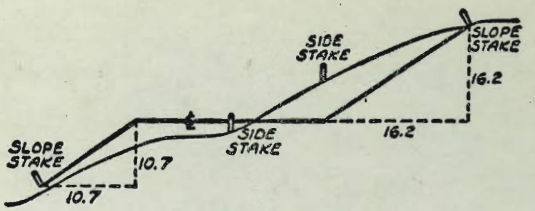
2306

X-SECT.

GRADE ESTABLISHED



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Index

X-Sec Alley Blk 20, Ocean Beach Park } 1
+ Alley 99, Ocean Bay Beach }

X Sec. Alley Cartagena to of Univ. College North 34

X-Sec Alley Blk 20,

0+10 - $20\frac{2}{}$ RT = 4" in AC. Parking area.

0+03 - $7\frac{2}{}$ LT = begin $2\frac{5}{}$ high board Rail fence

0+02 - $8\frac{3}{}$ LT = begin Stucco Bldg.

0+00 - $7\frac{3}{}$ RT = begin AC. Pave. Parking Area
= N'Wly Line Cable + N'wly edge AC. Pave.

$7\frac{3}{}$ RT
$7\frac{6}{}$ LT
0-07 = Bc's alley Returns - 3' Radius.

0-10 = Wly Curb Line Cable

TP$_2$	7.22	22.47	2.74	15.25
TP$_1$	9.04	17.99	4.96	8.95
BM	7.37	13.91		6.54

LT

RT

2

17.84 — $4\frac{63}{}$ — $7\frac{3}{}$ edge AC

18.12 — $4\frac{35}{}$ — $20\frac{2}{}$ Back edge AC. angle Point

17.75 — $4\frac{72}{}$ — $7\frac{6}{}$ CB

17.69 — $4\frac{70}{}$ — $7\frac{6}{}$ GUT

17.33 — $5\frac{14}{}$

17.70 — $4\frac{77}{}$ — $7\frac{3}{}$ GUT

17.83 — $4\frac{64}{}$ — $7\frac{3}{}$ CL

17.70 — $4\frac{77}{}$ — $7\frac{3}{}$ AC

17.67 — $4\frac{80}{}$ — $7\frac{6}{}$ CB

17.31 — $5\frac{16}{}$ — $7\frac{6}{}$ GUT

17.41 — $5\frac{06}{}$ — $7\frac{3}{}$ GUT

17.77 — $4\frac{70}{}$ — $7\frac{3}{}$ CL

17.20 — $5\frac{27}{}$ — 100 CB

16.75 — $5\frac{92}{}$ — 100 GUT

17.63 — $4\frac{84}{}$ — $10\frac{5}{}$ CB

17.21 — $5\frac{26}{}$ — $10\frac{5}{}$ GUT

17.23 — $5\frac{24}{}$ — $7\frac{5}{}$

17.29 — $5\frac{18}{}$

17.33 — $5\frac{14}{}$ — $7\frac{5}{}$

17.35 — $5\frac{12}{}$ — $10\frac{5}{}$ GUT

17.70 — $4\frac{97}{}$ — $10\frac{5}{}$ CB

17.72 — $4\frac{75}{}$ — 100 GUT

18.09 — $4\frac{38}{}$ — 100 CB

22.47 ℄
℄

NE BP. West Point Loma Ave + Bacon St

Alley Blk 20 - Ocean Beach Park } cont
Alley Blk 99 Ocean Bay Beach

LT S14 ℄ RT N14

Note! Direct elevation Rod used from here on - all elevs are true -

TP3	4.39	18.08	Nail in pole 6.9 LT sta 0+44 - # JPA 4910 -
0+44 - 6.9 LT = ℄ 12" power pole # JPA 4910			
0+41 - 8.6 LT = end stucco Bldg -			
0+40			18.1 / 4.4 / 7.5 ; 17.9 / 4.6 ; 18.0 / 4.5 / 7.5
0+39 - 7.8 RT = begin stucco Bldg - ; 7.1 RT = end A.C. Paved Parking Area			17.96 / 4.5.1 / 7.1 A.C. ; 18.22 / 4.2.5 / 20.2 A.C.
0+36 - 6.9 LT = end 2" iron pipe guard fence			
0+29 - 6.9 LT = begin 2" Iron pipe guard Rail around 4 gas Meters			
0+28 - 6.7 LT = end 2.5 high board Rail fence			
0+20 - 7.3 RT = edge AC			18.2 / 4.3 / 7.5 ; 17.9 / 4.6 ; 18.07 / 4.4.9 / 7.3 edge A.C. ; 18.07 / 4.4.0 / 7.5 ; 18.33 / 4.1.7 / 20.2 edge A.C.

22.47 K

X-Sec Alley Cont | LT | ℄ | RT | 4

1+00 - 7^{3} Rt = Near edge A.C. Apron — 16^{6}_{25} — $16^{4}_{7^{5}}$ — 16^{3} — $16^{6}_{7^{3}}$ gr — $16^{63}_{7^{3}}$ Apron — $16^{69}_{7^{5}}$ Gr AC — 17^{04}_{10} Gr AC

A.C. Apron continues - Conc floor in gar

0+87 RT = beg in 2 car garage under Apt house — $16^{84}_{7^{3}}$ AC Apron — $17^{25}_{11^{5}}$ Brk in Apron — $17^{45}_{15^{0}}$ gar Floor

0+77 - 11^{6} Rt = ℄ doorway to Apt

$18^{07}_{11^{6}}$ Floor

0+73 - 10^{7} LT = end 3 car garage Conc floor & Apron — $18^{09}_{12^{2}}$ gar floor — $18^{00}_{10^{7}}$ Apron

0+60 — 17^{7}_{10} — $17^{6}_{7^{5}}$ — 17^{3} — $17^{41}_{7^{5}}$ AC — $17^{72}_{11^{4}}$ AC

Parallel to ℄ Alley.

0+58 - 7^{5} Rt = Near edge A.C. Walk behind Apt — $17^{52}_{7^{5}}$ Near edge — $17^{78}_{11^{4}}$ Far edge AC

0+53 - 11^{4} RT = ℄ 3' Conc Walk — $17^{81}_{11^{4}}$ Walk — $17^{80}_{3^{14}}$ Walk

0+49 - 7^{9} RT = end Stucco Bldg

Floor

0+45 - 10^{7} LT = beg in 3 car garage - Conc Apron & — $18^{08}_{12^{5}}$ gar Floor — $17^{98}_{10^{7}}$ Apron

X-Sec of Alley Cont

	LT	℄	RT	5
1750 - 9.1 RT = end Conc Block Wall; 7.3 RT = end A.C. Apron	15.6 / 15	15.7 / 7.5	15.5	15.72 / 7.3 A.C.; 15.75 / 7.5; 15.8 / 9.1 gr; 15.7 / 9.1 Footing; 15.8 / 15
1748 - LT = end 2 car garage. Conc floor + Apron	16.35 / 15.7 gar floor	16.00 / 7.7 Apron.		
1735 - 9.0 RT = Behind A.C. Apron begin Conc block Wall				16.2 / 9.0 on AC; 15.7 / 9.2 Footing; 18.53 / 9.2 Top Wall
1726 - 7.7 LT = begin 2 car garage Conc Apron + Floor	16.37 / 15.7 Conc floor	16.24 / 7.7 Apron		
1717 - 7.2 RT = ℄ Single garage A.C. Apron + Conc floor				16.25 / 7.3 Apron; 16.30 / 7.5; 16.98 / 15.0 Floor
1710 - 14.7 RT = ℄ 3' conc Walk; 7.3 RT = Near edge A.C. Apron				16.48 / 7.3 A.C.; 16.55 / 7.5 on Ac; 16.90 / 14.7 Walk; 16.90 / 24.7 Walk
A.C. Apron and Apts above Garage continue. 1707 - 7.3 RT = end 2 car garage - A.C. Apron Conc floor -				16.52 / 7.3 A.C. Apron; 16.57 / 7.5 on AC; 17.24 / 15 on Conc Floor

Direct elev Rod

X-Sec Alley Cont

W. Point Loma

2+19 - 7.5 RT = NWly Cor garage opens to

2+15 - 6.5 Rt = ℄ begin 2' wide, 7' high hedge

faces West Point Loma Blvd

2+01 - 7.5 RT = SWly Cor Double garage

2+00 -

1+99 - 7.3 RT = end Stucco garage - opens to Sly -

1+81 - 7.5 RT = begin Stucco gar opening to Sly -
7.5 Rt = NWly Cor conc slab

1+50.0 - 7.8 LT = ℄ 10" power pole # PA 4930

1+54 - 7.5 RT = SWly Cor Conc Slab -

LT ℄ RT

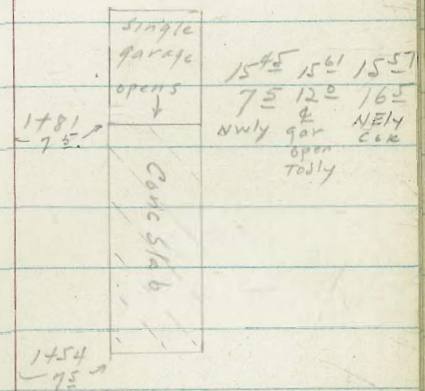
6

14.7
7.5
ground

14.8
7.5
ground

14.8 14.8 14.6 14.8 14.9
15 7.5 7.5 25

14.8
7.3
ground



Direct elev Rid

X-Sec Alley Cont

3+08 - $9\frac{2}{}$ Rt = ℄ Single gar dirt floor
Dirt floor

3+00

2+98 = ℄ Sewer manhole

2+86 - $6\frac{9}{}$ RT = ℄ 4' Conc Walk

2+51 - $5\frac{7}{}$ Rt = ℄ Single gar. Conc floor + Apron

2+50

2+33 - $6\frac{5}{}$ RT = end 2' Wide + 7' high hedge

LT ℄ RT

$13\frac{4}{}$
$9\frac{2}{}$
Dirt floor

$13\frac{8}{15}$ $13\frac{9}{7\frac{5}{}}$ $13\frac{5}{}$ $13\frac{9}{7\frac{5}{}}$ $14\frac{0}{15}$

$13\frac{5\frac{3}{}}{}$
Rim MH

$14^{0\frac{3}{}}$ $14^{0\frac{3}{}}$ $14^{0\frac{5}{}}$
$6\frac{9}{}$ $7\frac{5}{}$ $17\frac{5}{}$
Walk Walk Walk

$14\frac{0}{5\frac{7}{}}$ $14\frac{0}{6\frac{7}{}}$
Apron Floor gar

$14\frac{0}{25}$ $14\frac{1}{7\frac{5}{}}$ $14\frac{1}{}$ $14\frac{3}{7\frac{5}{}}$ $14\frac{5}{25}$

Direct elev. Rod

X-Sec Alley.

3+67 - 8[9] LT = begin 7' high board fence

3+67 - 8[9] LT = NELy cor garage - opens to Sly

3+51 - 7[4] RT = begin frame dwelling

8.9 LT = SE cor single gar - conc floor - opens to Sly.

3+50 - 5[9] RT = end 4' high Cyclone fence

3+49 - 7[0] RT = ℄ 2' conc walk

3+34 - 7[5] RT = ℄ 2' conc walk

3+18 - 18[0] LT = ℄ single garage - conc floor

3+14 - 6[5] RT = begin 4' high Cyclone fence

LT ℄ RT

12[5] / 8[9] ground

13[0] / 7[4] ground — 14[30] / 7[4] Floor

20[6] SW cor gar.. — 13[16] / 14[7] ℄ opening garage conc floor — 12[8] / 7[5] — 12[8] — 13[0] / 7[5] — 13[1] / 15

13[21] / 7[0] walk — 13[25] / 17[0] walk

13[50] / 7[5] walk — 13[56] / 17[5] walk

13[43] / 18[0] Floor

Direct elev Rod.

X-Sec Alley cont

	LT	℄	RT	
4+51 – 11° LT = ℄ single garage – Conc Floor	$11\frac{5}{5}$ 11^{0} Floor			
4+50 – $9\frac{4}{}$ Rt = Wly edge Conc Apron	$11\frac{4}{7\frac{5}{}}$	11^{1}	$11\frac{3}{7\frac{5}{}}$	$11\frac{38}{9\frac{4}{}}$ Apron $11\frac{58}{11\frac{4}{}}$ Floor
4+26 – $9\frac{4}{}$ RT = beam 4 Car garage + Apron – Conc floor			$11\frac{55}{9\frac{4}{}}$ Apron	$11\frac{66}{11\frac{4}{}}$ garage Floor
4+23 – $6\frac{5}{}$ LT = end 7' high board fence				
3 4+00	$11\frac{0}{15}$	$12\frac{0}{7\frac{5}{}}$	12^{2}	$12\frac{3}{7\frac{5}{}}$ $12\frac{5}{15}$
3+95 – $7\frac{7}{}$ RT = NWly Cor garage – opens to Nly			$12\frac{5}{7\frac{7}{}}$ 9r	12^{5} $7\frac{7}{}$ approx Floor
3 3+77 – 7^{0} LT = ℄ 10" Power Pole – # PA 4960 unobtainable $7\frac{7}{}$ RT = SWly Cor garage – opens to Nly – Type Floor			$12\frac{6}{7\frac{7}{}}$ 4 round	
3 3+74 – $7\frac{3}{}$ RT = end frame dwelling				12^{9} $7\frac{3}{}$ 9r

Direct elev Rod

X-Sec Alley Cont

	LT	℄	RT
5+04 - 9^{5} RT = ℄ 4' Conc Walk			11^{27} 9^{5} Walk; 11^{32} 19^{5} Walk
7^{0} LT = ℄ 10" Power pole # PP 4980			
5+01 - 9^{5} RT = end 4 car garage - Conc Floor + Apron			11^{0} 9^{5} Gr; 11^{28} 9^{5} Apron; 11^{42} 11^{7} Floor
5+00 -	10^{8} 2^{5}	11^{0} 7^{5}	10^{6}; 10^{7} 7^{5}; 11^{28} 9^{5} Apron; 11^{42} 11^{7} Floor
4+80 - 7^{9} LT = ℄ Dead Man -			
11^{0} LT = ℄ Single garage - Conc floor			
4+66 - 9^{4} RT = begin 4 car garage - Conc Floor + Apron	11^{57} 11^{0} Floor		11^{35} 9^{4} Apron; 11^{46} 11^{6} Floor
Same Apts served by garages			
Conc Apron Continues between garages -			
4+64 - 11^{4} RT = ℄ 4' Wide Walk			11^{23} 9^{4} Apron; 11^{25} 11^{4} Walk
4+62 - 9^{4} RT = end 4 car garage Conc Apron + Floor			11^{34} 9^{4} Apron; 11^{60} 11^{4} Floor
			Direct elev Rod

X-Sec Alley Cont

	LT	RT
5+65 - 6.9 LT = end frame + tin shed		
5+47 - 7.0 LT = Conc floor begin frame + tin shed	10.32 / 7.0 Floor ; 10.7 / 7.0 ground	
5+47 - 18.0 RT = end 5 car garage - Conc floor + Apron		10.73 / 18.0 Apron ; 10.80 / 20.2 Floor
5+42 - 5.2 LT = ℄ Single garage - Conc floor + Apron (Apron is Rough)	10.45 / 7.8 Floor ; 10.47 / 5.0 Apron	
5+34 - 4.8 LT = ℄ 2.5 Wide conc walk	10.90 / 17.5 ; 10.80 / 7.5 Walk ; 10.64 / 4.8 Walk	
5+21 - 7.3 LT = NElycor frame house.	11.6 / 7.3 Floor ; 10.7 / 7.3 gr	
5+06 - 17.4 RT = begin 5 car garage Conc floor + Apron		11.14 / 17.4 Apron ; 11.08 / 19.4 Floor
5+04 - 7.8 LT = SElycor frame house	11.6 / 7.8 Floor ; 10.4 / 7.8 grat house	

X-Sec Alley Cont

6+07.70 = Sly Curb Line Bacon

6+06.7 = Sly Curb B.C. 1' Radius S alley Returns

6+01 = ℄ Sewer Manhole

Alley Apron is in Poor condition

5+97.70 = LT 9.2 = Sly end Alley RoT
RT. 7.5 = Sly end Alley RoT
Sly edge A.C. Alley Apron.
Sly Line Bacon -

5+96 - 7.5 RT = end Stucco bldg -

5+75

5+74. 7.5 RT = begin Stucco Bldg.

LT ℄ RT

(Won't Drain)

9.35	8.62	9.34	8.65	8.65	8.60	8.67	8.67	9.32	8.61	9.22
50 Cb	50 GuT	8.2 Cb	8.2 GuT	7.5		7.5	8.5 GuT	8.5 Cb	50 GuT	50 Cb

9.35	8.74	8.70	9.33
7.2 Cb	7.2 GuT	7.5 GuT	7.5 Cb

8.89
RIM
SMH

9.52	9.28	9.00	9.06	9.48
7.2 Cb	7.2 GuT		7.5 GuT	7.5 Cb

10.2	9.8	9.7	
7.5		7.5	
		Grat Bldg	

Direct Rod -

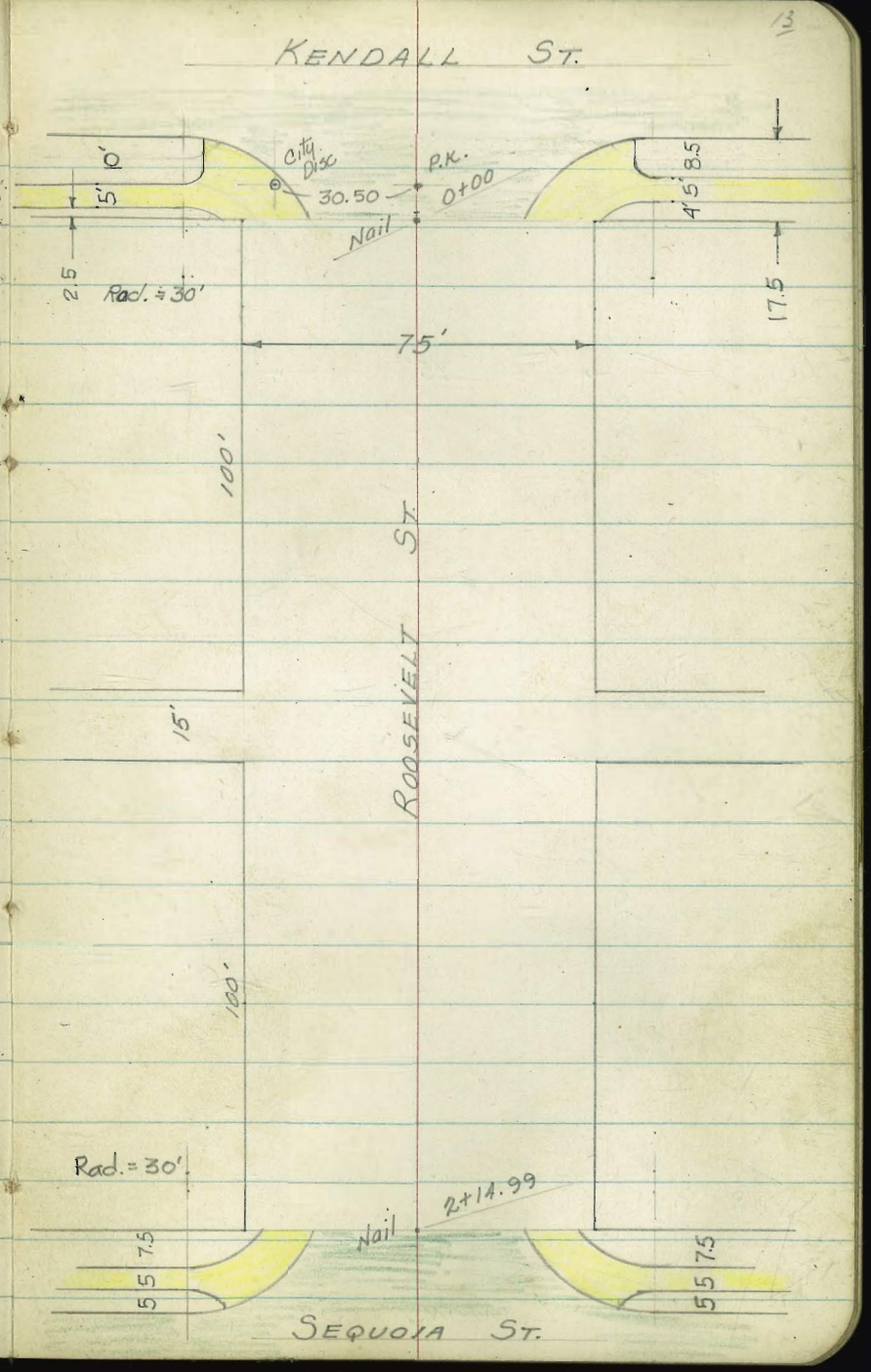
X-Sect. Roosevelt St. from easterly line of Kendall St. to Crown Pt. Drive

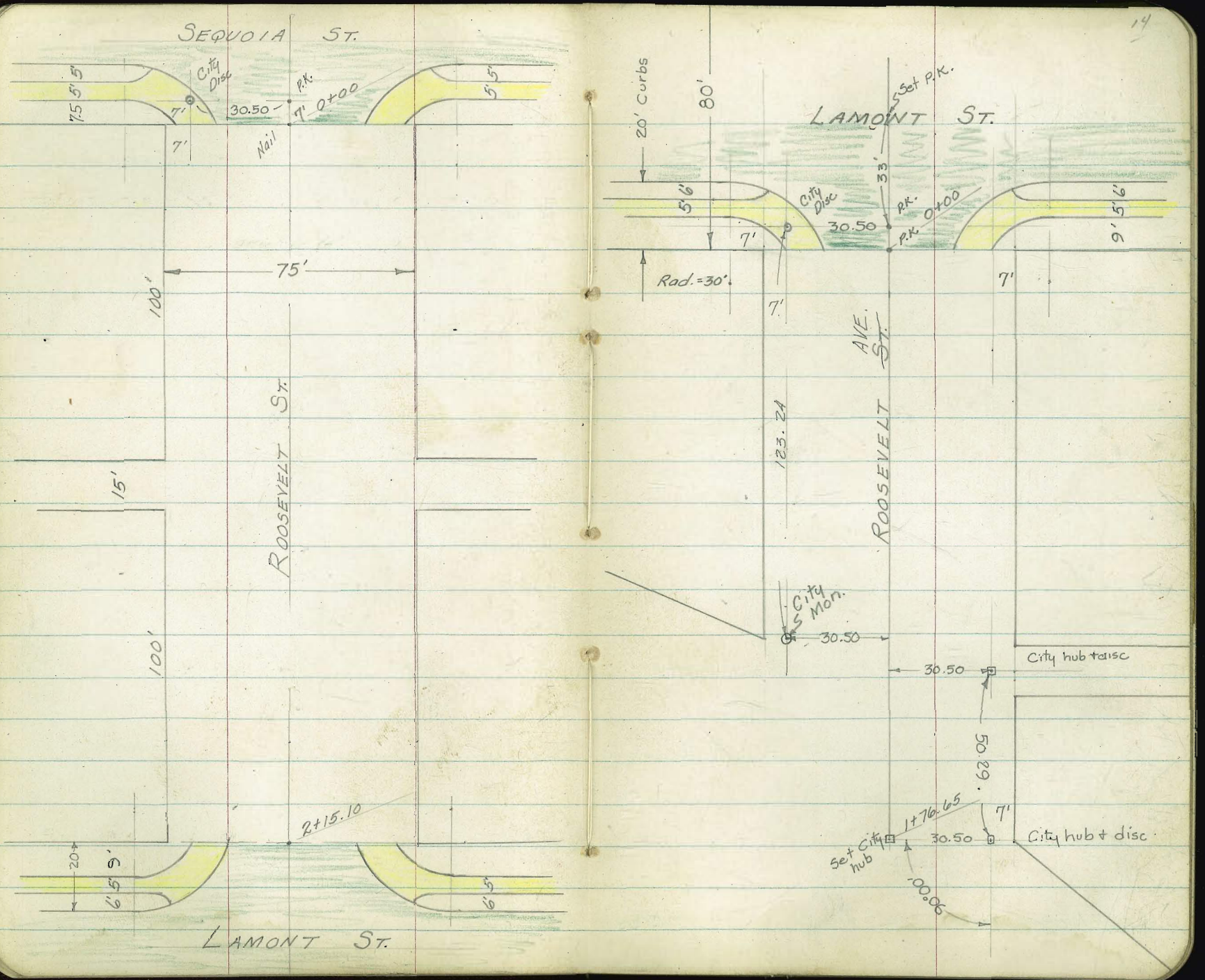
C. Hatch W.O. # 32452

R. Whipple 8-18-54

W. Presley T.P. Map 891

F.B. 2147-11




SEQUOIA ST.
City Disc
P.K.
30.50
7'
0+00
Nail
5'
5'
7'
75'
100'
ROOSEVELT ST.
15'
100'
2+15.10
20'
6'
5'
5'
6'
5'
LAMONT ST.
20' Curbs
80'
Set P.K.
LAMONT ST.
33'
5'6"
City Disc
P.K.
30.50
0+00
P.K.
9'
5'6"
Rad.=30'
7'
7'
7'
AVE.
ST.
123.24
ROOSEVELT
City S Mon.
30.50
City hub + disc
30.50
50.09
62.09
1+76.65
7'
Set City hub
30.50
City hub + disc
-00.06

X-Sect Roosevelt st. East cb. line of Kendall st. to Crown Pt. Dr.

0+71 ~ 37.5 Rt. = ℄ 8' conc. drive. thru planting

0+67 ~ 37.7 Lt begin 6' wood fence

0+60

0+54.5 ~ 37' Rt. begin planting

0+54 ~ 37.6 Lt. = ℄ 14' conc. drive

0+46.5 ~ 26 Lt. = ℄ southly edge hedge 2.5 high and 3.5 wide

0+25

0+22 ~ 34.3 Lt = ℄ 3" Silver spruce

0+00 = East line Kendall st. A.C. 0.5 west.

0-17.5 = East curb line of Kendall st.

Elev. Rod used for X-Sect. Notes

			4.93	26.29 =
T.P. #2	3.81	31.22	4.37	27.41
T.P. #1	8.07	31.78	5.18	23.71
B.M.	4.00	28.89		24.89

Lt.		℄		Rt.	
				26.90	28.90
				37.5 edge drive	47.8 floor gar.
27.0	25.9	25.1	25.5	25.0	26.2
37.5	20	14		20	37.5 prop
	28.15	26.90			
	54.2 floor garage	37.6 edge drive			
27.3	26.2	25.9	25.2	25.5	25.4	26.8
37.5	20	15	14		20	37.5
26.04	25.39	25.61	25.76	25.70	25.46	26.13
top cb.	gut 22.7 end ret.	10		10	gut 22.7 end ret.	Top cb
26.51	25.92	25.79	26.07	25.80	25.90	26.54
50 top	50 gut P.C.	25 Cross gut		20	50 gut. P.C.	50 top

Actual Elevs.

Set B.M. N.E. city disc Cor. Kendall & Roosevelt st.

La Playa St. c.t. in north curb ℄ of Yosemite st.

	Lt.			℄		Rt.		
						24.55	25.43	25.80
1+62 ~ 22.2 Rt. = ℄ 10' loose brick drive						22.2	36.3	42.3
36.3 rt. = ℄ 10' conc drive						edge brick drive	edge conc. apron	floor gar.
1+56 ~ 37.6 Lt. = ℄ 15' conc. apron		25.36	25.24					
1+55 ~ 29' Rt = ℄ 1" Tree + 26.9 ℄ 2" Tree		40.7 gar. floor	37.6 edge drive					
1+50 ~ 24' Rt. end hedge and planting	25.2	25.2	24.8	24.6		24.7	26.1	26.7
	37.5 prop.	20	14			20	25	37.5
1+43.5 ~ 37.6 Lt. = ℄ 2.5 walk (conc.)		25.52	25.50					
		45 on walk	37.6 on walk					
1+35	25.4	25.2	24.7	24.9		25.0	26.2	26.7
	37.5	20	14			20	25	37.5
						27.06	27.15	
1+34 ~ 38.8 Rt. = ℄ 3' conc. walk thru planting ~ hedges parallels walk back to porch step						38.8 edge walk	42.1 at step	
1+31 ~ 37.6 Lt. = ℄ 3' conc. walk		25.68	25.63					
		40.5 at porch step	37.6 on walk					
1+24 ~ 38.8 Rt. = ℄ 20" elm tree.								
1+16 ~ 24 Rt. begin ℄ 2×2 hedge bordering planting								
1+15 ~ 37.5 Lt. ℄ Southly 8" conc. block wall 4.5 high								
1+07.5 = ℄ alley								
1+01 ~ 27.4 Rt. = ℄ Power pole #P1825	26.1	25.8	25.0	24.9	25.2	25.1	26.5	27.2
1+00 ~ 37.2 Lt. end 6' wood fence and end planting on right	50	37.5	20	14		20	37.5	50

Set B.M. N.E 7' City Disc Roosevelt and Sequoia ~ 22.26

	Lt	℄	Rt.
0+40 ~ 27.5 Lt. = ℄ 2' conc. walk	25.02 24.92 22.90 37.5 34.7 27.5 on walk break 3' walk edge 2' walk		
34.7 spreads to 3' conc. walk			
0+10	25.1 25.0 22.6 21.6 21.8 37.5 30 25 15 along wall	21.5 20	23.0 37.5
0+00 = East prop. line Sequoia St. 25.12 37.5 bott. wall A.C. 0.5 West 37.5 Lt. begin 6" conc. block wall Flowers and shrubs parallels wall 6" out.	22.37 22.20 21.57 21.75 21.83 34 Top Curb 22.6 end ret. gut. 10 edge walk	21.79 10	21.56 22.20 22.8 end ret. Top Curb
0-17.5 = Eastly curb line Sequoia St.	22.31 21.62 21.84 21.88 50 50 25 Top Cb P.C. gut	21.94 25	22.23 22.88 50 50 P.C. gut Top Cb
2+32.5 = Westly curb line Sequoia St.	22.79 22.12 22.13 22.27 50 50 25 Top Cb P.C. gut	22.34 25	22.70 23.34 50 50 Pc gut Top Cb
2+14.99 = West line of Sequoia St. and 0.8 west of A.C. pave.	22.90 22.23 22.52 22.58 Top Cb. 22.7 end return gut. 10	22.48 10	22.23 22.81 gut. end ret. 22.7 Top Cb.
2+00 ~ 35.9 Rt. end of conc. block planter	25.3 25.6 23.0 22.9 37.5 20 14	22.6 26.02 20 35.9 top planter	24.3 24.4 37.5 grd. 38.0 along house
1+80	25.4 25.6 25.6 24.0 23.6 37.5 20 15 13	23.3 20	24.7 26.50 35.9 grd. 35.9 Top planter
1+75.5 ~ 35.7 Rt. begin conc. block planter box parallel to house.		24.8 grd. 35.7	26.61 Top Conc. planter 35.7
1+72 ~ 22' Rt. = ℄ 3.5 loose brick walk ~ 36.3 = ℄ 3.5 conc. walk.		24.43 22 brick walk	25.19 25.38 36.3 40 conc walk

	Lt.			℄	Rt.			
2+15.10 = West prop. line Lamont St. A.C. and curbs 0.6 West.	20.96 Top Curb	20.45 21.6 end ret.	20.64 10	20.73	20.56 10	20.09 21.6 end ret. gut.	20.56 21.6 Top Cb.	
2+13-28' Rt = ℄ Power pole # 1899								
2+00	22.8 37.5	23.3 30	21.2 25	20.5 17	21.0	20.3 20	21.3 25	22.1 37.5
1+61 ~ 37.5 Lt. = ℄ 8' conc. apron		23.73 41.5 floor gar.		23.40 37.5 edge apron				
1+60	23.3 37.5.	21.8 25	208 17	21.4	20.7 20	22.4 37.5	22.97 40.2 edge conc. walk	
1+20	24.3 37.5 along 4' lattice fence	24.3 30	21.8 24	20.9 16	21.6	21.0 20	22.2 37.5	22.95 40.1 on conc. walk para to ℄
1+07.5 = ℄ alley	24.1 50	23.7 37.5	21.1 20	21.6	21.1 20	22.0 37.5	22.10 40 on A.C. pave	22.51 50
1+01 ~ 37' Lt. end 2' hedge								
0+96 ~ 28' Rt. = ℄ of Power pole # P1875								
0+91	24.5 37.5	24.3 32	21.2 20	21.6	21.2 20	22.7 37.5	23.82 40.2 break in walk	
0+75 ~ 27.5 Rt. = ℄ Deadman		24.98 46 at steps		24.50 36.6 on walk				
0+70.5 ~ 36.6 Lt. = ℄ 3.5 conc. walk thru hedge								
0+53 ~ 37' Lt. begin hedge 2' high and 2' wide	24.9 37.5	24.8 30	22.1 20	21.3 17	21.7	21.4 20	22.4 35	23.5 37.5
0+50								
0+49.5 ~ 37.7 Lt. end 6" conc. wall 5' high also end row of shrubs 1' out from wall.				25.0 37.7 along wall				

Set B.M. S.E. 7' City Disc Roosevelt and Lamont St. = 20.85

	Lt.			℄	Rt.			19
1+34 ~ 37.9 Lt. begin 3' high picket fence								
1+26.36 = ℄ alley to North ℄ Sewer M.H.	20.2 50	20.0 37.5	19.7 20	19.77 rim manhole	19.3 20		19.2 37.5	
1+18 ~ 39.2 Rt. = ℄ 10" tree								
1+15.5 ~ 37.3 Rt. end 6' board fence								
1+14 ~ 27.5 Rt. = ℄ Power pole #1925								
0+70	21.2 37.5	20.8 20	19.8 18	20.2	19.5 20	20.2 25	20.2 37.0 along fence	
					21.02 35.5 edge apron.		21.23 38.5 floor gar.	
0+50 ~ 35.5 Rt. = ℄ 16' conc. apron to double car garage thru 6' board fence								
					20.60 29 edge walk		20.68 37.5 of fence	
0+37 ~ 29' Rt. = ℄ 3' brick + conc. walk								
0+34.5 ~ 28.4 Rt = ℄ 24" conc. base for mail box								
0+25 ~ 37.1 Rt. = ℄ 20' conc. apron to double car garage thru 6' board fence	21.4 37.5	21.3 22	20.2 20	20.2	20.0 20	20.90 37.1 edge apron	21.05 38.0 floor gar.	
0+13 ~ 36.5 Rt = ℄ shrub 4'x4'								
0+00 = P.K. Eastly prop line Lamont St. edge A.C. is 0.8 east. 37' Rt. begin 6' board fence	20.59 Top Cb.	20.09 21.3 end ret. gut	20.39 10	20.56	20.96 10	20.23 22 end ret. gut.	20.73 Top Cb.	
0-20 = Eastly Curb line Lamont St.	20.96 50 Top Cb.	20.45 50 gut PC	20.62 25	20.89	20.65 25	20.13 50 gut. PC	20.63 50 Top Cb.	
2+35.1 = Westly Curb line Lamont St.	21.04 50 Top	20.54 50 Gut.	20.37 25	20.25	20.16 25	19.95 50 gut. P.C.	20.40 Top Cb.	

Lt. ℄ Rt. 20

1+90 = Top bank which drops straight down to bay water level

1+88.5 ~ 1.2 Rt. North end guard rail

1+76.65 = 2"x2" Hub

1+76 ~35.5 Lt. end picket fence

1+74.5 ~ 19.8 Rt. south end of 2x6 guard rail

1+71 ~ 34.8 Rt. = ℄ Dead man

1+64 ~ 34.2 Lt. = ℄ guide pole no #

19.8	19.7	19.7	20.2
37.5	20	15	Top bank

20.6	19.7	19.6	19.6	19.6	20.2	19.2
37.5	30	20		8	20	Top bank

Additional Notes ~ X-Sect.

Roosevelt St.

Kendall St. to beginning of A.C. 90' West (Naval Housing)

12-13-54

W.O. 32452

1+07.5 = ℄ alley .8 left = ℄ Sewer M.H.

1+00 = East line of alley ~17' left end A.C. & begin conc. approach to alley

0+89.8 ~ Begin A.C. Pav. and Curbs

Curbs are 10' Radius

0+50 ~ 18.2 Lt. = Westly of 3' Conc. walk

0+10

0+00 = West prop. line Kendall St. also edge of A.C. pave and end conc. return (A.C. ends at edge of gut.)

0-17.5 = West Curb line of Kendall St.

0-37.5 = ℄ Kendall St.

B.M. = N.E. 7' City Disc Kendall and Roosevelt St. 26.29

see page 15

Lt.				℄					Rt.
27.50	27.41	27.37	26.79	27.10	27.10	26.76	27.44	27.53	27.96
60 on A.C. Strip	37.5 on oiled A.C.	31.2 end Conc.	17 end AC begin conc.	.8 rim M.H.		17 edge cov. conc. on A.C.	31.5 end conc.	37.5 on A.C. Strip	60 on A.C.
28.4		27.56	26.86	26.99		26.81	27.66		28.1
37.5		gut. & Top Same	31.4 end conc.	17 Con. cov. with A.C.		17 conc cov. with A.C.	31.5 end conc.	end ret. Same as gut.	37.5
29.2	28.7	27.18	26.93	26.85	26.87	26.91	26.87	27.09	28.2 28.7
37.5	25	18.1 Top end return	18.1 gut	10		10	17.9 gut	17.9 Top end return	25 37.5
	28.5	28.1	26.6	26.7		26.6	27.11	27.87	28.25
	37.5	25	15			17	18.2 conc. walk	24 on walk	37.5 on walk
	28.1	28.1	26.5	26.7		26.7	27.1	27.7	
	37.5	25	15			17	20	37.5	
27.57	27.36	27.14	26.51	26.75	26.82	26.79	26.53	27.16	27.36 27.4
37.5	32.5 edge walk	Top	22.2 gut end cb.	10		10	22.3 end cb. gut	Top	32.2 edge walk 37.5
27.01	26.37	26.50	26.35	26.56		26.37	26.27	26.42	26.44 27.10
Top	499 P.C. gut	37.5	20			20	24 cross gut.	37.5	50 P.C. gut Top
26.56	26.33	26.02	26.26			26.07	26.03	26.26	26.46
50	37.5	20				20	22.5 cross gut.	37.5	50

Actual Elevations

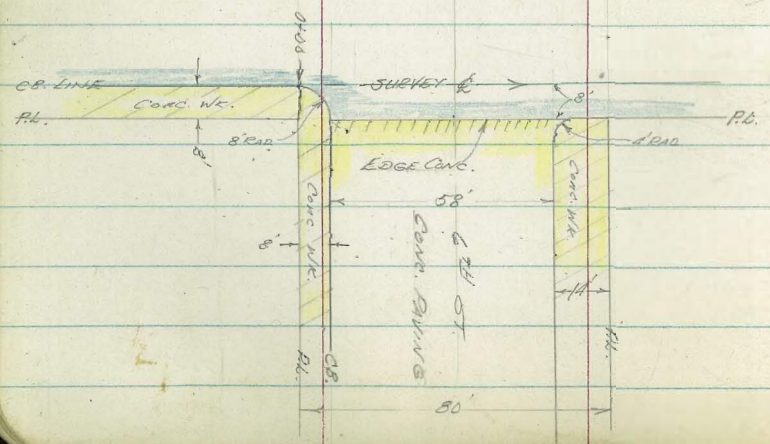
	Lt.	℄	Rt.
1+75 – extra section for drainage	27.06 18 Top	26.56 26.93 18 gut.	26.66 27.11 18 gut. Top
1+25 – opposite 10' alley P.C.'s	27.20 Top	26.76 26.98 17.8 gut.	26.78 27.22 gut. Top 18.3
1+17 – 33.5 Lt. ℄ Power Pole #1775			
1+15 = West line alley	27.7 37.5	27.52 26.82 31.4 gut & end rst. same	27.02 26.85 27.51 27.8 17 17 31.6 37.5 edge A.C. on A.C. gut + Top covered end conc. conc approach Actual Elevs. To alley

- X-SECTIONS 6th & "L"

COTA
CABER
KELLEY
W.O. #2766A
3-29-55

N 19

"L" ST = A.C. PAVING



X-Secs. 6TH ℄ L - Cont'd.

	Lt.		℄	Rt.		
0+16	2.39 10	2.23 3	2.85	2.51 8 Conc edge	2.47 20	
0+24	2.29 10	2.05 3	2.05	2.30 8 Edge Conc	2.30 20	
0+16 5² RT TO CENTER OF 2'x2' METAL COVER OF M.H. to STORM DRAIN						
0+08 W'LY CB. LINE 6TH	2.21 10	1.97 3 Low Pt.	2.04	2.13 8 Gut. B.C.	2.50 8 CB	1.83 38 Gut. 2.38 38 CB.
0+00 WEST. RL. 6TH	2.19 10	1.96 3 Low Pt.	2.18	2.45	2.65 8 on Walk	
0-30			2.12 Gut.	2.12 CB.		

B.M. = N.W.S.P. 6TH ℄ L = 2.11

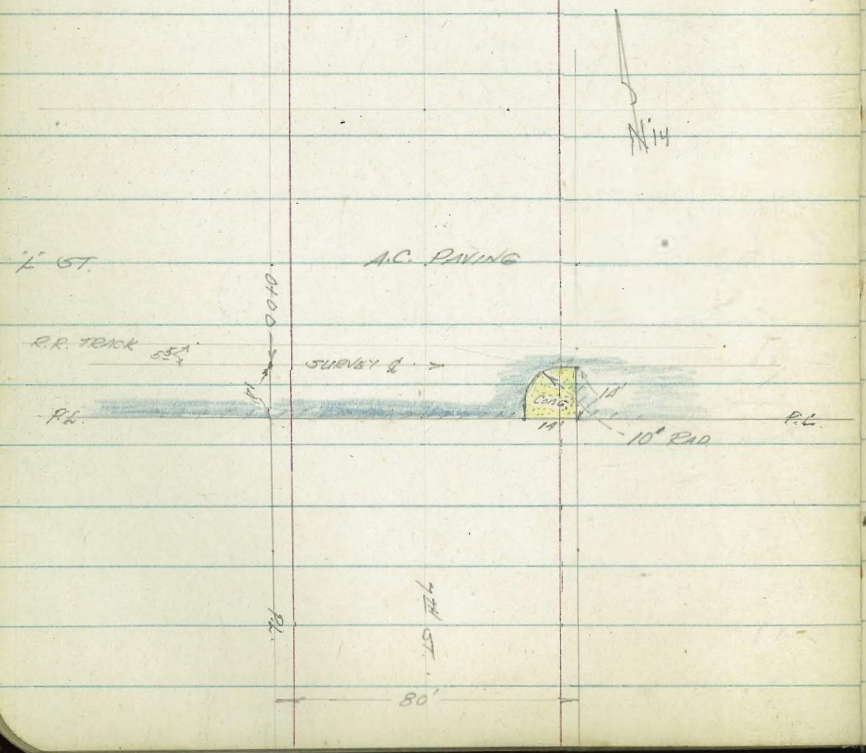
USED DIRECT ELEV. ROD

X-SECTIONS 6TH & L - CONT'D.

	LT.		℄	RT.		
1+00	2.78 10	2.77 3	2.90	3.30 7.6 @ Idg.		
0+80 ELY RL. 6TH	2.58 10	2.50 3	2.63	2.97 7.2 CUT.	3.25 7.2 CB.	3.50 15
					2.97 20 CB.	2.49 20 9 Ht
0+60 ELY. CB. LINE 6TH.	2.28 10	2.35 3	2.40	2.57 8	2.51 12 9 Ht	3.00 12 CB.

EC. of return

2-SECS. 7TH & L.

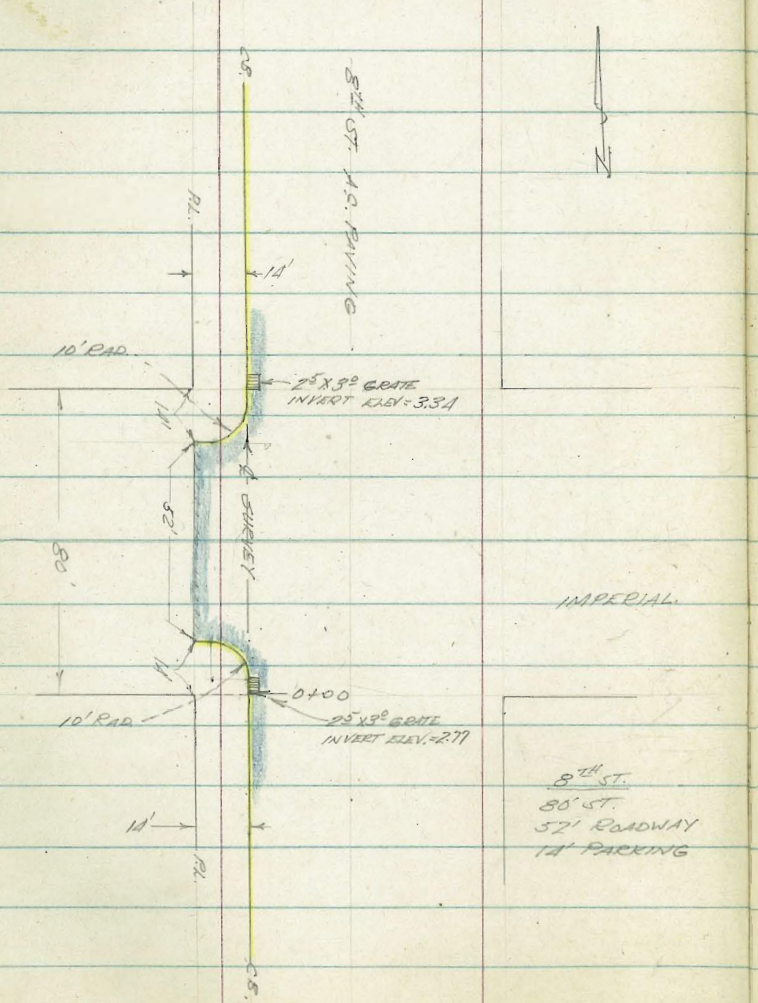


X-SECTIONS 7th ℄ L STS.

	LT. (NO.)	℄	RT. (SO.)
0+43.3 ℄ CROSSES R.R. TRACK	? 5		9.10
0+38.3 ℄ CROSSES R.R. TRACK			5.04
0+30	5.07 5-C TRACK	5.02	4.93 1A edge A.C. 4.7 25
0+14	4.87 5	4.71	4.64 3 4.68 1A edge A.C.
0+00 {W.L.Y. PROP. LINE 7th 5 ft. Lt. to edge railroad track	4.72 5	4.51	4.49 3 4.98 14
0-30 5° LT. (No.) TO SO. EDGE TRACK	4.25 5	4.13	4.08 3 4.60 1A Edge Bldg.

Z-SECTIONS 7TH & 2" STS.

	Lt.	℄	Rt.
1+00	5.82 5.5	5.53	6.2 14
0+80 END CB.	5.60 5.5	5.40 9#H	6.03 CB 6.15 14 edge conc.
0+76 CB. B.C. 2" ST.	5.52 5.5 TRACK	5.39 9#H.	6.01 CB 6.12 14 edge Conc 5.8 25
0+66 ELY CB. LINE 7TH	5.46 5.5 TRACK	5.39	5.21 10 9#H BC 5.93 10 CB 5.17 14 9#H 5.39 14 CB END OF CB. 5.2 25
0+50	5.32 5.5 TRACK	5.36	5.16 14 edge A.C. 4.8 25



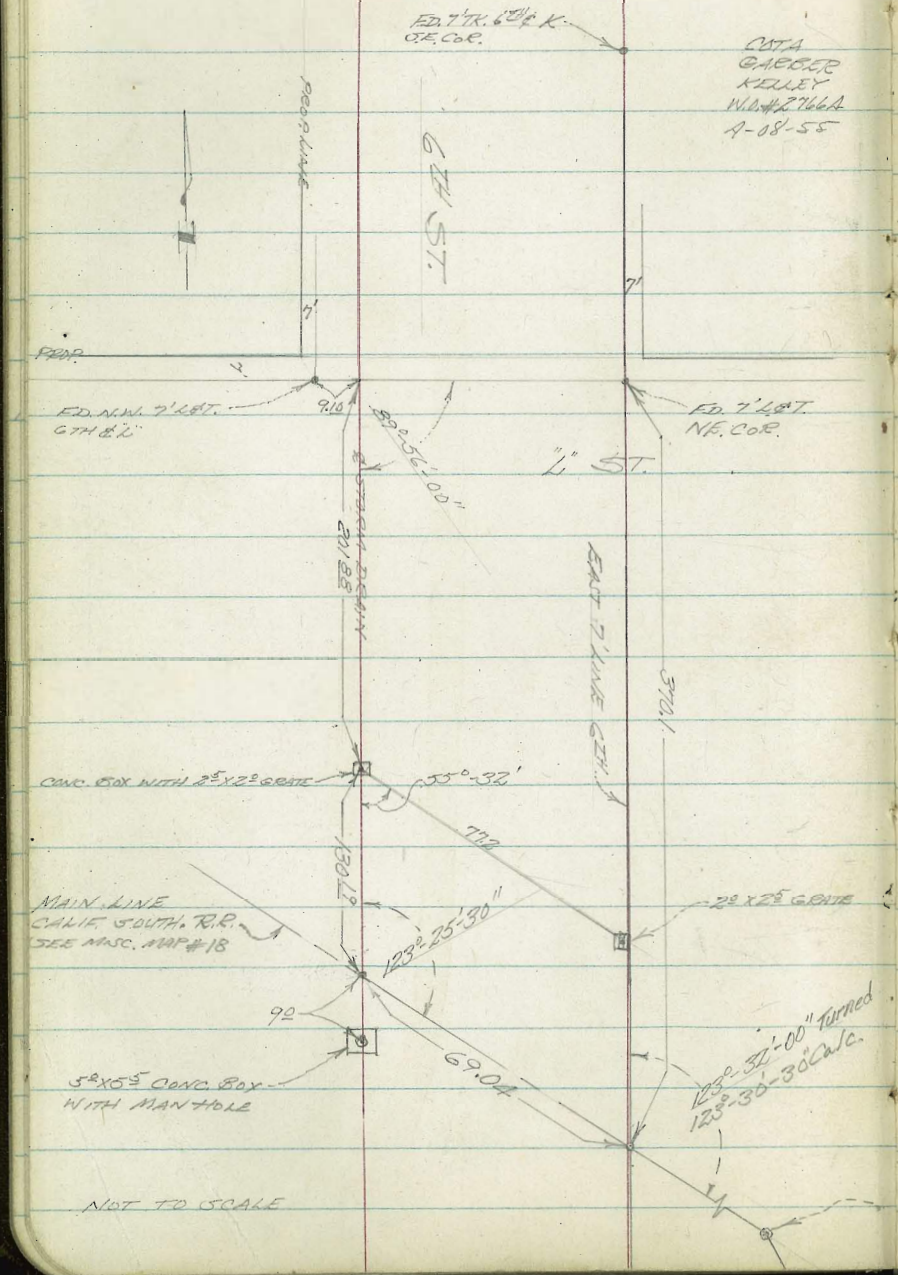
IMPERIAL

8TH ST.
80' ST.
52' ROADWAY
14' PARKING

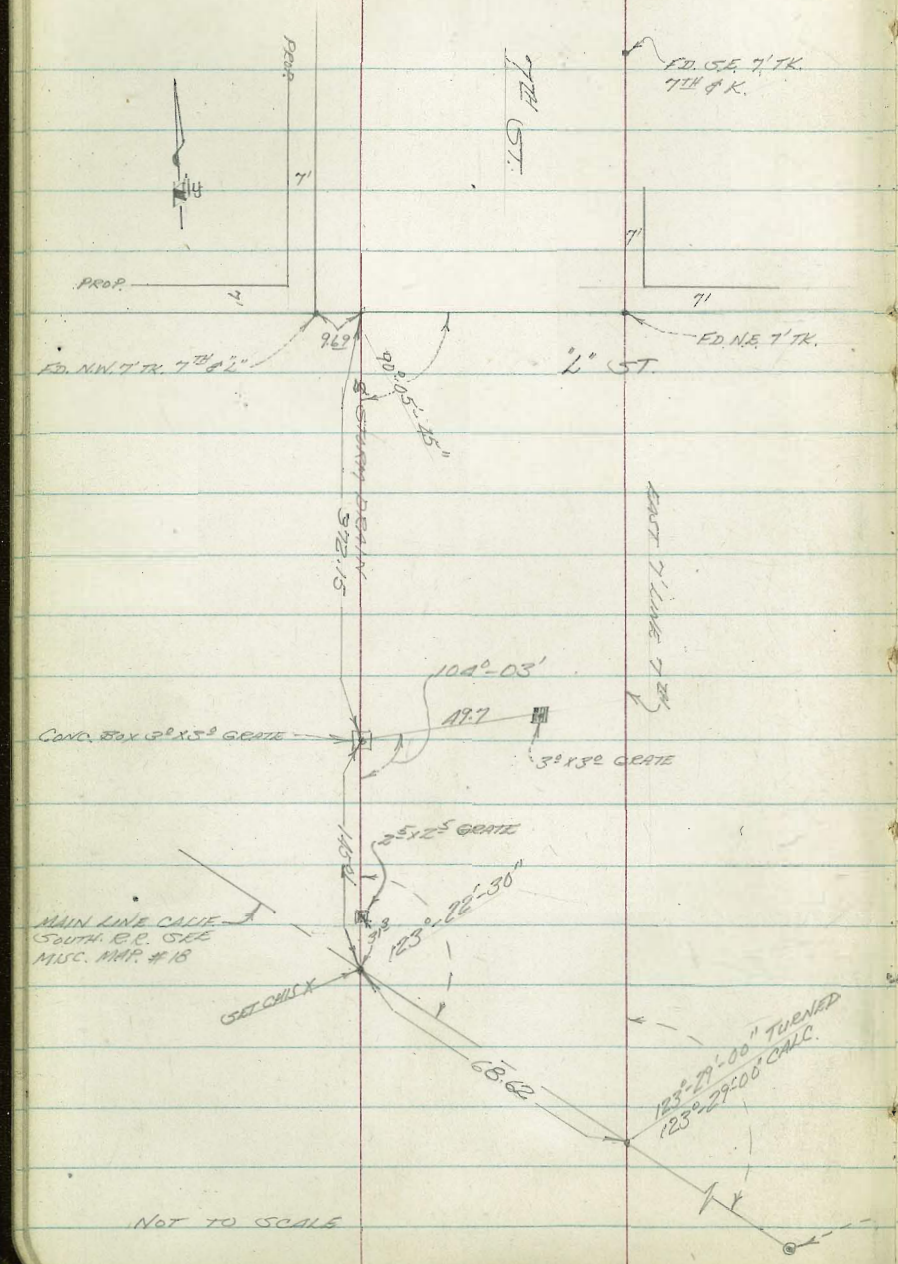
	LT. (WEST.)	℄	RT. (EAST)
0+28.9 ℄ CROSSES NORTH RAIL (FLUSH WITH A.C.)		4.15 RAIL	
0+20 ℄ CROSSES SOUTH RAIL (RAIL FLUSH WITH A.C.	4.07 10	4.11 RAIL	4.15 10
0+14 5 L.Y. C.B. LINE IMPERIAL - CURB & GUTTER - SAME ELEV.	3.94 14 C.B. & gut and c.b. 4.00 10 E.C. C.B. & gut	4.04	4.18 10
0+04 B.C. OF RETURN	3.9 10	4.01 C.B. & gut	4.07 10
0+00 { G.L.Y. PROP. LINE IMPERIAL CURB & GUTTER = SAME ELEV.	3.9 10	3.96 C.B. & gut	3.98 10
0-01	3.8 10	2.84 gut.	3.86 C.B. 2.87 2.5 3.39 3 3.87 10
0-30	3.7 10 DIT	2.99 gut.	3.57 C.B. 3.54 10 A.C.

	LT (WEST)	℄	RT (EAST)
1+10	4.4 / 10	4.06 9WH	4.68 CB. 4.55 / 10
0+86	4.2 / 10	3.88 9WH.	4.51 CB 4.30 / 10
0+80 NORTH. RL IMPERIAL (CB. & 9WH SAME ELEV.)	4.1 / 10	4.45 CB. & 9WH.	4.31 / 10
0+76 B.C. CURB RETURN (CURB & GUTTER SAME ELEV.)	4.1 / 10	4.41 CB. & 9WH	4.35 / 10
0+66 N.LY CB. LINE IMPERIAL	4.16 1A END CB 3.83 14 END A.C. 4.22 / 10 EC. CB. 3.95 / 10 EC. 9WH.	4.28	4.32 / 10
0+47.9 ℄ CROSSES NORTH RAIL		4.41 RAIL	
0+42.8 ℄ CROSSES SOUTH RAIL FINISH WITH AC	4.10 / 10	4.45 RAIL.	4.16 / 10

TIES ON STORM DRAIN, 6TH ST. & "L" ST.



TIES ON STORM DRAIN, 7TH ST. & L ST.



COTA
GARREE
KELLEY
W.O. #27662
4-08-55

--FD. CONC. FILLED PIPE ON R.L. OF R.R. MAIN LINE
STA. 148+41 ON MISC. MAP #18

X-Sec for Proposed Alley
125'± Nly of University Ave ~~and~~
from College Ave to Cartagena Drive

C.H.S.
Begg
Sohalin
Flora.

6-27-55
W.O. 21383

County Field Books # 908
1358

Maps # 2016- sheet #2
2518
2398

T.P. book. #
New book on Univ Ave.
No# as yet

Station on Base line is calculated.
Base line is 3' So. of sly. line of
College Ave Tract #1 + Tract #3. (Map. Dist.

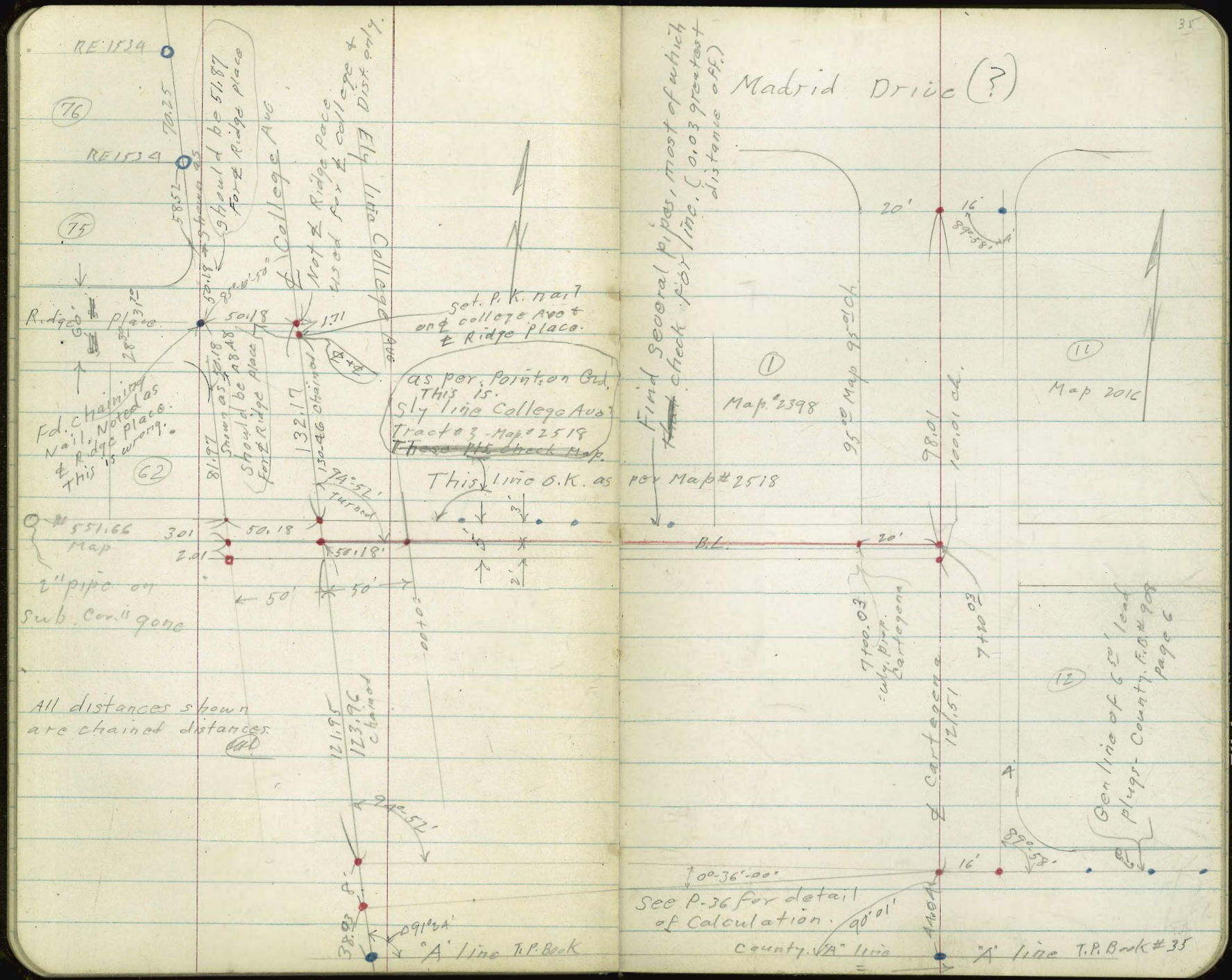
0+00 = Ely. line College Ave
7+00.03 = Wly. line Cartagena Dr.
B.W. = denotes base of wall footing
T.W. " Top " " "
E.P. " edge of Pave.

NOTE!
Line used as sly. line of College Ave. Tract #3 does not check @ map #2518 ~~but~~ fits survey points found on ground. Sly. line of Prop. pipes found on lots #75 + #76

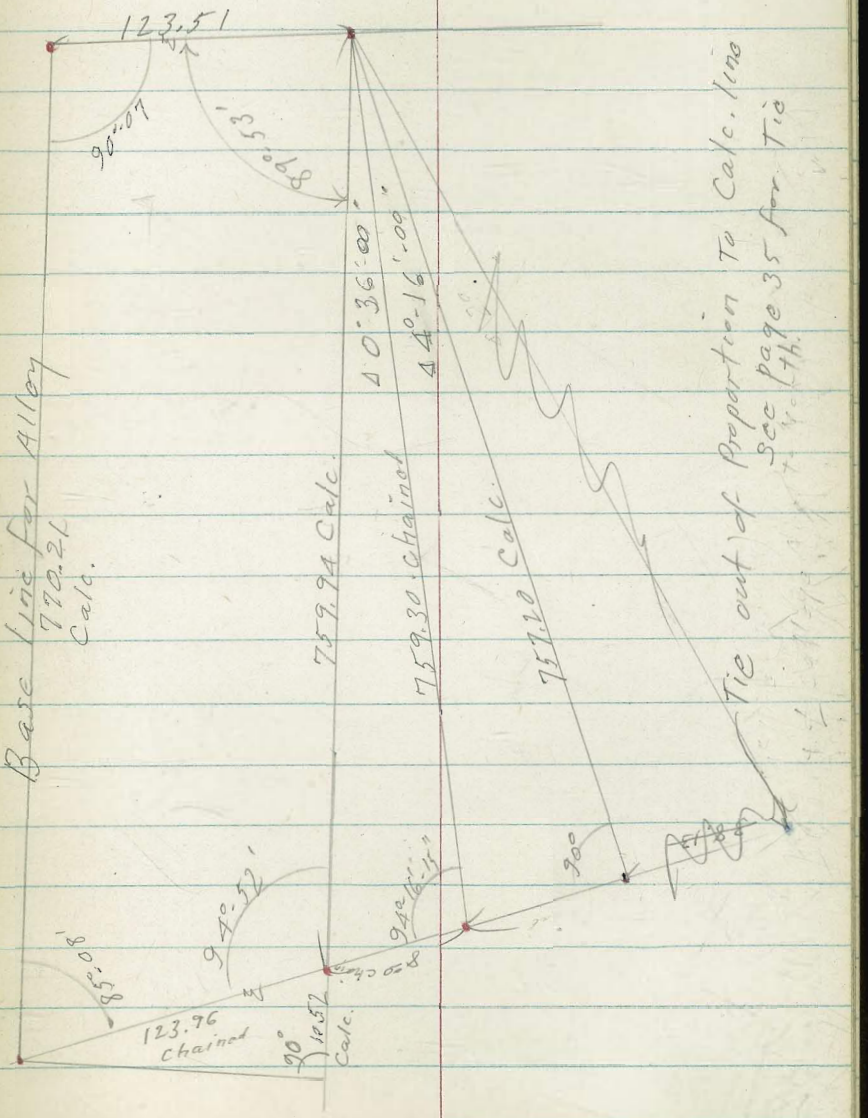
"A" line replaced from County Ties.
Base line set from pipes in ground

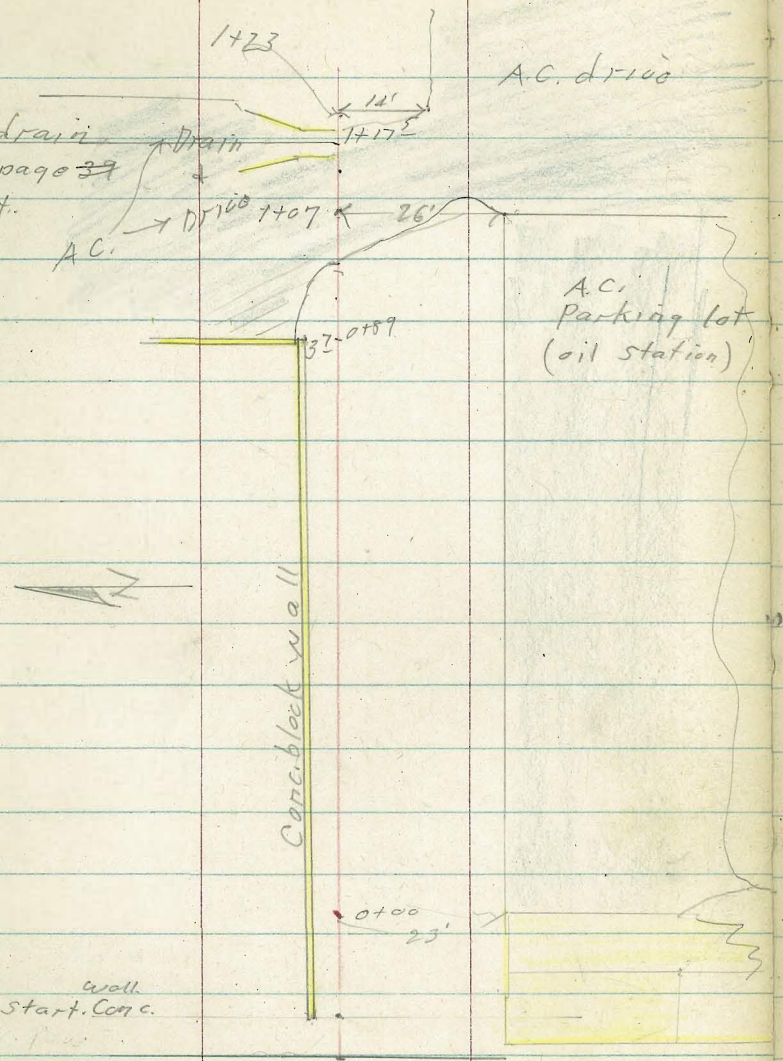
Note.
(Ridge Drive is in correct location, but points ~~in~~ Fd. in Pave. are wrong)

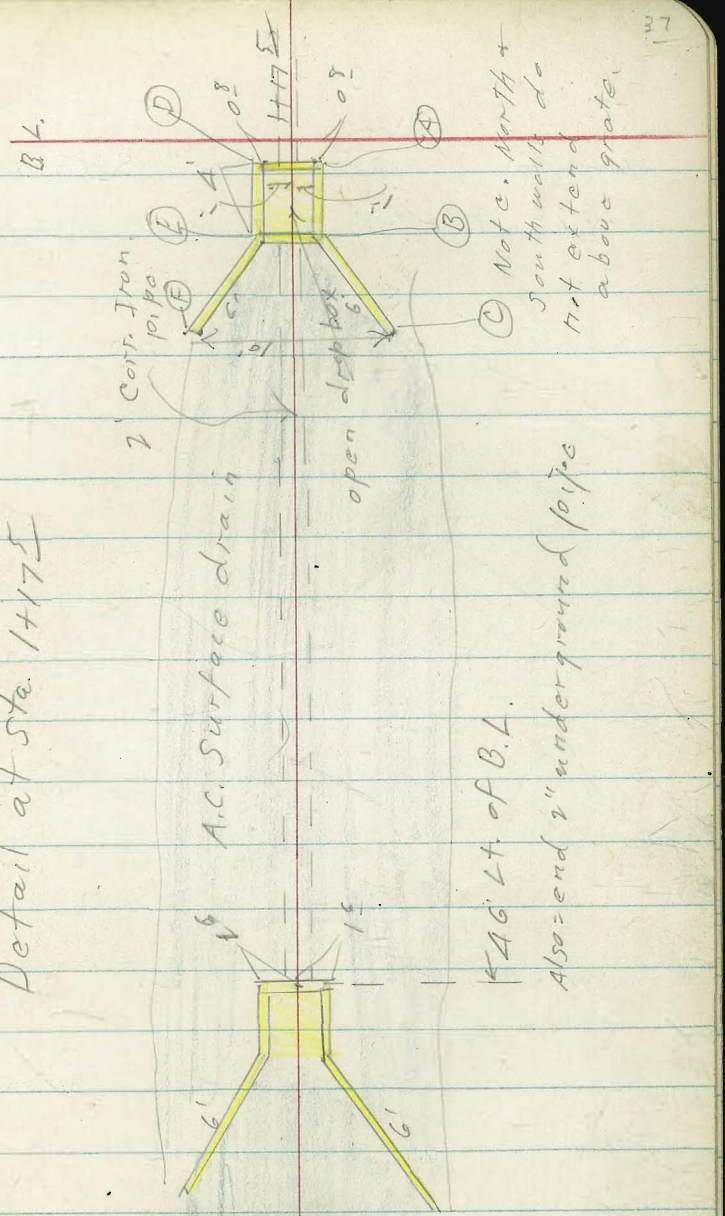
Points on Ridge Drive as set in Pave. set along southern boundary as College Ave. Tract #3 pipe found. are O.K. O.K. as shown on page 35.


RE 1534
76
RE 1534
75
58.52
T.M. 25
Should be 51.87
for ℄ Ridge place
College Ave
Not ℄ Ridge place
used for ℄ college &
Disk only.
Ely line College Ave
Ridge place
Fd. chaining Nail. Noted as Ridge place. & This is wrong.
62
50.18
1.71
Set P.K. nail on ℄ college Ave & ℄ Ridge place.
as per Pointon Cert. This is Sly line College Ave
Tract 3 - Map # 2518
Those pts check Map.
This line O.K. as per Map # 2518
81.87
Should be 98.48
for ℄ Ridge place
132.17 chained
130.46
74°-57'
Turned
551.66
Map
3.01
2.01
50.18
50'
50'
2" pipe on Sub. Cor. is gone
All distances shown are chained distances.
121.95
123.96 chained
74°-57'
38.03
91°-03'
"A" line T.P. Book
Find several pipes, most of which check pipe line. (0.03 greatest distance off.)
Madrid Drive (?)
1
Map # 2398
95°-01' Map 95°-01' calc.
98.01
100.01 calc.
11
Map 2016
20'
16'
89°-58'
B.L.
20'
7+00.03
Mtg. Bk. Cartagena
7+20.03
℄ Cartagena
121.51
12
Gen line of 6 ft lead plugs - County F.B. # 908 page 6
A
89°-58'
16'
0°-36'-00"
See P-36 for detail of Calculation.
90°-01'
Mtg
County "A" line
"A" line T.P. Book # 35

Detail of Calc. for stationing on base line.




1+23
14'
℄ drain
See page 39
on Rt.
Drain
1+17
A.C. drive
Drive
1+07
26'
A.C.
A.C.
Parking lot
(oil station)
37'-0"89
Conc. block wall
0+00
23'
37' Lt. wall.
0-16 Start. Conc.
0-21 = End AC
0-50
℄ College.

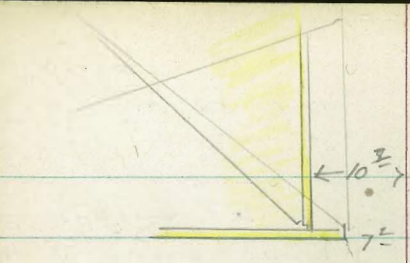

B.L.
1+17
0.8'
0.8'
D
A
E
B
F
C
2' Corr. Iron pipe
open drop box
Note. North + South walls do not extend above grade.
Detail at Sta. 1+17
A.C. Surface drain
46' Lt. of B.L.
Also = end 2" underground pipe

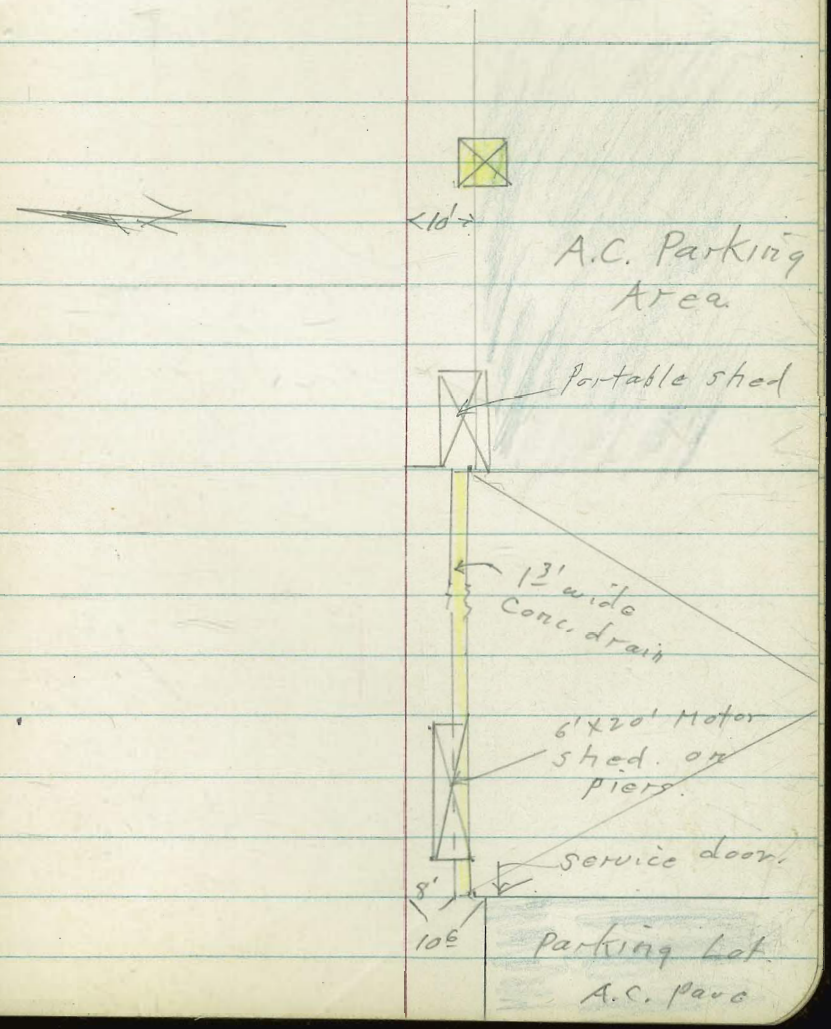
3' overhanging roof
Conc. foundation
4+17 10' Lt. = start 1 story Bldg.
4+17 = 7' Lt. = ℄ 8" wide N. + So. wall

7' x 7' conc. block incinerator
3+82 = 7' Rt. = ℄ North face of

10' Rt. = start Parking Area.
6' Rt. = start 7' x 23' wooden beer shed.
3+53 9' Rt. = end store Bldg.

2+40 9' Rt. = start conc. store Bldg.
10' Rt. = End parking Area.





7+05 = Curb line Cartagena.

10' Lt.
7+00 23 Start. Comb. walk. + ch.
Δ wlg. Cartagena. = end wall
6+99 E 16 7 Rt. = end wall + start curb. + walk

11 9 Rt. = end Bldg. + start. Conc. walk
6+83. 10' Lt. = end Bldg. start. Conc. walk

5+37 = Jog in Bldg.

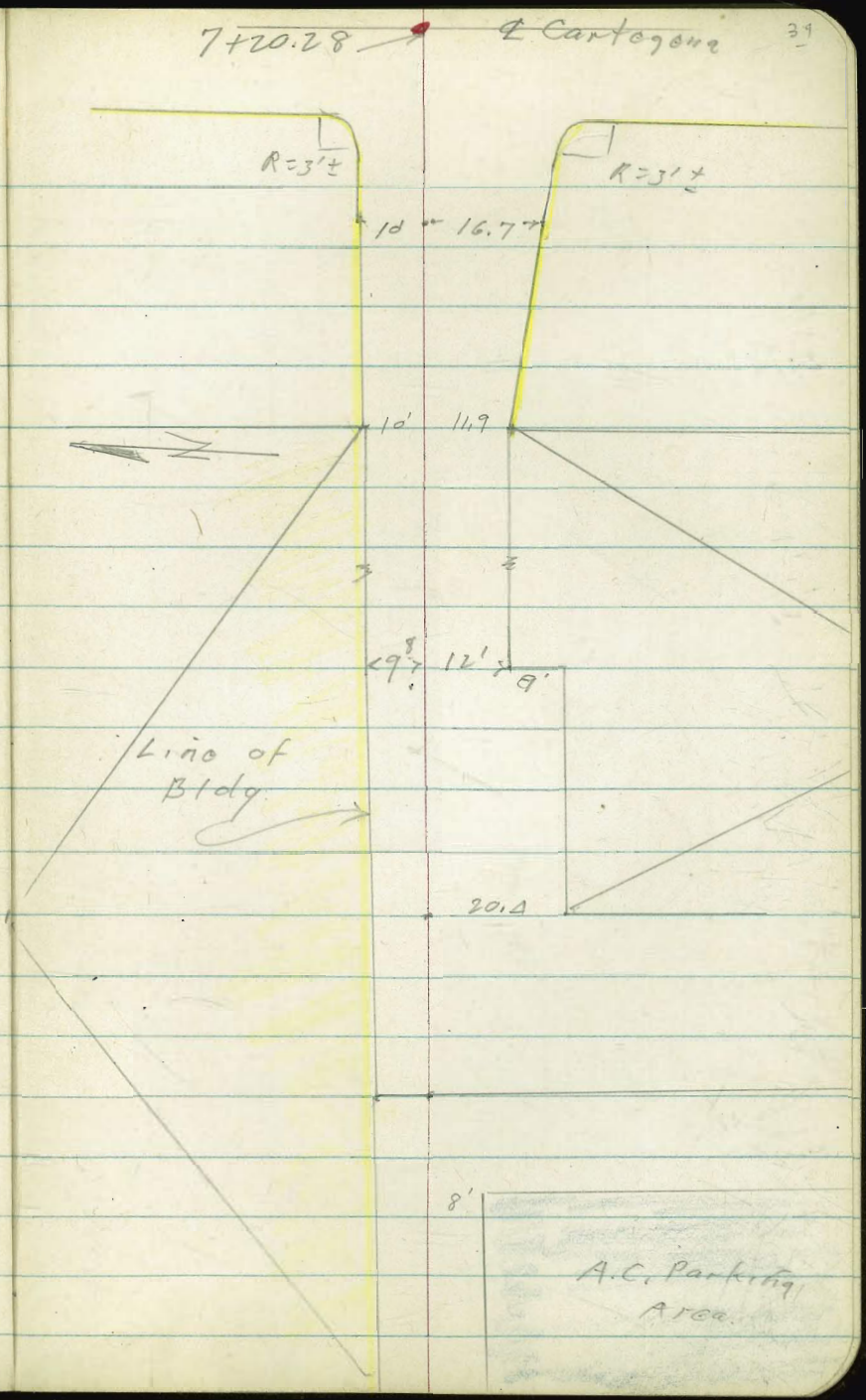
3+

(Garages - storerooms etc.)
4+96 - 20 Rt. = N.W. Cor. 1 story Bldg.

3" thick oil mix.
4+82 = start drive + parking Area

4+79 - 8' Rt. = end parking Area

2+



0-18 { 24' Rt. = deadman
3.8 Lt. = ctr. 14" P.pole # P37010

10.60 11.28 10.57
50 58 58
in drive C ℄

0-20 { 23' Rt. = Nly end existing curb

1.7 5.7 7.7 7.90 8.43
50 22 23 ℄ 23 ℄

0-21 { 23' Rt. = Meet A.C. Pave. Full width
= ~~ely.~~ edge pave.

2.10 6.45 8.47
50 23

3-

0-34

1.10 5.54 10.12
50 50

0-50 18 ℄ College Ave

0.54 5.16 9.80
50 50

336.04

T.P. 6.59 336.04 2.67 329.45

2- 9.90 332.12 — 322.22

□ Wly. end N.Wly. C.I. 21 min. + College

F.B. 1685
74

B.L.

drive.
4' Lt. = S. wly. cor 2" to 3" thick A.C.

0+89 - 3½ Lt. = end conc. wall.

and south. (No good)
0+50 1 2⅝ Lt. found piped leaning west

0+50

0+48 11⅝ Lt. = S. Ely Cor. House

0+12 9⅝ Lt. = S. wly Cor. house

T.P. 9.30 338.01 7.33 328.71
18" square conc. base.

0+01 - 23' Rt. = 4" pipe flood light stand.
23' Rt. = start A.C. Parking Area
23' Rt. = N. Ely Cor. Conc. walk

0+00 = Ely. line College

2 0-16 - 3⅞ Lt. = start conc. wall.

3.52 / 25 on pave — 4.01 / 4 / E.P.

1.9 T.W. — 7.4 / 32 B.W. — 4.1 / 32

3.7 / 20 — 3.9 / 5

336.1 — 330.5 — 332.2 — 332.2 — 330.9 — 327.7 — 325.9

1.9 T.W. — 7.5 / 38 B.W. — 5.8 / 39 — 5.8 / 3 — 7.1 — 10.3 / 7 — 12.10 / 25 E.P. — 7.02 / 50

338.01

334.4 — 331.2 — 331.3 — 330.5 — 329.3 — 328.62

2.0 / 30 — 2.9 / 5 — 1.6 / 37 T.W. — 4.8 / 32 B.W. — 4.7 / 35 — 5.5 — 6.7 / 6 — 7.42 / 23 A.C., walk + Grd. — 10.00 / 50 walk & A.C.

3.9 T.W. — 5.6 / 37 B.W.

336.04

Shown on page 37 - on right.
Rod for Throat of Catch Basin as

1+11 10' Lt. = wly. edge A.C. Surface drain
ely. edge drive

1+08 See page 37 - on Lt.
Rt. = Wly. edge drive

1+07 26' Rt. = N. Ely Cor. parking Lot.

1+03 = wly. edge A.C. drive

26' Rt. = E.P.
1+00 2' Lt. = E.P.

B.L. 332.05

333.45	333.03	333.44		333.80	331.71	333.37	332.01	333.39	332.10	333.44	331.73
4.56	5.98	4.57	5.96	4.71	6.30	4.64	6.00	4.62	5.91	4.57	6.28
F	E	F	F	A	A	B	B	C	C	D	D
T.W.	drain	T.W.	drain	T.W.	Grate	T.W.	drain	T.W.	drain	T.W.	~~drain~~ grate

				336.05		334.08		332.48		328.83		327.69			
				1.76		3.93		5.53		9.18		10.32			
				50		10				23		50			
										E.P.		on pave.			
334.91		334.31							330.91		329.6		329.61		327.51
3.10		3.70						5.5	7.20	7.0	8.4	8.40	10.50		
35		12							10	11	22	25	50		
									E.P.	Grd	Grd.	E.P.	E.P.		

									11.30		11.40				
									26		46				
									E.P.		E.P.				
									N. Ely. Cor.						

3.9
E.P.

334.3		333.81		333.4		333.3		328.0		326.6		326.4			
3.5		4.20		4.6		4.7		10.0		11.40		11.6			
20		2				2		9		26		46			
		E.P.								E.P.					

338.81

1+24				
T.P.	9.46	345.29	2.18	335.83
1+23	10' Lt. = Ely. edge drain			
1+19 = leave A.C.				
1+17 5	0 8 Lt. = ℄ drain + catch basin (P-37 Rt)			

B.L

331.4 — 3.9 / 50

331.0 — 4.3

334.3 — 11.0 / 2

334.0 — 11.3 / 10

328.64 — 16.65 / 17 / E.P.

327.74 — 17.55 / 40

345.29

335.82 — 2.19 / 45 / E.P. + Grd

332.9 — 5.10 / 10 / E.P. + Grd

334.01 — 4.0 / 7 / Grd.

333.5 — 4.5

329.7 — 8.3 / 14

328.70 — 9.31 / 16 / E.P. / Δ in pave

327.43 — 10.38 / 40

331.71 — 6.30 / 0 8 / E.P.

331.66 — 6.35 / E.P.

330.15 — 8.86 / 15 / Δ in pave

327.41 — 10.60 / 40

333.61 — 4.40 / 43 / ℄ drain at C.B.

332.01 — 6.00 / 5 / ℄ drain

332.01 — 6.10 / 4 8 / top of Nly. Edge box

8.93 / 4 8 / I.E. pipe to north

327.16 — 11.85 / I.E. box + pipe to South

332.61 — 6.40 / Ctr. grate

332.56 — 6.45 / 0 8 / Throat of drain

331.59 — 6.42

328 — 9.95 / 25

327.41 — 10.60 / 40

338.01

B.L.

3+46 12' Lt. = Large apricot tree

3+00

2+91 4^{E} Lt. = Pole # P. 277029

gutter (Page 38)

8^{E} Rt. = ℄, start 1^{3} w.de conc.

2+40 (add to notes below)

T.P. 6.65 349.41 2.53 342.76

2+40 9^{3} Rt. = start Conc. store Bldg.

2+00

1+50

1+45 – 3^{E} Lt. = deadman

1+33 42^{E} Rt. = N.wly. cor. Bldg.

8' Rt. = deadman

1+28 – 3^{E} Lt. = 12" pole # P 277030

	346.6	345.0	344.0	333.9	333.5	332.81
	2.8	5.1	5.4	15.5	15.9	16.60
	30		1	7	8	PG
					Edge of drain	T.E. drain
			331.5		333.08	
			17.9		15.53	
			8		8^{2}	
			Cul		drain	invert

349.41

	345.3	342.6	334.2	330.87	330.51
	0.3	2.7	11.1	14.42	14.78
	40		4	10^{6} E.P.	40
	344.3	341.6	335.1	329.67	329.23
	1.0	3.7	10.2	15.62	16.06
	40		3	11 E.P.	40
	342.5	341.1	333.3	328.98	328.44
	2.8	4.2	12.0	16.31	16.85
	40		4	14 E.P.	40
				328.15	
				17.14	
				42^{E}	

345.29

Conc. Floor + foundation.

4+17.5 10½ Lt. = start main Bldg.

4+17 { 7½ Lt. = ℄ N. + So. Bldg wall
5⁵ Lt. = Ctr. 14" P. pole # P 277028
7⁵ Lt. = end chain link fence.

T.P. 7.49 346.16 10.74 338.67

4+00

3+82 paving at incinerator

3+75 6⁵ Rt. = end portable shed.

3+65± = ⅂ P.O.T.

3+53½ 9' Rt. = start paved parking area

3+53 { 8⁵ Rt. = Elg. end drain
9½ Rt. = end Conc. Bldg.
6⁵ Rt. = start board shed - (P 38)
2⁹ Lt. = start 4' high chain link fence

345.6 344.7
0.6 1.5
10½ 10
Floor End

346.16.

346.1 345.1 345.1 334.4 332.8 332.4
3.3 4.3 4.3 15.0 16.6 17.0
10 1 7 10 30
E.P.

3.3 1.9
17.5
14

17.45
9
E.P.

345.6 345.0 332.4 332.3 331.71
3.8 4.4 17.0 17.1 17.70
30 6 8 8⁵
Edge of drain I⁵ drain

349.41

B.L.

5+00

339.45 — 338.65 — 337.90 — 337.92
6.71 — 7.51 — 8.26 — 8.24
10 — 10 — 20 — 20
line of Bldg — at Bldg

4+96 20' Rt. = N.W. Cor. Bldg

337.75
8.41
20
pave

parking area.
& start paved 2" thick plant mix.

4+82 = Cross chain link fence.

339.86 — 338.92 — 337.40 — 337.31
6.30 — 7.24 — 8.76 — 8.85
10 — E.P. — 20 — 40
E.P. — E.P. — E.P.

4+80 10' Lt. = line of Bldg

337.9 — 338.6 — 337.2 — 336.8
6.3 — 7.6 — 9.0 — 9.4
10 — 20 — 40

4+79 — 8' Rt. = end parking lot.

339.8 — 338.5 — 334.5 — 333.9
6.4 — 7.7 — 11.7 — 12.3
10 — 8 — 40
ab Bldg — E.P. & Gr'd. — on Elg. E.P.

4+50

342.8 — 342.5 — 339.7 — 334.8 — 333.94 — .32
3.4 — 3.7 — 6.5 — 11.4 — 12.22 — 12.84
10 — 3 — 4 — 8 — 40
at Bldg — E.P.

4+33 — 10' Lt. = ℄ 7' wide door

345.6
0.6
10'
Floor

346.16

T.P. 7.58 347.29 6.45 339.71

In Bldg.

10' Rt. = ℄ start loading dock

5+85 12' Rt. = ℄ 8' wide doorway

344.06
2.10
10
Floor level

340.12
6.04
12
doorway

5+70 12' Rt. = ℄ 4' doorway

340.17 339.89 339.52 339.74 340.12 340.15
5.99 6.27 6.64 6.42 6.04 6.01
10 9 11 12 12
at Bldg Pave doorway

5+50

339.70 339.33 339.52
6.46 6.83 6.64
9 12 12
pave Pave Pave
line of Bldg

5+37 - 20' Rt. } Jog in Bldg.
12' Rt. }

6.95 7.54
12 20
pave pave

340.14 339.65
6.02 6.53
10 10
Floor E.P.

5+35 10' Rt. = ℄ 3' wide door.

338.38
7.78
20±
floor level

5+24 - 20' Rt. = ℄ double Gar. door

346.16

B.L.

7+02 — 10' Lt. = cl. B.C.

7+00 — 10' Lt. = end wall + start cl
= wly Cartagena

6+99 — 22' Rt. = 14" stub to pole # P 270968
16½ Rt. = end wall - start curb
6+99 - 11½ Lt. = Pole # P 270968

6+83 — 119 Rt. / 10' Lt. = end Bldg + start Conc. wall.

6+74 — 10' Lt. = end loading dock.

6+52 — 12' Rt. = ℄ 7' wide doorway.

6+16 — 12' Rt. = ℄ 7' doorway

344.77	341.30			340.41	340.81	
4.39	4.86			5.75	5.35	
10	10			17½	17½	
cl	C			C	cl	
	341.86	341.47	341.00	340.56	340.88	
	4.30	4.69	5.16	5.60	5.28	
	10	10		16½	16½	
	cl	C		C	cl	
				340.56	340.88	
				5.60	5.28	
				16½	16½	
				C	cl. + T.W.	
	342.98	339.54	339.16	339.32	340.85	
	3.18	6.60	7.00	6.84	5.31	
	10	10		11⅞	11½	
	T.W.				T.W.	
	342.93					
	3.23					
	10					
	337.06		338.82	338.02	339.02	
	7.10		7.34	7.14	7.14	
	10			12	12	
					floor	
340.46	338.96		338.61	338.76	339.02	339.36
6.83	7.20		7.55	7.40	7.14	6.80
10	9			10	12	12
at Bldg					Pcac	Floor

347.29

orig. B.M. College + Union		5.79	322.19	322.22
T.P.	2.82	327.98	8.80	325.16
T.P.	1.94	333.96	9.32	332.02
T.P.	2.10	341.34	8.05	339.24

N ly end (chiseled □)
N.a. cl. Rct. Cartagena + Univ.

7+20 $\frac{03}{=}$ ℄ Cartagena

3.25 5.00 6.72
50 50

3.01 3.41 in drive 7.83 7.32
50 50 50 70 70
cl C C cl

7+05 $\frac{0}{=}$ = w ly. cl. line Cartagena

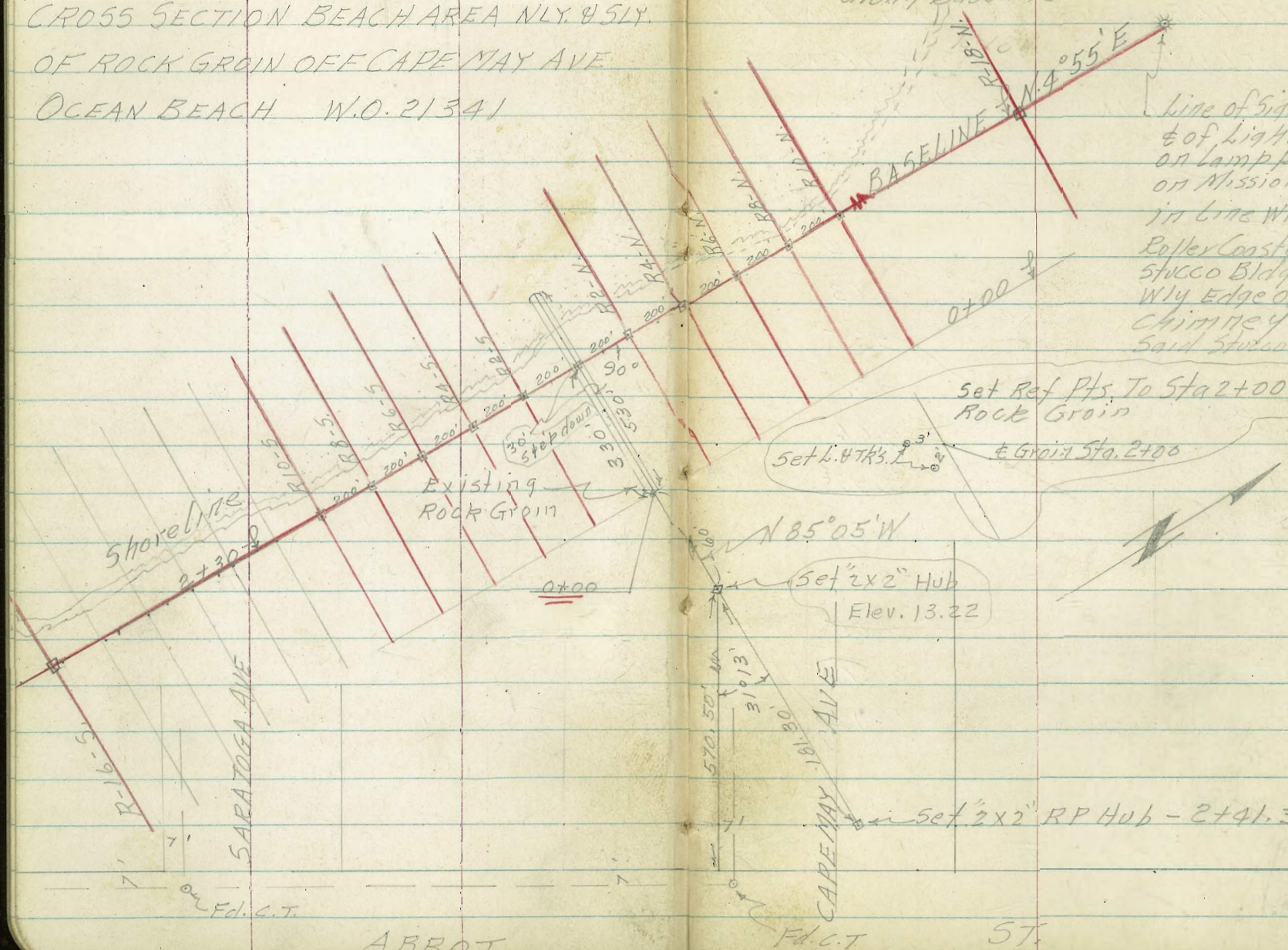
4.31 4.94 5.09 5.35 6.02 6.42 5.50
13 13 cc cl. cl. 21 21
cl. C P.I. P.I C cl.
E.C. E.C.

347.29

Ref G-348 8-18-55 T.A. Stamper (50)

NOTE: Set 2"x2" Hubs @ 100' Sta's along Baseline

CROSS SECTION BEACH AREA N'LY. & S'LY. OF ROCK GROIN OFF CAPE MAY AVE OCEAN BEACH W.O. 21341



PROFILE LEVELS ALONG CONTROL BASELINE FOR CROSS SECTIONS OF ROCK GROIN BEACH AREA

W.O. 21341

Sta	+	H.I.	-	Elev.
R10-S. 3+30				9.32
R9-S. 3+30				9.63
R8-S. 3+30				9.35
R7-S. 3+30				9.76
R6-S. TP 3+30				9.66
R5-S. 3+30				9.97
R4-S. 3+30				8.85
R3-S. 3+30				8.30
R2-S. 3+30				9.05
R1-S. 3+30				8.27
T.B.M.				8.42
T.B.M.			6.85	13.22
	+2.17	20.07		
B.M.				17.90

8-18-55 Stamper Huffman Presley Blunt

NOTE: (See Sketch Pg. 50)

Used direct Elev. Rod for Profile

Top of 2" x 2" Hub

" " "

" " "

" " "

" " "

" " "

" " "

" " "

" " "

" " "

Top of 2" x 2" Hub (N. 45, 0+00) = 3+30 W'ly

Top 2" x 2" Hub - 2+41.30 (See Sketch)

N.W.B.P. Cape May & Abbot St
U.S.C. & G.S. M.L.L.W. Datum

PROFILE LEVELS CONT'D.

	Elev.
T.B.M.	13.21 ~ 13.22
T.B.M.	8.42 ~ 8.42 ~
T.P.	5.38 ~ 5.38
R10 - N. 3+30	6.22
R9 - N. 3+30	5.02
R8 - N. 3+30	4.54
R7 - N. 3+30	4.87
R6 - N. T.P. 3+30	5.38
R5 - N 3+30	5.88
R4 - N. 3+30	6.63
R3 - N. 3+30	7.32
R2 - N. 3+30	8.02
R1 - N. 3+30	9.62
T.B.M.	8.42 ~ 8.42 ~
T.P.	9.66 ~ 9.66 ~

NOTE: 8-18-55

Direct Elev. Rod used for Profile Levels

Cont'd. Pg. 54

Top 2x2 Hub Sta -2+41.30

Top 2x2 Hub (0+00 N+5 3+30 W. B/L)

Top 2x2 Hub Sta 3+30 B/L. Sta.

" " " " "

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Top 2x2 Hub (0+00 N+5) 2+30

Top 2x2 Hub Sta 3+30 R6-S.

PROFILE LEVELS CONTD.

Sta	+	H.I	-	Elev

8-19-55 Stamper Huffman Presley Blunt (54)

CROSS SECTIONS OF BEACH AREA N'LY & S'LY OF ROCK GROIN OFF CAPE MAY AVE. OCEAN BEACH W.O. 21341

SEC. R1 - SOUTH		Elev
T.P.	-3.00	8.42
0+00	-2.0	9.4
0+30	-2.8	8.6
0+80	-4.4	7.0
1+30	-5.0	6.4
1+80	-4.8	6.6
2+30	-4.0	7.4
2+80	-4.1	7.3
5+80	-12.8	-1.4
5+30	-10.6	0.8
4+80	-8.0	3.4
4+30	-4.6	6.8
4+00 Break	-1.3	10.1
3+80	-1.6	9.8
3+30	-3.2	8.2
+3.00	∡ 11.42	
B.M. Top Hub (0+00 B/L 3+30)		8.42

SEC. R2 - SOUTH

		Elev.
0+00	-1.8	9.6
0+30	-3.9	7.5
0+80	-4.4	7.0
1+30	-5.2	6.2
1+80	-4.6	6.8
2+30	-3.8	7.6
2+80	-3.4	8.0
5+80	-13.0	-1.6
5+30	-10.9	0.5
4+80	-8.3	3.1
4+30	-4.6	6.8
4+00 break	-0.4	7.0
3+80	-1.2	10.2
3+30	-2.4	9.0
∡ 11.42		
B.M. (Hub R2-5, 3+30)		9.05

SEC. R3 - SOUTH

			Elev
0+00		- 2.8	9.2
0+30		- 4.2	7.2
0+80		- 4.4	7.0
1+30		- 5.0	6.4
1+80		- 4.5	6.9
2+30		- 3.8	7.6
2+80		- 3.2	8.2
5+80		-13.2	-1.8
5+30		-11.5	- 0.1
4+80		- 8.7	2.7
4+30		- 5.2	6.2
3+95	break	- 0.4	11.0
3+80		- 0.8	10.6
3+30		- 3.1	8.3

Δ 11.42

B.M. (Hub 3+30 R3-5) 8.30

SEC. R4 - SOUTH

		Elev.
0+00	-2.2	9.2
0+30	- 4.1	7.3
0+80	- 4.5	6.9
1+30	- 4.6	6.8
1+80	- 4.4	7.0
2+30	- 3.7	7.7
2+80	- 3.6	7.8
5+80	-13.7	-2.3
5+30	-11.8	-0.4
4+80	- 9.0	2.4
4+30	- 5.7	5.7
3+90 break	- 0.6	10.8
3+80	- 0.9	10.5
3+30	- 2.6	8.8

Δ 11.42

B.M. (Hub 3+30 R4-5) 8.85

SEC. R 5 - SOUTH

		Elev.
0+00	- 2.2	9.2
0+30	- 4.5	6.9
0+80	- 4.8	6.6
1+30	- 4.7	6.7
1+80	- 4.3	7.1
2+30	- 3.6	7.8
2+80	- 2.8	8.6
5+80	-13.6	-2.2
5+30	-12.0	-0.6
4+80	-9.2	2.2
4+30	-6.0	5.4
3+90 break	- 0.4	11.0
3+80	-0.5	10.9
3+30	-1.5	9.9
	∆ 11.42	
B.M. (Hub 3+30 R 5-S)		9.97

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SEC. R 6 - SOUTH

		Elev.
0+00	-3.5	7.9
0+30	-3.6	7.8
0+80	- 3.7	7.7
1+30	- 3.7	7.7
1+80	- 3.7	7.7
2+30	- 3.3	8.1
2+80	- 3.0	8.4
5+80	- 13.8	- 2.4
5+30	- 11.8	- 0.4
4+80	- 9.4	2.0
4+30	- 6.3	5.1
3+85 break	- 0.3	11.1
3+80	- 0.5	10.9
3+30	- 1.8	9.6
	∆ 11.42	
B.M. (Hub 3+30 R 6-S)		9.66

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SEC. R-7 SOUTH

		Elev.
0+00	-2.2	9.2
0+30	-2.3	9.1
0+80	-2.1	9.3
1+30	-1.8	9.6
1+80	-1.7	9.7
2+30	-1.9	9.5
2+80	-1.9	9.5
5+80	-13.1	-1.7
5+30	-12.1	-0.7
4+80	-9.4	2.0
4+30	-6.5	4.9
3+80 break	-0.6	10.8
3+30	-1.7	9.7
	⍋ 11.42	
B.M. (Hub 3+30 R7-5)		9.76

SEC. R-8 SOUTH

		Elev.
1+30	0.0	11.3
1+80	+1.0	12.32
2+30	-2.2	9.1
2+65	-3.3	8.0
2+80	-3.5	7.8
5+30	-11.9	-0.6
4+80	-8.9	2.4
4+30	-6.3	5.0
3+80 break	-0.9	10.4
3+30	-2.1	9.2
	⍋ 11.32	
B.M. (Hub 3+30 R8-5)		9.35

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SEC. R9-SOUTH

		Elev
1+80	0.0	11.4
2+30	-0.3	11.1
2+80	-1.4	10.0
5+30	-11.8	-0.4
4+80	-8.9	2.5
4+30	-6.0	5.4
3+80 break	-0.5	10.9
3+30	-1.8	9.6
	∓ 11.42	
B.M. (Hub 3+30 R-9-5)		9.63

SEC. R-10 SOUTH

		Elev.
1+30	Checked 9-16-55 T.A.S.	+ 0.5 ~~+0.9~~ 11.9
1+80	~~+1.2~~ 0.2	~~10.2~~ 11.3
2+30	- 1.7	9.7
2+80	- 2.3	9.1
5+80	- 12.6	- 1.2
5+30	- 11.2	0.2
4+80	- 8.6	2.8
4+30	- 5.5	5.9
3+85	- 0.8	10.6
3+80	- 0.9	10.5
3+30	- 2.1	9.3
	∓ 11.42	
B.M. (Hub 3+30 R10-5)		9.32

SEC. R1 - NORTH

		Elev.
0+00	- 4.2	9.5
0+30	- 4.2	9.5
0+80	- 4.9	8.8
1+30	- 6.8	6.9
1+80	-10.0	3.7
2+30	- 8.9	4.8
2+80	- 5.6	8.1
	+4.10 ℄ 13.72	
5+80	- 12.9	- 1.6
5+30	- 11.4	- 0.2
4+80	- 9.7	1.6
4+30	- 8.1	3.2
3+80	- 6.7	4.6
	+1.70 11.32	
B.M. (Hub 3+30 R1-N.)		9.62

SEC. R2 - NORTH

		Elev
0+00	- 3.3	10.4
0+30	- 2.6	11.1
0+80	- 4.8	8.9
1+30	- 6.4	7.3
1+80	- 9.6	4.1
2+30	- 7.1	6.6
2+80	- 5.2	8.5
	℄ 13.72	
5+80	- 12.8	- 1.5
5+30	- 11.3	0.0
4+80	- 9.8	1.5
4+30	- 8.2	3.1
3+80	- 7.0	4.0
3+30	- 3.3	8.0
	11.32	
BM. (Hub 3+30 R2-N)		8.02

8-19-55

SEC. R3 - NORTH

		Elev.
0+00	- 3.7	10.0
0+30	- 3.8	9.9
0+80	- 4.7	9.0
1+30	- 5.7	8.0
1+80	- 9.2	4.5
2+30	- 7.0	6.7
2+80	- 5.3	8.4
	⍓ 13.72	
5+80	- 12.4	- 1.1
5+30	- 10.9	0.4
4+80	- 9.3	2.0
4+30	- 8.0	3.3
3+80	- 7.1	4.2
3+30	- 4.0	7.3
	⍓ 11.32	
B.M. (Hub 3+30 R3-N.)		7.32

SEC. R4 - NORTH

		Elev.
0+00	- 3.0	10.7
0+30	- 3.0	10.7
0+80	- 4.0	9.7
1+30	- 5.2	8.5
1+80	- 8.6	5.1
2+30	- 7.2	6.5
2+80	- 5.1	8.6
	⍓ 13.72	
5+80	- 12.0	- 0.7
5+30	- 10.6	0.7
4+80	- 9.0	2.3
4+30	- 7.7	3.6
3+80	- 7.1	4.2
3+30	- 4.7	6.6
	⍓ 11.32	
B.M. (Hub 3+30 R4-N.)		6.63

8-19-55

SEC R5 - NORTH

		Elev
0+00	- 3.3	10.4
0+30	- 3.1	10.6
0+80	- 3.7	10.0
1+30	- 4.5	9.2
1+80	- 7.1	6.6
2+30	- 6.0	7.7
2+80	- 5.9	7.8
	⏊ 13.72	
5+80	- 11.1	0.2
5+30	- 9.8	1.5
4+80	- 8.5	2.8
4+30	- 7.4	3.9
3+80	- 6.8	4.5
3+30	- 5.4	5.9
	⏊ 11.32	0.2

BM (Hub 3+30 R5 N.) 5.88

SEC R6 - NORTH

		Elev.
0+00	- 3.1	10.6
0+30	- 3.1	10.6
0+80	- 3.3	10.4
1+30	- 4.0	9.7
1+80	- 6.5	7.2
2+30	- 6.4	7.3
2+80	- 7.3	6.4
	⏊ 13.72	
6+30	- 11.8	- 0.5
5+80	- 10.6	0.7
5+30	- 9.3	2.0
4+80	- 8.1	3.2
4+30	- 7.4	3.9
3+80	- 6.8	4.5
3+30	- 5.9	5.4
	⏊ 11.32	

BM (Hub 3+30 R6-N.) 5.38

8-19-55

SEC. R7 - NORTH

		Elev
0+00	-3.5	10.2
0+30	-3.5	10.2
0+80	-3.2	10.5
1+30	-4.0	9.7
1+80	-5.1	8.6
2+30	-7.4	6.3
2+80	-8.0	5.7
↑ 13.72		
6+30	-11.5	-0.2
5+80	-10.0	1.3
5+30	-8.8	2.5
4+80	-8.0	3.3
4+30	-7.3	4.0
3+80	-7.0	4.3
3+30	-6.5	4.8
↑ 11.32		
BM (Hub 3+30 R7-N)		4.87

SEC. R8 - NORTH

		Elev
0+00	-2.7	11.0
0+30	-3.0	10.7
0+80	-3.7	10.0
1+30	-3.7	10.0
1+80	-4.3	9.4
2+30	-5.2	8.5
2+80	-8.0	5.7
↑ 13.72		
6+80	-12.2	-0.9
6+30	-11.0	0.3
5+80	-9.7	1.6
5+30	-8.6	2.7
4+80	-7.8	3.5
4+30	-7.4	3.9
3+80	-7.3	4.0
3+30	-6.8	4.5
↑ 11.32		
BM (Hub 3+30 R8-N)		4.54

8-19-55

SEC R9 - NORTH		ELEV.
0+00	- 2.2	11.5
0+30	- 3.2	10.5
0+80	- 3.0	10.7
1+30	- 3.1	10.6
1+80	- 3.5	10.2
2+30	- 5.4	8.3
2+80	- 6.4	7.3
↑ 13.72		
6+80	-11.5	-0.2
6+30	-10.3	1.0
5+80	- 9.3	2.0
5+30	- 8.4	2.9
4+80	- 7.8	3.5
4+30	- 7.6	3.7
3+80	- 7.5	3.8
3+30	- 6.3	5.0
	↑ 11.32	
BM (Hub 3+30 R9-N.)		5.02

SEC. R10 - NORTH		ELEV
TBM. (Hub 3+30 R1-N.)	- 4.16	9.62
0+00	- 2.6	11.1
0+30	- 3.3	10.4
0+80	- 2.7	11.0
1+30	- 2.7	11.0
1+80	- 3.5	10.2
2+30	- 3.4	10.3
2+80	- 5.5	8.2
↑ 13.72		
7+30	- 11.9	-0.6
6+80	- 10.9	0.4
6+30	- 9.7	1.6
5+80	- 8.9	2.4
5+30	- 8.4	2.9
4+80	- 8.1	3.2
4+30	- 8.0	3.3
3+80	- 6.9	4.4
3+30	- 5.1	6.2
↑ 11.32		
BM (Hub 3+30 R10-N.)		6.22

9-16-55

NOTE: See Sketch Pg. 50

Stamper
Garber
Kelley
Blunt

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ADDITIONAL CROSS SECTIONS N'LY. & S'LY OF ROCK GROIN OFF CAPE MAY AVE OCEAN BEACH W.O. 21341

Sta.	+	H.I.	-	Elev.
	5.82	14.20		
TP			8.33	8.38
T.B.M. (Side Shot)			3.55	13.16 = 13.22
	7.29	16.71		
TP			11.08	9.42
Top Hub R16-S			6.76	13.74
Top Hub R15-S			5.60	14.90
Top Hub R14-S			6.22	14.28
	9.40	20.50		
Top Hub R13-S TP			5.22	11.10
Top Hub R12-S			4.75	11.57
Top Hub R11-S			5.64	10.68
	8.25	16.32		
TP			8.49	8.07
	3.34	16.56		
T.B.M.				13.22

Sta	+	H.I	-	Elev.
T.B.M.			3.89	13.18 ~ 13.22
	4.79	17.07		
TP			3.27	12.28
	5.10	15.55		
TP Top Hub			5.46	10.45
R18-North Top Hub			7.06	8.85
R17-North Top Hub			6.89	9.02
R16-North Top Hub			6.02	9.89
R15-North Top Hub			5.34	10.57
R14-North Top Hub			5.86	10.05
R13-North Top Hub			5.66	10.25
R12-North			7.15	8.76
	8.55	15.91		
Top Hub R11-North TP			6.84	7.36
		14.20		
Top of "2X2" Hub - 2				41.30 (See Pg. 51)

9-16-35

SECTION R16 - SOUTH

Stg		Elev
5+80	-13.0	0.3
5+30	-12.0	1.3
4+80	-9.5	3.8
4+30	-4.4	9.0
	⊼ 13.35	
Top Hub. R13-South	13.35	
.TBM. +2.25		11.10
Top bank		
4+25	-9.7	10.8
3+80	-8.0	12.5
1+80	-5.7	14.8
2+30	-6.1	14.4
2+80	-6.1	14.4
3+30	-6.8	13.7
	⊼ 20.50	

SECTION R15 - SOUTH

-

5+80	-14.2	-0.9
5+30	-11.4	2.0
4+80	-10.0	3.3
4+30	-7.0	6.3
	⊼ 13.35	
Top bank		
4+12	-8.2	12.3 EHA
3+80	-7.1	13.4
1+50	-6.0	14.5
1+80	-7.1	13.4
2+30	-7.0	13.5
2+80	-6.6	13.9
3+30	-5.6	14.9
	⊼ 20.50	

9-16-55

SECTION R14 - SOUTH

Sta		Elev
5+80	-14.5	-1.2
5+30	-12.2	1.1
4+80	-10.6	2.7
4+30	-8.5	4.8
	⊼ 13.35	
Top bank 3+97	-8.8	11.7
3+80	-9.0	11.5
0+80	-6.1	14.4
1+30	-6.9	13.6
1+80	-6.7	13.8
2+30	-6.0	14.5
2+80	-5.6	14.9
3+30	-6.2	14.3
	⊼ 20.50	

SECTION R13 - SOUTH

Sta		Elev
5+30	-12.9	0.4
4+80	-11.0	2.3
4+30	-9.0	4.3
	⊼ 13.35	
Top bank 3+75	-10.2	10.3
0+30	-6.1	14.4
0+80	-5.7	14.8
1+30	-5.7	14.8
1+80	-5.4	15.1
2+30	-7.5	13.5
2+80	-8.6	11.4
3+30	-9.4	11.1
	⊼ 20.50	

9-16-55

SECTION R12 - SOUTH

Sta		Elev
5+80	-14.8	-1.5
5+30	-12.9	0.4
4+80	-11.1	2.2
4+30	-9.0	4.3
	⅄ 13.35	
Top bank		
3+78	-9.0	11.5 E.H.A.
0+30	-5.9	14.6
0+80	-6.7	13.8
1+30	-6.0	14.5
1+80	-6.3	14.2
2+30	-7.0	13.5
2+80	-8.2	12.3
3+30	-9.0	11.5
	⅄ 20.50	

SECTION R11 - SOUTH

Sta		Elev
5+80	-15.0	-1.7
5+30	-13.3	0.0
4+80	-11.4	2.0
4+30	-9.5	3.8
	⅄ 13.35	
Top bank		
3+75	-9.2	11.3
0+30	-6.4	14.1
0+80	-7.5	13.0
1+30	-6.4	14.1
1+80	-7.2	13.3
2+30	-8.4	12.1
2+80	-10.1	10.4
3+30	-9.8	10.7
	⅄ 20.50	

9-16-55

SECTION R 10 - SOUTH

Sta		Elev
NOTE: This Sec. Taken as Check on Original Section		
T.B.M. Top Hub R13-South	-2.25	11.10
5+80	-15.3	-2.0
5+30	-13.2	0.1
4+80	-11.4	2.0
4+30	-9.5	3.8
Σ	13.35	
Top bank 3+80	-9.3	11.2
0+00	-6.7	13.8
0+30	-7.9	12.6
0+80	-7.5	13.0
1+30	-8.4	12.1
1+80	-9.3	11.2
2+30	-10.7	9.8
2+80	-11.2	9.3
3+30	-10.4	10.1
Σ	20.50	

SECTION R 11 - NORTH

Sta		Elev
7+80	-11.4	-0.5
7+30	-10.4	0.5
6+80	-9.6	1.3
6+30	-8.8	2.1
5+80	-8.1	2.8
5+30	-7.3	3.6
4+80	-6.6	4.3
4+30	-4.8	6.1
3+80	-3.3	7.6
Σ	10.89	
T.B.M. +3.53	10.89	7.36
0+00	-5.1	10.8
0+30	-5.2	10.7
0+80	-5.7	10.2
1+30	-5.2	10.7
1+80	-4.8	11.1
2+30	-6.0	9.9
2+80	-6.5	9.4
3+30	-8.6	7.3
Σ	15.91	

9-16-55

SECTION R12 - NORTH

Sta		Elev
8+30	-11.7	-0.8
7+80	-10.7	0.2
7+30	-9.8	1.1
6+80	-9.0	1.9
6+30	-8.2	2.7
5+80	-7.6	3.3
5+30	-7.0	3.9
4+80	-6.1	4.8
4+30	-4.4	6.5
3+80	-3.1	7.8
	↑ 10.89	
✓ 0+30	-5.3	10.6
0+80	-5.1	10.8
1+30	-6.0	9.9
1+80	-5.3	10.6
2+30	-5.0	10.9
2+80	-6.3	9.6
3+30	-7.1	8.8
	↑ 15.91	

SECTION R13 - NORTH

Sta		Elev
8+80	-12.1	-1.2
8+30	-11.0	-0.1
7+80	-10.0	0.9
7+30	-9.2	1.7
6+80	-8.6	2.3
6+30	-8.1	2.8
5+80	-7.5	3.4
5+30	-6.8	4.1
4+80	-5.8	5.1
4+30	-3.6	7.3
3+80	-2.7	8.2
	↑ 10.89	
✓ 0+30	-5.6	10.3
0+80	-5.6	10.3
1+30	-6.5	9.4
1+80	-6.4	9.5
2+30	-5.4	10.5
2+80	-5.6	10.3
3+30	-5.7	10.2
	↑ 15.91	

9-16-55

SECTION R14 - NORTH

Sta		Elev.
8+80	-11.6	-0.7
8+30	-10.6	0.3
7+80	-9.8	1.1
7+30	-9.0	1.9
6+80	-8.5	2.4
6+30	-8.1	2.8
5+80	-7.5	3.4
5+30	-6.8	4.1
4+80	-5.5	5.4
4+30	-2.8	8.1
	⅄ 10.89	
break 3+80	-6.2	9.7
✓ 0+30	-6.1	9.8
0+80	-5.8	10.1
1+30	-5.9	10.0
1+80	-6.4	9.5
2+30	-6.5	9.4
2+80	-5.5	10.4
3+30	-5.9	10.0
	⅄ 15.91	

SECTION R15 - NORTH

Sta		Elev.
9+30	-10.6	0.3
8+80	-10.3	0.6
8+30	-10.0	0.9
7+80	-9.5	1.4
7+30	-9.1	1.8
6+80	-8.5	2.4
6+30	-7.8	3.1
5+80	-7.1	3.8
5+30	-6.0	4.9
4+80	-3.5	7.4
	⅄ 10.89	
break 4+56	-7.2	8.7
4+30	-6.4	9.5
3+80	-6.1	9.8
✓ 0+80	-6.0	9.9
1+30	-6.8	9.1
1+80	-6.7	9.2
2+30	-6.8	9.1
2+80	-6.1	9.8
3+30	-5.3	10.6
	⅄ 15.91	

9-16-53

SECTION R16 - NORTH

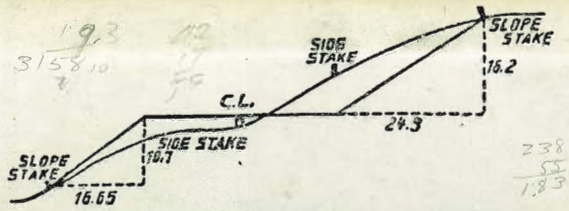
Sta.		Elev.
9+30	-10.4	0.5
8+80	- 9.9	1.0
8+30	- 9.4	1.5
7+80	- 8.8	2.1
7+30	- 8.4	2.5
6+80	- 7.9	3.0
6+30	- 7.3	3.6
5+80	- 6.4	4.5
5+30	- 4.6	6.3
	Δ 10.89	
Top bank 5+00	- 7.3	8.6
4+80	- 7.0	8.9
4+30	- 6.2	9.7
3+80	- 6.6	9.3
1+30	- 6.8	9.1
1+80	- 7.5	8.4
2+30	- 7.4	8.5
2+80	- 6.7	9.2
3+30	- 6.0	9.9
	Δ 15.91	

SECTION R17 - NORTH

Sta		Elev.
9+30	-10.0	0.9
8+80	- 9.4	1.5
8+30	- 8.8	2.1
7+80	- 8.2	2.7
7+30	- 7.6	3.3
6+80	- 7.1	3.8
6+30	- 6.3	4.6
5+80	- 4.6	6.3
5+60 break	- 2.9	8.0
5+30	- 2.5	8.4
	Δ 10.89	
Top bank 4+80	- 6.4	9.5
4+30	- 6.9	9.0
3+80	- 6.7	9.2
0+80	- 7.2	8.7
1+30	- 7.1	8.8
1+80	- 7.0	8.9
2+30	- 7.2	8.7
2+80	- 8.4	7.5
3+30	- 6.9	9.0
	Δ 15.91	

9-16-53

SECTION R-18 - NORTH Sta		Elev	
T.B.M.	-3.53	7.36~7.36	Starting Bench (see Pg. 68)
7+30	-7.3	3.6	Toe Setty
6+80	-6.0	4.9	
6+30	-4.7	6.2	
5+80	-3.1	7.8	
	Δ 10.89		
Top bank 5+46	-6.5	9.4	
5+30 -	-6.5	9.4	
4+80	-7.4	8.5	
4+30	-7.5	8.4	
3+80	-7.9	8.0	
✓ 0+80	-8.1	7.8	
1+30	-7.5	8.4	
1+80	-10.1	5.8	
2+30	-7.8	8.1	
2+80	-7.9	8.0	
3+30	-7.1	8.8	
	Δ 15.91		



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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