589

ENGINEERS'

LEVEL BOOK

No. 10

92

F.B. 589

29596

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

SW
546

491.54
94.75
586.29
13 35
599.64

36

INDEX

Mission Ave

480.55 ℄ Alignment Univ Ave South

∠Lt 0°-12'-06"

90-13 } Direct
180-25-30 }

270-39 } Rev.
360 51-20 }

0.19' ℄ Intersection Castle St and Mission Ave

∠ 0°-0'-58"

180°00'

∠Rt 0°00'-58"

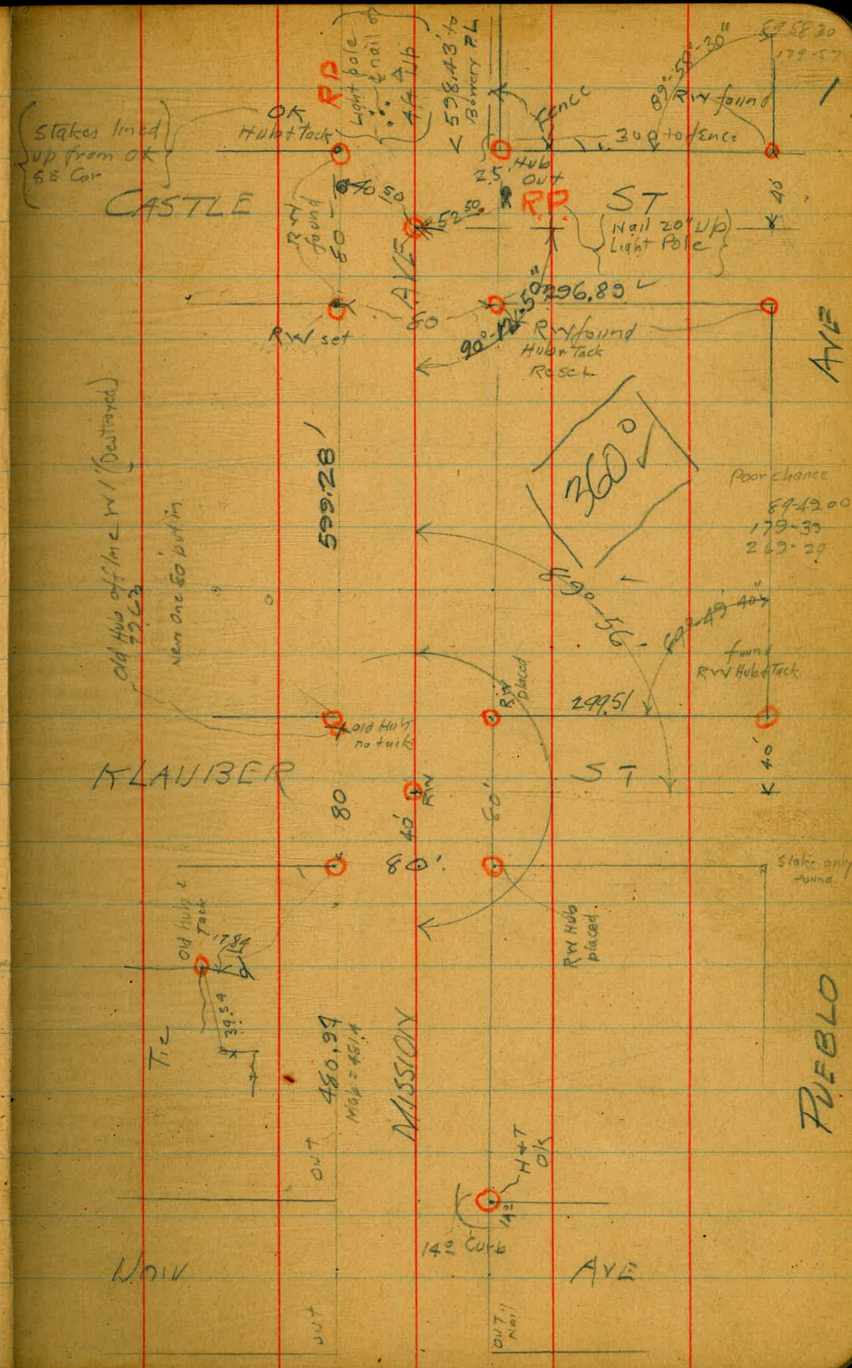
89-56 } Direct
179-52 }

269-48 } Reverse
359-44 }

℄ Intersection Klauber St and Mission Ave

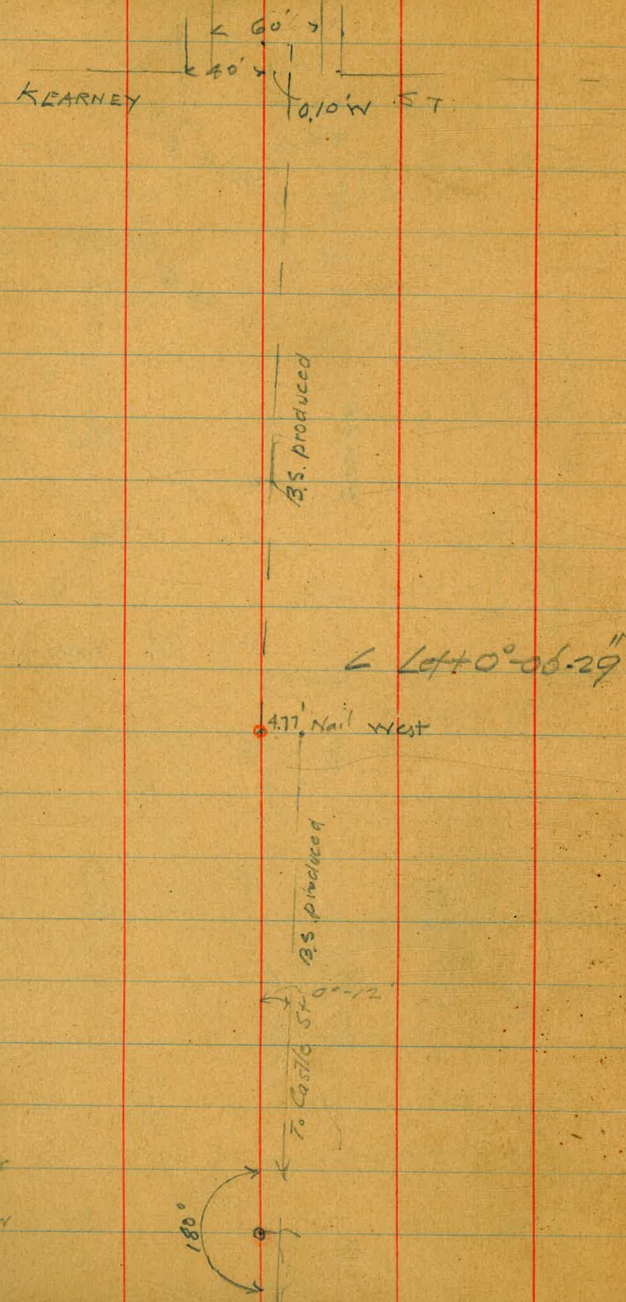
Mission Ave Summary of Alignment to Kearney

Sta ℄ Int	Street Intersections	Angles Lt	Angles Rt
32+55.66	Kearney		
25+75.98	Fulton	0°-0'-29"	
18+98.68	Bowery	0	0
12+00.25	Castle	0°-12'-06"	
5+20.97	Klauber		0°-00'-58"
0+00 = ℄	Univ & Mission	?	



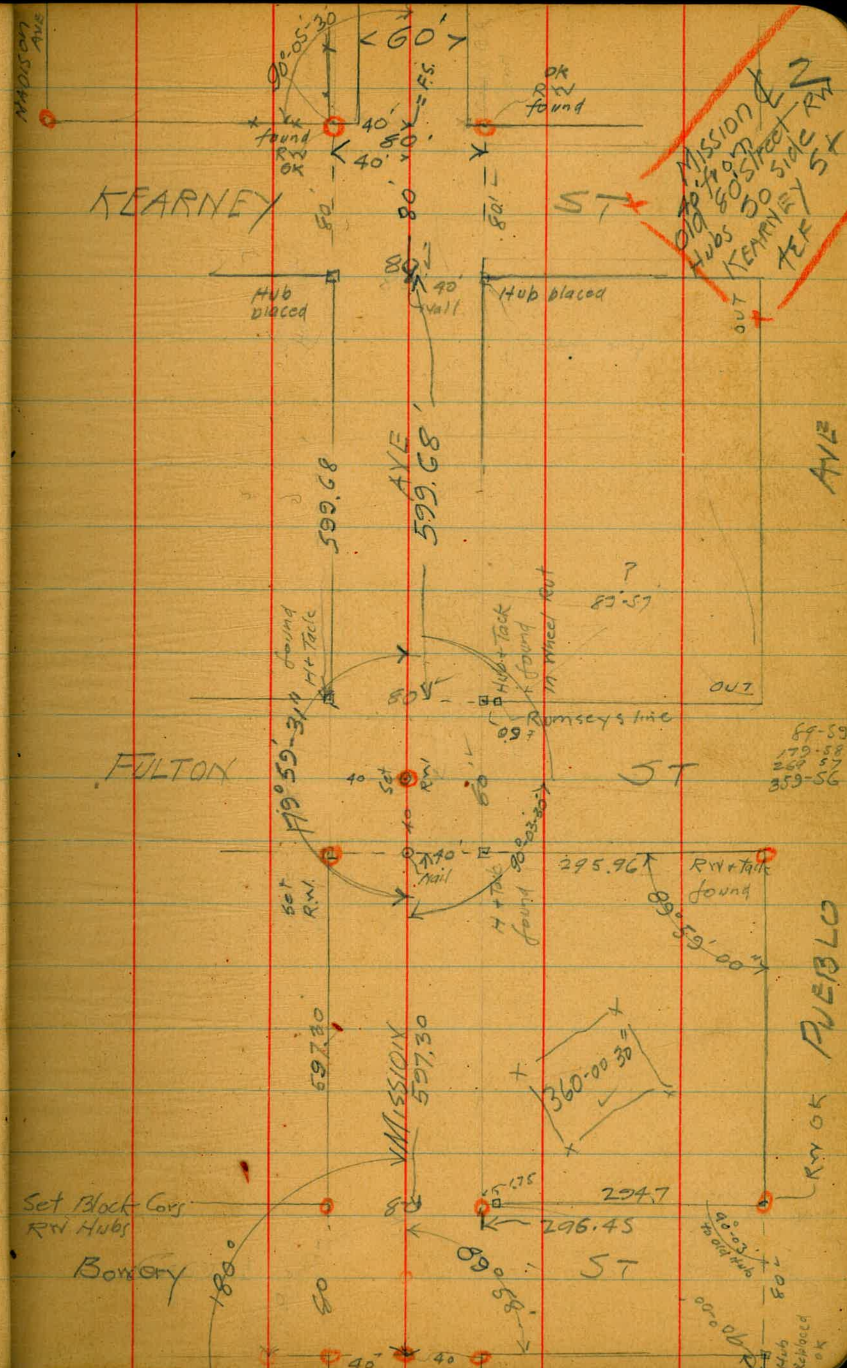
Stakes lined up from OK SE Cor
OK Hub & Tack
RP
Light pole
598.43' to Bowery Pl
Fence
89°-59'-30"
R/W found
30 to fence
CASTLE
ST
RP
Nail 20' up Light Pole
40'
R/W set
296.89
R/W found Hub & Tack Reset
AVE
599.28
360°
Poor chance
89-49-00
179-39
269-29
89°-56'
Old Hub off line W/ (Destroyed)
new one 60 put in
found R/W Hub & Tack
249.51
Old Hub no tack
KLAUBER
ST
80
80'
Stake only found
Old Hub & Tack
RW Hub placed
480.97
MISSION
14' Curb
H&T OK
Univ
AVE
PUEBLO

90-05-30
180 11



90-03-30
180-07
270-11
360-14

90°-02 } Dir
180-04
270-06 } Rev
360-08

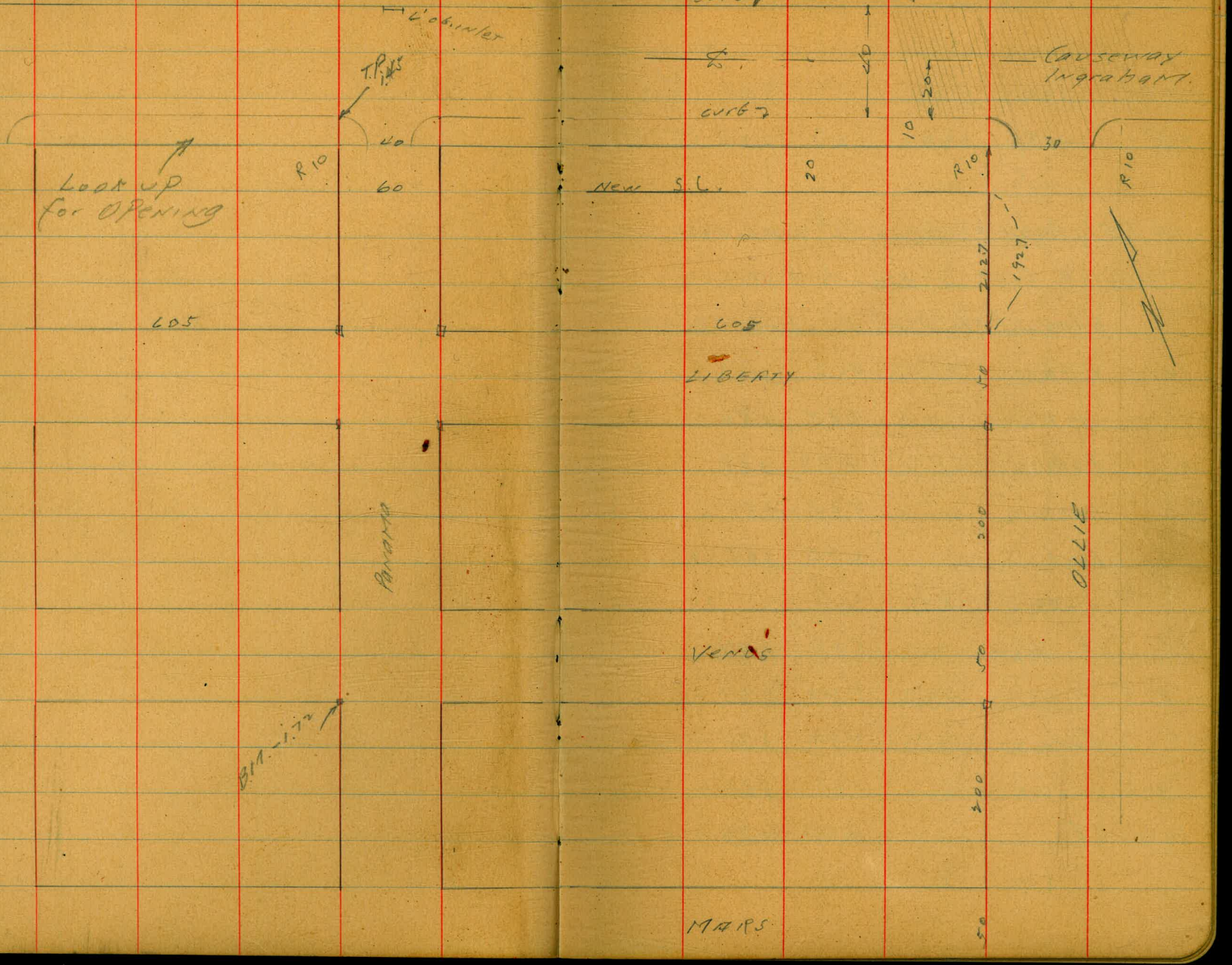


MADISON AVE
90°-05'-30
60'
OK RW found
found OK
40'
80'
KEARNEY
ST
Mission ℄ 2' from old 80' street RW Hubs 50 side KEARNEY St. AEF
Hub placed
Hub placed
599.68
AVE
599.68'
OUT
OUT
found H+Tack
Hub+Tack found
in wheel rut
89-57
Romsey's line
FULTON
ST
179°-59'-30"
Set RW
Nail
90°-03'-30"
295.96'
RW+Tack found
89°-59'-00"
89-59
179-58
269-57
359-56
H+Tack found
597.30
MISSION
597.30
360-00-30"
PUEBLO
RW OK
Set Block Cors RW Hubs
Bowery
294.7
296.45
ST
89°-58'
180°
40'
40'
Hub Replaced OK

Levels to Estab. Grades of STS. in Druckers Add

Indexed C.S.K.

Moore 8-28-39.



Curb Levels on Ingraham St

B.M. B.P.	5.22	8.22		3.00	S. Culv hd. wall nly of Pt. Lom R.R. on Ingraham
T.P.	4.15	6.68	5.69	2.53	

214' SEly from Ely Cor. of P.L.# 218 = 0+00

Wly = to Left — Ely = to Right

0+00 = SEly Line Nashville to N.E.

Wly	curb	4.15	2.53
	gut	4.82	1.86
c	Pav	4.79	1.89
	gut	5.31	1.35
Ely	Curb	4.70	1.98
	0+50		
Ely	cb drive	5.24	1.44
gut		5.44	1.24
c	Pav	4.92	1.76
gut		5.01	1.67
Wly	cb	4.35	2.33

6.68 Indexed C.S.K. 2

1+00		
Wly cb	4.44	2.24
gut	5.10	1.58
c Pav	5.08	1.60
gut	5.42	1.26
Ely cb drive	5.31	1.37
1+50		
Ely cb drive	5.23	1.45
gut	5.37	1.31
c	5.00	1.68
gut	5.20	1.48
Wly cb	4.56	2.12
1+89		
Wly cb	4.69	1.99
gut	5.28	1.40
c Pav	5.06	1.62
gut	5.38	1.30
Ely cb	4.73	1.95
2+14 = ℄ Ollie St		
Ely cb	4.78	1.93

6.68

Ely gut.	5.41		
c Pav. on Ld. plug	5.10	1.58	C.T.B.M.
wly cb on Pav	5.14	1.56	
wly " "	5.11	1.57	
2+39 = Nly Oilic St = 0+00			
wly cb	4.57	2.11	
gut	5.19	1.49	
c	5.06	1.62	
gut	5.40	1.28	
Ely cb	4.75	1.93	
0+50			
Ely cb	4.68	2.00	
gut	5.34	1.36	
c	5.04	1.64	
gut	5.19	1.49	
wly cb	4.58	2.10	
1+00			
wly cb	4.74	1.94	
gut	5.17	1.51	
c	4.95	1.73	

6.68

gut	5.33	1.35
Ely	4.66	2.02
1+50		
El	4.61	2.07
gut	5.19	1.39
c	4.94	1.72
gut	5.17	1.51
wly cb	4.55	2.13
2+00		
wly cb	4.49	2.19
gut	5.10	1.58
c	4.93	1.75
gut	5.20	1.48
Ely cb	4.56	2.12
2+50		
Ely cb	4.56	2.12
gut	5.15	1.53
c	4.94	1.74
gut	5.08	1.60
Wly cb	4.45	2.23

		4.68		
3+00				
W/y c6			4.54	1.36
gut			5.15	1.53
c			4.94	1.74
gut			5.25	1.43
E/y c6			4.41	2.07
TP	4.37	4.57	4.48	2.20
3+50				
E/y c6			4.51	20.6
gut			5.15	1.48
c			4.94	1.65
gut			5.13	1.44
W/y c6			4.51	2.06
4+00				
W c6			4.65	1.92
gut			5.29	1.28
c			4.94	1.65
gut			5.25	1.32
E/y c6			4.07	1.95

		4.57		
4+50				
E c6			4.74	1.81
gut			5.40	1.17
c			5.04	1.53
gut			5.39	1.18
W c6			4.74	1.83
5+00				
W c6			4.93	1.64
gut			5.54	1.03
c			5.24	1.33
gut			5.53	1.04
E/y c6			4.88	1.69
5+50				
E/y c6			4.94	1.65
gut			5.58	0.99
c			5.25	1.32
gut			5.54	1.03
W/y c6			4.93	1.64
6+05. S/y Paralving				
W c6			4.94	1.65
gut			5.55	1.02

6.57

C		5.28	1.19	
gut		5.73	0.84	
Ely cb		5.05	1.52	
4+35 E Paxarina				
E cb		5.13	1.44	
gut E cb, inlet		5.99	0.58	
c Par		5.60	0.97	
cb Line on Par		5.54	1.03	
W "		5.43	0.94	
0+00 N/x Paxarina				
W cb		5.17	1.48	
gut		5.79	0.78	
C		5.54	1.01	
gut		5.89	0.68	
Ely cb		5.22	1.38	
1+00				
Ely		5.11	1.46	
gut		5.78	0.79	
C		5.41	1.10	

6.57

gut		5.63	0.94	
W/y cb		4.99	1.58	
T.P	5.10	6.55	5.12	1.45	Top West Return
2+00				
W/y cb		4.87	1.68	
gut		5.46	1.09	
c		5.27	1.28	
gut		5.66	0.89	
E/y cb		5.02	1.53	
3+00				
Ely cb		4.70	1.85	
gut		5.33	1.22	
c		5.03	1.52	
gut		5.40	1.15	
W/y cb		4.72	1.83	
4+00				
W/y cb		4.65	1.90	
gut		5.30	1.25	
c		4.97	1.58	

		4.55			
qvt			5.33	1.22	
E/y c6			4.74	1.81	
	5+00				
E/y c6			4.44	2.09	
qvt			5.08	1.47	
c			4.78	1.77	
qvt			5.24	1.33	
W/y			4.55	1.00	
	6+05 S/y P.T				
W/y c6			4.24	2.29	
qvt			4.90	1.65	
c			4.63	1.92	
qvt			4.96	1.59	
E/y c6			4.34	2.22	
	6+30 E P.T				
E/y			4.20	2.35	
qvt			4.85	1.70	
c	Ld + C.T.		4.59	1.96	B.M.
qvt	Pav		4.45	1.90	
W c	"		4.45	1.90	

		6.55			
6+55 N/y P.T = 0+00					
W/y c6			4.19	2.36	
qvt			4.83	1.72	
c			4.55	2.00	
qvt			4.85	1.70	
E/y c6			4.24	2.31	
T.P.	4.48	4.64	4.59	196	Ld C.T.
	1+00				
E/y c6			4.74	1.88	
qvt			5.40	1.24	
c			5.19	1.45	
qvt			5.45	1.21	
W/y c6			4.87	1.77	
	2+00				
W/y c6			4.74	1.90	
qvt			5.34	1.28	
c			5.09	1.55	
qvt			5.35	1.29	
E/y c6			4.71	1.93	

Camulos Parking Levels

N = PT + S = LT

T.P.	4.58	4.83	1.45	W Ret. Panama

~~Why~~ Ingraham = 00 = S. Edge Paving
0+20 = SL Street

N/y c/l	2.83	1.20
gut	3.37	0.66
c Pav	3.09	0.94
gut	3.14	0.89
S/y c/l	2.41	1.42
0+20		
S	4.8	-0.8
c	5.3	-1.3
N	4.4	-0.4
0+50		
N	4.9	-0.9
c	4.5	-0.5
S	4.6	-0.6
1+00		
S	5.7	-1.7
c	5.8	-1.8
N	5.4	-1.6

4.03 Indexed C.S.K.

1+50		
N	5.0	-1.0
c	5.0	-1.0
S	5.0	-1.0
2+17 = Ely Liberty		
S	4.8	-0.8
c	5.0	-1.0
N	5.0	-1.0
0+00 Wly Liberty		
N	4.9	-0.9
c	5.0	-1.0
S	4.9	-0.9
1+00		
S	5.2	-1.2
c	5.0	-1.0
N	4.9	-0.9
2+00 Ely Venus		
N	5.4	-1.4
c	5.5	-1.5
S	5.4	-1.6

4.03

W/y Venus = 00

S		5.9	-1.9
C		5.9	-1.9
N		5.8	-1.7
T.P. 2 x R.W.	5.37	3.65	5.75	-1.72	W. Cor. Panama Venus

1+00

N		5.1	-1.4
C		5.2	-1.5
S		5.0	-1.3

2+00 E/y Mars

S		4.5	-0.8
C		4.5	-0.8
N		4.6	-0.9

0+00 W/y Mars = 00

N		4.5	-0.8
C		4.4	-0.7
S		4.4	-0.7

3.65

1+00

S		4.6	-0.9
C		4.6	-0.9
N		4.7	-1.0

2+00 = E/y Williams

N		3.8	-0.1
C		4.1	-0.4
S		4.1	-0.4

00 W/y Williams

S		3.8	-0.1
C		3.9	-0.2
N		3.9	-0.2

1+00

S		3.8	-0.1
C		3.8	-0.1
N		4.0	-0.3

2+00 E/y Prince

		5.5	+1.8
C		4.9	-1.2
S		4.8	-1.1

3.65

2+30 Top Bank Est 1.0 -0.3

2+35 in Slough 7.2 -3.5 30' wide

Indexed
C.S.K.

Liberty Levels
Panama to Ollie

BM Hub	5.67	3.95	-1.72	Panama Venus
100' S/y of Panama				
E = RT		4.8	-0.8	
C } NOTE!		4.7	-0.7	
W = RT		5.0	-1.0	
200 S/y				
W		4.4	-0.6	
C		4.7	-0.7	
E		4.4	-0.6	
300 S/y				
E		4.3	-0.3	
C		4.5	-0.5	
W		4.3	-0.3	
400 S/y				
W		4.2	-0.2	
C		4.3	-0.3	
E		4.1	-0.1	

3.95

500 S/y

E	4.4	-0.4	
C	4.4	-0.4	
W	4.3	-0.3	
T.P.	3.86	+0.09	Earth NC Liberty & Ollie

6+05 = N/y Ollie, see p 11

Indexed C.S.K.

OLLIE Levels

N = Rt S = Lt.

0-30 = Pueblo Line or ℄ of Street

C.T.B.M. 3.27 4.80 1.58 P3

00 = ~~W~~ Ingraham 15. Edge of Paving End Rel

South line of Street = 0+20

N Top cb. Rt.	2.84	1.96	
gut Par.	3.44	1.36	
C "	3.20	1.60	
gut "	3.49	1.31	
S Top end cb.	2.88	1.92	
0+47			
S	3.8	1.0	
C	3.7	1.1	
+17 ℄ 14' Cem Dr.	3.62	1.18	
W +4.7 E do. gar. Cem.	3.48	1.12	
1+00			
N'	4.3	0.5	
C	4.0	0.8	
S	4.1	0.7	
1+50			
S	4.1	07	
check to T.P. P10	4.74	0.06	8.09

4.80

C	4.7	0.6
N	4.8	0.0
.2+13.7 = Ely Liberty		
N	5.4	-0.6
C	4.6	+0.2
S	4.5	+0.3
00 = Wly Liberty		
S	4.3	0.5
C	4.3	0.5
N	4.5	0.3
0+50		
N'	4.8	00
C	4.0	0.8
S	4.7	0.1
1+00		
S	4.5	0.3
C	4.4	0.4
N	4.8	00
1+50		
N	4.5	0.3

4.80

E			4.4	0.4	
S			4.6	0.2	
2+00 E/y Venus					
S			4.8	0.5	
C			4.x.	0.4	
N			4.6	0.2	
00 = W/y Venus					
N			4.5	+0.3	
C			4.9	-0.1	
S			4.0	+0.8	
T.P.	3.5	5.17	3.17	1.43	Top Latch.
0+50					
S			4.5	0.7	
C			4.5	0.7	
N			4.6	0.6	
1+00					
N			5.2	.00	
C			4.9	0.3	
S			5.0	0.2	

5.17

1+50				
S			5.1	0.1
C			5.1	0.1
N			5.2	00
2+00 E/y Mars				
N			4.8	0.4
C			4.9	0.3
S			4.9	0.3
00 = W/y Mars				
S			4.5	0.7
C			4.5	0.7
N			4.7	05
0+50				
N			4.6	0.6
C			4.7	0.5
S			4.6	0.6
1+00				
S			4.0	0.8
C			4.7	0.5
N			4.5	0.7

5.17

	1+20		
N		4.4	0.8
C		4.5	0.7
+20		4.4	0.8
S	IN Slough	8.4	-3.4
	1+50		
S	IN slough	9.6	-4.4
	+15	8.6	-3.4
	+20	5.2	00
C		4.8	0.4
N		4.5	0.7
	1+45		
N'		4.3	0.9
C		4.9	0.3
+5	IN slough	9.5	0.7
S		10.0	-4.8
	0+00 E/y WILLIAMS ST.		
S	IN slough	9.6	-4.4
C	" "	9.6	-4.4
+15	" "	9.0	-3.8

5.17

+20		4.4	-1.2
N		5.2	00

Indexed
C.S.K.

Venus Levels

Ollie to Pairama

W = LT E = PT

5:17

T.P.	2.84	4.47	3.54	1.63	Lark

0+00 Mly of Ollie

1+00

W		5.1	-0.6
C		5.1	-0.6
E		5.0	-0.5

2+00

E		5.4	-0.5
C		5.4	-1.1
W		5.5	-1.0

3+00

W		5.5	-1.0
C		5.7	-1.2
E		6.0	-1.5

4.47

4+00

E		6.0	-2.1
C		6.0	-1.5
W		5.9	-1.4

5+00

W		5.9	-1.4
C		6.5	-2.0
E		5.8	-1.3

6+05 you have P7

Indexed
C.S.K.

Mars Levels

E = LT W = PT

4.47

00 = S/y Panama

1+00

E	5.0	-0.5
C	5.1	-06
W	4.9	-0.4

2+00

W	5.0	-0.5
C	5.1	-0.6
E	4.9	-0.4

3+00

E	4.8	-0,3
C	4.4	-0.1
W	4.4	+0.1

4+00

W	4.4	+0,1
C	4.5	00
E	4.4	-0,1

4.47

5+00

E	4.4	+0,1
C	4.3	+02
W	4.4	+03

6+05 you have on 011.C

Williams Levels

E = LT W = RT

4.47

0+00 = Sly Panama P8
Camalos

1+00

E	5.9	-1.4
c	5.8	-1.3
W	5.6	-1.1

2+00

W	4.5	00
c	4.5	00
E	4.5	00

3+00

E	4.3	+0.2
c	4.3	+0.2
W	4.4	+0.3

4+00

W	4.3	+0.2
c	4.1	+0.4

Indexed
C.S.R.

4.47

E	4.0	+05

5+00

E	4.0	+05
C	3.9	+0.6
W	4.2	+03

5+50

W	5.0	-05
c	3.8	+07
E	3.8	+07

5+70

E	3.7	+08
c	6.0	-1.5
W in Slough	8.3	-3.8

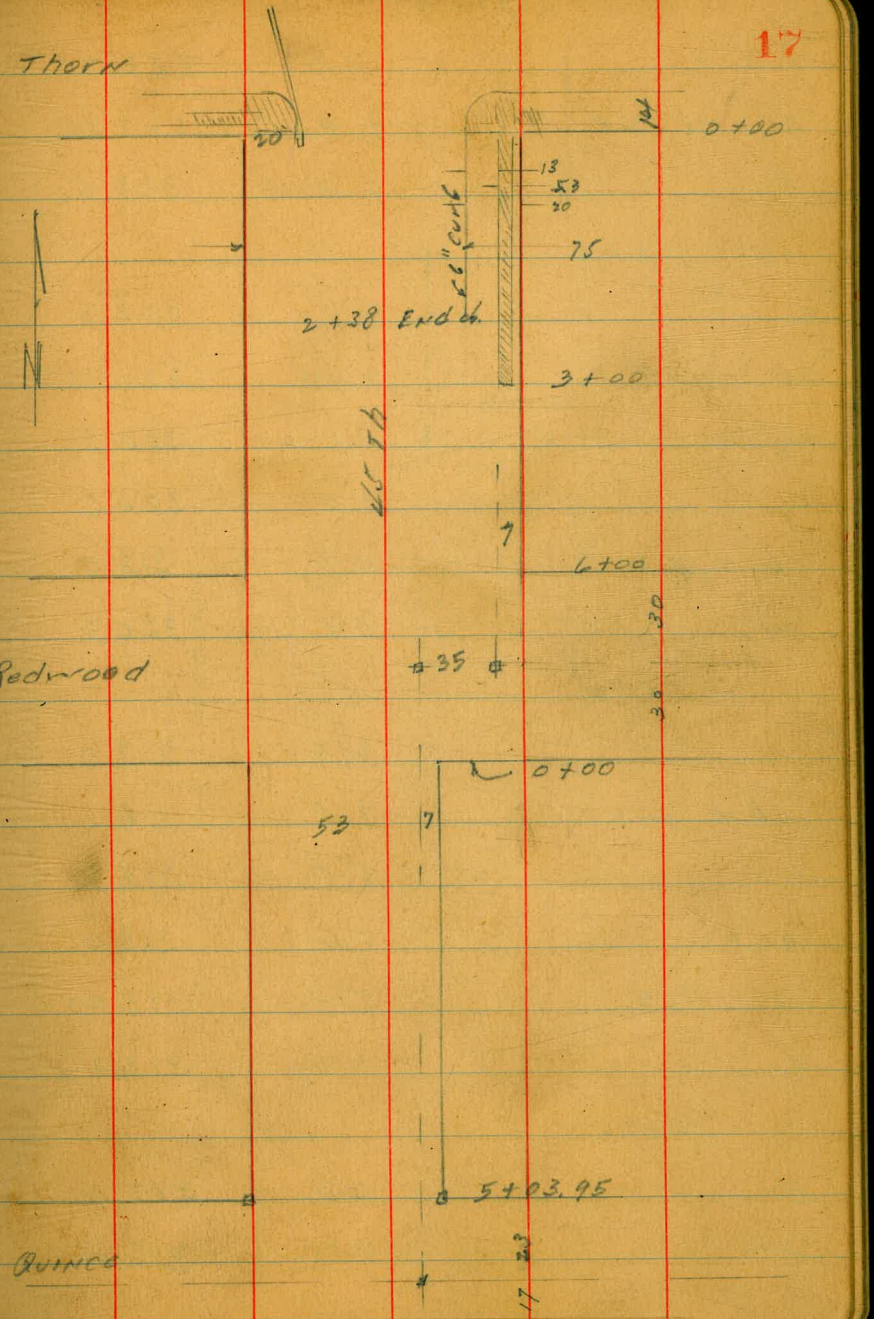
6+05 you have on Ollie P13

INDEXED
EEB

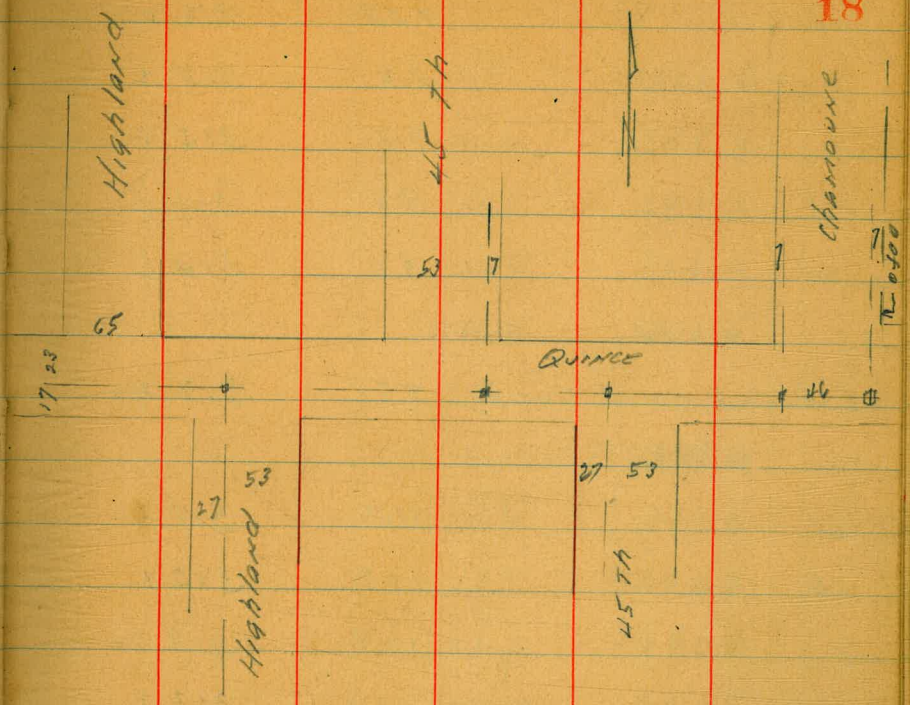
X sec of 45th St.
Thorn to Quince

			Thorn	
NWBP	1.05	334.01	332.96	Chartrune
0+0 SL Thorn				
E		7.2	326.8	
cb Top		7.50	326.51	
gut		8.5	325.5	
C		8.3	325.7	
gut FL. outlet drain		10.0	324.0	
cb Top		6.81	325.20	
W		8.8	325.2	
T.P.	0.98	327.61	11.38	327.63
0+50				
W		0.7	322.9	
cb & gut		1.9	321.7	
C		0.0	323.6	

Reduced & Plot on Profile 1669 3/7/40 CBH



	323.61		
qvT		0.3	323.3
E cb Top		+ 0.25	323.86
E		+ 0.X	324.0
1+00			
E		1.3	322.3
cb Top		2.4X	321.17
qvT		3.1	320.5
c		3.0	3206
cb & qvT		4.7	318.9
W		3.3	320.3
1+50			
W		6.6	317.0
cb & qvT		7.5	316.1
c		5.5	318.1
qvT		5.6	318.0
cb Top		5.71	318.40
E		4.7	318.9
2+00			
E		6.3	317.3
+ ~		7.71	316.4



		323.61 ✓		
c6			7.58	316.03
q.t			8.8	315.3
c			7.7	315.9
c6			9.7	314.4
w			9.0	314.6
2+38				
E c6. Top end curb			9.71	313.90
2+50				
w			11.7	311.9
c6			11.5	312.1
c			10.8	313.2
c6			10.8	313.3
E			9.7	313.9
2+90				
E			12.0	311.6
c6			12.4	311.2
c			12.9	310.7
c6			13.0	310.6
w			13.4	310.2
T.P.	0.58	311.49 ✓	12.70	310.91

		311.49 ✓		
3+10				
w			2.9	308.6
+15			2.6	308.9
c			13.3	298.2
c6			2.4	308.9
E			0.0	311.5
3+50				
E			2.1	309.4
+15			4.2	307.3
c			17.2	294.3
+10			21.1	290.4
c6			21.0	290.5
w			10.6	301.1
+10			7.0	304.5
4+00				
-10			10.4	301.1
w			15.5	296.0
c6			25.5	286.0
+15			26.6	285.1
c			18.6	292.9

311.49 ✓

c6 + 5		6.0	305.5
E		4.~	307.3
4+50			
E		6.9	304.6
+15		8.6	302.9
C		~3.~	288.3
+10		28.3	283.2
c6		~8.5	283.0
W		19.3	292.2
+10		15.5	296.0
T.P.	0.76	~99.57 ✓ 12.68	~98.81
5+00			
-10		7.0	292.6
W		10.0	289.6
c6+5		21.1	278.5
" +15		19.7	279.9
C		14.1	285.5
+3~		0.0	299.6
E		+4.1	303.7

299.57

20

5+50			
E		+4.0	303.6
+10		0.0	299.6
C		16.1	283.5
+10		~3.1	276.5
c6		~3.5	276.1
W		16.7	282.9
+10		12.8	286.8
6+00 N.L Redwood			60' wide
-15		~8.~	271.4
W		~5.1	274.5
C		6.6	293.0
T.P.	9.50	308.~ ✓ 0.85	~98.7~
C +30		5.8	302.4
E		4.~	303.8
E Redwood			
E - bet. cons		8.~	300.0
C to North		12.~	296.0

308.22

C+37	21.0	287.2
W	05.6	282.6
+15	31.1	277.1
S.L. Redwood: 0+0 45th 60' wide here		
-15	31.8	276.4
W	26.8	281.4
C	18.1	290.1
+15	13.3	294.9
E	12.8	295.4
0+20		
E	14.2	294.0
+20	14.5	293.7
C	19.3	288.9
+10	25.2	283.0
W	28.3	279.9
+15	28.8	279.4
0+50		
-15	17.2	291.0
W	18.0	290.2
+20	18.0	290.2

308.22

C	14.8	293.4
E	13.6	294.6
0+75		
E	10.5	297.7
+10	13.2	295.0
C	13.4	294.6
W	10.8	297.4
1+00		
W	8.6	299.6
C	9.2	298.8
+8	11.5	296.7
+16	10.8	297.4
E	8.6	299.6
1+50		
E	5.2	303.0
+20	4.6	301.6
C	5.5	302.7
W	3.2	304.8
1+65		
W	2.7	305.5

308.27

C	3.3	304.9	
+15	6.0	302.2	
E	3.5	304.7	
1+73			
E	4.0	304.2	
+20	6.0	302.2	
C	7.3	300.9	
W	10.9	297.3	
1+95			
W	12.3	295.9	
C	11.3	296.9	
+10	6.7	302.0	
+19	6.1	302.1	
+24	11.7	297.0	
E	11.5	296.7	
2+07			
E-10			
E	10.4	298.8	
+10	9.1	299.1	
+15	5.3	302.9	

308.27

C	6.5	301.7	
W	2.9	305.3	
+10	2.9	302.3	
2+25			
W	2.4	305.6	
+24	2.2	306.0	
C	4.1	304.1	
+15	4.2	304.0	
+20	1.9	306.3	
E	2.3	305.9	
2+50			
E	3.0	305.2	
C	2.7	305.5	
W	2.7	305.7	
T.P. 27	307.19	3.30	304.92
3+00			
W	3.4	303.8	
C	3.0	304.2	
E	3.7	303.5	

307.19 ✓

3+50				
E		5.7	302.0	
C		4.9	302.3	
W		5.4	301.8	
4+00				
W		7.0	300.2	
C		6.7	300.5	
E		6.6	300.6	
4+50				
E		8.1	299.1	
C.		8.5	298.7	
W		9.0	298.2	
5+03.95 N.L Quince				
W	on pipe Cor.	10.73	296.46	Set B.M.
C		10.1	297.1	
E	on hub	10.25	296.94	

INDEXED
EF3

Xsec of Quince 40 wide
Chamoune to Highland

B.M. Pipe NW Cor.	9.18	305.64 ✓	296.46	45 ft Quince

E.L. Chamoune N of Quince = 60' wide

N	3.7	301.9	
C	4.6	301.0	
S	5.7	299.9	
Set BM. 16 N 7+17	4.81	300.83	SE Quince Chamoune

E Cham to N.

S	5.4	300.2	
C	4.4	301.2	
N	3.4	302.4	

W+Chamoune = 0+00 beg. Quince 40' wide

N	5.1	300.5	
C	5.6	300.0	
S	6.4	299.2	

305.64 ✓

0+50

S	9.8	295.8	
C	9.1	296.5	
N	8.3	297.3	

0+75

N	10.4	295.2	
C	11.4	294.2	
S	12.4	293.2	
T.P.	0.44	=93.61 ✓	12.47	=93.17

1+00

S	5.5	288.1	
C	4.5	289.1	
N	3.4	290.4	
N	8.6	285.0	
C	9.8	283.8	
S	10.6	283.0	
T.P.	0.85	=81.73 ✓	12.73	=80.88

Notes Reduced and Plat and new profile 3/17-1940 C.B.H.

281.73

1+50

S	6.7	275.0
C	7.3	274.4
N	6.5	275.2

1+67.5 EL 45Th to So.

N	15.3	266.4
C	17.7	264.0
S	20.1	261.6

1+87.5

— 22	33.1	248.6
S	14.6	267.1
C	8.6	273.1
N	7.5	274.2
+30	12.4	269.3

2+07.5 E to So.

N	1.0	280.7
C	3.8	277.9
S	7.1	274.6
+15	11.1	270.6

281.73

TP	11.88	293.35	281.47

2+47.5 = EL 45Th South

S	9.8	283.6
C	7.6	285.8
N	6.2	287.2

T.P	8.28	300.32	1.31 + 9 = 0.4

2+75

N	8.5	291.8
C	9.8	290.5
S	11.5	288.8

2+00

S	7.7	292.6
C	6.7	293.6
N	5.9	294.4

2+25.9 EL 45Th to North

N	2.4	297.9
C	4.4	295.9
S	5.6	294.7

300.32

2+55.9 ℄ 4+75

S		4.7	295.6
C		4.1	296.2
N		3.1	297.2

3+85.9 W⊥ 4+75 to N

N Top Pipe		3.87	296.45
C		4.9	295.4
S		5.5	294.8

4+10

S		7.4	292.9
C		6.3	294.0
N		5.3	295.0

4+40

N		8.8	291.5
C		9.8	290.5
S		10.3	290.0

T.P.	0.75	288.27	12.30	288.02

288.27

4+70

S		4.9	283.4
C		4.0	284.3
N		1.4	286.7

4+95

N		8.7	279.6
C		9.8	278.5
S		10.3	278.0

TP	0.00	275.31	12.94	275.31

5+25

S		7.5	267.8
C		6.7	268.6
N		5.8	269.5

5+47.5 E⊥ Highland to S.

N		12.8	262.5
C		14.2	261.1
S		14.2	261.1

		275.31			
T.P.	0.31	267.82	12.80	262.51	
	5+87.5	E to	50.		
S			14.3	248.5	
C			13.7	249.1	
N			14.6	248.2	
T.P.	4.11	254.31	12.62	250.20	
Set B.M. 13. Con. M.			10.92	243.39	Quince Highland
	6+13				
N			18.0	236.3	
C			16.1	238.2	
S			13.7	240.6	
	6+27.5	E to	No. 9		
S-25			21.0	233.3	
S			20.5	233.8	
C			20.0	234.3	

		254.31			
N			19.5	234.8	
+25			19.0	235.3	
	6+38				
N			21.4	232.9	
C			21.0	233.3	
S			23.1	231.2	
+30			24.2	229.9	
	6+48				
S			21.5	232.8	
C			21.6	232.7	
N			20.2	234.1	
	6+56	EC Highland to	No.		
N			16.1	238.2	
C			17.7	236.6	
S			18.2	236.1	
T.P.	12.73	266.66	0.38	253.93	
	6+88.5	E to	No.		
S			16.8	249.9	

		266.66		
C			14.1	252.6
N			13.9	252.8
7 ft rt Highland to No				
N			5.0	261.7
¢			6.2	260.5
S			10.2	256.5
+ 10			13.3	253.4
T.P.	8.89	273.27	2.28	264.38
T.P.	12.17	284.57	0.87	272.40
T.P.	11.90	296.12	0.41	284.16
T.P.	10.48	305.74	0.86	295.26
T.P.	4.16	308.45	1.45	304.29
T.P.	2.90	308.60	2.75	305.70
SWBP 44th + Thorn			4.45	304.15

Please check

No record in office
CBH

INDEXED
EFB

X Sec of Catalina Blvd

Pt. Loma Ave to Hill St.

See 1348-1 for sketch

Paloma & Cat.		0.27	234.89		234.62	N.W.B.F.
T.P		6.89	229.24	12.54	222.35	
0+18						
W	Pav			7.68	221.56	
cb	"			8.86	220.38	
1/4	"			9.82	219.42	
c	"			10.07	219.17	
+11	edge			10.18	219.06	
1/4				10.5	218.7	
gut				10.88	218.36	
cb + r	Cen end			10.27	218.97	W+68
E				10.5	218.7	
0+00						
E				9.3	219.9	
cb				9.4	219.8	
+1				10.2	219.0	

Notes Red. & Plot on Profile # 1057 4-7-40 C.B.H.

80' wide
14' cbs
13' 1/4

229.24

Moore
4-4-40

1/4			9.9	219.3
c	Pav		9.28	219.96
1/4	"		8.99	220.25
cb	"		8.34	220.90
W	"		7.53	221.71
0+02				
W	gut		7.44	221.80
W	cb Top Ret.		6.80	222.44
℄ Ret				
W Top cb			7.25	221.99
gut			7.91	221.33
0+22				
W	on walk		6.66	222.58
cb			7.06	222.18
gut	Pav		7.82	221.42
1/4	"		7.98	221.26
c			8.7	220.5
1/4			9.1	220.1
+9			9.7	219.5

		29.24		
+11		8.1	221.1	
cb		8.1	221.1	
E		7.9	221.3	
0+50				
E		6.6	222.8	
cb		6.5	222.7	
+4		6.7	222.5	
+5		8.8	220.4	
1/4		8.3	220.9	
c		7.4	221.6	
1/4		7.1	222.1	
qut		6.9	222.3	
cb		5.90	223.34	
W	walk	5.66	223.58	
1+00				
W	"	3.60	225.64	
cb		3.77	225.47	
qut		5.4	223.8	
1/4		5.3	223.9	
c		5.4	223.6	

		29.24		
1/4		6.5	222.7	
+3		6.8	222.4	
+5		4.2	225.0	
cb		4.2	225.0	
E		4.7	224.5	
1+50				
E		3.0	226.2	
cb		3.3	225.9	
+5		3.4	225.8	
+7		5.2	224.0	
1/4		4.9	224.3	
c		3.9	225.3	
1/4		3.6	225.6	
qut		3.6	225.6	
cb		1.83	227.41	
W	walk	1.72	227.52	
1+75				
W		0.86	228.38	
cb		1.04	228.20	
qut		2.8	226.4	

		29.24		
1/4			2.8	226 4
C			3.1	226 1
1/4			3.9	225 3
+5			4.4	224 8
+6			2.7	226 5
CL			2.8	226.4
E			3.0	226 2
T.P.	10.52	37.32	2.44	226.80
		7+00		
E			10.4	226.9
CL			10.3	227.0
+7			10.0	227.3
+8			11.7	225 6
1/4			11.4	225.9
C			10.6	226 7
1/4			10.2	227.1
QUT			10.0	227.3
CL			8.47	228 85
W		HEAK	8.78	229.04

		37.32		
		7+50		
W			7.31	230 01
CL			7.50	229 82
QUT			8.8	228 5
1/4			8.9	228.4
C			9.2	228.1
1/4			10.2	227.1
+4			10.5	226 8
+5			8.7	228.6
CL			9.8	228 0
E			10.0	227 3
		3+00		
E			9.0	228 3
CL			8.4	228 9
+8			8.1	229.2
+9			9.4	227 9
1/4			9.1	228.2
C			8.1	229 2
1/4			7.7	229.6
QUT			7.6	229.7

	237.34			
CB		4.47	230.85	
W	WK	6.26	231.06	
3+50				
W	WK	5.18	232.14	
CB		5.40	231.92	
QUT		6.4	230.9	
1/4		6.6	230.7	
C		7.1	230.2	
1/4		8.1	229.2	
4+4		8.1	229.2	
4+5		6.4	230.7	
CB		7.3	230.0	
E		7.9	229.4	
4+00				
E		7.1	230.2	
CB		6.7	231.1	
4+8		5.7	231.6	
4+9		7.4	229.9	
1/4		7.1	230.2	
C		6.1	231.2	

	237.34			
1/4		5.7	231.6	
QUT		5.5	231.8	
CB		4.41	232.91	
W		4.18	233.13	
4+50				
W		3.45	233.87	
CB		3.64	233.68	
QUT		5.0	232.3	
1/4		5.2	232.1	
C		5.5	231.8	
1/4		6.5	230.8	
4+3		6.4	230.9	
4+4		4.7	232.6	
CB		5.5	231.8	
E		6.0	231.3	
5+00				
E		5.6	231.7	
CB		6.8	232.5	
4+9		6.8	232.5	
4+10		5.8	231.5	

		237.32		
1/4			5.7	231.6
c			5.1	232.2
1/4			4.7	232.6
gut			4.5	232.8
cb			3.05	234.27
w			2.80	234.52
	5+29.37 Rt.			
w			2.26	235.06
cb			2.72	234.60
gut			3.9	233.4
1/4			4.4	232.9
c			4.8	232.5
1/4			5.2	232.1
+ 5			4.2	233.1
cb			4.2	233.1
E			4.2	233.1
+10			6.5	230.8
	5+39.36 N.L. Paloma			
w			1.97	235.35
+12	= cb Ret		2.57	234.75
"	gut		3.22	234.10
cb	Pav.		3.30	234.02

	237.32			
N cb Paloma on Ret			10.3	S of N cb
w	Top cb Ret		2.07	235.25
"	gut		2.60	234.72
N cb Paloma				
-10 cb			1.28	236.04
+10 gut			1.94	235.38
w	Pav.		2.55	234.77
w cb	"		2.99	234.33
N 1/4				
-10	Pav		1.46	235.86
w	"		2.11	235.21
cb	"		2.88	234.44
℄				
-10	Pav		1.06	236.26
w	"		1.75	235.57
cb	"		2.63	234.69
1/4			3.6	233.7
c			4.2	233.1
1/4			4.9	232.4
+5			3.3	234.0

		237.82		
cb			3.6	233.7
+11			6.9	230.4
E			7.1	230.2
+10			8.0	229.3
S cb				
-10			8.1	229.2
E			6.0	231.3
cb			3.5	233.8
+6			3.0	234.3
+8			4.6	232.7
1/4			4.7	232.6
c			4.1	233.2
1/4			3.5	233.8
+8			3.1	234.2
cb			2.2	235.1
W			0.5	236.8
T.P.	10.04	245.47	1.89	235.43

		245.47			
0+00 St Paloma. Catalina = 70' wide 10 cb on W					
				236.9	1/4 + ℄ regular
0-10			8.4		E cb "
W			9.6	235.9	
cb = W+10			9.98	235.49	This old
gut			11.6	233.9	curb
1/4			11.7	233.8	is
C			12.1	233.4	N.G.
1/4			12.7	232.8	
+3			12.7	232.8	
+4			11.1	234.4	
cb regular			10.5	235.0	
E			13.4	232.1	
+10			15.4	230.1	
0+50					
-10 = Line to N			15.2	230.3	
E			12.5	233.0	
cb			9.8	235.7	
+10			12.0	233.5	
1/4			12.0	233.5	

2 4 5 4 7

C		11.4	234.1
1/4		11.1	234.4
QUT		11.1	234.4
1/4 + 7 = 06		9.7N	235.75
C6 + 8		9.4	236.1
W		7.4	238.1
+ 10 LINE TO N		6.4	239.1
1 + 00 S			
- 10		5.7	239.8
- N		6.N	239.3
W		7.6	237.9
+ N		8.4	237.1
C6		8.7N	236.75
QUT		10.N	235.3
1/4		10.1	235.4
C		10.6	234.9
1/4		11.1	234.4
+ 5		10.8	234.7
+ 10		9.3	236.2
C6		9.4	236.1

2 4 5 4 7

E		13.5	232.0
1/10		15.0	230.5
1 + 50			
- 10		14.6	230.9
E		12.4	233.1
C6		8.7	236.8
+ 4		7.8	237.7
+ 8		10.1	235.4
1/4		10.2	235.3
C		9.6	235.9
1/4		9.N	236.3
+ 7 QUT		9.4	236.1
" C6		7.80	237.67
+ 8		7.4	238.1
W		6.N	239.3
+ 1		5.7	239.8
+ 10		4.6	240.9
N + 0.2			
- 10		3.5	242.0
- N		4.N	241.3

		245.47						
W			6.7	239.3				
CB			6.53	238.94				
GUT			8.3	237.2				
1/4			8.2	237.3				
C			8.7	236.8				
1/4			9.2	236.3				
+6			9.1	236.4				
+7			7.4	238.1				
CB			7.5	238.0				
E			11.6	234.9				
+10			12.6	232.9				
	2+50							
-10			11.1	234.4				
E			9.5	236.0				
CB			5.5	240.0				
+6			5.7	239.8				
+7			7.8	237.7				
1/4			7.9	237.6				
C			7.8	237.7				
1/4			7.4	238.3				

		245.47						
GUT			7.4	238.3				
CB			5.70	239.77				
W			5.4	240.3				
+1			3.5	241.0				
+10			2.4	243.1				
T.P.	8.60	252.33	1.74	243.73	nail in pole 3+00			
	3+00							
-10			8.4	244.1				
-1			9.0	243.3				
W			10.4	241.9				
+1			11.1	241.2				
CB			11.52	240.81				
GUT			12.9	239.4				
1/4			12.9	239.4				
C			12.9	239.4				
1/4			13.9	238.4				
+5			13.6	238.7				

	252.33		
+7		11.6	240.7
cb		11.5	240.8
E		15.4	236.9
+10		16.4	235.9
3+15			
-10		12.6	239.7
E		11.5	240.8
cb		11.5	240.8
+4		11.8	241.0
+4		13.1	239.2
1/4		13.5	238.8
c		12.7	239.6
3+50			
-10		12.1	240.2
E		11.6	240.7
cb		10.4	241.9
+5		10.5	241.8
+6		12.2	240.1
1/4		12.7	239.6
c		12.0	240.3

	252.33		
1/4		11.5	240.8
qcT		11.7	240.6
cb		10.07	242.26
W		9.4	242.7
+2		7.4	244.9
+10		6.5	245.8
4+00			
-10		5.2	247.1
-2		6.0	246.3
W		8.4	243.9
cb		8.60	243.73
qcT		10.4	241.9
1/4		10.1	242.2
c		10.5	241.8
1/4		11.5	240.8
+8		11.0	241.3
+9		9.2	243.1
cb		9.1	243.2
E		10.1	242.2
+10		11.0	241.3

	252.33		
4+50			
-5	9.1	243.2	
E	8.7	243.6	
cb	8.0	244.3	
+2	8.2	244.1	
+10	10.2	242.1	
1/2	10.6	241.7	
c	9.1	243.2	
1/2	8.7	243.6	
+7 qu T	9.0	243.3	
" cb	7.0x	245.29	
W	7.0	245.3	
+2	4.3	248.0	
+10	3.7	248.6	
5+00			
-10	2.2	250.1	
-2	2.7	249.6	
W	5.4	246.9	
cb	5.31	247.02	
qu T	7.6	244.7	

	252.33		
1/4		7.2	245.1
c		7.5	244.8
1/4		8.8	243.5
+3		8.6	243.7
cb		6.4	245.7
E		7.1	245.2
+10		7.8	244.5
5+50			
-10		6.3	246.0
E		5.2	247.1
cb		5.0	247.3
+5		6.0	246.3
+6		7.4	244.9
1/4		7.3	245.0
c		6.1	246.2
1/4		6.0	246.3
qu T		6.4	245.9
cb		3.75	248.58
W		3.7	248.6
+2		1.4	250.9
+10		0.7	251.6

		252.33		
6+00.31	N L Verona			
-10	+ W L to So.	0.5	251.8
W			1.2	251.1
cb			2.28	250.05
gut			4.8	247.5
1/4			4.4	247.9
c			4.7	247.6
1/4			5.7	246.6
+5			6.0	246.3
+6			4.0	248.3
+11	10" Acasia			
cb			3.8	248.5
E			4.9	247.4
+10			5.5	246.8
N cb				
-10			5.4	246.9
E			4.7	247.6
cb			3.3	249.0
+4			4.0	248.3
+7			5.6	246.7

		252.33			
1/4			5.6		246.7
c			4.5		247.8
1/4			4.1		248.2
gut			4.3		248.0
W	old cb P.C.		2.06		250.27 of P
"	gut		2.8		249.5
+10	" + cb		1.22		251.11 10' old cb on N side of Verona
℄					
-10	pav		0.18	252.15	N.C. should be 1/2 c℄
W	"		1.12		251.21
cb	"	cb 14' new	2.57		249.76
+8			3.9		248.4
1/4			3.6		248.7
c	SMH Rim		3.66		248.67
1/4			5.2		247.1
+1			5.2		247.1
+8			2.7		249.6
cb			2.9		249.4
E			4.6		247.7
+10			5.7		246.6

≠57.33

E+4 & E+7 12" Pepper tree

Sob

~10 against	City pump building	5.6	246.7
E		5.0	247.3
cb		2.7	249.6
+4		2.6	249.7
+8		4.3	248.0
1/4		4.6	247.7
c		3.4	248.9
1/4		3.2	249.1
+5		3.5	248.8
cb Par.		2.46	249.87
W	"	1.46	250.89
+10	" gut	0.40	251.93
"	cb	+0.20	252.53

Mid. S.W. Rot

cb		1.73	250.60
gut par		2.26	250.07

≠57.33

S2 Varona = 0+00

W sdw		0.89	251.44
cb		1.83	250.50
gut Par		2.32	250.01
0+10			
W	walk	1.02	251.31
cb	on BM BP	1.56	≠50.77 ≠50.82
gut		2.2	2501
1/4		2.5	249.8
c		2.8	2495
1/4		3.4	248.9
+5		3.5	248.8
+10		2.1	2502
cb		2.5	249.8
E		4.7	247.6
+10		5.6	246.7

Date

0715 E+5 30" Palm

		257.33		
0+37				
E - 21.4 E	shop + gar.	5.87	246.46	cem fl.
E - 4.5 Sedge	8' con. apron	5.00	247.33	
0+50				
E + 4.5	24" Pepper			
E + 6.5	gas Pump			
E + 15.5	Tank inlet cap			
-10		4.9	247.4	
E		3.7	249.1	
cb		1.7	250.6	
+5		1.7	250.6	
+6		2.4	249.9	
1/4		2.7	250.1	
c		1.9	250.4	
1/4		1.7	250.6	
qut		1.7	250.6	
cb		0.60	251.73	
W	walk	0.31	252.02	
T.P.	9.68	260.45 ✓	1.56	250.77 250.8 ✓
BM SW Cat. + Varong				

	260.45 ✓		
0+70			
E + 6	20" Pepper Tree		
0+79 E + 3	P. Pole		
1+00			
W	on walk	7.30	253.15
cb		7.51	252.94
qut		8.8	251.7
1/4		8.7	251.8
c		8.7	251.8
1/4		9.3	251.2
+4		9.5	251.0
+7		9.0	251.5
cb		9.3	251.2
E		10.7	250.3
+10		11.0	249.5
1+50			
E		7.8	252.7
cb		7.0	253.5

	260.45		
c6 +4	7.9	252.6	
+6	8.6	251.9	
1/4	8.4	252.1	
C	7.7	252.8	
1/4	7.6	252.9	
QUT	7.7	252.8	
c6	6.20	254.25	
W WALK	5.95	254.50	
2 +00			
W	4.57	255.88	
c6	4.98	255.47	
QUT	6.3	254.2	
1/4	6.7	253.8	
C	6.9	253.6	
1/4	7.0	252.9	
+7	7.8	252.7	
+8	5.8	254.7	
c6	5.5	2550	
E	6.3	254.2	

	260.45		
2 +10			
QUT	5.5	2550	
W c6 P.C.	4.80	255.65	
W.	4.20	256.25	
2 +20 N.L. Reduced		Savoy St.	
W	3.56	256.89	
+11 c6 Ret	4.35	256.10	
QUT Pan	4.97	255.48	
c6 "	5.24	255.20	
1/4	6.2	254.3	
C	6.7	253.8	
1/4	7.1	253.4	
+7	7.4	253.1	
+8	5.7	254.8	
c6	5.5	2550	
E	5.8	254.7	
W. c6			
W — 10 c6	2.20	258.25	
" QUT	2.82	257.63	
W c6	8.14	257.31	
" QUT	3.80	256.65	
c6 Pan	4.93	255.52	

260.45

E Savoy				
-10	par	2.46	258	19
W	"	3.46	257.	19
cb	"	4.58	255.	87
1/4		5.7	254.	8
c		6.7	254	3
1/4		4.7	253.	8
+7		4.9	253	6
+8		5.0	255	5
cb		4.4	256.	1
E		5.3	255.	2
S cb				
W cb	par	4.48	255.	97
W	"	3.36	257.	09
+10	gut	4.38	258.	07
"	cb	1.75	258.	70
S L Savoy -00				
W	wk	4.96	257	49
+ 11	cb	3.80	256.	65
"	gut	4.38	256.	07
cb	par.	4.5~	255.	93

260.45

1/4	5.3	255	2
c	5.5	255	0
1/4	6.0	254	5
+7	4.4	254	1
+10	4.3	256	2
cb	4.5	256	0
E	5.1	255	4
0 +10			
W gut	4.7	255	8
W cb pc	3.74	256.	71
W walk	3 3~	257.	13
0 + 50			
W	4.94	257.	49
W cb	3.17	257	28
gut	4.5	256	0
1/4	4.4	256	1
c	4.1	256.	4
1/4	4.9	255	6
+9	5.5	255.	0.
+10.	3.9	256.	6

	260.45		
eb	3.6	256.9	
E	3.8	256.7	
1+00			
E	3.3	257.2	
eb	2.8	257.7	
+2	2.7	257.8	
+3	2.7	258	
1/4	2.2	256.3	
c	3.7	256.8	
1/4	3.6	256.9	
gut	3.6	256.9	
eb	2.34	258.11	
wl walk	2.1	258.33	
1+50			
wl	1.40	259.05	
eb	1.58	258.87	
gut	2.4	257.9	
1/4	2.8	257.7	
c	2.9	257.6	
1/4	3.4	257.1	

	260.45		
+9	3.8	256.7	
+10	2.5	258.0	
eb	2.3	258.2	
E	2.5	258.0	
2+00			
F	1.9	258.6	
eb	1.7	258.8	
+4	1.7	258.8	
+5	3.1	257.4	
1/4	2.9	257.6	
c	2.3	258.2	
1/4	2.2	258.3	
gut	2.1	258.4	
eb	0.84	259.61	
wl	0.60	259.85	
2+25			
wl	0.32	260.13	
eb	0.51	259.94	
gut	2.0	258.5	
1/4	2.0	258.5	

		260.45		
C			2.0	258.5
1/4			2.6	257.9
+7			2.9	257.6
+8			1.2	259.3
cb			1.0	259.5
E			1.5	259.0
T.P.	6.41	264.22	2.64	257.81
2+50				
E			4.9	259.3
cb			4.9	259.3
+5			4.9	259.3
+6			6.5	257.7
1/4			6.2	258.0
C			5.7	258.5
1/4			5.7	258.5
QUT			5.6	258.6
cb			4.08	260.14
W			3.90	260.32

		264.22		
2+75				
W			3.86	260.36
cb			4.08	260.14
QUT			5.6	258.6
1/4			5.4	258.8
C			5.7	258.5
1/4			6.0	258.2
+6			6.3	257.9
+7			4.8	259.4
cb			4.6	259.6
E			4.6	259.6
3+00				
E			4.7	259.5
cb			4.4	259.8
+6			4.8	259.4
+7			6.2	258.0
1/4			6.0	258.2
C			5.5	258.7
1/4			5.6	258.6

	264.22		
gut	5.6	258.6	
cb	4.16	260.16	
W	4.00	260.22	
3+50			
W	4.28	259.94	
cb	4.51	259.71	
gut	5.7	258.5	
1/4	5.7	258.5	
C	5.7	258.5	
1/4	6.7	258.0	
+5	6.4	257.8	
+11	4.6	257.6	
cb	4.6	257.6	
E	5.1	259.1	
4+00			
E	4.8	259.4	
cb	5.1	259.1	
+5	5.10	259.0	
+6	6.7	257.5	
1/4	6.5	257.7	

	264.22		
C	6.0	258.2	
1/4	5.9	258.3	
gut	5.9	258.3	
cb	4.82	259.40	
W	4.61	259.61	
4+50			
W	4.94	259.28	
cb	5.13	259.09	
gut	6.0	258.2	
1/4	6.2	258.0	
C	6.4	257.8	
1/4	6.9	257.3	
+5	7.0	257.2	
+6	5.4	258.8	
cb	5.12	259.0	
E	5.5	258.7	
5+00			
E	5.9	258.3	
cb	5.5	258.7	
+5	5.4	258.8	

	264.22		
+4	7.3	256.9	
1/4	7.1	257.1	
c	6.6	257.6	
1/4	6.4	257.8	
gut	6.2	258.0	
cb	5.42	258.80	
W	5.18	258.04	
5+45 approx cb P.C.			
W	4.62	259.60	
cb	5.42	258.78	
gut	6.2	258.0	
5+51.79 opposite NW Santa Barbara.			
W	4.07	259.75	
+13 cb Rec	5.26	258.99	
gut	6.0	258.2	
1/4	6.4	257.8	
c	6.6	257.6	
1/4	7.1	257.1	
+6	7.2	257.0	
+7	5.4	258.8	

	264.22		
cb	5.5	258.7	
E	7.1	257.1	
+10	8.1	256.1	
5+60.2		560.13×8-20	
-10	8.2	256.0	
E	7.3	256.9	
cb	5.9	258.3	
+5	5.9	258.3	
+7	7.3	256.9	
1/4	7.1	257.1	
c	6.6	257.6	
1/4	6.1	258.1	
cb	5.9	258.3	
W gut	4.90	259.30	
" cb	4.39	259.83	
No change to Sta.			
NW1 Santa Barb. + Cat.	3.41	260.61	260.48

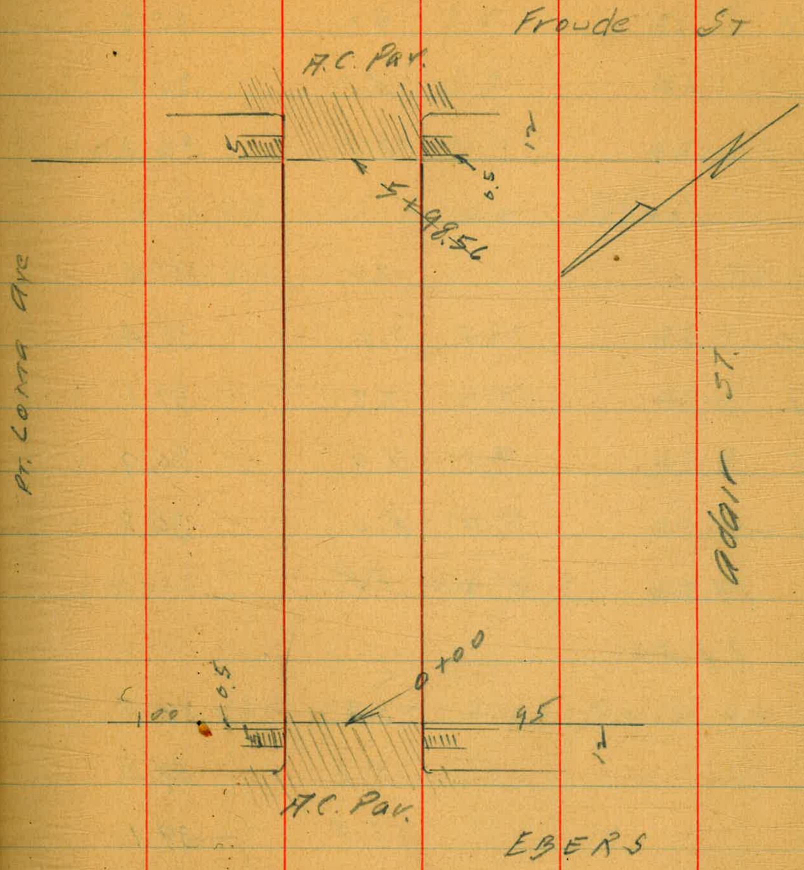
Moore
4-4-40

INDEXED
EFB

X sec. alley 20' wide
Blk 3 Sunset Cliffs

SWBP	10.79	44.83	34.04	Pt. Loma Ebers
0+12 Ely of Ebers				
N Pav.		12.84	32.01	
S "		13.03	31.80	
0+00 Ely Ebers				
S cb		12.07	32.76	
" Pav		12.52	32.31	
C "		12.73	32.10	
N "		12.43	32.40	
" cb		12.06	32.77	
0+05				
N		11.2	33.6	
C		11.6	33.2	
S		11.3	33.5	
0+50				
C 20		9.1	35.7	
S		9.3	35.5	

Red'x Plot. New Profile 4-5/40/ C.B.H



44.83

C	9.2	35.6
N	8.7	36.1
1+20	8.4	36.4
1+00		
-20	7.1	37.7
N	7.4	37.4
C	7.7	37.1
S	7.9	36.9
1+20	8.0	36.8
1+20 S + 0.7 P.P.		
1+50		
-20	6.3	38.5
S	5.8	39.0
C	5.7	39.1
N	5.9	38.9
1+20	5.4	39.4
2+00		
-20	3.0	41.8
N	3.4	41.2

44.83

C	3.5	41.3
S	3.7	41.1
1+20	4.2	40.6
2+40 S - 0.2 P.P.		
2+50		
-20	2.1	42.7
S	1.2	43.6
C	1.0	43.8
N	0.7	44.1
1+20	0.4	44.4
T.P. 1+85	57.02	0.66 44.17
3+00		
-20	10.3	46.7
N	11.1	45.9
C	11.4	45.6
S	11.7	45.3
1+20	12.1	44.9

57.0 N

3+50

-20	10.9	46.1
S	10.2	46.8
C	9.8	47.2
N	9.4	47.6
+	8.7	48.3

3+60 S+0.3 P.P.

4+00

-20	7.4	49.6
N	8.5	48.5
C	9.0	48.0
S	9.6	47.4
+20	9.8	47.2

4+50

-20	8.1	48.9
S	8.3	48.7
C	7.7	49.3
N	7.3	49.7
+20	6.3	50.7

57.0 N

4+80 S+1.0 P.P.

5+00

-20	5.1	51.9
N	6.5	50.5
C	6.4	50.6
S	6.9	50.1
+20	6.9	50.1

5+50

-20	5.2	51.8
S	4.6	52.4
C	4.6	52.4
N	4.4	52.6
+20	3.3	53.7

5+96 S on line P.P.

5+98.56 W/y Froude

1' ab.	0.45	56.77
N far	0.78	56.24
C "	1.37	55.65
S "	1.49	55.53

		57.02		
S cb			1.08	55.94
T.P.	10.45	66.10	1.17	55.85
	W/y cb line Froude			
S	Par		11.04	55.06
N	"		10.05	56.05
Sw BP	Plowing Froude		1.22	64.88 64.90

Moore
5-17-40

16' wide

Garage Levels Mission Beach Alleys

					San Juan
B.M.	0.41	7.48		7.07	Seawall
T.P. #1			7.8N	−0.3L	Top C6
T.P. #1N	3.85	3.52	7.81	−0.33	" "

alley B/K 155

E.L. Blvd = 00 to Bayside Lane

0 + 27				
S − 2.5	W end apron		3.95	−0.43
S − 4.5	" " rear gar.		3.76	−0.24
0 + 33				
N + 0.5	W. end apron		4.20	−0.68
N − 1	" " rear gar.		4.08	−0.56
0 + 51				
S − 2.4	E end apron		4.03	−0.51
S − 4.4	" " gar.		3.78	−0.26
0 + 59				
N + 0.4	E. end apron		4.31	−0.79
N − 1.1	" " gar.		4.09	−0.57

INDEXED
EFS

	3.5N		
0 + 87			
S	W end apron	4.78	−1.26
S + 5	" " gar.	4.56	−1.04
1 + 07			
S	E end apron	4.77	−1.25
S + 5	" gar.	4.58	−1.08
1 + 2N			
S − 0.6	E apron	5.36	−1.84
S − 4.7	" gar	5.10	−1.48
1 + 84			
S + 0.5	E apron	5.28	−1.76
S − 4.6	" gar	5.15	−1.63
1 + 41			
N	W end apron	5.39	−1.87
N − 7.5	" " gar	5.14	−1.62
1 + 69			
N	E end apron	5.48	−1.96
N − 8	" " gar	5.05	−1.53
1 + 99.1			
N − 1	W end apron	5.18	−1.66
N − 47	" " gar	5.03	−1.51

Con. floors unless noted d.f.

3.5 ± alley Blk 155

1+84 ±

N -1	E end apron	4.96	-1.44
N -4.7	" " gar.	5.00	-1.48

16' alley Blk 160 Blvd=00 to B.S. Lane

TP #1	3.48	3.1 ±	-0.3 ±
	0+1 ±		
S -8.5	E do. apron	3.30	-0.16
S -11.5	" " gar	3.18	-004
	0+40		
S	W edg apron	3.91	-0.27
	0+48		
S	E apron	4.01	-0.87
S -3.5	E gar.	3.78	-0.64
	0+56		
S	E edge apron	4.11	-0.97
	1+30		
N 0.7	E do. apron	4.83	-1.69
1.2	" " gar.	4.8 ±	-1.65

3.1 ±

1+46

S -0.4	E apron	4.91	-1.77
S -3	" S.K. gar.	4.7 ±	-1.60
	1+61		
N -5	E do. gar.	4.63	-149

T.P.	4.5 ±	3.59	4.07	-0.93

16' alley Blk 163 El Blvd=00 to Bayside

	0+00		
S +0.7	W edge apr.	3.71	-0.16
S -0.3	" " 3 car gar.	3.49	+0.10
	0+24		
S -1.8	E edge apr	3.6 ±	-003
S -2.8	" " gar	3.43	+016
	0+75		
N -4.5	W edge gar	4.33	-0.74
	0+91		
S -3.8	W edge "	4.61	-1.02

Plot Plan #3

3.59

0+93

N -3 E edge gar. 4.37 -0.78

1+09

S -3.7 E edge " 4.65 -1.06

1+23

S -5.5 Sin gar 5.6 -2.0 dirt

T.P. 5.16 4.01 4.74 -1.15

16' alley Blk 168 El Blvd=00 to Bay Side Lane

0+36

S -1.0 W edge apr. 4.81 -0.80

S -3.0 " " gar. 4.66 -0.65

0+56

S -1 E edge apr. 4.69 -0.68

S -3 " " gar. 4.57 -0.56

0+65

S -4.7 E Sin. gar. 4.78 -0.77

4.01

1+35

N +0.4 E apron 5.33 -1.32

N -3.4 " Sin. gar. 5.15 -1.14

1+96

N -3 E apron 5.24 -1.23

N -5 " gar. 5.06 -1.05

2+09

N -2.5 E apron 5.22 -1.21

N -5.2 " Sin. gar 5.15 -1.14

T.P. 4.97 4.63 4.35 -0.34

16' alley Blk 171 E of Blvd=00 to E/p

0+05

N -0.9 W edge 3 car gar. 4.45 -0.02

0+31

N -4.0 E " " " 4.65 -0.02

		4.63		
	0+55			
S -0.5	W edge	apr.	5.15	-0.52
S -6.5	" "	gar.	4.92	-0.29
	0+77			
S -0.6	E edge	apr.	5.12	-0.49
S -6.5	" "	gar.	4.91	-0.28
	0+86			
N	℄	apr.	5.16	-0.53
N -2	"	Sin gar.	4.98	-0.35
	1+43			
S -1.0	℄	apr.	5.28	-0.65
S -5	"	Sin gar	5.15	-0.52
	1+83			
S -1.0	℄	apr.	5.42	-0.79
S -5.5	"	gar	5.29	-0.66
	2+02			
S -1.0	℄	apr.	5.53	-0.90
S -2.5	"	Sin gar.	5.43	-0.80
T.P.	4.67	4.58	4.72	-0.09

16' alley Blk 176 E L Blvd=00 to Ely.

		4.58			
	0+73				
N -1.5	Sin	gar.	4.5	+0.1	dirt
S -4.0	"	"	4.60	-0.02	Con. ribbon
	1+00				
S -0.4	W edge	apr.	4.97	-0.39	
S -3.8	"	gar.	4.55	+0.03	
	1+18				
N -3	℄ do.	gar.	4.6	00	dirt
	1+25				
S -0.2	E edge	apr.	4.89	-0.31	
S -3.7	"	gar.	4.59	-0.01	
	1+49				
S +0.3	℄	apr.	5.37	-0.79	
S -0.9	"	Sin. gar.	5.23	-0.65	
	1+86				
N -1.2	Sin.	gar.	5.22	-0.64	
	1+90				
S +0.7	W edge	apr.	5.26	-0.68	

		4.58			
S − 2		w edge gar.	4.82	−0.24	
	2+05				
S − 0.7	E	" apr.	5.20	−0.62	
S + 2	"	" gar.	4.87	−0.29	
T.P.	7.92	7.80	4.70	−0.12	BM 8P Santa Clara + Seaman
T.P. BM.	2.47	9.77	0.50	7.30	7.19
T.P.	2.46	9.65	2.58	7.19	
check to orig. BM.			2.45	7.20	7.07

Alley Block 195 Mission Beach
Bet. Rockaway & San Jose
Mission Blvd to Bayside Lane

BM	0.39	7.47		7.08	B.P. S.W. San Jose Seawall
BM	4.64	4.28	7.83	-0.36	S.E. B.P. San Jose & Mission Blvd
	0+0 = E.L. Mission				
℄ Sta.	0+34				
N = ℄ 3' Door Conc.			4.46	-0.18	
+1' = ℄ 2.4 Bottom Conc Step.			5.00	-0.72	
	0+43				
N = ℄ 2.9 Conc Walk			4.49	-0.21	
N Ground			5.1	-0.82	
	1+36				
N-0.9' = ℄ Garage Conc Floor			4.97	-0.69	
N on Conc. Apron			5.05	-0.77	
+0.4 = ℄ + Sly 11' Conc Apron			5.10	-0.82	
S			5.3	-1.0	
+6' = ℄ Garage Dirt Floor			5.1	-0.8	
	1+42.5				
N-0.4 = ℄ 1.6 Conc Walk			4.96	-0.74	

May 20-40
Sivas
Hortheny
W Moore

	4.28			
	1+50			
S-6.8 = Wly Conc Slab		5.05		-0.77
	1+64.5			
S-6.8 = Ely Conc Slab.		5.07		-0.79

Alley Block 200 Mission Beach
Bet San Jose - Salem   New Garage Levels
Mission Blvd to Bayside Lane

S.E.B.P. San Jose St

BM	5.81	5.45		-0.36	
TP	4.62	3.78	6.29	-0.84	
℄ Stations 0+0 = E.L M					
0+76					
S + 0.2 = ℄ 8' Conc Gateway			3.98	-0.20	
0+83					
S = Wly Conc Apron			4.23	-0.45	
S - 3.7 " " "			3.73	+0.05	
0+96					
S = Ely Conc Apron			4.20	-0.42	
S - 3.7 = Ely Garage Conc Floor			3.82	-0.04	
1+25					
S - 0.7 = ℄ Garage Conc Floor 10' wide			4.23	-0.45	
TP	5.13	4.15	4.76	-0.98	

May 21-40
Sisson
Northern
& Moore

Alley Block 203 Mission Beach
Between Salem - Seagirt
Mission Blvd to Bayside Lane

4.15 Bt. Ford

℄ Sta. 0+0 = E.L Mission Blvd		
0+30		
S - 0.5 = Wly Conc Slab	4.35	-0.20
S Ground	4.8	-0.65
0+61.5		
S - 0.5 = Ely Conc. Slab	4.48	-0.33
S Ground	4.7	-0.5
1+13		
N - 1.0 = ℄ 2.5 Conc Walk	4.88	-0.73
1+16		
N - 0.3 = Wly Conc Back Yard	4.63	-0.48
1+31		
N - 0.3 = Ely Conc Back Yard	4.88	-0.73
1+37		
S - 1.3 = Wly + Wly 2' Conc Walk	4.94	-0.79

4.15

1+46

N-0.5 = ℄ 10.5 Garage Dirt Floor 5.1 -0.9

1+62

S-0.9 = N½ E½ Conc Walk 4.97 -0.82

TP 5.05 3.94 5.26 -1.11

Alley Block 208 Mission Beach
Between Seagirt - Sunset
Mission Blvd to Bay Side Lane

3.94 Bx Ford

0+00 = EL Mission Blvd.

0+92

S-2.6 = ℄ 10' Garage Conc Floor 4.68 -0.74

S-1.9 = N½ Conc Apron 4.90 -0.96

1+16

S-2.6 = ℄ 10' Garage Conc Floor 4.75 -0.81

1+21

S-1.6 = N½ Conc Apron 5.03 -1.09

S-2.6 = N½ Yard Level 4.66 -0.72

1+31

S-1.6 = E½ Conc Apron 4.92 -0.98

S-2.6 = E½ Yard Level 4.73 -0.99

TP 3.31 4.48 2.77 1.17

Alley Block 211 Mission Beach
Between Sunset - Tangiers
From Mission Blvd to Bayside Lane

4.48 Bk. Ford.

0+00 = F.L. Mission Blvd.

0+34

N-0.2 = ℄ 4' Conc. Landing		3.42	1.06
N Ground		4.4	0.1
0+40			
N Ground		4.4	0.1
N-0.4 = ℄ 9' Conc. Apron		3.96	0.52
N-8.7 = ℄ 9' Garage Conc Floor		3.47	1.01
1+13			
S = 8.5 = ℄ 12' Conc Apron		5.19	-0.71
S-4.5 = ℄ 12' Garage Conc Floor		4.94	-0.46
TP	2.70	3.87	3.31	1.17
TP	5.17	4.22	4.82	-0.95

Alley Block 216 Mission Beach
Between Tangiers - Toulon
Mission Blvd to Bayside Lane

4.22 Bk. Ford

0+00 = F.L. Mission Blvd.

0+34

N = ℄ 10' Conc Apron	4.71	-0.49
N-4 = ℄ 10' Garage Conc Floor	4.10	+0.12
0+86		
S = ℄ 4' Conc Landing	4.28	-0.06
S-3 = " " " "	4.25	-0.03
S-3 = ℄ 4' Top Conc Strip	3.62	+0.60
0+47		
S = ℄ 8.7' Conc Apron	4.73	-0.51
S-5.1 = ℄ 8' Garage Conc Floor	3.63	+0.59
0+58		
S = ℄ 9.3 Conc Slab	4.78	-0.56
S-5.3 on Conc Slab	4.53	-0.31
0+64		
N = ℄ 10' Conc Apron	4.69	-0.47
N-1.2 = ℄ 9' Garage Conc Floor	4.69	-0.47

4.22

1+06

H-0.5	= Sly Garage Dirt Floor West Entrance	5.6		-1.4
TP		3.55	4.23	3.54	0.68

Alley Block 219 Mission Beach
Between Toulon - Vanitie
From Mission Blvd to Bayside Land

4.23 Bt. Ford

0+00 = E.L. Mission Blvd

0+56.5

H	= Wly Conc Apron	4.79	-0.56
H-8'	= " " "	4.69	-0.46

0+60

H-8	on Conc Apron	4.89	-0.66
H	= Low Point Conc Apron	4.96	-0.73

0+62

H	= Sly Garage Conc Floor East Entrance	4.88	-0.65
H-8	= Nly Garage Conc Floor 8' Wide East Entrance	4.88	-0.65

0+57

S-1.7	= Nly Garage Conc Floor	5.00	-0.77

0+57.6

S-1.7	= Nly Conc Apron	5.26	-1.03

0+95

S-1.0	= Nly 9' Garage Dirt Floor West Entrance	5.4	-1.2

0+95

S+0.5	= Nly Conc Apron	5.44	-1.21
S-1.0	= Sly Garage Conc Floor	5.23	-1.00

Alley Block 224 Mission Beach
Between Vanitie - San Rafael
Mission Blvd to Bayside Lane

4.23 Bl. Ford

TP	3.65	4.36	3.52	0.71
	0+0 = E.L. Mission Blvd.			
	0+47			
S+0.7 = W/y Conc Aprox			5.03	-0.80
S-2' = " " Garage			4.90	-0.67
	0+59			
S - E/y Conc Aprox			5.07	-0.84
S-2' = E/y Garage Conc. Floor			4.90	-0.67
	0+70			
S Ground			5.2	-1.0
S-0.3 = ℄ 3' Tile Walk			4.82	-0.59
	0+70.5			
N-1' = ℄ 9' Garage Conc. Floor			5.18	-0.95
TP	3.50	3.90	3.96	0.40

Alley Block 232 Mission Beach
Between Venice - Verona
Mission Blvd to Bayside Lane

3.90 Bl. Ford

0+0 = E.L. Mission Blvd			
0+03			
S+1.5 = W/y Conc Aprox	4.74	-0.84	
S-0.4 = W/y Garage Conc Floor	4.86	-0.76	
0+16			
S+1.5 = E/y Conc Aprox	4.64	-0.74	
S Ground	4.8	-0.9	
S-0.4 = E/y Conc Walk Joint Conc Aprox	4.64	-0.74	
0+30			
N = ℄ 3' Conc Walk	4.59	-0.64	
0+36			
N+0.4 = ℄ 7.8 Conc Aprox	4.74	-0.84	
N-0.4 = ℄ 7.8 Garage Conc Floor	4.67	-0.77	
0+46			
N+0.4 = ℄ 7.8 Conc Aprox	4.93	-1.03	
N-0.4 = ℄ 7.8 Garage Conc Floor	4.78	-0.88	
TP	8.21	7.82	4.29	-0.39
BM			0.68	7.14

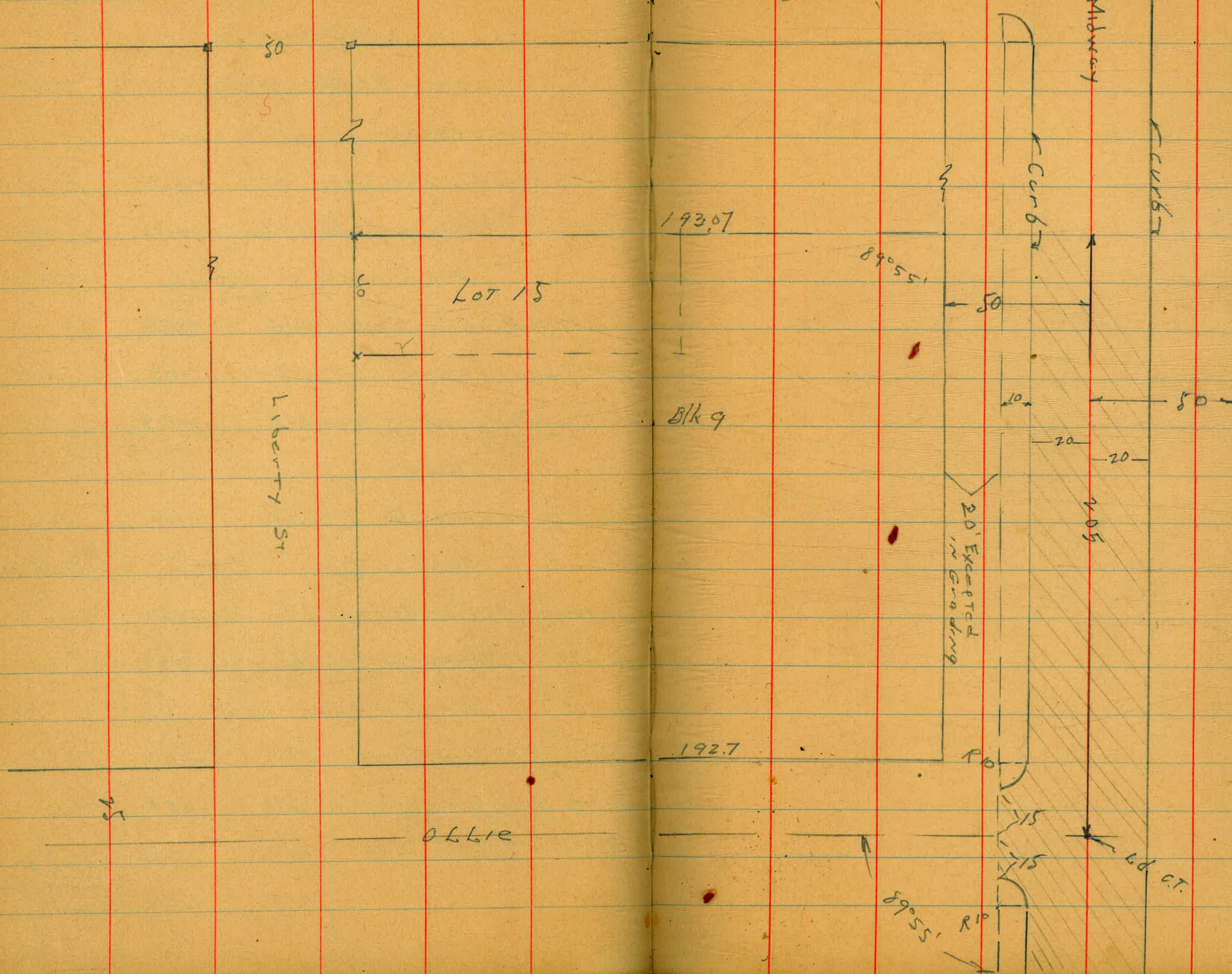
S/W R.P. San Rafael & Seawall 7.13

Set Lath, Front Line Lot 15
Blk 9 Drucker's add

Moore
Somermeyer
WFM
11-14-45

Indexed
G.S.K.

Camulos



Sta	+	H.I	−	Elev
	490			343.29
Center of Howard		348.19		
Curb & Gutter Elevs				
0+00				
0+50				
1+00				
1+50				
2+00				
T.P.			6.76	341.43
2+50	2.10	343.53		
3+00				
3+50				
4+00				
4+50				
5+00				
5+50				
6+00				

X Sec Col. Howard to Clark Line 2

78

W P.L.	W Gutter	½	℄	½	E Gutter	E P.L.
	N.W.C. Col. & Howard					
4.7 / 343.5	4.7 / 343.5	4.5 / 343.7	4.5 / 343.7	4.6 / 343.6	4.5 / 343.7	4.5 / 343.7
	W Curb Elev 5.19 / 343.00	W Gutter Elev 6.61 / 341.58		E Gutter Elev 6.33 / 341.86	E Curb Elev 4.91 / 343.28	
342.8	4.6 / 341.6	5.1 / 343.1	4.7 / 343.5	5.0 / 343.7	4.3 / 341.9	343.1
342.5	6.4 / 341.8	5.7 / 342.5	5.1 / 343.2	5.4 / 342.9	6.2 / 342.0	342.7
342.2	6.6 / 341.6	5.9 / 342.3	5.4 / 342.8	5.8 / 342.4	6.5 / 341.7	342.4
341.9	6.9 / 341.3	6.1 / 342.1	5.7 / 342.5	6.3 / 341.9	6.7 / 341.5	342.
341.6	7.1 / 341.1	6.7 / 341.5	6.2 / 342.0	6.3 / 341.9	7.1 / 341.1	341.7
341.4	T.P. Sta 2+50 west side					
341.4	2.7 / 340.8	2.3 / 341.2	1.9 / 341.6	2.3 / 341.2	2.8 / 340.7	341.3
26', 341.3	3.4 / 340.1	2.9 / 340.6	2.4 / 341.1	2.8 / 340.7	3.7 / 340.2	341.3 @ 26'
340	4.4 / 339.1	3.8 / 339.7	3.5 / 340.0	3.9 / 339.6	4.4 / 339.1	340. 340
338.7	5.0 / 338.5	5.1 / 338.4	4.7 / 338.8	5.1 / 338.4	5.5 / 338.0	338.7
337.5	6.8 / 336.7	6.5 / 337.0	6.2 / 337.3	6.5 / 337.0	6.8 / 336.7	337.5
336.2	7.9 / 335.6	7.6 / 335.9	7.2 / 336.3	7.7 / 335.8	8.0 / 335.5	336.2
335	9.1 / 334.4	8.8 / 334.7	8.4 / 335.1	9.1 / 334.4	9.4 / 334.1	335
333.5	11.0 / 332.5	9.9 / 333.6	9.5 / 334.0	10.8 / 333.5	11.0 / 332.0	333.5
	W Curb 9.86 / 333.67	W Gutter 11.01 / 332.52	E Gutter 11.0 / 332.53	E Curb 9.91 / 333.63		

E.C. 343.52

W.C. 343.29 N.W.C. Howard. - Colonial

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.33
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.