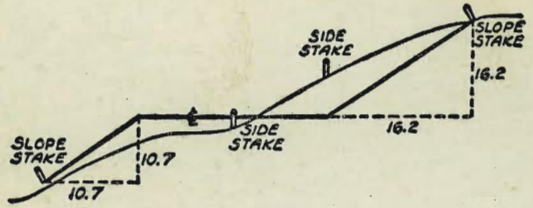
2336

SEWER



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

(X) Sec All streets in Floral Terrace 1-78

Sub

also see FB 2337 1-35

INDEXED

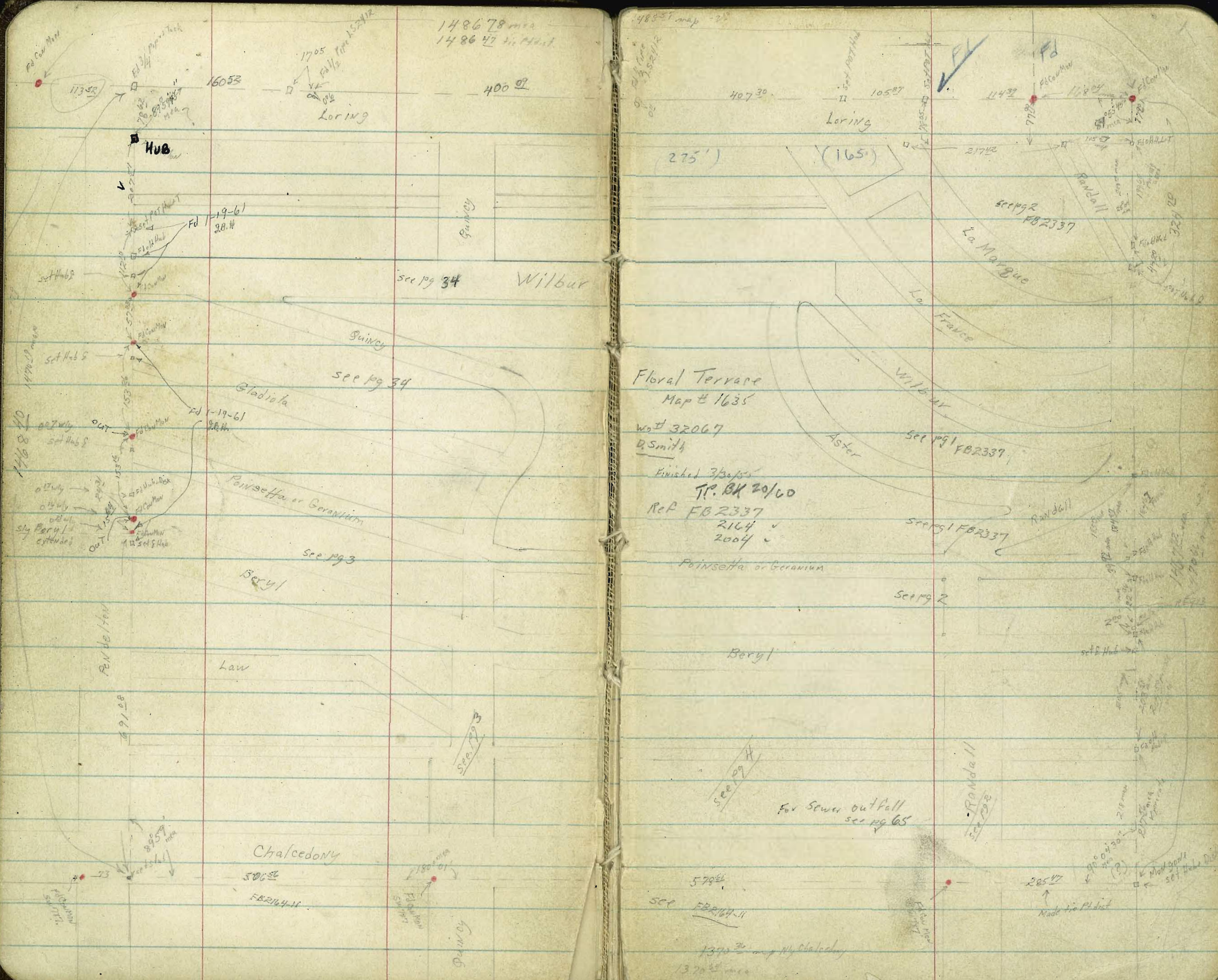
APR 1 1955

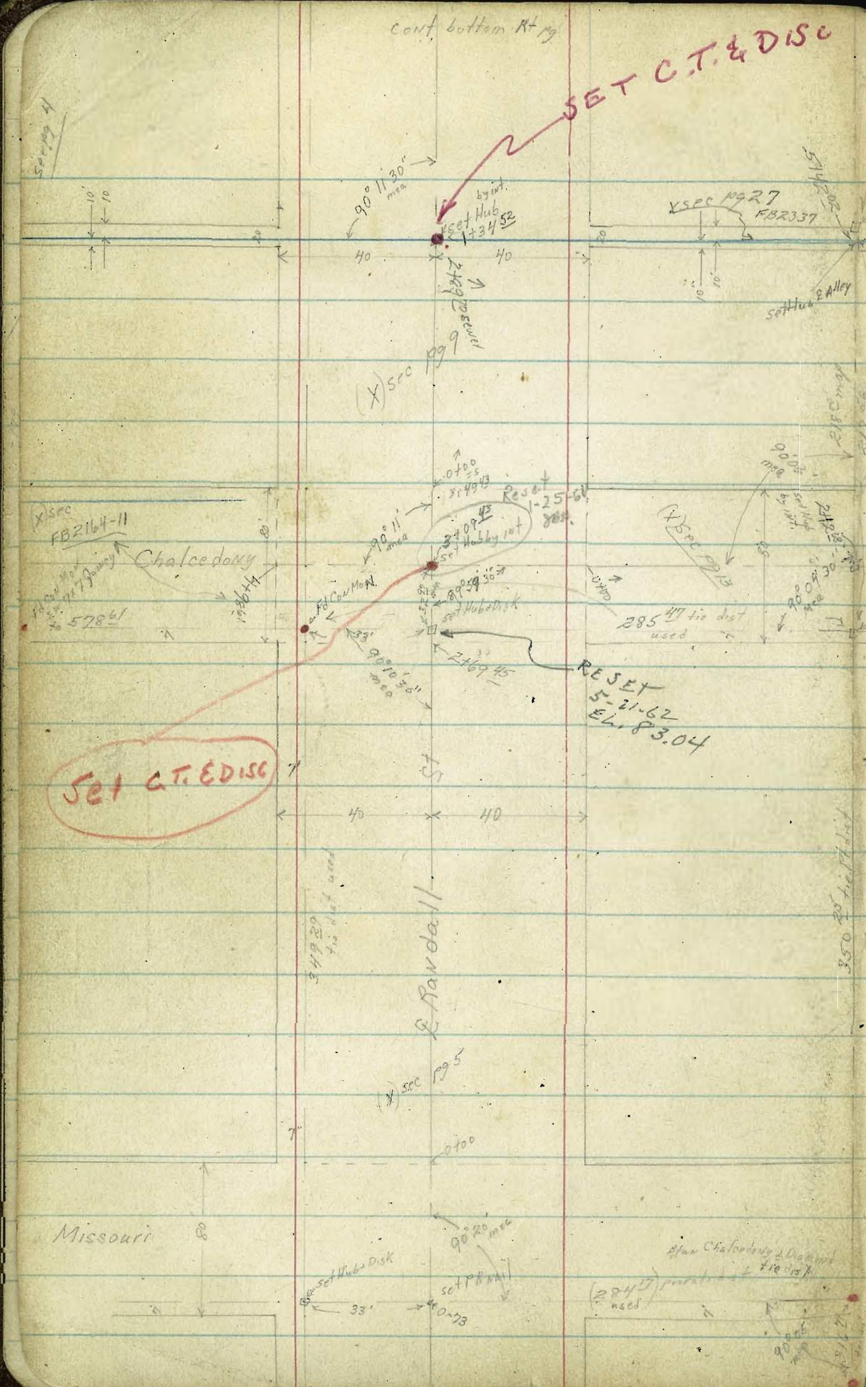
MER

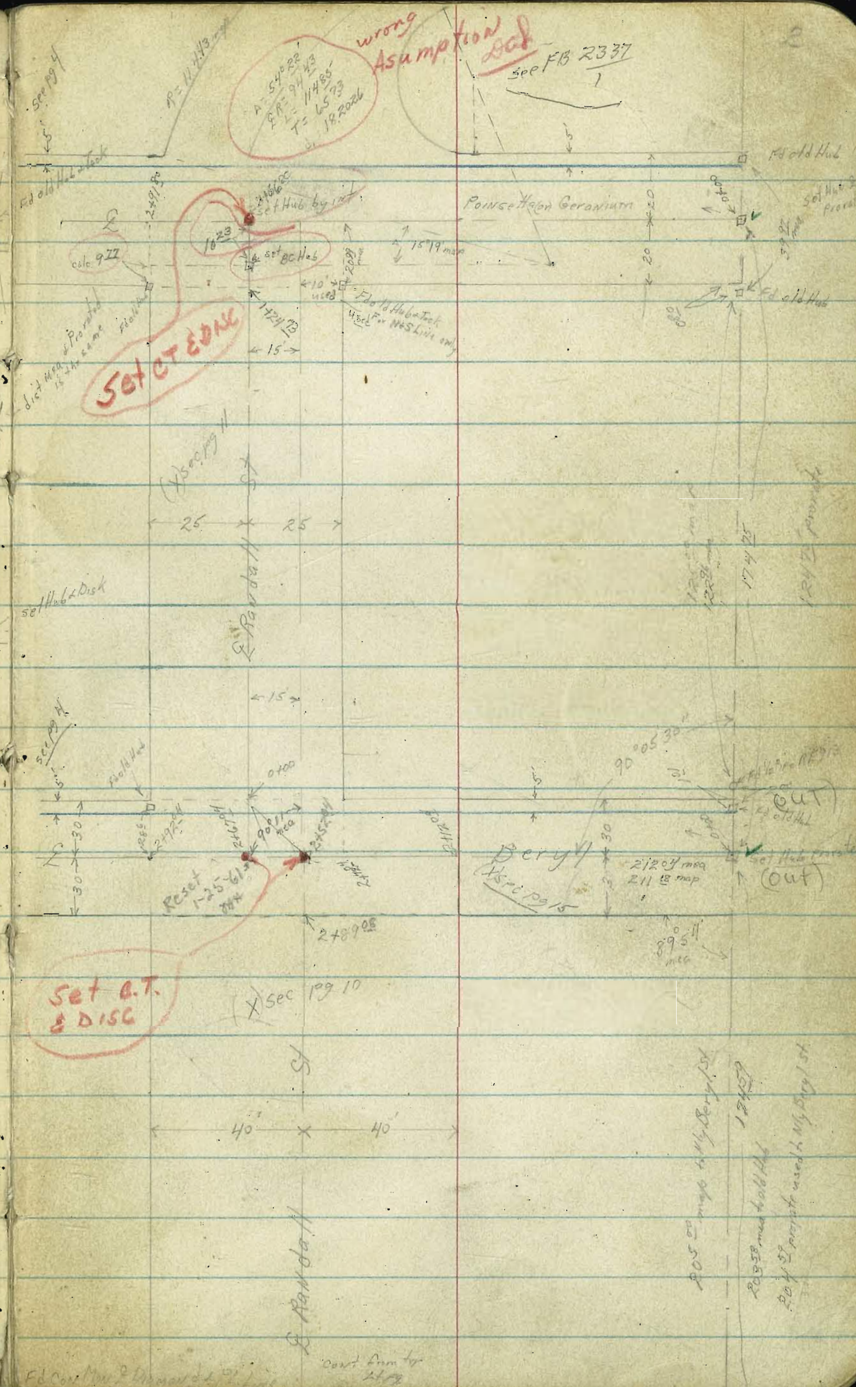
Floral Terrace
Map # 1635

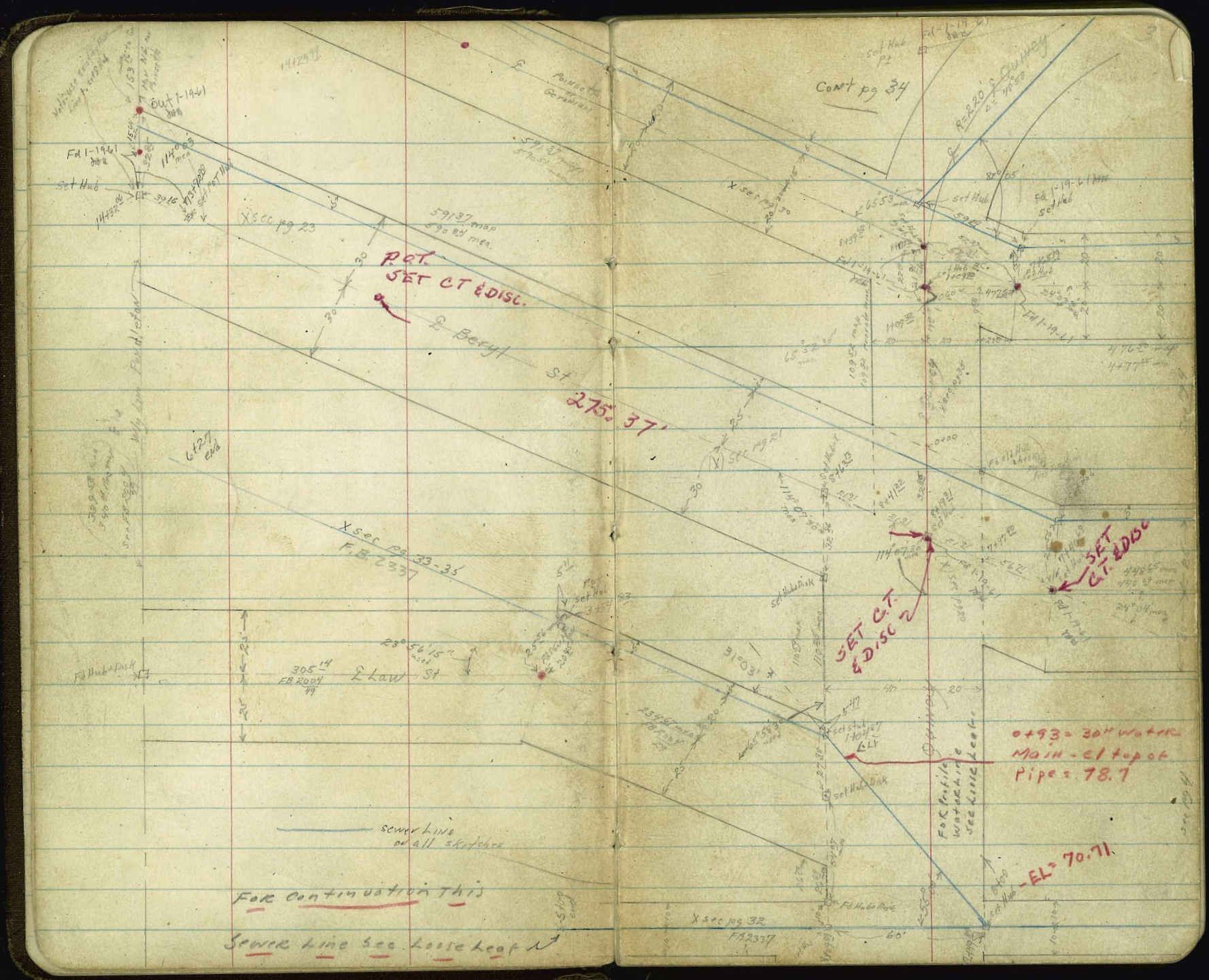
WO # 32067
D. Smith

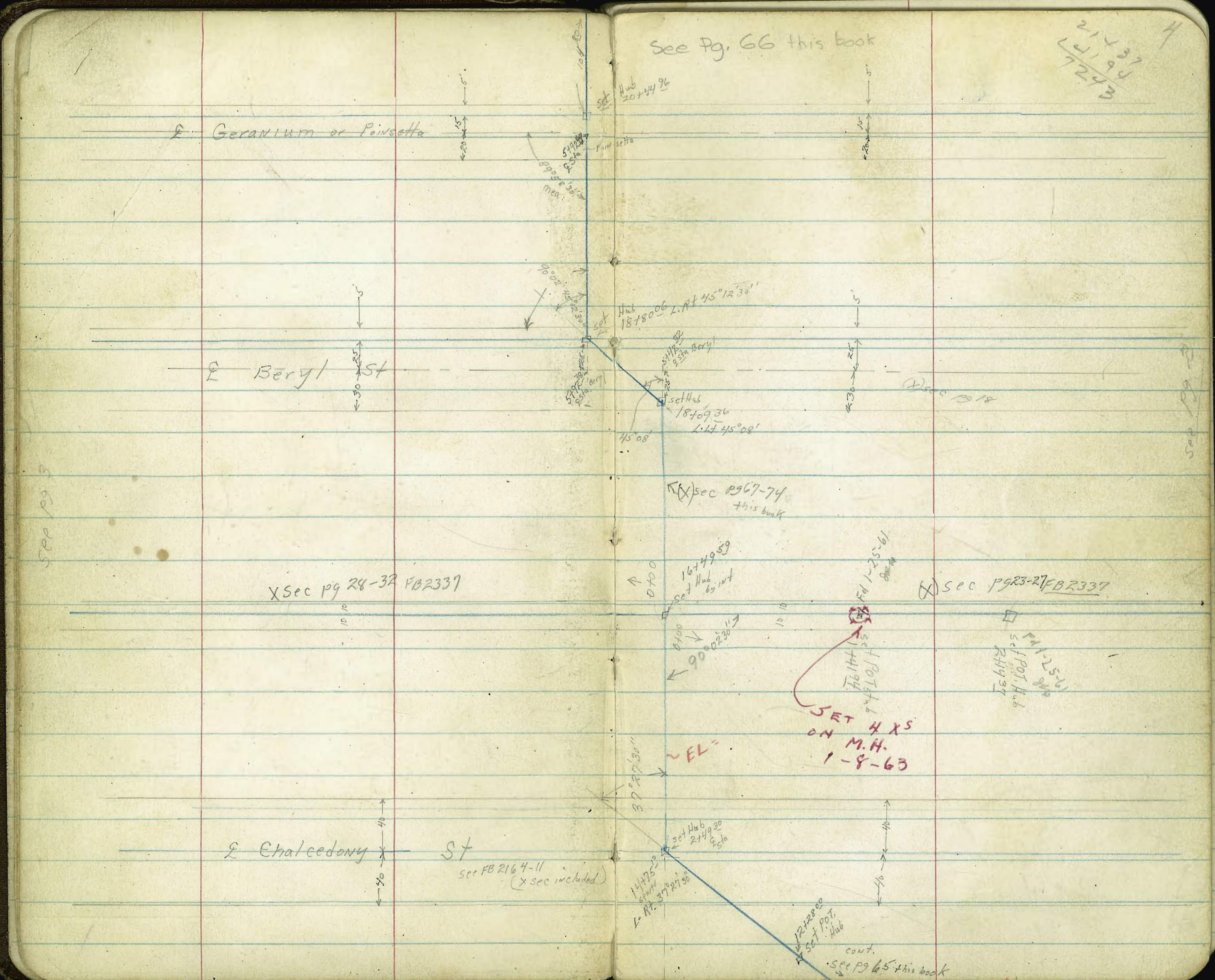
Finished 3/30/55
TP. BK 20/60
Ref FB 2337
2164 ✓
2004 ✓




Cont. bottom Rt. pg
SET C.T. & DISC
See pg 4
90° 11' 30"
Set Hub by int.
1+34.52
40
40
X sec pg 27
FB 2337
Set Hub & Alley
(X) sec pg 9
(X) sec FB 2164-11
Chalcedony
Fd Con Mon
3+09.43
Set Hub by int
Reset 1-25-61
90° 11' mea
89° 59' 30"
Set Hub & Disk
285.47 tie dist used
(X) sec pg 13
2+69.45
RESET 5-21-62 EL. 83.04
90° 00' 30" mea
Set C.T. & DISC
40
40
℄ Randall St
(X) sec pg 5
Missouri
90° 20' mea
Set PK nail
Set Hub & Disk
33'
0+73
(284.5) prorated


wrong
Asumption
See FB 2337
Set Hub by int
Set C.T. & DISC
Poinsettia
Geranium
Fd old Hub
Fd old Hub
Set Hub & Prorate
(X) sec pg 11
25
25
Set Hub & Disk
℄ Randall St
15
See pg 4
Fd old Hub
0+00
Reset 1-25-61
2+89.08
Beryl
(X) sec pg 15
212.03 mea
211.18 map
89° 5' 11" mea
90° 05' 30"
(OUT)
(OUT)
Set C.T. & DISC
(X) sec pg 10
40
40
℄ Randall St
Cont. from top


Cont pg 34
P.O.T. SET CT & DISC.
℄ Beryl St
275.37'
X sec pg 23
X sec pg 33-35
F.B. 2337
℄ Law St
sewer line on all sketches
For continuation THIS Sewer Line See Loose Leaf
SET CT. & DISC
SET CT. & DISC
0+93 = 30" Water Main - el top of Pipe = 78.7
EL = 70.71
For Profile Waterline See Loose Leaf
X sec pg 32
FB 2337



See Pg. 66 this book
4
21+37
21.94
7243
℄ Geranium or Poinsetta
Set Hub 20+44.96
℄ Sta Poinsetta
89°58'30" mea.
90°00'
Set Hub 18+80.06 L.Rt 45°12'30"
℄ Beryl St
℄ Sta Beryl
Set Hub 18+09.36 L.Lt 45°08'
45°08'
See Pg 3
(X) Sec pg 67-74 this book
(X) Sec pg 18
16+49.59 Set Hub by int
X Sec pg 28-32 FB2337
(X) Sec pg 23-27 FB2337
Fd 1-25-61
Set POT Hub 21+49.37
90°02'30"
SET 4 XS ON M.H. 1-8-63
~EL~
37°27'30"
℄ Chalcedony St
See FB 2164-11 (x sec included)
Set Hub 2+49.30 ℄ Sta
L.Rt 37°27'30"
Set POT. Hub
cont. See pg 65 this book

"X" Sec Randall St
Missouri to Geranium or Poinsetta

0-68 ℄ int. Nly edge A.C. Rd					
0-80	{ 33.9 Lt ℄ deadman / Sly Line Missouri				
0-90	21.5 Lt ℄ 8" T Pole #61424				
0-99	{ 11.3 Lt ℄ Fire Hyd / ℄ int Sly edge A.C. Rd.				
TP_5	6^{52}	53^{17}	11^{79}	46^{66}	
0-130	30.0 Rt ℄ 10" Acacia tree = 50' Sly of S Line Missouri				
TP_4 BM	9^{95}	58^{44}	6^{09}	48^{49}	ON S.W. 7x7 Hub & Disk Missouri & Randall
TP_3	3^{67}	54^{58}	12^{78}	50^{91}	
TP_2	0^{31}	63^{69}	11^{67}	63^{38}	
TP_1	0^{02}	75^{05}	13^{30}	75^{03}	
B.M.	2^{40}	88^{33}		85^{93} ✓	S.W. 7x7 con mon Randall & Chalcedony

Lt = Wly ℄ Rt = Ely

51.7	49.32	47.52	47.01	46.6	43.5	42.6	40.5	38.69	35.20	
1^{5}	3^{85}	5^{65}	6^{16}	6^{6}	9^{7}	10^{6}	12^{7}	14^{48}	17^{97}	
60	40 Sly edge A.C.	20 ℄ A.C. Rd.	Nly edge A.C.	13	20	30	40	43 Sly top ditch Con	50 ℄ ditch	

52.9	49.9	48.04	46.22	46.05	45.87	45.5	42.6	41.9	41.0	38.00
0^{3}	3^{4}	5^{13}	6^{95}	7^{12}	7^{30}	7^{7}	10^{6}	11^{3}	12^{3}	15^{17}
60	40	25 Sly edge AC	5 ℄ AC		14 Nly edge AC Rd	20	25	40	54	64.0 Sly top edge Con drain ditch

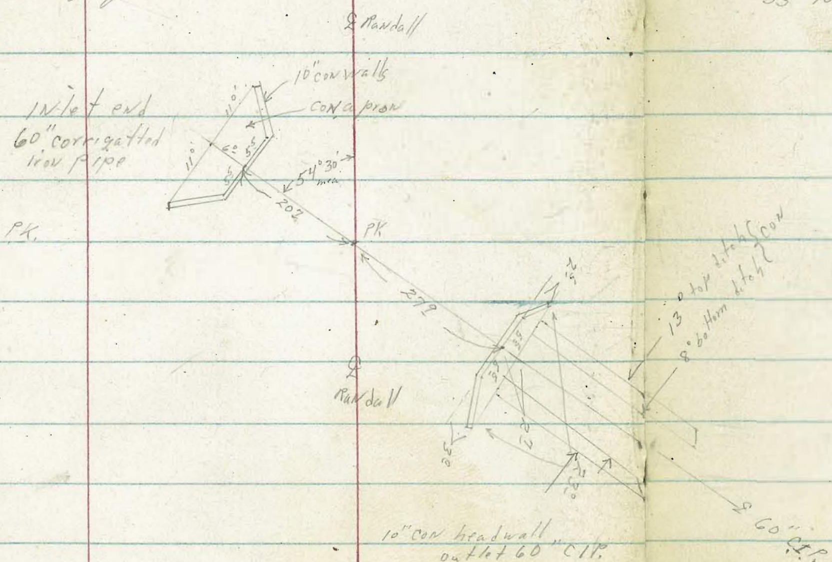
54.0	50.7	48.2	45.73	44.03	43.31	43.21	42.1
0^{8}	2^{5}	5^{0}	7^{44}	9^{14}	9^{86}	9^{96}	11^{1}
60	40	20	AC edge	20 ℄ AC	40	44.0 Nly AC Rd	60

↑ 53^{17}

55.8	52.6	50.1	47.5	44.9	42.09	40.59
2^{6}	5^{8}	8^{3}	10^{9}	13^{5}	16^{35}	17^{85}
60	40	20		20	40 Sly edge AC	60 ℄ AC

↑ 58^{44}

TP 7	11^{83}	70^{42}	2^{02}	58^{59}
0+50				
0+25				
TP 6	9^{07}	60^{61}	1^{63}	51^{54}
0+00 Nly Missouri St				
0-17.5 ℄ crosses Wly of N+S AC.				
0-27.09 set P.K.				
0-50				



Lt = Wly ℄ Rt = Ely 6

49.4	48.2	45.0	45.5	47.4	48.8	50.5	51.5	57.99	57.47	58.16	59.2		
11^{2}	12^{4}	15^{6}	15^{1}	13^{2}	11^{8}	10^{1}	9^{1}	2^{62}	3^{14}	2^{45}	1^{4}		
65	60	40	35	30	20		6	22 wly AC.	31	40 Ely AC.	60		
48.9	45.9	43.7	43.6	49.1	49.4	50.3	54.1	54.27	54.03	54.99	54.9	54.5	
11^{7}	14^{2}	16^{9}	17^{0}	11^{5}	11^{2}	10^{3}	6^{5}	6^{34}	6^{58}	5^{62}	5^{7}	6^{L}	
62	52	40	33	18		9	15	18.5 wly AC.	26	37 Ely AC.	40	60	

⊼ 60^{61}

51.9	47.8	43.0	41.8	50.0	50.1	51.18	51.13	52.02	52.5	50.9
1^{3}	5^{4}	10^{2}	11^{4}	3^{2}	3^{1}	1^{99}	2^{04}	1^{15}	0^{7}	2^{3}
60	48	40	20	4		10 wly AC.	20	30 Ely AC.	40	60

52.5	49.1	45.6	40.1	46.36	49.4	49.73	49.60	50.27	50.2	49.1	47.5
0^{7}	4^{1}	7^{6}	13^{1}	6^{81}	3^{8}	3^{44}	3^{57}	2^{90}	3^{0}	4^{1}	5^{7}
53	40	35	19	18	11	wly AC	10.5 ℄ AC.	21 Ely AC.	30	40	55

40.07	46.08	43.96	37.93
13^{10}	7^{09}	9^{21}	15^{24}
20.7 ie. inlet	20.7 top headwall	27.9 top headwall	27.9 ie outlet

51.43	49.52	48.65	48.07	47.7	44.0	39.49	35.84	39.07	43.8	
1^{74}	3^{65}	4^{52}	5^{09}	5^{5}	9^{2}	13^{68}	17^{33}	14^{10}	9^{4}	
60 Sly edge AC.	40 ℄ AC.	22 Nly AC.	Ely Nly edge [illegible] N+S	11	20	21.2 top Sly ditch	31 ℄ ditch	40 Nly edge ditch	55	

⊼ 53^{17}

2+00					
1+75					
1+67	37° Rt to SW cor house of housing				
TP8	11^{27}	80^{96}	0^{73}	69^{69}	Stub 14° Rt @ 1+50
1+50					
1+25					
1+00					
0+75					

Lt = Wly ℄ Rt = Ely

	61.6	66.9	69.0	73.0	78.1	75.7	75.4	76.2	76.5	76.3		
	18^{4}	14^{1}	12^{0}	8^{0}	2^{9}	5^{3}	5^{6}	4^{8}	4^{5}	4^{2}		
	60	40	30	15		8	30	33	40	47.5 to house here		
	53.8	57.6	64.2	69.6	73.7	73.8	73.0	72.7	73.5			
	27^{2}	23^{4}	16^{8}	11^{4}	7^{3}	7^{2}	8^{0}	8^{3}	7^{5}			
	60	40	20		8	11	13	30	40 to house here			

HI 80^{96}

52.0	54.4	56.7	60.3	63.9	69.1	69.9	69.1	69.9	69.2		
18^{4}	16^{0}	13^{2}	10^{1}	6^{5}	$+0^{3}$	0^{5}	0^{3}	$+0^{5}$	$+1^{2}$		
60	40	25	15		16	18	35	40	60		
50.1	52.0	53.8	60.1	68.2	67.7	68.5	68.77	68.42	69.38		
20^{3}	18^{4}	16^{6}	10^{3}	2^{2}	2^{7}	1^{9}	1^{65}	2^{00}	1^{04}		
60	40	25		19	22	40	42 Wly A.C.	52	68 Ely A.C.		
47.5	49.1	50.1	51.8	53.4	56.0	58.2	64.52	64.51	64.70	65.28	65.4
22^{9}	21^{3}	20^{3}	18^{6}	17^{0}	14^{4}	12^{2}	5^{20}	5^{21}	5^{72}	5^{14}	5^{0}
60	50	40	20	8		8	26 Wly A.C.	35	40	46 Ely A.C.	50
50.2	47.6	46.2	49.5	50.7	52.9	54.6	61.14	60.73	61.20	61.50	61.9
20^{2}	22^{8}	24^{2}	20^{9}	19^{7}	17^{5}	15^{8}	9^{28}	9^{69}	9^{22}	8^{92}	8^{5}
65	55	50	40	20		10	24 Wly A.C.	32	40	42.0 Ely A.C.	60

HI 70^{42}

3+29.43					
TP₁₀ BM	10^{73}	96^{66}	3^{32}	85^{91} (85^{93})	SW cor Mon 7x7 Chalcedony · Randall
3+09.43 ℄ Chalcedony					
2+89.45					
2+69.45 Sly Chalcedony					
2+50					
2+25 30° Lt ℄ 3" tree (Euc)					
2+20 51.5 Rt to NW cor house					
2+05 28° Lt ℄ 3" Eucaleptetus tree					
TP9	10^{84}	89^{23}	2^{57}	78^{39}	

Lt = Wly ℄ Rt = Ely

87.2 9.5/40 · 87.8 8.9/25 · 87.9 8.8/15 · 88.5 8.2 · 88.5 8.2/15 · 88.1 8.6/26 · 88.7 8.0/40

π 96.66

85.8 3.4/40 · 86.3 2.9/26 · 87.1 2.1/12 · 87.1 2.1/9.5 · 87.06 2.17 on Hub · 86.6 2.6/20 · 86.6 2.6/30 · 87.2 2.0/40

86.0 3.2/55 · 84.8 4.4/50 · 85.3 3.9/40 · 85.3 3.9/25 · 85.4 3.8/15 · 85.8 3.4 · 85.2 4.0/10 · 84.3 4.9/25 · 85.0 4.2/36 · 86.2 3.2/40 · 88.0 1.2/60

83.4 5.8/60 · 84.6 4.6/40 · 85.9 3.3/30 · 86.9 2.3/18 · 85.0 4.2/10 · 83.9 5.3 · 82.5 6.7/20 · 82.0 7.2/40 · 82.2 7.0/60

80.6 8.6/60 · 83.1 6.1/40 · 85.3 3.9/20 · 85.7 3.5/5 · 82.9 6.3 · 81.3 7.9/5 · 80.5 8.7/25 · 80.8 8.4/40 · 81.0 8.2/60

69.7 17.5/60 · 75.8 13.4/40 · 81.6 7.6/20 · 83.6 5.6/3 · 81.1 8.1 · 78.7 10.5/5 · 78.0 11.2/30 · 78.5 10.7/32 · 78.4 10.8/40 · 78.6 10.6/60

π 89.23

4 8/48/96

1+24.52 Sly Alley

1+00

0+75

0+50

TP,	12.25	107.20	12.1	94.25

0+25

0+00 ↑
=S
3+49.43 ↓ Nly Chalcedony

Lt = Wly ℄ Rt = Ely

103.7	3.5	60
103.5	3.2	40
104.1	3.1	25
104.9	2.3	12
102.8	4.4	7
102.7	4.5	
102.9	4.3	10
102.6	4.6	20
102.8	4.4	25
101.9	5.3	40
100.5	6.7	60

97.2	10.0	60
98.3	8.9	40
98.6	8.6	25
99.9	7.3	10
100.2	7.0	
100.6	6.6	10
100.4	6.8	20
100.9	6.3	21
102.0	5.2	24
100.5	6.7	40
99.6	7.6	60

96.0	11.2	60
96.8	10.4	40
97.0	10.2	20
97.4	9.8	
98.1	9.1	12
97.9	9.3	23
98.6	8.6	25
100.6	6.6	30
99.7	7.5	40
98.1	9.1	60

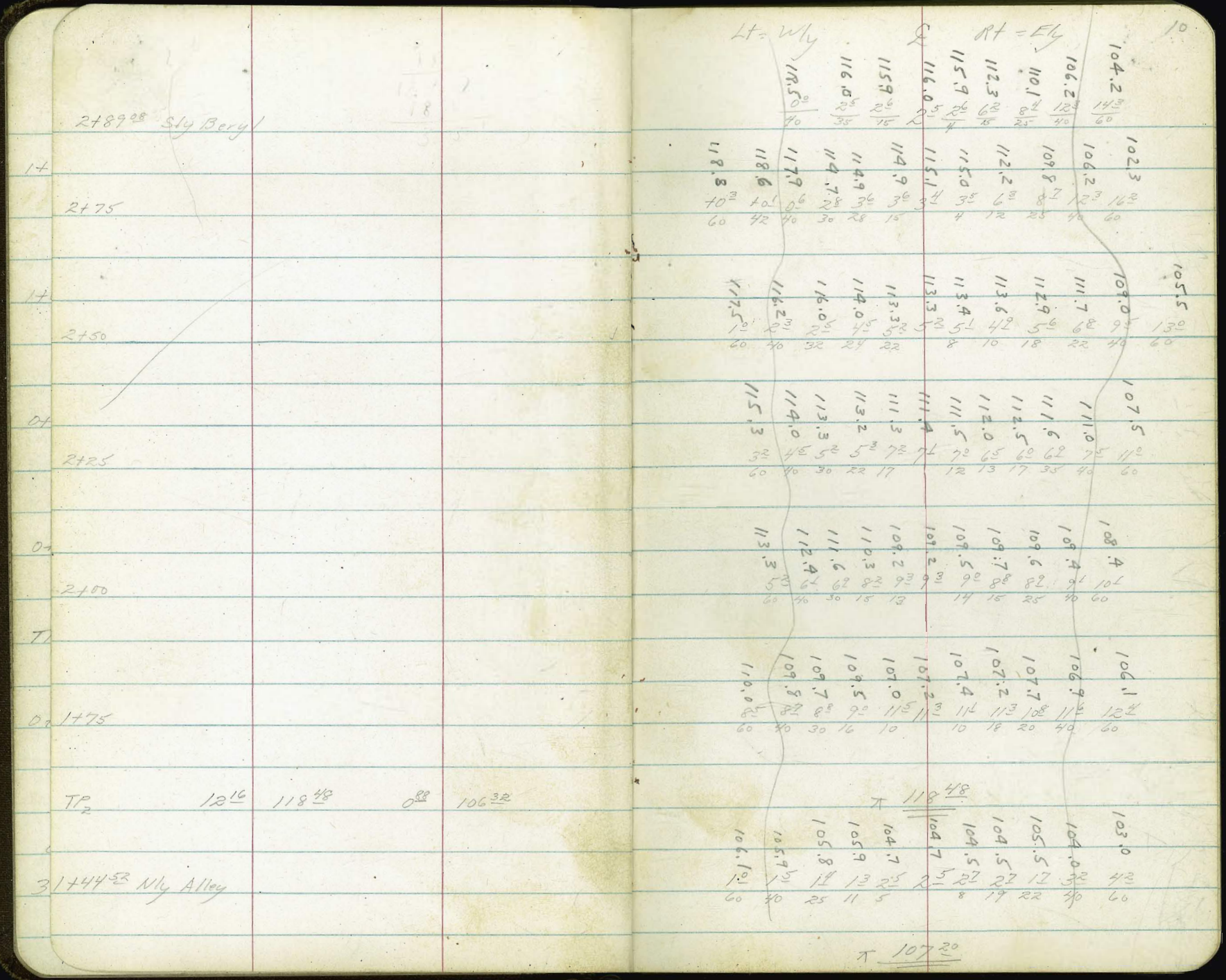
93.8	13.4	60
94.3	12.9	40
94.5	12.7	25
94.8	12.4	15
94.9	12.3	
95.5	11.7	12
95.4	11.8	24
96.0	11.2	26
97.8	9.4	34
98.0	9.2	40
96.4	10.8	60

⊼ 107.20

91.5	5.5	60
91.9	4.8	40
92.2	4.5	25
92.6	4.1	15
92.5	4.2	
92.9	3.8	10
92.5	4.2	30
96.0	0.7	34
96.0	0.7	40
95.2	1.5	60

89.4	7.3	40
89.3	7.4	25
89.9	6.8	15
90.1	6.6	
90.5	6.2	10
89.8	6.9	25
90.7	6.0	35
92.4	4.3	38
92.9	3.8	40

⊼ 96.66


Lt = Wly
℄
Rt = Ely
10
2789.88 Sly Beryl
14
2+75
17
2+50
04
2+25
01
2+00
TL
01
1+75
TP2 12.16 118.48 0.88 106.32
3 1744.52 Nly Alley

1+00					
0+75					
TP4	12^{13}	140^{26}	0^{33}	128^{13}	
0+50					
0+25					
0+00 = 2+49.08	Nly Beryl				
2+19.08 ℄ Beryl St					
TP3 BM	10^{56}	128^{46}	0^{58}	117^{90}	℄ int Hub Beryl & Randall (Sly)

132.5 / 7^{8} / 40 — 132.1 / 8^{2} / 25 — 132.1 / 8^{3} / 22 — 132.9 / 7^{4} / 15 — 132.9 / 7 — 132.8 / 7^{5} / 15 — 132.7 / 7^{6} / 18 — 133.1 / 7^{3} / 25 — 132.6 / 7^{2} / 30 — 132.5 / 7^{8} / 40

129.3 / 11^{0} / 40 — 129.1 / 11^{2} / 25 — 129.4 / 10^{9} / 20 — 129.1 / 11^{2} / 17 — 129.3 / 11^{0} — 129.1 / 11^{2} / 12 — 128.6 / 11^{7} / 20 — 127.7 / 12^{6} / 25 — 127.2 / 13^{1} / 40

π 140^{26}

126.7 / 1^{8} / 40 — 125.4 / 3^{1} / 28 — 125.3 / 3^{2} / 25 — 126.0 / 2^{5} / 15 — 126.1 / 2^{4} — 126.0 / 2^{5} / 15 — 125.2 / 3^{3} / 25 — 123.8 / 4^{7} / 40

124.5 / 4^{0} / 40 — 122.7 / 5^{8} / 25 — 123.3 / 5^{2} / 15 — 123.6 / 4^{9} — 123.5 / 5^{0} / 15 — 119.6 / 8^{9} / 25 — 118.4 / 10^{1} / 40

122.1 / 6^{4} / 40 — 121.0 / 7^{5} / 26 — 119.9 / 8^{6} / 25 — 120.8 / 7^{2} / 15 — 121.0 / 7^{5} / ℄ Nly — 121.0 / 7^{5} / 9 — 120.1 / 8^{4} / 15 ℄ Sly — 118.3 / 10^{2} / 25 — 113.5 / 15^{0} / 40 — 111.6 / 16^{2} / 55

60 — 117.8 / 10^{7} / 40 — 118.5 / 10^{0} / 30 — 118.2 / 10^{3} / 15 ℄ Nly — 118.2 / 10^{3} / ℄ Sly — 118.0 / 10^{5} / 2 — 114.1 / 14^{4} / 9 — 110.5 / 18^{0} / 34 — 108.6 / 19^{9} / 40 — 105.7 / 21^{8} / 43 — 103.2 / 23^{3} / 60

π 128^{46}

1+64.73 Nly Geranium or Poinsetta on E. Randall [extended] from Sly

1+44.73 ℄ Geranium or Poinsetta

TP5 BM 11.55 148.70 3.11 137.15 [Top Lath on SW Prop Cor Randall & Geranium]

1+24.73 Sly Geranium or Poinsetta

Lt = Wly ℄ Rt = Ely

Station							
1+64.73	142.2 $\frac{6.5}{40}$	142.7 $\frac{6.0}{25}$	141.2 $\frac{7.5}{18}$	141.6 7.1	141.5 $\frac{7.2}{12}$	141.7 $\frac{7.0}{25}$	140.9 $\frac{7.8}{40}$
1+44.73	139.5 $\frac{9.2}{40}$	139.7 $\frac{9.0}{25}$	139.5 $\frac{9.2}{12}$	139.3 9.4	139.1 $\frac{9.6}{12}$	139.0 $\frac{9.7}{25}$	139.3 $\frac{9.4}{40}$

π 148.70

Station						
1+24.73	138.4 $\frac{1?}{25}$	136.8 $\frac{3.5}{15}$	136.5 3.8	136.5 $\frac{3.8}{10}$	136.4 $\frac{3.9}{22}$	137.0 $\frac{3.3}{25}$

⊼ 140.26

(X) Sec Chalcedony
Randall Ely to Sub Line

Lt = N'ly ℄ Rt = S'ly

Sta.				
1+25				
TP.	0^{31}	81^{83}	11^{63}	81^{52}
1+00				
0+75				
0+50				
0+25				
0+00 Ely Chalcedony (Randall				
BM	7^{22}	93^{15}	85^{93}	SW 7X7 con Mon Randall & Chalcedony

See FB 2164-11 for other X sec Pendelton to Randall

1+25

									℄						
Elev	71.1	71.8	73.2	76.6	75.8	75.8	74.7	75.5	74.6	70.5	71.5	75.5	81.3	81.8	~~81.1~~ 82.5
Rod	10^{7}	10^{0}	8^{6}	5^{2}	6^{0}	6^{0}	7^{1}	6^{3}	7^{2}	11^{3}	10^{3}	6^{3}	0^{5}	0^{0}	$+0^{7}$
Dist	60	45	40	34	30	12	7	2		9	17	25	40	44	60

π 81^{83}

1+00

							℄					
Elev	83.2	81.6	83.0	79.8	79.7	78.6	79.7	81.5	81.8	83.9	83.6	82.7
Rod	10^{0}	11^{6}	10^{2}	13^{4}	13^{5}	14^{6}	13^{5}	11^{7}	11^{4}	9^{3}	9^{6}	10^{5}
Dist	60	40	35	32	15	3		3	15	25	40	60

0+75

						℄						
Elev	88.6	87.7	85.4	83.5	83.1	82.7	84.9	85.2	86.9	83.7	83.1	82.6
Rod	4^{6}	5^{5}	7^{8}	9^{7}	10^{1}	10^{5}	8^{3}	8^{0}	6^{3}	9^{5}	10^{1}	10^{6}
Dist	60	40	34	33	15		8	26	29	35	40	50

0+50

						℄								
Elev	90.4	89.5	88.2	86.3	85.9	85.6	85.3	87.0	87.0	88.0	87.5	83.0	83.0	82.1
Rod	2^{8}	3^{7}	5^{0}	6^{9}	7^{3}	7^{6}	7^{9}	6^{2}	6^{2}	5^{2}	5^{7}	10^{2}	10^{2}	11^{1}
Dist	60	40	35	32	15		8	11	24	27	31	37	40	50

0+25

					℄						
Elev	94.5	93.4	88.3	87.9	87.4	86.9	87.4	88.6	82.0	82.9	81.2
Rod	$+1^{3}$	$+0^{2}$	4^{2}	5^{3}	5^{8}	6^{3}	5^{8}	4^{6}	9^{3}	10^{3}	12^{0}
Dist	60	40	34	15		11	15	25	35	40	60

0+00

				℄						
Elev	92.9	90.3	87.5	87.2	86.6	85.9	86.2	87.0	84.6	~~82.2~~ 82.8
Rod	0^{3}	2^{2}	4^{7}	6^{0}	6^{6}	7^{3}	7^{0}	6^{3}	8^{6}	11^{0}
Dist	40	38	15		10	20	22	29	32	40

π 93^{15}

BM starting pg 13			3^{17}	85^{93} ✓ 85^{93} ✓
TP3	12^{40}	89^{10}	0^{20}	76^{70}
$2+12^{68}$ Sub Line				
2+10 32^{5} Rt ℄ 12" Power Pole #R62033				
2+00				
1+87 32^{5} Rt ℄ deadman				
1+85 5^{5} Lt to Sly end (outlet) 36" RCP				
1+80 45^{0} Lt to Nly end (inlet) 36" RCP				
1+75				
TP2	6^{43}	76^{90}	11^{36}	70^{47}
1+50				

Lt-Nly ℄ Rt-Sly

77.6	76.9	75.9	72.9	71.9	71.4	71.62	67.9	66.1	64.3	63.5	62.5
10^{7}	0^{0}	1^{0}	4^{0}	5^{0}	5^{5}	5^{28}	9^{0}	10^{8}	12^{6}	13^{4}	14^{4}
60	50	40	34	15	2	on Hub	8	16	20	40	60

73.9	72.6	72.0	71.7	71.2	67.4	65.6	64.5	63.7	63.3
3^{0}	4^{3}	4^{9}	5^{2}	5^{7}	9^{5}	11^{3}	12^{4}	13^{2}	13^{6}
60	40	35	21	8		5	20	40	60

65.47 / 11^{43} / 5.5 ←

65.47 / 11^{43} / 5^{5} ie

67.47 / 9^{43} / 45^{0} ie

70.1	69.2	71.1	71.7	71.8	71.3	66.4	65.1	65.6	65.3	64.8	66.2	65.0
6^{8}	7^{7}	5^{8}	5^{2}	5^{1}	5^{6}	10^{5}	11^{8}	11^{3}	11^{6}	12^{1}	10^{7}	9^{9}
60	45	40	39	20	10		10	16	30	40	48	60

HI 76^{90}

69.6	69.6	71.1	73.5	73.2	73.4	72.6	68.6	67.3	68.1	71.3	77.7
12^{2}	12^{2}	10^{7}	8^{3}	8^{6}	8^{4}	9^{2}	13^{2}	14^{5}	13^{7}	10^{5}	4^{1}
60	43	40	36	34	20	7		2 / 7	30	40	60

HI 81^{83}

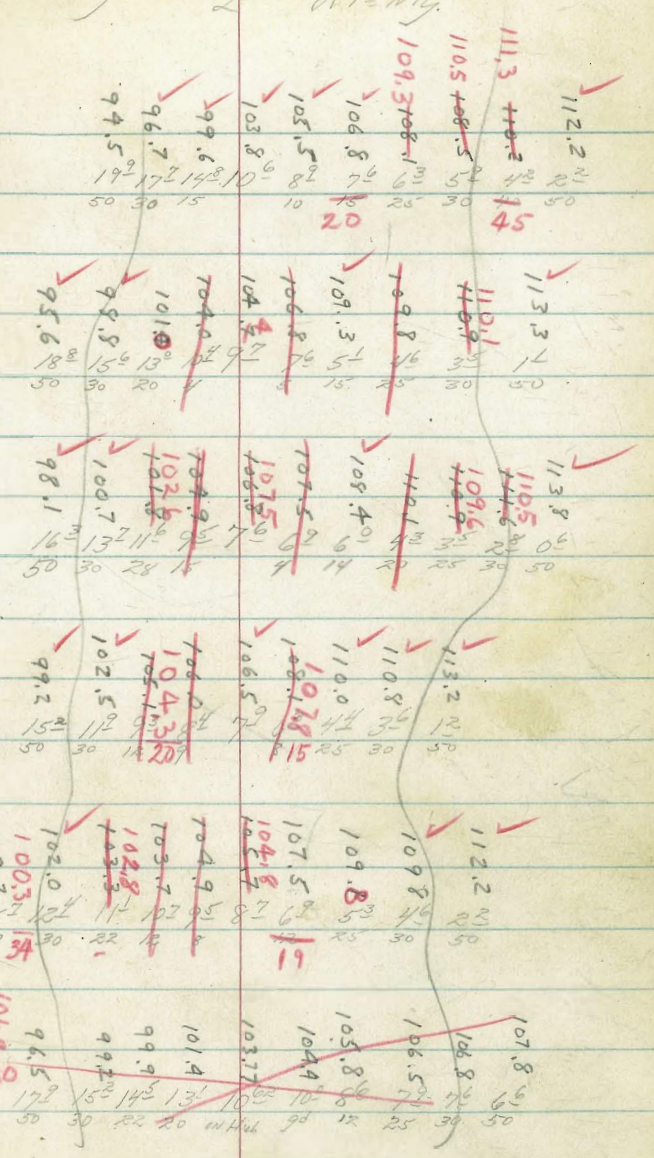
"X" Sec, Beryl St

Ely Line Sub to Ely Line Pendleton

Lt = Sly

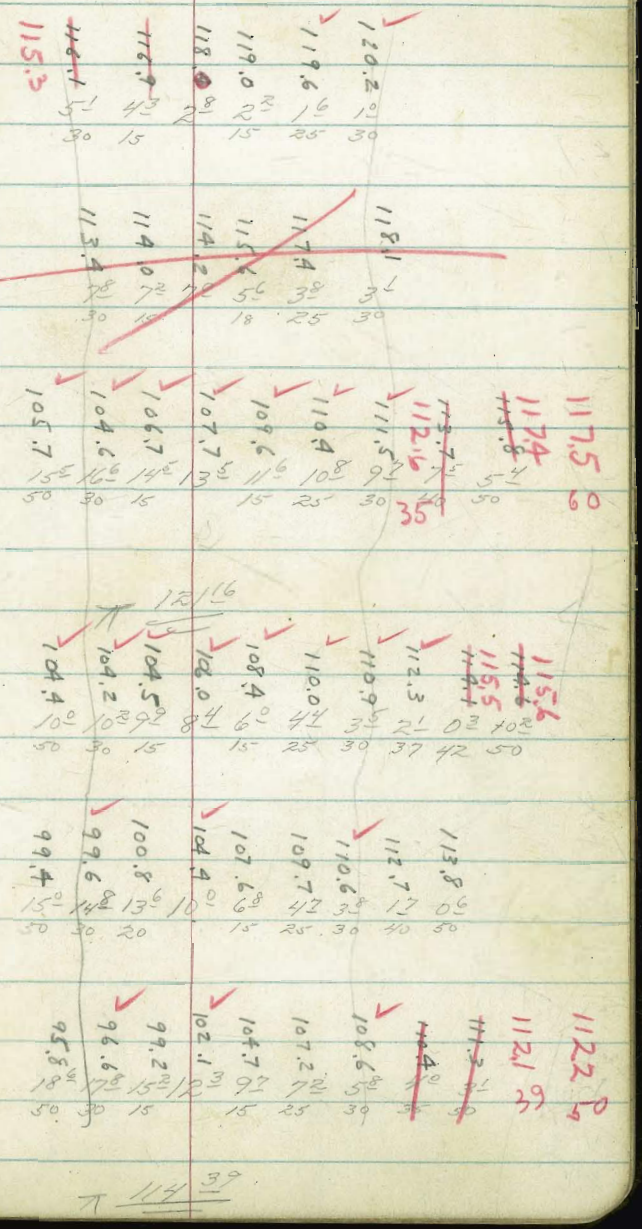
℄

Rt = Nly.



				1179.90	Int Hub Randall Sly
TR BM		10.64	128.54	3.26	117.90 Beryl
2+52.04	E Randall Sly				
2+42.04	Ely Randall to Mly				
2+12.04	Ely Line Randall Sly				
TR2		12.25	121.16	5.48	108.91
2+00					
1+75					
1+50					

Lt. Sly | Rt. Mly



Lt = Sly ℄ 112.5 Rt = Nly

4+25

113.2	111.6	111.7	~~113.6~~	~~112.0~~ 112.1	112.8	114.7	116.7	119.6	
15^{3}	16^{9}	16^{8}	~~12^{9}~~	16^{5}	15^{7}	13^{8}	11^{8}	8^{9}	
50	30	15	~~4~~	4	23	25	30	50	

4+00

116.5	117.9	117.3	116.6	114.7	114.1	115.1	118.3	119.8	121.7
12^{0}	11^{1}	11^{2}	11^{9}		14^{4}	13^{4}	10^{2}	8^{7}	6^{8}
50	30	25	9	5		20	25	30	50

3+75

118.4	119.5	120.0	115.7	115.6	116.5	119.5	122.2	122.7	124.4
10^{1}	9^{0}	8^{5}	12^{8}	12^{9}	12^{0}	9^{5}	6^{3}	5^{8}	4^{1}
50	30	12	5		18	21	25	30	50

3+50

119.2	120.7	121.5	116.7	116.7	117.5	120.4	124.1	124.5	126.0
9^{3}	7^{8}	7^{0}	11^{8}	11^{8}	11^{0}	8^{1}	4^{4}	4^{0}	2^{5}
50	30	14	9		16	20	25	30	50

3+25

119.3	120.1	120.7	117.0	117.1	117.7	120.8	123.1	123.4	123.5	124.8
9^{2}	8^{4}	7^{8}	11^{5}	11^{4}	10^{8}	7^{7}	5^{4}	5^{1}	5^{0}	3^{7}
50	30	20	~~4~~ 18		13	17	21	25	30	50

2+92.04 Wly Randall

~~116.1~~ 119.1	116.3	117.2	117.9	118.9	119.3	~~120.6~~	121.0
12^{4}	12^{2}	11^{3}	10^{6}	10^{1}	9^{2}	~~7^{9}~~	7^{5}
30	25	12		15	25	~~27~~	30

2+67.04 ℄ Randall Nly

115.9	~~116.2~~	~~117.2~~	118.1	~~119.4~~	~~120.4~~	120.9
12^{6}	~~12^{3}~~	~~11^{3}~~	10^{4}	~~9^{1}~~	~~8^{1}~~	7^{9}
30	~~25~~	~~12~~		~~15~~	~~25~~	30

π 128^{54}

Station				
6+00				
5+75				
5+50				
		5+00 to 5+75 Full of Trash		
	Note	~~5+00 to 5+50~~ undesirable fill		
5+25				
TP5	3.57	108.75	11.34	105.18
5+00				
4+75				
4+50				
TP4	1.19	116.52	13.21	115.33

Lt = S'ly — ℄ — Rt = N'ly

Station											
6+00	103.3 +1.5/50	110.7 +1.2/30	110.5 +1.7/15	104.5 4.3/5	104.0 4.8	104.5 4.3/10	104.4 4.4/25	105.0 3.8/30	104.4 4.4/50		
5+75	110.1 +1.3/50	108.7 0.1/30	107.8 1.0/20	101.0 7.8/5	101.2 7.6	103.3 5.5/3	103.6 5.2/15	103.3 5.5/25	101.6 7.2/30	99.3 9.5/35	99.1 9.7/50 (104.2)
5+50	94.8 14.0/50	91.2 17.6/30	92.6 16.2/15	98.4 10.4	102.8 6.0/8	103.3 5.5/25	103.6 5.2/30	104.1 4.7/50			
			Toe Fill								
5+25	84.2 24.6/50	88.0 20.8/30	90.6 18.2/20	99.7 9.1	103.4 5.4/8	104.0 4.8/25	104.4 4.4/30	105.0 3.8/50			
			Toe Fill								
			HI 108.75								
5+00	88.5 28.0/50	91.8 24.7/30	94.6 21.9/14	102.3 14.2	105.5 11.0/5	105.0 11.5/6	105.6 10.9/25	106.0 10.5/30	112.9 3.6/45	113.8 2.7/50	
4+75	95.0 21.5/50	97.9 18.6/30	103.5 13.0/7	106.6 9.9	107.7 8.8/3	~~108.3~~ 107.7 8.2/25	109.6 6.2/30	115.3 1.2/35	119.4 +2.9/50		
4+50	102.1 14.4/50	103.5 13.0/30	105.5 11.0/9	110.5 6.0	109.8 6.7/2	110.6 5.9/27	111.7 4.8/25	116.2 0.3/30	112.0 +4.5/50		

OK

HI 116.52

7+70			
7+40^{69} L. Rt 24°04'		taken on split	
7+25			
7+00			
6+75			
6+50			
6+25			
TP$_{6}$	11^{88}	116^{60} 4^{03}	104^{72}

Lt = S/y ℄ Rt = N/y

					℄					
	110.7 / 5^{9} / 50	111.2 / 5^{4} / 30	111.8 / 4^{8} / 15	113.9 / 2^{7} / 10	114.0 / 2^{6}	114.1 / 2^{5} / 12	114.1 / 2^{5} / 25	114.5 / 2^{1} / 30	115.9 / 0^{7} / 50	
		110.8 / 5^{8} / 50	111.0 / 5^{6} / 30	111.8 / 4^{8} / 14	112.5 / 4^{1}	112.6 / 4^{0} / 15	112.9 / 3^{7} / 25-5	112.8 / 3^{8} / 30	114.1 / 2^{5} / 50	
	110.9 / 5^{7} / 50	111.1 / 5^{5} / 30	111.4 / 5^{2} / 15	112.3 / 4^{3} / 7	112.0 / 4^{6}	112.0 / 4^{6} / 13	112.2 / 4^{4} / 25	112.5 / 4^{1} / 30	113.9 / 2^{7} / 50	
	112.0 / 5^{6} / 50	112.2 / 5^{4} / 30	112.1 / 4^{5} / 10	111.5 / 5^{1} / 3	108.0 / 8^{6}	110.9 / 5^{7} / 5	111.6 / 5^{0} / 25	111.8 / 4^{8} / 30	113.6 / 3^{0} / 50	
111.0 / 5^{6} / 50	111.4 / 5^{2} / 30	111.2 / 5^{4} / 16	108.3 / 8^{3} / 5	106.7 / 9^{7} / 4	106.7 / 9^{9}	109.3 / 7^{3} / 2	109.6 / 7^{0} / 15	110.2 / 6^{4} / 25	110.3 / 6^{3} / 30	112.3 / 4^{3} / 50
110.9 / 5^{7} / 50	110.9 / 5^{7} / 30	110.9 / 5^{7} / 17	106.9 / 9^{7} / 10	106.3 / 10^{3} / 4	105.9 / 10^{7}	107.2 / 9^{4} / 1	107.1 / 9^{5} / 20	107.6 / 9^{0} / 25	108.3 / 8^{3} / 30	110.7 / 5^{9} / 50
110.5 / 6^{1} / 50	110.6 / 6^{0} / 30	111.0 / 5^{6} / 13	106.0 / 10^{6} / 5	105.5 / 11^{1} / 2	104.6 / 12^{0}	105.4 / 11^{2} / 6	105.5 / 11^{1} / 20	106.0 / 10^{6} / 25	106.7 / 9^{9} / 30	109.1 / 7^{5} / 50

⊼ 116^{60}

9+75

9+50

9+25

9+00

8+63[13] Wly Quincy to Sly taken along line of

8+41[22] Wly Quincy to Nly taken along line of

8+19[31] E Quincy to Nly taken along line of

7+97[40] Ely Quincy taken along line of

TP7 11[88] 126[18] 2[30] 114[30]

Lt = Sly ℄ Rt = Nly

	123.1	123.3	124.2	124.7	125.4	125.6	126.0	126.5	127.2	
	3.1/50	2.9/30	2.0/15	1.5	0.8/15	0.6/24	0.0/25	+0.9/30	+1.0/50	
	121.7	122.3	123.2	124.2	124.8	125.1	125.4	125.9		
	4.5/50	3.9/30	3.0/15	2.0	1.4/17	1.1/25	0.8/30	0.3/50		
119.8	122.2	123.1	122.8	123.4	124.0	124.4	124.5	125.1		
6.4/50	4.0/30	3.1/23	3.4/18	2.8	2.2/15	1.8/25	1.7/30	1.1/50		
120.0	121.6	122.4	122.2	122.4	122.7	123.3	123.5	123.7	124.2	
6.2/50	4.6/30	3.8/25	4.0/15	3.8	3.5/13	2.9/22	2.7/25	2.5/39	2.0/50	
115.2	118.9	120.2	120.4	121.1	121.5	121.9	122.4	122.6	123.1	
11.0/50	7.3/32.8	6.0/25	5.8/13	5.1	4.7/13	4.3/25	3.8/26	3.6/32.8	3.1/50	
113.4	116.3	119.0	119.1	119.6	120.3	120.8	121.2	122.3		
12.8/50	9.9/32.8	7.2/15	7.1/10	6.6	5.9/15	5.4/25	5.0/32.8	3.9/50		
111.3	112.1	114.6	117.5	117.7	118.6	119.0	119.6	120.5		
14.9/50	14.1/40	11.6/32.8	8.7/16	8.5	7.6/12	7.2/25	6.6/32.8	5.7/50		
111.1	111.3	112.1	114.8	115.5	115.9	116.2	117.2	118.7	119.0	120.0
15.1/50	14.9/32.8	14.1/28	11.4/20	10.7/15	10.3	10.0/13	9.0/25	7.5/30	7.2/32.8	6.2/50

HI 126[18]

11+25'					
TP10	11^{87}	152^{52}	0^{95}	140^{65}	
11+00					
10+75'					
10+50					
TP9	11^{78}	141^{60}	0^{85}	129^{82}	
10+25'					
10+00					
TP8 B.M.	12^{99}	130^{67}	8^{50}	117^{68}	ON Hub 84193 & 1st Beryl "Quincy Nly

Lt-Sly ℄ Rt=Nly

Elev.	135.3	136.2	137.2	137.8	138.7	138.9	139.5	139.8	141.5
Rod	17^2	16^3	15^3	14^7	13^8	13^6	13^0	12^7	11^0
Dist.	50	30	15		12	24	25	30	50

HI 152^{52}

Elev.	134.0	134.8	135.1	135.4	136.0	136.5	137.4	137.6	138.9
Rod	7^6	6^8	6^5	6^2	5^6	5^0	4^2	4^0	2^7
Dist.	50	30	15		10	22	25	30	50

Elev.	133.2	133.3	132.5	132.5	132.8	133.5	134.1	134.8	135.1	136.0
Rod	8^4	8^3	9^2	9^2	8^8	8^1	7^5	6^8	6^5	5^6
Dist.	50	30	20	15		10	24	25	30	50

Elev.	129.0	129.6	130.2	130.2	130.6	131.3	131.9	132.4	133.8
Rod	12^6	12^0	11^4	11^4	11^0	10^3	9^7	9^2	7^8
Dist.		30	25	15		12	25	30	50

HI 141^{60}

Elev.	126.8	127.4	128.0	128.4	128.7	129.5	130.2	130.0	130.7
Rod	3^9	3^3	2^7	2^3	2^0	1^2	0^5	0^7	0^0
Dist.	50	30	15		12	25	26	30	50

Elev.	124.7	125.1	125.9	126.2	126.7	127.1	127.7	127.7	128.7
Rod	6^1	5^6	4^8	4^5	4^0	3^6	3^0	3^2	2^0
Dist.	50	30	15		12	20	25	30	50

HI 130^{67}

13+00				
TP11	8.81	158.89	2.44	150.08
12+75				
12+50				
12+25				
12+00				
11+75				
11+50				

Lt = Sly ℄ Rt = Nly

Sta.						℄					
13+00	139.7 19.3/50	145.6 13.3/35	146.8 12.1/30	147.8 11/24	148.6 10.3/15	150.1 8.8	151.4 7.5/13	152.0 6.9/25	152.5 6.4/30	153.7 5.2/50	
					⊼ 158.89						
12+75	136.5 16.0/50	143.3 9.2/30	144.3 8.3/25	146.9 5.6/20	147.3 5.2/15	149.1 3.4	149.9 2.6/10	150.7 1.8/25	151.0 1.5/30	152.3 0.2/50	
12+50	139.6 12.9/50	144.7 7.8/30	146.4 6.1/20	146.9 5.6/12		147.8 4.7	148.6 3.9/12	149.3 3.2/25	149.9 2.6/30	151.4 1.1/50	
12+25	142.9 9.6/50	144.5 8.0/30	145.6 6.9/15			146.3 6.2	146.8 5.7/12	147.5 5.0/25	148.0 4.5/30	149.6 2.9/50	
12+00	142.5 10.0/50	143.0 9.5/30	143.6 8.9/15			144.4 8.1	145.0 7.5/10	145.3 7.2/24	146.0 6.5/25	146.7 5.8/30	148.1 4.4/50
11+75	140.4 12.1/50	141.4 11.1/30	141.8 10.7/15			142.5 10.0	143.1 9.4/9	143.5 9.0/24	144.2 8.3/25	144.3 8.2/30	145.4 7.1/40; 145.7 6.8/50
11+50	137.9 14.6/50	138.9 13.6/30	139.3 13.2/20	139.4 13.1/15		140.3 12.2	140.9 11.6/12	141.4 11.1/24	142.0 10.5/25	142.3 10.2/30	143.9 8.6/50

π 152.52

TP_{13} BM			1^{15}	168^{69}	℄ Hub Geranium Ely Pendelton
TP_{12}	12^{55}	169^{84}	1^{60}	157^{29}	set stub to check into later on Geranium
$14+32^{06}$	Ely Pendelton taken along Line of.				
14+00					
13+75					
13+50					
13+25					

Station	Lt = Sly					℄	Rt = Nly			
$14+32^{06}$		131.7 27^{2}/50	134.1 24^{8}/32^{8}		135.9 23^{0}/15	136.7 22^{2}	139.2 19^{2}/17		141.9 17^{0}/32^{8}	146.2 12^{7}/50
14+00		136.1 22^{8}/50	145.2 13^{2}/30		149.0 9^{2}/15	152.2 6^{7}	152.9 6^{0}/12	153.6 5^{3}/25	153.6 5^{3}/30	156.2 2^{7}/50
13+75		141.1 17^{8}/50	151.1 7^{8}/30		152.2 6^{7}/12	152.7 6^{2}	153.1 5^{8}/12	154.1 4^{8}/25	154.7 4^{2}/30	156.4 2^{5}/50
13+50		142.6 16^{3}/50	150.1 8^{8}/30	151.1 7^{8}/25	150.9 8^{0}/15	152.1 6^{8}	152.9 6^{0}/12	153.8 5^{1}/25	154.4 4^{5}/30	155.9 3^{0}/50
13+25	140.9 18^{0}/50	141.2 11^{7}/35	148.3 10^{6}/30	149.6 9^{3}/25	149.9 9^{0}/15	150.9 8^{0}	152.1 6^{8}/13	152.6 6^{3}/25	153.1 5^{8}/30	154.7 4^{2}/50

HI 158^{89}

X Sec Geranium or Poinsetta

1+00				
0+75				
T. P_{2}	10^{63}	144^{08}	1^{56}	133^{45}
0+50				
0+25				
0+00 Ely P.L. line				
TP_{1}	6^{79}	135^{01}	12^{92}	128^{22}
BM = TP_{5} pg. 12	3^{99}	141^{14}		137^{15} top lath S.W. Prop cor. Geranium / Randall

Lt. Sly ℄ Rt. Nly

Station											
1+00	127.8 16^{3} / 40	130.9 13^{2} / 25	132.1 12^{0} / 20	134.0 10^{1} / 17	134.0 10^{1} / 10	134.8 9^{3}	134.7 9^{4} / 8	134.8 9^{3} / 15	137.1 7^{0} / 18	137.6 6^{5} / 20	141.6 2^{5} / 40
0+75	126.9 17^{2} / 40	130.3 13^{8} / 22	131.6 12^{5} / 20	132.2 11^{9} / 18	133.0 11^{1} / 8	133.2 10^{9}	133.1 11^{0} / 7	133.1 11^{0} / 15	136.1 8^{0} / 19	136.1 8^{0} / 20	139.9 4^{2} / 40

⊼ 144^{08}

Station										
0+50	124.8 10^{2} / 40	127.5 7^{5} / 20	128.4 6^{6} / 18	130.1 4^{9} / 10	130.3 4^{7}	130.6 4^{4} / 7	130.7 4^{3} / 14	133.6 1^{4} / 18	133.9 1^{1} / 20	138.0 $+3^{0}$ / 40
0+25	119.7 15^{3} / 40	120.9 14^{1} / 20	121.0 14^{0} / 16	125.3 9^{2} / 6	125.9 9^{1}	127.1 7^{9} / 9	127.4 7^{6} / 15	129.3 5^{2} / 18	129.4 5^{6} / 20	134.5 0^{5} / 40
0+00	115.0 20^{0} / 40	116.2 18^{8} / 20	118.2 16^{8} / 10	122.31 12.70 on Hub	124.1 10^{9} / 5	124.6 10^{4} / 12	125.0 10^{0} / 20	130.5 4^{5} / 40		

⊼ 135^{01}

Lt = Sly ℄ Rt = Nly

2+41.80 Ely RANDALL ST. to SOUTH

	Lt = Sly				℄			Rt = Nly		
										146.4
									144.9	
								143.2		
							142.1			
						140.7				
					139.3					
				138.2						
			136.9							
2+41.80 Ely RANDALL ST. to SOUTH			7½	5½	4⅝	3¼	2⅛	0⅔	+0⅝	+2⅜
			20	10		10	20	30	40	50
									144.3	146.6
				138.6				142.5		
			137.1				141.1			
		136.3				139.9				
	134.0				139.7					
2+21	10⅓	7⅞	7⅒	5⅝	4¼	4½	3⅛	1⅝	+0½	+2⅝
	40	25	20	12		10	20	30	35	50
									144.9	
								142.3		
							139.5			
						138.9				
					138.7					
				138.4						
			137.9							
		135.2								
	134.3									
2+00	13⅔	9⅞	8⅞	6½	5¼	5¼	4⅙	1⅞	+0⅝	
	40	25	20	16	10		10	17	20	40
										144.9
									140.6	
								140.0		
							138.3			
						137.7				
					137.7					
				137.3						
			136.9							
		135.0								
	132.8									
1+75	12⅔	11⅜	9⅛	7⅔	6¼	6¼	5⅝	4⅛	3⅝	+0⅝
	40	25	20	16	12		8	15	18	20
										143.1
									139.5	
								138.9		
							137.1			
						136.5				
					136.7					
				136.3						
			133.2							
		132.5								
	129.1									
1+50	12⅝	11⅝	10⅔	7⅝	7¼	7⅝	7⅒	5⅔	4⅝	1⅒
	40	22	20	14		8	14	18	20	40
										142.7
									139.0	
								138.5		
							136.2			
						135.7				
					135.9					
				135.3						
			133.2							
		132.1								
	129.1									
1+25	15⅔	12⅝	10⅔	8⅛	8½	8¼	7⅔	5⅙	5¼	1¼
	40	25	20	14		7	14	18	20	40

T 1440

Station										
	Lt=S'ly					℄				Rt=N'ly
4+00	132.8 / 9.3 / 40	134.6 / 7.5 / 24	137.3 / 4.8 / 18	137.4 / 4.7 / 10		137.9 / 4.2	138.6 / 3.5 / 8	138.9 / 3.2 / 15	140.8 / 1.3 / 18	140.9 / 1.2 / 20	142.9 / +0.8 / 40
3+75	133.7 / 8.4 / 40	135.8 / 6.3 / 25	137.9 / 4.2 / 20	138.1 / 4.0 / 18	138.5 / 3.6 / 9	138.6 / 3.5	139.0 / 3.1 / 8	139.7 / 2.4 / 15	141.2 / 0.9 / 18		143.7 / +1.6 / 40
3+50	133.6 / 8.5 / 40	135.7 / 6.4 / 25	137.9 / 4.2 / 20	138.7 / 3.4 / 18		138.9 / 3.2	139.2 / 2.9 / 8	139.5 / 2.6 / 15	142.3 / +0.2 / 18	142.9 / +0.8 / 20	144.0 / +1.9 / 40
3+20	133.4 / 8.7 / 40	135.3 / 6.8 / 26	138.1 / 4.0 / 20	139.0 / 3.1 / 18	139.0 / 3.1 / 10	139.0 / 3.1	139.4 / 2.7 / 8	139.8 / 2.3 / 15	142.1 / 0.0 / 19	142.1 / 0.0 / 20	144.1 / +2.0 / 40

T.P.3 T.B.M. 2.86 142.09 4.85 139.23 ℄ RANDALL ST. ℄ GERANIUM

Λ 142.09

Station								
2+91.80 W'ly RANDALL ST. to SOUTH	137.1 / 7.0 / 20	138.3 / 5.8 / 18	138.7 / 5.4 / 10	139.6 / 4.5 (℄)	140.0 / 4.1 / 10	140.9 / 3.2 / 18	142.4 / 1.7 / 20	142.3 / +1.8 / 40
2+66.80 ℄ RANDALL ST. to SOUTH (26665 Rec.)	136.3 / 7.8 / 20	138.2 / 5.9 / 10	139.5 / 4.6 (℄)	140.8 / 3.3 / 10	142.0 / 2.1 / 20	143.5 / 0.6 / 30	144.5 / +0.4 / 40	

Λ 144.08

5+20

T.P.5 2^{30} 121^{21} 12^{20} 118^{91} ON ESTub 5+16

T.P.4 1^{81} 131^{11} 12^{79} 129^{30}

5+15 = E/y Rim

5+00

4+75

4+50

4+25

Lt = S/y ℄ Rt = N/y

110.2 $11^{0}/40$ 110.7 $10^{5}/20$ 111.0 $10^{2}/10$ 111.2 10^{0} 111.4 $9^{3}/15$ 111.6 $9^{6}/20$ 113.2 $8^{0}/40$

T 121^{21}

126.1 $16^{0}/40$ 126.8 $15^{3}/20$ 128.3 $13^{8}/10$ 129.9 12^{11} 131.0 $11^{1}/10$ 132.8 $9^{3}/20$ 135.1 $7^{0}/40$

132.1 $10^{0}/40$ 133.5 $8^{6}/20$ 134.1 $8^{0}/10$ 135.5 6^{4} 136.1 $6^{0}/10$ 136.9 $5^{2}/20$ 138.9 $3^{2}/40$

132.4 $9^{7}/40$ 133.9 $8^{2}/20$ 135.1 $7^{0}/10$ 135.8 6^{3} 136.3 $5^{8}/10$ 137.1 $5^{0}/18$ 137.1 $5^{0}/20$ 139.7 $2^{4}/40$

131.8 $10^{3}/40$ 133.7 $8^{4}/20$ 135.4 $7^{2}/15$ 135.5 $7^{6}/10$ 136.2 5^{7} 136.7 $5^{4}/10$ 137.1 $5^{0}/20$ 139.5 $2^{6}/40$

131.1 $11^{0}/40$ 133.3 $8^{8}/25$ 134.6 $7^{5}/20$ 136.2 $5^{9}/15$ 136.5 $5^{6}/10$ 136.8 5^{3} 137.3 $4^{8}/8$ 137.8 $4^{3}/16$ 138.8 $3^{3}/20$ 142.1 $1^{0}/40$

T 142^{09}

					Lt=Sly			℄			Rt=Nly	
6+40					121.7 11.5/40	124.1 9.1/20	125.5 7.7/10	127.2 6.0	128.2 5.0/15	128.7 4.5/20	129.7 3.5/28	132.2 1.0/40
6+30					120.0 13.2/40	122.3 10.9/20	122.7 10.5/10	124.8 8.4	126.2 7.0/4	126.7 6.5/15	127.0 6.2/20	127.6 5.6/40
T.P.6	12.65	133.17	0.69	120.52				⊼ 133.17				
6+15					111.6 9.6/40	115.2 6.0/20	117.7 3.5/10	120.20 1.20	120.4 0.8/15	120.5 0.7/20	120.5 0.7/40	
5+95					104.8 16.4/40	105.9 15.3/20	106.8 14.4/10	107.2 14.0	107.4 13.8/15	107.8 13.4/20	110.1 11.1/40	
5+60					106.0 15.2/40	106.5 14.7/20	106.9 14.3/10	107.2 14.0	107.8 13.4/15	107.9 13.3/20	108.8 12.4/40	
5+34					106.3 14.9/40	107.0 14.2/20	107.2 14.0/10	107.2 14.0	107.5 13.7/15	107.6 13.6/20	108.8 12.4/40	

⊼ 121.21

TP7 BM	12.51	140.57	5.11	128.06	℄ int Hub Quincy & Geranium
8+17.52 ℄ int Geranium & Quincy taken along line Quincy					
7+95.61? ~~7+85.61~~ Ely Quincy to South taken along line Quincy					
7+65.19 ∡ 24°03'30" Rt taken on split					
7+50					
7+25					
7+00					
6+70					

Lt = Sly ℄ Rt = Nly

126.2 $\frac{7.0}{21.9}$ 126.3 $\frac{6.9}{10}$ 128.1 5.1 129.6 $\frac{3.6}{15.2}$ 130.1 $\frac{3.1}{21.9}$

126.2 $\frac{7.0}{21.9}$ 126.9 $\frac{6.3}{10.5}$ 127.5 5.7 128.9 $\frac{4.3}{15.2}$ 129.7 $\frac{3.5}{21.2}$ 131.7 $\frac{1.5}{30}$

123.8 $\frac{9.4}{40}$ 125.4 $\frac{7.8}{20.5}$ 123.0 $\frac{10.2}{10}$ 127.0 6.2 128.6 $\frac{4.6}{15.34}$ 129.2 $\frac{4.0}{20.5}$ 131.3 $\frac{1.9}{40}$

123.6 $\frac{9.6}{40}$ 125.2 $\frac{8.0}{20}$ 126.9 $\frac{6.3}{10}$ 127.7 $\frac{5.5}{7}$ 128.1 5.1 129.3 $\frac{3.9}{15}$ 129.8 $\frac{3.4}{20}$ 131.7 $\frac{1.5}{40}$

124.2 $\frac{9.0}{40}$ 126.2 $\frac{7.0}{20}$ 128.5 $\frac{4.7}{8}$ 129.4 3.8 130.8 $\frac{2.4}{15}$ 131.4 $\frac{1.8}{20}$ 133.8 $\frac{+0.6}{40}$

122.9 $\frac{10.3}{40}$ 126.0 $\frac{7.2}{20}$ 128.5 $\frac{4.7}{10}$ 130.5 2.7 131.9 $\frac{1.3}{8}$ 132.5 $\frac{0.7}{15}$ 132.9 $\frac{0.3}{20}$ 135.5 $\frac{+2.3}{40}$

122.1 $\frac{11.1}{40}$ 125.2 $\frac{8.0}{20}$ 127.6 $\frac{5.6}{10}$ 129.6 3.6 132.4 $\frac{0.8}{15}$ 132.7 $\frac{0.5}{20}$ 134.9 $\frac{+1.7}{40}$

⊼ 133.17

TP8	12^{05}	152^{43}	0^{9}	140^{38}

Lt = Sly | ℄ | Rt = Nly

9+50

133.4	135.0	136.4	137.1	138.0	139.0	139.9	142.1
7^{3}	5^{6}	4^{2}	3^{5}	2^{6}	1^{6}	0^{7}	$+1^{5}$
40	20	10		12	15	20	40

9+25

131.6	133.1	134.3	134.9	136.1	136.6	137.6	141.4
9^{0}	7^{5}	6^{3}	5^{7}	4^{5}	4^{0}	3^{0}	$+0^{8}$
40	20	10		13	15	20	40

9+00

129.6	131.3	132.3	132.0	134.1	134.6	135.6	137.1
11^{0}	9^{3}	8^{3}	7[illegible]	6^{5}	6^{0}	5[illegible]	3^{5}
40	20	10		13	15	26	40

8+75

129.0	129.2	129.6	130.4	131.1	132.1	133.1	134.0	136.4
12^{6}	11^{4}	11^{0}	10^{2}	9^{5}	8^{5}	7^{5}	6[illegible]	4^{2}
40	20	15	10		11	15	20	30. 40

8+50

127.0	128.6	129.1	128.7	129.3	130.1	131.6	132.4	132.8	135.1
13^{6}	12^{0}	11^{5}	11[illegible]	11^{3}	10^{5}	9^{0}	8^{3}	7^{8}	5^{5}
40	20	15	10		12	15	17	20	40

8+39 43 Wly Quincy to South taken along Line Quincy

128.0	127.9	128.8	130.3	132.5	132.2	134.6
12^{0}	12^{2}	11^{8}	10^{3}	8[illegible]	8[illegible]	6^{0}
22	15		15	20	22	40

T1 140^{57}

Lt = Sly ℄ Rt = Nly

Station				
11+00				
TP9	12.89	164.60	0.72	151.71
10+75				
10+50				
10+25				
10+00				
9+75				

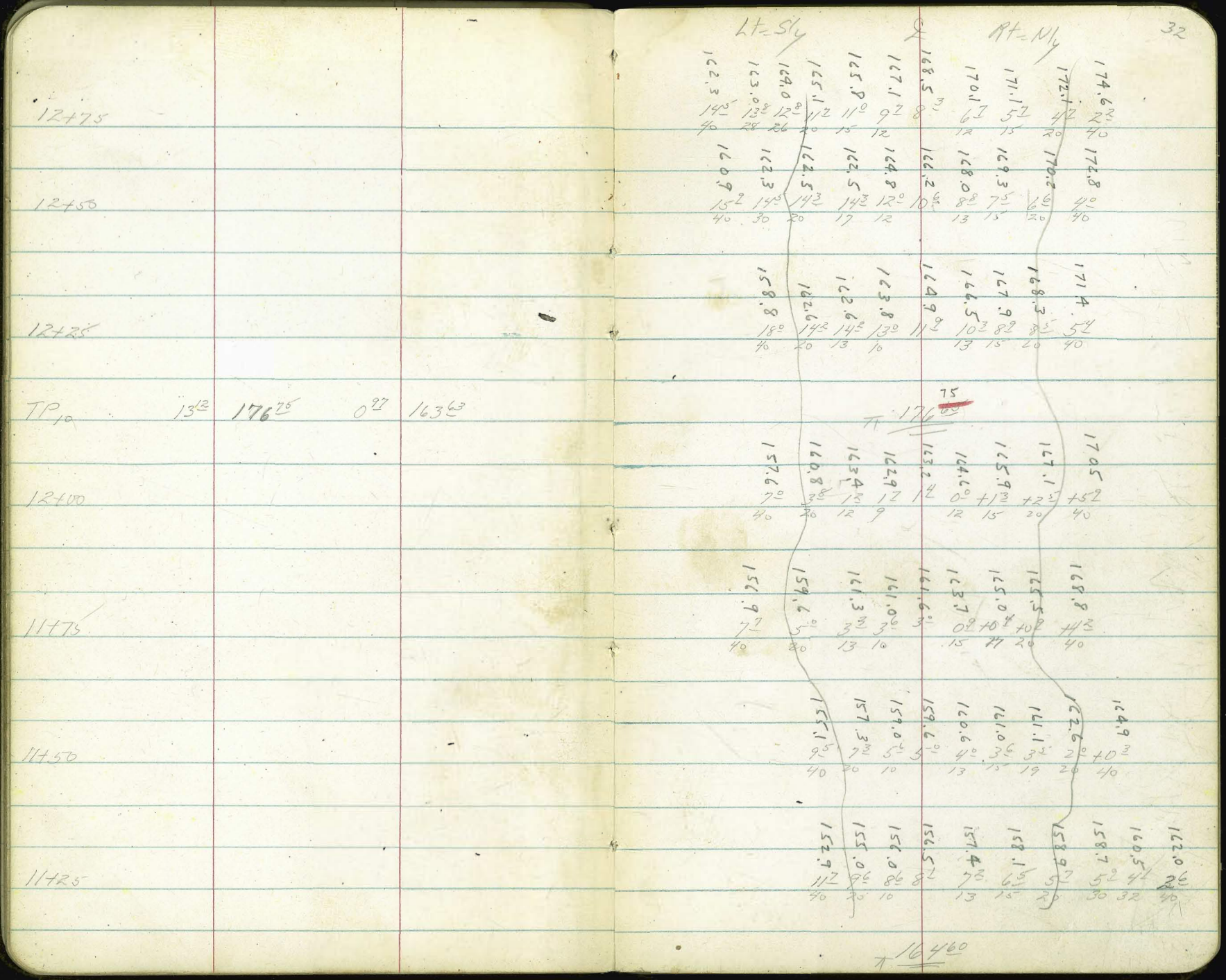
Cross sections (elevation / rod / distance):

Station										
11+00	149.9 / 14.7 / 40	152.0 / 12.6 / 20	153.1 / 11.5 / 10	153.7 / 10.9	154.4 / 10.2 / 11	155.6 / 9.0 / 15	156.5 / 8.1 / 20	157.2 / 7.4 / 27	157.3 / 7.3 / 38	158.7 / 5.9 / 40

HI 164.60

Station									
10+75	148.1 / 4.3 / 40	149.4 / 3.0 / 20	150.8 / 1.6 / 10	151.0 / 1.4	152.1 / 0.3 / 15	152.4 / 0.0 / 20	155.4 / +3.0 / 40		
10+50	144.3 / 8.1 / 40	145.8 / 6.6 / 20	146.8 / 5.6 / 10	147.6 / 4.8	148.0 / 4.4 / 11	149.1 / 3.3 / 15	149.6 / 2.8 / 16	149.7 / 2.7 / 20	152.2 / 0.2 / 40
10+25	142.4 / 10.0 / 40	144.1 / 8.3 / 20	145.1 / 7.3 / 10	145.8 / 6.6	146.2 / 6.2 / 13	146.4 / 6.0 / 15	147.8 / 4.6 / 20	150.4 / 2.0 / 40	
10+00	139.4 / 13.0 / 40	141.4 / 11.0 / 20	142.4 / 10.0 / 10	143.0 / 9.4	143.8 / 8.6 / 13	144.3 / 8.1 / 15	145.4 / 7.0 / 20	148.1 / 4.3 / 40	
9+75	136.0 / 16.4 / 40	137.6 / 14.8 / 20	139.4 / 13.0 / 10	139.8 / 12.2	141.0 / 11.4 / 13	141.8 / 10.6 / 15	142.5 / 9.9 / 20	144.9 / 7.5 / 40	

HI 152.43


Lt=Sly
℄
Rt=Nly
12+75
12+50
12+25
TP10
13.12
176.75
0.97
163.63
12+00
11+75
11+50
11+25
176.75
164.60

Station					Notes
					168.69 ✓ −0.03
TP_{12} BM pg 23			12.66	168.66 ✓	TP_{12} BM pg 23 ℄ Hub Geranium & Pendelton
14+29.94 Ely Pendelton taken along line of Pendelton					
14+00					
13+75					
13+50					
TP_{11}	6.31	181.32	1.74	175.01	on POT Hub 13+54.07
13+25					
13+00					

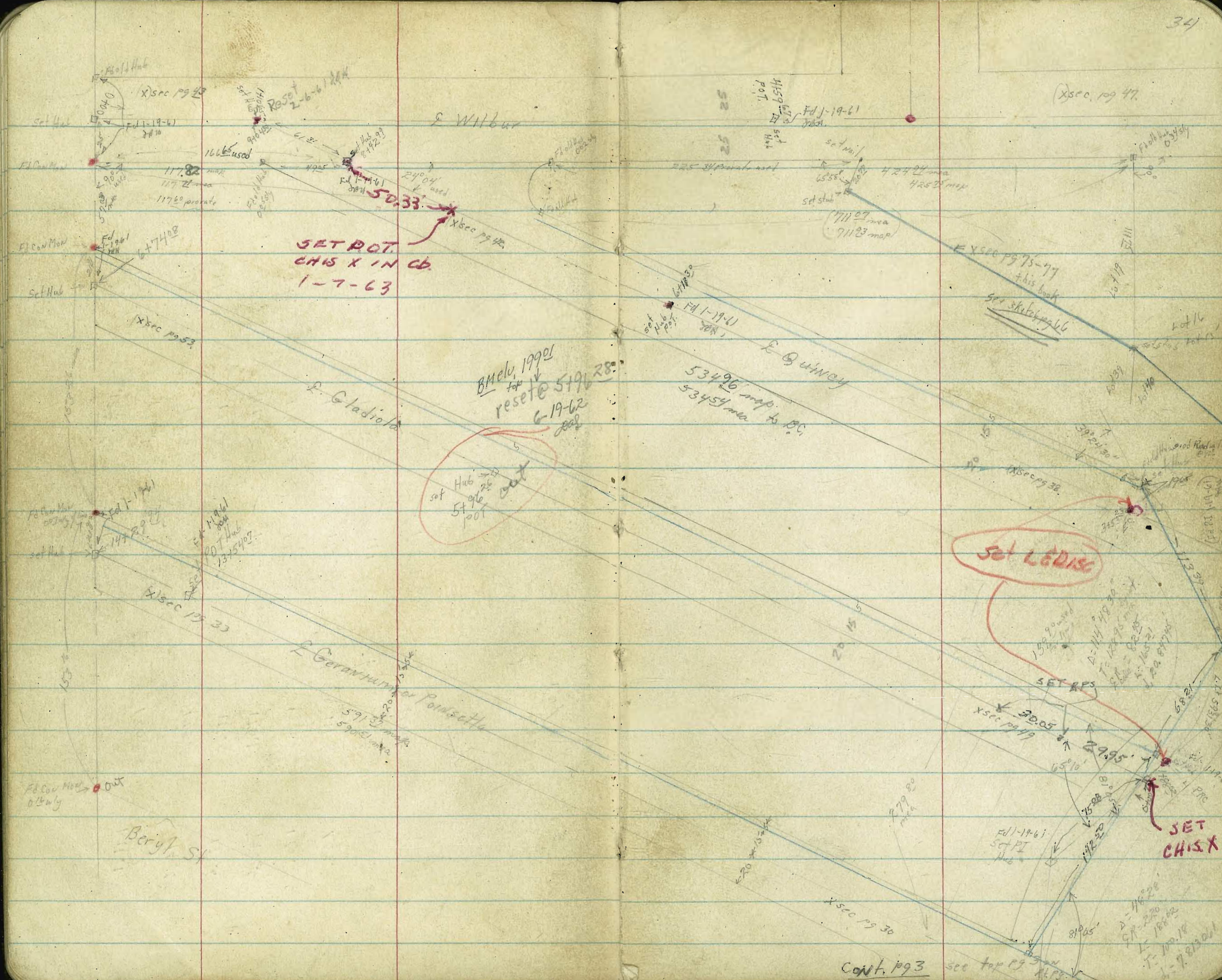
Lt-Sly ℄ Rt-Nly

Station												
14+29.94		157.8 23.5/40	162.4 18.9/22	163.0 18.3/20	165.9 15.4/10	168.7 12.6 (℄)	171.3 10.0/10	173.6 7.2/22	176.9 4.4/40			
14+00			162.7 18.6/40	168.7 12.6/20	172.2 9.2/10 rim	174.9 6.4 (℄)	176.7 4.6/10	176.7 4.6/15	177.5 3.8/20	180.7 0.6/40		
13+75	161.2 20.1/50	166.1 15.2/40 rim	167.7 13.6/25	170.8 10.5/20	172.3 9.0/18	173.2 8.1/10	174.7 6.6 (℄)	176.5 4.8/11	179.2 2.1/15	181.3 0.0/18	181.7 +0.4/20	184.6 +3.3/40
13+50		165.9 15.4/40	171.0 10.3/20	173.3 8.0/12	175.0 6.3 (℄)	177.0 4.3/12	179.0 2.3/15	179.8 1.5/17	180.3 1.0/20	183.2 +1.9/40		

⊼ 181.32

Station									
13+25	165.8 11.0/40	169.4 7.4/20	170.4 6.4/15	171.6 5.2/12	173.3 3.5 (℄)	175.1 1.7/12	177.0 +0.2/15	177.6 +0.8/20	180.6 +3.8/40
13+00	164.7 12.1/40	168.3 8.5/20	169.8 7.0/13	170.8 6.0 (℄)	172.6 4.2/13	173.6 3.2/15	174.6 2.2/20	177.1 +0.3/40	

⊼ 176.75



(X)sec pg 43
Reset 2-6-61
℄ Wilbur
Set Hub
Fd Con Mon
SET ROT. CHIS X IN Cb. 1-7-63
50.33'
Xsec pg 42
Set Hub
Xsec pg 53
℄ Gladiola
BM elev 199.01 for reset @ 5+96.28
6-19-62
set Hub 5+96.28 pot
out
Xsec pg 33
℄ Geranium or Poinsetta
591.33 map
590.81 mea
Fd Con Mon Out
Beryl St
(X)sec pg 47
Fd 1-19-61
set Nail
424.24 mea
425.28 map
711.27 mea
711.23 map
℄ Xsec pg 75-77 this book
See sketch pg 66
Lot 16
℄ Quincy
534.96 map to B.C.
534.54 mea
(X)sec pg 38
Set L&Disc
SET R.P.S
Xsec pg 49
30.05
29.95
SET CHIS.X
Fd 1-19-61 Set PI Hub
Xsec pg 30
Cont. pg 3

see top pg 3

"X" Sec Quincy St

Beryl to Wilbur

Station				Lt-Wly	℄	Rt-Ely
0+25	3° 15.3265'			131.1 / 10.2 / 40; 128.7 / 1.7 / 20; 128.5 / 1.4 / 10	128.5 / 1.4	128.6 / 1.3 / 10; 128.2 / 1.7 / 20; 128.3 / 1.6 / 40
c=24.99						
{0+00 ±s {1+09.92 BC	0° 00'	section taken @ 90° to line		127.4 / 2.5 / 40; 127.7 / 2.2 / 20; 128.1 / 1.8 / 16; 126.4 / 3.5 / 12	126.4 / 3.5	126.1 / 3.8 / 14; 127.3 / 2.6 / 17; 126.6 / 3.3 / 20; 126.9 / 3.0 / 40
1+09.32	Sly Poinsetta or Geranium St	taken along line of		128.1 / 1.8 / 21.9; 128.4 / 1.5 / 17; 126.6 / 3.3 / 14	126.3 / 3.6	125.9 / 4.0 / 14; 122.2 / 3.7 / 21.2
0+75				125.2 / 4.7 / 40; 125.1 / 4.8 / 20; ~~125.2~~ / 4.2 / 17; 124.7 / 5.2 / 13	124.1 / 5.8	124.1 / 5.8 / 10; 123.7 / 6.2 / 20; 123.5 / 6.4 / 40
0+50				~~124.3~~ 123.7 / 5.6 / 40; 123.3 / 6.6 / 30; ~~123.9~~ 123.2 / 6.0 / 20; ~~123.4~~ / 5.7 / 17; 123.3 / 6.6 / 14	122.8 / 7.1	122.5 / 7.4 / 10; 122.2 / 7.7 / 20; 121.7 / 8.2 / 40
0+25				~~122.7~~ 122.6 / 6.8 / 40; ~~122.4~~ 121.8 / 7.5 / 20; 121.5 / 8.4 / 10	121.4 / 8.5	120.9 / 9.0 / 10; 121.3 / 8.6 / 15; 120.8 / 9.1 / 20; 120.0 / 9.2 / 40
0+00	Nly line Beryl St	taken along line of		121.6 / 8.3 / 30; 121.3 / 8.6 / 21.9; 120.4 / 9.5 / 15	119.9 / 10.0	118.8 / 11.1 / 12; 119.7 / 10.2 / 16; 119.0 / 10.9 / 21.9; 118.3 / 11.6 / 30
BM+P8	12.25	129.93	117.68	Exist. Hub Beryl-Quincy N'ly pg 21		

Note Secs in Red Taken 2-8-61

HI 129.93

1+50	19°31.9590'				
1+25	16°16.6325'				
TP2	12.02	150.22	2.76	138.20	ON PI Hub
1+00	13°01.3060'				Δ = 48°58' 1/2Δ = 24°29' R = 220' L = 188.02 T = 100.18 d1 = 7.813061'
0+75	9°45.9795'				
0+50	6°30.6580'				
0+38	6.5 Lt	Int Hub sewer line Quincy & Geranium			
TP1 BM	12.89	140.96	1.86	128.07 (128.06)	℄ Int Hub Geranium & Quincy

pg 23 TP1

Lt - Wly — ℄ — Rt - Ely — 36

1+50:

Elev.	152.6	150.5	149.4	148.7 / 148.1	148.2	148.2	148.9	148.3	148.2	145.1	144.2
Rod	+2.4	+0.3	0.8	1.4	2.0	2.0	1.3	1.2	2.0	5.1	6.0
Dist.	40	20	10		10.3 to ℄ sewer	16	19	20	23	29	40

1+25:

Elev.	146.6	144.6	144.0	145.7	144.2	144.7	144.0	144.3	143.2	140.7	139.8
Rod	3.6	5.6	6.3	4.5	6.0	5.5	6.8	5.9	7.0	9.5	10.4
Dist.	40	20	17	12	5		11.2 to ℄ sewer	18	20	25	40

HI 150.22

1+00:

Elev.	141.0	139.2	139.0	141.2	140.2	140.0	140.6	137.5	136.8
Rod	0.0	1.8	2.0	+0.2	0.8	1.0	0.9	3.5	4.2
Dist.	40	20	15	10		10 to ℄ sewer	20	28	40

0+75:

Elev.	136.6	135.8	135.2	136.5	135.8	135.7	136.5	134.5	133.6
Rod	4.4	5.2	5.8	4.5	5.2	5.3	4.5	6.5	7.4
Dist.	40	20	12	9		6.0 to ℄ sewer	20	25	40

0+50:

Elev.	133.6	133.0	133.0	131.3	131.6	131.6	131.5	131.9	130.7
Rod	7.4	8.0	8.0	9.7	9.4	9.4	9.5	9.1	10.3
Dist.	40	20	15	10	1.5 to ℄ sewer		10	20	40

129.32 — 11.64 — 6.5 on Hub

HI 140.96

2+50	21°32.5426'				
2+47	9= Rt to Sewer ℄ Lt. Hub				Δ = 114°48'30" meas ½Δ = 57°24'15" made by int T = 128^{85} meas ER = 82^{45} calc L = 165^{21} d_1 = 20.84745'
2+25	12°51.3563'				
					on rock
TP_4	12^{43}	174^{25}	0^{36}	161^{82}	
c = 24^{90}					
2+00	4°10.1700'				
c = 11^{97}					
	0°00' ↗				
$1+88^{02}$	24°29.00' ↙	P.R.C.			
$1+81^{5}$	5= Rt to ℄ sewer int Hub Gladiola + Quincy				
c = 13^{02}					
1+75	22°47.2855'				
					on rock
TP_3	12^{78}	162^{18}	0^{82}	149^{40}	

Lt = Wly ℄ Rt = Ely

(ok)
169.8 / 4^{5} / 40 — 168.3 / 6^{0} / 20 — 167.8 / 6^{5} / 18 — 165.9 / 8^{4} / 15 — 166.0 / 8^{3} — 166.5 / 7^{8} / 7^{0} to ℄ Sewer — 166.7 / 7^{6} / 20 — 167.0 / 7^{3} / 22 — 163.8 / 10^{5} / 26 — 163.0 / 11^{3} / 40

165.80 / 8^{40} / 9^{0} to ℄ Sewer on Hub

167.6 / 6^{7} / 40 — 166.5 / 7^{8} / 27 — 164.1 / 10^{2} / 20 — 162.0 / 12^{3} / 15 — 161.9 (161.4) / 12^{4} — 161.8 (162.0) / 12^{5} / 14 (12) to ℄ Sewer — 162.7 / 11^{6} / 20 — 159.6 / 14^{7} / 25 — 158.2 / 16^{1} / 40

⊼ 174^{25}

(ok)
164.8 / $+12^{6}$ / 40 — 163.6 / $+1^{4}$ / 25 — 161.7 / 0^{5} / 20 — 157.9 / 4^{3} / 12 — 157.1 / 5^{1} — 157.0 / 5^{2} / 1^{0} to ℄ sewer — 157.0 / 5^{2} / 15 — 155.8 / 6^{4} / 20 — 154.8 / 7^{4} / 40

(H)
164.3 / $+12^{1}$ / 40 — 162.7 / $+10^{5}$ / 26 — 160.2 / 2^{0} / 20 — 159.3 / 2^{9} / 16 — 155.8 / 6^{4} / 10 — 154.15 / 8^{038} on Hub Grd — 154.6 / 7^{6} / 3^{5} to ℄ sewer — 154.4 / 7^{8} / 20 — 154.2 / 8^{0} / 26 — 151.7 / 10^{5} / 34 — 150.9 / 11^{3} / 40

153.41 / 8^{77} / 5^{0} on Hub

158.2 / 4^{0} / 40 — 157.0 / 5^{2} / 30 — 154.9 / 7^{3} / 20 — 153.5 / 8^{7} / 15 — 153.1 / 9^{1} / 10 — 152.7 / 9^{5} — 152.7 / 9^{5} / 6^{5} to ℄ Sewer — 152.7 / 9^{5} / 18 — 153.5 / 8^{7} / 20 — 153.4 / 8^{8} / 23 — 151.6 / 10^{6} / 27 — 150.2 / 12^{0} / 33 — 149.5 / 12^{2} / 40

⊼ 162^{18}

Lt = SWly ℄ Rt = NEly

4+00

25' Stations per D. Smith

3+75

TP 8M 12.81 193.27 π 4.92 180.46 ON ℄, Hub ℄ 3+53.23

3+53.23 EC, 57° 25' 25.250"

C = 28.13

3+25 47° 36' 10.15"

3+00 38° 54' 9.152"

TP 6 12.10 185.38 0.99 173.28

2+75 30° 13' 7.289" Nail POC.

	180.6	181.6	184.8	186.1	187.0	188.9	191.9	194.3
BNL	12.7	11.7	8.5	7.2	6.3	4.4	1.4	+3.0
	40	32	20		13	15	20	40

	179.6	181.9	183.4	184.0	186.9	190.8	190.8	193.8
	13.7	11.4	9.9	9.3	6.4	2.5	2.5	+0.5
	40	20		11	15	18	20	40

193.27 π

	177.3	179.4	179.8	180.7	180.46	181.5	183.4	186.9	188.1	188.7	191.6
BNL	8.1	6.0	5.6	4.7	4.92	3.9	2.0	7.5	+2.2	+3.8	+6.8
	40	20	18	38	on Hub	8	12	15	16	20	40

	175.1	176.6	176.3	177.0	177.1	178.1	182.9	181.7	181.4
BNL	10.3	8.8	9.1	8.4	8.3	7.3	2.5	3.7	4.2
	40	20	15	22 +2 Sewer		7	15	20	40

	173.2	173.4	173.0	173.9	173.9	174.6	176.0	176.7	176.6
BNL	12.2	12.0	12.4	12.0	11.5	10.8	9.4	8.2	8.8
	40	20	15	7 +℄ Sewer		12	20	24	40

℄ 185.38

	171.9	171.2	170.2	169.5	169.7	170.1	171.7	168.5
BNL	24	3.7	4.1	4.8	4.6	4.2	2.6	5.8
	40	24	20	14	4.2 +℄ Sewer		20	40

℄ 174.25

Station				
5+50				
5+25				
5+00				
T.P.	12.13	205.12 ⊼	0.28	192.99
4+75				
4+50				
4+25				

193.27 ⊼

Lt = Sly ℄ Rt = Nly

Station	Left				℄	Right				
5+50 elev.	192.8	196.9	200.1		200.1 ✓	200.6	201.5	203.5	206.4	
5+50 rod	12.3	8.2	5.0		5.0	4.5	3.6	1.6	+1.3	
5+50 dist.	40	20	14			14	15	20	40	
5+25 elev.	189.9	193.5	197.4		197.7	198.3	199.3	201.4	204.4	
5+25 rod	15.2	11.6	7.7		7.4	6.8	5.8	3.7	0.7	
5+25 dist.	40	20	13			13	15	20	40	
5+00 elev.	187.1	191.1	195.2		195.3	195.9 ✓	196.6	199.5	199.6	203.0
5+00 rod	18.0	14.0	9.9		9.8	9.2	8.5	5.6	5.5	2.1
5+00 dist.	40	20	13			14	15	19	20	40

205.12 ⊼

Station	Left				℄	Right				
4+75 elev.	184.9	189.1	192.8		193.03	193.8	194.8	197.8	201.1	
4+75 rod	8.4	4.2	0.5		0.3	+0.5	+1.5	+4.5	+7.8	
4+75 dist.	40	20	14			13	15	20	40	
4+50 elev.	182.9	187.0	190.7		190.8	191.8 ✓	193.3	196.3	196.6	199.7
4+50 rod	10.4	6.3	2.6		2.5	1.5	0	+3.0	+3.3	+6.4
4+50 dist.	40	20	15			13	15	18	20	40
4+25 elev.	181.8	186.1	187.6	188.3	188.5	189.3	190.8	193.0	193.3	198.1
4+25 rod	11.5	7.2	5.7	5.0	4.8	4.0	2.5	0.3	0	+4.8
4+25 dist.	40	20	17	11		14	15	19	20	40

193.27 ⊼

Sta.				
7+00				
6+75				
6+50				
6+25				
T.P.	12.22	217.14 ⊼	0.20	204.92
6+00				
5+75				

205.12 ⊼

Lt — ℄ — Rt

7+00
- Elev.: 207.4, 209.7, 212.1, 212.1, 212.3, 214.6, 219.9
- 9.7/40, 7.4/20, 5.0/15, 5.0 (℄), 4.8/15, 2.5/20, +2.8/40

6+75
- Elev.: 205.5, 208.6, 210.3, 210.38, 210.8, 211.9, 213.3, 216.2
- 11.6/40, 8.5/20, 6.8/15, 6.8 (℄), 6.3/14, 5.2/15, 3.8/20, 0.9/40

6+50
- Elev.: 203.5, 207.1, 209.1, 208.8, 209.2, 210.7, 212.0, 214.5
- 13.6/40, 10.0/20, 8.0/16, 8.3 (℄), 7.9/14, 6.4/15, 5.1/20, 2.6/40

6+25
- Elev.: 200.6, 204.7, 207.1, 207.0, 207.3, 208.5, 210.2, 210.6, 213.5
- 16.5/40, 12.4/20, 10.0/15, 10.1 (℄), 9.8/14, 8.6/15, 6.8/19, 6.5/20, 3.6/40

217.14 ⊼

6+00
- Elev.: 198.3, 202.8, 205.1, 205.0, 205.0, 206.0, 208.2, 211.1
- 6.8/40, 2.3/20, 0/15, 0.1 (℄), 0.1/13, +0.9/15, +3.1/20, +6.0/40

5+75
- Elev.: 195.0, 196.7, 199.7, 202.8, 202.6, 203.2, 204.2, 205.8, 206.1, 209.1
- 10.1/40, 8.4/30, 5.4/20, 2.3/14, 2.5 (℄), 1.9/13, 0.9/15, +0.7/18, +1.0/20, +4.0/40

205.12 ⊼

Station				
8+25				
8+00				
T.P.	4.24	221.05 ⊼	0.33	216.81
7+75				
7+50				
7+36 (7+36)				
7+25				
		217.14 ⊼		

Station	Lt				℄			Rt
8+25	210.4 / 10.7 / 40	211.9 / 9.2 / 30	213.5 / 7.6 / 20	215.4 / 5.7 / 16	216.1 / 5.0 ✓			
8+00	210.6 / 10.5 / 40	213.5 / 7.6 / 20	215.9 / 5.2 / 15		216.4 / 4.7 ✓	216.9 / 4.2 / 10	217.9 / 3.2 / 20	
				221.05 ⊼				
7+75	209.9 / 7.2 / 40	212.7 / 4.4 / 20	215.5 / 1.6 / 13		216.1 / 1.0	216.6 / 0.5 / 15	217.3 / +0.2 / 20	219.8 / +2.7 / 40
7+50	209.1 / 8.0 / 40	212.0 / 5.1 / 20	214.1 / 3.0 / 15		215.1 / 2.0 ✓	215.7 / 1.4 / 15	216.4 / 0.7 / 20	219.3 / +2.2 / 40
7+36	208.3 / 8.8 / 40	211.8 / 5.3 / 20	214.3 / 2.8 / 15		214.4 / 2.7 (2.7)	214.9 / 2.2 / 15	217.2 / +0.1 / 20	219.7 / +2.6 / 40
7+25	208.3 / 8.8 / 40	211.2 / 5.9 / 20	213.6 / 3.5 / 15		213.8 / 3.3	214.0 / 3.1 / 15	216.5 / 0.6 / 20	219.4 / +2.3 / 40
				217.14 ⊼				

				Lt	℄ Rt
check			9.14	168.67 = 168.69	on ℄ Hub Geranium and Ely Line Pendleton See page 23
T.P.	2.10	177.81	12.97	175.71	
T.P.	1.16	188.68	11.70	187.52 = on	℄ Hub Gladiola (6+74.08) and Ely Line Pendleton
T.P.	1.37	199.22	13.19	197.85 = on	℄ Hub Wilbur (0+00) and Ely Line Pendleton
T.P.	0.37	211.04	10.38	210.67	
8+75					211.5 / 9.6 / 40 — 213.7 / 7.4 / 20 — 214.5 / 6.6 / 18 — 215.1 / 6.0
8+42.99				℄ Quincy & Ely Line Wilbur	210.8 / 10.3 / 40 — 213.6 / 7.5 / 20 — 215.2 / 5.9 / 17 — 215.51 / 5.51 on Hub
		221.05			221.05

Levels on Wilbur Street

Pendleton Ely

1+25				
1+00				
0+75				
0+50				
T.P.	12.28	222.16 ⊼	1.02	209.88
0+28				
0+00 Ely Line Pendleton				
BM	210.90 ⊼		13.05	197.85

See Page 42

Lt — ℄ — Rt

1+25

				℄			
219.8	219.1	218.2	215.0	214.7	214.2	213.3	211.7
2.4	3.1	4.0	7.2	7.5	8.0	8.9	10.5
50	25	10	6		25	30	50

1+00

				℄			
218.7	216.7	215.8	213.4	213.2	213.0	212.7	211.5
3.5	5.5	6.4	8.8	9.0	9.2	9.5	10.7
50	25	11	8		22	25	50

0+75

				℄			
215.7	214.3	213.4	212.0	211.9	211.9	210.8	210.4
6.5	7.9	8.8	10.2	10.3	10.3	11.4	11.8
50	25	13	8		23	25	50

0+50

		℄					
213.2	211.9	210.7	209.8	208.3	206.9	205.3	206.7
9.0	10.3	11.5	12.4	13.9	15.3	16.9	15.5
50	25		22	25	28	40	50

T.P. — 222.16 ⊼

0+28

			℄		
209.1	207.9	210.2	209.5	208.0	203.0
1.8	3.0	0.7	1.4	2.9	7.9
50	25	12		25	50

0+00

		℄		
199.2	198.6	197.8	196.0	193.8
11.7	12.3	13.1	14.9	17.1
50	25		25	50

BM — 210.90 ⊼

Sta.				
2+75				
2+50				
2+25				
T.P.	7.78	228.08 ⊼	1.86	220.30
2+00				
1+75				
1+50				

222.16 ⊼

Lt				℄			Rt
226.7	224.7	223.9	223.0	222.2	221.5	220.2	220.8
1.4	3.4	4.2	5.1	5.9	6.6	7.9	7.3
50	25	13	10		10	23	25

225.7	224.2	223.2	222.2	221.6	220.6	219.1
2.4	3.9	4.8	5.9	6.5	7.5	9.0
50	25	11	8		10	25

224.7	223.3	222.8	220.7	220.2	219.7	218.2
3.4	4.8	5.2	7.4	7.9	8.4	9.9
50	25	12	8		10	25

228.08 ⊼

223.5	221.7	221.1	219.1	218.8	217.0	214.3
+1.3	0.5	1.1	3.1	3.4	5.2	
50	25	10	6		25	40

221.1	219.8	218.8	217.6	217.2	216.1	215.6	213.8
1.1	2.4	3.4	4.6	5.0	6.1	6.6	8.4
50	25	9	6		25	46	50

220.3	219.0	218.2	216.1	215.9	215.1	215.2	213.4	212.1
1.9	3.2	4.0	6.1	6.3	7.1	7.0	8.8	10.1
50	25	9	6		25	35	41	50

222.16 ⊼

	Lt.				℄	Rt.			
4+00	227.9	225.6	223.4		222.2	220.7	219.6		216.1
	0.2	2.5	4.7		5.9	7.4	8.5		12.0
	50	25	14	11		12	25		50
3+75	227.5	225.2	223.8	222.3	221.3	220.2			216.8
	0.6	2.9	4.3	4.8	5.8	7.9			11.3
	50	25	14	11		25			50
3+50	227.6	224.5	223.9	223.5	222.5	219.9			217.0
	0.5	3.6	4.2	4.6	5.6	8.2			11.1
	50	25	14	12		25			50
3+25	227.5	225.1	224.5	223.6	222.7	221.2	220.6		217.4
	0.6	3.0	3.6	4.5	5.4	6.8	7.5		10.7
	50	25	13	10		18	25		50
3+00		227.0	225.1	223.4	222.7	221.6	221.2	220.3	217.4
		1.1	3.0	4.7	5.4	6.5	6.9	7.8	10.7
		50	25	10		17	25	35	50
2+85		226.6	224.8	224.0	222.5	221.1	221.3	220.8	219.2
		1.5	3.3	4.1	5.6	7.0	6.8	7.3	8.9
		50	25	13	10	19	22	25	40

228.08 ℄

228.08 ℄

Station					
5+50					
5+25					
T.P.	2.92	223.24 ⊼	7.76	220.32	* Rock opposite End Sewer.
5+00					
4+75					
4+50					
4+25					
		228.08 ⊼			

Cross sections (elevation, rod reading over distance):

Station	Lt				℄				Rt
5+50	219.2 4.0/50	219.8 3.4/25	220.1 3.1/14	219.7 3.5/11	219.4 ✓ 3.8	219.0 4.2/10	218.5 4.7/21	218.0 5.2/25	214.0 9.2/50
5+25	220.4 2.8/50	220.6 2.6/25	220.4 2.8/14	220.0 3.2/12	219.6 3.6	219.1 4.1/11	218.4 4.8/22	217.5 5.7/25	214.0 9.2/50
T.P.					223.24 ⊼				
5+00	221.4 6.7/50	221.2 6.9/25	221.1 7.0/14	220.6 7.5/12	220.1 ✓ 8.0	219.3 8.8/10		218.1 10.0/25	214.1 14.0/50
4+75	223.0 5.1/50	222.5 5.6/25	222.0 6.1/14	221.5 6.6/12	220.8 7.3	220.0 8.1/10		218.7 9.4/25	214.5 13.6/50
4+50	226.2 1.9/50	224.2 3.9/25	223.1 5.0/14	222.7 5.4/11	221.7 ✓ 6.4	220.5 7.6/10		218.9 9.2/25	215.1 13.0/50
4+25	226.7 1.4/50	224.9 3.2/25	223.9 4.2/14	223.1 5.0/12	222.1 6.0	219.5 8.6/18		218.8 9.3/25	216.5 11.6/50
					228.08 ⊼				

Smith

T.P.	0.82	211.04 ⊼	13.02	210.22

Lt | ℄ | Rt

7+00

200.0	202.5	201.3	201.4	202.1	201.6	203.4 ✓	200.5	199.1	198.8
11.0	8.5	9.7	9.6	8.9	9.4	7.6	10.5	11.9	12.2
50	45	42	25	18	16		25	28	50

6+75

207.4	207.0	206.7	206.3	205.5	205.6	205.0	206.3	206.2	204.0
3.6	4.0	4.3	4.7	5.5	5.4	6.0	4.7	4.8	7.0
50	25	17	15		10	20	23	25	50

T.P.

211.04 ⊼

6+50

212.2	211.9	212.2	211.2	210.2 ✓	210.2	210.3	210.2	206.9
11.0	11.3	11.0	12.0	13.0	13.0	12.9	13.0	16.3
50	25	16	14		10	20	25	50

6+25

214.6	215.0	215.3	214.9	214.7	214.7	214.4	211.7
8.6	8.2	7.9	8.3	8.5	8.5	8.8	11.5
50	25	15	13		10	25	50

6+00

216.4	217.8	218.3	218.1	217.9 ✓	217.8	217.1	213.8
6.8	5.4	4.9	5.1	5.3	5.4	6.1	9.4
50	25	14	12		10	25	50

5+75

218.2	219.0	219.4	219.1	218.9	218.4	217.7	214.3
5.0	4.2	3.8	4.1	4.3	4.8	5.5	8.9
50	25	11		10	22	25	50

223.24 ⊼ 223.24 ⊼

						Lt	℄	Rt
T.P.			6.06	180.75 = 180.46			on ℄ Hub 3+53.23 Quincy See Page 38	
T.P.	1.27	186.51	13.09	185.24	=		on top Lath near ℄ in sewer line 111.75' So. of So. Line Wilbur.	
T.P.	0.47	198.33	13.18	197.86				
		Mercy Goodness! But it goes down from here!						
7+16	Edge of Canyon					191.0	194.8	195.2
						20.0	16.2	15.8
						50	25	13
		211.04 ℄						

	Lt	℄	Rt
	197.7	196.3	194.8
	13.3	14.7	16.2
		8	25
	211.04 ℄		

193.9
17.1
50

Levels on Gladiola
Quincy to Pendleton

Lt — ℄ — Rt

1+25

149.5 151.6 154.9 158.3 159.2 160.3 161.7 163.3 163.9 169.4
16.8 14.7 11.4 8.0 7.1 6.0 4.6 3.0 2.4 +3.1
40 35 20 12 13 15 18 20 40

1+00

147.3 150.3 154.3 157.2 156.3 157.2 158.3 159.5 161.5 167.0
19.0 16.0 12.0 9.1 10.0 9.1 8.0 6.8 4.8 +0.7
40 29 20 13 11 14 15 20 40

0+75

145.5 148.5 153.5 156.4 154.8 155.4 156.4 157.1 160.0 165.0
20.8 17.8 12.8 9.9 11.5 10.9 9.9 9.2 6.3 1.3
40 30 20 12 6 14 15 20 40

0+50

145.7 147.7 151.7 155.3 153.0 153.5 155.0 155.4 158.3 166.3
20.6 18.6 14.6 11.0 13.3 12.8 11.3 10.9 8.0 0.0
40 30 20 13 5 14 15 20 40

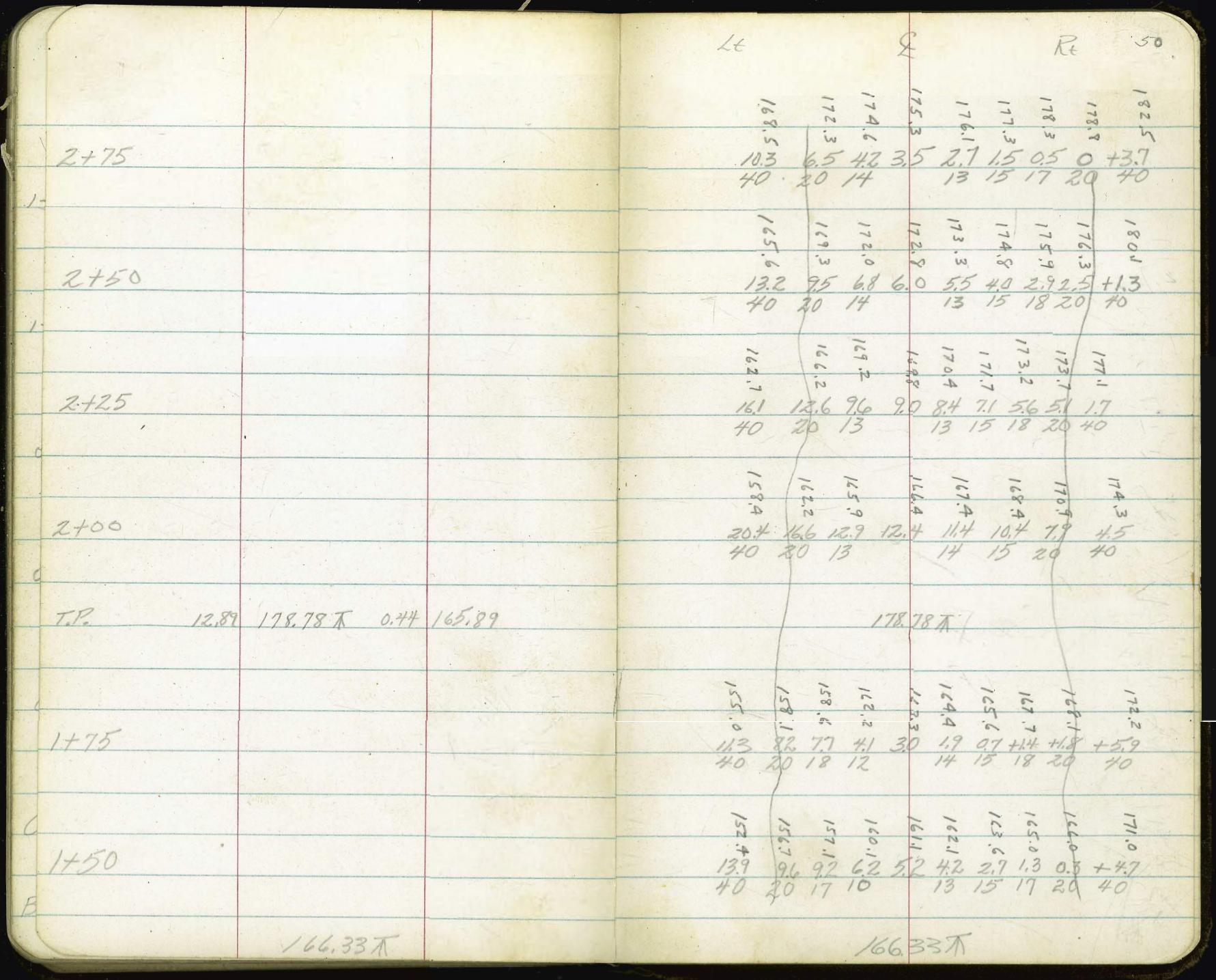
0+25

142.8 146.7 149.5 149.6 151.9 154.8 157.5 163.8
23.5 19.6 16.8 16.7 14.4 11.5 8.8 2.5
40 28 20 18 15 20 40

0+00 ℄ Gladiola and Semi-tangent Quincy

147.6 151.1 153.3 154.2 158.4
18.7 15.2 13.0 12.1 7.9
20 15 20 40

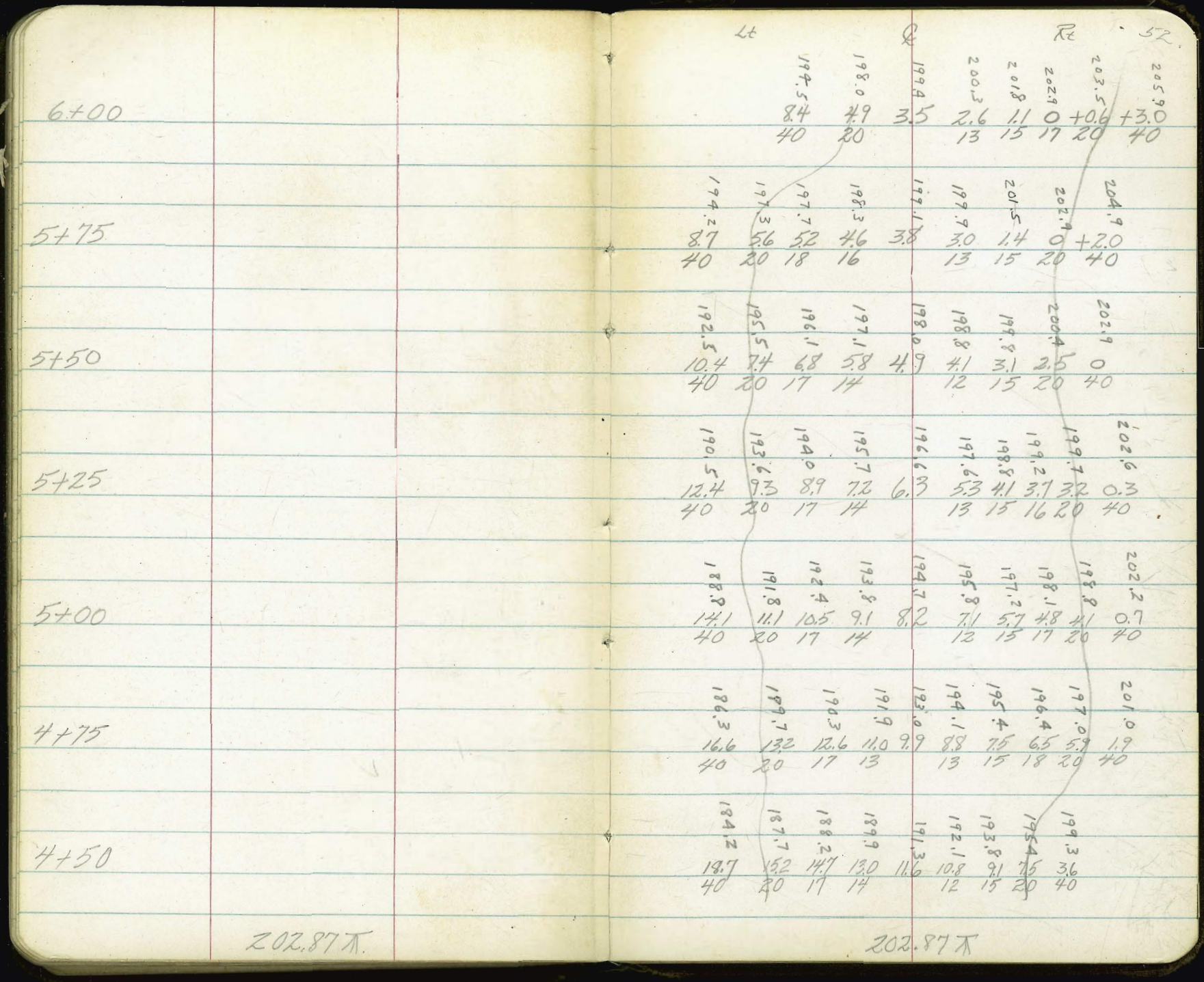
B.M. 12.18 166.33⊼ 154.15 on ℄ Hub 1+88.02 P.R.C. Quincy 166.33⊼


Lt
℄
Rt
50
2+75
2+50
2+25
2+00
T.P. 12.89 178.78 0.44 165.89
1+75
1+50
166.33
166.33

T.P.	12.10	202.87 ⊼	0.06	190.77
4+25				
4+00				
3+75				
3+50				
3+25				
T.P.	12.10	190.83 ⊼	0.05	178.73
3+00				
		178.78 ⊼		

Lt ℄ Rt 57

					189.1	190.0	191.3	192.8	193.0	197.8		
181.4	185.2	185.6	188.0									
9.4	5.6	5.2	2.8	1.7		0.8	+0.5	+2.0	+2.2	+7.0		
40	20	18	14			13	15	18	20	40		
					186.9	188.0	189.3	190.3	190.9	195.5		
180.1	184.0	185.7										
10.7	6.8	5.1		3.9		2.8	1.5	0.5	+0.1	+4.7		
40	20	15				13	15	18	20	40		
					184.8	185.5	186.6	188.1	188.6	192.7		
178.5	181.2	183.8										
12.3	9.6	7.0		6.0		5.3	4.2	2.7	2.2	+1.9		
40	20	14				13	15	18	20	40		
					182.5	183.2	184.4	185.9	186.5	190.3		
176.0	179.4	181.6										
14.8	11.4	9.2		8.3		7.6	6.4	4.9	4.3	0.5		
40	20	14				13	15	18	20	40		
					180.1	180.9	182.0	184.2	188.1			
173.8	177.0	179.2										
17.0	13.8	11.6		10.7		9.9	8.8	6.6	2.7			
40	20	14				13	15	20	40			
					190.83 ⊼							
					177.6	178.2	179.2	180.7	181.7	185.4		
171.0	174.5	175.0	176.8									
7.8	4.3	3.8	2.0	1.2		0.6	+0.4	+1.9	+2.7	+6.6		
40	20	17	14			13	15	18	20	40		
					178.78 ⊼							


52
Rt
℄
Lt
6+00
5+75
5+50
5+25
5+00
4+75
4+50
205.9 0 +3.0 40
203.5 +0.6 20
202.9 0 17
201.8 1.1 15
200.3 2.6 13
204.9 +2.0 40
202.9 0 20
201.5 1.4 15
199.9 3.0 13
199.1 3.8
202.9 0 40
200.4 2.5 20
199.8 3.1 15
198.8 4.1 12
198.0 4.9 3.5
202.6 0.3 40
199.7 3.2 20
199.2 3.7 16
198.8 4.1 15
197.6 5.3 13
196.3
202.2 0.7 40
198.8 4.1 20
198.1 4.8 17
197.2 5.7 15
195.8 7.1 12
194.7 8.2
201.0 1.9 40
197.0 5.9 20
196.4 6.5 18
195.4 7.5 15
194.1 8.8 13
193.0 9.9
199.3 3.6 40
197.5 5.4 20
192.1 10.8 12
193.8 9.1 15
191.3 11.6
202.87 ℄
202.87 ℄

check 10.94 187.53 = 187.52

6+74.08 Section taken on line of Pendleton

6+74.08 Ely Line of Pendleton

T.P. 7.88 198.47 ℄ 12.28 190.59

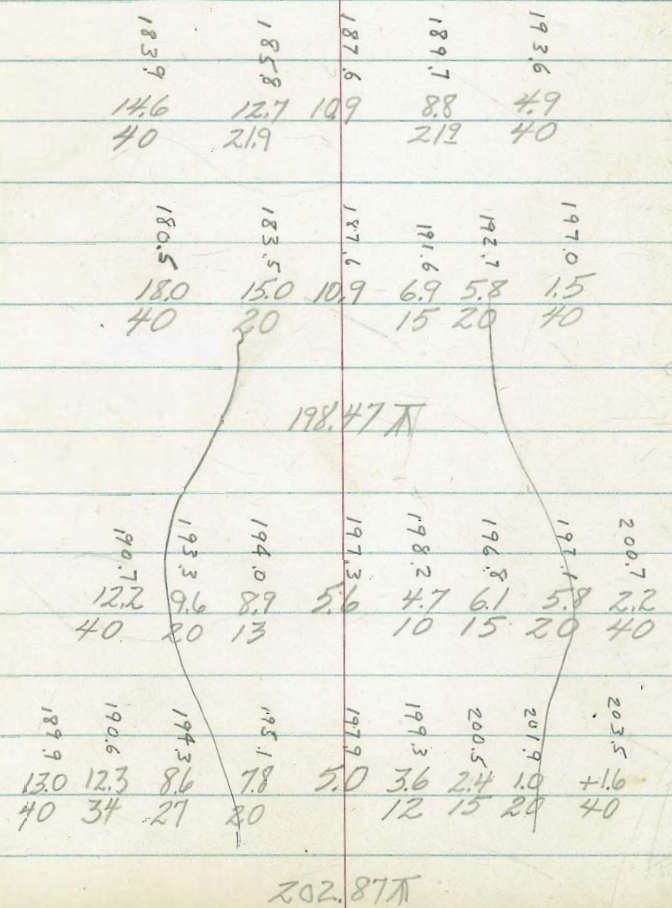
6+42

6+25

202.87 ℄

Lt. ℄ Rt.

See page 42



Levels on Randall Street
Geranium to Loring

Sta.				
1+25		1° 41.1633'		
T.P.	13.06	162.43 ⊼	2.10	149.37 on ℄ P.R.C. Hub
0+96.75		0° 00.0' / 34° 43.500' P.R.C.		
0+75		26° 55.0725'		
0+50		17° 56.7150'		
0+25		8° 58.3575'		
0+00		0° 00.0' / B.C. Randall ±2' ahead (Wly) ℄ Geranium		
BM	12.24	151.47 ⊼	3.08	139.23 on ℄ ℄ Hub Geranium & Randall see page 26
BM PS 12, 24	5.16	142.31		137.15 top Lath SW prop Cor Randall & Geranium

$\Delta = 69°27.0'$
$\Delta/2 = 34°43.5'$
℄R = 79.82' Calc.
T = 55.32'
L = 96.75'
$d_1 = 21.5343'$
chd. = 24.90 for 25' Arc

S = ℄ Sewer

Cross sections (elevation / rod / distance):

Sta.	Lt				℄				Rt
1+25	155.4 / 7.0 / 40	153.8 / 8.6 / 25	152.6 / 9.8 / 20	152.1 / 10.3 / 17	150.7 / 11.7	150.7 / 11.7 / 14 S	150.7 / 11.7 / 12	149.4 / 13.0 / 16	148.9 / 13.5 / 20 — 146.2 / 16.2 / 40
T.P.					162.43 ⊼				
0+96.75	154.3 / +2.8 / 40	152.8 / +1.3 / 20	152.8 / +1.3 / 18	151.0 / 0.5 / 14	149.6 / 1.9	148.9 / 2.6 / 10.3 S	148.6 / 2.9 / 17	148.0 / 3.5 / 20	145.5 / 6.0 / 40
0+75	152.8 / +1.3 / 40	151.5 / 0 / 20	150.7 / 0.8 / 12	148.9 / 2.6 / 7	148.3 / 3.2	147.2 / 4.3 / 13.3 S	146.8 / 4.7 / 20	143.2 / 8.3 / 50	
0+50	149.7 / 1.8 / 40	148.6 / 2.9 / 20	148.0 / 3.5 / 10	146.6 / 4.9 / 7	145.8 / 5.7	144.8 / 6.7 / 12.7 S	144.2 / 7.3 / 20	143.2 / 8.3 / 30	140.8 / 10.7 / 50
0+25	146.0 / 5.5 / 40	144.8 / 6.7 / 20	144.8 / 6.7 / 16	143.2 / 8.3 / 13	142.7 / 8.8	142.7 / 8.8 / 0.8 S	141.9 / 9.6 / 25	139.7 / 11.8 / 50	
0+00		139.1 / 12.4 / 50	139.6 / 11.9 / 35		139.7 / 11.8		140.0 / 11.5 / 35	139.4 / 12.1 / 50	
BM					151.47 ⊼				

		Lt			℄			Rt	
2+75	10° 38.3109'	163.9	161.3	160.0	159.1	159.6	157.8	156.5	153.6	152.3
		+1.5	1.1	2.4	2.8	3.8	4.6	5.9	8.8	10.1
		40	20	19	14.5 S		16	20	31	40
2+68	Approximate ℄ Aster									
2+50	9° 08.7863'	160.6	159.1	158.5		157.2	156.3	154.8	152.7	151.3
		1.8	3.3	3.9	5.2		6.1	7.6	9.7	11.1
		40	20	14.7 S			15	20	30	40
	$\Delta = 29°29.0'$									
	$\frac{\Delta}{2} = 14°44.5'$									
	$\mathcal{R} = 480.00'$									
2+25	$T = 126.30'$ 7° 39.2617'	160.2	157.8	156.8		155.9		154.3	152.0	150.2
	$L = 247.00'$	2.2	4.6	5.6	6.5			8.1	10.4	12.2
	$d_1 = 3.580985'$	40	20	14.1 S				20	28	40
	chd. = 25' for 25' Arc									
2+00	6° 09.7371'	159.4	156.2	155.2		154.5	153.5	153.2	150.5	149.2
		3.0	6.2	7.2	7.9		8.9	9.2	11.9	13.2
		40	20	12.5 S			18	20	31	40
1+75	4° 40.2125'	157.2	154.9	153.7	153.4	153.1	152.2		151.2	148.3
		5.2	7.5	8.7	9.0	9.3	10.2		11.2	14.1
		40	20	18	8.4 S		17		20	40
1+50	3° 10.6879'	156.4	154.7	153.0	151.9	151.9	151.7		150.3	147.3
		6.0	7.7	9.4	10.5	10.5	10.7		12.1	15.1
		40	24	20	4.3 S		14		20	40
		162.43 ℄					162.43 ℄			

						Lt	℄	Rt	SC
						166.5 7.7 50	165.2 9.0 12	165.5 8.7	13
0+25						165.6 8.6 32	164.4 9.8 30	163.4 10.8 6	161.0 13.2 30	156.1 18.1 50	
					164.8	164.2 9.4 50	162.8 11.4 44	162.6 11.6 42	163.0 11.2 30	162.6 11.6 20	5	160.6 13	158.5 15.7 16	154.6 19.6 30	149.4 24.8 50	15
0+00	℄ used = Subdivision Line Between Aster & Wilbur (See sketch)				9.4											
T.P.	BM	3.93	174.23 ℸ	1.79	170.30	(Just South of Wilbur. stub 32' Lt of Sta. 0+56)							174.23 ℸ			
						168.1 4.0 40	165.4 6.7 20	163.9 8.2 17	163.8 8.3 6.2 S	163.8 8.3	163.3 8.8 15	160.8 11.3 20	159.0 13.1 30	155.8 16.3 40	
3+43.75	14°	44500' E.C. (Section taken radially.)														
						166.9 5.2 40	164.5 7.6 20	162.8 9.3 16	162.1 10.0 9.5 S	162.1 10.0	161.3 10.8 16	159.9 12.2 20	158.1 14.0 24	154.7 17.4 40	
3+25	13°	37.3601'														
						165.3 6.8 40	162.9 9.2 20	161.3 10.8 17	161.0 11.1 12.5 S	159.9 12.2	159.3 12.8 15	157.3 14.8 20	153.4 18.7 40		
3+00	12°	07.8355'														
T.P.	BM	10.67	172.09 ℸ	1.01	161.42	= on	stub 21' Lt of 2+75 ℄ (close to N.W. Prop. Cor. Aster & Randall)						172.09 ℸ			
			162.43 ℸ													

T.P.	12.96	199.58 ℄	0.22	186.62
1+50				
1+25				
1+07	Approximate ℄ Wilbur			
1+00				
T.P.	12.78	186.84 ℄	0.17	174.06
0+75				
0+50				

174.23 ℄

Lt ℄ Rt 57

10

189.2	187.1	185.4	183.2	181.4	179.4	178.4
+2.4	+0.3	1.4	1.6	1.7	1.9	3.4	6.3	8.4
50	30	26	20	1		3	30	50

9

183.9	182.2	180.7	180.5	180.1	179.4	178.8	176.1	174.8
2.9	4.6	6.1	6.3	6.7	7.4	8.0	10.7	12.0
50	30	26	20	2		2	30	50

9

178.0	176.5	175.8	175.7	173.9	171.7	170.4
8.8	10.3	11.0	11.1	12.9	15.1	16.4
50	30	20		5	30	50

186.84 ℄

10

174.1	172.6	172.0	171.8	172.7	169.6	167.7	166.4
0.1	1.6	2.2	2.4	1.5	4.6	6.5	7.8
50	30	26	20		7	30	50

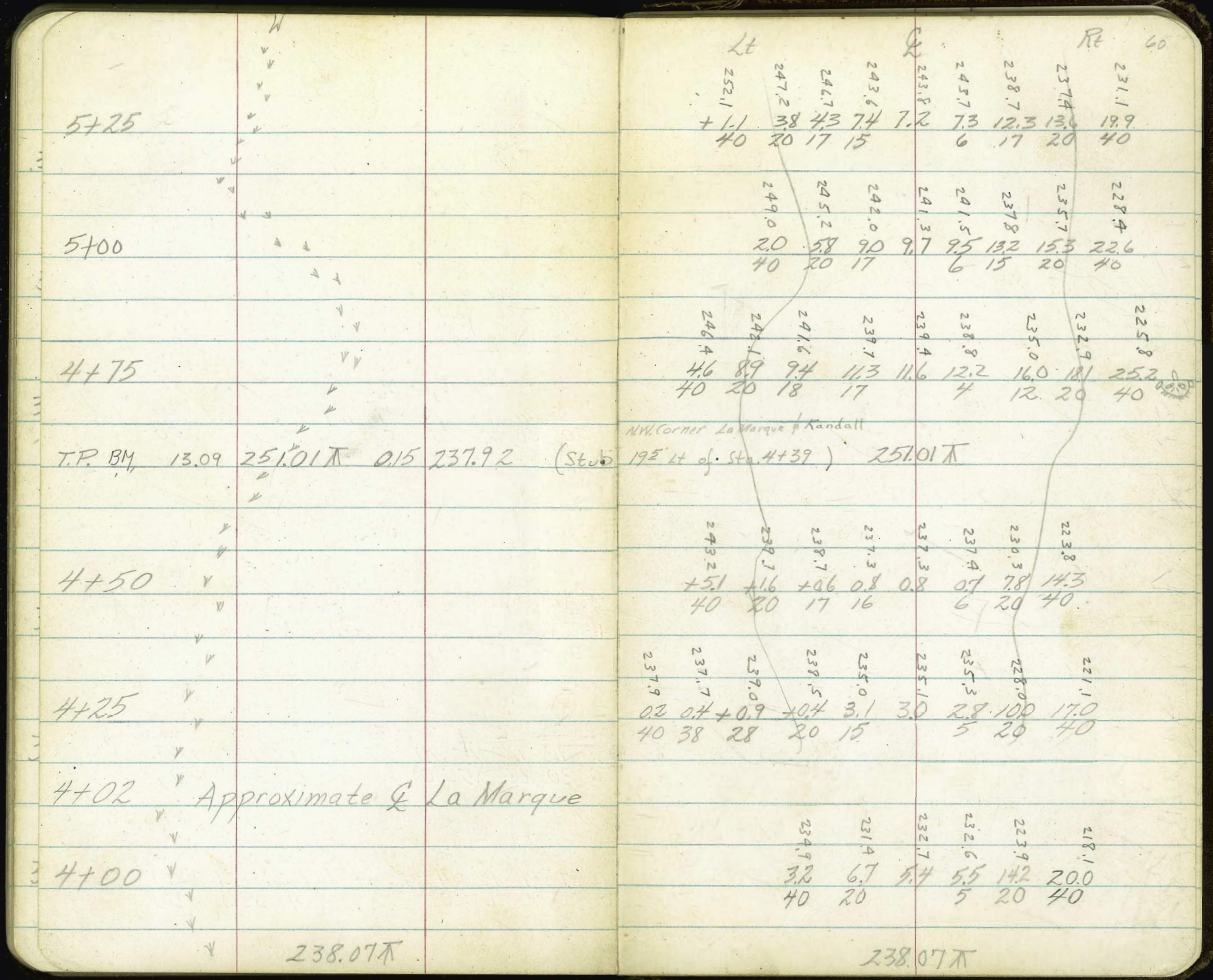
12

169.8	168.9	168.0	168.1	168.9	166.3	164.8	161.2
4.4	5.3	6.2	6.1	5.3	7.9	9.4	13.0
50	30	27	20		6	30	50

174.23 ℄

					Lt	℄	Rt
					NW. Corner LaFrance & Randall.		
T.P BM	12.33	224.86 ⊼	0.11	212.53	(Stub. 33' Left of Sta. 2+75)		
2+75					216.4 +38 50 / 214.4 0.2 30 / 212.3 0.3 29 / 210.8 1.8 26 / 210.7 1.9 20	210.7 1.9	207.6 5.0 6 / 204.5 8.1 30 / 200.4 12.2 50
2+50	Approximate ℄ La France				209.8 2.8 50 / 206.8 5.8 30 / 205.9 6.7 20	206.2 6.4	206.2 6.4 2 / 203.7 8.9 7 / 199.7 12.9 30 / 195.7 16.9 50
2+25					205.0 7.6 50 / 203.0 9.6 30 / 201.2 11.4 20	201.3 11.3	201.1 11.5 1 / 197.9 14.7 7 / 194.6 18.0 30 / 191.8 20.8 50
T.P.	13.21	212.64 ⊼	0.15	199.43		212.64 ⊼	
2+00					200.4 +0.8 50 / 198.2 1.4 30 / 196.0 3.6 26 / 196.0 3.6 20	195.7 3.9	192.9 6.7 7 / 190.0 9.6 30 / 187.2 12.4 50
1+75					195.3 4.3 50 / 192.7 6.9 30 / 191.0 8.6 26 / 190.9 8.7 20 / 190.6 9.0 1	190.5 9.1	187.9 11.7 5 / 184.6 15.0 30 / 183.5 16.1 50
		199.58 ⊼				199.58 ⊼	

			Lt			℄			Rt	
						231.0	221.3	219.9	216.6	59
			233.7	229.8	229.8					
3+84			3.4	8.3	8.3	7.1	16.8	18.2	21.5	
			40	23	20		20	28	40	
						226.2	220.1	219.8	214.5	
			231.9	227.5	227.9	229.3				
3+71.57	(Section at Rt ∠s to forward tangent)		6.2	16.6	10.2	8.8	11.9	18.0	18.3	23.6
			40	26	20	5		16	20	40
						226.2	219.6	215.3	209.8	21
			235.6	230.7	229.1	228.8	229.4			
3+71.57 ∠ Left	(Section at Rt ∠s to back tangent.)		2.5	7.4	9.0	9.3	8.7	11.9	18.5	22.8	28.3
			50	30	27	20	5		16	30	50
T.P.	13.24	238.07 ℸ 0.03 224.83						238.07 ℸ			
						221.8	216.7	213.5	208.6	17
		232.9	228.4	228.1	224.9	224.7	225.9			
3+50		+8.0	+3.5	+3.2	0	0.2	+1.0	3.1	8.2	11.4	16.3	
		50	30	28	25	20	6		10	30	50	
						217.3	215.1	211.1	206.4	13
			227.7	223.6	223.1	220.4	220.2	220.4			
3+25			+2.8	1.3	1.8	4.5	4.7	4.5	7.6	9.8	13.8	18.5
			50	30	28	25	20	6		3	30	50
						214.1	211.7	207.8	203.2	15
			222.3	218.0	217.5	215.4	215.5	215.6				
3+00			2.6	6.9	7.4	9.5	9.4	9.3	10.8	13.2	17.1	21.7
			50	60	28	26	20	3		4	30	50
		224.86 ℸ						224.86 ℸ				


Lt
℄
Rt
60
5+25
5+00
4+75
T.P. BM 13.09 251.01℄ 015 237.92 (Stub
NW Corner La Marque & Randall
192' Lt of Sta 4+39) 251.01℄
4+50
4+25
4+02 Approximate ℄ La Marque
4+00
238.07℄
238.07℄

	Lt.			℄		Rt.	
6+43.76 (Section Parallel to Loring)	264.0	260.2	256.5	255.4	253.2	250.3	247.3	243.3
	+0.3	3.5	7.2	8.3	10.5	13.4	16.4	20.4
	40	22	15		17	22	28	40
6+43.76 So. Line Loring (Section at Rt ℄ to back tangent)	262.5	259.2	256.8	255.4	254.8	252.4	249.3	242.7
	1.2	4.5	7.9	8.3	8.9	11.3	18.4	21.0
	40	20	13		16	20	32	40
6+25	260.8	257.0	254.7	252.6	252.7	248.7	246.3	241.2
	2.9	6.7	9.0	10.5	11.0	15.0	17.4	22.5
	40	20	13	12	11	20	24	40
T.P. 12.90 263.66 ℄ 0.25 250.76				263.66 ℄				
6+00	258.5	254.4	254.1	250.0	249.8	248.8	246.9	241.3	239.4
	+7.5	+3.4	+3.1	1.0	1.2	2.2	4.1	9.7	11.6
	40	20	18	13		17	20	32	40
5+75		257.0	251.7	247.8	247.4	246.4	244.0	240.3	236.8
		+6.0	+0.7	3.2	3.6	4.6	7.0	10.7	14.2
		40	20	14		14	20	28	40
5+50		254.7	250.4	249.3	246.0	245.7	244.9	241.1	240.6	233.2
		+3.7	0.6	1.7	5.0	5.3	6.1	9.9	10.4	17.8
		40	20	17	15		11	18	20	40
	251.01 ℄			251.01 ℄						

Levels on Loring St.

Randall West

					Lt						℄		Rt		
1+75					265.7	266.3	266.3	264.5	264.9	266.8	266.22	265.6	264.5	264.6	264.6
					8.7	8.1	8.1	9.9	9.5	7.6	8.2	8.8	9.9	9.8	9.8
					60	40	38	35	16	12		14	30	40	60
T.P.	11.27	274.40 ℸ	0.21	263.13							274.40 ℸ				
1+60					263.0	264.1	262.1	262.7	263.3	264.8	264.0	263.3	261.1	261.5	260.7
					0.3	+0.8	1.2	0.6	0	+1.5	+0.7	0	2.2	1.8	2.6
					60	40	34	18	15	11	8		21	40	60
1+37.43	Opposite S.W. Corner Randall & Loring				259.4	260.0	257.8	259.7	260.1	257.3		258.6	256.5	256.0	
					3.9	3.3	5.5	3.6	3.2	6.0		4.7	6.8	7.3	
					60	40	36	20	10			25	40	60	
1+15.37	Opposite ℄ Randall					252.9	255.2	256.5	255.9	252.8		252.0	251.9	250.7	250.3
						10.4	8.1	6.8	7.4	10.5		11.3	11.4	12.6	13.0
						60	40	30	9			12	27	40	6
0+93.31	Opposite S.E. Corner Randall & Loring					250.8	250.2	249.7	246.1	245.8		245.1	244.3	244.0	
						12.5	13.1	13.6	17.2	17.5		18.2	19.0	19.3	
						60	40	20	7			20	40	60	
0+00	East Line of Floral Terrace														
T.P.	0.64	263.34 ℸ	0.96	262.70											
											263.34 ℸ				
		263.66 ℸ									on S.T. in conc. mon. S.W. Corner P.L. 1787				

	Lt				℄	Rt		
3+32.79 Opposite ℄ La Marque	261.0	262.4	264.0	266.3	268.0	269.0	271.0	
	13.4	12.0	10.7	8.1	6.7	5.4	3.7	
	60	40	23		20	40	60	
3+11.04 Opposite S.E. Corner La Marque & Loring	261.4	262.3	263.8	265.1	266.2	267.8	270.7	272.4
	13.0	12.1	10.6	9.3	8.2	6.6	3.7	2.0
	60	46	40	24	20		40	60
3+00	263.1	264.7	265.5	266.1	267.2	268.6	271.5	273.2
	11.3	9.7	8.9	8.3	7.2	5.8	2.6	1.2
	60	43	40	22	20		40	60
2+75			265.7	267.1	268.0	270.2	272.9	274.3
			8.7	7.3	6.4	4.2	1.5	0.1
			60	40	20		40	60
2+50			267.8	269.0	269.2	270.8	273.1	273.7
			4.6	5.4	5.2	3.6	1.3	0.7
			60	40	18	15	40	60
2+25			269.7	270.8	269.1	269.2	271.2	271.7
			4.7	3.8	5.3	5.2	3.2	2.7
			60	40	36	17	14	60
2+00				269.5	267.3	267.7	269.4	268.7
				4.9	7.1	6.7	5.0	5.7
				60	35	16	12	60

27+40 ℄

27+40 ℄

check		1.50	263.59 = 263.45	old hub S.E. Corner La Marque & Loring	See FB 2103 pg 5

Heavens to betsy, but it goes down down from here.

4+00					
T.P.	3.05	265.09 ℄	12.36	262.04	on Hub

℄ La Marque & So. Line Loring

3+75					
3+54.54	Opposite S.W. Corner La Marque & Loring				

274.40 ℄

Lt ℄ Rt 64

250.2	254.3	256.6	257.3	259.1	259.9	264.0
14.9	10.8	8.5	7.8	6.0	5.2	1.1
60	40	20		20	40	60

265.09 ℄

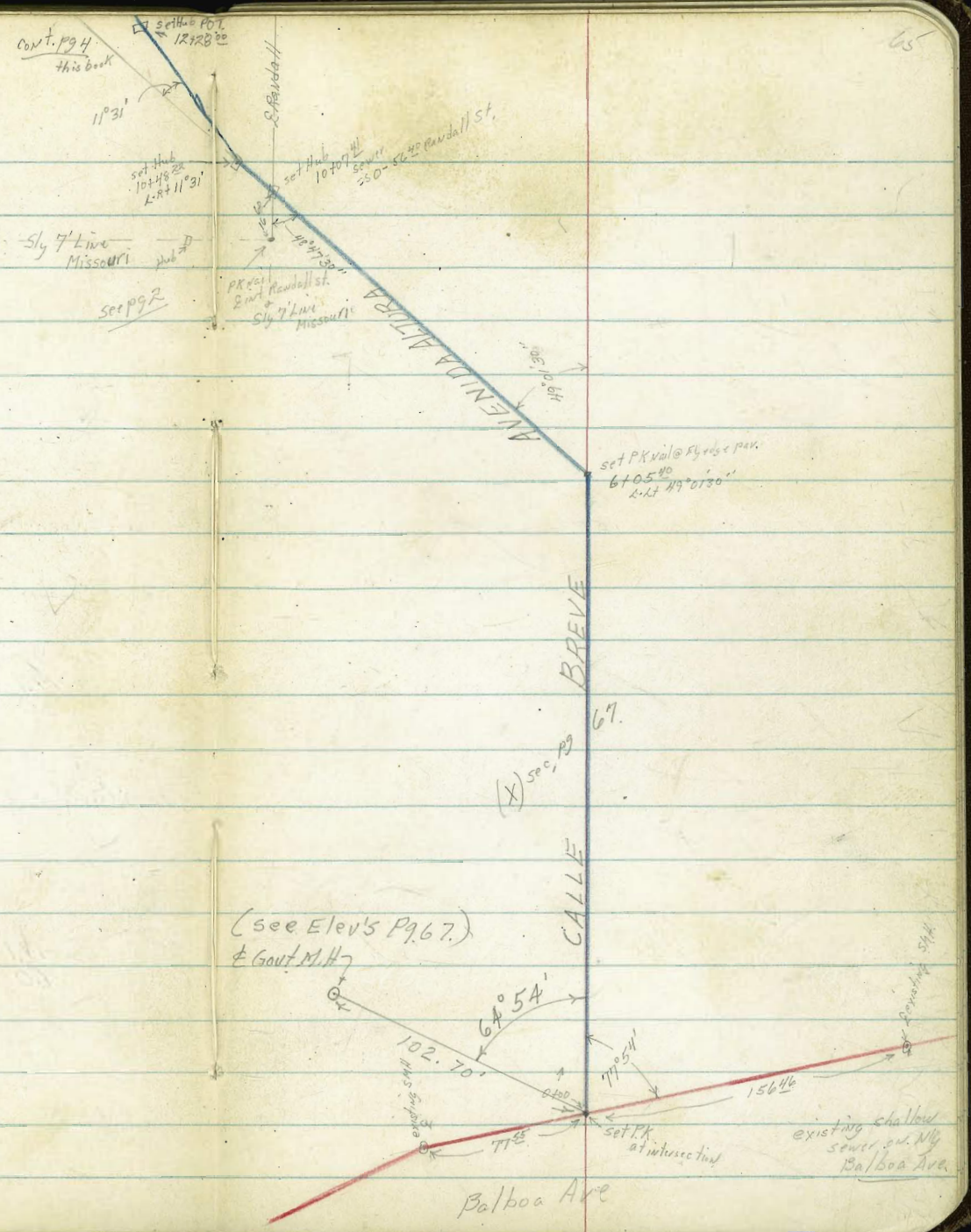
257.3	260.0	261.2	263.2	264.7	266.4	267.9
17.1	14.4	13.2	11.2	9.7	8.0	6.5
60	40	20		20	40	60

259.8	262.0	262.8	265.0	266.2	266.7	269.5
14.6	12.4	11.6	9.4	8.2	6.7	4.9
60	40	20		20	40	60

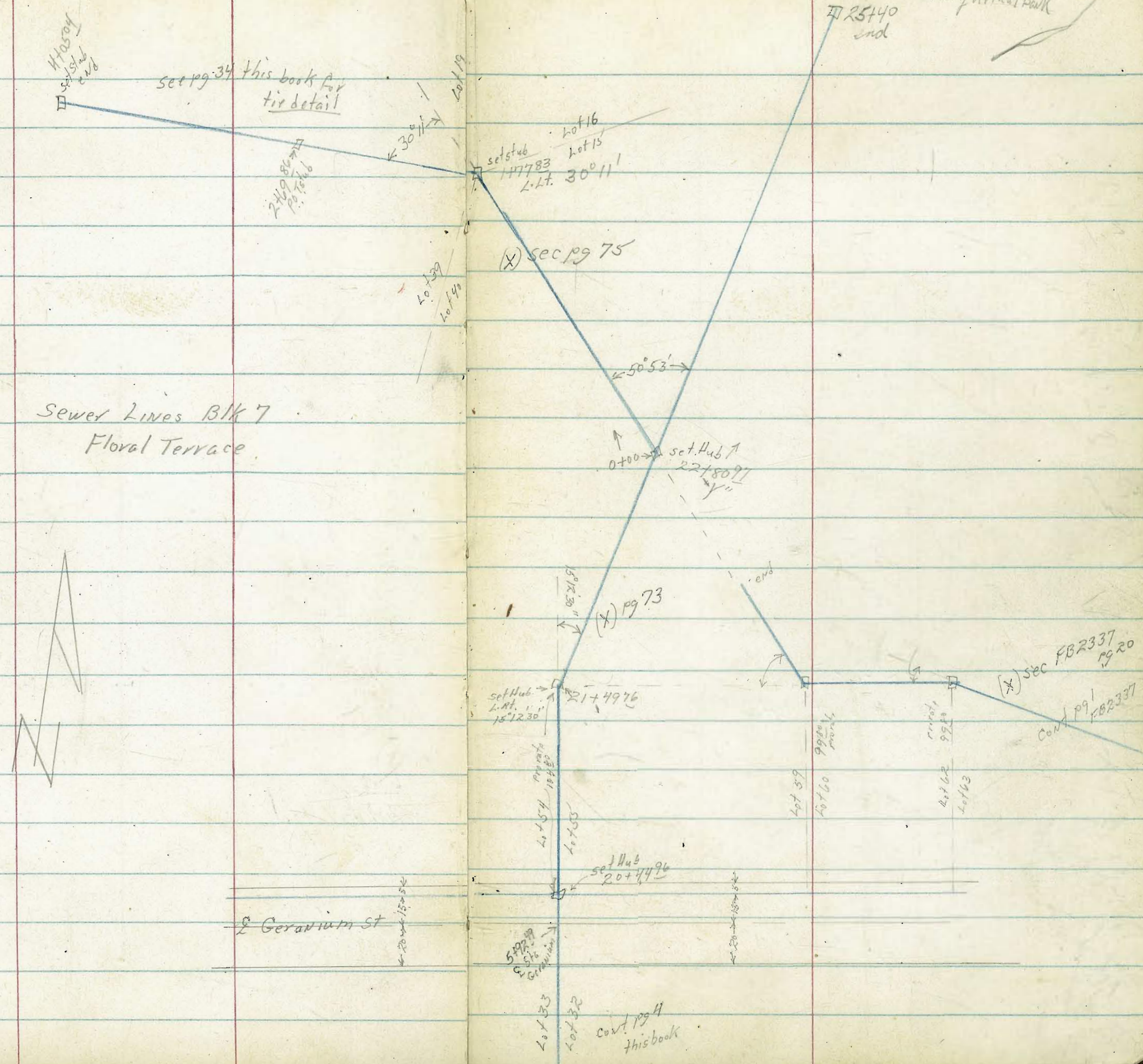
274.40 ℄

D. Smith
D. Chipman
R. Taylor
C. Stephens

see pg. 1, 2, 3, 4 this Book
see pg. 1, 2 FB 2337
see pg. 11 FB 2164



Sewer Lines Blk 7
Floral Terrace



"X" Sec Outfall Sewer Floral Terrace
Balboa Ave Nly
Sketch Pg 65

0+64 6 Rt ℄ Fire Hyd.

0+50

L 24" C.I.P. inlet 24" C.I.P.
0+44 7 Lt ℄ 5' along line by 4' wide Storm drain Box inlet

0+32 25 Rt ℄ 24" C.I.P. outlet into drainage ditch
0+25'

0+00

∢ 64°54' Lt. of for Tan.
0+00 = Tie & Elev. of Govt M.H.
(see Sketch Pg. 65)

BM			5.22	13.67	13.72 Bench Bo. K SEBP on Rose Creek Bridge on Balboa Ave
TP4	2.55	18.89			
TP3	0.62	28.63	12.29	~~16.34~~ 16.34	
TP2	2.01	38.27	10.26	28.01	
TP1	0.57	49.06	12.80	36.26	
BM TP4 on pg 5				48.49	SW 7x7 Hub Disk Missouri & Randall

Lt. Wly — Base Line — Rt. Ely

0+50: 12.69 / 6.20 / 10 — 13.31 / 5.58 — 13.5 / 5.4 / 2.5 Epav. — 13.6 / 5.3 / 10

0+44: 8.71 / 10.18 / 7.0 ie — 12.48 / 6.4 / 7.0 Grate — 13.14 / 5.75 — 13.39 / 5.50 / 4 Epav — 13.5 / 5.4 / 10

0+25: 13.62 / 6.27 / 10 — 12.59 / 6.30 / 7 — 12.94 / 5.95 — 13.28 / 5.41 / 8 Epav — 13.3 / 5.6 / 10 — 5.78 / 13.11 / 25.5 / 14

0+00: 13.41 / 5.48 rim — 7.49 / 11.42 ie / 77.55 Old SMH — 12.97 / 5.92 / 16 Epav — 12.86 / 6.03 / 10 — 12.73 / 6.16 — 12.83 / 6.06 / 10 — 13.12 / 5.77 / 17 Epav — 7.29 / 11.60 ie — 13.67 / 5.22 rim / 156.46 Old SMH

(14.10 5.71 direct Elev Rod
102.7 102.7
Sly Rim Inv. Elev.)

TP 18.89

Sta.	Lt = Wly		Base Line	Rt = Ely			
2+25	17.66 / 1.23 / 10	17.83 / 1.06 / 5 E pav.	17.9 / 1.3	17.3 / 1.6 / 5	17.16 / 1.73 / 6.0 top ditch		
2+00	16.78 / 2.1 / 10	16.97 / 1.92 / 5 E pav.	16.98 / 2.1	16.5 / 2.4 / 5	16.17 / 2.72 / 6.2 top ditch	12.89 / 6.00 / 13.2 ℄ Ditch	
1+75	16.05 / 2.84 / 10	16.23 / 2.66 / 5 E pav.	16.1 / 2.8	15.6 / 3.3 / 5	15.30 / 3.59 / 6.3 top ditch		
1+50	15.37 / 3.52 / 10	15.60 / 3.29 / 5 E pav.	15.5 / 3.4	14.9 / 4.0 / 6	14.31 / 4.58 / 7.0 wly top drainage ditch		
1+25	14.78 / 4.11 / 10	15.01 / 3.88 / 5 E pav.	14.9 / 4.0	14.7 / 4.2 / 3	13.5 / 5.4 / 7	13.39 / 5.50 / 7.0 wly top drainage ditch	
1+00	14.18 / 4.71 / 10	14.45 / 4.44 / 3.6 E pav.	14.4 / 4.5	14.1 / 4.8 / 5	12.4 / 6.5 / 10 top Ditch	9.89 / 10.00 / 16.3 ℄ Ditch	
0+77 ℄ crosses Ely edge pav.	13.46 / 5.43 / 10	13.86 / 5.03 / E pav.		13.8 / 5.1 / 6	13.2 / 5.7 / 10		

18.89

Sta.	Lt = Wly		Base Line	Rt = Ely			
4+00	24.78 / 5.45 / 10	25.00 / 5.23 / 5 E pav.	24.4 / 5.8	24.4 / 5.8 / 3	23.52 / 6.71 / 5.2 top ditch	20.17 / 10.06 / 12.2 ℄ Ditch	
3+75	23.84 / 6.39 / 10	24.03 / 6.20 / 5 E pav.	23.5 / 6.7	22.9 / 7.3 / 5	22.61 / 7.62 / 6 top ditch		
3+50	22.80 / 7.43 / 10	23.00 / 7.23 / 5 E pav.	22.6 / 7.6	22.2 / 8.0 / 5	21.69 / 8.54 / 6.0 top ditch		
3+25	21.63 / 8.60 / 10	21.84 / 8.39 / 5 E pav.	21.6 / 8.6	21.2 / 9.0 / 5	20.75 / 9.48 / 6.0 top ditch		
3+00	20.63 / 9.60 / 10	20.81 / 9.42 / 5 E pav.	20.4 / 9.8	20.1 / 10.1 / 5	19.81 / 10.42 / 6.0 top ditch	16.59 / 13.64 / 12.7 ℄ Ditch	
2+75	19.66 / 10.55 / 10	19.83 / 10.40 / 5 E pav.	19.3 / 10.9	19.0 / 11.2 / 5	18.77 / 11.46 / 6.0 top ditch		
TP3	11.85 ⊼ 30.23				0.51	18.38	
2+50	18.60 / 0.29 / 10	18.83 / 0.06 / 5 E pav.	18.8 / 0.3	18.1 / 0.8 / 5	18.01 / 0.88 / 6.0 top ditch		

⊼ 18.89

	Lt - Wly		Base Line		Rt - Ely		
TP6	8.43	T.I. 38.43	0.23	30.00			
5+50	29.66 / 0.57 / 10	29.79 / 0.44 / 5 E pav	29.39 / 0.9	28.8 / 1.4 / 7	28.4 / 1.8 / 10	27.37 / 2.86 / 14.5 top ditch	
5+25	28.92 / 1.31 / 10	29.11 / 1.12 / 5	28.72 / 1.81	27.8 / 2.4 / 7	27.6 / 2.6 / 10	26.72 / 3.51 / 13 top ditch	
5+00	28.08 / 2.15 / 10	28.34 / 1.89 / 5 E pav	27.6 / 2.6	27.1 / 3.1 / 6	26.6 / 3.6 / 10	26.08 / 4.15 / 11 top ditch	22.73 / 7.50 / 17.7 ℄ Ditch
4+75	27.38 / 2.85 / 10	27.61 / 2.62 / 5	26.93 / 3.3	26.4 / 3.8 / 7	25.39 / 4.84 / 9.6 top ditch		
4+50	26.54 / 3.69 / 10	26.77 / 3.46 / 5	26.3 / 3.9	25.8 / 4.4 / 6	24.81 / 5.42 / 8.5 top ditch		
4+25	25.71 / 4.52 / 10	25.93 / 4.30 / 5 E pav	25.4 / 4.8	25.3 / 4.9 / 4	24.23 / 6.00 / 7.5 top ditch		

T.I. 30.23

	Lt - S. Wly		Base Line	Rt - N. Ely		
6+75	32.86 / 5.57 / 10	33.15 / 5.28 / 4.0 E pav	33.2 / 5.2	33.6 / 4.8 / 10		
6+50		32.58 / 5.85 / 9.5 E pav	32.8 / 5.6	33.1 / 5.3 / 10		
6+33		31.91 / 6.52 / 10	32.27 / 6.16 E pav Wly	32.62 / 5.81 / 10		
6+19		31.45 / 6.98 / 10	31.64 / 6.79	32.10 / 6.33 / 10		
6+13 End Ext 60" Culvert						26.68 / 11.75 F.L. Rbe 41.0 90° to Fwd Tan
6+05 4.0 L.Lt 49°01'30 taken on split		31.33 / 7.10 / 10	31.96 / 6.47 E pav on PK	32.0 / 6.4 / 5	31.9 / 6.5 / 10	25.28 / 13.15 24.0 ℄ Ditch 90° to Bk Tan
6+00	31.25 / 7.18 / 10	31.72 / 6.71 E pav	31.6 / 6.8	31.5 / 6.9 / 5	31.1 / 7.3 / 10	
5+75	30.54 / 7.89 / 10	30.70 / 7.73 / 4.5 E pav	30.5 / 7.9	30.3 / 8.1 / 5	29.9 / 8.5 / 10	

T.I. 38.43

Lt = SWly   Base Line   Rt = NEly

8+25
36.40 / 2.03 / 10 — 36.54 / 1.89 / 4.5 E pav. — 36.8 / 1.6 — 36.1 / 1.7 / 10

8+00
35.63 / 2.80 / 10 — 35.77 / 2.66 / 4 E pav. — 35.8 / 2.6 — 35.7 / 2.7 / 10 — 34.83 / 3.60 / 39.4 Top Ditch — 32.03 / 6.40 / 46.1 ℄ Ditch

7+80
35.45 / 2.98 E pav.

7+75
34.89 / 3.54 / 10 — 35.29 / 3.14 — 35.32 / 3.11 / 1.0 E pav. — 35.1 / 3.3 / 10

7+50
34.18 / 4.25 / 10 — 34.58 / 3.85 — 35.12 / 3.31 / 10 E pav.

7+25
33.61 / 4.82 / 10 — 34.00 / 4.43 — 34.45 / 3.98 / 10

7+00
33.14 / 5.29 / 10 — 33.69 / 4.74 E pav. — 34.08 / 4.35 / 10 — 32.53 / 5.90 / 51 T. Ditch — 30.18 / 8.25 / 58.1 ℄ — 9.50 / 58 FL

6+90 End 60" Culvert

6+80 6.5 Rt to SWly edge 5' clump Eucalypetus

⊼ 38.43

70

Lt = SWly   Base Line   Rt = NEly

9+82
45.74 / 3.73 / 10 — 45.88 / 3.59 / 8.0 E pav. — 46.1 / 3.4 / 6 — 43.7 / 5.8 — 42.9 / 6.5 / 10

9+75
45.23 / 4.24 / 10 — 45.37 / 4.10 / 7.8 E pav. — 45.5 / 4.0 / 5 — 42.8 / 6.7 — 42.5 / 7.0 / 10

9+50
43.45 / 6.02 / 10 — 43.58 / 5.89 / 7.0 E pav. — 43.7 / 5.8 / 5 — 43.1 / 6.4 — 41.9 / 7.6 / 5 — 41.7 / 7.8 / 10

9+25
41.86 / 7.61 / 10 — 41.99 / 7.48 / 6.0 E pav. — 42.0 / 7.5 — 41.6 / 7.9 / 4.0 — 41.0 / 8.5 / 10

9+00
40.23 / 9.24 / 10 — 40.36 / 9.11 / 5.3 E pav. — 40.7 / 8.8 — 40.4 / 9.1 / 10 — 37.5 / 12.0 / 28.5 Top Ditch — 33.67 / 15.80 / 35.3 ℄ Ditch

8+75
38.72 / 10.75 / 10 — 38.90 / 10.57 / 5.5 E pav. — 39.2 / 10.3 — 39.1 / 10.4 / 10

TP7 11.11 ⊼ 49.47 0.07 38.36

8+50
37.44 / 0.99 / 10 — 37.60 / 0.83 / 5.5 E pav. — 37.9 / 0.5 — 37.8 / 0.6 / 10

⊼ 38.43

Station	Lt.=SWly	Base Line	Rt.=NEly
10+75	52.7 / 6^5 / 10	48.9 / 10^3	46.0 / 13^2 / 7 ; 44.7 / 14^5 / 10
10+60	41.7 / 7^5 / 10 ; 50.6 / 8^6 / 7	47.5 / 11^7	43.5 / 15^7 / 10
10+48.22 L. Rt 11°31' (taken on split)	50.58 / 8^{59} / 11 Epav. ; 50.7 / 8^5 / 10 ; 50.7 / 8^5 / 5	50.2 / 9^0	48.9 / 10^3 / 6 ; 47.9 / 11^3 / 10 ; 40.47 / 18.70 / 20' FL 60" Pipe
10+47 End 60" Pipe			
TP8 Start BM. pg 67	10^{68} ⊼ 59^{17}	1^{00}	48^{47} ; 48^{49} / -0^{02}
10+34	48.96 / 0^{51} / 10	49.01 / 0^{46} / Epav.	48.95 / 0^{52} / 10
10+09	47.48 / 1^{99} / 10	47.71 / 1^{76} / Epav.	48.24 / 1^{23} / 10
10+00	46.89 / 2^{58} / 10 ; 46.95 / 2^{52} / 7.0 Epav.	47.2 / 2^3	47.4 / 2^1 / 10 ; 37.97 / 11.50 / 25' FL Pipe ; 35.87 / 13.60 / 25' FL Ditch
9+99 Begin 60" Pipe			
9+93	46.37 / 3^{10} / 10 ; 46.47 / 3^{00} / 8^5 Epav.	46.7 / 2^8	~~44.5~~ 44.5 / 5^0 / 6 ; 42.8 / 6^7 / 10

⊼ 49^{47}

Station	Lt.=SWly	Base Line	Rt.=NEly
12+50	59.3 / 4^8 / 10	61.5 / 6^3	55.8 / 8^3 / 6 ; 54.4 / 9^7 / 10
12+25	60.4 / 3^7 / 10	59.7 / 4^5	58.7 / 5^4 / 6 ; 57.5 / 6^6 / 10
12+00	60.2 / 3^2 / 10	59.1 / 5^0	58.2 / 5^2 / 6 ; 57.1 / 7^0 / 10
11+75	59.4 / 4^7 / 10	57.9 / 6^2	56.3 / 7^8 / 7 ; 55.0 / 9^1 / 10
TP9	5^{67} ⊼ 64^{10}		0^{74} 58^{43}
11+50	56.9 / 2^3 / 10 ; 56.4 / 2^8 / 4	54.6 / 4^6	52.4 / 6^8 / 4 ; 50.5 / 8^7 / 10
11+25	55.6 / 3^6 / 10 ; 54.6 / 4^6 / 7 ; 54.5 / 4^7 / 4	52.2 / 7^0	51.0 / 8^2 / 2 ; 49.6 / 9^6 / 10
11+00	53.5 / 5^7 / 10 ; 52.6 / 6^4 / 6	51.1 / 8^1	47.9 / 11^3 / 10

⊼ 59^{17}

Lt=SWly	Base Line	Rt=NEly
14+25	59.1 58.5 59.5 5⁰ 4⁸ 4⁶ 10 10	
14+00	58.4 58.5 58.2 5⁷ 5⁷ 5⁹ 10 10	
13+75	59.7 58.7 57.5 57.1 4⁴ 5⁴ 6⁶ 7⁰ 10 8 10	
13+50	60.3 59.9 58.5 57.9 56.7 3⁸ 4² 5² 6² 7⁴ 10 8 5 10	
13+25	58.1 57.5 57.5 56.4 55.7 6⁰ 6⁶ 7⁴ 7² 8⁴ 10 8 6 10	
13+00	56.4 55.8 54.5 55.1 54.6 7⁷ 8³ 8⁷ 9⁰ 9⁵ 10 8 6 10	
12+75	57.3 56.7 55.5 53.8 6⁸ 7⁴ 8⁸ 10³ 10 6 10	
	T 64¹⁰	

Lt=Wly	Base Line	Rt=Ely
16+00	71.7 68.7 70.7 2⁰ 5⁰ 3⁰ 10 10	
15+75	70.9 68.9 67.3 2⁸ 5³ 6⁴ 10 10	
15+50	69.2 67.1 66.5 4⁵ 6⁶ 7² 10 10	
15+25	67.5 67.2 66.1 6² 6⁵ 7⁶ 7⁶ 10 5⁰ 10	
15+00	63.7 62.6 62.8 10⁰ 11¹ 10⁹ 10 10	
14+75	61.0 60.6 60.9 12¹ 12⁸ 12⁸ 10 10	
	1. At 37°27'30" on split 14+75 Lt 4 int Chalcedony	
	TP 10 12⁸³ T 73⁷¹	32² 60⁸⁸ on Ht. 6 14+75 Lt E Chalcedony & Base Line
14+50	59.6 60.5 60.4 4⁵ 3² 3² 10 10	
	64¹⁰	

		Lt=Wly	Base Line	Rt=Ely
17+50		96.6 / 0.5 / 10	90.3 / 6.8	84.6 / 12.5 / 10
17+25		92.9 / 4.2 / 10	87.4 / 9.7	82.9 / 14.2 / 10
TP12	11.80 π 97.08			0.57 85.28
17+00		88.9 / +3.0 / 10	83.4 / 2.5	78.2 / 7.2 / 10
16+75		85.9 / 0.0 / 10 ; 83.5 / 2.4 / 5	79.9 / 6.0	75.8 / 10.1 / 6 ; 75.2 / 10.2 / 10
16+49.59 Base line int. Alley			74.36 / 11.49 on Hub	
TP11	12.96 π 85.85			0.82 72.89
16+25		73.5 / 0.2 / 10	71.2 / 2.5	70.7 / 3.0 / 10

π 73.71

		Lt=Wly	Base Line	Rt=Ely
19+25		103.9 / 5.0 / 10 ; 101.9 / 7.0 / 6	101.3 / 7.6	101.0 / 7.2 / 10
19+00		107.2 / 1.7 / 10	100.4 / 8.5	100.2 / 8.7 / 2 ; 99.3 / 9.6 / 10
18+80.06 on split L.Rt 45°12′30″		104.7 / 4.2 / 10	103.68 / 5.23 on Hub	103.9 / 5.0 / 9d ; 103.9 / 5.0 / 6 ; 102.9 / 6.0 / 10
18+50 ↑ undesirable fill area		103.5 / 5.4 / 10	103.6 / 5.3	103.1 / 5.8 / 10
TP13	11.90 π 108.91			0.07 97.01
18+09.36 on split L.Lt 45°10′08″		91.3 / 5.8 / 10	88.57 / 8.51 on Hub	88.9 / 8.2 / 9d ; 89.5 / 7.6 / 10
18+00		94.1 / 3.0 / 10	89.2 / 7.9	86.1 / 11.0 / 10
17+75		97.6 / +0.5 / 10	91.0 / 6.1	86.7 / 10.4 / 10

π 97.08

Station		Lt-Wly	Base Line	Rt-Ely	
21+00		120.8 4.0 10	116.5 3.3	113.1 6.7 10	
20+75′		116.9 2.9 10	112.2 7.6	110.2 9.6 10	
20+50		113.0 6.8 10	107.8 12.0	108.2 11.6 10	
TP14	12.56	HI 119.82	1.65	107.26	on Hub 20+44.96
20+25′		111.3 +2.4 10 · 106.8 2.1 3	106.7 2.2	107.4 1.5 10	
20+00		107.5 1.4 10 · 105.6 3.3 4	105.4 3.5	105.3 3.6 10	
19+75′		105.5 3.4 10	104.2 4.2	104.3 4.6 10	
19+50		103.1 5.8 10	102.1 6.8	102.4 6.5 10	

HI 108.91

Station		Lt-Wly	Base Line	Rt-Ely	
0+00 Wly "Y" =S 22+80.97		125.8 6.1 10	122.87 8.98 on Hub	122.16 9.3	
22+50		125.7 6.2 10	121.8 10.1	120.9 11.0 10	
22+25		127.5 4.4 10	123.5 8.4	120.6 11.3 10	
22+00		127.3 4.6 10	122.9 9.0	118.2 13.7 10	
21+75		127.1 4.8 10	122.8 9.1	119.8 12.1 10	
21+49.76 ∠ Rt 15°12′30″ on split		124.6 7.3 10	120.42 11.43 on Hub	115.6 16.3 10	
TP15	12.92	HI 131.85		0.69	119.13
21+25′		120.0 +1.0 10	114.7 5.1	111.6 8.2 7 · 111.2 8.6 10	

119.82

Lt=Wly Base Line Rt=Ely

TP16 13 27 144 08 19 4 130 81 on rock ✓ 24424 45 Lt

24+00 13.5 13.4 13.2 12.9 12.9.1 12.8.9 13.0.1
0 4 0 5 1 7 2 8 3 0 1 8
10 7 5 wash 5 10

23+96 13.0.0
1.5
top bank

23+75 12.9.7 12.9.6 12.9.4 12.7.4 12.7.0
2 2 2 3 2 5 4 5 4 2
10 4 5 wash 10

23+50 12.8.2 12.7.5 12.7.2
5 2 4 4 4 2
10 10

23+25 12.7.4 12.6.5 12.5.8 12.5.0
4 5 5 4 6 1 6 9
10 8 10

23+00 12.5.7 12.4.5 12.4.1 12.3.6
6 3 7 2 7 8 8 3
10 6 10

131 85

Lt=Wly Base Line Rt=Ely ✓

TP19 = TP16 ✓

9 24 130 81 ✓

TP14 10 7 140 05 13 28 138 98

25+40 end. toe Lbank on Ely side canyon 14.4.9 149 29 ✓
7 4 2 97
10 on Hub

25+20 14.3.3 14.7.2 15.0.1
9 0 5 1 2 2
10 8 toe Lbank

25+00 14.0.9 14.5.5 15.0.9
11 4 6 8 1 4
10 10

TP17 9 83 152 26 16 5 142 43

24+75 13.3.2 13.3.6 13.6.6 13.9.0 14.6.1
10 9 10 5 7 5 5 1 12 0
14 10 10
wash wash

24+50 13.1.8 13.3.1 13.4.1 13.7.4 14.2.5
12 3 11 0 10 0 6 1 1 6
10 7 3 10
wash

24+25 13.1.1 13.0.4 13.1.4 13.4.1 13.5.4
13 0 13 2 12 2 10 0 8 2
10 6 5 10
wash

144 08

Lt = Swly Base Line Rt = NEly

Sewer Wly (Blk 7)

1418 72 Rt

TP_{19}	12^{35}	π 174^{31}	0^{47}	161^{96}
1+00			0^{7}_{10} 161.7	4^{4} 158.0 6^{7}_{10} 155.7
0+75'			11^{2}_{10} 150.7	13^{5} 148.9 15^{4}_{10} 147.0
TP_{18}	12^{71}	π 162^{43}	0^{22}	149^{72}
0+50			7^{0}_{10} 142.9	8^{6} 141.3 11^{6}_{10} 138.3
TP_{17}	11^{98}	π 149^{94}	0^{85}	137^{96}
0+25			5^{3}_{10} 133.5	7^{0} 131.8 7^{9}_{4} 130.9 11^{2}_{10} 127.1
0+00 "Y" to sewer Wly Blk 7 =5			14^{7}_{10} 124.1	15^{6} 123.2 15^{8}_{10} 123.0
22+80.22 outfall				
TP_{16} 109.74	8^{00}	π 138^{81}	130^{81}	

75

Lt = Swly Base Line Rt = NEly

2+50			9^{2}_{10} 200.8	8^{7} 201.8 7^{5}_{10} 203.0
TP_{22}	12^{22}	π 210^{47}	0^{16}	198^{25}
R+25'			3^{3}_{10} 195.1	2^{6} 195.8 2^{0}_{10} 196.4
2+00			7^{4}_{10} 191.0	7^{5} 190.9 7^{5}_{10} 190.9
TP_{21} = $TP_{19.48}$	13^{13}	π 198^{41}	1^{59}	185^{28} ✓ 185.24
1+77.83 L. Δ 30°11'	on split		17_{10} 185.1	3^{31} 183.51 on stub 2^{7}_{10} 184.1
1+50			9^{9}_{10} 176.9	12^{2} 174.6 14^{5}_{10} 172.3
TP_{20}	12^{76}	π 186^{82}	0^{25}	174^{06}
1+25'			7^{6}_{10} 166.7	8^{0} 166.3 9^{1}_{10} 165.2
		π 174^{31}		

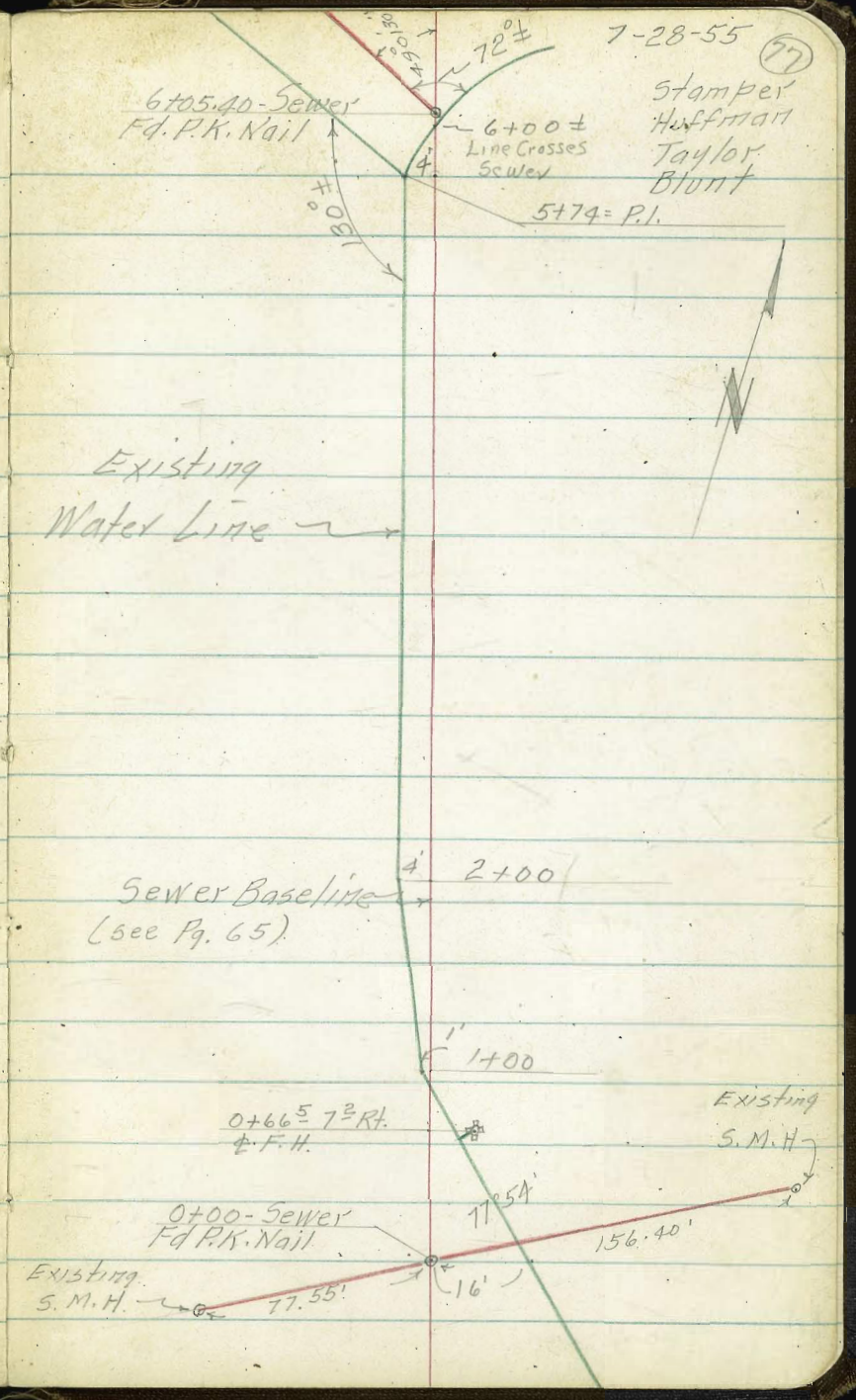
Station		Lt = Swly	Base Line	Rt = NEly
TP BM ⇔ on rock Sta 5+20 w. Ilbur St pg 46 this book				1^80 220^35 (220^32, +0.03)
4+05.07 End		213.9 8^3 10	215.20 6^25 0 Sta 6	216.6 5^6 10
3+75		212.6 9^6 10	213.6 8^6	214.4 7^8 10
3+50		211.1 11^6 10	211.8 10^4	213.4 8^8 10
TP 23	11^78 π 222^15			0^10 210^37
3+25		208.8 1^7 10	210.2 0^3	211.7 +1^2 10
3+00		207.1 3^4 10	208.2 2^3	208.8 1^7 10
2+75		203.9 6^6 10	204.8 5^7	205.5 5^0 10

π 210^47

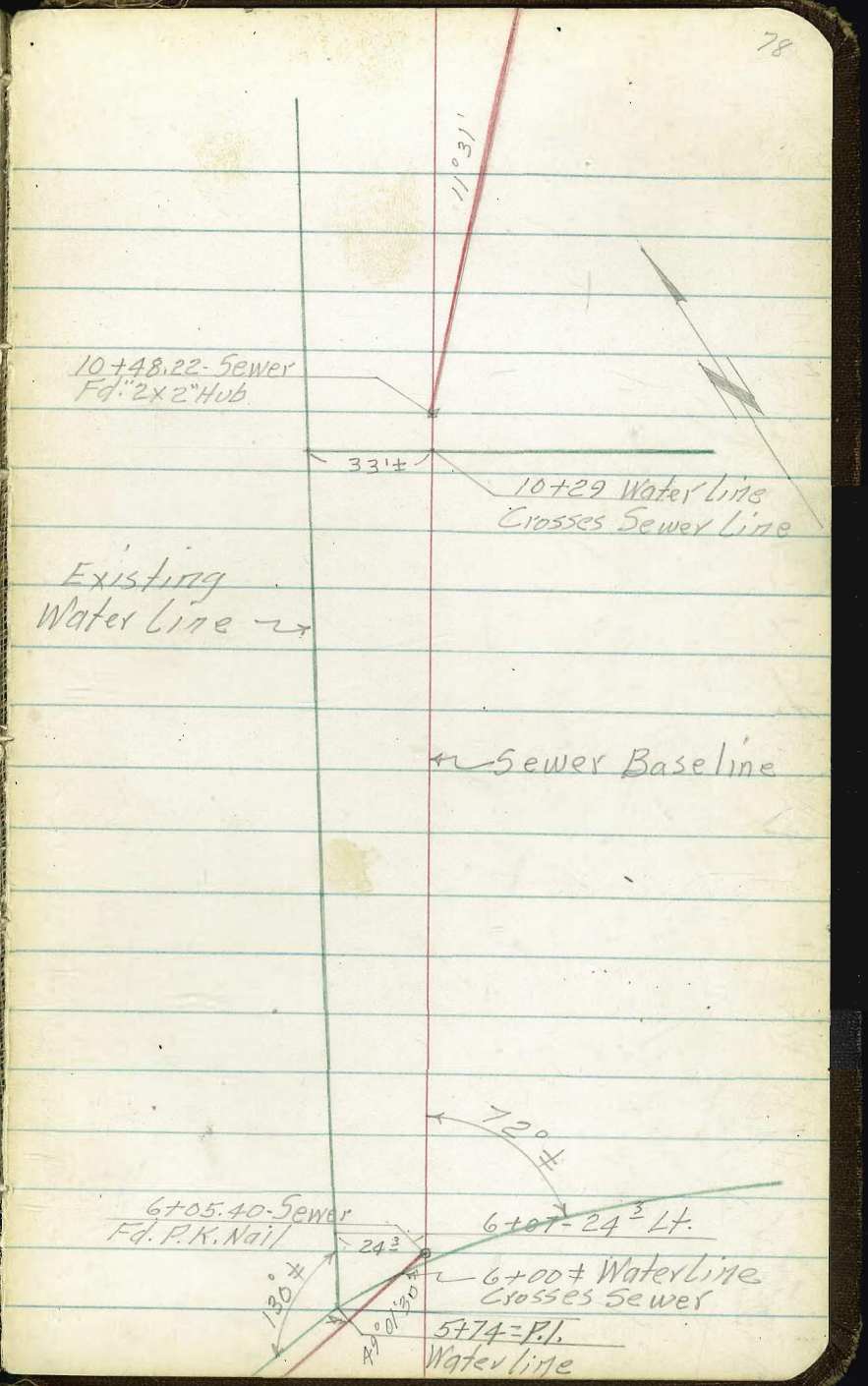
INDEXED

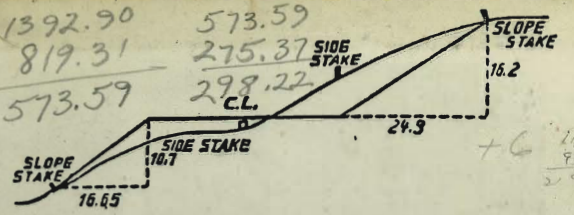
TIES TO WATER MAIN CALLE BREVE & AVENIDA ALTURA W.O. 32067

Sta	Lt.	Rt
72° Rt. on for Tan. 6+00		℄ on Line Ely.
P.I. Waterline 5+74	4.0	
5+00	4.0	
4+00	4.0	
3+00	4.0	
2+00	4.0	
1+00	1.0	
0+66 5		7.2 F. Hyd
0+50		4.0'
0+00		16.0'



TIES TO WATER MAIN





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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