.06

575

5⁵

352.85

596

5⁵

352.85

596

5⁵

4750

4725

4700

3775

3750

3725

BM start.

TP2

1056 364⁰³

5³⁴

353.47

346.49

343.88

352.98

353.11

353.15

353.17

4768

33

12³²

14²⁸

6³³

5²⁰

5⁶⁶

5⁶⁴

1402 Lt & SMH.

Flour St. N (two) Rooms Sly

NO. Vissell
SMH
Sec. Sec'y
Dept.

358⁸¹

358⁸¹

INDEXED

OCT 7 1954

Pipe - RE 4847

24.84

La Jolla Rancho Rd.

25

25

2+74.69 = 2" Pipe - RE 4847
= P.O.T.

20

⊙ 0+00 = Exist. M.H.
La Jolla Mesa Dr.

6+01.18 = PK
= P.O.T.

15+81.74 = PK
R to N.

027 PK. to stub & tack

44

2" pipe
R.F. 4847

24.73

15+57.4

La Jolla Senic Dr.

La Jolla Rancho Rd.

1/2" Pipe - RE 4847

25

12+54.13 = Nail
P.O.T.

25

25

Lt.

±

Rt.

Req. Levels along ± of Prop. Sewer
in La Jolla Rancho Road. from Exist.
M.H. in La Jolla Mesa Dr. to La Jolla
Senic Dr. - sketch-P. 44

W.O. 32508 - 10-5-54 7.0

3+50

45.8

3+00

43.7

2+50

42.2

2+00

41.1

1+50

40.5

1+00

40.1

0+83.5-4.6 Rt. = ± 8" Gate Valve cap.

0+50

39.7

0+30 = end Reg. A.C. Pave - Beg. Rough A.C.

39.66

6+18 - Cross. Gas Co. Ditch - ?

39.6

0+00 = ± Exist. M.H.

39.49
Rim21.00
I.E.

La Jolla Mesa + La Jolla Rancho

Set B.M. = S.F. σ in Ret.

539.72

500' fig. Not. noted.

B.M. = spike in Pole - By M.H. 21
at New Rd. to E.

529.73

Actual Elev. shown.

			LT.	+	RT.
13+00					52.7
12+54.43-25'	1" = 1/2 Pipe	Set B.M. 555.35 = on Pipe			46.7 100
12+00					53.2
11+50					53.0
11+00					46.3 100
10+50					53.1
10+00					52.9
9+50					52.8
9+00					47.2 100
8+50					53.1
8+00					53.9
8+35 - 90'	Lt. = front of House - opp. tank in	Back	57.21 floor.	56.2 90-gr.	55.6
7+51 on Rt.					56.5
Set. B.M. = PK in Brick wall		559.06			
7+45 - 148'	1" = 4" C.I. to Tank		50.22		57.2
7+00			148 = Top 4" C.I.		57.3
6+50					57.1
6+00					56.6
5+50					55.3
5+00 - 154'	Lt. = Wly. Cor. of House		52.50 floor.	51.5 154 = ground	53.5
4+50					51.1
4+00					48.5

L.

←

Rt.

47

Set B.M. on 2nd Pipe - 15+574 - 24.74 L.

541.12 = High Pt.

15+81.74 = P.K. = End

38.26

15+40

39.9

15+00

42.2

14+92 - 16' Rt. = FH. - Set B.M.
(Has been Moved)

544.15

was 544.39 - See B. 1741-P. 27

14+50

45.4

42.8

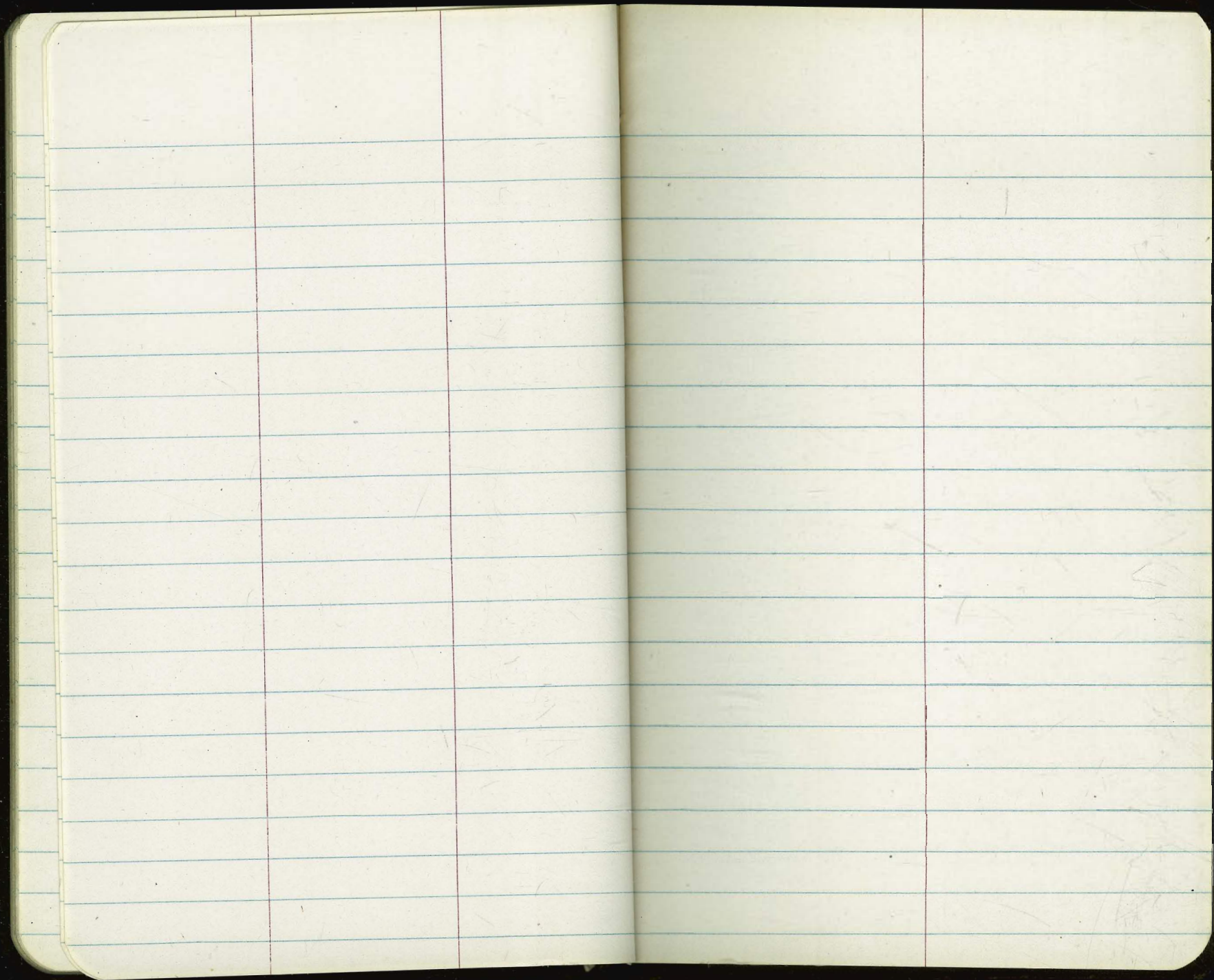
14+00

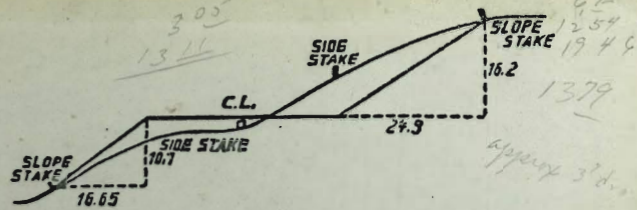
48.60
on P.K.

75

13+50

51.3





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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