

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

1643  
4.9

L-7

10701-





TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Page

SEWER - Lot 16, CAVE + M<sup>c</sup>HATON SUBDIV

2

" BLK 22, CHOATES ADDN.

5

" OUTFALL - DRUCKER'S SUBDIV.

8

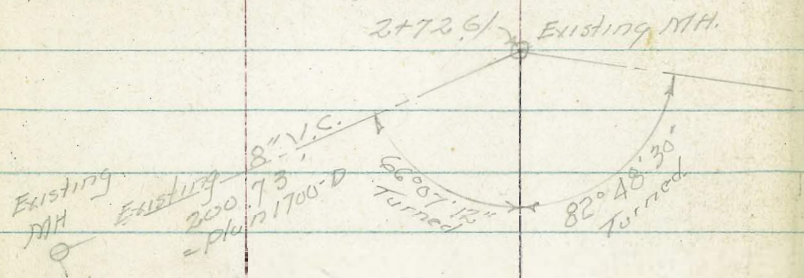
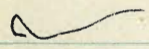
Drain Survey in Pl. 243, 259, Midway Dr } 46-  
To Lapwai St



# Alignment - Proposed Sewer in Lot 16 - CARR & N. HATTON

Walker  
Pape  
Roller  
Whipple  
9-3-53

Subdivision - Map # 159  
No 62347

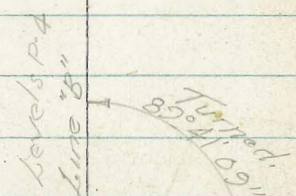


Exist. 8" V.C.  
200.73  
= Plan 1700-D

Existing MH

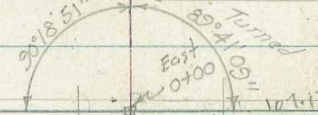
Existing 8" V.C.  
200.73  
= Plan 1700-D

2+72.61 Existing MH.



POT 0+75.00

set Spk



East 0+00

Line 8"  
A-levels P.3

148.52

17.84

Turned  
90°19'45"

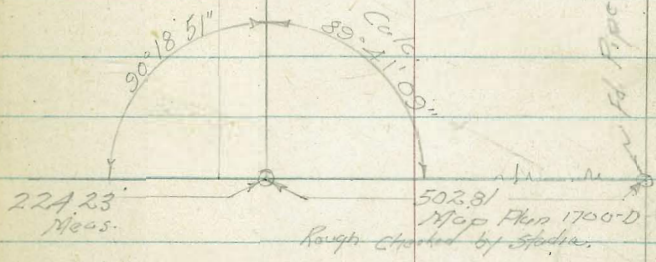
12.52

140.16  
= POT

Cut  
Chisled Conc.  
Cross in Pot

132.01  
Meas. Lot 15

SCHOOL  
PROP.



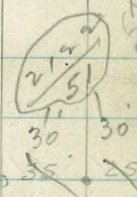
22A.23 Meas.

90°18'51"

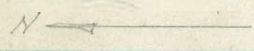
99°41'09"

502.81  
Map Plan 1700-D  
Rough checked by stadia.

Al. Prop. FE



30 30  
35 35



35 35

58TH

FE DISC. 17 CONC. FE 1534  
Also 8" M. = 296.82  
FB 2122-16

FE DISC. 17 CONC. FE 1534  
Also 8" M. = 296.82  
FB 2122-16

ch. line  
ch. line  
54



LEVELS - PROPOSED SEWER  
 on "A" line - sketch P. 2

1+85 = End "A" line

289.76	286.0	281.6
10.87	14.6	13.0
on	21	40
stub		

1+50

291.1	289.0	284.1
2.5	11.5	16.5
	17	40

1+07.16 = P.O.T.

292.4
8.31
on
stub

0+50

293.5	288.4
7.1	11.9
	40

0+00

This side  
 Above 2

293.85	289.8
6.78	10.8
on	40
stub	

3.81 / 300.63

296.82

F.A.  
 21/22  
 16



LEVELS - PROPOSED SEWER

"B" LINE - sketch P2

			0.15	
E.M.H.	Existing		221.09	→ Plan 1700-D
2+72.61	Invert	20.02	221.24 ✓	
	on Rim			
2+72.61	Exist. MH	8.97	232.29 ✓	
TR	3.78	(241.26) ✓	12.98	(237.48) ✓
	2+50		140	236.5 ✓
TR	0.47	(250.46) ✓	12.99	(249.99) ✓
	2+00		138	249.2 ✓
TR	0.04	(262.78) ✓	13.00	(262.94) ✓
	1+50		139	262.0 ✓
TR	0.77	(275.94) ✓	13.13	(275.17) ✓
	1+00		133	275.0 ✓
	0+75 = P.O.T.		81	280.2 ✓
	0+53		38	284.5 ✓
TR	0.99	(288.30) ✓	13.32	(287.31) ✓
	0+41		132	287.4 ✓
	0+00		221	292.42 ✓

(300.63) P-3

INDEXED  
SEP 4 1953



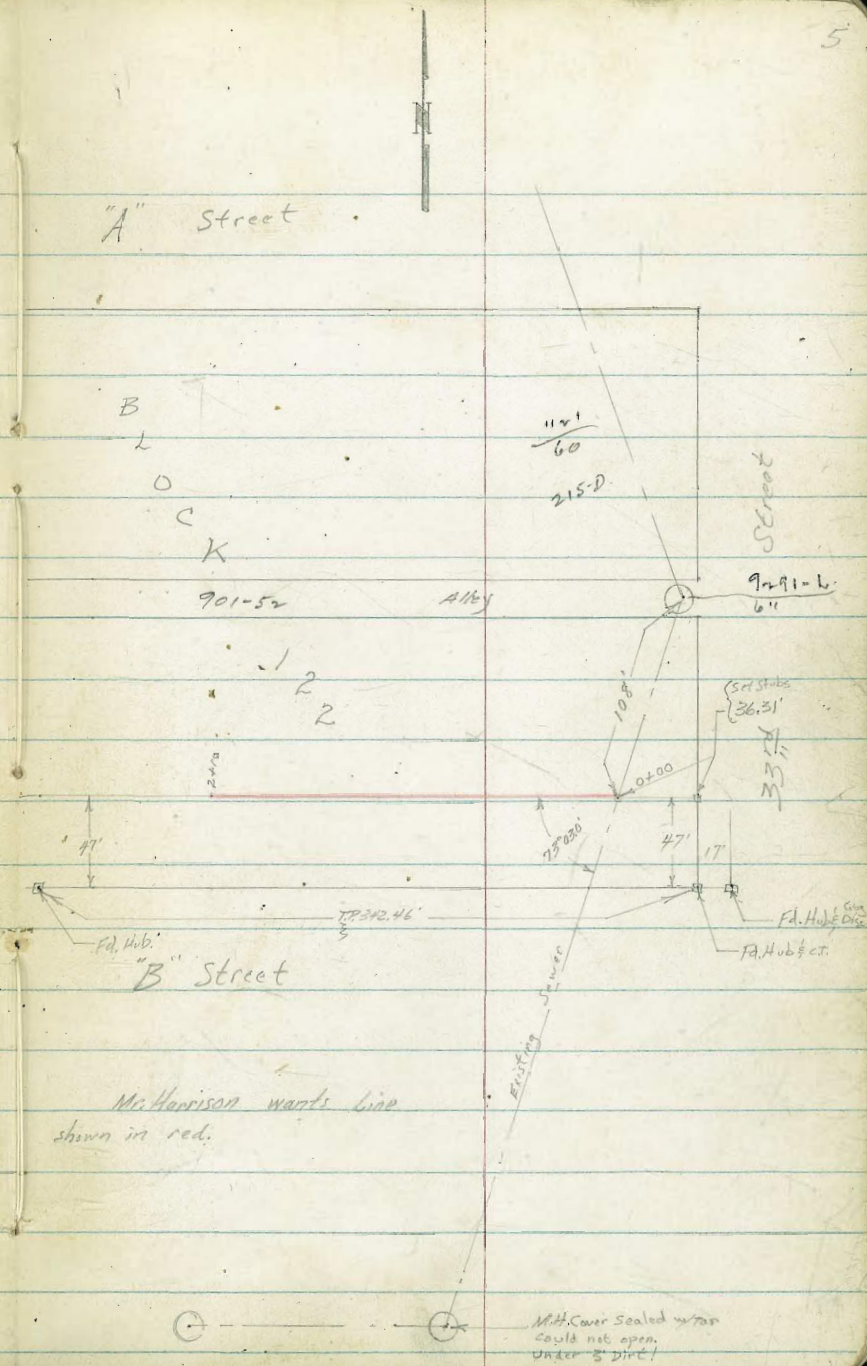
Roberts  
Cota  
Moore  
Morales  
9-11-53  
W.O. # 6238

Survey For Sewer BIK 122, Choates Add.

33' 4" E B R

5

INDEXED  
SEP 15 1953





0+68

✓ 133.1	✓ 133.1	✓ 133.6	✓ 135.9	✓ 136.0
7.8	7.7	7.3	5.0	4.7
15		3	7	15

0+65

✓ 133.1	✓ 133.4	✓ 134.0
7.8	7.5	6.9
15		15

0+34

✓ 132.9	✓ 133.4	✓ 134.0
8.0	7.5	6.6
15		15

0+15

✓ 127.9	✓ 128.6	✓ 130.6
18.7	17.3	10.3
15		15

0+00 Proposed M.H.

✓ 126.9	✓ 126.2	✓ 126.5	✓ 128.9
14.0	14.7	14.4	12.0
15		5	15

TBM 15.88 (14.88) ✓

125.00

Plan 16-D  
 { I.E. From Plans  
 of MH in Alley  
 BIR, 122, Chocates  
 Add. F 335A

140.88 ✓

BM

(could not find)

162.73 ✓  
 N.E. Mon.  
 A & 3rd  
 23.7



Cont'd From Page 6

24

E

R2

7

2+10

✓  
132.0  
89  
15

✓  
133.1  
7.8

✓  
134.9  
6.0  
15

1490

✓  
132.9  
8.0  
15

✓  
132.9  
8.0

✓  
135.9  
5.0  
3

✓  
136.2  
4.7  
15

1450

✓  
132.8  
8.1  
15

✓  
132.9  
8.0

✓  
132.9  
8.0

✓  
136.3  
4.6  
5

✓  
136.3  
4.6  
15

1400

✓  
132.5  
8.4  
15

✓  
132.9  
8.0

✓  
133.0  
7.9  
4

✓  
135.9  
5.0  
7

✓  
136.1  
4.8  
15

140.88

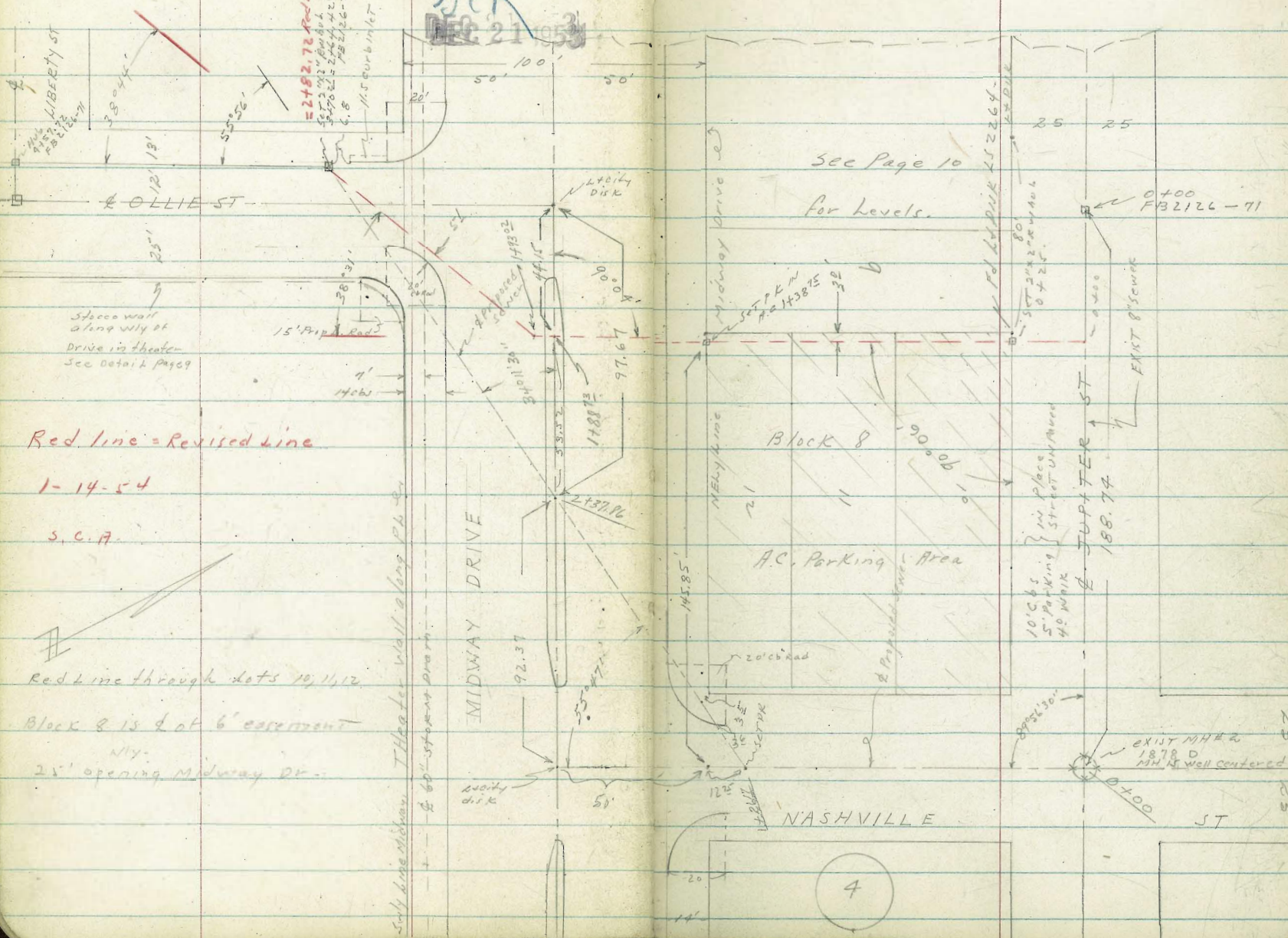
140.88



Change of Alignment Portion of  
 Proposed Sewer Druggers Sub Division  
 See FB 2126-71  
 C. Allen, D. Sisson, C. Powell.  
 12-16-52

INDEX  
 YER  
 DEC 21 1953

See page 10 for Levels  
 See page 14 for Levels on Red Line



See Page 10  
 for Levels.

Red line = Revised line

1-14-54

S.C.A.

Red line through lots 10, 11, 12

Block 8 is lot 6' extension

25' opening Midway Dr.

4







W/enclosure wall

Levels for prepared Sewer Line  
Change in Druckers sub-  
See Sketch page 8-  
See Also FR 2126-71

LT

Prepared  
SEWER

RT

10

3/4 Ret along curb Ret - New end curb P

1+44.8 = face type G curb = on Ret

7.28 gutter  
6.72 Top curb

1+26.17 = L. 55°47' to right

6.73  
mark

1+00

6.2

0+50 - (Rough Acc.)

7.0

0+00 = Sewer MH @ Nashville + Top of ST 5

7.37  
7.61  
7.61  
2  
16.17  
1.15

BM - 8.05 7.61  
- 0.44

2" x 2" Redwood hub 0+00 AB. 2126-92



LT

Prop  
Sewer

RT

11

3400

6<sup>05</sup>

2+50 - ON A.C. Pave - IN South bound traffic lane

5<sup>73</sup>  
AC

2+41<sup>0</sup> & proposed Sewer intersects Wly edge  
4' traffic island Midway pr

5<sup>21</sup>

5<sup>72</sup>

2+37<sup>86</sup> & proposed Sewer intersects & Midway

TOP  
CH

GUTTER

2+34<sup>6</sup> & proposed Sewer intersects Ely edge  
4' wide traffic island

5<sup>83</sup>

5<sup>24</sup>

GUTTER

EN TOP ISLAND

IN North bound Traffic Lane  
2400 - ON A.C. Pave Midway drive

6<sup>25</sup>

in driveway to cafe  
1+74 = Top type G. curb

6<sup>75</sup>

6<sup>85</sup>

LIP.  
DRIVE

GUTTER

1+53.2 3<sup>5</sup> RT = Property COR - NEly COR  
Midway Nashville

6<sup>6</sup>

7<sup>61</sup>

7



Proposed Sewer Drucker sub

LT

Prop  
Sewer  
66

RT 12

3+50

Type G curb

61110

Curb Return also end of curb side

3+37<sup>2</sup> Proposed sewer is on wly end of

570

625

Top curb  
Wly end cb

90  
Type G

3+34<sup>5</sup> - 12<sup>9</sup> LT = property E.C. 15' Radius

of 15' PL Radius

3+24<sup>6</sup> 10<sup>2</sup> LT = property Line at center

51

ground

for Levels + Details on Stucco Wall see page 9

3+22<sup>6</sup> 9<sup>0</sup> RT = face curb on Return

556

618

90  
Top  
cb

90  
GUTTER

3+18<sup>6</sup> ± 9<sup>0</sup> LT = Prop B.C. 15' PL Radius

3+02<sup>2</sup> = face wly curb Midway Dr - Type G

615

554

GUTTER

Type G  
2

761



Proposed Sewer Druckers

LT-

Prop  
Sewer

RT

1.5

TP,

6.35 1.26

ON PK Walk 1457<sup>21</sup> FB 2126 - 72

L. 55° 56 LT.

3470<sup>21</sup> = 2+64.42 FB 2126 Page 71

7°  
ground

721  
on Hub  
2

basin NW 1/4 Cor Midway + Ollie St

3459° 15<sup>2</sup> = 2 grate (3<sup>5</sup> x 2<sup>2</sup>) 11<sup>5</sup> catch

691 1216  
15<sup>2</sup> 15<sup>2</sup>  
grate IF Box

761



Levels for Proposed Sewer - Druckers  
 Subdivision See Red Line on sketch page 8

Location as used.

Fence goes parallel to &

0+26<sup>3</sup> } 1<sup>3</sup> RT = NELY COR Board Fence  
 & crosses 4' high board fence

0+25 = <sup>514</sup> Wly Line Jupiter ST

A.C. 3"  $\pm$  thick  
 0+24 } 1<sup>3</sup> RT = NELY A.C. Parking Area  
 w/ly edge walk + Begin A.C. Parking area

0+20 = w/ly edge walk

Curb in poor condition

0+15 = <sup>w/ly</sup> face curb

Jupiter ST at this point under water - 1-14-54

0+00 = & Jupiter + exist 8" sewer

BM. 6.02  $\leftarrow$  6.26  $\rightarrow$  O.R.H

LT

6'  
 care

RT

14

✓ 1	✓ 0	✓ 0
6 <sup>2</sup>	6 <sup>3</sup>	6 <sup>3</sup>
10	PC	10
PC		

✓  
1.6  
6.43

✓  
2.7  
6.53

✓ -3	✓ -1.0	✓ -1.0	✓ -1.3	✓ -1.1	✓ -1.4
6.54	7.3	7.3	6.60	7.4	6.71
10 <sup>0</sup>	10	DIRT	2	10	10
CB	90T	90T	TOP	90T	TIP
			CB		CB

✓ -1	✓ -1	✓ -1
6.5	6.5	6.4
10		10

$\leftarrow$  6.26  $\rightarrow$

Right Manhole page 10 - 0+00



Prop Sewer Drickers Sub

LT

6' case.

RT

15

Type G curb  
1+52.75 = NELY Curb Line Midway Drive

1.0	1.61	1.64	1.1	1.67	1.1
5 <sup>25</sup>	4 <sup>65</sup>	4 <sup>58</sup>	5 <sup>20</sup>	4 <sup>59</sup>	5 <sup>20</sup>
10	10	Top	2	10	10
9UT	Top	cb	Type	Top	9UT
	cb		6 9UT	cb	

Neon sign - set in conc  
8<sup>5</sup> LT = 4 5" steel pipe supporting  
1<sup>3</sup> RT = edge AC + sly Board fence

1+38.75 = NELY Line Midway Drive

1.7	1.6	1.6	1.8
4 <sup>6</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>5</sup>
10	AC	1 <sup>3</sup>	10
AC		AC	

set in conc -  
1+35 - 1<sup>9</sup> LT = 2 3" steel pipe - light std

1+25 - 1<sup>3</sup> RT = edge AC + sly board fence

1.4	1.4	1.4	1.4
4 <sup>9</sup>	4 <sup>9</sup>	4 <sup>9</sup>	4 <sup>9</sup>
10	AC	1 <sup>3</sup>	10
AC		AC	

1+00 - 1<sup>3</sup> RT = edge AC + sly board fence

1.1	1.1	1.1	1.1
5 <sup>2</sup>	5 <sup>2</sup>	5 <sup>2</sup>	5 <sup>2</sup>
10	AC	1 <sup>3</sup>	10
AC		AC	

0+75 - 1<sup>3</sup> RT = edge AC + sly fence

.8	.8	.8	.8
5 <sup>5</sup>	5 <sup>5</sup>	5 <sup>5</sup>	5 <sup>5</sup>
10	AC	1 <sup>3</sup>	10
AC		AC	

0+50 - 1<sup>3</sup> RT = edge AC + sly board fence

.5	.5	.5	.6
5 <sup>8</sup>	5 <sup>8</sup>	5 <sup>8</sup>	5 <sup>7</sup>
10	AC	1 <sup>3</sup>	10
AC		AC	

16.26



Proposed Sewer - Drucker's Sub

Sec along Wly edge AC  
 + Approx Wly Line Midway Drive  
 2+56 = Wly edge AC Midway Drive

Nearest  $\phi$  comes to Return  
 2+41.5 - 5' LT = curb Return SW cor.

2+34

2+00

1+93.02 =  $\angle$   $38^{\circ}31'$  to Right

Traffic Island Midway Drive  
 1+90.82 = SWly face curb  $3\frac{1}{2}$ ' wide conc

Island in  $\phi$  Midway -  
 1+87.02 = NEly face  $3\frac{1}{2}$ ' wide Conc Traffic

LT		$\phi$	RT
1.88 <sup>✓</sup>	2.26 <sup>✓</sup>	1.16 <sup>✓</sup>	1.0 <sup>✓</sup>
4 <sup>38</sup>	4 <sup>88</sup>	5 <sup>10</sup>	5 <sup>28</sup>
10 <sup>0</sup>	10		10
Top CB	along Prop Midway		
2.09 <sup>✓</sup>	1.41 <sup>✓</sup>	1.53 <sup>✓</sup>	
4 <sup>23</sup>	4 <sup>85</sup>	4 <sup>73</sup>	
5 <sup>L</sup>	5 <sup>L</sup>		
CB	9UT		
		1.38 <sup>✓</sup>	
		4 <sup>88</sup>	
		1.81 <sup>✓</sup>	
		4 <sup>45</sup>	
		1.81 <sup>✓</sup>	
		4 <sup>45</sup>	
		2.31 <sup>✓</sup>	1.81 <sup>✓</sup>
		3 <sup>95</sup>	4 <sup>45</sup>
		Top Island	$\phi$ 9UT
		1.44 <sup>✓</sup>	2.27 <sup>✓</sup>
		4 <sup>54</sup>	3 <sup>77</sup>
		9UT	$\phi$
		Top Island	Island
		6.26 <sup>✓</sup>	



Proposed Sewer Drucers

LT

RT

17

TP, starting BM.

6.02 0.24 ✓

2+82.72 = 1.38°44' 2T ✓ = 2+64.42 EP 2126  
71

2+81 - 6° RT = Wly end curb + vly end. Throat

2+71.11 8° RT = ∅ catch basin

1.7 ✓  
4  
5.86 - 5.6  
Hub ∅ ground

6 ✓ 71 ✓ 1.55 ✓  
5.7 5.55 4.71  
6° 6°  
IF Throat Top Ch

5.6 ✓ 6.9 ✓ 4.51 ✓  
5.7 5.57 10.83 ✓

6.26 X 11.8 grate 11.8



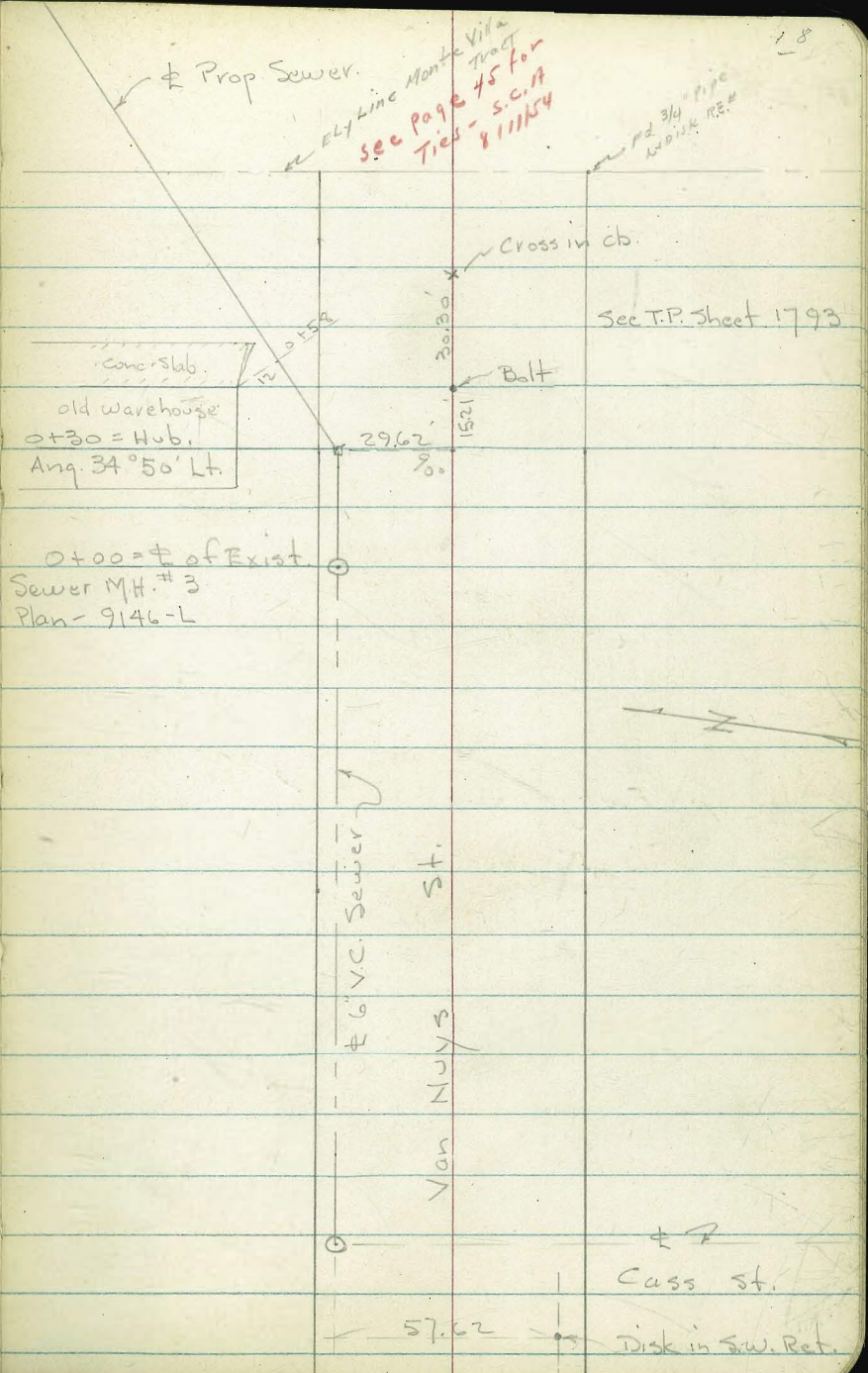
Beq. Survey for Prop. Sewer in Canyon  
Thru. P.L. 1781 To Muirlands Vista

W.O. 21234 - 4-14-54 F.O.

0+30 = Hub. Ang.  $34^{\circ} 50' Lt$

0+00 =  $\pm$  of MH

RECEIVED  
APR 20 1954





5+41.75 = Hub. - Ang.  $13^{\circ} 08' \text{ Lt.}$

*Should be 4+28.52 See page 45*

4+23.52 = Hub. = Int. S.L. of P.L. 1781

Every sta. ahead  
is 5' short. Reason

± of Prop. Sewer →

19  
Conc. Mon.  
S.E. Cor. 1781

~ Fd. Hub + Disk  
= Pot. on Top of  
Hill

P.L.  
1781

60+75

$35^{\circ}$

Conc. Mon.  
S.W. Cor. 1781



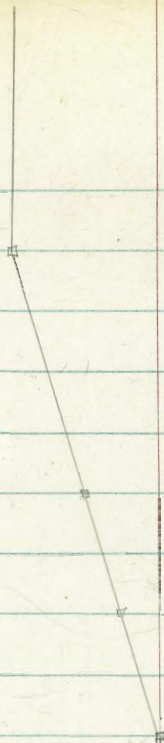
25 + 84.18 = Hub. Ang.  $18^{\circ}37'$  Rt.

20 + 61.19 = Hub. - P.O.T.

18 + 65 = stub. - P.O.T.

16 + 44.65 = Hub. - Ang.  $29^{\circ}33'$  Lt.

By white Bluff.





41 + 42.57 = Hub. - Ang.  $22^{\circ}19'15''$  Lt.

38 + 44.09 = Hub. - P.O.T. on Ridge

35 + 59.63 = Hub. = Int. with P.L. line = Sub. line  
= S.L. of Muirlands Vista

33 + 95.00 = Hub. Ang.  $6^{\circ}18'$  Lt.

30 + 41.53 = Hub. Ang.  $4^{\circ}49'30''$  Rt. =

Int. Sewer line from Muirlands Vista  
Sta. 8 + 93.53 - from West.

Sub. Line B  $59^{\circ}55'15''$

305.16

Sub. Line

Mon. S.E. Cor.  
P.L. 1774

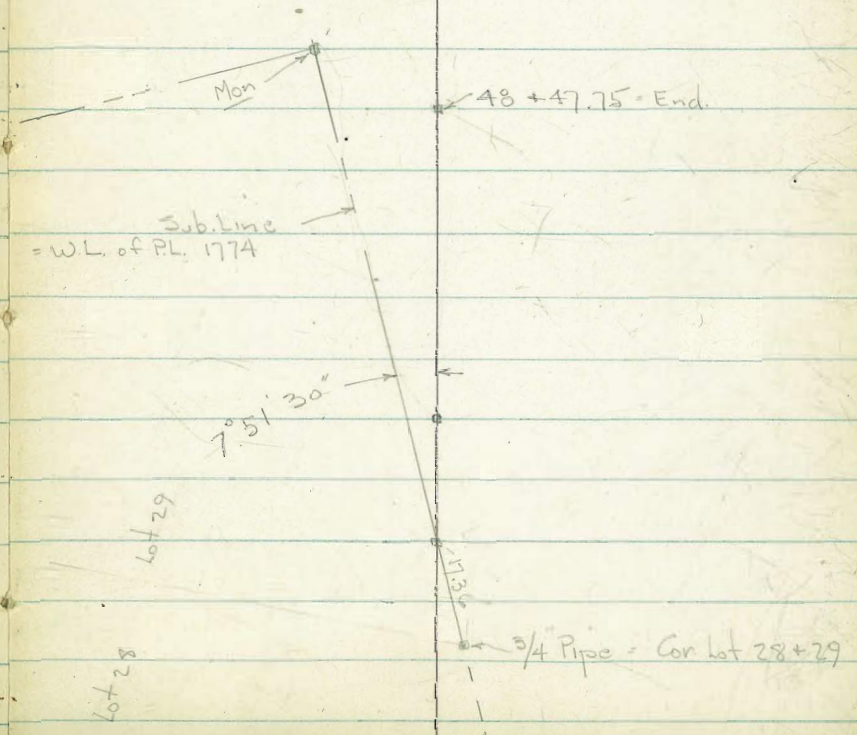
$76^{\circ}33'$



48+47.75 = Hub. = End. at Int. of 2 Canyons.

42+90.03 = Hub. = P.O.T.

42+32.13 = Hub. P.O.T. = Int with P.L. Line  
= E.L. of Sub: - Ang: 7°51'30"





Req. Levels along  $\pm$  of Prop. Sewer  
 from Van Nuys - E. of Cass to Muirlands  
 Vista. - See sketch - P. 18. = 4-21-54  
 1+05 = in wash

0+92

12.23 190.66

Set B.M. = (17) on  $\pm$  Top of Headwall 8.47 178.43  
 + 10' Conc. Headwall

0+67.5 - 25.2 Rt. =  $\pm$  of inlet of 48" R.C. culvert  
 old warehouse

0+64 - 2' Lt. = Near Cor. of Conc. Slab. for

0+30 - 3.3' Rt. = cb. face on Bul. de Sac.

T.P. 6.17 186.90 0.10 180.73

0+30 = Hub. = Ang. Pt.

0+00 = Exist. M.H. #3

B.M. 12.23 180.83

168.60 = S.W.

7 Mon. Cass + Van Nuys - Book 2056 - P. 66

Notes reduced  
 5-10-54  
 R. Larson

Lt.

$\pm$

Rt.

23

177.9

12.8

181.4

9.3

190.66

172.97

176.43

13.93  
 25.2  
 I.E. inlet

8.47  
 Top

180.8

181.79

181.0

6.1  
 91.

5.11  
 2 =  
 Top  
 conc.

5.9

180.79

180.30

6.11

6.60

3.3 = Top

cut.

186.90

180.73

0.10

on Hub.

179.95

174.92

0.88  
 Rim

5.91  
 I.E.

180.83



2+20

2+80

2+40

T.P. 13.02 202.50 118 189.48

2+20

1+80

1+65

1+50

1+35

1+18 = in Wash

Lt.

+

Rt.

21

188.3

14.2

22

+ Creek

192.2

10.3

10

193.5

9.0

193.8

8.7

188.9

13.6

202.50

187.5

3.2

185.8

4.9

187.2

3.5

188.5

2.2

185.7

5.0

178.5

12.2

190.66

196.8

5.7

40 = Tbc

190.1

12.4

10

191.3

+ 0.6

20 = Tbc

188.8

1.9

10

194.5

+ 3.8

10

191.1

+ 0.4

10



5+65

5+41.75 = Ang. Pt. - Sect 90° to forward Tang

T.P. 12.01 212.75 1.76 200.74 = Hub. 5+41.75

5+15

4+96 = Cross Barb wire fence

4+75

4+47

4+40 = † Creek

4+33

4+00

3+60

Lt.

±

Rt.

21

201.1

201.4

200.74

201.1

199.4

11.7  
4.5  
Toe

12.01  
on Hub.

11.7  
10

13.4  
17

212.75

† Creek

200.2

198.3

198.7

2.3

4.2

33 = † Creek

198.7

198.3

196.0

3.8  
40  
Toe

3.8

4.2

6.5

14  
† Creek

197.1

5.4

195.1

7.4

199.5

3.0

199.8

193.6

198.0

199.0

199.0

8.9  
70  
† Creek

4.5

3.5

3.5

190.8

197.1

197.3

197.6

12.7  
18  
† Creek

11.7  
10

5.4  
8

5.2

4.9  
30

202.50



8+00

7+80

7+65 =  $\neq$  Creek

7+55

7+40

7+00

6+40

6+05

5+95 =  $\neq$  Creek

5+40

Lt

211.2  
1.5  
25

209.9  
2.9  
208.6  
4.2

Rt.  
208.4  
4.0  
12

26  
206.8  
6.0  
18  
 $\neq$  Creek

205.2  
7.6  
207.7  
5.1

207.3  
5.5  
17

204.5  
8.3  
12

209.9  
2.9  
30

203.1  
9.7  
20

$\neq$  Creek  
206.1  
6.7  
10

207.4  
5.4  
206.6  
6.2

209.2  
3.6  
20  
Toe

208.2  
4.6  
30

201.2  
11.6  
15  
 $\neq$  Creek

203.7  
9.1  
10

204.0  
8.8

204.6  
9.2  
20

207.9  
7.9  
40

202.7  
10.1

200.2

200.5  
12.6

12.3  
212.75



T.P. 12.79 234.45 1.26 221.66

10+00

9+50

9+23

9+13 = E Creek

9+07

8+85

8+50

8+25

T.P. 12.51 222.92 2.34 210.41

217.4  
 5.5  
 78 = E  
 Creek  
 215.7  
 7.2  
 59  
 E Creek  
 220.1  
 2.8  
 62  
 218.3  
 4.6  
 50  
 222.9  
 0.0  
 218.3  
 4.6  
 215.5  
 212.1  
 10.8  
 214.7  
 8.2  
 215.1  
 7.8  
 217.2  
 5.7  
 25  
 213.2  
 9.7  
 8  
 212.7  
 10.2  
 211.2  
 11.7  
 209.7  
 13.2  
 40 = E Creek  
 208.5  
 17.4  
 26  
 E Creek  
 207.3  
 14.6  
 40  
 E Creek

8+10 - 10' Rt.  
= Chisel Cross on Rock

222.92



Lt.

Rt.

12+07

12+00 =  $\pm$  Creek

11+95

11+60

11+30

11+00

10+80

10+70 =  $\pm$  Creek

10+55

10+30

229.6

4.9

227.3

7.2

$\pm$  Creek

229.5

5.0

232.9

1.6  
20

229.4

5.1

227.5

7.0  
38

225.4

9.1

48 =  $\pm$  Creek  
= Toe

227.0

7.5

224.8

9.7  
10

225.5

9.0

224.0

10.5

43

$\pm$  Creek

224.3

10.2

221.4

13.1

$\pm$  Creek

224.7

9.8

218.2

16.3

80

$\pm$  Creek

224.8

9.7

230.0

4.5

25

234.45



Lt.

±

Rt.

29

13+70

13+60 = ± Creek

13+46

13+30

T.P. 12.75 245.82 1.38 23 3.07

12+75

12+36

12+30 = ± Creek

12+23

12+10

236.4

9.4

234.6

11.2

± Creek

237.4

8.4

241.2

236.7

236.3

235.3

232.1

4.6  
30

9.1  
10

9.5

10.5  
45

12.7  
50

On Rock - 12+73

245.82

± Creek  
± Toe

234.0

233.1

233.6

231.1

0.5  
45

1.4

0.9  
40

3.4  
50

± Creek  
± Toe

231.3

3.2

229.4

5.1

± Creek

230.6

3.9

228.9

230.1

5.6  
25

4.4

± Creek

234.45



16+70

16+44.65 = Ang. Pt.

16+00

T.P. 12.06 257.24 044 245.18

15+50

15+00

14+60

14+50 = ± Creek

14+20

13+85

Lt.

±

Rt.

30

253.7

3.5  
15

252.7

4.5

250.1

7.1  
4.5

247.7

9.5  
6.5

245.3

11.9  
7.0

± Creek  
± Toe

250.34

6.9  
on Hub

245.7

11.5  
3.0

245.9

11.3

246.0

11.2  
15

244.0

13.2  
35

242.7

14.5  
42

± Creek  
± Toe

257.24

243.5

2.3  
5.0

244.0

1.8

243.2

2.6  
15

240.9

4.9  
20

± Creek

242.3

3.5  
5.0  
Toe

241.8

4.0

241.8

4.0  
10

239.8

6.0  
15

± Creek

240.4

5.4

237.5

8.3

239.5

6.3

239.5

6.3

239.2

6.6  
10

244.0

1.8  
3.8

236.2

9.6  
2.5

237.3

8.5  
2.0

237.0

8.8  
1.3

236.6

9.2  
5

238.3

7.5

237.4

8.4  
1.5

238.6

7.2  
4.5 = Toe

245.82



19+10 = E. Creek

18+95

18+65 = P.O.T. Stub

18+50

18+00

T.P. 13.27 270.02 0.49 256.75

Set B.M. - on Rock - 17+15 - 4 ft. 3.37 253.87

17+40

17+12

17+05 = E. Creek

16+95

Lt.

E

Rt.

31

260.7

9.3

E. Creek

262.7

7.3

256.0

14.0

95

E. Creek

259.6

8.47

94.6

260.9

9.1

253.4

16.6

57

E. Creek

258.1

11.9

50

257.4

12.6

270.02

264.0

C.O.

40 = Toe

258.1

11.9

10

250.9

6.3

75

E. Creek

252.9

4.3

65

254.9

2.3

251.9

5.3

40 = Toe

251.3

5.9

248.1

9.1

251.0

6.2

257.24



21+20

20+85

20+80 = ± Creek

20+75

20+50

T.P. 12.48 282.11 0.37 269.63

20+00

19+60

19+37

19+27

Lt.

±

Rt.

32

271.9

10.2  
20

272.4

9.7

272.2

9.9  
20

269.8

12.3  
27 = ± Creek

270.0

12.1

268.3

13.8

± Creek

271.2

10.9

265.4

14.7  
85

± Creek

267.2

14.9  
77

271.6

10.5

282.11

274.1

8.0

15 = Toe

263.0

7.0  
36

± Creek

265.6

4.4  
25

261.7

8.3  
10

± Creek

267.9

2.1

264.0

6.0

269.4

0.0

15

268.7

1.3

23 = Toe

263.1

6.9

261.1

8.9

270.02



Lt.

±

Rt.

285.1

97

281.0

282.5

284.0

283.9

284.6

13.8

12.3

10.8

10.9

10.2

±Creek

53

55

35

25 = Toc

278.6

282.2

16.2

12.6

10

±Creek 294.81

277.7

281.0

281.3

281.7

4.4

1.1

0.8

0.4

20

13

10

±Creek

275.0

277.8

279.5

282.1

7.1

4.3

2.6

0.0

55

50

20

±Creek

273.8

276.0

278.5

8.3

6.1

3.6

45

30

±Creek

274.3

78

271.4

10.7

±Creek

273.7

84

282.11

23+80

23+50

23+10

T.P. 13.32 294.81 0.62 281.49

23+00

22+50

22+00

21+77

21+67 = ±. Creek

21+57



Lt.      ♀      Rt.

27+10

26+80

26+35

T.P.      11.87      305.33      135      293.46

25+84.18 = Ang. Pt. - Sect 90° to Back Tang.

25+50

Set B.M. on Rock      5.56      289.25  
13' Lt. ↗  
25+00 ↘

24+50

24+20

23+90 = ♀ Creek

298.1

297.7

292.3      295.1      296.6      300.2

13.0      10.2      8.7      5.1  
60      50      50 = Toe  
♀ Creek      305.33

289.3      293.2      293.46      295.4

5.5      1.6      1.35      + 0.6  
35      30      on Hub.      50  
♀ Creek

291.9

287.1

291.1

292.2

7.7      3.7      2.6  
40      15  
♀ Creek      288.6      290.0

285.0      288.8

9.8      6.0      6.2      4.8  
35      20      20 = Toe  
♀ Creek

287.4

283.3

11.5  
♀ Creek  
294.81



Lt.

±

Rt.

Fence - (3 Posts)  
Set B.M. = on Rock By Cor. of 3.04 313.04

29+50

29+00

28+60 = ± Creek = y of 2 creeks

28+30

T.P. 11.84 316.08 1.09 304.24 = lat 28+00

27+85

27+50 = ± Creek

27+44

27+35

27+20 = ± Creek

		306.5	309.6	311.3	307.3
		9.6	6.5	4.8	8.8
		17		15	32
		± Creek = Main			± Creek
311.1	307.7	304.6	307.2	305.4	308.9 310.1
5.0	8.4	11.5	8.9	10.7	7.2 6.0
59	15	6		5	20 50
Toe		± Creek		± Creek	
			302.8		
			13.3		
			305.2		
			10.9		
			316.08		
		300.7	303.0	302.7	
		4.6	2.3	2.6	
		22		35	
		± Creek			
			298.9		
			6.4		
			± Creek		
			301.2		
			4.1		
		300.9	300.6	297.7	
		4.4	4.7	7.6	
		25		20	
			296.2	± Creek	
			9.1		
			305.33		



32+15

31+90

31+60 = ± Creek

31+40

31+10

30+70

30+41.53 = Ang. Pt. = Sewer Line from Sub.

T.P. 12.25 327.81 0.52 315.56

30+10

29+73 = ± Creek + Cross Barb wire Fence

322.5

5.3

317.8

319.4

321.6

323.1

10.0  
4.5  
± Creek

8.4  
3.3

6.2

4.7  
20 = Top

316.1

11.7

± Creek

318.0

9.9

317.6

10.2

322.8

318.2

317.3

311.5

5.0  
50

9.6

10.5  
20

16.3  
35

± Creek  
Top of Bank

317.98

9.83 = on Stub.

316.83

317.28 = 13.53

10.98

on Line =  
8+80 = Mill.

327.81

317.1

315.0

309.1

+1.0  
40

1.1

7.0  
2.5

307.0

± Creek + Top of  
Bank

9.1

316.08



T.P. 13.16 352.16 0.78 339.00 = Pole

35+05 = ± Creek

34+90

34+66 - 14.3 Rt. = ± P. pole # 0.78 339.00  
61960

34+65

34+20 = ± Creek

33+95 = Angl Pt. = Sect 90° to Back Tang.

33+45

T.P. 12.71 339.78 0.74 327.07 = Lat h - 33+00

33+00

32+45

32+20 = ± Creek

Lt.

±

Rt.

37

333.4

6.4

332.5

335.0

7.3

4.8

22

± Creek

333.9

332.6

334.9

340.0

59

7.2

4.9

+0.2

36

22

20

Toe

± Creek

329.0

10.8

± Creek

332.9

329.99

328.3

329.7

6.9

9.79

11.5

10.1

20

on Hub.

6

18

332.7

329.3

± Creek

Toe

7.1

10.5

14.4

11.9

20

339.78

± Creek

20

Toe

328.4

327.1

323.6

325.0

+0.6

0.7

4.2

2.8

15

6

± Creek

35- Toe

325.1

323.8

321.5

2.7

4.0

6.3

20

40

± Creek

318.9

8.9

± Creek

327.81



37+00

36+80

36+60

36+40 =  $\Phi$  Creek

36+00 =  $\Phi$  Creek

35+91

35+80

35+50 =  $\Phi$  Creek

35+46

35+30

38

	Lt.	$\Phi$	Rt.	
	360.7	353.2	350.3	346.5
	+8.5	+1.0	1.9	5.7
	20		5	23
		350.1	348.8	$\Phi$ Creek
		2.1	3.4	345.4
			10	6.8
		352.4	348.8	25
	+0.2	3.4	347.0	$\Phi$ Creek
	15		5.2	344.3
	352.6	347.3	15	7.9
	+0.4	4.9		45
	20	7	$\Phi$ Creek	$\Phi$ Creek
			342.2	344.8
			$\Phi$ Creek	7.4
				20
			329.8	
			12.4	
			$\Phi$ Creek	
			344.4	
			7.8	
			338.3	343.4
			13.9	344.0
			8.8	8.2
			17	20
			$\Phi$ Creek	
			+Toe	
			337.4	
			14.8	
			$\Phi$ Creek	
			340.1	
			12.1	
			344.6	340.8
			7.6	337.9
			15	335.3
				16.9
				30
				$\Phi$ Creek
			352.16	



39+80

39+35 ✓

38+90

T.P. 11.64 376.47 0.33 364.83

38+50

38+43- 14' Rt. =  $\Phi$  P. Pole # 61959 1.80 363.36 = spike = BM.

38+20

38+08

37+65

37+50

T.P. 13.26 365.16 0.26 351.90

37+20

Lt. 365.3  $\Phi$  362.7 Rt. 359.1

11.2 20 12.8 40  $\Phi$  Creek 355.8  
363.0 359.6 20.7  
13.5 20 16.9 23  $\Phi$  Creek

370.8 363.7 362.2 361.5 355.8 356.7  
5.7 12.8 14.3 15.0 21.7 19.8  
25 13 4 10 20  
376.47  $\Phi$  Creek

368.1 364.5 360.9 352.4  
+ 2.9 0.7 4.7 12.8  
20 20 49  $\Phi$  Creek  
363.2

366.9 359.7 355.4 350.1  
+ 1.7 5.5 9.8 15.1  
20 15 52  $\Phi$  Creek  
358.9 355.6

6.3 9.6  
20  $\Phi$  of wash to  
361.2 354.1 347.4  
4.0 11.1 17.8  
20 37  $\Phi$  Creek  
365.16

350.4

1.8  
352.16



42+15

41+70

41+52.5 - 17.8 Rt. =  $\pm$  P. Pole # 6988

T.P. 12.79 388.65 0.61 375.86

41+42.52 = Ang. Pt. - Sect 90° To Back Tang

41+25

41+00 =  $\pm$  Creek

40+78

40+50

40+20

39+93 =  $\pm$  Creek

	Lt.	$\pm$	Rt.
369.9	375.0	375.7	377.8
18.8	13.7	13.0	10.9 = Toe
27	15		15
$\pm$ Creek			
368.3	375.6	378.0	381.7
20.4	13.1	10.7	7.0
40	15		25 = Toe
$\pm$ Creek			

388.65

367.6	375.86	382.3
8.9	0.61	+ 5.8
46	on Hub	25
$\pm$ Creek		

366.1 369.8

10.4 6.7

14  $\pm$  Creek

369.1

365.0

379.8

7.4

11.5

+ 3.3

20

$\pm$  Creek

30

Toe

370.2

377.6

6.3

+ 1.1

30

363.2

368.3

13.3

8.2

29

$\pm$  Creek + Toe

362.9

364.1

364.6

13.6

12.4

11.9

35

20

$\pm$  Creek

362.2

+ Toe

14.3

$\pm$  Creek

376.47



44+36 = ± Creek

44+25

44+00

43+75

43+37 = ± Creek

43+17 - 15' Rt. - ± P. pole #6 1957

43+15

43+07 = ± Side wash

43+00

42+80

42+55

Lt.

±

Rt.

41

380.6

8.1

388.2

± Creek

383.0 380.9

381.4

0.5  
15

5.7

-7.8

7.3

387.7

380.7

± Creek  
379.5

382.5

1.0

8.0

9.2

6.2

382.3

380.8

± Creek  
375.7

383.4

384.3

2.4

7.9

13.0

5.3

4.4

383.1

374.3

± Creek  
382.0

385.3

2.8  
Toe

5.6

14.4

6.7

2.4

20

± Creek

8

20

380.2

8.5

378.0

10.7

383.9

389.4

4.8

+ 0.7

30

372.6

380.8

383.4

16.1

7.9

5.3

33

15

± Creek

370.7

378.8

380.3

383.1

18.0

9.9

8.4

5.6

40

15

20

± Creek

389.65



46+40

46+00

45+76-22 Rt. = ± P. pole # 61956

45+65

45+45

45+40 = ± Creek

45+25

T.P. 13.22 401.15 072 387.93

45+05

44+77 = ± Creek

44+60

Lt.

±

Rt.

42

388.2

392.4

397.8

13.0

8.8

3.4

10  
± Creek

20

392.5

387.7

395.2

397.2

401.2

8.7

13.5

6.0

4.0

0.0

25

11

12

15

± Creek

392.2

399.4

9.0

0.8

20

387.1

388.8

14.1

12.4

27

± Creek

384.6

16.6

± Creek

387.8

13.4

401.15

390.7

386.1

386.6

383.2

+2.0

2.6

2.1

5.5

20

10

21

382.9

± Creek

5.8

380.7

± Creek

383.9

383.8

387.6

8.0

4.8

4.9

1.1

20

8

12

± Creek

388.65



48+20

48+13 -  $\oplus$  Creek

48+05

T.P. 11.02 410.06 2.11 399.04

47+70

47+35

47+10

47+00 -  $\oplus$  Creek

46+66 =  $\oplus$  Creek

46+60

Lt.

$\oplus$

Rt.

43

403.2

6.9  
40.  
in  $\oplus$  of side  
wash

396.4

13.7

394.4

15.7

$\oplus$  Creek

397.9

12.2

410.06

392.8

395.8

397.2

398.9

402.5

8.4 5.4  
24 17  
 $\oplus$  Creek

4.0

2.3

+1.3

15

20.

391.9

394.9

397.0

9.3  
17  
 $\oplus$  Creek

6.3

4.2

15.

393.2

8.0

395.9

393.2

390.4

394.7

396.7

5.3 8.0  
20 5

10.8

6.5

4.5

$\oplus$  Creek

5

20

389.2

17.0

$\oplus$  Creek

391.5

9.7

401.15



Lt.

±

Rt.

44

Set B.M. in Pole By End.

3.64

406.42.

48 + 47.75 = End

405.2

402.4

398.75

397.2

399.1

4.9

7.7

11.31

12.9

11.0

15

3

on Hub.

12

30

410.06

± Creek

Toe



Additional ties Meirlands ety out fall

Sewer - See page 19.

W o # 21224

Aug 11, 1954

Ref - Page 19

C. Allen

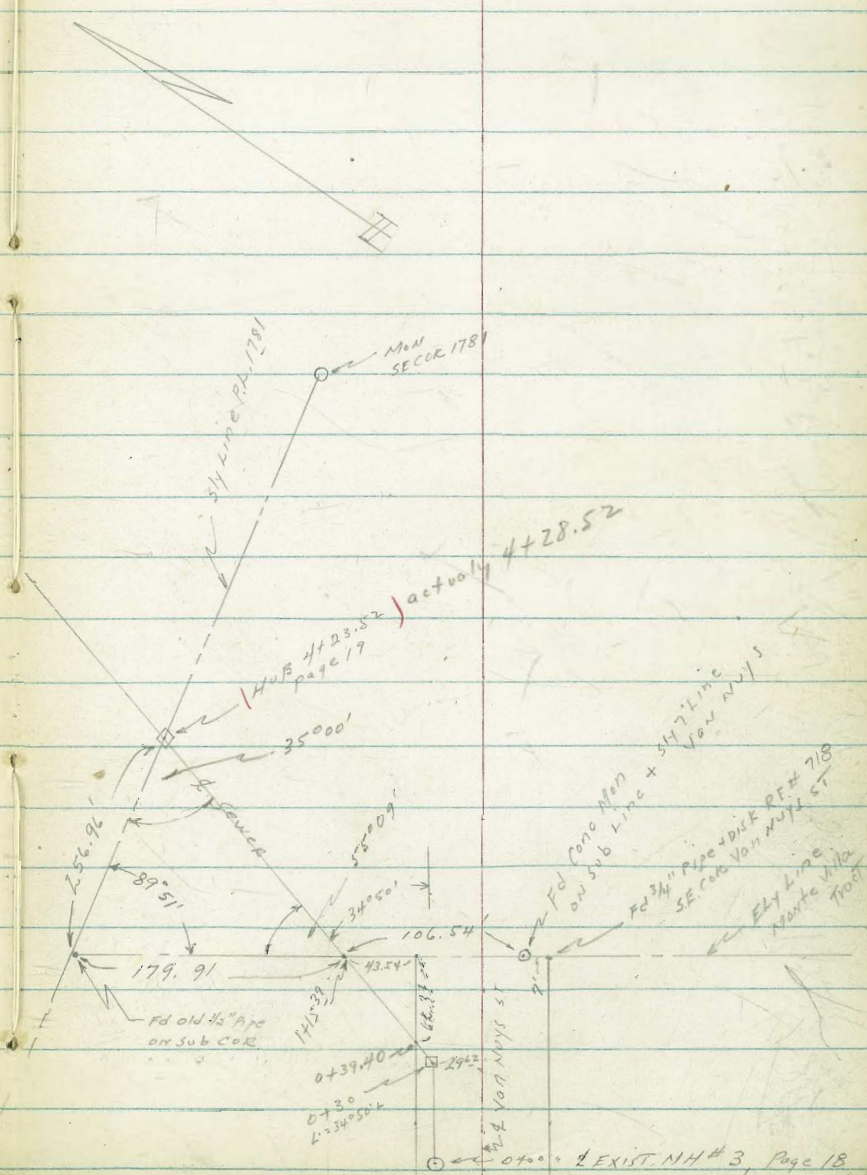
Dwg 9146-2, TP 1793

D. Sisson

Maps # 928, 839

C. Powell

INDEXED  
AUG 12 1954





See Page 47.

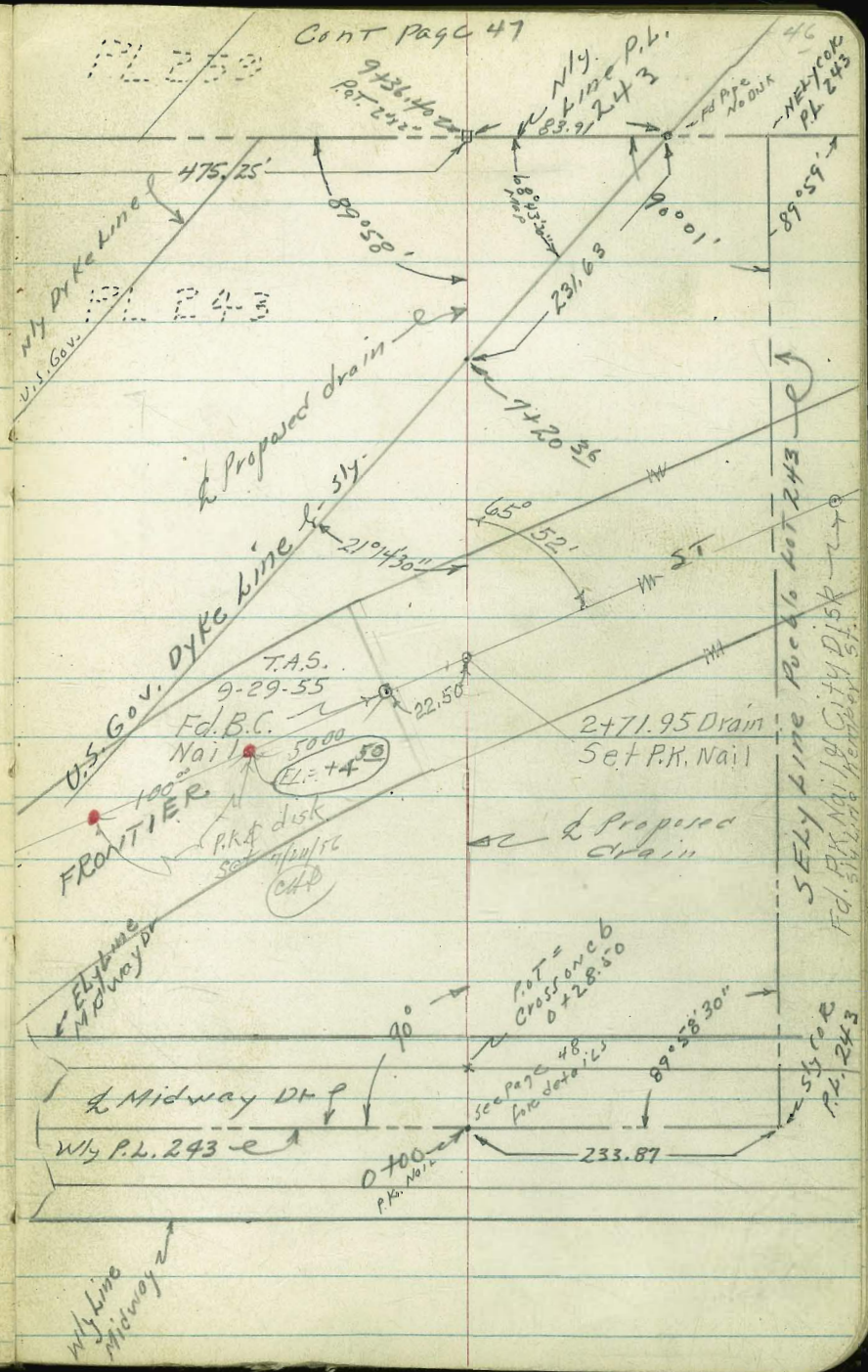
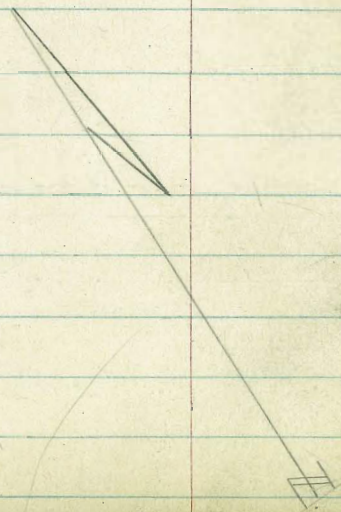
LAPWAI ST

Mt Wly Cor 259

Proposed drain, Midway drive. Thru Pueblo  
Lots 243, 259, and 258 to intersection  
Lapwai St + Nashville St in Drucker  
Subdivision.

Pueblo Lot Line angles from FB 1526-25  
+ Tie point Sheet 637-A

425.35' Measured along Wly Line Knoxville  
St is Per Map # 1497- shown different  
on survey By N. Davason



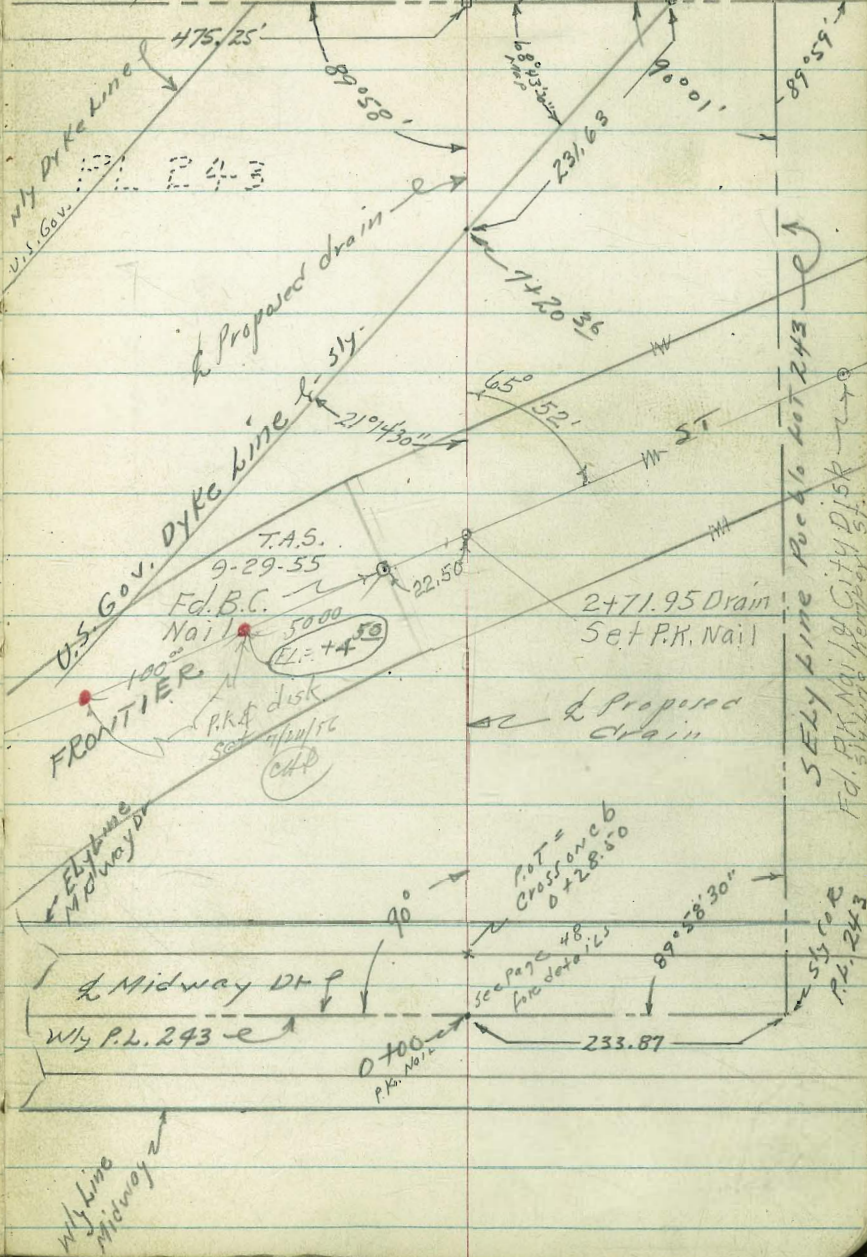
Cont Page 47

FL 259

9+36.40  
P.T. 252

N14. line P.L.  
83.92  
243

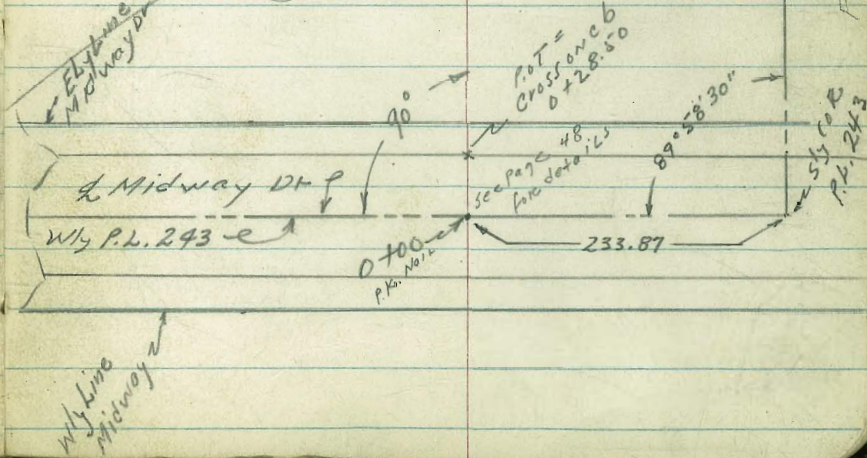
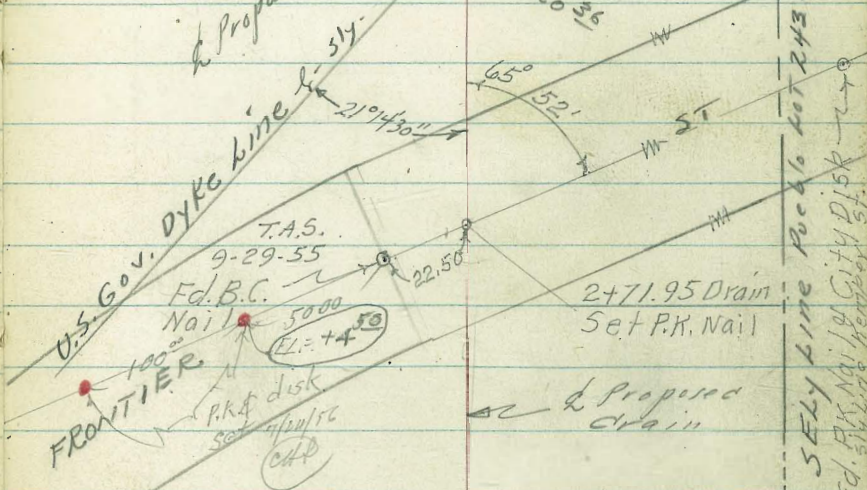
46  
NEW YORK  
P.L. 243



Wly Dyke line  
U.S. Gov.

475.25'  
89°58'  
Proposed drain

90°01'  
231.63  
90°01'  
89°59'





MAXWELL ST

U.S. Govt dyke  
line - San Diego  
River channel

15' Alley

KING ST

Alley = 15'

PL 258

LAPWAI ST

See Page 48 Portion

26+76.83

Why most  
corner  
pt 259  
Ed Mon

KNOXVILLE ST  
54 line Pt. 258  
w/aly line Pt. 259

135.00

425.91  
(map)  
132.00

132.00

900.00

Stub P.O.T.

18+63.72-57

20+19.59

195° 33' 45"

900° 30"

50'

100°

E of Survey &  
U.S. Govt Dyke  
Line - Sky  
dyke

MASHVILL

INDEXED  
JER  
JUL 25 1955

47

Proposed Drain

P.O.T. Stub  
16+00

set 1/4" disk  
8-26-56 C.H.S.

13+63.00  
set 2" x 2"

89° 49' 30"

Proposed  
Drain

PL 259

475.25

PL 243

900.00

97+36.40  
P.O.T.

83.91

U.S. Govt Dyke Line  
54'

100.00

Prop.  
drain

MUNTEH Rte. R.L. 2+3

cont from page 46







Levels + Tops. Proposed Drain  
See sketches Page 46-48

$\left. \begin{array}{l} 12^{\circ} \text{ RT} = \text{ely end Throat} \\ 2^{\circ} \text{ LT} = \text{why end Throat} \end{array} \right\} \text{Modified B-2 Inlet}$   
 wing to cly-  
 0+28 = face Nly Curb

0+00 = Midway Drive -

$\left. \begin{array}{l} 8^{\circ} \text{ RT} = \text{ely end of Throat} \\ 6^{\circ} \text{ LT} = \text{why end of Throat} \end{array} \right\} \text{Modified Type A-2 Catch Basin}$   
 15' throat  
 0-28 + sly Cor & Midway Drive

	5.23	6.28	10.26	1.05
TP	7.83	11.31	2.55	3.48
BM	5.79	6.03		0.24

LT	B.L.	RT	49
		0.38	0.94
		5.90	5.34
		50	50
		9UT	T.C.

0.82	1.09	0.38	-0.93	0.34	1.08	0.41	1.10
5 <sup>-46</sup>	5 <sup>17</sup>	5 <sup>90</sup>	7 <sup>21</sup>	5 <sup>94</sup>	5 <sup>20</sup>	5 <sup>87</sup>	5 <sup>18</sup>
50	25	25	2	9UT	2	120	120
9UT	T.C.	9UT	Bottom Box	Top CB		9UT	Topcb
Drive No							
Curb				1.38			
				4.90			
				A.C.			

1.29	0.71			0.38	1.00
4.99	5.57			5.90	5.28
50	50			50	50
T.C.	9UT			9UT	T.C.

1.08	0.08	-1.93	0.00	1.05	0.05	1.03
5 <sup>20</sup>	6 <sup>20</sup>	8 <sup>21</sup>	6 <sup>28</sup>	5 <sup>23</sup>	6 <sup>23</sup>	5 <sup>25</sup>
65	65	2	9UT	2	85	85
Topcb	9UT	Bottom Box	Top CB		9UT	Topcb

6.28 X

= X top Curb over Catch basin 0-28<sup>U</sup>

Nashville St - Page 14.  
Rim exist Sewer Manhole - Jupiter +



Drain cont.

LT

R, L,

RT

58

0+82-0<sup>5</sup> RT= begin 8' high board fence

0+80-1<sup>2</sup> LT= 10" Tele pole #463827H

2.06 1.5

4<sup>22</sup> 4<sup>8</sup>

Top A.C.  
Cb - 4

0+79= end 6" Curb - Curb belongs to  
Ambulance service

2.00 2.0

4<sup>28</sup> 4<sup>3</sup>

Top A.C.  
Cb

0+75-

0+66-1<sup>5</sup> LT= 1/2 deadman-

1.72 1.83

4<sup>36</sup> 4<sup>45</sup>

Top Top  
Curb

0+59= begin 6" curb (conc)

1.6

1.5

1.4

0+50

4<sup>7</sup>

4<sup>8</sup>

4<sup>9</sup>

0+43= begin A.C. Parking - Ambulance  
Standard

10  
A.C.

0NA.C.

10  
A.C.

0+42<sup>5</sup> 5<sup>0</sup> LT= 1/2 6" Iron Pipe sign

0+36-3<sup>9</sup> LT= 1/2 4" Iron pipe lite standard

0+30= 4<sup>6</sup> LT= 1/2 12" Power pole #JP4654

6.287



Drain Survey cont

1+25

1+23.30 - P.O.T. P.K. Nail in A.C.

8° LT = sly of conc slab } To show

1+12 - 10° LT = sly of conc slab } Jog.

2' RT = begin 5' Picket fence

1+07 - 2' RT = end frame office Bldg

Sits on slab - Drive in Cafe  
1+00-13° LT = begin stucco Bldg -

for drive in cafe  
0+96-10° LT = begin Conc Slab

Bldg. - 15' deep  
0+87 - 2° RT = begin Frame office

0+87 - 2° RT = end 8' Board Fence

LT

B.

L.

RT

51

2.5

3.8

3.29

2.8

2.99

3.5

10.8

10.8

Top  
Slab

A.C.

2.5

3.8

2.1  
9r.

3.43

2.5

2.85

3.8

13.6  
Floor

3.34

2.68

2.94

3.60

10.6  
Top  
Slab

10.6  
A.C.

2.3

3.53

4.0

2.75

2.5

2.5

9r

Floor

6.28 T



2+14- } 2<sup>3</sup> RT = begin 6' chain link fence  
 2<sup>3</sup> RT = end 8' high board fence

2+03- 1<sup>3</sup> LT = 4" iron pipe sign Standard

2+00

2.9

5.8

8.68

TP 5.13 8.68 2.73 3.55

2+00

2.8

3.5

1+75

1+58- } 2<sup>0</sup> RT = begin 8' high Board fence <sup>with sign</sup>  
 1<sup>4</sup> RT = end 5' Picket fence

1+80

2.6

3.2

Curving away from Base Line -

15<sup>0</sup> LT = sty wall of Drive in (stucco)

1+39- 7<sup>5</sup> LT = end Conc slab

3.56 2.8

27<sup>2</sup> 3<sup>5</sup>

7<sup>5</sup> 7<sup>5</sup>  
 Topslab A.C.

6.28 X



Drain cont

LT

B.L.

RT

53

2+70± = 2 A.C. Paving strip Frontier ST

405

463

A.C.

3.70

498

A.C.

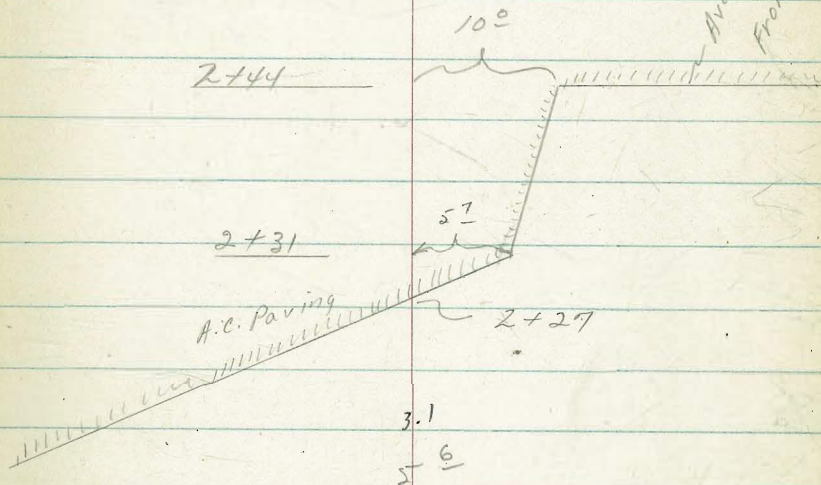
2+50

2+29-8<sup>2</sup> RT = 9 10" Telephone Pole #P3867  
+ Power

2+27 - Begin A.C. Frontier ST -

2+25

3<sup>8</sup> RT = end 6' chain link fence  
2+20± = approx sly line Frontier ST



3.1

5.6

3.2

5.5

8.687



Drain

3+51- 12<sup>8</sup> LT = 2 dead man

3+50

TP 4.93

8.23 5.38

3.30

3+28 = Top drainage ditch

3+23 = Bottom drainage ditch

3+00

2+94<sup>5</sup> = Ely edge H.C. Paving  
Frontier ST

LT

B.L.

RT

54

3.0

8<sup>2</sup>

8.23 X

# 518976-H

Nail in Power pole

11<sup>2</sup> RT of Sta. 3+62

2.6

4<sup>1</sup>

0.7

8<sup>0</sup>

3.4

5<sup>3</sup>

3.33

5<sup>35</sup>

A.C.

8.68 X



Drain Survey Cont

IT

B.L.

RT

SS

4+25

3.6

4.6

4+00

3.2

5.0

3+85 - 35° RT = Cor. House - Standard

Project Temporary P.H.A

3.8

4.8

4.9

3.4

35°

35°

9"

FLOOR

3+84-15° RT = of leadman

3.1

3+75

5.1

3+65 - 10° RT = Cor. House - Standard Temporary

Project House - P.H.A.

4.53

3.2

3.70

5.0

10°  
Floor

10°  
9"

3+62 - 11° RT = of 10" P.W. Tel pole # 5189764

2.83

3+60 = of 3' conc walk - nly + sly

5.40

conc  
walk

8.23 T



Drain cont

LT

BL

RT

SB

5+00

4+92-12<sup>2</sup> RT =  $\phi$  10" pole # 82  $\frac{30}{73}$

4+87 =  $\phi$  deadman on d.

4+75

3.2

5.0

3.3

4.9

4.68 3.5

3.55 4.7

5.35 5.35  
Floor 9v

Project House P.H.A. (Sec 3465)  
4+61-53<sup>2</sup> LT = Cor. House - Standard Temp.

1 Floor - 4 families

Temporary P.H.A. (Sec 3485)

4+53-4<sup>5</sup> RT = Cor. House - Standard

3.7 4.73

4.5 3.50

4.5 4.5  
9v Floor

4+80

3.7

4.5

4+45 = Sly edge of NEL, + Swly Conc Walk

2 5' inside conc.  
4+39 = Nly edge of NEL to Swly Walk

3.60

4.63

8.23



Drain cont

6+75

6+50-90° LT = toe dyke -

6+25

6+00-111° LT = toe dyke - <sup>River Channel -</sup> old San Diego

5+75

5+50

5+25

LT

BL

ET

ST

2.7

5.5

1.0

1.2

0.1

2.9

72

94

83

5.3

90

52

50

Toe Dyke

Bottom Ditch

3.0

5.2

1.7

0.5

1.0

1.5

3.0

65

77

92

67

5.2

111

100

72

50

Toe Dyke

Bottom Ditch

Bottom Ditch

3.0

5.2

3.2

5.0

3.2

5.0

8.25 X



Drain cont

7+75

TP 7.28 10.06 5.45 2.78

7+73. 7° RT = 2' 12" Power pole # C3465

7+50 - 50° LT = Toe dyke

7+25

7+20<sup>35</sup> Dyke - intersects sky R/W Line

7+00 - 69° LT = Toe dyke

LT

BL

RT

SP

0.0

10<sup>L</sup>

10.06

Nail in pp # C3465 7° RT of station 7+73

1.3

-0.8

0.7

2.6

69

9°

75

56

50

17

25

1.4

6.8

1.5

6.7

P.I.

1.2

-0.9

2.2

7°

9°

6°

69°

34

LT = Toe

dyke

8.23 T



Drain cont

9+36.40 = intersection Nly Line P.L. 243

9+12 = Top Dyke - dyke is 16' wide

8+75 = Toe dyke

8+50 - 16° LT = Toe dyke

8+25

8+00 - 35° LT = Toe dyke

LT

B.L.

RT

596

8.49

157

ON HUB  
94 same

23

8.8

8.9

2.9

-1.1

78

13

12

72

112

38

18

12

47

Toe  
dyke

Topdyke

Toe  
dyke

Bottom  
ditch

8.9

2.1

-0.9

0.9

2.5

12

80

110

92

76

16  
Top  
dyke

34  
Bottom  
ditch

3.4

1.0

-0.8

1.7

67

91

109

84

12

Toe dyke

22  
Bottom  
ditch

50

0.5

96

2.8

2.0

0.9

-0.6

2.8

73

81

92

107

73

35

22

21

50

10,067



Drain Cont

10+50-28<sup>0</sup> RT= Toe dyke

10+20

10+07

10+00 - ON Roadway to Top of Dyke

9+85 = Toe of dyke

9+75

9+52 = Nly top Dyke

LT

B.L. RT

60

-0.9	0.5	2.1	8.9
11 <sup>0</sup>	9 <sup>0</sup>	8 <sup>0</sup>	1 <sup>2</sup>
50		28 <sup>0</sup>	43
		Toe Dyke	Top Dyke

2.1  
8<sup>0</sup>

4.7  
5<sup>4</sup>

2.7	2.7	4.5	7.5	7.9	2.2
7 <sup>4</sup>	7 <sup>4</sup>	5 <sup>6</sup>	2 <sup>6</sup>	2 <sup>2</sup>	7 <sup>9</sup>
50	28		22	37	60
			Top Dyke	Top Dyke	Toe Dyke

5.0  
5<sup>1</sup>

5.4  
4<sup>7</sup>

1.3	1.8	8.7	8.9	1.8	1.1
8 <sup>8</sup>	8 <sup>3</sup>	1 <sup>4</sup>	1 <sup>2</sup>	8 <sup>3</sup>	11 <sup>2</sup>
25	15		17	27	65
	Toe dyke	10.06	Top Dyke	Toe Dyke	Bot Top ditch



Drain cont

RT

B.L.

RT

61

11475

1.6

6 Z

8.26 T

TP - 4.42

8.26

6.22

3.84

Nail in Power Pole # 2799 - See Below

11474 - 218 L T = 2 16" Power pole # 2799

2.8

1.4

0.6

1.5

11450

73

8 Z

10 Z

86

50

38

50

11435

1.5

8 E

11425

0.1

10 Z

2.1

1.0

1.1

1.2

2.8

11400 - 58° RT = Toe dyke

8°

9°

11°

11°

73

50

18

8

58

Toe dyke

10475

1.0

11

10.06 T



Drain Cont

13+25

13+00

12+92

12+75

12+50

12+25

12+00

LT

B.L.

RT

62

0.5

7<sup>0</sup>

0.3

0.7

2.1

2.5

8<sup>0</sup>

7<sup>6</sup>

6<sup>2</sup>

5<sup>8</sup>

50

10

50

3.1

2<sup>2</sup>

3.0

5<sup>2</sup>

0.2

-0.1

2.7

2.6

1.4

8<sup>2</sup>

8<sup>4</sup>

56

57

69

50

40

26

50

2.6

57

2.6

2.3

-0.8

57

60

92

50

50

8.26



Drain Cont

14+50

14+35

14+30

14+25

14+00

13+75

13+63.00 L Section taken on split

13+50

LT

BL

PT

63

-0.4

8<sup>2</sup>

50

-0.2

8<sup>5</sup>

-0.2

8<sup>5</sup>

-1.3

9<sup>6</sup>

-0.4

8<sup>2</sup>

0.2

8<sup>1</sup>

50

0.9

7<sup>4</sup>

0.2

8<sup>1</sup>

0.2

8<sup>1</sup>

50

0.26

8<sup>00</sup>

Hub  
9.10.11

0.0

8<sup>3</sup>

8.26 x

0.7

7<sup>6</sup>

50

0.0

8<sup>3</sup>

50

0.9

7<sup>4</sup>

30

3.1

5<sup>2</sup>

50



Drain Cont

on stub at  
P.O.T. 16400

TP 5.69 8.32 5.63 2.63

16400 = Begin Grid fore pump station

15+75

15+50

15+25

15+00

14+75

14+62

LT

13.4

RT

64

8.32 T

3.3 2.8 2.9 2.6 2.7 2.5 2.6 3.1 3.0

5<sup>0</sup> 5<sup>5</sup> 5<sup>4</sup> 5<sup>7</sup> 5<sup>6</sup> 5<sup>8</sup> 5<sup>7</sup> 5<sup>2</sup> 5<sup>3</sup>  
100 75 50 25 25 50 75 100

3.0

5<sup>3</sup>

3.3

3.1

3.3

5<sup>0</sup>  
50

5<sup>2</sup>

5<sup>0</sup>  
50

3.3

5<sup>0</sup>

2.9

3.1

4.0

3.7

5<sup>4</sup>

5<sup>2</sup>

4<sup>3</sup>

4<sup>6</sup>

50

42

50

2.8

5<sup>5</sup>

0.3

0<sup>0</sup>

8.26 T



Drain cont

L.T.

B.L.

R.T.

65

17+75

2.0	2.3	2.5	2.7	2.9	3.3	3.1	3.4	3.6
6 <sup>2</sup>	6 <sup>0</sup>	5 <sup>8</sup>	5 <sup>6</sup>	5 <sup>4</sup>	5 <sup>2</sup>	5 <sup>2</sup>	4 <sup>9</sup>	4 <sup>7</sup>
100	75	50	25	25	25	50	75	100

17+50

2.1	2.1	2.1	2.1	2.8	3.0	3.3	3.3	3.3
6 <sup>2</sup>	6 <sup>2</sup>	6 <sup>2</sup>	6 <sup>2</sup>	5 <sup>5</sup>	5 <sup>3</sup>	5 <sup>0</sup>	5 <sup>0</sup>	5 <sup>0</sup>
100	75	50	25	25	25	50	75	100

17+25

2.2	2.3	2.3	2.1	2.3	3.1	3.4	3.5	3.7
6 <sup>1</sup>	6 <sup>0</sup>	6 <sup>0</sup>	6 <sup>2</sup>	6 <sup>0</sup>	5 <sup>2</sup>	4 <sup>9</sup>	4 <sup>8</sup>	4 <sup>6</sup>
100	75	50	25	25	25	50	75	100

17+00

2.5	2.4	2.9	2.5	2.3	2.3	2.8	3.2	3.2
5 <sup>8</sup>	5 <sup>9</sup>	5 <sup>4</sup>	5 <sup>8</sup>	6 <sup>0</sup>	6 <sup>0</sup>	5 <sup>5</sup>	5 <sup>1</sup>	5 <sup>4</sup>
100	75	50	25	25	25	50	75	100

16+75

2.1	2.1	2.4	2.4	2.7	2.3	2.5	2.5	2.8
6 <sup>2</sup>	6 <sup>2</sup>	5 <sup>8</sup>	5 <sup>9</sup>	5 <sup>6</sup>	6 <sup>0</sup>	5 <sup>8</sup>	5 <sup>8</sup>	5 <sup>5</sup>
100	75	50	25	25	25	50	75	100

16+50

2.6	2.9	2.3	2.4	2.3	2.5	3.0	2.9	3.0
5 <sup>7</sup>	5 <sup>4</sup>	6 <sup>0</sup>	5 <sup>9</sup>	6 <sup>0</sup>	5 <sup>8</sup>	5 <sup>3</sup>	5 <sup>4</sup>	5 <sup>3</sup>
100	75	50	25	25	25	50	75	100

16+25

2.8	2.7	2.7	3.0	2.8	2.7	2.6	3.0	3.0
5 <sup>5</sup>	5 <sup>6</sup>	5 <sup>6</sup>	5 <sup>3</sup>	5 <sup>5</sup>	5 <sup>6</sup>	5 <sup>7</sup>	5 <sup>3</sup>	5 <sup>3</sup>
100	75	50	25	25	25	50	75	100

8.321



Drain cont

19+50

19+25

19+00

18+75

18+63.72 = Nly line Knoxville St

18+50

18+25

18+00

LT

B.L.

RT

66

1.1	0.4	0.0	-0.5	-1.4	-1.0	7.1	7.7	8.7	9.8
72	72	83	88	92	93	12	06	+04	+15
100	75	50	25		11	39	50	75	100

1.8	1.1	0.3	-0.7	-0.7	1.3	1.1	5.8	6.9	7.9
65	72	80	90	90	96	94	25	14	04
100	75	50	25		25	33	50	75	100

1.6	1.8	0.8	0.1	-0.4	-0.8	0.7	0.2	2.2	5.5
67	65	75	82	87	91	90	85	61	28
100	75	50	25		25	50	68	80	100

1.6	1.4	0.9	0.8	0.8	0.3	4.2	3.3	3.6	3.9
67	62	74	75	78	80	41	50	47	44
100	75	50	25		20	27	50	75	100

1.5	1.2	0.7	0.6	0.7	4.2	3.3	3.6	3.4	3.7
68	71	76	77	76	41	50	47	42	45
100	75	50	25		7	25	50	75	100

1.8	1.4	0.9	0.6	0.9	3.6	3.3	3.3	3.3	3.4
65	69	74	77	74	47	50	50	50	42
100	75	50	25	15	6		25	50	75

2.6	2.5	1.9	2.9	3.6	2.9	2.9	2.9	3.1
57	58	64	54	53	54	54	54	52
100	75	50	25		25	50	75	100

8.32x



20413<sup>59</sup> - Section 90° to Forward Tangent

Base Line from herein is sly Dyke Line

Per L.S. 2201

= 21 44° 06' 15" to LT

20413<sup>59</sup> Section 90° to Back Tangent

20400-36° RT = Toe dyke

19475-75° RT = Toe dyke

TP 6.20 14.32 0.20 8.12

19470 = Top of Bank

19461 = Toe of Bank

23	11	0.5	0.6	0.1	8.6	9.1	10.5	11.5	13.1	13.2
12 <sup>0</sup>	13 <sup>2</sup>	13 <sup>8</sup>	14 <sup>2</sup>	14 <sup>4</sup>	5 <sup>7</sup>	5 <sup>2</sup>	3 <sup>8</sup>	2 <sup>8</sup>	1 <sup>2</sup>	1 <sup>1</sup>
150	125	100	75	56	48	25	25	35	75	
				Toe BANK	Top BANK		Toe dyke	Top dyke	Top dyke	
0.4	9.4	9.4	8.7	9.9	10.5	11.3	13.3	13.5	13.7	
14 <sup>7</sup>	4 <sup>9</sup>	4 <sup>9</sup>	5 <sup>6</sup>	4 <sup>4</sup>	3 <sup>8</sup>	3 <sup>0</sup>	1 <sup>0</sup>	0 <sup>8</sup>	0 <sup>6</sup>	
96	88	75	50	25	HUB 9" same	25	50	75	100	
Bottom cut	Top cut					Toe dyke	Top dyke			
0.3	0.9	0.2	8.3	9.1	10.3	10.7	11.2	11.8	13.3	13.6
14 <sup>6</sup>	15 <sup>2</sup>	14 <sup>5</sup>	6 <sup>0</sup>	5 <sup>2</sup>	4 <sup>0</sup>	3 <sup>6</sup>	3 <sup>1</sup>	2 <sup>5</sup>	1 <sup>0</sup>	0 <sup>7</sup>
100	75	60	50	25		25	36	50	75	100
		Bottom cut	Top cut			Toe dyke				
0.6	0.4	0.8	0.6	8.1	8.4	9.5	10.4	11.0	12.7	
13 <sup>2</sup>	14 <sup>2</sup>	15 <sup>1</sup>	14 <sup>2</sup>	6 <sup>2</sup>	5 <sup>2</sup>	4 <sup>8</sup>	3 <sup>9</sup>	3 <sup>3</sup>	1 <sup>6</sup>	
100	75	50	25	15		25	50	75	100	
			Bottom cut	Top cut			Toe dyke	cut dyke		

14.32 T

8.3

0.0

1.4

9.2

8.32 T



Drain

cont

LT

B.L.

RT

68

	0.4	-0.5	0.3	9.4	9.4	9.6	9.5	9.6	7.4	7.9	12.3	13.2
21+75	13 <sup>2</sup>	14 <sup>8</sup>	14 <sup>0</sup>	4 <sup>9</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>8</sup>	4 <sup>7</sup>	6 <sup>2</sup>	6 <sup>4</sup>	7 <sup>0</sup>	1 <sup>1</sup>
	150	125	115	107	100	75	50	25		25	40	73
			Toe	Top	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	0.9	-0.4	-0.5	9.4	9.7	9.6	8.9	8.7	9.2	12.5	12.9
21+50	13 <sup>4</sup>	14 <sup>2</sup>	14 <sup>8</sup>	4 <sup>9</sup>	4 <sup>6</sup>	4 <sup>7</sup>	5 <sup>4</sup>	5 <sup>6</sup>	5 <sup>1</sup>	1 <sup>8</sup>	1 <sup>4</sup>
	150	125	106	96	75	50	25		22	40	73
			Toe	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	1.1	-0.5	-0.3	-0.2	9.9	9.6	9.1	9.1	9.7	10.4	12.8	12.9
21+25	13 <sup>2</sup>	14 <sup>8</sup>	14 <sup>6</sup>	14 <sup>5</sup>	4 <sup>4</sup>	4 <sup>7</sup>	5 <sup>2</sup>	5 <sup>2</sup>	4 <sup>6</sup>	3 <sup>9</sup>	1 <sup>5</sup>	1 <sup>4</sup>
	150	125	100	92	84	75	50	25		20	40	73
			Toe	Top	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	0.9	0.7	-1.0	-0.1	9.5	9.5	9.5	9.4	10.4	10.9	13.1	13.1
21+00	13 <sup>4</sup>	13 <sup>6</sup>	15 <sup>2</sup>	14 <sup>4</sup>	4 <sup>8</sup>	4 <sup>8</sup>	4 <sup>8</sup>	4 <sup>9</sup>	3 <sup>9</sup>	3 <sup>4</sup>	1 <sup>2</sup>	1 <sup>2</sup>
	150	125	100	86	77	75	50	25		20	36	73
			Toe	Top	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	1.3	0.4	-0.5	-0.2	9.8	9.3	9.3	10.8	11.5	13.2	13.3
20+75	13 <sup>0</sup>	13 <sup>9</sup>	14 <sup>8</sup>	14 <sup>5</sup>	4 <sup>5</sup>	5 <sup>0</sup>	5 <sup>0</sup>	3 <sup>5</sup>	2 <sup>8</sup>	1 <sup>1</sup>	1 <sup>0</sup>
	150	125	100	80	68	50	25		20	36	73
			Toe	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	3.0	1.1	0.2	0.1	0.1	8.8	8.7	9.8	10.5	11.3	13.3	13.5
20+50	11 <sup>3</sup>	13 <sup>2</sup>	14 <sup>1</sup>	14 <sup>2</sup>	14 <sup>2</sup>	5 <sup>5</sup>	5 <sup>6</sup>	4 <sup>5</sup>	3 <sup>8</sup>	3 <sup>0</sup>	1 <sup>0</sup>	0 <sup>8</sup>
	150	125	100	75	70	58	50	25		20	35	73
			Toe	Top	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

	2.3	1.7	0.4	-0.5	0.0	8.4	9.5	10.5	10.2	13.0	13.5
20+25	12 <sup>0</sup>	13 <sup>1</sup>	13 <sup>9</sup>	14 <sup>8</sup>	14 <sup>3</sup>	5 <sup>9</sup>	4 <sup>8</sup>	3 <sup>8</sup>	3 <sup>1</sup>	1 <sup>3</sup>	0 <sup>8</sup>
	150	125	100	75	58	50	25		20	35	73
			Toe	Top	Top	Top	Top	Toe	Top	Top	Top
			Bank	Bank	Bank	Bank	Bank	Dyke	Dyke	Dyke	Dyke

14.327



23+25

9.2	9.7	4.7	4.2	6.3	11.6
4 <sup>5</sup>	4 <sup>0</sup>	9 <sup>0</sup>	9 <sup>5</sup>	7 <sup>4</sup>	2 <sup>1</sup>
50	26	17		30	40 <sup>0</sup>
				Top Dike	Top Dike

TP 6.59 13.65 7.26 7.06

13.65 ↑

23+00

9.5	9.4	9.4	9.9	10.6	5.5	4.0	4.1	6.0	11.6
4 <sup>8</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>4</sup>	3 <sup>2</sup>	8 <sup>8</sup>	10 <sup>3</sup>	10 <sup>2</sup>	8 <sup>3</sup>	2 <sup>7</sup>
150	125	100	75	58	50	25		27	40 <sup>0</sup>
Top Bank								Top Dike	Top Dike

22+75

0.3	9.6	9.4	9.4	9.4	9.5	4.4	4.0	4.3	6.1	12.2	13.0
14 <sup>0</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>8</sup>	9 <sup>2</sup>	10 <sup>3</sup>	10 <sup>0</sup>	8 <sup>2</sup>	2 <sup>1</sup>	1 <sup>3</sup>
150	141	125	100	75	67	50	25		30	40	73
Top Bank	Top								Top Dike	Top Dike	Top Dike

22+50

0.5	0.2	9.3	9.3	9.3	8.9	7.1	5.5	4.7	6.3	11.7	13.0
14 <sup>8</sup>	14 <sup>5</sup>	5 <sup>0</sup>	5 <sup>0</sup>	5 <sup>0</sup>	5 <sup>4</sup>	7 <sup>2</sup>	8 <sup>8</sup>	9 <sup>6</sup>	8 <sup>0</sup>	2 <sup>4</sup>	1 <sup>3</sup>
150	140	130	125	100	75	50	25		30	40	73
Top Bank	Top Bank								Top Dike	Top Dike	Top Dike

22+25

0.2	0.4	0.6	9.3	9.4	9.0	8.4	8.4	6.6	5.9	5.4	6.2	12.2	13.0
14 <sup>5</sup>	14 <sup>2</sup>	14 <sup>6</sup>	5 <sup>0</sup>	4 <sup>2</sup>	5 <sup>3</sup>	5 <sup>9</sup>	5 <sup>9</sup>	7 <sup>2</sup>	8 <sup>4</sup>	8 <sup>2</sup>	8 <sup>1</sup>	2 <sup>1</sup>	1 <sup>3</sup>
150	125	120	110	100	75	50	45	25	15		26	41	74
		Top Bank	Top Bank								Top Dike	Top Dike	Top Dike

22+00

0.0	0.8	0.1	9.4	9.4	9.3	8.6	7.5	6.1	6.0	7.1	12.4	13.0
14 <sup>3</sup>	15 <sup>1</sup>	14 <sup>4</sup>	4 <sup>2</sup>	5 <sup>0</sup>	5 <sup>2</sup>	6 <sup>8</sup>	8 <sup>2</sup>	8 <sup>3</sup>	7 <sup>2</sup>	1 <sup>2</sup>	1 <sup>3</sup>	
150	125	110	100	75	50	25	13		25	40	73	
		Top Bank	Top Bank						Top Dike	Top Dike	Top Dike	

14.32 K



Drain Cont

25+00

0.7 0.7 2.5 3.4 4.4 12.1  
 13<sup>0</sup> 13<sup>0</sup> 11<sup>2</sup> 10<sup>3</sup> 9<sup>5</sup> 1<sup>6</sup>  
 50 25 15  
 26  
 Topdyke Topdyke

24+75

1.0 0.9 3.3 3.9 5.0 12.4  
 12<sup>2</sup> 12<sup>8</sup> 10<sup>4</sup> 9<sup>8</sup> 8<sup>7</sup> 1<sup>3</sup>  
 50 25 16  
 27  
 Topdyke Topdyke

24+50

0.6 1.0 1.7 4.2 5.3 12.6  
 13<sup>1</sup> 12<sup>2</sup> 12<sup>0</sup> 9<sup>5</sup> 8<sup>4</sup> 1<sup>1</sup>  
 50 25 19  
 27  
 Topdyke Topdyke

24+25

1.0 1.6 2.3 4.3 4.7 6.0 12.8  
 12<sup>2</sup> 12<sup>1</sup> 11<sup>4</sup> 9<sup>4</sup> 9<sup>0</sup> 7<sup>2</sup> 0<sup>9</sup>  
 50 25 10 4  
 28  
 Topdyke Topdyke

24+00

4.4 3.6 5.8 5.9 6.5 12.4  
 9<sup>3</sup> 10<sup>1</sup> 7<sup>2</sup> 7<sup>8</sup> 7<sup>2</sup> 1<sup>3</sup>  
 50 28 11  
 26  
 Topdyke Topdyke

23+75

7.9 6.8 6.4 7.2 12.3  
 5<sup>8</sup> 6<sup>9</sup> 7<sup>3</sup> 6<sup>5</sup> 1<sup>4</sup>  
 50 25  
 30  
 Topdyke Topdyke

23+50

9.3 8.5 7.7 5.7 6.8 11.7  
 4<sup>4</sup> 5<sup>2</sup> 6<sup>0</sup> 8<sup>0</sup> 6<sup>9</sup> 2<sup>0</sup>  
 50 25 4  
 30  
 Topdyke Topdyke

13.65-T



Drain cont

26+25

26+16- 20<sup>E</sup> RT = 2 dead men (2)

26+06- 11<sup>E</sup> RT = 12" Power pole # P4500

TP 1.22 4.22 10.65

3.00

26+00

25+89- 16<sup>E</sup> RT = 2 dead man

25+75

25+50

25+25

LT

B.L.

RT.

71

-0.8

5<sup>0</sup>

25

-0.3

45 29

17  
Toe  
dyke

1.3

11.8

+ 7<sup>E</sup>

40  
Top dyke

4.22

π

#P4500

Nail in Power pole - 11<sup>E</sup> RT Sta 26+06

-0.6

14<sup>3</sup>

50

0.3

13<sup>4</sup>

25

0.5

13<sup>2</sup>

19  
Toe  
dyke

1.9

11<sup>8</sup>

45  
Top  
dyke

11.9

1<sup>8</sup>

0.4

13<sup>3</sup>

50

0.4

13<sup>3</sup>

25

1.7

12<sup>0</sup>

10

1.2

12<sup>5</sup>

22  
Toe dyke

2.6

11<sup>1</sup>

40  
Top dyke

11.9

1<sup>8</sup>

40  
Top dyke

1.3

12<sup>4</sup>

50

0.8

12<sup>2</sup>

25

2.4

11<sup>3</sup>

10

2.3

11<sup>4</sup>

24  
Toe dyke

4.0

9<sup>2</sup>

40  
Top dyke

12.0

1<sup>7</sup>

40  
Top dyke

0.7

13<sup>0</sup>

50

1.1

12<sup>6</sup>

25

3.2

10<sup>5</sup>

10

2.8

10<sup>2</sup>

25  
Toe dyke

4.1

9<sup>6</sup>

40  
Top dyke

12.0

1<sup>2</sup>

40  
Top dyke

13.65 π



Prain cont

LT

B.L.

RT

72

508
42
<hr/>
-083

TP 4.62 {0.24} ✓  
0.24

Starting B.M. Page 49-

TP 6.11 4.86 5.47 - 1.25

↳ The 5th U.S. Govt Dyke Line  
26+76<sup>83</sup> - Intersection of Nashville St

~~1.8~~ -0.8

505  
Hub  
Pr Same

26+60-5<sup>9</sup> LT = of Fire Hydrant

26+50-28<sup>5</sup> RT = of Sewer Man hole

0.6	1.1	1.68	5.43	11.8
4.8	3.1	2.54	9.65	+7.6
2.5	2.85	2.85	4.5	
Toedye	Rim	I.E.	TOP	DYKE
	SMITH	MIN		
4.22	^			







The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. Each page is divided into three vertical columns by two red lines. The left column is the narrowest, the middle column is the widest, and the right column is the narrowest. The pages are otherwise blank, with no handwriting or printed text. The notebook is bound in the center, and a dark cover is visible at the edges. The page number '74' is written in the top right corner of the right page.



The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. The notebook is bound in the center, and the dark cover is visible at the edges. The pages are mostly blank, with some faint, illegible markings and a small handwritten number '74' in the top right corner of the right page.



The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. A metal fastener is visible in the center gutter, consisting of a vertical wire with four circular loops. The right page has the number '75' written in the top right corner. The notebook is set against a dark background.





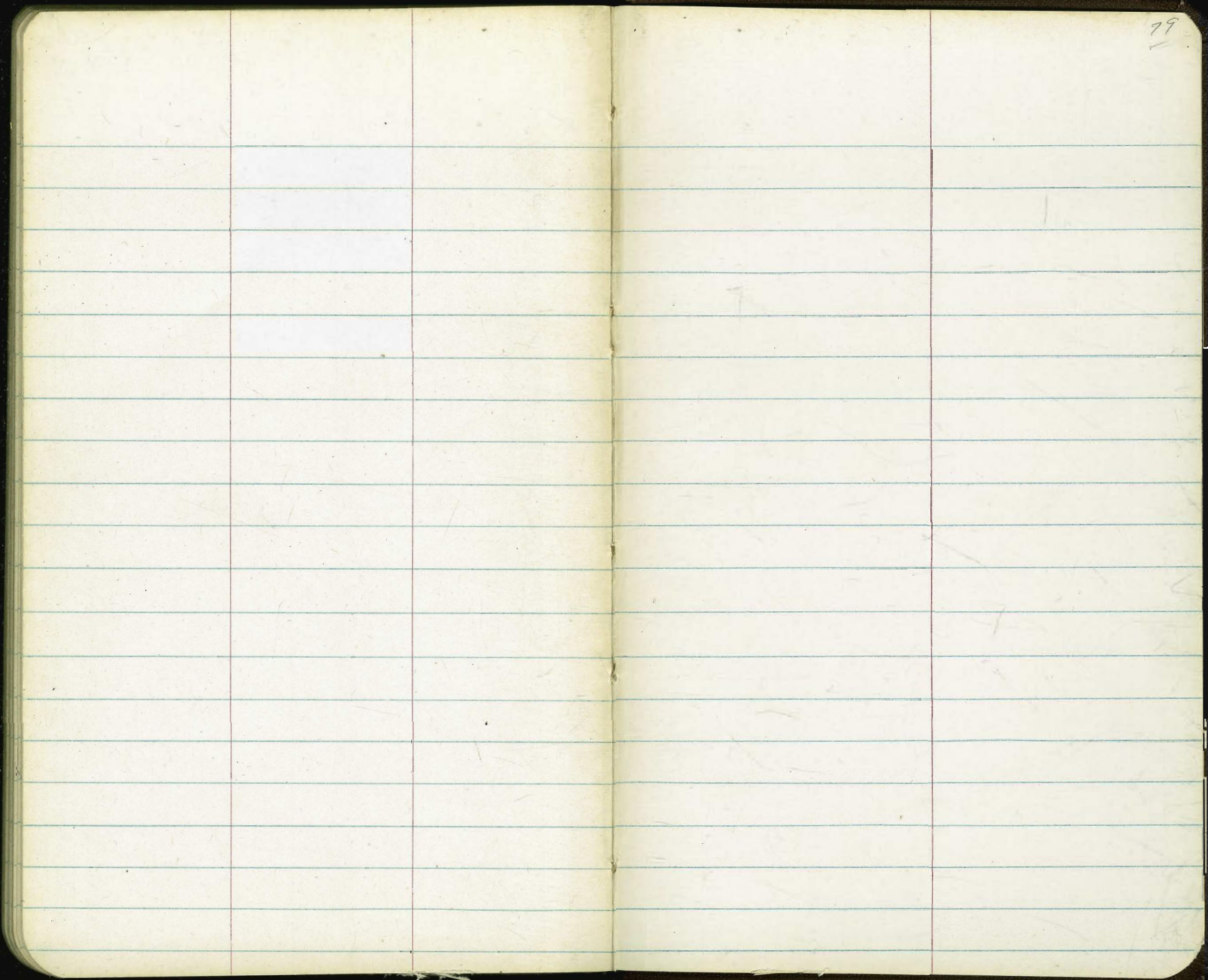




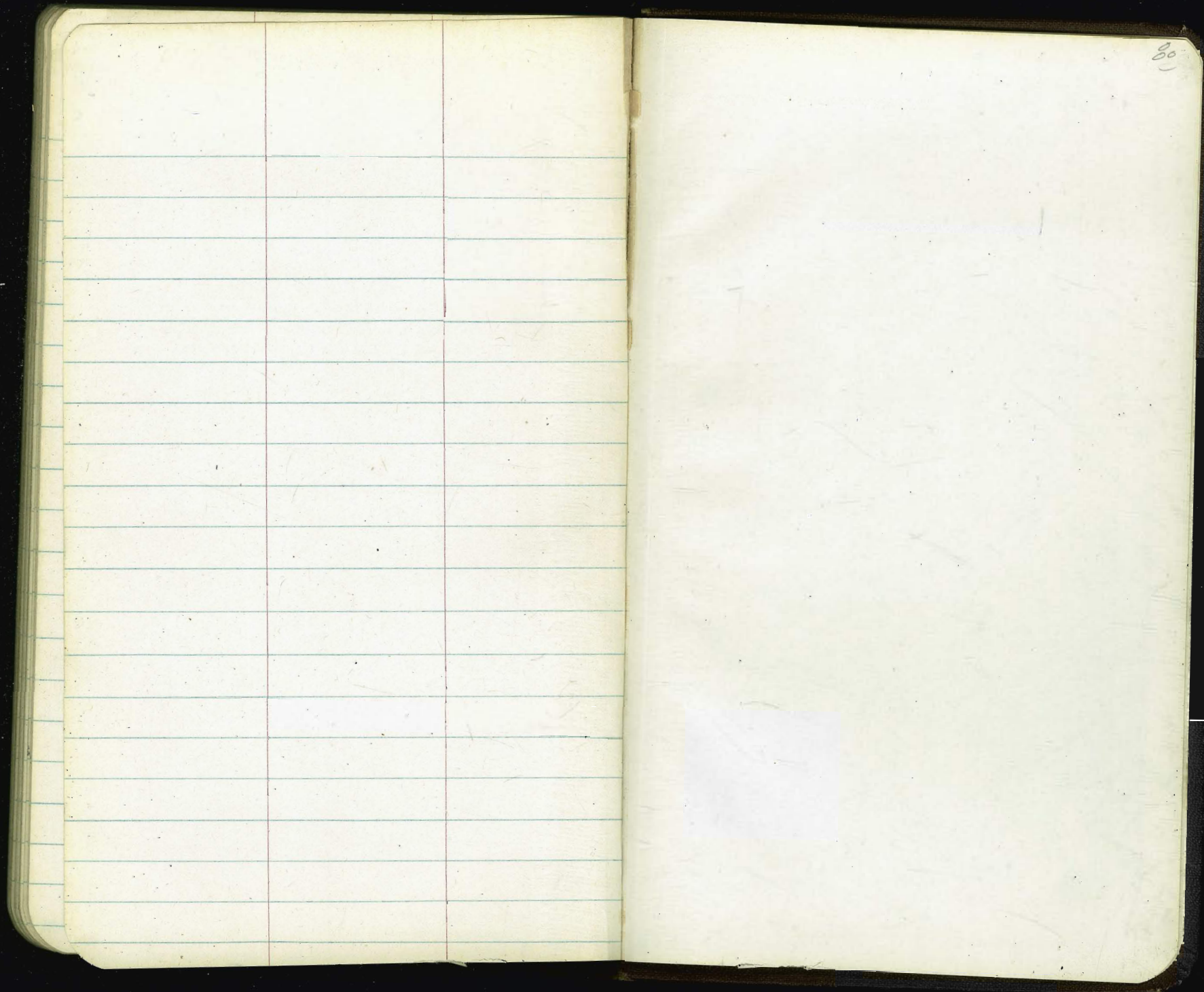














Thibodow

7.28  
60°  
12.88  
123.87  
16.6

2580-B

2597-L

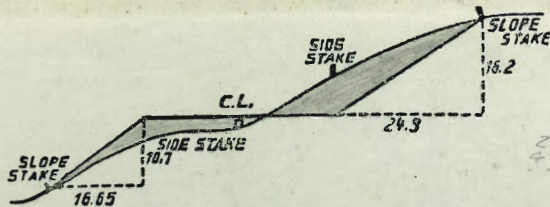
1118-D

2712-B

2680-B

Tue 2120-50  
2122-50

168.60 = S.W. 7 Mon. Cass + Van Noys  
B. - 2056-P. 66



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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