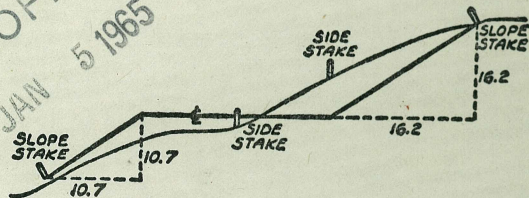






MICROFILMED  
JAN 5 1965



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.58	.65	.72	.79
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.887	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

*Index -*

*Sewer extension from Vista Rd + Baltic - 1*

*Sewer Survey Prop Sewer Muir lands Acres 7-*

*" " " " 75<sup>rd</sup> + Saranac 10*



INDEXED  
MER

Proposed sewer extension in Linda Vista

Road Near Baltic ST.

WO # 62341-

8-21-53

C. Allen

D. Sisson

C. Powell

Ref. 9432-L - Sheet 8.

4326-B

Line should be moved 514

from 1400 to 2+30.74.

Radmond  
BKC  
9/15/53

Proposed Sewer extension

Shown thus 

**Note!** Water Lines

in intersection, under

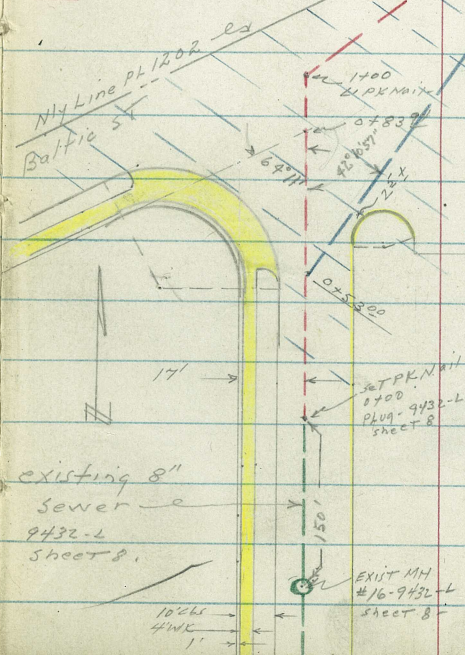
Construction and

proposed, should be

watched.

Revised Plans line

Shown thus 



existing 8" sewer  
9432-L  
Sheet 8.

EXIT MH  
#16-9432-L  
Sheet 8

20' Concrete  
Topped with  
1/2"

4+87.58 Set CW Hub

4+87.58 Red  
4+71.53 Blue

2+30.74

2+30.74 Red  
2+14.69 Blue

Blue line

would be best to

miss future

water

installations

in intersection

Blue line

is Figure 6

Linda Vista Road



Levels for Sewer extension  
Near Baltic St & Linda Vista Road  
See sketch Page 1

LT= WLY

Proposed  
Sewer  
#16.22  
/ 43

Rt=ely

(2)

1400 = L. 56° 09 Rt - sec taken on Split

416.20  
145

416.30  
35  
10

16  
edge AC  
NY Limits Run  
Baltic St

0+90 - 2 Crosses gas line of unknown size  
+ Depth

414.62  
30.3  
10

415.32  
2.33

415.00  
1.85  
10

0+83.94 - Sly Line Baltic St to Wly

413.34  
4.31  
70  
cb  
BC

412.84  
4.81  
70  
90T

413.12  
4.53

0+44.79 Lt = bc, wly curb line accessed

70 Lt = Wly curb line Linda Vista accessed  
Plug -

0+00 = 150' North SMH #16-9432-L Sheet 8

410.90  
6.75  
7.2  
cb

410.40  
7.25  
7.0  
90T

410.64  
7.01  
RC

0-150 = SMH #16-9432-L Sheet 8

397.50  
20.5 404.14  
13.51  
1E RIM

BM 1.37

417.65

416.28

Spike in pole SW cor Baltic & Linda Vista Road

417.65 T



Levels for Proposed Sewer Extension  
Near Baltic St + Linda Vista Rd

1+89<sup>4</sup> = 2 1/2' edge 20' strip conc Linda Vista

420.82  
8'7"  
2.5'  
along edge  
edge conc

419.52  
9'7"  
Topped  
Ac

418.34  
10'6.5"  
2.5'  
along edge  
edge conc

1+77 - approx 4' concrete strip

419.33  
9'7.0"

1+64<sup>5</sup> = wly edge Portland Conc strip 20' wide  
Main Linda Vista road

419.26  
9'7.3"  
10'  
along edge  
pavement

418.28  
10'2.0"  
Topped with  
Ac

418.28  
10'6.1"  
10'  
along edge  
pave

(investigate possibility of swing sewer south to Miss)  
Pipe not yet laid this far

1+58 - 2' crosses 20" C.I. water line under const

413.33  
15'7"  
Approx 1/2"  
C.I. pipe  
From cut stake

1+50 - 6.5' LT = wly edge MC Pavc - along P.L. Line

418.34  
10'6.5"  
6.5'

418.18  
10'8.1"

417.79  
11'2.3"  
10'

T.P., 11.58 428.99 0.24 417.41

428.99

1+29 - 2<sup>3</sup> LT = 4' 12" power pole # P178655

417.65



TR 12.02 440.05 0.96 428.03

3400

2750

Section taken on split

Failure to parallel probably due to using 2 Manholes

2730<sup>74</sup> 2"x2" hub L. 56°01' to Left

2706

2704 - 5° Rt = 4 anchor pole 8"

1794<sup>6</sup> for widening  
ely edge H.C. Linda Vista Rd

423.26  
574  
308  
ely edge  
ACPUT

422.7  
63  
23

440.05<sup>1</sup>

422.1  
29

428.9  
10  
45

422.9  
6

421.8  
72  
10

422.16  
683  
on hub  
ground  
same

422.3  
67  
5.90  
SW COR  
LOT

422.6  
64  
25

420.5  
85

419.5  
95

419.49  
951

428.99 x



Proposed Sewer Near Balfie St +  
Linda Vista Rd

LT Wly

±

Ret:ely.

(5)

TP<sub>3</sub> - Starting B.M. 10.80 416.28

TP<sub>3</sub> 0.09 427.08 13.06 426.99

4487<sup>58</sup> approx 10' Nly Lot Cor

431 <sup>69</sup> 83 <sup>6</sup>	431 <sup>9</sup> 82	43 <sup>26</sup> 74	43 <sup>57</sup> 431	0 <sup>0</sup>
315 edge AC	24	22	ON HUB 9' round SATTIC	40.0

4450

433<sup>4</sup>  
6<sup>6</sup>  
10

434<sup>4</sup>  
5<sup>6</sup>

435<sup>3</sup>  
4<sup>7</sup>  
10

4400

IMPROVED  
SEWER  
AUG 24 1953

427<sup>83</sup>  
12<sup>22</sup>  
30  
edge  
AC

427<sup>6</sup>  
12<sup>4</sup>  
23

429<sup>3</sup>  
10<sup>7</sup>  
22

431<sup>8</sup>  
8<sup>2</sup>

437<sup>1</sup>  
2<sup>9</sup>  
50

3450

428<sup>6</sup>  
11<sup>4</sup>  
10

429<sup>3</sup>  
10<sup>7</sup>

430<sup>6</sup>  
9<sup>4</sup>  
10

440.05 ↑



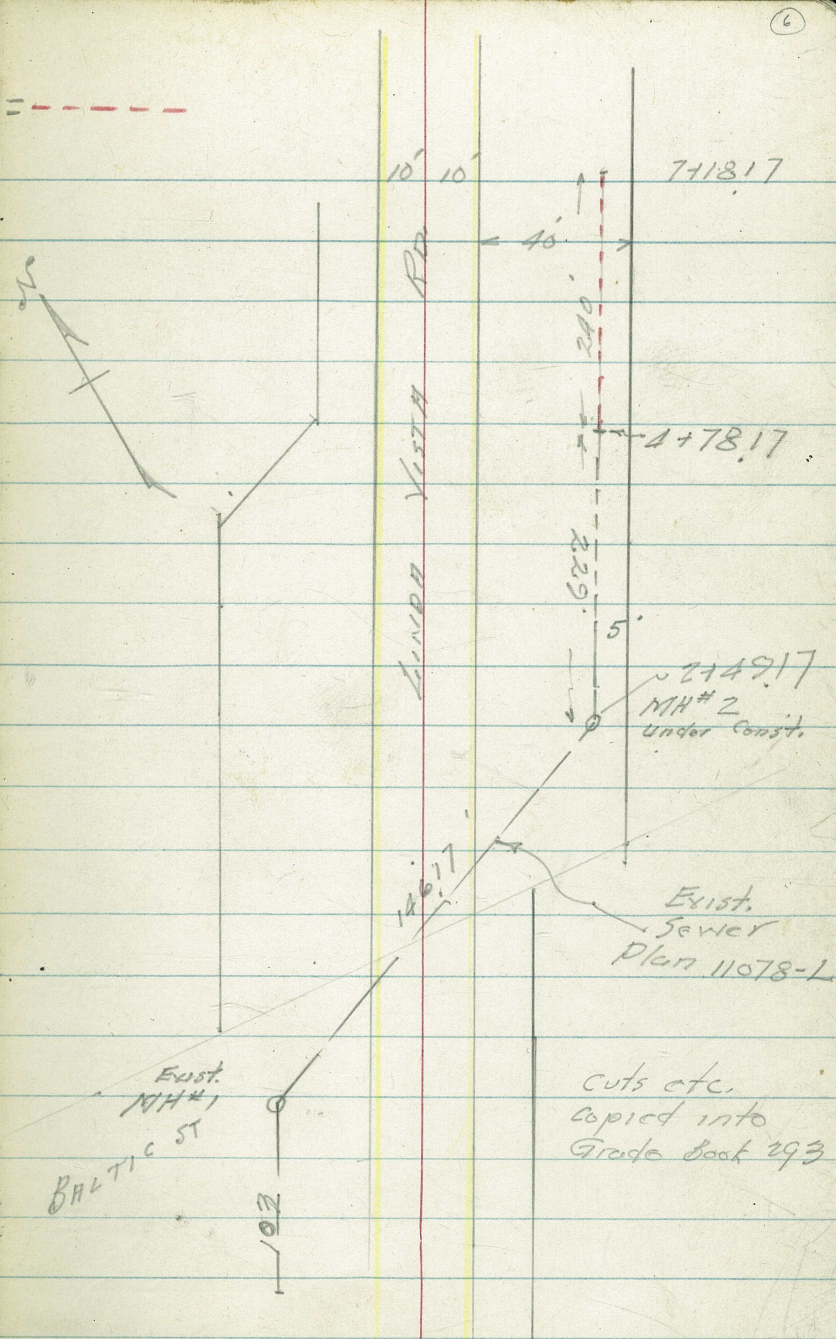
Preliminary Levels

Walker Proposed Extension Sewer  
 Pipe in LINDA VISTA RD.

Pilled  
 Olney North BALTIC ST

11-4-53 From 4+78.17 to 7+18.17

Sta.	Ground		NO 62.341		Cuts
	Elev. 2'	Elev. 6' offset Lt. on stakes	Elev. Invert		
End = 7+18.17	442.4	441.89	432.04	C 9.85	
6+90	442.7	442.47	431.89	C 10.58	
6+55	441.4	441.05	431.72	C 9.33	
6+20	440.9	440.40	431.54	C 8.86	
5+85	439.5	438.25	431.37	C 7.58	
5+50	438.2	437.50	431.19	C 6.31	
5+15 = MH	438.0	436.77	431.02	C 5.75	
4+78.17			428.52		
chk cut stake 4+15.43		$\frac{0.03}{434.04}$ 434.01	426.29	7.75	
B.M. on 6' offset	Plan =		428.52	6.67	
4+78.17	B.M. =		$\frac{6.67}{435.19}$		

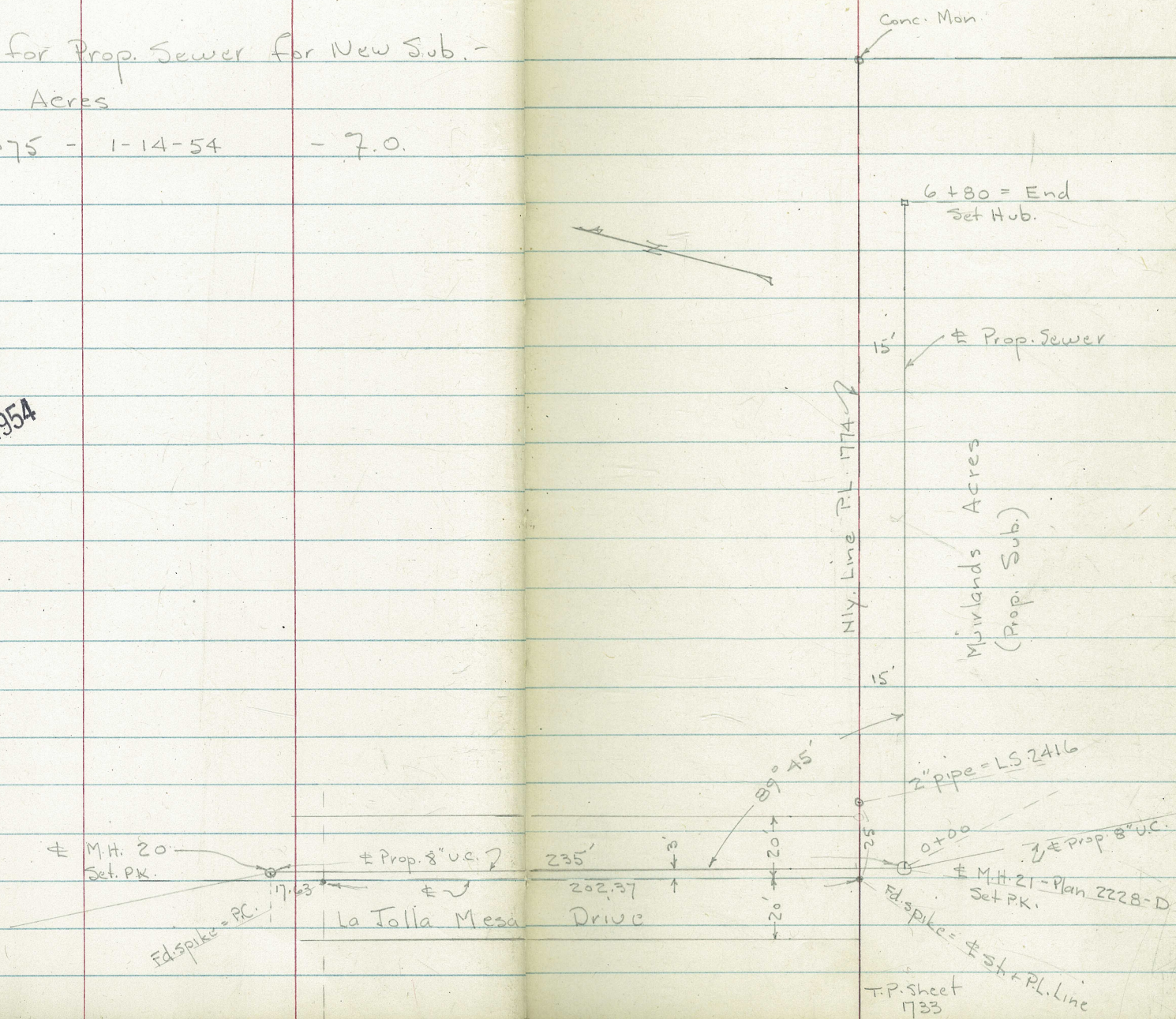




Survey for Prop. Sewer for New Sub. -  
 Muirlands Acres

w.O. 21075 - 1-14-54 - 7.0.

INDEXED  
 JER  
 JAN 15 1954





Lt. # Rt

Levels along # of Prop. Sewer - See sketch - P. 7

2+50

38.8

2+00

37.0  
15      36.5      36.3  
15

1+74 - 10.4' Lt. = # P. pole # 6201  
to Line in Dr. from S. end of House

1+50 - Note: Long. House on Rt. should Conn.

34.3

1+27 - 13.5' Rt. = end - A.C.

33.35

1+06 - 14.4' Rt. = Bed - Cor. of A.C. Parking to S.

13.5 = cor.  
A.C.      32.65      32.93  
14.4      30  
cor.      A.C.

1+00

32.8  
15      32.5      32.4  
15

0+70

31.8

8' E to E Ave - 12" diam.

0+35 - 15' Lt. = Beg. Row of Eve. Trees about

0+30

30.9  
15      30.2      30.1  
15

0+09 = edge A.C. pave

27.82

0+00 = # Prop. M.H. No. 21 - Plan 2228-D

28.12

B.M. = Spike in Pole  
Book - 2207 - P. 32

530.41

on PK.  
Note: 500' Sig. Not Noted.

Actual Elev. shown



6+80 = end

6+63.5 = opp. Lot Cor. on Rt.

6+40

6+00

5+64 - 9.3' Lt. = P. pole # J.P.C. 6207

5+50

5+00

4+50

4+00

3+51 - 9' Lt. = P. pole # C 6205

3+50

2+00

Lt.

E

Rt.

②

61.3 60.63 60.6 60.0 59.0  
15 on Hub. 15 100 150

58.6

56.9 56.6 56.4  
15 15

54.2

Smooth Lot  
even slope

51.8 51.6 51.5  
15 15

49.0

46.8 46.5 46.8 47.5 48.3  
15 100 150

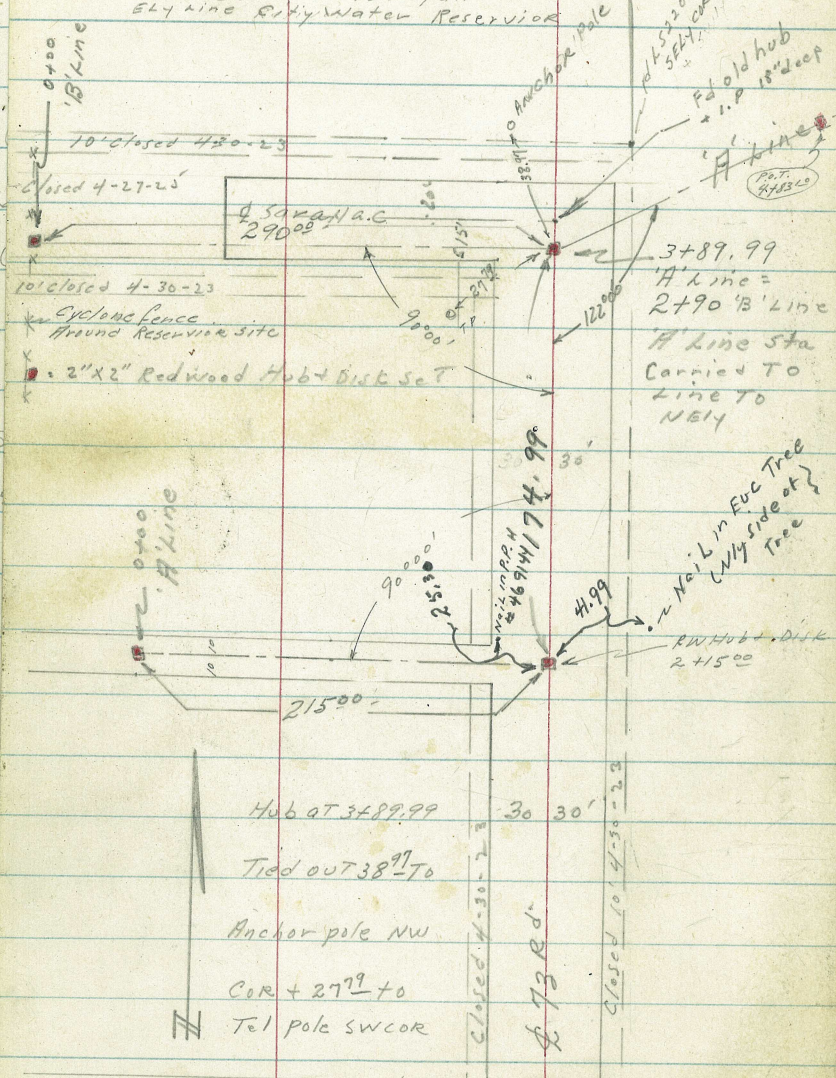
43.9

41.4 41.2 41.1  
15 15



Plan line Sanitary sewer at 73rd +  
 Saranac to Alvarado Canyon sewer  
 W.O. 62371 - March 10, 1954 -  
 C. Allen, Disisson, C. Powell  
 Ref TP Sheet 4312 1888-D

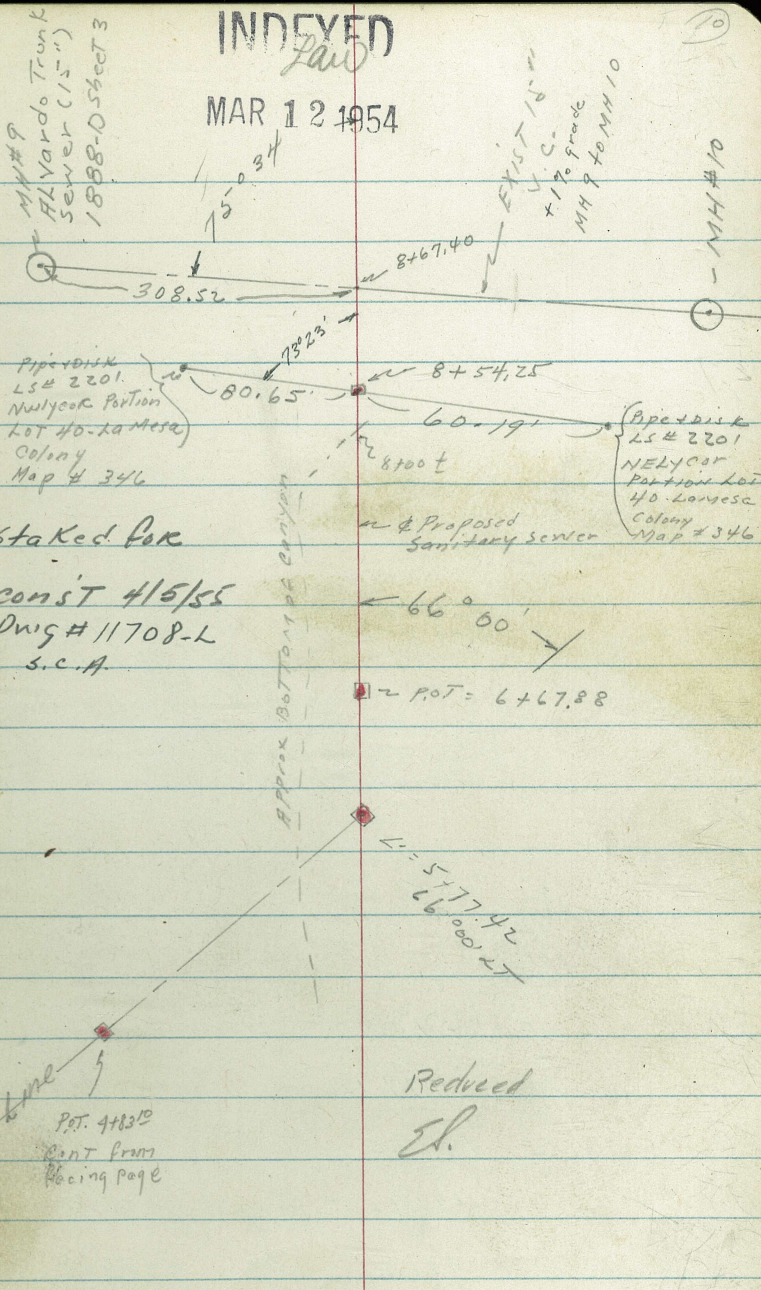
Found disk L.S. 2201 on site line  
 Saranac extended to Wyan on S  
 84 line City Water Reservoir



MOHAWK ST  
 Fd used state hwy Mon &  
 E.L. Co. Jan 73rd St

Fd I.P. &  
 Mohawk + 73rd

INDEXED  
 Law  
 MAR 12 1954



staked for  
 const 4/5/55  
 DWG # 11708-L  
 S.C.A.

Redwood  
 E.L.



Levels for proposed Sanitary  
Sewer 73<sup>rd</sup> + Saranac and in portion  
of Lot 40 - La Mesa colony  
see page 10

LT = N1/4

'B'  
line  
2

RT = S1/4

11

TP<sub>6</sub> 0.61 498.79 12.62 498.18

498.79 π

0+25

501.1  
92

0+00 'B' line

0+00 'B' line is Redwood Hub +  
City Disk 260' Wly of Wly line  
73<sup>rd</sup> + 5' Nly of S1/4 line of

Saranac extended  
500 RT pipe + Disk LS 2201  
1500 LT = NELY cor cyclone fence  
around City Reservoir property

498.2

504.0

507.6

512.8

12<sup>4</sup>

6<sup>8</sup>

3<sup>2</sup>

2<sup>4</sup>

+ 2<sup>0</sup>

35  
Nly Prop  
extended

15

5<sup>0</sup>  
on pipe  
+ Disk

35

0-40

510.8  
0<sup>0</sup>

TP<sub>5</sub> 12.62 510.80 0.95 498.18

510.80

TP<sub>4</sub> 12.74 499.13 0.26 486.39

TP<sub>3</sub> 11.75 486.65 6.83 474.90

TP<sub>2</sub> 2.85 481.73 12.36 478.88

TP<sub>1</sub> 10.42 491.24 1.82 480.82

BM 2.18 482.64 480.46

Top Fire Hyd - SW cor 73<sup>rd</sup> + Saranac  
Nail in PP - SWly cor 73<sup>rd</sup> + Alley Nly of Mahowick  
Pole # 46143H -

SW BP 70<sup>th</sup> + EL Cajon -



Levels 'B' Line Cont.

1792-57° RT = 2 frame house

1780

1725

TP<sub>7</sub> 5.89 491.35 13.33 485.46

1400-4° RT = 12" power pole # (No Number)

04

0+80-4° RT = 2 Dead man

0+60-0° 2T = 6" tree.

0+50-40° LT = 2 <sup>of 514 wall</sup> New stucco house (in county)

2T = N14

1/3' line

PT = 514

12

478.8	481.2	481.3	483.7	484.3	488.5	490.78
12 <sup>6</sup>	10 <sup>2</sup>	10 <sup>1</sup>	7 <sup>7</sup>	7 <sup>1</sup>	2 <sup>9</sup>	0 <sup>57</sup>
58	35	15		5	510 Ground	510 Floor

484.7  
67

483.8	484.9	485.6	486.9	487.7	491.3
7 <sup>6</sup>	6 <sup>5</sup>	5 <sup>8</sup>	4 <sup>6</sup>	3 <sup>7</sup>	0 <sup>1</sup>
58	35	15		5	50

491.35 ±

488.0  
10<sup>8</sup>

488.5	490.1	490.5	491.0	494.6
10 <sup>3</sup>	8 <sup>7</sup>	8 <sup>3</sup>	7 <sup>8</sup>	4 <sup>2</sup>
35	15		5 <sup>2</sup>	30

479.7	479.9	490.1	493.0	495.4	496.9	501.8
9 <sup>1</sup>	8 <sup>2</sup>	8 <sup>7</sup>	5 <sup>8</sup>	3 <sup>4</sup>	1 <sup>9</sup>	+3 <sup>0</sup>
40 <sup>2</sup> Floor	40 <sup>2</sup> Gr.	35	15		5 <sup>2</sup> Prop	35

498.79 ±



'B' Line CONT

TP11 13.12 513.53 0.02 500.41

TP10 13.07 500.43 0.07 487.36

TP9 12.54 487.43 4.15 474.89

2+90 = end 'B' line = } 473.80 ±  
3+89.99 ON 'A' Line

2+60 = Wly line 73rd ±T

2+30

TP8 0.72 479.04 13.03 478.32

2+23-40<sup>±</sup> RT = Frame house } House has basement  
see 1+48 page  
15' forelev.

2+00

2  
'B' Line

13

513.53

ON Fire Hyd. TP3 Page 11-

469.7 469.98  
9<sup>±</sup> 9<sup>±</sup>  
ground 2  
in hub

471.4 471.8 472.7 473.0 473.5  
7<sup>±</sup> 7<sup>±</sup> 6<sup>±</sup> 6<sup>±</sup> 5<sup>±</sup>  
35 15 5 5 25

474.6 474.9 477.5 478.0 478.9  
4<sup>±</sup> 4<sup>±</sup> 1<sup>±</sup> 1<sup>±</sup> 0<sup>±</sup>  
35 15 5 5 25

479.04 T  
481.3 482.24  
10<sup>±</sup> 9<sup>±</sup>  
40<sup>±</sup> 40<sup>±</sup>  
ground floor

475.2 478.0 478.4 480.4 480.8 484.9  
16<sup>±</sup> 13<sup>±</sup> 13<sup>±</sup> 11<sup>±</sup> 10<sup>±</sup> 6<sup>±</sup>  
50 35 15 5 50

491.35 x



'A' Line Cont

LT-N14-

'A' Line  
Page 10

RT=514 14

1400-

489.8	489.2	489.9	491.6
10 <sup>8</sup>	11 <sup>4</sup>	10 <sup>2</sup>	9 <sup>0</sup>
10		10	50

0497- 85° LT = 2 Frame House

(1472 on 'B' Line p. 9 & 12)

490.66	490.1		
9 <sup>98</sup>	10 <sup>5</sup>		
85° Floor	85° ground		

0450

498.3	498.2	498.2	499.6	500.8
2 <sup>3</sup>	2 <sup>4</sup>	2 <sup>4</sup>	1 <sup>0</sup>	+ 0 <sup>2</sup>
50	10		10	50

TP<sub>12</sub> 0.23 500.64 13.12 500.41

500.64 π

0425

503.6  
99

0400 'A' Line { 0400 'A' Line is Redwood Hub 40th  
Disk 185° feet Wly of Wly Line  
73rd St + 2 Alley Block 16,  
La Mesa Colony Map 346  
63° RT = 2 Frame House  
(This house on Sewer on Mohawk)

7 <sup>8</sup>	4 <sup>8</sup>	507.9	510.3	512.4	515.4
50	10	560	32	12	+ 9
		on Hub 9 same	10	63° 9r	63° Floor

'A' Line

513.53 π

π brought forward from page 13



'A' Line Cont

TP<sub>14</sub> 1.82 476.29 13.10 474.47

2+15° = 473<sup>rd</sup> - L = 90°00' Ely to Nly.

1+85 = Wly 73<sup>rd</sup> at

1+68 - 77° RT = 2 story frame house

House has basement  
ON Ely side of House

(2+23 on B' line page 13)

1+48 - 91° LT = 2 frame house -

1+25

TP<sub>12</sub> 0.21 487.57 13.28 487.36

LT = N14

4  
'H' line

RT = S14 15

476.29 π

478.5  
13<sup>1</sup>

478.4

478.3

479.8

9<sup>2</sup>  
10

9<sup>3</sup>

8.8  
10

480.2

481.5

490.8

7<sup>4</sup>

3<sup>1</sup>  
77<sup>2</sup>  
ground

+ 3<sup>2</sup>  
77<sup>2</sup>  
floor

175.09

482.25

479.0

482.3

482.5

482.6

124<sup>8</sup>

5<sup>32</sup>

86

5<sup>3</sup>

5<sup>1</sup>

5<sup>0</sup>

9<sup>2</sup>  
Base.  
Floor

9<sup>2</sup>  
Top  
Floor

9<sup>1</sup>  
ground

10

10

10

485.5

484.7

486.2

487.9

2<sup>1</sup>  
10

2<sup>2</sup>

1<sup>4</sup>  
10

+ 0<sup>3</sup>  
50

487.57 π

500.64 π



'A' Line Cont

LT=W1Y

2  
'A' Line

RT=ELY 16

4+00

469.7  
6 6

3+89.99 - L. deflection angles = 58°00' RT

469.7  
6 6

3+58 - 70° RT = Wly rim of N+5 Canyon

470.7 469.3 468.6 459.1  
5 6 7 2 11 2 17 2  
30 70° 80°  
Rim Canyon on Wly Wall of Canyon

3+18.46° LT = Entrance to basement of house SWly cor 73rd + Saranac

475.14  
1 5  
462  
Floor of Basement

3+00

472.0  
4 3

2+50

473.1  
3 2

2+18 - 84° RT = d. Frotte house (in County)

474.7 472.7 473.2  
1 6 3 6 3 2  
84 84  
92 Floor

476.29 π



'A' Line Cont

LT=WM

X

RT=ely

17

'A' Line

TP6- 0.33 455.23 12.83 454.90

455.23 X

5701 - 30° RT= Wly Rim N+S Canyon

453.2  
14.5 14°  
30  
Rim  
Canyon

456.93 455.5

4496 - 26° LT= SWly Cor house under Const

10.8° 12.2°  
26° Floor Upper 26° ground

457.5

458.5

459.00

4490 - 27° RT= NE COR house under Const

10.2°

9.2°

8.7.3

27° ground

27° Basement Floor

4483 -

463.0  
4.7

House has lower floor - see 4490

4462 - 11° RT= NWly Cor house Nearest Cor

464.7

467.27

3.0

0.4.6

11.0 ground

11.0 upper floor

TP15 2.48 467.73 11.04 465.25

467.73 X

466.6

465.8

465.9

4450

9.7

10.5

10.4

10

10

476.29 X



A' Line Const

(Section taken on split)

5+77.42 = L. angle = 66°00' LT

5+68 = Wly edge of bench dozed along Ely  
Wall Canyon

5+56 = Ely bottom Canyon

5+47 = Wly bottom Canyon

TP.7 0.50 442.54 13.19 442.04

5+25 - 23° LT = SELy cor house under const

5+15 = Wly Rim Wly + Sly Canyon

LT-NWly

9'  
A'

RT=SEly - 18

440.7

18  
90  
Wly edge  
Bench

441.29

11.25  
20 sub  
25 same

441.54

10  
30  
Ely edge  
bench

449.0

+6.5  
10  
Ely Top  
bench

441.3

12

433.3

92

434.4

81

442.54 x

446.5

87

230  
Lower  
Floor

446.5

87

230  
ground

451.5

37  
Rim

455.23 x



'A' Line cont

5+ 7+25

5+6 7+00 - 26° LT = bottom canyon

5+2 TP<sub>10</sub> 0.49 429.78 13.25 429.29

5+ 6+65 - 31° LT = bottom canyon

6+55 = Top bench

TP<sub>1</sub> All houses to east are 20' ± higher than

5+ 6+17 = wly edge top bench

5+ 6+00 - 23° LT = bottom canyon

LT = Wly

2  
A Line

RT = e ly

19

419.9 419.9 423.9  
9° 9° 5°  
2° 3°

415.5 426.2 426.2 429.8 433.0  
14° 3° 3° 0° + 3°  
26° 8° 2° 10°  
Bottom canyon

429.78 X

422.5 433.5 433.4 437.4 443.4  
20° 9° 9° 5° + 1°  
31° 12° 20° 20°  
Bottom canyon Wly top bench  
442.2  
0 3

438.0 438.4 443.8  
4° 4° + 1°  
8° Top Bench 4 Top Bench

430.2 439.5 439.9 440.1 446.6  
12° 3° 2° 2° + 4°  
23° 8° 30° 6°  
Bottom canyon Wly Top bench Ely bottom bench Ely Top bench  
442.54



'H' Line Cont

LT=W14

2  
A

RT=C14

20

399.19

5 8+54.25 = Nly Lot line Portion Lot 40

17<sup>76</sup>

ON HUB  
GROUND  
SAME

5+ 8+53-9 Proposed Sewer crosses E+W - gas line  
15" Hi pressure

399.4

398.4

398.0

8+25

17<sup>6</sup>

18<sup>6</sup>

19<sup>0</sup>

25

25

402.6

401.7

400.5

399.3

8+00

14<sup>4</sup>

15<sup>3</sup>

16<sup>5</sup>

17<sup>7</sup>

25

25

50

405.2

404.5

406.0

406.0

402.2

7+75-15<sup>2</sup> LT= bottom canyon

11<sup>8</sup>

12<sup>5</sup>

11<sup>0</sup>

11<sup>0</sup>

14<sup>8</sup>

15

5

10

20

bottom  
canyon

77

3 TP19 0.31 416.95 13.14 416.64

416.95

409.3

414.8

413.8

414.0

416.0

20<sup>5</sup>

15<sup>0</sup>

16<sup>0</sup>

15<sup>8</sup>

13<sup>8</sup>

23<sup>0</sup>

5

6

9<sup>0</sup>

Bottom

5 7+50-23<sup>0</sup> LT= bottom canyon

429.78 \*



A Line Cont

RT=WHY

4'

RT=ELY

21

5

TP29

2.39

starting BM.  
L 486.425  
480.44

Starting BM. Page 11

TP26

2.03

482.83

8.32

480.80

5

TP25

12.73

489.12

0.43

476.39

TP24

10.42

476.82

0.40

466.40

TP23

12.99

466.80

0.37

453.81

5

TP22

12.16

454.18

0.42

442.02

TP21

12.68

442.44

0.11

429.76

TP20

13.23

429.87

0.31

416.64

7

and 15" Alvarado Trunk Sewer

8+67.46 = Intersection proposed sewer

396.5

20.5

1/4 creek

396.5

20.5

399.2

17.8

8+60 = sly bottom E+W DIRT Channel

8+59 = sly top bank E+W DIRT Channel

416.95  $\pi$

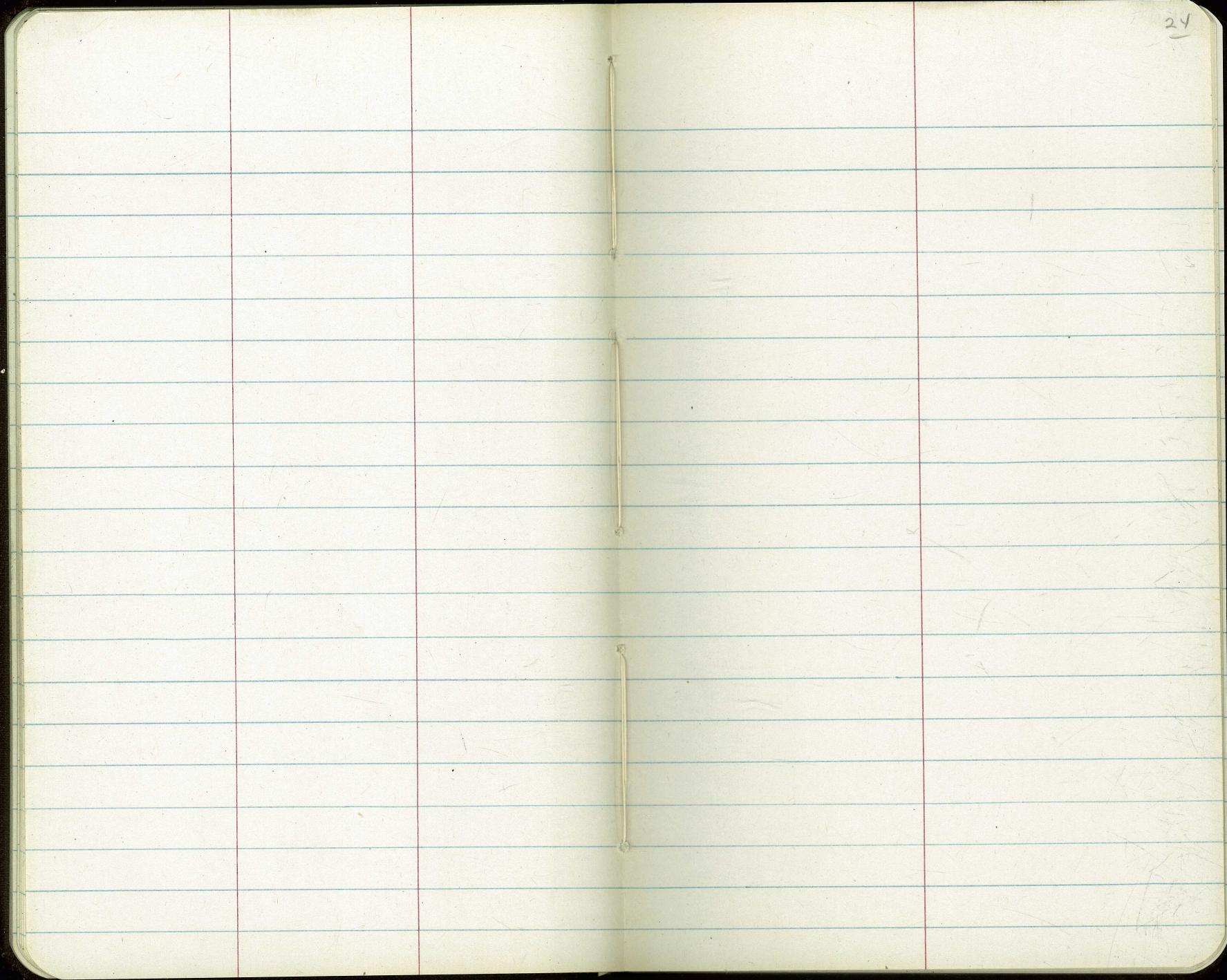








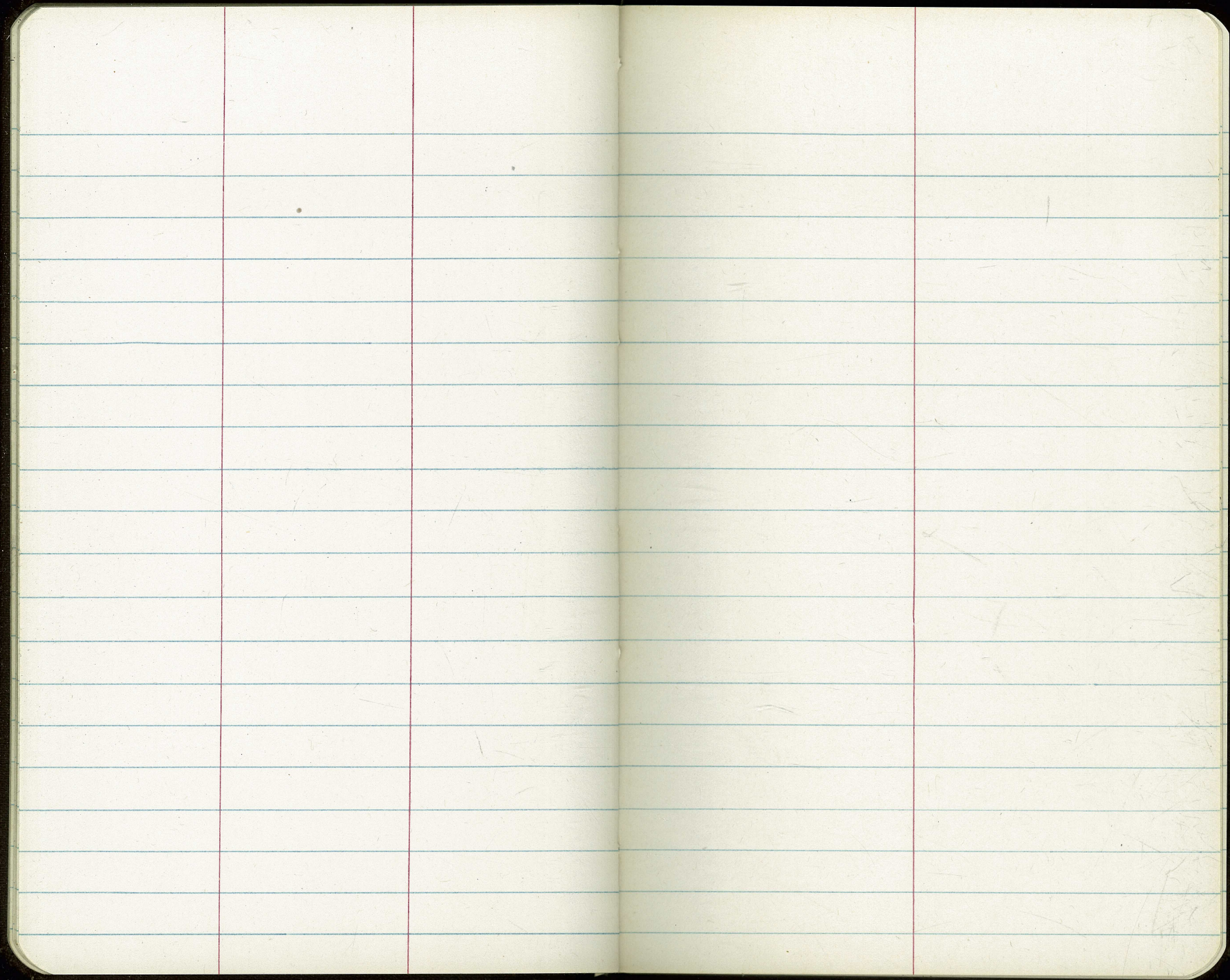








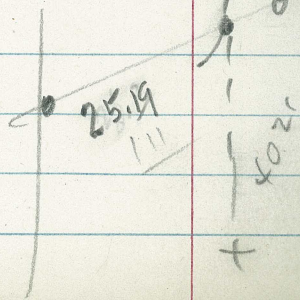






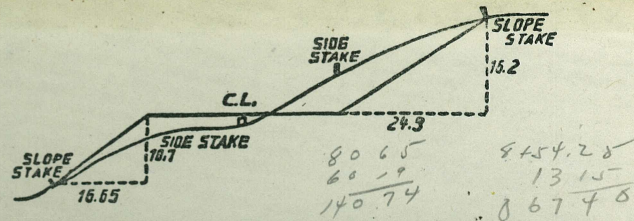
See 111729

64.02  
115-58





291  
215  
75



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**

**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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