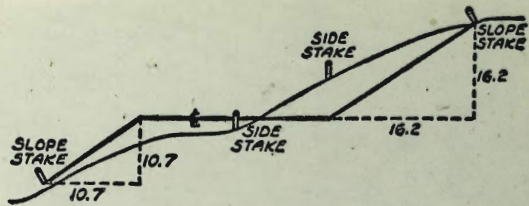


10-37 - 50'



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.971	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.78	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Drawing
E. M. H. #1 - (12875-L) - P 76

Line lots #21 & 22 - P-79

Sewer
Sierra Mar. to Primrose St
thru Lot #84 Villa Tract. 2

La Jolla Hills Sewer

List of references P 11

From Torrey Pines Ad. at Roseland Dr.

Thru lots #19-22 to Lookout Dr. 11

Boulevard Place line 26

Lookout Drive Boulevard }

Place to Soledad Ave } 33

Lookout Drive from }

Lot #21 Ely to Lot #28 } 43

Lookout Drive - Wly + }

Nly to Lot #33 } 45

Line to Lots #22-23-24 - P 46

" Thru Lot #30 P-43

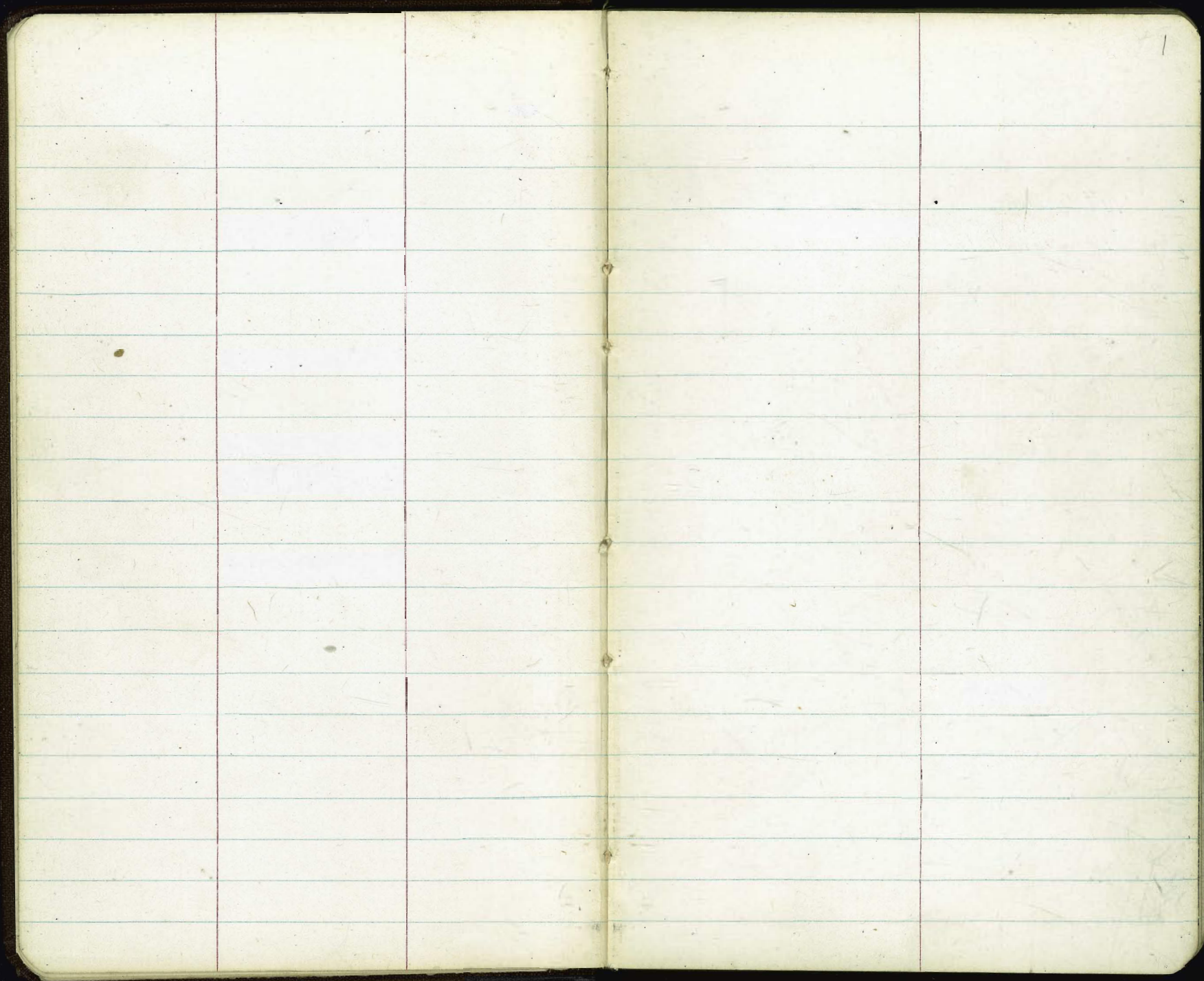
" " Lots #59-60-62-67 - P 57

" Hillside Dr. to sewer } P-68

Lot #61 also

Lots #68-69-70 - P 68

Also Book 2333



"B" line thru Lot # 84
 Villa Tract - La Jolla Park
 Map # 1535

Continuation of Sierra Mar
 Line from Sta 6456.35
 in F.B. 2028 - page 2c

81-36-30
 2 59
 84 35-30

For this line
 see FB 2333
 p. 63

Cont. P-3

11+62.71
 $\Delta 72^\circ - Lt_1$

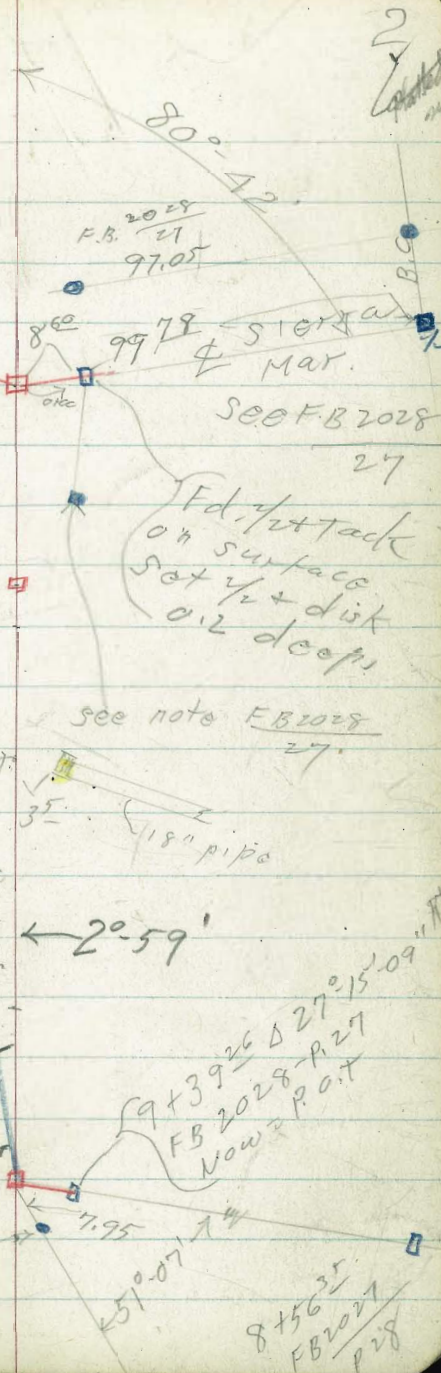
11+09.68 P.O.T.
 112

10+59

"C" line

C.H.S. 10-
 10-1-24

Right
 $\Delta 81^\circ - 36' - 30''$
 9+53
 7837.39 P.O.T.
 Prop. pin



F.B. 2028
 21
 97.05

See FB 2028
 27

Ed. 1/4 tack
 on surface
 set 1/2 + disk
 0.2 deep

see note FB 2028
 27

18" pipe

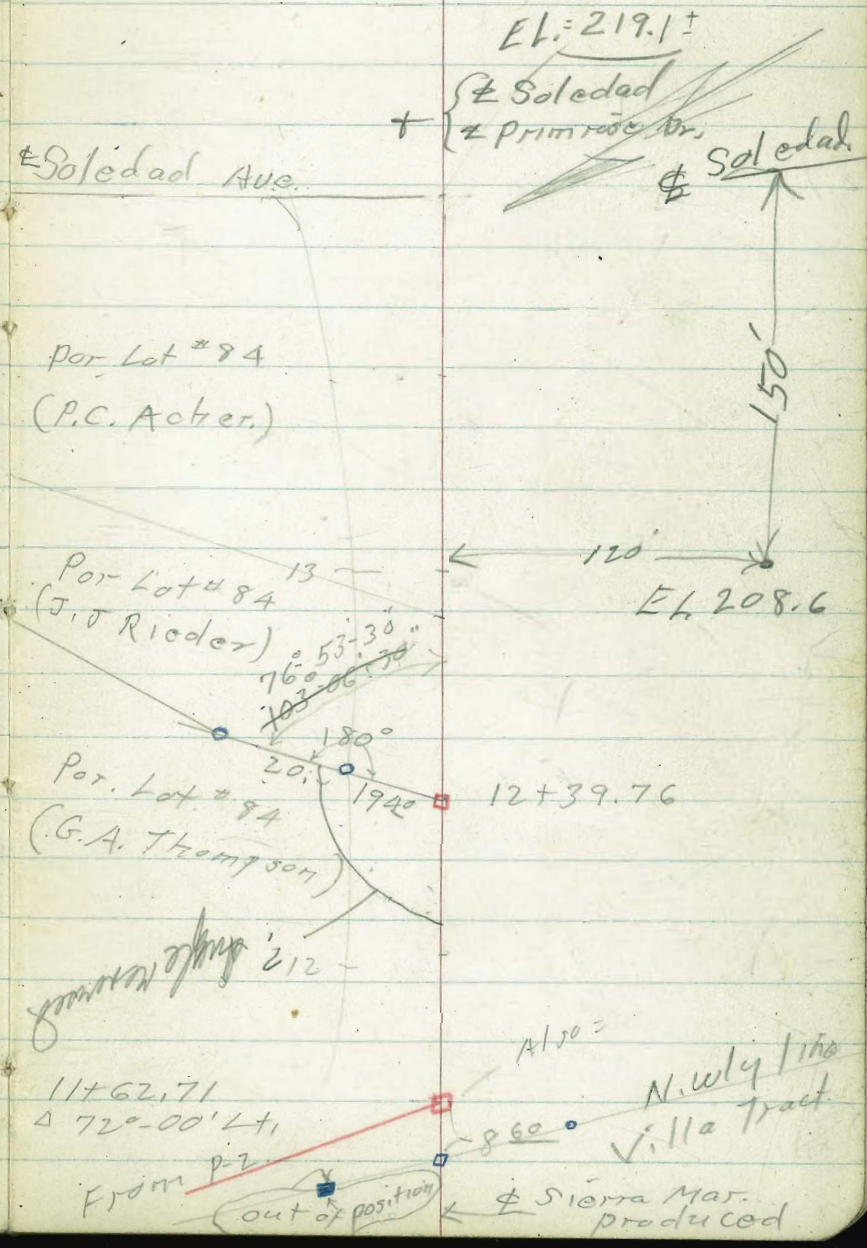
2°-59'

9+39.26 $\Delta 27^\circ - 15' - 09''$
 FB 2028 - P. 27
 Now P.O.T.

7.95
 $\Delta 51^\circ - 07'$

8+56.35
 FB 2027
 p. 28

2
 2



Change Sierra Mar
line = B. Line 6/14/54

±

4
✓

Continued from FB 2028
P 32

9+60

171.2 ✓	170.4 ✓	169.8 ✓	164.1 ✓	163.7 ✓
6.2	7.0	7.6	13.3	13.7
10		1	7	10

start improved grounds.

9+54 7 Lt. = 2" diam apricot tree

5' North = Nearest point of wall
3' Lt. = small palm.

9+53¹⁵ } - Δ 81° 36' 30" RR.

171.2 ✓
6.2

9+46 4⁵ Lt. = start rock wall

174.8 ✓	170.8 ✓	170.8 ✓	168.1 ✓
2.6	6.6	6.6	9.3
45	45	4	
T.W.	B.W.		

9+39²⁶ old A, Now = P.O.T.

165.0 ✓
12.4

T.P.

1.71 <177.41> ✓ 11.60 <175.70> ✓

177.41 ✓
7/24/54

FL 18203

5.32 182.04 ✓
.01 ✓

check stub 11+15⁴³ FB 2028 - P 35

B.N. 71

3.72 <187.36> ✓ - <183.64> ✓

Stub 12+46⁸⁰ FB 2028 - P 36

10+25

169.5	167.9	167.8	166.5	166.3
7.9	9.5	9.6	10.9	11.1
10		6	8	10

T.P.

8.88

177.41

8.88

168.53

177.41

7' Rt. = start rock wall
can come out.

10+00

5' Rt. = 6" diam tree

stumps 8" to 14" - 5'± apart.

3' Lt. = start row of short

168.9	168.2	168.0	167.2	163.5	163.4
8.5	9.2	9.4	10.2	13.9	14.0
10		3	7	9	15

9+98 - 2' Lt. = 7' high avocado

9+90 = end same.

8" to 12" - 1' high stumps

9+84 - 3' Rt. = start row of 4

9+83 6' Lt. = 3" avocado tree

169.4	168.7	164.3	164.0
8.0	8.7	13.1	13.4
10		8	12

9+80

9+79 - 5' Rt. = 6" diam. tree

9+67 { 4' Lt. = 3" diam. Avocado
(old 2' stump on line.)

177.41

10+95 5' Rx: 24" eucalyptus

10+85

170.0	172.0	171.0	172.4	173.0
10.0	8.2	9.2	7.8	7.2
10	4		4	10

T.P. 8.90 <180.22> 6.09 <171.32>

10+77 32' Lt. = door to house

added. 9-20-54 CH.S.

169.9
8.0
32"
Floor

169.9	171.3	172.4
7.5	6.1	5.0
10		10

10+72

170.3	170.2	169.1	170.8
7.1	7.2	8.3	6.6
10	5		5

flows to right (N. side)
conc. throat to 18" culvert.

10+59

5' Rx = ctr. 2'x3' grate +

169.7	169.3	170.2	170.6
7.7	8.1	7.2	6.8
10		5	10
		J.E Box	

10+53

5' Rx = end row of stump

169.8	168.9	168.3	167.5	167.1
7.6	8.5	9.1	9.9	10.3
10		5	7	10

10+50

177.41

11+48 - 7' RT. = 24" eucalyptus.

11+43 = cross ϕ of 2' wide steps.

RT. = start Conc. wall.

11+27 - 6' ³ 1/2 ϕ - start 2' wide Conc. steps.

184.1 ✓	185.4 ✓	186.3 ✓
7.0	5.7	4.8
10		8
		at wall

178.8 ✓	179.3 ✓	180.5 ✓	181.5 ✓	180.4 ✓	188.7 ✓
12.3	11.8	10.6	9.6	10.7	2.4
10	6.5			7.2	7.2
	steps			B.W.	T.W.

11+20

179.0 ✓
12.1

11+19

178.0 ✓
13.1

T.R. 13.03 $\langle 191.15 \rangle$ 2.10 $\langle 178.12 \rangle$

$\langle 191.15 \rangle$

11+09.68 1/2 P.O.T 3.19 177.03

11+04

174.1 ✓	172.5 ✓	176.5 ✓	176.8 ✓	176.5 ✓
6.1	7.7	3.7	3.4	3.7
15	10	4		10
	wash			

$\langle 180.22 \rangle$ ✓

B. Line - Sierra Mar

T.P. 12.73 \leftarrow 198.39 \rightarrow 5.49 \leftarrow 185.66 \rightarrow

12+40

12+15

12+00

$\frac{1}{2}$ 3.64

(also = 000 to N west. see P-2)

11+62 $\frac{1}{2}$ } $\frac{1}{2}$ disk = Δ 72° left.

11+51

4 N. = $\frac{1}{2}$ - end of steps

11+49

9' N. = end wall

8
✓
+9.3
200
+4.0
225

✓ 182.9	✓ 183.3	✓ 185.1	✓ 185.3	✓ 185.3	✓ 195.6	✓ 201.3
8.2	7.8	6.0	5.8	5.8	+4.5	+10.2
20	12	7		10	50	100

added 9-20-54

184.7
6.4

✓ 185.0	✓ 184.9	✓ 184.8	✓ 198.6	✓ 191.
6.1	6.2	6.3	+7.5	0.0
10		10	100	170

added
9-20-54

187.8
3.3

✓ 186.5	✓ 187.5	✓ 188.2	✓ 188.7
4.6	3.6	2.9	2.4
10		4 steps	10

✓ 188.5	✓ 187.7	✓ 193.3
4.6	3.9	+2.2
9	9	9
B.W.	T.W.	

191.15 ✓

4.

Dated

9

✓

12+50

193.9 [✓]	195.8 [✓]	196.6 [✓]	198.4 [✓]	197.7 [✓]	197.7 [✓]
4.5	2.6	1.8	0.0	0.7	0.7
50	3		3	10	20

↙ Far enough

13+00

189.9 [✓]	189.7 [✓]	191.3 [✓]	191.5 [✓]	190.9 [✓]
8.5	8.7	7.1	6.9	7.5
20	7	3		10

12+75

188.8 [✓]	188.3 [✓]	188.1 [✓]
9.6	10.1	10.3
10		10

<198.39>[✓]

Line N.W. along
E of Sierra Mar.

0+00 = 11+62.71 - Page 2

BM #1 Page A

6.62 $\left\langle \begin{matrix} 0.03 \\ 183.61 \end{matrix} \right\rangle$

183.54

T.P.

3.80 $\left\langle 190.23 \right\rangle$ 11.96 $\left\langle 186.43 \right\rangle$

0+50

189.1 ✓
8.7
10

190.2 ✓
8.2

190.0 ✓
8.4
10

0+30

189.3 ✓
9.1
10

189.6 ✓
8.8

189.4 ✓
9.0
10

0+09 = start 2" thick rock to 1'

188.0 ✓
10.4
10

188.4 ✓
10.0

188.3 ✓
10.1
5

188.5 ✓
9.9
10

0+08⁶⁰ = 1/2 P.O.T. 10.36 (188.03)
on disk

187.1 ✓
10.7

0+00 to NW in unnamed St Ph. 1285
from Primrose Drive.

11+62.71 2nd

T₂ from P. 9 $\left\langle 198.39 \right\rangle$

$\left\langle 198.39 \right\rangle$

La Jolla Hills

Sewer Prelim. - "H" Line

C.H.S.
Begg
Schelin
Pullen

7-6-54
W.D. #31841

From Torrey Road + Roseland Dr.
thru lots #19-#22 - to
Lookout Drive.

Set up on coordinate system
so as to calculate portions
of line that run thru dense
poison oak.

Field Books

1360

1673

1564

2016

2027

2028 - 125-27

2031

2056

2333

T.P. Book 17 - P39

G.B. 124

G.B. 290

RS# 585

615

677

867

868

871

712

MS 1143

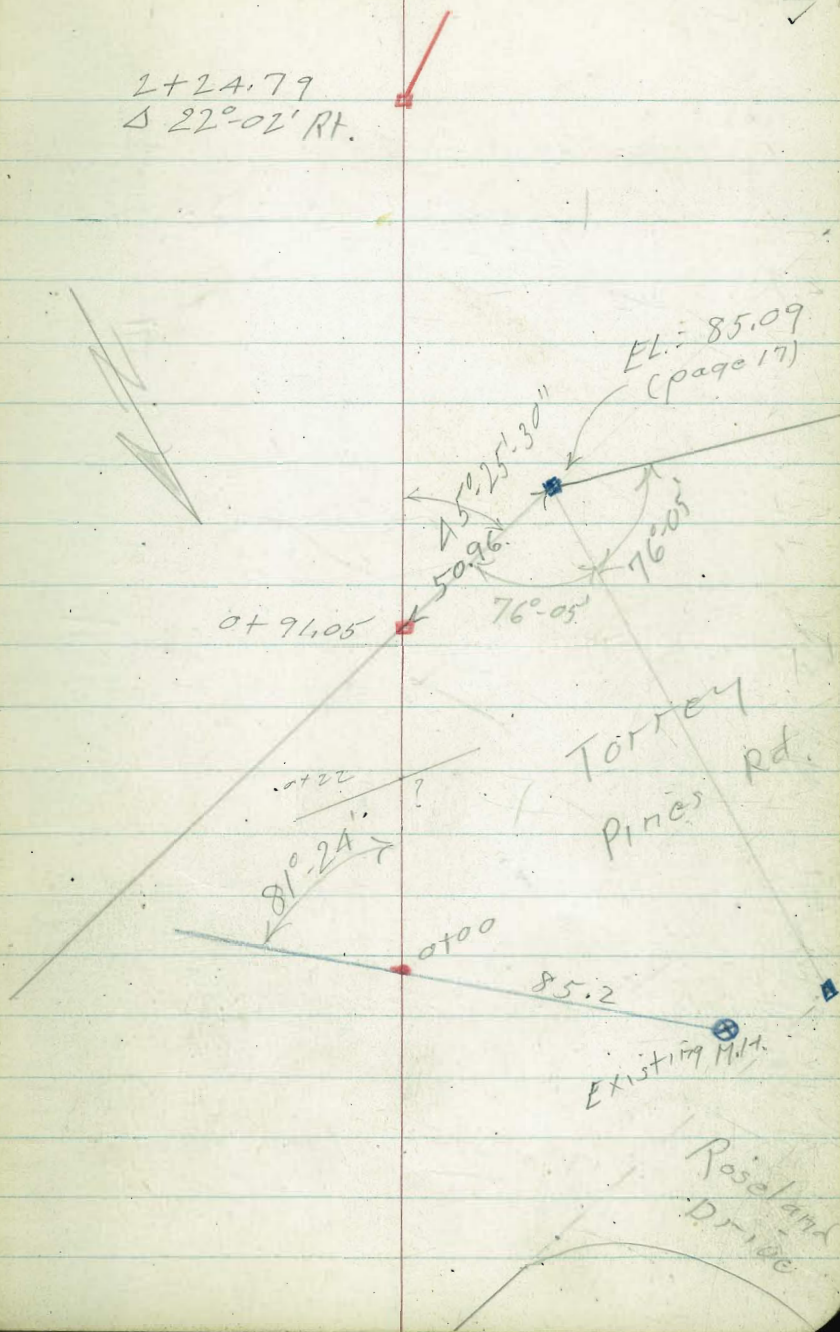
2+24.79 { 66.38 North
 94.62 East
 start of poison oak.

2+24.79
 $\Delta 22^{\circ}02' \text{ Rt.}$

{ 184.40 North
 157.53 East
 0+91.05 = S. Ely line Torrey Rd.

check for under ground
 0+22 cross patch in cold lay
 sewer.

0+00 = ϕ Trench for existing
 { 264.75 North
 200.36 East



Cont. on P. 16

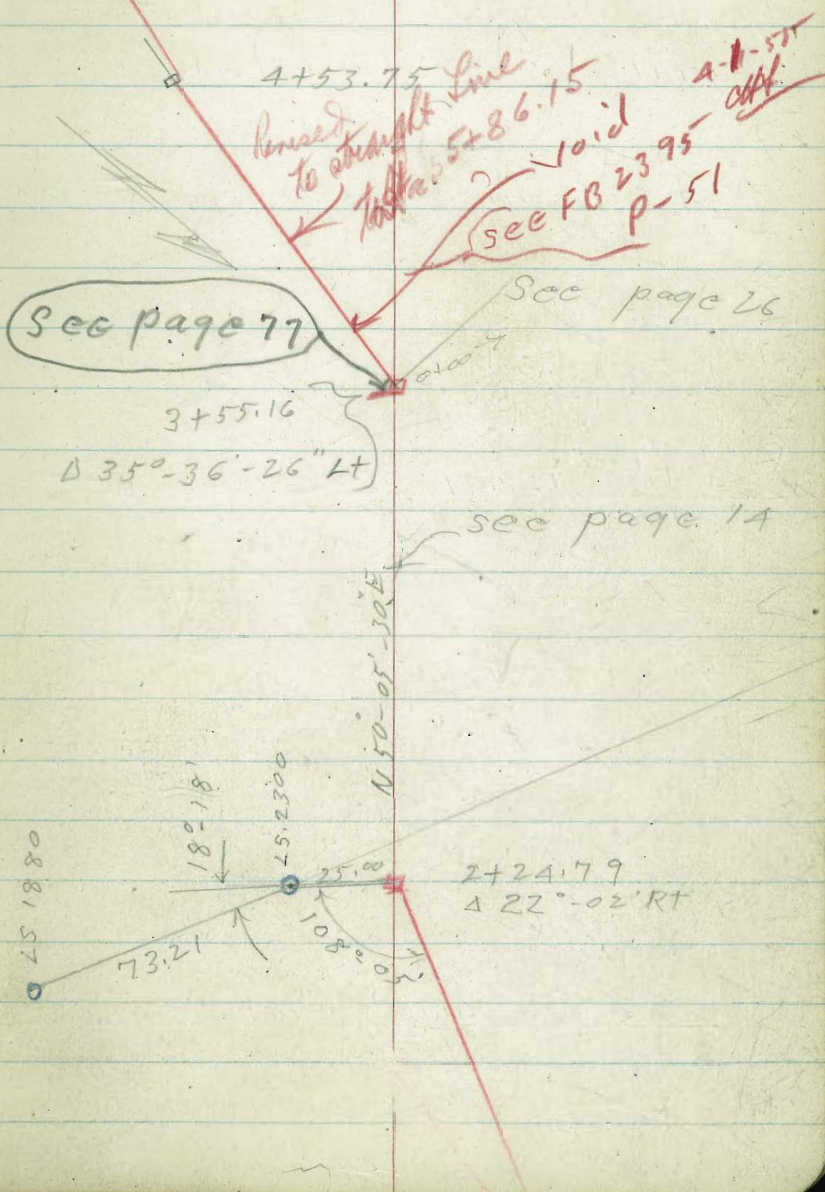
No hub set,

4+53.75 = Δ 2°-14'-56" RL (Calc.)
112.72 South
30.04 West

This point set. Poison oak ^{here} not dense

3+55.16 = Δ 35°-36'-26" Lt.
17.26 South
5.38 West

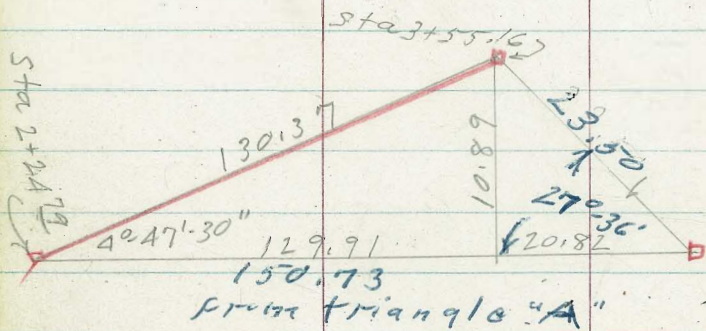
2+24.79 = Δ 22°-02" RL



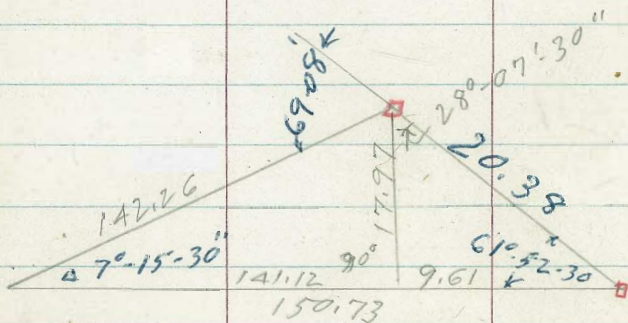
Detail of triangulation

Inked figures chained or
Pencil " Calculated.

"A" - from opposite page →



"A" opposite page

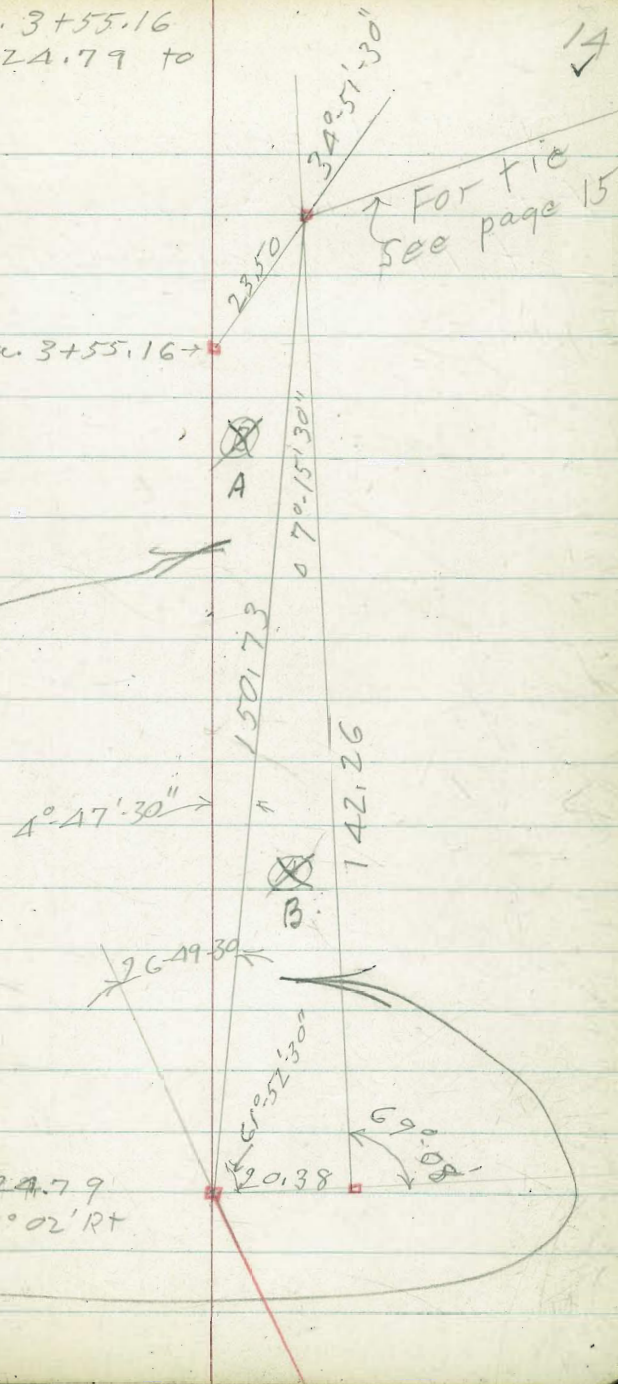


Triangle "B"

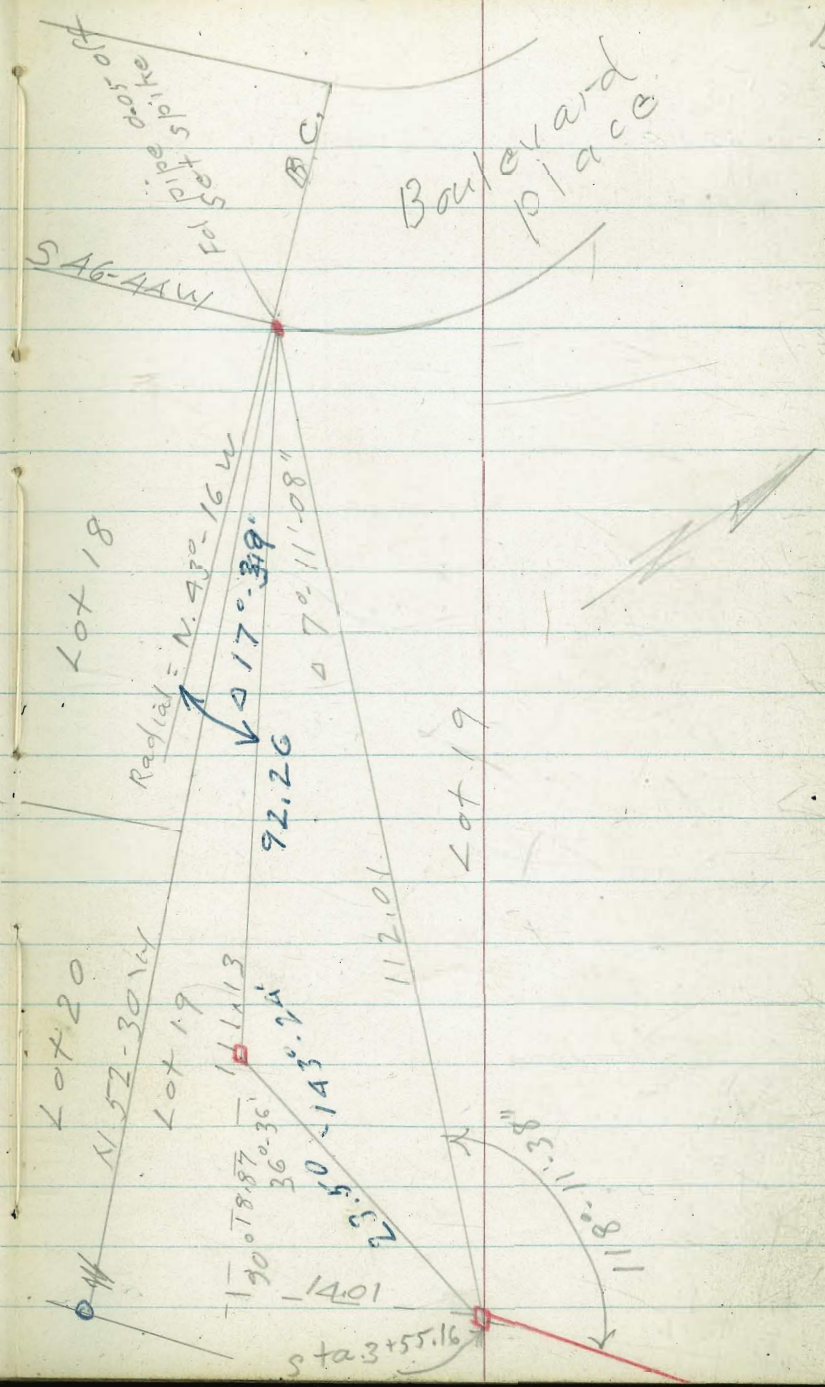
Sta. 3+55.16
Sta. 2+24.79 to

14 ✓

Sta. 3+55.16 →



Detail of triangulation
Par. tie to ~~N~~ S Wly Cor.
Lot 19 - La Jolla Hills

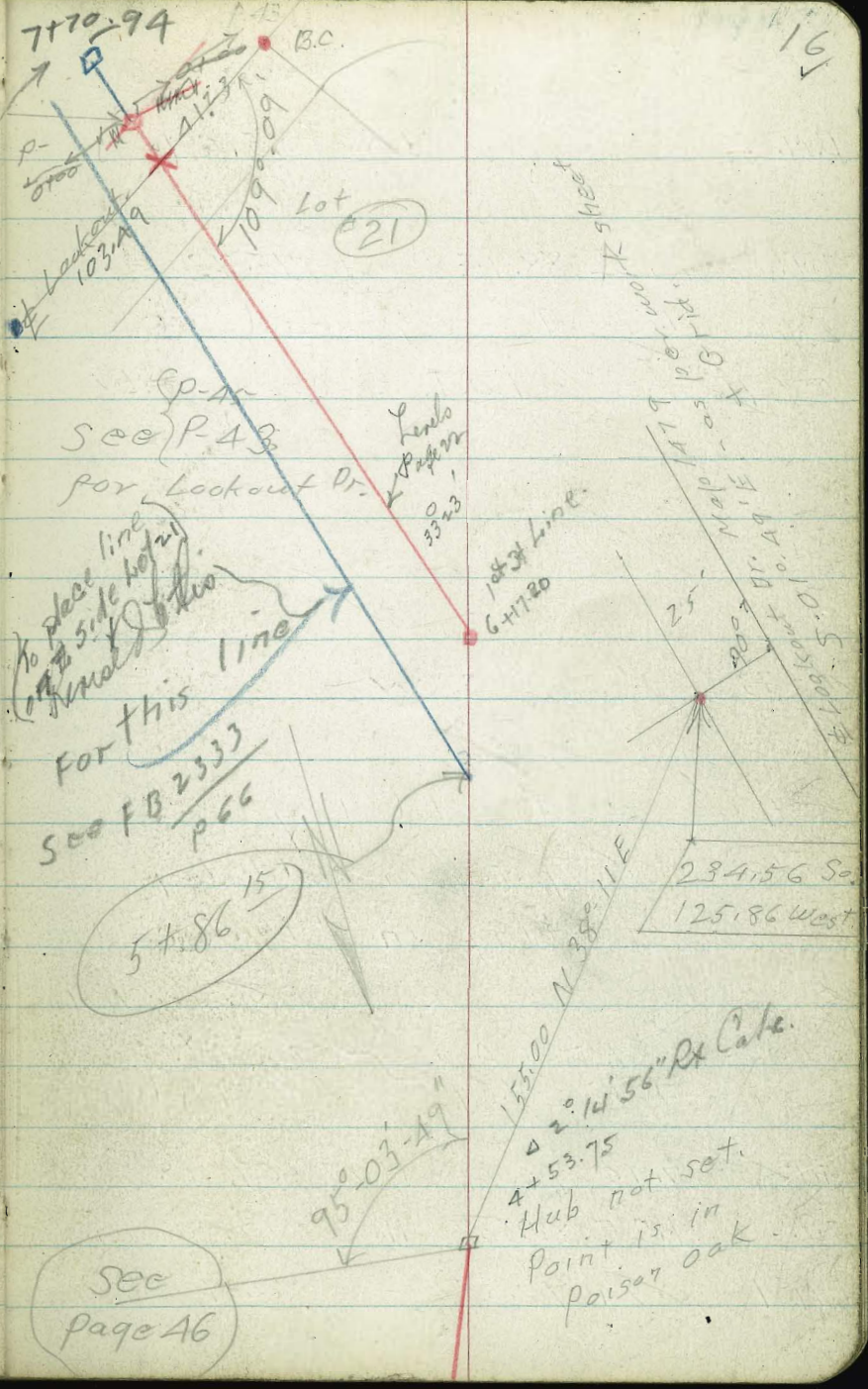


$\left\{ \begin{array}{l} 414.51 \text{ South} + 33.56 \text{ west.} \\ \text{End of line} \end{array} \right.$ changed
 $7+68.82 = \cancel{70^\circ 51' 19"}$ 8/14/84
 $7+55.06 = \text{cross \& Lookout.}$
 $\left\{ \begin{array}{l} 401.33 \text{ south} \\ 37.50 \text{ West} \end{array} \right.$

B.M. 47 elevation Rod.
 El. of γ = 153.67 set by direct
 Sta. $6+170 \frac{1}{2} = \Delta 33^\circ - 23' \text{ Lt.}$
 $\left\{ \begin{array}{l} 269.07 \text{ S} \\ 77.05 \text{ W} \end{array} \right.$

5+70 $\frac{1}{2}$ end of Poison oak

4+53.75 from page 13



B.M.#2

3.86 85.09

T.P. 13.22 88.95 1.21 75.73

line Torrey road

0+91 ^{0.5} = 1/4 P.O.T. = cross S.Ely.

0+50

0+33 - 1' Lt. = 3 (W)

0+30 = end cold lay

0+22 = cross patch in cold lay

starting in 1" thick cold lay

0+01 set Point 10' S.E. Existing M.H.

0+00 - 85' Rt at Δ of 98° 36' Rt =
45' Rt = N.Ely. edge Torrey Rd paco.

T.P. 7.46 <76.94> 11.07 <69.48>

T.P. 1.25 <80.55> 11.55 <79.30>

B.M.#1 0.74 <90.85> - 90.11

Charged 10' at 0+01 to clear Gas + water Main S. See Dwg 3031-D

50.96 - S. wly from P.O.T. Sta. 91105
Mon. Δ in S.Ely. line Torrey road

15.9
1.0
5

75.73
1.21
5

15.9
1.0
5

13.5
3.4
5

13.1
3.2
5

13.9
3.0
5

12.5
4.4
5

12.2
4.5
5

12.2
4.7
5

10.8 10.91 11.0 64.25 54.80
6.1 6.03 5.9 12.69 22.14
5 3.4 4.5 8.5 8.5
↑
at 98° Rim I.E.

<76.94> at 98° 36' Rt.

N.W. B.P. Torrey Road + Little St.

4

17

11.03 $\left\langle \begin{array}{c} \uparrow \\ 99.47 \\ \downarrow \end{array} \right\rangle$ #

1+75-43
TP Stub 009

-1.72

$\left\langle 88.44 \right\rangle$

18

1+75

84.1 ✓
6.1
15
W

87.2 ✓
3.0
5

88.1 ✓
13

89.7 ✓
0.5

1+50

81.0 ✓
9.2
11 W

83.1 ✓
7.1
7

85.1 ✓
5.1

85.9 ✓
4.3
5

1+28

78.0 ✓
12.2
5
W

80.1 ✓
10.1

81.1 ✓
9.1
5

1+22

77.6 ✓
12.6
W

1+15

78.4 ✓
11.8
5

78.3 ✓
10.9

77.3 ✓
12.9
5. W

507 $\left\langle \begin{array}{c} 90.16 \\ \downarrow \\ \uparrow \end{array} \right\rangle$

BM #2

85.09

$\left\langle 90.16 \right\rangle$ ✓

+ #1 - EL

T.P. 0.92 (144.33) 1257 (131.76) ✓
 T.P. 1.38 (156.45) 1304 (143.41) ✓
 B.M. #5 2.66 (156.45) 1.38 (155.09) ✓
 T.P. 13.17 (154.60) 0.81 (153.79) ✓
 B.M. #4 P.O.T. on Boulevard 9.94 (141.69) 0.22 (141.47) ✓
 13.34 (131.91) 0.16 (131.75) ✓
 11.92 (119.28) 0.71 (118.57) ✓
 T.P. 1.55 (107.36) ✓

on City disc. & Lookout Dr. S.E. 4.
 Radial to Prop Lookout & Boulevard
 of S.W. cor. Lot #19
 1/2 P.O.T. Ely Boulevard place + 10' south

3+55.16 }
 B.M. #3 } + 0100 ft.
 Δ } = 2+0.14
 35° 36' 26" Δ 13.14 (108.91) ✓
 T.P. rock - 370 (95.77) ✓

6.35 102.56

Levels for profile Cont. on P-20

R. + 2479 Δ

88.5	91.2	92.37	95.0
11.0	8.3	7.10	4.5
6	3		5
w			

Z. + 00

86.3	88.0	89.0	90.8	92.0
13.2	11.5	10.5	8.7	7.5
18	13	5		5
w				

(99.47) ✓

(99.47) ✓

	+ HI	- EI
3+45		
BM #3	1004	102.56
23+55	112.60	102.56

106.9	106.5	101.5	105.1
5.7	6.1	11.1	7.5
5		11	18

112.60

3+00

Levels from
 start thru sta. 3+45
 are shown as near
 correct as I could estimate
 thru. Poison oak.
 ("I aint about
 to get into it.")
 G.M.

2+40

99.47

Levels for profile Coat. from p. 19

91.5	90.47	92.5
8.0	9.0	7.0
5		5

99.47 from page 19

BM #1	1.46	96.69	661	(90.11) - B.M. #1
T.P.	0.21	107.54	12.31	90.08
T.P.	0.15	120.49	13.16	95.23
T.P.	1.92	133.68	13.34	107.33
				120.34
				131.76

90.11 ft of beginning

sat
B.M.#6

4.85 $\langle 181.36 \rangle$

B.M.#6 = cross & Lookout 7+55⁰⁶ Page 16

T.P. 8.38 $\langle 186.21 \rangle$ 0.36 $\langle 177.83 \rangle$

T.P. 10.30 $\langle 178.19 \rangle$ 10.30 $\langle 167.89 \rangle$

T.P. 13.18 $\langle 178.19 \rangle$ 1.45 $\langle 165.01 \rangle$

B.M.#5 11.39 $\langle 166.46 \rangle$ — $\langle 155.07 \rangle$

from page 19

cont page 22

3+70

\checkmark 110.5	\checkmark 110.0	\checkmark 103.0	\checkmark 109.6	\checkmark 109.8
2.1	2.6	9.6	3.0	3.8
17	12	5		5
		W		

A
3+~~45~~ 16
= 0+00 to RA

\checkmark 107.0	\checkmark 102.6	\checkmark 106.9	\checkmark 102.1
5.6	10.0	5.7	10.5
7	W	7	16
			W to Right

3+50 7' RA = Junction of \checkmark washes
 $\langle 112.60 \rangle$

\checkmark 106.9	\checkmark 104.6	\checkmark 102.9
5.7	28.0	10.6
5	$\langle 112.69 \rangle$	7
		W

T.P. 12.29 $\langle 170.00 \rangle$ 5.05 $\langle 157.71 \rangle$

6+20

6+17²⁰ A 33°-23' Lt. Lt. (P.16)

6+00

5+80 thru this area.
seem to run fairly constant.
Poison oak. Graded waste
Sta. A+60 to 5+80 is thick with
9.09 $\langle 162.76 \rangle$ - 153.67

Note elevations. These are actual
A+53.75 \rightarrow $\Delta 2^\circ-14'-56''$ Rt.

154.6 152.76 155.3
8.2 10.0 7.5
5 w 5

152.0 149.1 152.8 153.69 155.1
10.8 13.7 10.0 9.1 7.7
10 6 3 5
w

151.1 147.8 152.5 154.2
11.7 15.0 10.3 8.6
10 5 5
w

151.6 149.0 145.3 149.2 151.0
11.2 13.8 17.5 13.6 11.8
10 5 w 5 10

$\langle 162.76 \rangle$

B.M. #7-page 16 - (6+10.25)

131.0 128.0 131.0
5 w 5

T.P. 9.53 $\langle 186.83 \rangle$ 0.66 $\langle 177.30 \rangle$

7+26

7+00

T.P. 9.40 $\langle 177.96 \rangle$ 1.44 $\langle 168.56 \rangle$

6+98 = end of small wash

6+90 2' Rt. = Main wash
2' Rt. = small wash

or cess pool.
probably from septic tank

6+76 out = outlet 4" drain.
(drains from east)

6+35 12' H. = lime tree,
save this tree,

174.1 ✓
3.7 ✓
5 ✓
174.3 ✓
3.7 ✓
5 ✓
175.0 ✓

166.6 ✓
11.4 ✓
5 ✓
166.3 ✓
11.7 ✓
5 ✓
166.3 ✓
11.7 ✓
5 ✓

$\langle 177.96 \rangle$

165.9 ✓
4.1 ✓
5 ✓
165.8 ✓
4.2 ✓
w ✓
165.8 ✓
4.2 ✓
5 ✓

164.8 ✓
5.2 ✓
5 ✓
163.6 ✓
6.4 ✓
162.0 ✓
8.0 ✓
2 ✓
w ✓
164.7 ✓
5.3 ✓
5 ✓
158.8 ✓
11.2 ✓
22 ✓
w ✓

162.95 ✓
7.05 ✓
14. ✓

159.0 ✓
10.8 ✓
5 ✓
156.0 ✓
14.0 ✓
154.6 ✓
15.4 ✓
3 ✓
w ✓
158.4 ✓
11.6 ✓
5 ✓

$\langle 170.00 \rangle$

Junction of
2 washes

on Lookout drive
also = 0+00 both ways

7+68^{.82} = end of line

182.05 ✓
4.78
1/2

Edge of pavc.
on Δ 70°-51' RT along

7+65⁷ = end Conc. pavc.

181.74 ✓
5.09
5
181.66 ✓
5.17
5
181.53 ✓
5.30
5

check B.M.

7+55.06 = Δ Look out = X on pavc.

181.49 ✓
5.34
5
181.36 ✓
5.47
5
181.27 ✓
5.56
5

Along Pavement Δ 70°-51' RT,

7+44^E = start Conc. Pavc.

181.24 ✓
5.59
5
181.11 ✓
5.72
5
181.01 ✓
5.82
5

7+44

181.4 ✓
5.4
5
181.4 ✓
5.4
5
181.4 ✓
5.4
5

7+36

181.4 ✓
5.4
5
181.4 ✓
5.4
5
181.4 ✓
5.4
5

186.83

186.83 ✓

B.M. check

25

7+70.9A - on hub end of line

182.39 ✓
5.26

187.65 ✓

6.29 187.65 - 181.36

B.M.#6 - P-21

7+70.94 = end of new line

Move ahead to

7+68.82 end of old line (P16)

From p-16

6.44 155.08 ✓

155.07 = B.M.#5 - Page 19.

T.P. 2.22 161.52 ✓ 11.70 159.30 ✓

T.P. 0.46 171.00 ✓ 13.18 170.54 ✓

T.P. 2.36 183.72 ✓ 5.47 181.36 ✓

B.M.#6 - P-21

186.83 ✓

From page 24

T.P. 13.18 178.19 1.45 165.01

~~11.39 166.46 - 155.07~~

~~B.M.#5 P 19~~

Boulevard Place line

2+40

= Δ 60° 42' Lt.
1+45.23 = $\frac{1}{2}$ Boulevard Place

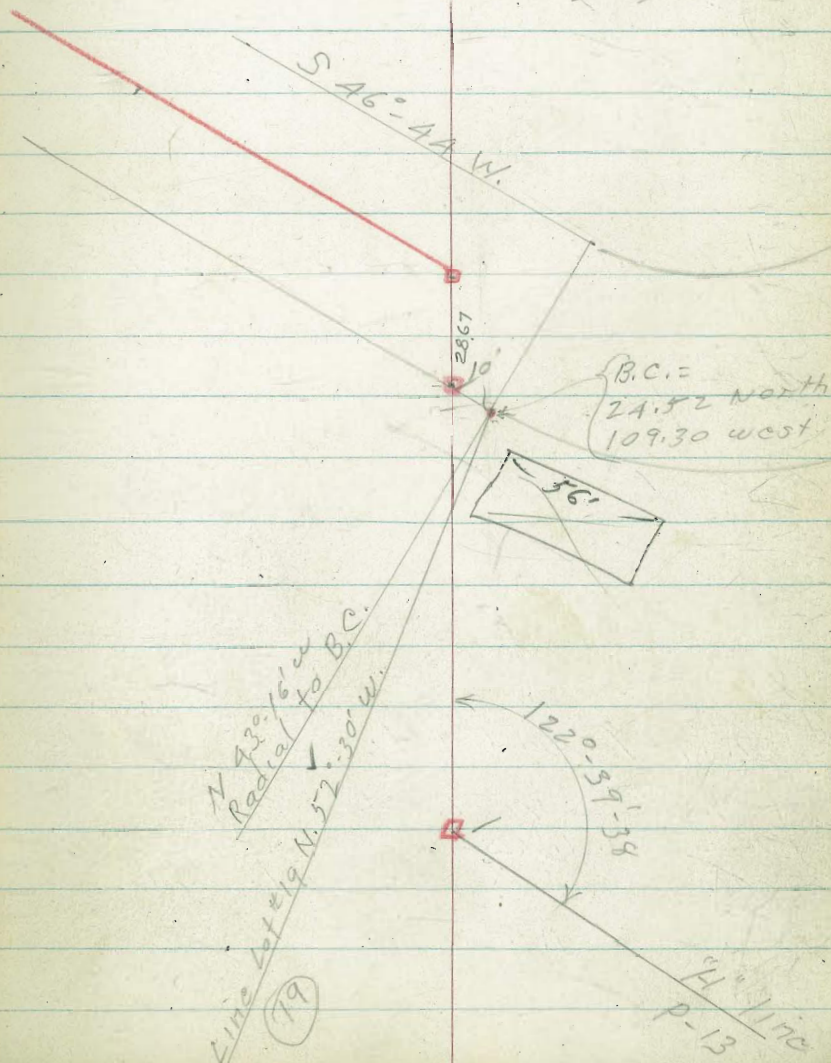
28.67

1+16.56 = $\frac{1}{2}$ P.O.T. on S.E. line Boulevard Place

= 0+00

3+55.16 Page 13 =

{ 17.26 South
5.38 West





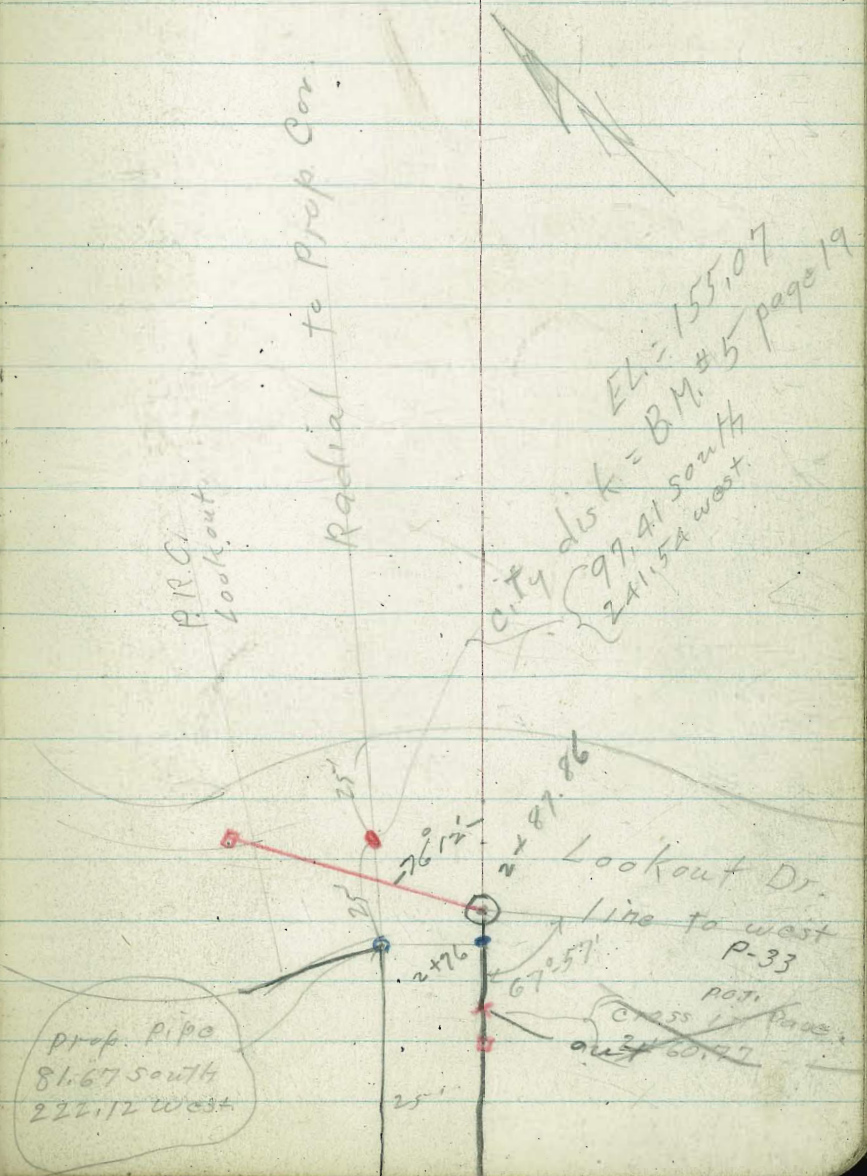
See F.B. 2333 page 45

9-10-54 - Change from 2+76⁰⁰ on
To miss inlet Box

57
86
267.3
20.56

287.86

3+57.47 = 1/2 end of Line
 2+87.86 = Δ 76° 12' Lt. = Nail
 2+76.00 = Fd. disk 18236-90° to S.E. cor.
 Lookout + Boulevard
2+67.3 = Culvert - See F.B. 2333-p 68
 2+57.86 = 1/2 P.O.T.
 a/24/55



Boulevard Pl. Wine
to
Weekout Dr.

±

28

0+48

115.7 ✓	107.4 ✓	114.4 ✓	114.7 ✓
5.0	13.5	6.3	6.0
17	9		5
	W		

TIP

9.83

⟨120.69⟩ ✓

1.97

⟨110.86⟩ ✓

⟨120.69⟩ ✓

0+37

cross wash

114.4 ✓	112.8 ✓	104.8 ✓	112.8 ✓	112.8 ✓
+ 1.6	0.0	8.0	0.0	0.0
75	6	W	12	15

0+28

110.0 ✓	109.3 ✓	102.7 ✓	109.5 ✓	109.3 ✓
2.8	3.5	10.1	3.5	3.5
5		8	18	20
		W		

0+06

108.1 ✓	107.1 ✓	106.9 ✓	101.7 ✓	105.8 ✓
4.7	5.7	5.9	11.1	7.0
5		4	10	15
			W	

0+00 = 3+55¹⁶ Page 13

~~4.7~~
102.56 ✓
10.27
W to left.
⟨112.83⟩ ✓

B.M. #3 101.27 ⟨112.83⟩ - ⟨102.56⟩ Pg 19

B.M. #3 - Page (19-3+55.16) = 0+00 this line

T.P. 8.78 $\left\langle \frac{50.26}{0.09} \right\rangle \left\langle \frac{1411.48}{1+16.64} \right\rangle$

1+06- 12³ RT = end House

0+90

T.P. 11.20 $\left\langle \frac{141.57}{0.74} \right\rangle \left\langle \frac{130.37}{1} \right\rangle$

0+77 - 5^c RT. start House

0+72 10' Lt. = 12" Diam Live oak.

T.P. 10.75 $\left\langle \frac{131.11}{0.33} \right\rangle \left\langle \frac{120.36}{1} \right\rangle$

0+57

136.5 ✓
5.1
5

135.3 ✓
6.3
5

135.0 ✓
6.6
5

134.9 ✓
6.7
12.3
at House

128.4 ✓
26.0
48
W

130.9 ✓
10.7
15

129.6 ✓
12.0
5

128.6 ✓
13.0

128.5 ✓
13.3
5

$\left\langle \frac{141.57}{1} \right\rangle$

128.6
7.5
5^c End at house

121.6 ✓
9.5
5

121.3 ✓
9.8

121.6 ✓
9.5
5

$\left\langle \frac{131.11}{1} \right\rangle$

119.7 ✓
1.0
2.0

110.3 ✓
10.4
13
W

116.7 ✓
9.0
6

116.4 ✓
4.3

116.0 ✓
4.7
5

120.69 ✓

1+50

141.8 ✓ 142.3 ✓
8.5 8.0
6:00 of bank

= \perp Boulevard Place

1+45²³ = $\Delta 60^\circ - 42' \text{ Lt.} = \frac{1}{2}$

140.9 ✓
9.40
Hub.

1+27

141.1 ✓
9.2

1+22 start traveled road

140.9 ✓ 140.3 ✓ 139.7 ✓
9.4 10.0 10.6
5 5

1+21

142.8 ✓ 142.3 ✓ 140.0 ✓ 139.1 ✓
7.5 8.0 10.3 11.2
5 5 10

1+16.56 = cross S.Ely. line Boulevard

142.5 ✓ 141.5 ✓ 139.9 ✓
7.8 8.8 10.4
5 5

150.26 ✓

60.4
57.9
2.5

90° to Fund Targ.

2+87.86 = Δ 76°-12' Lt. = Nail

Note for change see FB 2332
9-10-54

47.45

2+76.00 = 25' Lt. = Prop. disk
at 90° cov

sec. along edge of Pavc

2+60.4 = start Conc. Pavc.

cannot locate out lot.
crossing of 18" culvert.

2+57.86 = 1/2 P.O.T. = approximate
(Δ 67°-22' Rt to line of pipe)
54' Rt = curb in lot

2+20

TR. 11.75 <160.77> 112.4 <149.02>

2+00

<150.26>

4

31

154.04
6.73
5

154.04
6.68
5

154.07
6.70
5

153.79
6.98

153.21
7.56
5

153.12
7.65
5

153.04
7.73
5

152.84
7.95

151.47
9.30

147.27
13.50

54
9 rate
54
IE. Box

151.6
9.2

151.5
9.3

6
Toe of bank

<160.77>

147.8
2.5

147.8
2.5

7
Toe of bank

<150.26>

5.69 $\langle 155.08 \rangle$

(155107)
B.M. #5 - Page 19

stated
n

32

3+57A = $\frac{1}{2}$ = end of line

158.63[✓]
2.14
Hub

sec. along edge of pavc.
3+57A = end conc. Pavc.

158.64 [✓]	158.45 [✓]	158.14 [✓]
2.08	2.32	2.63
5		5

3+40

156.90 [✓]	156.8 [✓]	156.77 [✓]
3.87	3.95	4.00
5		5

3+15

154.77 [✓]	154.97 [✓]	155.10 [✓]
6.00	5.80	5.67
5		5

box to curb inlet
3+08 9⁵ LK = 4 near edge of

154.17 [✓]	154.67 [✓]
6.60	6.10
95	

3+00 = cross water line.

154.19 [✓]	154.24 [✓]	154.41 [✓]
6.58	6.53	6.36
5		5

$\langle 160.77 \rangle$

Lookout Drive Line

From Boulevard Place

Nly - wly - & S. Ely to

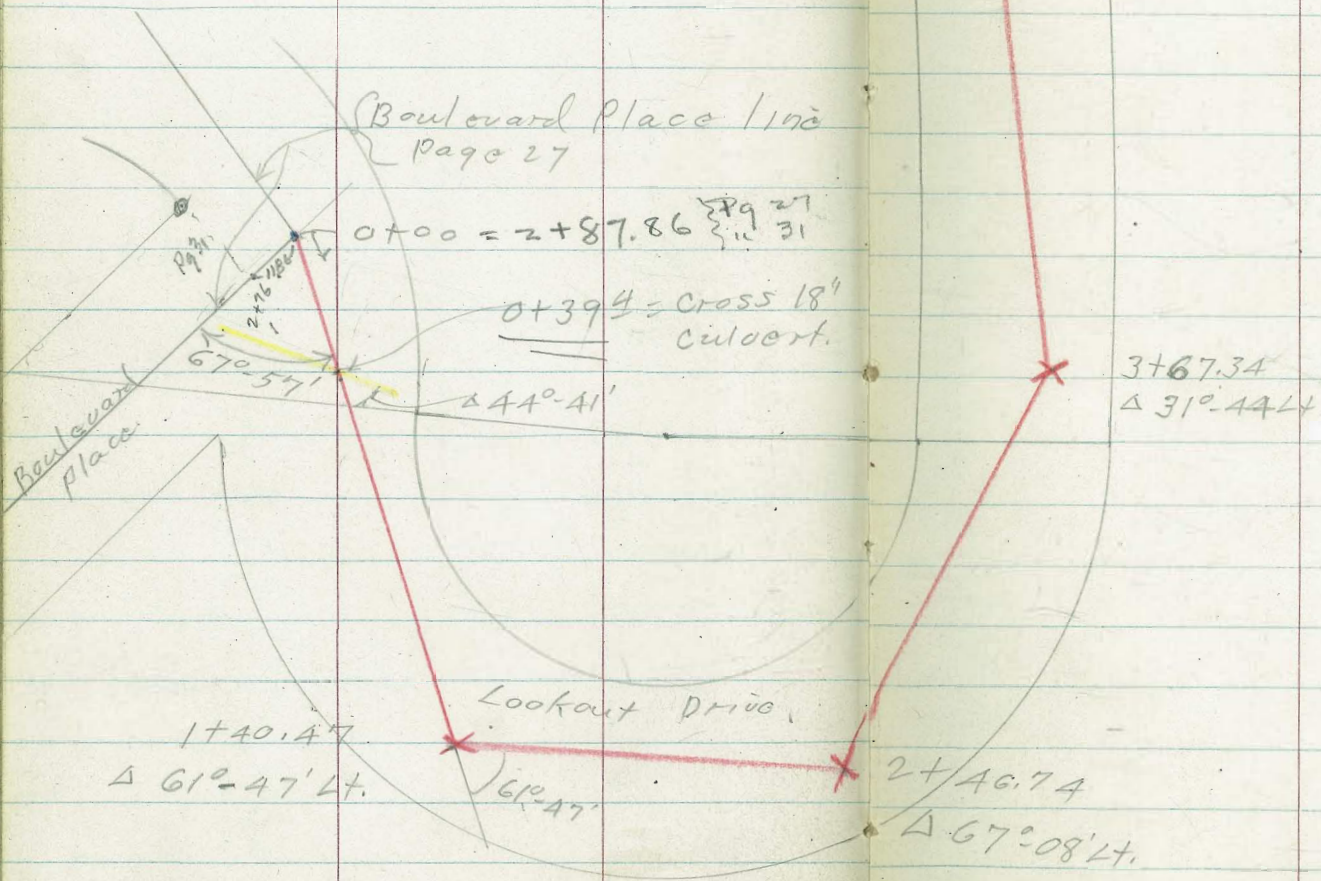
Soledad Road.

X denotes cut cross in conc.

• = Fd. disk LS2236

not used 39 ✓

0.5750



32.66
267.79
300.45

6+67.79
 $\Delta 16^{\circ}30'44''$

Lookout Drive

5+50

32.21
232.57
265.78

9+38.00

Soledad 326.11

9+33.57
= P.I.
Disk

Lookout Dr.

25 + 25

Hillside Dr. 25

30' 30"

35
not used

+ HI - EI.

not need - 36 ✓

1+00

152.27 ✓ 6.29 30 EP	152.37 ✓ 6.19 30 EP	153.34 ✓ 5.22 30 EP	6/10/54
------------------------------	------------------------------	------------------------------	---------

0+85

152.01 ✓ 6.49 30 EP	152.11 ✓ 6.39 30 EP	153.21 ✓ 5.35 22.0 EP
------------------------------	------------------------------	--------------------------------

0+60

151.14 ✓ 7.12 60 EP	152.01 ✓ 6.56 60 EP	153.02 ✓ 5.53 31 EP
------------------------------	------------------------------	------------------------------

0+48

151.47 ✓
7.09 grade
12.3 ft on line
of culvert

147.27 ✓
11.29
invert

0+39⁴ crosses Culvert 18" at 44'41'

12.3

152.15 ✓ 6.41 12 EP	152.73 ✓ 5.83 12 EP	153.03 ✓ 5.53 12 EP	152.83 ✓ 5.73 19 EP
------------------------------	------------------------------	------------------------------	------------------------------

Edge Paving

= 0+00

154.12 ✓
4.44

2+87.86 Page 27 =

349 (158.56)

155.07

(158.56) ✓

BM#5-P-19

+ H1

- Elev

not used 37 ✓

2+30 Floor Elev 7764 look Out

144.10 ✓
15.38 Old entry
48.0 permit
Floor Elev

2+20

153.6 ✓
5.76
5.0
EP

153.71 ✓
5.61

154.44 ✓
4.94
15.0
EP

159.38

505 (159.38) 423 (154.33)

2+00

153.31 ✓
5.25
1.0
EP

153.33 ✓
5.23

154.23 ✓
4.33
19.0
EP
42
Floor El
788 look

1+70

152.95 ✓
5.61
4.0
EP

153.10 ✓
5.46

153.92 ✓
4.62
17
EP

1+40 47 A 4
61° 47 Lt.

152.71 ✓
5.85
16.0
EP

153.49 ✓
5.07

153.70 ✓
4.86
4.0
EP

1+07

152.48 ✓
6.08
1.0
EP

152.52 ✓
6.04

153.36 ✓
5.20
19
EP

(158.56)

(158.56)

3+67.34 L
Lt 31° 44'

3+45

3+00

132.9 $\left\langle \begin{array}{l} 172.52 \\ \text{wall} \end{array} \right\rangle$ 0.15 $\left\langle \begin{array}{l} 159.23 \\ \text{wall} \end{array} \right\rangle$

3+70

3+60 House corner

3+46.74 Lt 67° 08'

$\left\langle \begin{array}{l} 159.38 \\ \text{wall} \end{array} \right\rangle$

Not read 38

166.67 ✓
5.85
17 EP

167.06 ✓
5.46
3.0
EP

167.15 ✓
5.37
EP

164.46 ✓
8.06
9.0
EP

164.51 ✓
8.01
12
EP

164.57 ✓
7.95
EP

159.5 ✓
13.0
4.0
wall

159.18 ✓
13.34
EP

160.16 ✓
12.36
20
EP

$\left\langle \begin{array}{l} 172.52 \\ \text{wall} \end{array} \right\rangle$

155.69 ✓
3.79
6.0
EP

155.93 ✓
3.45
15.0
EP

156.96 ✓
2.42
EP

151.09 ✓
8.29
58.0
floor Elev #7764

154.33 ✓
5.05
17.0
EP

154.99 ✓
4.39

155.13 ✓
4.25
4.0
EP

$\left\langle \begin{array}{l} 159.38 \\ \text{wall} \end{array} \right\rangle$

not used 39

6 + 00

178.47[✓]

4.75

7
EP

176.49[✓]

4.73

178.51[✓]

4.65

12
EP

5 + 50

176.41[✓]

6.81

5
EP

176.43[✓]

6.79

176.66[✓]

6.56

15
EP

5 + 00

176.4[✓]

6.8

3.6

174.39[✓]

8.83

5
EP

174.44[✓]

8.78

174.69[✓]

8.53

15 EP

4 + 60

173.25[✓]

9.97

7
EP

172.89[✓]

10.33

173.25[✓]

9.97

7
EP

11.54 183.22 0.84 171.68

183.22

4 + 30

171.1[✓]

0.8

50
garage floor

171.59[✓]

0.93

9
EP

171.83[✓]

0.69

171.97[✓]

0.55

10
EP

4 + 00

172.52

168.1

4.4

46
Floor

169.74[✓]

3.78

12
EP

170.15[✓]

3.37

170.43[✓]

3.09

7
EP

172.52

7 + 00

186.66✓
7.24

183.00✓
10.90

max road 49
183.08✓
10.82

6 + 8.0

16
EP 181.45✓
12.45
18
EP

182.02✓
11.88

14 EP
182.08✓
11.82.
12
EP

6 + 67.79 ΔH 16° 30'

180.6
13.3
20
EP

180.9 181.24✓
13.00 12.66
18

180.84✓
13.08
10
EP

1266 (193.90) 1.98 (181.24)

(193.90)

6 + 57

176.89✓ 180.91✓
6.33 2.91
18
invert grate

~~12" culvert~~

6 + 50

180.23✓
2.99
18
EP

180.47✓
2.75

179.97✓ 175.64✓
3.25 7.58
7
EP
grate
Culvert

(183.22)

(183.22)

9+33.77 Disc PI
Sec
Sketch of gfs

9+00

943 $\left\langle \begin{array}{l} 20327 \\ \hline \end{array} \right\rangle$ 0.06 $\left\langle 193.84 \right\rangle$

8+66 approx BC

8+50

8+00

7+50

$\left\langle 193.90 \right\rangle$

Not rec'd. 4 ↓

199.18 ✓
4.09

196.11 ✓
7.16
1.84
EP

196.00 ✓
7.37

194.75 ✓
8.52
195
EP

$\left\langle 203.27 \right\rangle$

192.94 ✓
0.96
7.0
EP

192.89 ✓
1.03

192.56 ✓
1.34
1.7
EP

191.65 ✓
2.25
6
EP

191.52 ✓
2.38

191.39 ✓
2.51
14 EP

188.15 ✓
5.75
5
EP

188.17 ✓
5.73

188.43 ✓
5.47
15
EP

185.24 ✓
8.66
7
EP

185.36 ✓
8.54

185.61 ✓
8.39
13
EP

$\left\langle 193.90 \right\rangle$

= 0100 Lt. + RT (P-

End of line

= B.M.

9+3806 X in Pauc. 374 <199-53>

<203.27>

199.64 [✓]	199.53 [✓]	199.36 [✓]
3.63	3.74	3.91
5		5

<203.27>

Lajolla Hills
Lookout Drive Line

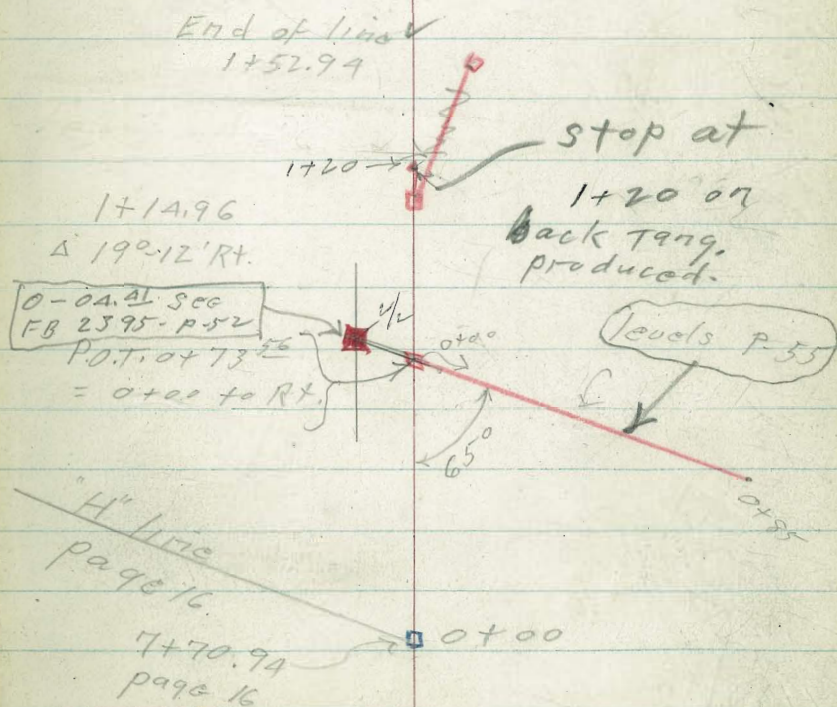
From Lot #21 Ely to Lot #28

8/4/54

□ = Fd Hub.

▣ = Set " + Disk

43 ✓



1+49 26 II at end

1+44 leaves Pav

1+00

0+75 28 LXX 61°46 X on Pav

Void

0+38

L-C-S

0+10

0+00

3.44 18480
18436

-0+00 See page 43

57468.52 - p-16

3.2
5

6.21

6.56
3 EP

44

6.45
EP

5.54
15
EP

6.04

6.55
10 ft grate
no collect across street

4.75
5.0
EP

5.03

5.25
5

Void

3.95
3
EP

4.28

4.40
5

2.8
5

3.39
EP

3.49
5

0.75 2.33
5 3 EP
BM #6 - P.21

2.74

3.16
3

Lookout Drive Line
 From Lot # 21 wly. + Nly. To
 Lot # 33 La Jolla Hills

8-4-54

□ denotes Ed 1/2 + disk

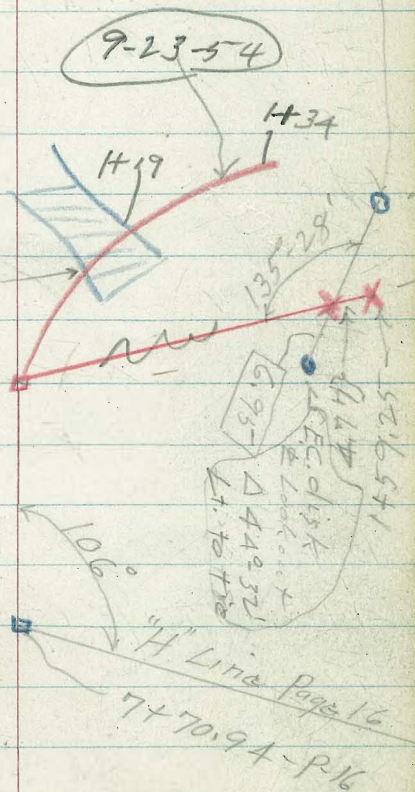
□ " Set " "

x " Cut cross

E.P. " edge of pavement

Levels - P-49.

1+34	180.2
1+19	179.8
0+99	180.2
0+85	181.0



From 20 to Lots
Lino # Lots #23424,
La Jolla Hills

■ denotes set $\frac{1}{2}$ disk

{ 140.28 South
102.43 East

1+35.28 = End of line

Revised
see 89 77-78

0+00

4+53.75 page 16 =

46

Levels - P-52

Revised
see 89 77-78

11" line

95° 03' 49"

2" line ahead

Lookout Drive

Ely from Lot 21 8/1/54

Sketch - page 43

E.P. = edge of pav.

cut stone drive

0+82 start comb. Conc. &
(25 ft. = old trench looks
to be water line)

0+77

0+55

0+35

0+00

7470-94 - P-16.

6.29 <187.65>

<181.36>

B.M. # 6 - page 21

±

47

✓ 183.4 ^v	✓ 183.27	✓ 183.8	✓ 184.3
4.23	4.38	3.80	3.35
5 E.P.	4 drive		5 on drive

✓ 183.73	✓ 185.5	✓ 181.4
4.36	2.1	0.4
5 E.P.		6

✓ 182.8	✓ 183.5	✓ 185.8	✓ 187.0	✓ 187.5
4.86	4.1	1.8	0.6	0.1
5 E.P.	3		2	6

✓ 182.33	✓ 183.6	✓ 184.7	✓ 185.0
5.32	4.0	2.9	2.0
5 E.P.		5	6

✓ 183.1	✓ 182.4	✓ 183.0	✓ 184.4
4.50	5.26	4.7	3.2
5 E.P.		2	6

<187.65>

Look out Dr.
end of line
1+64 on ϕ = start Conc. drive

185.03
4.64

1+52 ⁹⁴ $\frac{1}{2}$ P.O.T. =

184.67 185.84 ✓ 189.7
5.00 3.83 0.0
5
E.P. 4

1+37 3' Max 6' High bush

184.36 ✓ 184.9 ✓ 186.7 ✓ 190.3 ✓
5.31 4.8 3.0 + 0.6
70 3 5
E.P.

1+14 ²⁶ = Δ 19° 12' RT.

184.1 ✓ 184.4 ✓ 185.4 ✓ 188.0 ✓
5.60 5.3 4.26 1.7
5 2 $\frac{1}{2}$ 5
E.P.

T.P. 5.58 $\langle 189.67 \rangle$ 3.56 $\langle 184.09 \rangle$

$\langle 189.67 \rangle$ ✓

T.W. = top of wall

also = end of drive
1+08 } on ϕ = Nly end rock + Conc. wall

183.94 ✓ 184.27 ✓ 185.6 187.6
3.71 3.38 2.0 0.0
5 drive ϕ 5
E.P. T.W. T.W. + Ord
to south
+ east

1+00

183.78 ✓ 184.0 ✓ 184.3 ✓
3.87 3.64 3.36
5 5
E.P.

$\langle 187.65 \rangle$ ✓

Lookout Drive
Wly from Lot #21

8/5/54

Sketch - page 45

0+73 = start Conc. Pave.

Sec. at 90° to back Tang.

0+62⁸⁶ = Δ 75° 40' Rt.

0+36

0+30

0+00

7+70.9A - page 16 =

8.42 $\langle 189.78 \rangle$ - $\langle 81.36 \rangle$

BM #6 - page 21

49

181.0
8.8
5

180.35
9.43

180.3
7.47
5

185.5
4.3
5

183.9
5.85
1/2

183.5
6.3
2

180.8
9.0
5

180.5
9.26
8'
E.P.

189.2
0.6
10

188.3
15
6

184.0
5.8
3

182.5
7.3

180.86
8.92
5
E.P.

189.2
0.6
10

188.7
11
7

184.0
5.8
3

182.5
7.3

181.0
8.80
5
E.P.

184.4
5.4
6

183.0
6.8
2

182.4
7.38

181.6
8.14
5
E.P.

$\langle 189.78 \rangle$

Lookout Dr.
Wly from Lot #21

= cross P.O.T.

E.C. Radial line (see sketch)

1+54.48 = cross Lookout Drive

1+35

Nearest point to \pm sewer

1+16 - 5' RT. = face of curb

also = corner nearest to \pm
ob. inlet.

1+09 - 4' RT. = S.W. cor. grate for

1+00

0+78^S 5' ft. = start pava

178.4	178.1	177.9
11.42	11.65	11.90
44		5
E.P.		

178.3	178.1	177.9
11.46	11.66	11.88
5		5

178.8	178.6	178.3	173.2
10.96	11.16	11.46	16.60
5		4	4.5
		S.W. cor. grate	J E Box

179.1	178.9	178.6
10.70	10.90	11.20
5		5

180.2	180.1	180.1
9.60	9.70	9.72
5		5
E.P.		on pava

189.78

Lookout Dr.
Wly from lot #21

±

57
✓

check B.M. #6

8.42

18136 ✓

1765

4^E RT = E.P.

182.0 ✓

178.9 ✓

178.0 ✓

7.8

10.9

11.75

5.

4^E

E.P.

1759^E = end page.

182.7 ✓

178.9 ✓

178.2 ✓

178.0 ✓

7.1

10.9

11.58

11.82

10

4

E.P.

5

on page

1759²⁵ = Point: cross on page.

178 ✓

11.58

189.78 ✓

Line to Lots # 22-23-24
La Jolla Hills
Sketch - Page 46

Cont. Page 53

	12.15	13.1	5.36	146.67
T.P.	7.04	154.03	12.15	146.99
T.P.				
Set B.M. #10	1.78	159.14	1.78	157.36
T.P.	8.63	159.14	3.17	150.51
Set B.M. #9	12.45	153.68	11.37	141.23
T.P.	1.26	152.60	12.31	151.34
T.P.	0.01	163.65	12.59	163.64
T.P.	0.63	176.23	13.00	175.60
Set B.M. #8	1.99	188.60	4.05	186.61
	9.30	190.66	-	181.36

154.03 ✓
~~154.03~~

1/2 1+35²⁸ - (Page 46)

3/4" pipe = Ely. Cor. Lot # 24

Ec.

Lookout Radial to Sly. Cor. Lot # 25

B.M. #6 p. 21

Little Lots

22-23-24

1400

~~Revised~~
see pg 77-78

T.P.

12.78 ~~(162.69)~~ 2.07 ~~(149.91)~~

0+55

T.P.

3.98 ~~(151.98)~~ 6.03 ~~(148.00)~~

0+25

0+1

(in poison oak)

0+18 ± $\left. \begin{matrix} 5' RT \\ 4' LT \end{matrix} \right\} = 6" \text{ Eucalyptus.}$

0+00 Elev. from page 22

0+00 = A+53⁷⁵ - Page 16

53

150.75

151.0

151.7

12.4

11.7

11.0

5

5

~~Revised~~
see pg 77-78

~~(162.69)~~

139.5

141.3

143.0

12.5

10.7

9.0

5

5

~~(151.98)~~

135.6

137.8

139.2

18.4

16.2

14.8

5

5

~~(154.03)~~ from page 52

EL. = 128.0

17 wash

Lots #22-#23-#24

~~Revised
see #1 77-78~~

~~1+56 2' Lt. = Newly. Con. House~~

~~1+43- 1' Mt. 6' High Tree~~

~~1+40~~

~~1+35²⁸ = P.O.T. approx end of line~~

~~1+30~~

4

54 ✓

~~Revised
see #1 77-78~~

~~160.0~~

~~2.7~~

~~End at
House~~

~~157.3~~

~~5.4~~

~~5~~

~~158.2~~

~~4.5~~

~~159.3~~

~~3.4~~

~~5~~

~~156.5~~

~~6.7~~

~~5~~

~~159.37~~

~~5.32~~

~~1/2~~

~~158.1~~

~~4.6~~

~~5~~

~~154.6~~

~~8.1~~

~~5~~

~~154.9~~

~~7.8~~

~~155.8~~

~~6.9~~

~~5~~

~~162.59~~

Line Thru Lot # 30
La Jolla Hills
(Sketch - p 43)

8-7-54

Lt.

Rt.

55

T.P. 10.60 $\left\langle \frac{203.43}{\underline{\quad}} \right\rangle - 0.31 \left\langle \frac{192.83}{\underline{\quad}} \right\rangle$

0+32 10.5 Lt. Begin House

0+32

185.7	184.9	184.7
0.3	1.1	1.3
6.6	0	5
Grid at Wall		

0+26 7¹/₂ Lt. Begins 8" Conc Wall 1' high
7¹/₂ Lt S.W. Cor Sing Car Garage

0+13 3^o Rt. 3" Acacia Tree

0+06 8.7 Lt. N.W. Cor Sing Car Garage

185.6	186.01	185.8
7.5	7.13	7.3
5	on Hub	5

0+00 (0+73¹⁶ - Page 43)

0-05 Edge of Post.

183.22 ✓
9.92
0

+11.78 $\left\langle \frac{193.14}{\underline{\quad}} \right\rangle$

B.M. # 6 - Level set in Pickle weed $\left\langle \frac{181.36}{\underline{\quad}} \right\rangle$
Note →

See Pg 21

✦ $\left\langle \frac{193.14}{\underline{\quad}} \right\rangle$

2.43
Cor. to Cor.

Lot # 30

Lt

€

Rt

56
✓

ck. BM #6

-124.3

181.42

✓ 181.36

T.P.

+1.02

19385

-10.60

19283

0+85.

End Line

203.4

199.6

199.5

199.0

195.7

0.0

3.8

4.1

4.4

7.7

40

5

0

5

80

0+85.

0⁶ Rt.

Near Edge

Group of 3-8" Euc. Trees

? 0+80 Stop Line

0+77

3'

Rt. Near Edge 24" Eucalyptus Tree

0+76+

(Fence corner)
Approx Prop Cor.

0+74

4' Lt. & E&W Wall

198.6

4.8

4'

Grid at wall

198.6

197.8

197.1

4.8

5.6

6.3

5

0

5

0+72

9' Lt. End House

203.43

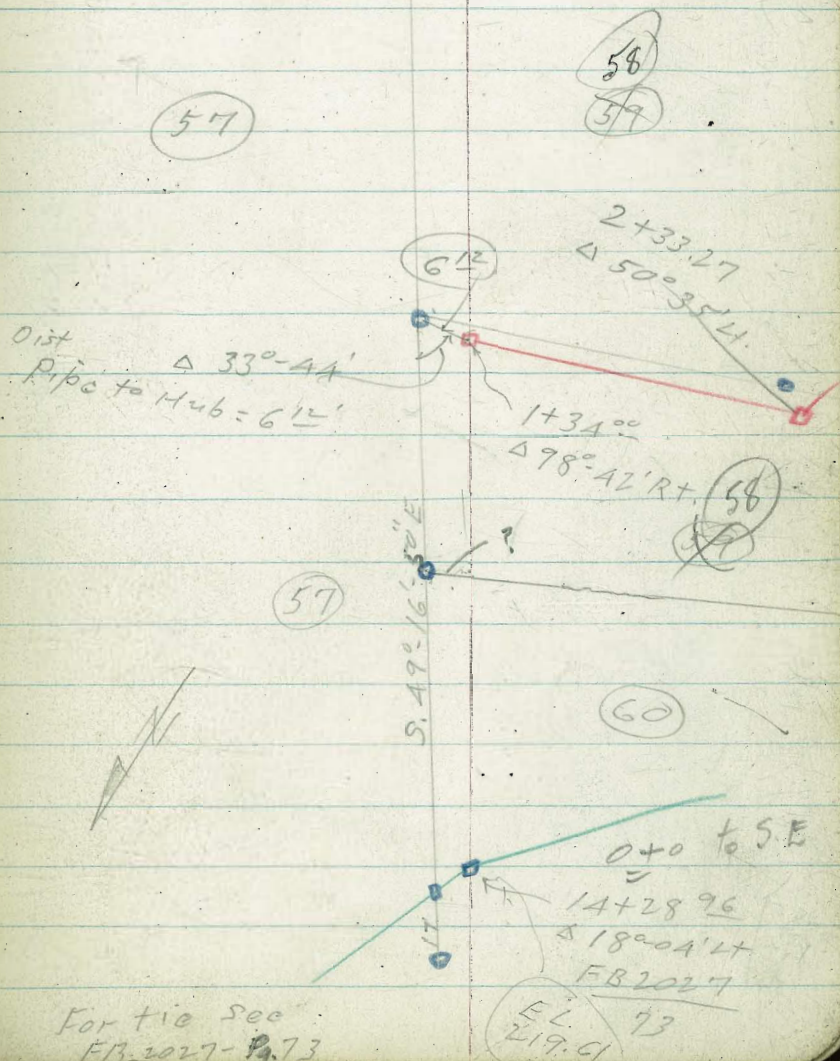
203.43

Line Thru Lots #59-60+62 +
 La Jolla Hills - on # 63
 To Existing Sewer in
 Resub La Jolla Hills #2-Map # 1713

C.H.S.
 Bogg
 Pullen
 Schelin

8/11/54
 W.O. 31841

57 ✓



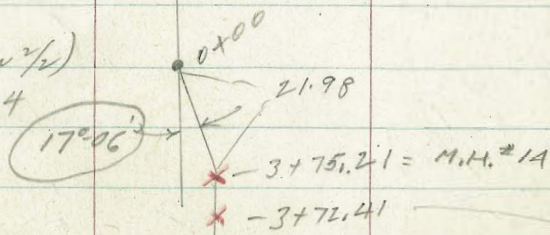
For tie see
 FB 2027-9.73

□ - 1/4 - 1150.28

F.B. 2031
P1

Note
Detail for tie

Nail (Now 1/2)
3+95.44



3+95.44 = Newly Cor Lot # 63 } Map #1479
N.E.ly Cor Lot # 62

3+72.41 = { 0+00 to west } page 68
 { 0+00 to East }

Common
Corner

pie shaped
portions of
Lot #58

→ □ Fd. 1/2 1150.28
FB 2031

58
Ⓟ

Now
= 4+98.98 = Δ 15-51' Lt
4+98.17 = Δ 18-29' Lt

(63)
This line for
P1-op. Tie only

Fd. Nail
Set 1/2 + disk
7-12-55

3+72.41
Δ 16-05' Lt

Use this

(62)

Radial
S = 2°-05'-30" E

3+95.44 = Fd. Nail =
0+00 FB 2031
P.O.T.

3+67.41 = 0-28°03'
Exit point
FB 2031

3+47.41
Δ 13-27' Lt
Now, P.O.T. at
Sewer line

2+77.76 P.O.T.

2+33.27
Δ 50-35' Lt

See F.B. 2031
1
for Existing line

2+43.25
Δ 90° 51' Lt.
F.B. 2031-R1

Existing pipe.
6+40 =

6+34.62 Exist. M.H.
Δ 190° 13' Lt.

136.45

4+98.17
Δ 180° 29' Lt.

Lots #59-#60-#62-#63
La Jolla Hills
Sketch - P. 57

8/14/54

1+25

1 ~

T.P.

10.83 $\langle 240.32 \rangle$ 1.38 $\langle 229.49 \rangle$

0+85

0+50

0+00 - P. 57

$\frac{1}{2}$
14+28.96

11126

$\langle 230.87 \rangle$

$\langle 219.61 \rangle$

4

60

234.8[✓]
5.5
5

234.6[✓]
5.7
5

234.8[✓]
5.5
5

231.6[✓]
8.7
5

231.9[✓]
8.4
5

232.0[✓]
8.3
5

$\langle 240.32 \rangle$ [✓]

228.9[✓]
2.0
5

228.9[✓]
2.0
5

229.0[✓]
1.9
5

224.3[✓]
6.6
5

224.3[✓]
6.6
5

224.4[✓]
6.5
5

219.7[✓]
11.2
5

219.61[✓]
11.26
 $\frac{1}{2}$

218.9[✓]
12.0
5

$\frac{1}{2} \times 0+00 = (14+28 \frac{96}{70} - \frac{FB, 2027}{70})$

$\langle 230.87 \rangle$ [✓]

Sec. on split of Δ
2+33.27 = A $50^\circ-35'$ Lt.

2+31 = cross thin hedge.

{ 4' = Δ it fence.

2+28 { 4' Lt. = 24" pine ←

2+10 3' Lt. = 20" Pine ←

2+00 Tree appears to have blight.

Holly Berry tree

1+87 2nd Rt. = 12" diam Calif.

T.P. 604 $\langle 243.01 \rangle$ 335 $\langle 236.97 \rangle$

{ 5th Lt. = 4" diam tree.

1+80 { 4th Lt. start wire fence.

1+67 6th Lt. 2" tree.

1+58 7th Lt. = 3" tree.

1+50

1+46 6th Lt. = 3" Eucalyptus

1+34 $\triangle 78^\circ-42'$ Rt. Sec. on split of Δ

$\langle 240.32 \rangle$

238.5[✓]
4.5
5

237.5[✓]
5.50
5

237.5[✓]
5.5
5

236.5[✓]
6.5
5

235.3[✓]
7.7

234.6[✓]
8.4
5

$\langle 243.01 \rangle$

238.4[✓]
1.9
5

236.8[✓]
3.5

236.4[✓]
4.1
5

237.1[✓]
2.6
5

237.1[✓]
3.2

236.2[✓]
4.1
5

236.3[✓]
2.0
5

236.6[✓]
3.71
5

235.8[✓]
4.5
5

$\langle 240.32 \rangle$

T.P. 13.10 $\langle 267.94 \rangle$ 0.92 $\langle 254.84 \rangle$

3+28

3+25 6^E Lt. = 2 ft outlet 36" culvert.

3+15 = 4 in ditch

3+04 = cross fence.

3+00 cross ditch.

1/2-2477.76

T.P. 12.99 $\langle 255.76 \rangle$ 0.24 $\langle 242.77 \rangle$

2+68 18' Lt. = 5" Avocado

2+67 7^E Lt. = 8" tree

2+63 - 4' Lt. = 1176 of fence

2+50

$\langle 243.01 \rangle$

251.5
4.3
5

251.6
4.2
5

252.1
3.7
5

248.11
7.65
6^E
I.E

249.7
6.1
6^E

250.4
5.4
5

251.4
4.4
5

251.9
3.9
5

249.2
6.6
5

248.8
7.0
1

247.7
8.1
1

248.5
7.3
1

249.1
6.7
5

246.7
9.1
5

246.7
9.1
1

245.7
10.1
1

246.2
9.6
1

246.4
9.4
5

$\langle 255.76 \rangle$

239.2
3.8
10

236.8
4.2
5

237.6
5.4
4

238.5
4.5
3

238.5
4.5
5

238.6
4.4
5

$\langle 243.01 \rangle$

3+72⁴¹ cross

T.P., 5.17 $\langle 268.14 \rangle$ 4.97 $\langle 262.97 \rangle$

also = 0+00 $\left\{ \begin{array}{l} \text{lines} \\ \text{Lt + Rt} \end{array} \right.$

3+72⁴¹ = Δ 16°-05' Lt. = X in pava

3+57³ = start conc. pava

3+56 5^E Rt = end fence

3+54

3+47⁴¹ = $\frac{1}{2}$ p.o.t. (Page 58)

3+40 ^v

$\langle 267.94 \rangle$

263.17^v
4.77
5

262.97^v
4.97
5

262.73^v
5.21
5

262.54^v
5.40
5

262.32^v
5.62
5

262.12^v
5.82
5

263.6^v
4.3
5

263.4^v
4.5
5

262.7^v
5.2
5

261.16^v
6.78

260.1^v
7.8
5

260.0^v
7.9
5

259.6^v
8.3
5

$\langle 267.94 \rangle$

4+50

TIP.

13.24

 $\langle 279.38 \rangle$

2.00

 $\langle 266.14 \rangle$

4+20

4+00

3+88-

11' Lt. = ϕ intake 36"

culvert

3+84 - 9' RT = Power pole #P 7638

3+77³ = leave Pave $\langle 268.14 \rangle$ 270.5[✓]
8.9
6270.6[✓]
8.8
5271.2[✓]
8.2271.7[✓]
7.7
5 $\langle 279.38 \rangle$ 264.3[✓]
3.8
14
w.264.9[✓]
3.2
5265.0[✓]
3.1266.1[✓]
2.0
5262.9[✓]
5.2
5263.0[✓]
5.1263.8[✓]
4.3
5258.54[✓]
9.60
112
I.E.262.3[✓]
5.8
5262.3[✓]
5.8263.1[✓]
5.0
5263.4[✓]
4.7
5263.4[✓]
4.7263.4[✓]
4.7
5263.36[✓]
4.78
5263.24[✓]
4.90262.93[✓]
5.21
5 $\langle 268.14 \rangle$

set. B. M. on Δ
A+98.17

SS.

13.12 279.43 ✓

T.P.

13.34

$\langle 292.55 \rangle$ ✓
0.17 $\langle 279.21 \rangle$ ✓

$\langle 292.55 \rangle$ ✓

A+95

278.9 ✓
0.5

A+90

278.4 ✓
1.0

A+84

275.8 ✓
3.6

A+75

274.9 ✓
4.5
5

274.9 ✓
4.5

274.8 ✓
4.6
W

A+57

272.4 ✓
7.0
5

271.9 ✓
7.5
W

270.3 ✓
7.1
5

$\langle 279.38 \rangle$ ✓

$\langle 279.38 \rangle$ ✓

F.B. 2027

check for M.H. at 3+10²³

G+40 = Existing sewer
of old M.H. Now removed
G+34⁶² = Δ 19°-13' Lt. = position

G+23. P.O.T.

T.P.	13.00	344.30	0.00	331.30
T.P.	13.00	331.30	0.00	318.30
T.P.	13.00	318.30	0.00	305.30
T.P.	13.05	305.30	0.30	292.25

by hand level

5+11

A+98.17 = Δ 18°-29' Lt = 2/2

292.55

345.3	342.3
+1.0	2.0
Ord.	F.E.

343.7
0.6

344.30

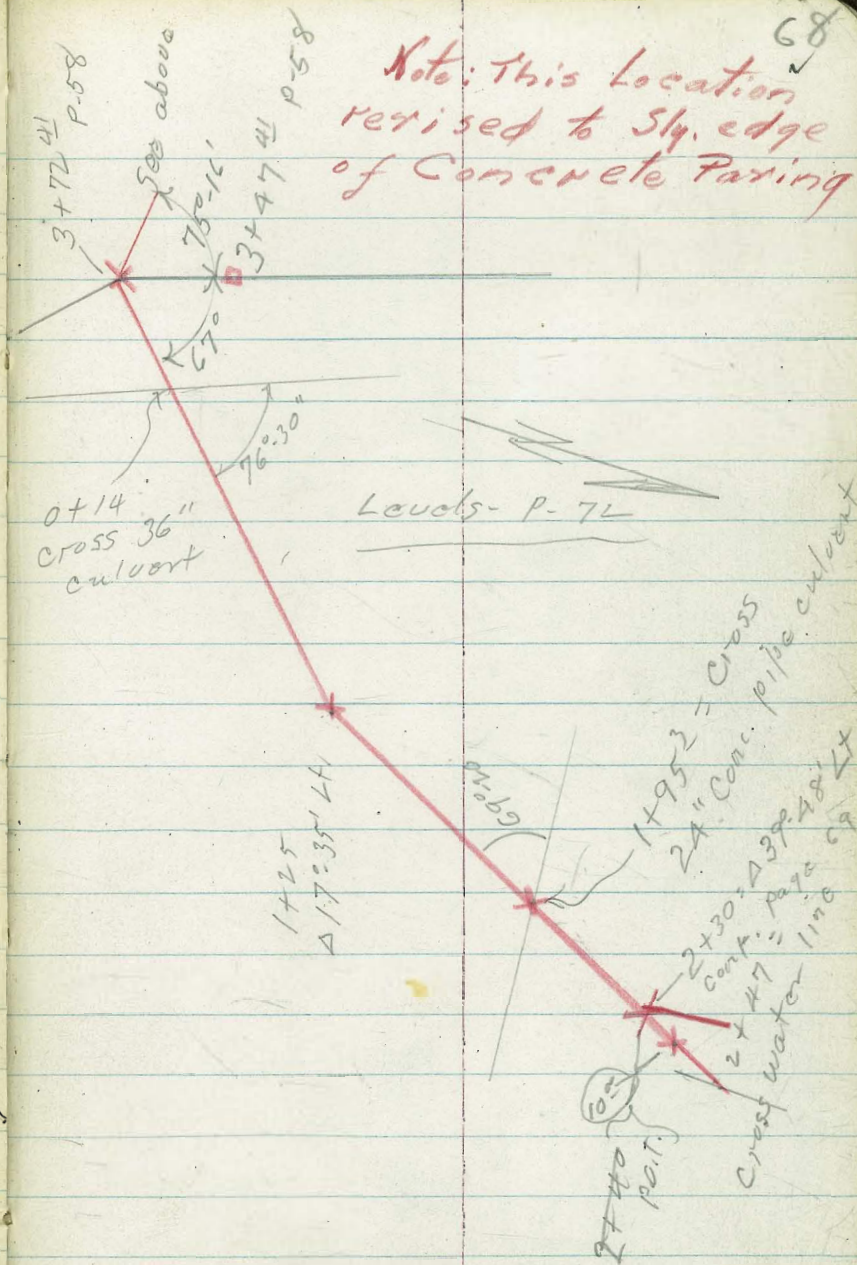
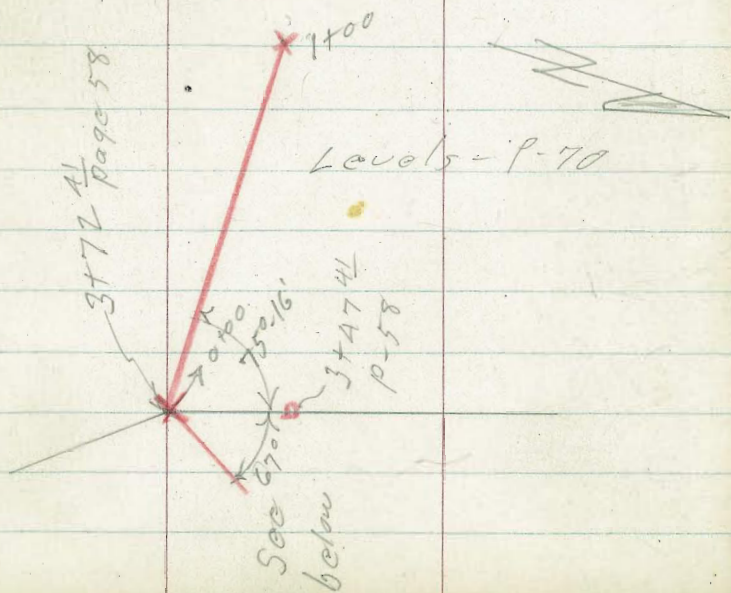
287.3	286.0	284.4		
5.2	6.6	8.1		
5	5	5		
280.5	279.4	279.3	279.7	279.2
12.0	13.1	13.12	12.8	13.3
5	2		5	10
				2

292.55

Hillside Drive
To serve Lot #61

8/16/54

Also to serve Lots #68-69-70



4 + 8 / 60
End of line



3 + 70 44
Δ 76° Rt

2 + 30° Δ 39° 48' Lt.
From page 68



To Serve Lot # 61
La Jolla Hills

Sketch - P. 68.

E.P. = Edge of Conc Pavc.

T.B. = Top of bank

(W) = water service

0+80

0+92 Cross (W)

0+60

0+30

0+01 14' Lt. = p-10 # P. 7638.

0+00 = 3+75.21 ^{M.H.} Revised to 2 in on Sly Side.
3+72.41 - P-58 = of Conc Pav + chained
along Edge Paving to E

6.41 <269.38> - <262.97>

257.16	258.16	257.92	257.47
11.8	11.22	11.46	11.91
11	7		14
T.B.	E.P.		E.P.

259.8	259.27	259.08	258.88
9.6	10.11	10.30	10.50
14	9.5		10
T.B.	E.P.		E.P.

261.38	261.16	260.96	260.85
8.0	8.22	8.42	8.53
15	11		9
T.B.	E.P.		E.P.

263.17	263.17	262.97	262.8
6.2	6.21	6.41	6.90
14	E.P.	<269.38>	15
T.B.			E.P.

B.M. = 3+72.41 x in Pavc. - Page 58 + C3

Line to Lot # 61

71

T.B.M. #2 S.S. 12.68 256.70

Cross in Pauc. 1400

1+15

269.3 [✓]	256.4 [✓]	255.23 [✓]
0.1	13.0	14.15
10	T.B.	7
		E.P.

= leave Pauc.
1400 = cross on Pauc.

251.21 [✓]	256.70 [✓]	256.03 [✓]
12.2	12.68	13.35
7	E.P.	21
T.B.		E.P.

0 + 92 = Cross (W)

269.38[✓]

269.38[✓]

Line To Lots. #68 #69 #70

Sketch - Page 68

1+25 = Δ 17° 35' Lt. 270.4

1+00

269.2

T.P. 8.2 <277.03> 0.56 <268.82>

0+80

+75

267.8

0+50

266.1

+37

265.2

7' Mt. for curb inlet
8' Mt. Near edge of box

0+14 = } Cross 36" culvert 263.7

0+00.
3+72.4 P.58 =

3+75.21 Mt. Revised to miss
curb inlet then
run along 5' from S.
of Pat.

<269.38>

M. From P-71

El. in Red taken on Sta 72
channeled along sedge par.

270.01 270.40 270.47 270.8
7.02 6.63 6.56 6.2
152 32 10
E.P. E.P. T.B.

<277.03>

268.06 268.46 268.4 268.6
1.32 0.92 1.00 0.8
72 118 17
E.P. E.P. T.B.

265.95 266.22 266.43 266.8
3.43 3.16 2.95 2.6
58 145 21
E.P. E.P. T.B.

254.45 262.85 263.23 263.56 257.10
14.93 6.53 6.15 5.82 12.28
85 85 7 7
I.E. grate grate I.E.

262.01 262.97 263.28
7.37 6.41 6.10
169 52
E.P. E.P.

<269.38>

Lime for Lots # 68 + 69 + # 70
La Jolla Hills.

±

73

T.P. 7.18 $\langle 280.97 \rangle$ 3.24 $\langle 273.79 \rangle$

T.P. on cross = Δ 2 + 30° = P 68

$\langle 280.97 \rangle$

X+00

272.4

272.08 [✓]	272.39 [✓]	272.39 [✓]	275.5 [✓]
4.95	4.64	4.64	1.5
87		114	15
E.P.		E.P.	

See P-68

98 RA. = } box to curb inlet

69 Lt. = } near edge of

1+95³ Cross 24" Culvert. #1

267.65 [✓]	272.17 [✓]	272.57 [✓]	272.33 [✓]	268.38 [✓]
7.98	4.86	4.66	4.70	8.65
67	69		98	98
I.E.	grate.		grate	I.E.

1+80

+75

272.3

272.16 [✓]	272.33 [✓]	272.53 [✓]	272.5 [✓]
4.87	4.70	4.50	4.5
84		98	10
E.P.		E.P.	T.B.

1+50

271.5

271.10 [✓]	271.40 [✓]	271.59 [✓]	271.7 [✓]
5.93	5.63	5.44	5.3
12		72	12
E.P.		E.P.	T.B.

$\langle 277.03 \rangle$

$\langle 277.03 \rangle$

3457 = Cross (W)

3450

276.8

277.73
3.24
13
E.P.

277.17
3.80

276.77
4.20
83
E.P.

+25

276.2

276.85
4.12
183
E.P.

276.09
4.88

276.02
4.95
12
E.P.

3420

3400

275.6

276.12
4.85
152
E.P.

275.64
5.33

275.57
5.40
38
E.P.

2480

+75

275.2

275.33
5.64
11
E.P.

275.34
5.63

275.31
5.66
82
R.T.

2455

+50

274.5

274.47
6.50
103
E.P.

274.69
6.28

274.82
6.15
10
E.P.

water line.
7² Rt = old ditch for
S.C.C. on split of A.

2430 = A 39° 48' Lt.

273.7

273.60
7.37
154
E.P.

273.79
7.18

273.80
7.17
42
E.P.

274.51
6.46
73
in drive

280.97

280.97

4+81⁶⁰ = X in Pavc. = end of line

281.5[✓]
5.08
92
E.P.

281.43[✓]
5.17

281.30[✓]
5.30
10
E.P.

4+75

281.05[✓]
5.55

269

280.3

4+58

280.3

280.48[✓]
6.12
132
E.P.

280.00[✓]
6.60

279.90[✓]
6.70
62
E.P.

4+34 - 392 L⁺ = Pin - Cor. lots[#] 54+⁴⁵⁵

279.40[✓]
6.90
17
E.P.

278.69[✓]
7.91

278.58[✓]
8.02
22
E.P.

4+15

+25

279.4

4+00

278.5

279.28[✓]
7.32
155
E.P.

278.29[✓]
8.31

278.0[✓]
8.60
5
E.P.

+77

277.7

71R

8.25 <280.60> 2.62 <278.35>

X-44 pavc. Δ sta 3+70⁴⁴

Sec. on split of A

3+70⁴⁴ = Δ 76° RT - page 69

278.47[✓]
2.50
17
E.P.

278.35[✓]
2.62

277.77[✓]
3.70
182
E.P.

<280.97>[✓]

<280.97>[✓]

	SS	0.66	390.69 ✓
Exist M.H.#29	I.E. =	7.60	(383.75) I.E. ✓
Exist M.H.#29	top.	0.90	(390.45) Rim ✓
12.37	* 391.35 ✓	0.05	378.98 ✓
12.93	379.03 ✓	0.05	366.10 ✓
13.24	366.15 ✓	0.11	352.91 ✓
13.09	353.02 ✓	0.17	339.93 ✓
12.97	340.10 ✓	0.24	327.13 ✓
13.12	327.37 ✓	0.09	314.25 ✓
13.20	314.34 ✓	0.12	301.14 ✓
13.28	301.26 ✓	1.63	287.98 ✓
8.18	289.61 ✓	-	281.43 ✓

Chisel □ on curb at water valve vault. N.W.ly nose of curve. N.W. of 7520 Hillside drive.

X 4+810 - page 75 - EL. = 281.43 ✓
 @AD 5/6/57

T.I.B.M.		12.41	246.04 ✓
T.P.	1.61	258.45 ✓	12.54 256.84 ✓
T.P.	0.75	269.38 ✓	8.76 268.63 ✓
T.P.	2.04	277.39 ✓	11.25 275.35 ✓
			286.60 ✓

stub.

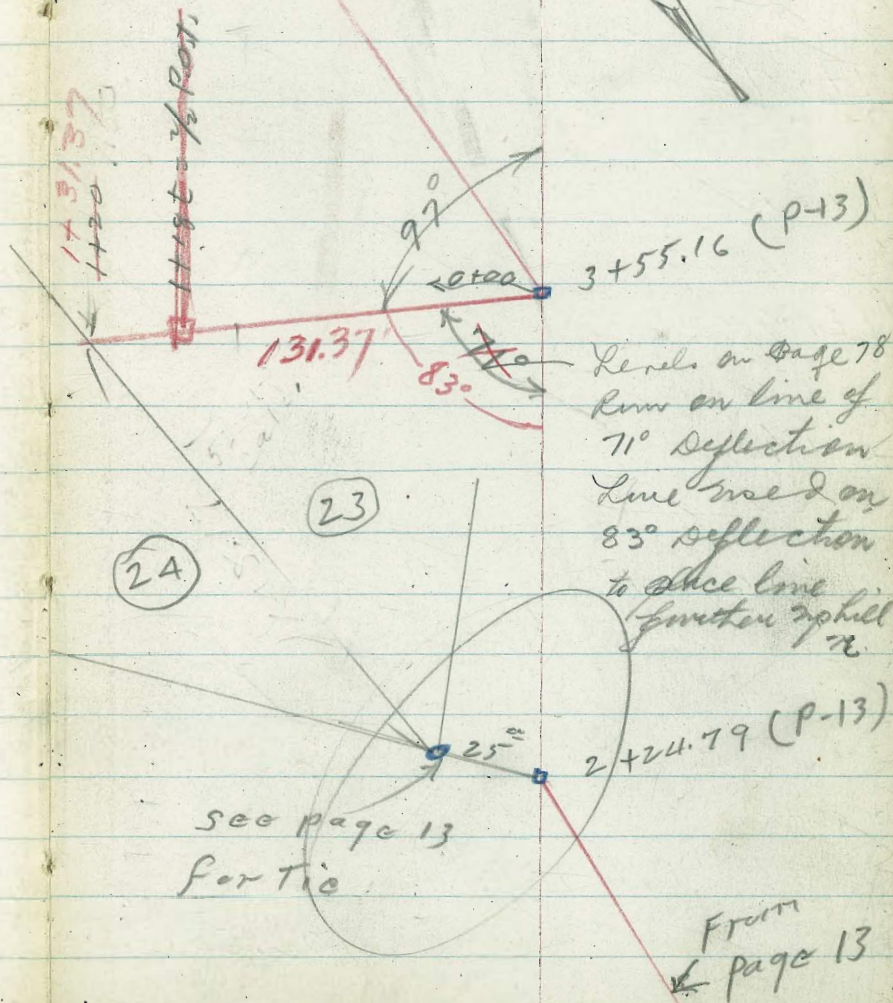
		18.93	359.32 ✓ I.E.
Top. M.H.# I (12875-L)	Drawing	12.73	365.52 ✓ Rim
T.P.	0.05	378.25 ✓	13.15 378.20 ✓
		* 391.35	

Line to Lots #23 + #24

Revised 77
Not Used

See FB.2395
51

1/1/55 CHP



Levels thru
Lots #23 + #24

Revised 78
Not used.

1+57⁸

148.0

1+50

147.0

1+18

141.0

0+90

132.0

0+45

116.6

0+07

107.8

= 0+00

102.6

3+55¹⁶ (P. 13)

102.60

3+55¹⁶ P. 13 + P. 21)

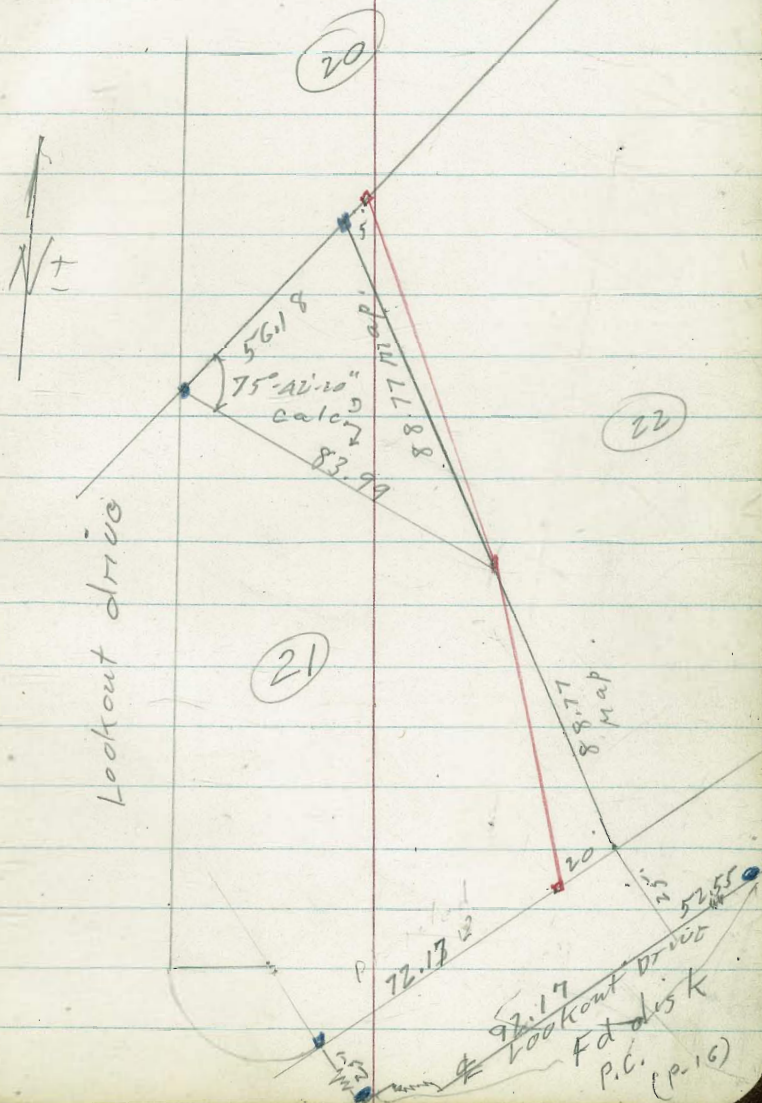
Actual Elevations shown

Line between Lots 21422
La Jolla Hills 1-7-55

Fd. points shown in blue

Set. " " " red.

Set. flags along line shown
in red.



76-30

Fd

Se

Se

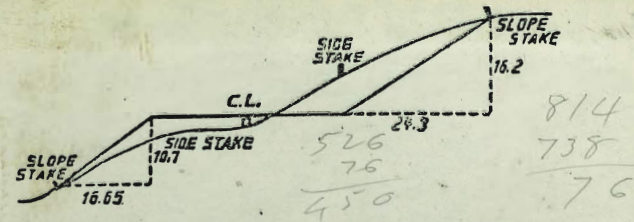
11

2444.49

5925
477
5448

3.80

Fd 125 102 90 04.55
So 5 5
15200
191.1
13.
204.1
53
209.4
77
29.1



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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