

Levels on El Cajon <sup>Bonnie / 20</sup> <sup>Each</sup>

ENGINEERS

LEVEL BOOK

NO. 10

F.B. 593

WILSON  
TRADE MARK

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

78 West of West 2 Center

593

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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El Cajon Section Page  
Cross section <sup>X.P.</sup> 10 to 12 incl  
From W. Boundary to Wabash  
Levels on El Cajon Boundary  
to Euclid. 1 to 8 incl

X Sec El Cajon Reed to Colonia 13-22  
X Sec Monroe E.P. 5<sup>th</sup> to 18<sup>th</sup> W.P. Central 22-26  
X Sec Stockton El Cajon to Monroe 27-29  
X Sec Conklin El Cajon to Monroe 30-32  
X Sec Central v - v 33-35  
X v 4<sup>th</sup> El Cajon Olive 36-37

Levels from Pacific Univ 19<sup>th</sup> to Boundary 9-8-23  
El Cajon

Ellis

Wells

1

	+	∧	-	
	10.4	371.89		
T.P.			0.30	371.59
	10.54	382.13		
T.P.			2.21	379.92
	5.57	385.49		
B.M.			6.28	379.21
T.P.			5.70	379.79
	2.17	381.96		
T.P.			7.06	374.90
	2.72	377.62		
T.P.			4.08	373.54
	2.08	381.62		
			4.62	377.00

B.M. NW Cor  
Pacific Univ Ave  
361.48

Taken from  
Book No 7284

Not in circuit of levels

B.M. SW Cor Swift Ave. El Cajon Brass Plug

T.P.M.B. SW Cor El Cajon & Boundary SE End of Return



+	+	-					
	385.31	6.45	378.86	SW Cor	Scott + El Cajon	Return in	
		6.45	378.86	SE Cor		Return not in	
					From NE Cor of Prospect + El Cajon 36' of low curb		Swift
		4.80	380.51	NW Cor	Sea view		
		4.50	380.81	NE Cor			
		6.10	379.21	SW Cor	Swift	Return not in	
		5.90	379.41	SE Cor	Swift	Return not in	
		3.45	381.86	NW Cor	Second St.	Return in	
		3.37	381.94	NE Cor			
		4.50	380.81	SW Cor		Return not in	
		4.14	381.17	SE Cor		Return in	
T.P.		3.37	381.94				
40.9	386.03	5.35	380.68	End of curb at <sup>west side</sup> Alley between Second + Wilson on South Side of El Cajon			
		5.75	380.88	SW Cor	Wilson Arc	Return not in	
		6.40	379.63	SE Cor			
		4.80	381.23	NW Cor		Return in	
		5.05	380.98	NE Cor			
		7.42	378.61	NW Cor	Staroy		
		7.89	378.14	NE Cor			

El Cajon  
 curbin  
 Sea view  
 Second St  
 Curbin  
 Wilson  
 Curbin  
 Staroy  
 curbin  
 Cherokee

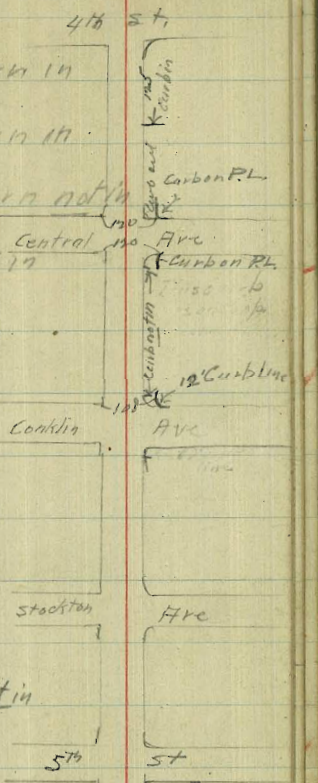


Levels on El Cajon-Boundary to Euclid

9-9-23  
Ellis  
Walker  
Prosser

5

	+	T	-				
		376.36	9.50	366.86	NW cor	Daley + El Cajon	Return in
			9.70	366.66	NE Cor	Daley + El Cajon	Return in
			8.60	367.76	S.W. Cor	✓ ✓	Return not in
			9.95	367.41	SE Cor	✓ ✓	Return not in
T.P.			9.70	366.66			
	5.04	371.70	5.35	366.35	N.W. Cor	4th + El Cajon	Return in
			5.05	366.65	NE Cor	✓ ✓	Return not in
			5.63	366.07	S.W. Cor	✓ ✓	Return not in
			5.98	365.72	SE Cor	✓ ✓	Return not in
			5.80	365.90	End of curb 4th East 125'	North side of El Cajon	
			7.06	364.64	S.W. Cor	Central Mass + El Cajon	Return in
T.P.			7.15	364.55	SE Cor	✓ ✓ ✓	Return not in
	5.64	370.19	4.90	365.29	N.W. Cor	✓ ✓ ✓	Return in but on Prop.
			5.10	365.09	NE Cor	✓ ✓ ✓	Return not in
			5.55	364.64	N.W. Cor	Conklin + El Cajon	Return in
			5.82	364.37	NE Cor	✓ ✓	Return not in
			5.65	364.54	S.W. Cor	✓ ✓	Return not in
			5.65	364.54	SE Cor	✓ ✓	Return not in
			4.52	365.67	N.W. Cor	Stockton + El Cajon	Return not in
			4.80	365.39	NE Cor	✓ ✓ ✓	Return not in





Levels on ElCajon Boundary to Euclid

9-9-23  
Ellis  
Walker  
Preston

6

	+	+	-						
		370.19	5.05	365.14	SW Cor	Stockton + ElCajon	Return	in	
			5.30	364.89	SE Cor				
T.P.			5.31	364.88					5th St
	5.16	370.04	5.61	364.43	N.W. Cor	5th Ave + ElCajon	Return	not in	
			6.00	364.04	N.E. Cor				
			6.50	363.54	N.W. Cor	Copeland			Copeland Ave
			6.80	363.74	N.E. Cor				
			7.00	363.04	S.W. Cor				
			7.00	363.04	S.E. Cor				VanDyke Ave
T.P.			7.04	363.00					
	5.34	368.34	4.75	363.59	SW Cor	VanDyke + ElCajon	Return	in	
			5.30	363.04	SE Cor				Pauly Ave
			3.80	364.54	N.W. Cor				
			No curb		N.E. Cor				
			10.80	357.54	N.W. Cor	Pauly			Fairmount Ave
			12.15	356.19	N.E. Cor				
			10.55	357.79	S.W. Cor				
T.P.			11.10	357.24	SE Cor				





9

X Sec E/Cajon Ave Boundary to Nahash

10-18-23

Sta + - Elev. 377.00

Grades SPL 1/4 1/4 1/4 N.P.L. 10 Grades

0+00 4.5 381.45

TP.B.M. S.W. Cor. E/Cajon + Boundary  
4.0 4.3 3.8

0+50

4.4 4.1 4.0 4.3 3.8  
377.05 377.35 377.45 377.15 76.95 77.3 377.65 ✓  
376.4 ✓

1+00

5.3 5.0 4.3 4.5 4.0 3.9  
76.1 76.4 77.15 76.9 76.5 77.1 77.5 ✓  
376. ✓

W.P.L. 345 ft N  
1+50

5.5 5.5 4.9 5.1 5.4 4.6 4.4  
375.95 375.95 376.5 76.4 76. 76.8 377.0 ✓  
375.2 ✓

E.P.L. 345 ft N  
1+50

5.9 6.2 5.4 5.6 6.0 5.2 5.1  
375.55 375.2 376. 76.8 375.4 76.3 ✓  
374.7 ✓

0+50

6.4 6.3 6.9 6.6 6.7 6.0 5.6  
75. 75.1 375.4 74.8 74.7 75.4 75.8 ✓  
374.3

1+00

7.0 6.9 6.6 6.9 7.2 6.4 6.4  
374.4 74.5 74.8 74.5 74.2 75. 75. ✓  
373.8

1+50

7.2 7.4 7.2 7.7 7.5 6.9 7.1  
374.2 74. 74.2 73.7 73.9 74.5 74.3 ✓  
373.4

2+00

8.3 8.0 7.7 7.9 8.2 7.5 7.3  
373.1 73.4 73.7 73.5 73.2 73.9 374.1 ✓  
372.9

307 ft N  
2+40

8.8 8.4 8.1 8.4 8.0 7.5  
372.65 373.05 373.05 73. 72.8 73.4 373.65 ✓  
372.5

373.5

XSec E/Cajon, Boundary to Nabash

All Dist. From E

10-1823

11

Stg  
3706.88  
EPL  
0730055N

+

K - Eley  
381.45

SPL	4	E	1/2 at Camb	A.P.L
371.15	104	98	93 96 89	83
			7185	
	71.05	71.95	72.15	72.55 373.15

372.7

T.P. 9.30 372.15

7.32 379.47

0+50 855.35

9.4	9.2	7.8	27 71.2	6.7
370.07	70.2	71.7	71.8 71.4	372.77
371.5				372.3

.566: Break in grade west of Boundary -

371.4 ✓

1400 - 4' East of break.

368.37	69.1	71.5	27 86 77	7.3
			71.8	
			71.8 70.9	372.12

371.5 ✓

1450

9.5	208 126	7.0	76 82 74	7.0
369.97	70.2 70.4	71.8	71.9 71.3	72.2
				372.5

371.8 ✓

2+00

8.0	8.1	7.1	7.5 78 69	6.6
371.47	71.4	72.4	71.7 72.4	372.87 ✓

372.1 ✓

2+50

7.2	6.8	6.8	7.1 73 65	6.3
372.3	72.7	72.7	72.4 72.2 73.	373.17 ✓

372.5 ✓

3+00

7.0	6.8	6.5	6.7 6.9 6.1	6.1
372.47	72.7	73.	72.8 72.6	73.4 ✓

372.8 ✓

3+50

6.7	6.7	6.1	6.4 6.5 5.7	5.7
372.8	72.8	73.4	73.07 72.97	73.8 374.07

373.7 ✓

373.3 ✓

10-18-23

12

XSec ElCajon Boundary to Wabash

Sta	+	-	Elev	SPL	W	E	4' cut	umb	N.P.L.	
4+00		329.47		372.97	73.3	73.8	73.6	73.4	5.1	374.37 ✓
				373.5						373.6 ✓
4+96	W.P.L.	1st N	Sissions South	373.47	73.6	74.4	74.5	74.7	4.3	375.17 ✓
				374.7						374.2
				374.7						374.7
5+76				373.6	74.1	75.1	75.1	74.5	3.6	375.87 ✓
0+00	E.P.L.	1st N	Sissions South	374.5						375.2 ✓
				374.5						375.2 ✓
				373.9	74.1	75.1	75.2	75.5	3.9	375.57 ✓
0+50				374.7						375.40
				374.17	74.3	75.3	75.3	75.7	3.7	375.77 ✓
				374.9						375.6 ✓
				374.57	74.2	75.57	75.6	76.1	3.2	376.27 ✓
				375.1						375.8 ✓
				375.77	74.77	75.87	75.77	76.3	2.7	376.77 ✓
				375.3						376.1 ✓
2+65	W.P.L.	Prospect on N	Wabash South	375.57	75.17	76.47	76.4	76.8	2.5	376.97 ✓
				375.6						376.4 ✓
T.P.	N.W. Co. ElCajon		Wabash	2.67		376.80				

X Sec E/Capm Reed to Colonial

Ellis  
Walker  
P. 6. 2. 1  
1/4 Ant. Cont. NPL

10-19-23

13

Sta	+	x	-	Elev	SPL	4	£		NPL		
				372 <sup>23</sup>							
					N.E.C Reed						
0+50	2.51	374.80			$\frac{3.8}{371.8}$	$\frac{3.7}{371.1}$	$\frac{2.8}{372.0}$	$\frac{3.2}{371.1}$	$\frac{4.0}{372.8}$	$\frac{3.2}{371.6}$	$\frac{3.8}{371.3}$ ✓
					372.2	373					372.7 ✓
1+00					$\frac{3.2}{371.6}$	$\frac{4.2}{370.6}$	$\frac{3.1}{371.7}$	$\frac{4.3}{370.5}$	$\frac{4.9}{369.9}$	$\frac{4.0}{370.8}$	$\frac{3.4}{371.4}$ ✓
					372.1						371.3 ✓
01+36 <sup>16</sup>	W.P.L	Thomas South			$\frac{3.4}{371.4}$	$\frac{3.7}{371.1}$	$\frac{3.3}{371.8}$	$\frac{4.4}{372.4}$	$\frac{5.1}{369.7}$	$\frac{4.2}{370.6}$	$\frac{4.1}{370.7}$ ✓
					372.2						370.9 ✓
1+36 <sup>16</sup>	E.P.L	Thomas South			$\frac{3.7}{371.1}$	$\frac{4.4}{370.4}$	$\frac{3.8}{371.0}$	$\frac{5.1}{369.8}$	$\frac{5.6}{367.3}$	$\frac{4.7}{370.1}$	$\frac{4.4}{370.4}$ ✓
					371.8 ✓						370.4 ✓
0+50					$\frac{4.3}{370.5}$	$\frac{5.2}{369.6}$	$\frac{4.3}{370.5}$	$\frac{5.6}{367.2}$	$\frac{6.0}{368.8}$	$\frac{5.4}{369.4}$	$\frac{4.6}{370.2}$ ✓
					371.3						369.7 ✓
0+84 <sup>84</sup>	W.P.L	Thomas North			$\frac{4.6}{370.2}$	$\frac{5.4}{369.4}$	$\frac{4.6}{370.2}$	$\frac{5.7}{369.1}$	$\frac{6.8}{368.0}$	$\frac{5.8}{369.0}$	$\frac{5.4}{369.4}$ ✓
					371						369.4 ✓
1+44 <sup>24</sup>	E.P.L	Thomas North			$\frac{4.1}{370.7}$	$\frac{5.6}{369.2}$	$\frac{5.1}{369.7}$	$\frac{6.3}{368.5}$	$\frac{7.2}{367.8}$	$\frac{6.2}{368.6}$	$\frac{6.0}{368.8}$ ✓
					370.5						369 ✓
1+44 <sup>84</sup>					$\frac{5.4}{369.4}$	$\frac{6.0}{368.8}$	$\frac{5.3}{369.5}$	$\frac{7.0}{367.9}$	$\frac{7.6}{367.2}$	$\frac{6.7}{368.7}$	$\frac{6.2}{368.6}$ ✓
					370						368.5 ✓
1+00					$\frac{4.4}{370.4}$	$\frac{6.4}{368.4}$	$\frac{5.8}{369.0}$	$\frac{7.3}{367.2}$	$\frac{7.8}{366.9}$	$\frac{7.2}{367.6}$	$\frac{6.6}{368.2}$ ✓
					369.6						368.0 ✓



XSec E/Cojon Reed St Colonial

Ellis Walker Preston 10-19-23

Sta	+	T	-	Elev	8 PL	4	4	Dip	W.P.L	N.P.L	14
1+50		374.90			6.7 368.7	6.3 368.5	6.3 368.5	7.8 367.0	8.4 7.7 366.4 367.1	6.9 367.9	✓ 367.6
2+00					5.0 369.8	5.5 369.3	6.7 368.1	8.0 8.8 8.1 366.8 366.0 366.7	7.7 367.1		✓
2+50	W.P.L. Daley North				7.2 367.6	8.3 366.5	7.3 367.5	8.2 9.4 8.6 366.2 365.4 366.2	8.3 366.2		✓ 367.1
T.P.		3.7 3		367.07	368.3						✓ 366.7
2+87	W.P.L. Rexmore Drive South	4.00		371.07	4.0 367.1	4.4 366.7	3.8 367.8	4.4 366.7	5.1 366.5		✓
3+10	E.P.L. Daley North				4.8 366.6	4.4 366.7	4.0 367.1	5.1 5.9 5.0 366.0 365.2 366.1	5.0 366.1		✓ 366.6
3+27	E.P.L. Rexmore South				4.4 366.7	4.8 366.3	4.0 367.1	5.2 5.6 5.1 365.9 365.5 366.0	4.6 366.5		✓ 366.5
0+50					4.1 367.0	4.8 366.3	4.2 366.9	5.3 5.8 5.3 365.8 365.3 365.8	5.0 366.1		✓ 366.4
1+60					4.7 366.4	5.1 366.0	4.3 366.8	5.4 6.0 5.4 365.7 365.1 365.9	5.0 366.1		✓ 366.3
1+50					5.2 365.9	5.3 365.8	4.3 366.8	5.3 6.0 5.2 365.8 365.1 365.8	5.1 366.0		✓ 366.3
					366.4						✓ 366.7

Sta	+	-	Elev	SPL	1/4	€	111.5 Haiter Reston Dibol 1/4 Cal Comb	10-4-23	15
2700			371.09	$\frac{5.0}{366.1}$	$\frac{4.8}{366.3}$	$\frac{4.4}{366.7}$	$\frac{5.3}{365.6}$ $\frac{6.0}{365.7}$ $\frac{5.9}{365.8}$	NPL $\frac{4.8}{366.3}$	✓
2748	WPL	4th St	South	$\frac{5.1}{366.0}$	$\frac{5.2}{365.9}$	$\frac{4.4}{366.7}$	$\frac{5.1}{366.0}$ $\frac{6.1}{365.0}$ $\frac{5.3}{365.8}$	$\frac{5.0}{366.1}$	✓
3728				$\frac{5.4}{365.7}$	$\frac{5.4}{365.7}$	$\frac{4.7}{366.4}$	$\frac{5.5}{365.6}$ $\frac{6.6}{364.3}$ $\frac{5.0}{366.1}$	$\frac{5.0}{366.1}$	✓
0+00	EPL	4th St		$\frac{6.9}{365.1}$	$\frac{5.8}{365.3}$	$\frac{5.6}{366.1}$	$\frac{5.9}{365.2}$ $\frac{6.4}{364.7}$ $\frac{5.4}{365.7}$	$\frac{5.7}{365.4}$	✓
0+50				$\frac{5.1}{366.0}$	$\frac{4.2}{364.9}$	$\frac{5.3}{365.8}$	$\frac{6.1}{365.0}$ $\frac{6.8}{364.6}$ $\frac{5.8}{365.3}$	$\frac{5.2}{365.6}$	✓
1+00				$\frac{4.0}{365.1}$	$\frac{6.2}{364.9}$	$\frac{5.3}{365.8}$	$\frac{5.9}{365.2}$ $\frac{6.7}{364.4}$ $\frac{5.3}{365.3}$	$\frac{5.7}{365.4}$	✓
1+25	West Alley Line	4th + Central	cont. on North Side Ends at this Sta.	$\frac{5.9}{365.2}$	$\frac{6.3}{364.8}$	$\frac{5.4}{365.7}$	$\frac{7.1}{364.0}$	$\frac{6.4}{364.7}$	✓
1+50				$\frac{6.3}{364.6}$	$\frac{6.6}{364.5}$	$\frac{5.7}{365.4}$	$\frac{7.2}{363.9}$	$\frac{6.5}{364.6}$	✓
2+00				$\frac{6.6}{364.8}$	$\frac{6.6}{364.5}$	$\frac{5.8}{365.3}$	$\frac{4.9}{364.2}$	$\frac{6.6}{364.5}$	✓
2+65	WPL	of Central		$\frac{6.6}{364.8}$	$\frac{6.6}{364.5}$	$\frac{5.8}{365.3}$	$\frac{4.9}{364.2}$	$\frac{6.6}{364.5}$	✓

366.1

366.1 ✓

365.9 ✓

366.1 ✓

365.6 ✓

366.5 ✓

365.4

366.2 ✓

365.2

366. ✓

365.1

365.8 ✓

365.

365.7 ✓

364.8

365.5 ✓

364.6 ✓

365.2 ✓

X Sec El Cajon Reed - Colonial

364.55

10-19-23

Ellis  
Walker  
Preston  
D. Del  
N.P.L.

16

Sta + - Elev SPL 1/4 1/4 1/4  
371.07

T.P. 204 364.03 DW Co. Central & El Cajon

3+25  
0+00 E.P.L. of Central  
4.97 369.00  
 $\frac{4.9}{364.1}$   $\frac{4.6}{364.7}$   $\frac{3.9}{365.1}$   $\frac{5.1}{363.9}$   $\frac{4.6}{364.4}$  ✓

0750  
 $\frac{4.8}{364.2}$   $\frac{4.9}{364.1}$   $\frac{4.0}{365.0}$   $\frac{5.2}{363.8}$   $\frac{4.6}{364.4}$  ✓  
364.6 365.1

1700  
 $\frac{5.6}{364.0}$   $\frac{5.0}{364.0}$   $\frac{4.0}{365.0}$   $\frac{5.5}{363.5}$   $\frac{4.6}{364.4}$  ✓  
364.5 365. ✓

1750  
 $\frac{5.0}{364.0}$   $\frac{5.0}{364.0}$   $\frac{3.9}{365.1}$   $\frac{6.5}{363.5}$   $\frac{4.6}{364.4}$  ✓  
364.4 364.9 ✓

2100  
 $\frac{5.2}{363.8}$   $\frac{4.0}{364.3}$   $\frac{4.1}{364.9}$   $\frac{5.9}{365.1}$   $\frac{4.0}{364.3}$  ✓  
364.4 364.9 ✓

2465 W.P.L. Conklin  
 $\frac{5.2}{363.8}$   $\frac{5.1}{363.9}$   $\frac{4.2}{364.8}$   $\frac{5.2}{363.8}$   $\frac{4.8}{364.2}$  ✓  
364.3 364.8 ✓

3+25  
0+00 E.P.L. Conklin South  
 $\frac{5.1}{363.9}$   $\frac{5.0}{364.0}$   $\frac{4.1}{364.9}$   $\frac{5.4}{363.6}$   $\frac{5.1}{363.9}$  ✓  
364.3 364.8 ✓

0750  
 $\frac{4.8}{365.2}$   $\frac{4.8}{365.7}$   $\frac{4.5}{364.5}$   $\frac{6.0}{363.0}$   $\frac{4.7}{364.3}$  ✓  
364.4 364.6 ✓

364.4 364.8 ✓

X Sec El Cajon Reed to Colonial

Ellis Walker  
Boston  
Dip  
N.P.L.

10-19-23

Sta	+	⊖	-	Elev	SPL	1/2	1/4	1/4	1/4	1/4
1400		369.00			$\frac{5.5}{363.5}$ 364.6	$\frac{4.9}{364.1}$	$\frac{4.3}{364.7}$	$\frac{5.7}{363.3}$	$\frac{5.2}{363.8}$	✓
1750					$\frac{5.3}{363.7}$ 364.7	$\frac{4.6}{364.4}$	$\frac{4.2}{364.8}$	$\frac{5.7}{363.3}$	$\frac{4.7}{364.3}$	✓
2100					$\frac{3.7}{365.3}$ 364.9	$\frac{5.2}{363.8}$	$\frac{4.1}{364.9}$	$\frac{4.8}{364.2}$	$\frac{4.4}{364.6}$	✓
2465	XV.P.L. Stockton				$\frac{4.3}{364.7}$ 365.1	$\frac{4.6}{364.4}$	$\frac{4.0}{365.0}$	$\frac{4.8}{364.2}$	$\frac{3.9}{365.1}$	✓
T.P.			4.47	364.53	SW Cor. Stockton + El Cajon.					
3725	404	368.57			$\frac{4.4}{364.2}$ 364.9	$\frac{4.6}{364.0}$	$\frac{3.5}{365.7}$	$\frac{4.6}{364.0}$	$\frac{4.2}{364.4}$	✓
6100	EL.P.L. Stockton				$\frac{4.8}{363.8}$ 364.8	$\frac{4.2}{364.4}$	$\frac{3.6}{365.0}$	$\frac{3.4}{365.2}$	$\frac{4.0}{364.6}$	✓
0750					$\frac{4.6}{364.0}$ 364.8	$\frac{4.9}{363.7}$	$\frac{3.8}{364.8}$	$\frac{5.3}{363.3}$	$\frac{4.5}{364.1}$	✓
7700					$\frac{5.1}{363.5}$ 364.5	$\frac{5.2}{363.4}$	$\frac{3.8}{364.8}$	$\frac{5.8}{363.1}$	$\frac{4.7}{363.9}$	✓
1450										364.8

17

364.9

365.7

365.3

365.6

365.4

365.2

365.

364.8

X Sec El Cajon Reed to Colonial

Ellis  
W.H.H.  
P. 2300  
Dibol  
NPL

10-19-23

Time	Notes	π	-	Elev	SPL	4	C	4	4.7	18
5+9					52	43	39	48	47	
2100		368.57			363.4	364.3	364.7	363.7	363.9	✓
					364.3					364.6 ✓
2+65	W.P.L. 5 <sup>th</sup> ST.				54	49	41	54	46	✓
					363.2	363.7	364.5	363.2	364.0	✓
					364.7 ✓					364.4 ✓
3+45					51	50	40	49	48	✓
0700	E.P.L. of 5 <sup>th</sup>				363.5	363.6	364.6	363.7	363.8	✓
					363.9 ✓					364.0 ✓
0750					45	48	39	53	48	✓
					364.1	363.8	364.7	363.3	363.8	✓
					363.7					363.9 ✓
1700					48	48	40	55	39	✓
					363.8	363.8	364.0	363.1	364.7	✓
					363.5					363.8 ✓
1750					48	45	40	61	47	✓
					363.8	364.1	364.0	362.5	363.9	✓
					363.4					363.7 ✓
2700					48	48	40	49	39	✓
					364.2	363.8	364.0	363.7	364.7	✓
					363.7					363.4 ✓
2765	W.P.L. Copeland				55	50	40	58	51	✓
					363.1	363.6	364.0	362.8	363.5	✓
					363 ✓					363.5 ✓

T.P. 6.19 362.38 SW cor Copeland & El Cajon  
7.13 369.57

Sta	X Sec El Cajon Road to Colonial	Elev	SPL.	1/4	E	1/2	N.P.L	19	
3+20 0700	E.P.L Copeland	36957	$\frac{67}{3628}$	$\frac{5.5}{364.0}$	$\frac{5.0}{364.3}$	$\frac{+180}{5.1}$ $\frac{+260}{7.9}$ $\frac{+320}{9.3}$ $\frac{+380}{5.8}$ $\frac{+440}{6.2}$	$\frac{364.4}{361.6}$ $\frac{365.2}{363.7}$ $\frac{365.8}{363.3}$	✓	
0750			363.0 ✓	$\frac{5.2}{369.3}$	$\frac{5.9}{369.6}$	$\frac{5.1}{369.4}$	$\frac{+180}{5.1}$ $\frac{+260}{8.0}$ $\frac{+320}{9.2}$ $\frac{+380}{5.2}$ $\frac{+440}{5.7}$	$\frac{364.1}{361.5}$ $\frac{365.1}{363.3}$ $\frac{365.7}{363.6}$	363.7 ✓
1400			363.0	$\frac{5.6}{363.9}$	$\frac{6.1}{363.4}$	$\frac{5.1}{364.4}$	$\frac{+180}{5.7}$ $\frac{+260}{8.0}$ $\frac{+320}{8.5}$ $\frac{+380}{6.6}$	$\frac{363.8}{361.5}$ $\frac{364.0}{362.9}$	363.8 ✓
1450			363.1	$\frac{5.1}{364.4}$	$\frac{4.1}{363.4}$	$\frac{5.0}{364.5}$	$\frac{+180}{5.0}$ $\frac{+260}{7.8}$ $\frac{+320}{8.3}$ $\frac{+380}{4.8}$	$\frac{364.5}{361.7}$ $\frac{365.2}{363.7}$	364.0 ✓
2100			363.2	$\frac{4.7}{364.8}$	$\frac{5.2}{364.3}$	$\frac{5.0}{364.5}$	$\frac{+180}{5.1}$ $\frac{+260}{7.8}$ $\frac{+320}{8.3}$ $\frac{+380}{5.2}$	$\frac{364.4}{361.7}$ $\frac{365.3}{364.3}$ $\frac{365.8}{364.3}$	364.2 ✓
2165	W.P.L. Van Dyke		363.3	$\frac{5.8}{363.7}$	$\frac{5.1}{364.4}$	$\frac{4.7}{364.8}$	$\frac{+180}{4.8}$ $\frac{+260}{7.7}$ $\frac{+320}{8.0}$ $\frac{+380}{5.0}$	$\frac{364.0}{361.8}$ $\frac{364.5}{364.5}$	364.4 ✓
3+25 0700	E.P.L. Van Dyke		363.4 ✓	$\frac{5.5}{364.0}$	$\frac{5.2}{364.3}$	$\frac{4.7}{364.8}$	$\frac{+180}{5.1}$ $\frac{+260}{7.8}$ $\frac{+320}{8.0}$ $\frac{+380}{5.0}$	$\frac{364.5}{361.7}$ $\frac{364.5}{364.5}$	364.6 ✓
0750			362.9 ✓	$\frac{5.3}{364.2}$	$\frac{5.3}{364.2}$	$\frac{5.1}{364.4}$	$\frac{+180}{4.9}$ $\frac{+260}{8.1}$ $\frac{+320}{8.4}$ $\frac{+380}{5.5}$	$\frac{364.6}{361.4}$ $\frac{364.6}{364.6}$	364.1 ✓
0782.5 = B mark, 1400			363.3	$\frac{5.8}{363.7}$	$\frac{5.4}{363.1}$	$\frac{6.2}{363.3}$	$\frac{+180}{4.9}$ $\frac{+260}{8.0}$ $\frac{+320}{8.4}$ $\frac{+380}{6.4}$	$\frac{363.5}{361.5}$ $\frac{364.1}{364.1}$	363.5 ✓
1+32.5 fall			363.2					363.0	
			362.9					362.6	

XSec ElCajon Reed to Colonial

Ellis  
Willow  
Pine from Dibel  
N.P.L. 70  
76  
3619

Sta	+	π	-	Elev	S.P.L	6	4	4	4	Ellis Willow Pine from Dibel N.P.L.	10-20-23
1450		349.51			4.6 362.9	6.0 363.8	7.6 361.9	7.4 362.1	7.4 362.1	76 3619	✓ 361.9
1+825 - Break.		South			1+50 1+825						
2+00					7.8 361.7	7.3 359.2	9.4 359.1	8.8 360.7	8.8 360.7	8.9 360.6	✓ 360
2+65		N.P.L. Parly			360.8 11.4 359.1	11.1 358.4	11.5 358.0	11.2 358.3	11.5 358.0	11.5 358.0	✓ 357.5
T.P.				11.92	357.99						
3+25		30.76		358.55							
0+00		E.P.L. Parly			1.7 356.8	2.7 355.8	2.4 356.1	3.1 356.4	2.7 355.8	2.7 355.8	✓ 356.1
0+50					3.6 354.9	3.0 356.2	4.2 354.3	6.0 352.5	5.7 352.8	5.7 352.8	✓ 354.5
1+00					4.6 352.5	5.6 352.9	5.4 353.1	6.9 351.6	7.8 350.7	7.8 350.7	✓ 353
1+32.5 = ally 4.					ally 352.4						ally - 352
1+50					6.8 351.7	5.7 352.8	6.0 352.5	7.2 351.3	7.9 350.6	7.9 350.6	✓ 351.8
2+00					7.2 351.3	6.4 352.1	6.3 352.2	7.1 351.4	7.5 351.0	7.5 351.0	✓ 351.5

X Sec El Cajon to Colonial

Sta + K - Elev  
 2765 W.P.L. Fairmount 35855

T.P. 6.50 352.05

3725 6.35 358.40  
 0400 E.P.L. Fairmount

0450

1400

1427 W.P.L. Orange wood North

1487 E.P.L. Orange wood North

2700

2750

SPL 1/2  
 $\frac{6.2}{352.3}$   $\frac{6.4}{352.1}$   $\frac{6.3}{352.2}$   
 351.9

80'  
 $\frac{5.6}{352.8}$   $\frac{4.6}{351.8}$   $\frac{4.4}{352.0}$   $\frac{6.5}{351.9}$   $\frac{7.1}{351.3}$   
 351.9

$\frac{5.6}{352.8}$   $\frac{4.0}{352.4}$   $\frac{4.5}{351.9}$   $\frac{6.6}{351.8}$   $\frac{4.7}{351.7}$   
 352.4

$\frac{5.3}{352.1}$   $\frac{5.5}{352.9}$   $\frac{4.2}{352.2}$   $\frac{4.2}{352.2}$   $\frac{4.2}{352.2}$   
 352.9

$\frac{5.1}{353.3}$   $\frac{5.0}{353.4}$   $\frac{5.6}{352.8}$   $\frac{5.8}{352.6}$   $\frac{5.9}{352.5}$   
 353.7

$\frac{4.6}{353.8}$   $\frac{4.5}{353.9}$   $\frac{5.1}{353.3}$   $\frac{5.3}{353.1}$   $\frac{4.8}{353.6}$   
 353.8

$\frac{4.4}{354.0}$   $\frac{4.3}{354.1}$   $\frac{5.2}{353.2}$   $\frac{5.1}{353.3}$   $\frac{4.6}{353.8}$   
 353.9

$\frac{3.9}{354.5}$   $\frac{3.5}{354.9}$   $\frac{4.2}{354.2}$   $\frac{4.4}{354.0}$   $\frac{4.1}{354.3}$   
 354.4

Ellis 10-20-23  
 Walk 4  
 10 est. Dibel 2)  
 N.P.L.

$\frac{7.3}{351.2}$   $\frac{7.4}{351.1}$

351.1

3

351.2

✓

351.7

352.2

✓

352.5

✓

353.2

✓

353.3

✓

353.8



X Sec ElCajon Reed to Colonial

Ellis  
Walker  
Princeton  
Bibel  
N.P.L. 10-20-23

Sta	+	-	Elev
2170	Colonial South	35840	
T.P.		3.61	354.79

SPL	1/4	1/2	3/4	1	2
39	3.4	10	4.1	3.8	22
3545	355.0	354.4	354.3	354.6	
354.7		80			354.0

D.N. Colonial & ElCajon



X See Monroe EPL 54st 1078' W of Center

Ellis 10-21-23

William Proctor  
Dated 24

Sta	+	-	Elev	S.P.L.	Cumlat	E	1/2 Cumlat	N.P.L.
3100			37365	$\frac{4.8}{368.9}$	$\frac{5.1}{368.6}$	$\frac{4.7}{368.8}$	$\frac{5.1}{368.6}$ $\frac{5.2}{368.5}$ $\frac{4.7}{369.0}$	$\frac{4.5}{369.7}$
				368.7				369.
3+45	E.P.L.		Stockton South	$\frac{4.6}{369.1}$	$\frac{5.1}{368.6}$	$\frac{4.6}{369.1}$	$\frac{5.0}{368.7}$ $\frac{5.2}{368.5}$ $\frac{4.3}{369.3}$	$\frac{4.1}{369.6}$
				368.9				369.7
0+00	W.P.L.		Stockton South	$\frac{4.6}{369.1}$	$\frac{4.8}{368.9}$	$\frac{4.2}{369.5}$	$\frac{4.6}{369.1}$ $\frac{4.8}{368.9}$ $\frac{4.0}{369.7}$	$\frac{3.8}{369.9}$
				369.0				369.5
0+28	E.P.L.		Marlborough North	$\frac{4.4}{369.3}$	$\frac{4.6}{369.1}$	$\frac{4.1}{369.6}$	$\frac{4.6}{369.1}$ $\frac{4.3}{369.2}$ $\frac{3.8}{369.7}$	$\frac{3.6}{370.1}$
				369.0				369.7
0+50				$\frac{4.3}{369.4}$	$\frac{4.4}{369.3}$	$\frac{4.0}{369.7}$	$\frac{4.0}{369.7}$	$\frac{4.0}{369.7}$
				369				369.7
0+88	W.P.L.		Marlborough North	$\frac{4.4}{369.3}$	$\frac{4.4}{369.3}$	$\frac{4.1}{369.6}$	$\frac{4.4}{369.1}$ $\frac{4.4}{369.7}$ $\frac{3.9}{370.0}$	$\frac{3.9}{369.8}$
				369.				369.7
1+00				$\frac{4.2}{369.5}$	$\frac{4.3}{369.4}$	$\frac{4.2}{369.5}$	$\frac{4.6}{369.1}$ $\frac{4.6}{369.1}$ $\frac{3.7}{370.0}$	$\frac{4.1}{369.6}$
				369.1				369.7
1+50				$\frac{3.8}{370.2}$	$\frac{4.1}{369.6}$	$\frac{3.8}{369.9}$	$\frac{4.0}{369.7}$ $\frac{4.3}{369.7}$ $\frac{3.8}{370.2}$	$\frac{3.7}{370.0}$
				369.1				369.8
2+00				$\frac{3.8}{369.9}$	$\frac{4.1}{369.6}$	$\frac{3.6}{370.1}$	$\frac{3.9}{369.8}$ $\frac{4.1}{369.6}$ $\frac{3.7}{370.2}$	$\frac{3.2}{370.0}$
				369.7				369.9

X Sec Monroe from EPL 50<sup>th</sup> St. to 78<sup>th</sup> W of W.P.L.  
 3<sup>rd</sup> Central

Ellis  
Walker  
Ruston  
D. B. W.

10-21-23

Sta	+	T	-	FK	SPL	Cut Cut: 1/4	d	1/4 Cut	Rest	N.P.L.	
2+50		37345			38 369.9	41 369.6	37 370.0	40 369.7	43 369.7	34 370.3	25
					369.3						370.
2+65	E.P.L.	Cooklin	South		43 369.4	43 369.4	36 370.1	38 369.9	42 369.5	33 370.4	33 370.4
T.P.		456			369.3						370.1
		291									372.00
0+00	W.P.L.	Cooklin	South		29 369.1	25 369.5	20 370.0	22 369.8	23 369.7	16 370.4	12 370.8
					369						370.2
0+20	E.P.L.	Kensington	North		28 369.2	25 369.5	21 369.9	21 369.9	22 369.8	16 370.4	12 370.8
					369.						370.3
0+50					36 368.4	28 369.2	22 369.8	20 370.0	20 370.0	20 370.0	
					369.						369.9
0+80	W.P.L.	Kensington	North		40 368.0	28 369.2	24 369.6	24 369.6	22 369.8	22 369.8	20 370.0
					369.1						369.6
1+00					42 367.8	28 369.2	23 369.9	26 369.4	28 369.2	22 369.8	28 369.2
					369.1						369.6
1+50					39 368.1	28 369.2	27 369.3	22 369.3	33 368.7	23 368.7	28 369.2
					369.2						369.6
2+00					43 367.7	31 368.7	24 369.6	26 369.4	30 369.0	24 369.8	32 368.8
					369.3						369.7

X Sec Monroe farm's <sup>50-15</sup> to 78' West of N.P.L. of Central

5113  
N.P.L.  
17-2-1923

10-21-23

Sta	+	-	Elev	SPL	Corr. Cont. $\frac{1}{2}$	$\frac{1}{2}$	Cont. Cont.	N.P.L.	26
2+50			372.00	$\frac{45}{367.5}$	$\frac{30}{369.0}$	$\frac{2.4}{369.6}$	$\frac{2.3 \ 2.8 \ 2.1}{369.2 \ 369.9}$	$\frac{3.0}{369.0}$	
				369.4					369.7
2+65	E.P.L. Central		South	$\frac{4.4}{367.6}$	$\frac{9.3}{368.7}$	$\frac{2.7}{369.6}$	$\frac{2.4 \ 2.7 \ 2.1}{369.3 \ 369.9}$	$\frac{2.6}{369.4}$	
				369.4					369.7
0+00	N.P.L. Central		South	$\frac{4.7}{367.3}$	$\frac{8.2}{368.8}$	$\frac{2.6}{369.4}$	$\frac{2.3 \ 2.5 \ 2.1}{369.3 \ 369.9}$	$\frac{2.3}{369.7}$	
				369.6					369.7
0+08	E.P.L. Terrace		North	$\frac{4.5}{367.5}$	$\frac{3.0}{369.0}$	$\frac{2.3}{369.7}$	$\frac{2.5 \ 2.5 \ 2.1}{369.5 \ 369.9}$	$\frac{1.8}{370.2}$	
				369.6			$\frac{2.0}{370.0}$		369.7
0+50				$\frac{4.3}{367.7}$	$\frac{3.2}{368.8}$	$\frac{2.3}{369.7}$	$\frac{2.0}{370.0}$	$\frac{2.3}{369.7}$	
				369.9					369.7
0+78				$\frac{3.8}{368.2}$	$\frac{3.2}{368.9}$	$\frac{2.3}{369.7}$	$\frac{2.2}{369.8}$	$\frac{2.8}{369.2}$	
				370					369.7

X Sec Stockton from El Cajon to Barro

File  
Vol 1  
Section 2  
1021-23  
29

Sta + π — Elev  
366.05

W.P.L. Sub. cont. & E. 4' cont. cont. E.P.L.  
NW Cor. Stockton, Olive

4.93 37.988  
0+00 N.P.L. El Cajon 6.05

$\frac{5.3}{365.7}$   $\frac{54.58}{365.6}$   $\frac{57}{365.3}$   $\frac{56}{365.4}$   $\frac{58}{365.4}$   $\frac{61.54}{365.4}$   $\frac{61}{364.9}$

0+50

$\frac{5.2}{365.8}$   $\frac{53.61}{365.7}$   $\frac{58}{365.2}$   $\frac{5.6}{365.4}$   $\frac{60.63}{365.0}$   $\frac{57}{364.7}$   $\frac{5.5}{365.5}$

1+00

$\frac{5.4}{365.6}$   $\frac{54}{365.6}$   $\frac{60}{365.0}$   $\frac{57}{365.3}$   $\frac{5.3}{365.7}$   $\frac{59}{365.1}$   $\frac{6.2}{364.8}$   $\frac{5.6}{365.4}$   $\frac{5.3}{365.3}$

1+50

$\frac{5.1}{365.9}$   $\frac{54}{365.6}$   $\frac{59}{365.1}$   $\frac{56}{365.4}$   $\frac{5.1}{365.9}$   $\frac{59}{365.1}$   $\frac{6.3}{364.9}$   $\frac{5.2}{365.5}$   $\frac{5.2}{365.8}$

2+00

$\frac{5.4}{365.6}$   $\frac{5.3}{365.7}$   $\frac{40}{365.0}$   $\frac{50}{365.4}$   $\frac{5.1}{365.9}$   $\frac{5.7}{365.3}$   $\frac{6.0}{365.0}$   $\frac{5.5}{365.3}$   $\frac{5.3}{365.7}$

2+50

$\frac{5.2}{365.8}$   $\frac{5.2}{365.8}$   $\frac{5.7}{365.3}$   $\frac{5.9}{365.6}$   $\frac{5.1}{365.9}$   $\frac{5.8}{365.2}$   $\frac{6.0}{365.0}$   $\frac{5.9}{365.7}$   $\frac{5.2}{365.8}$

3+00

$\frac{5.3}{365.7}$   $\frac{5.2}{365.8}$   $\frac{5.8}{365.2}$   $\frac{5.4}{365.4}$   $\frac{5.1}{365.9}$   $\frac{5.6}{365.4}$   $\frac{6.0}{365.0}$   $\frac{5.2}{365.8}$   $\frac{5.3}{365.7}$

3+50

$\frac{5.0}{366.0}$   $\frac{5.1}{365.9}$   $\frac{5.2}{365.3}$   $\frac{5.4}{365.4}$   $\frac{5.1}{365.9}$   $\frac{5.7}{365.3}$   $\frac{5.9}{365.1}$   $\frac{5.2}{365.8}$   $\frac{5.4}{365.6}$

X Sec Stockton El Cajon to Monroev

Ellis  
Walker  
Preston  
Dibel  
R.P.L.

10-21-23

28

Sta + X - Elev  
4400 37098

W.P.L	Comb	Grat	1/2	¢	1/4	Comb	R.P.L.
47	49	55	53	49	53	51	57
366.3	366.1	365.8	365.7	366.1	365.8	365.8	365.3

4450

49	49	52	57	49	56	58	51	5.0
366.1	366.1	365.8	365.7	366.1	365.9	365.2	365.9	366.0

5400

47	49	55	53	49	57	57	51	5.1
366.3	366.1	365.8	365.7	366.1	365.6	365.8	365.9	365.9

5450

46	47	54	52	47	53	56	5.0	5.2
366.4	366.2	365.6	365.8	366.3	365.7	365.4	366.0	365.8

64? SPL Olive

46	48	54	52	50	53	56	5.0	5.3
366.4	366.2	365.6	365.8	366.0	365.7	365.4	366.0	365.7

T.P. 493 36605

529 37134

0400 NPL Olive

51	53	56	56	55	58	58	53	5.3
366.2	366.0	365.7	365.7	365.8	365.5	365.6	366.0	366.0

0450

49	51	58	56	53	57	57	51	5.5
366.4	366.2	365.5	365.7	366.0	366.0	365.4	366.2	365.8

1700

54	49	56	54	51	53	56	4.8	7.3
365.9	366.4	365.7	365.9	366.2	366.0	365.7	366.5	367.0

1750

54	46	53	54	49	51	57	4.2	4.5
365.9	366.1	366.0	366.1	366.4	366.2	365.9	366.8	366.8

XSec Stockton El Cajon & Monroe

Ellis  
Muir  
Preston  
D. J. ...

10-21-23

29

Sta + - Elev  
2+00 371.34

W.P.L. Carb Cut 4 E 1/4 Cat Carb. S.P.L.  
 $\frac{4.4}{366.9}$   $\frac{4.3 \ 5.0 \ 4.8}{367.0 \ 366.7 \ 366.5}$   $\frac{4.6}{366.7}$   $\frac{4.5 \ 4.1 \ 4.2}{366.9 \ 368.2 \ 367.1}$   $\frac{4.2}{367.1}$

2+50

$\frac{3.8}{367.5}$   $\frac{4.1 \ 4.7 \ 4.6}{366.8 \ 366.6 \ 366.7}$   $\frac{4.3}{367.8}$   $\frac{4.7 \ 5.1 \ 4.1}{366.6 \ 366.4 \ 367.2}$   $\frac{4.6}{366.7}$

3+00

$\frac{3.8}{367.5}$   $\frac{3.8 \ 4.6 \ 4.2}{367.5 \ 366.7 \ 367.1}$   $\frac{3.8}{367.5}$   $\frac{4.5 \ 4.6 \ 3.8}{366.8 \ 367.1 \ 367.5}$   $\frac{3.8}{367.5}$

3+50

$\frac{3.8}{367.5}$   $\frac{3.7 \ 4.4 \ 4.0}{367.6 \ 366.9 \ 367.3}$   $\frac{3.9}{367.4}$   $\frac{4.3 \ 4.4 \ 3.7}{367.0 \ 366.9 \ 367.6}$   $\frac{3.5}{367.8}$

4+00

$\frac{2.9}{368.4}$   $\frac{3.2 \ 4.0 \ 3.8}{368.1 \ 367.3 \ 368.0}$   $\frac{3.6}{367.7}$   $\frac{4.0 \ 4.2 \ 3.4}{367.3 \ 366.9 \ 367.9}$   $\frac{3.5}{367.8}$

4+50

$\frac{2.9}{368.4}$   $\frac{3.1 \ 3.6 \ 3.6}{368.2 \ 367.7 \ 367.7}$   $\frac{3.2}{368.1}$   $\frac{3.6 \ 3.9 \ 3.2}{367.7 \ 367.7 \ 368.1}$   $\frac{3.4}{367.9}$

5+00

$\frac{2.4}{368.9}$   $\frac{2.9 \ 3.5 \ 3.4}{4 \ 368.7 \ 368.4}$   $\frac{3.0}{368.3}$   $\frac{3.3 \ 3.5 \ 2.9}{368.0 \ 368.8 \ 368.4}$   $\frac{2.5}{368.8}$

5+50

$\frac{2.5}{368.8}$   $\frac{2.5 \ 3.1 \ 3.0}{368.8 \ 368.2 \ 368.3}$   $\frac{2.6}{368.7}$   $\frac{3.0 \ 3.2 \ 2.6}{368.3 \ 368.1 \ 368.7}$   $\frac{2.6}{368.7}$

5+71, S.P.L. Monroe

$\frac{2.4}{368.9}$   $\frac{2.4 \ 2.6 \ 2.4}{368.9 \ 368.7 \ 368.4}$   $\frac{2.4}{368.9}$   $\frac{3.0 \ 3.0 \ 2.5}{368.3 \ 368.3 \ 368.8}$   $\frac{2.5}{368.8}$



X Sec Conklin El Cajon to Monroe

Sta + x - Elev  
366.05

4.98 37303

0+00 N.P.L. El Cajon

0+50

1+00

1+50

2+00

2+50

3+00

3+50

N.P.L. Cont Cut 1/4 E by Cont. Arb. E.P.L.

N.H.C. Stockton Olive

60'

$\frac{83}{364.7}$   $\frac{85}{364.5}$   $\frac{9.0}{364.0}$   $\frac{86}{364.4}$   $\frac{80}{364.8}$   $\frac{83}{364.8}$   $\frac{86}{364.4}$

$\frac{83}{364.7}$   $\frac{85}{364.5}$   $\frac{9.1}{363.9}$   $\frac{82}{364.3}$   $\frac{80}{365.0}$   $\frac{80}{365.0}$   $\frac{84}{364.6}$

$\frac{8.1}{364.9}$   $\frac{84}{364.6}$   $\frac{9.0}{364.0}$   $\frac{87}{364.3}$   $\frac{81}{364.9}$   $\frac{8.4}{364.6}$   $\frac{86}{364.4}$

$\frac{79}{365.1}$   $\frac{82}{364.8}$   $\frac{8.9}{364.1}$   $\frac{80}{364.6}$   $\frac{74}{365.6}$   $\frac{8.5}{364.7}$   $\frac{8.5}{364.5}$

$\frac{7.8}{365.2}$   $\frac{81}{364.9}$   $\frac{8.9}{364.4}$   $\frac{84}{364.4}$   $\frac{7.8}{363.7}$   $\frac{8.0}{365.0}$   $\frac{7.6}{365.4}$

$\frac{7.7}{365.3}$   $\frac{88}{364.7}$   $\frac{82}{364.8}$   $\frac{7.4}{365.6}$   $\frac{7.3}{365.7}$   $\frac{7.7}{365.3}$   $\frac{8.1}{364.9}$

$\frac{2.6}{365.4}$   $\frac{7.2}{365.3}$   $\frac{8.4}{364.6}$   $\frac{8.2}{364.8}$   $\frac{7.4}{365.6}$   $\frac{7.0}{366.0}$   $\frac{7.4}{365.4}$   $\frac{7.0}{366.0}$   $\frac{7.3}{365.7}$

$\frac{8.1}{365.9}$   $\frac{7.5}{365.8}$   $\frac{8.0}{365.0}$   $\frac{7.8}{365.7}$   $\frac{4.9}{366.1}$   $\frac{7.2}{365.8}$   $\frac{7.2}{365.6}$   $\frac{6.5}{366.2}$   $\frac{4.3}{366.7}$

Ellis  
Walker  
Pres'n  
Bishop  
E.P.L.

10-22-23

30

XSec Cont X/in Elkay to Naurac

Ellis  
Walker  
Preston

10-22-23

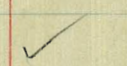
31

Sta	+	-	Elev	W.P.L	Cont Cont. 4	4	4 Cont Cont.	E.P.L
4+00		373.08		$\frac{67}{3663}$	$\frac{73}{3688}$ $\frac{77}{3683}$ $\frac{75}{3653}$	$\frac{66}{3664}$	$\frac{70}{3680}$ $\frac{74}{3656}$ $\frac{64}{3666}$	$\frac{66}{3664}$
4+50				$\frac{65}{3675}$	$\frac{67}{3663}$ $\frac{74}{3666}$ $\frac{70}{3660}$	$\frac{60}{3670}$	$\frac{65}{3665}$ $\frac{67}{3663}$ $\frac{59}{3671}$	$\frac{59}{3671}$
5+00				$\frac{57}{3673}$	$\frac{62}{3668}$ $\frac{69}{3661}$ $\frac{65}{3660}$	$\frac{57}{3673}$	$\frac{61}{3669}$ $\frac{62}{3668}$ $\frac{55}{3675}$	$\frac{55}{3675}$
5+50				$\frac{55}{3675}$	$\frac{56}{3674}$ $\frac{66}{3666}$ $\frac{62}{3668}$	$\frac{54}{3676}$	$\frac{57}{3673}$ $\frac{58}{3672}$ $\frac{57}{3679}$	$\frac{52}{3678}$
6+07	SPL Olive			$\frac{51}{3679}$	$\frac{52}{3678}$ $\frac{59}{3671}$ $\frac{57}{3672}$	$\frac{51}{3677}$	$\frac{54}{3676}$ $\frac{55}{3675}$ $\frac{48}{3682}$	$\frac{47}{3683}$
6+00	N.P.L Olive			$\frac{51}{3677}$	$\frac{53}{3677}$ $\frac{61}{3669}$ $\frac{57}{3673}$	$\frac{53}{3677}$	$\frac{56}{3678}$ $\frac{60}{3670}$ $\frac{51}{3679}$	$\frac{52}{3678}$
6+50				$\frac{53}{3677}$	$\frac{54}{3676}$ $\frac{63}{3667}$ $\frac{62}{3668}$	$\frac{54}{3676}$	$\frac{58}{3679}$ $\frac{61}{3669}$ $\frac{51}{3679}$	$\frac{53}{3675}$
7+00				$\frac{54}{3676}$	$\frac{54}{3676}$ $\frac{69}{3667}$ $\frac{59}{3671}$	$\frac{54}{3676}$	$\frac{57}{3678}$ $\frac{58}{3672}$ $\frac{50}{3680}$	$\frac{48}{3682}$
7+50				$\frac{52}{3676}$	$\frac{54}{3676}$ $\frac{63}{3667}$ $\frac{60}{3679}$	$\frac{53}{3677}$	$\frac{55}{3675}$ $\frac{58}{3671}$ $\frac{51}{3679}$	$\frac{50}{3680}$

X Sec Cont. In E. Cajon to Monroe

Ellis 10-22-23  
Walkway  
P. station D. bed  
EPL 32

Sta	+	π	-	Elev	W.P.L.	Corr. Cont. by	±	48 Cont. Carb.	EPL
2+00		373.03			$\frac{5.4}{367.6}$	$\frac{5.4 \ 6.3 \ 5.9}{367.6 \ 366.7 \ 367.1}$	$\frac{5.1}{367.9}$	$\frac{5.6 \ 6.0 \ 5.0}{367.9 \ 367.9 \ 368.0}$	$\frac{5.1}{367.9}$
2+50					$\frac{6.0}{367.0}$	$\frac{5.3 \ 6.2 \ 5.8}{367.1 \ 366.8 \ 367.2}$	$\frac{5.1}{367.9}$	$\frac{5.6 \ 5.9 \ 5.0}{367.9 \ 367.9 \ 368.0}$	$\frac{5.3}{367.7}$
3+00					$\frac{5.2}{367.6}$	$\frac{5.2 \ 6.1 \ 5.7}{367.8 \ 366.9 \ 367.3}$	$\frac{5.0}{368.0}$	$\frac{5.5 \ 5.7 \ 4.8}{367.8 \ 367.3 \ 368.2}$	$\frac{5.2}{367.8}$
3+50					$\frac{5.3}{367.7}$	$\frac{5.1 \ 6.1 \ 5.8}{367.9 \ 366.9 \ 367.2}$	$\frac{5.1}{367.9}$	$\frac{5.3 \ 5.6 \ 4.6}{367.9 \ 367.4 \ 368.4}$	$\frac{4.9}{368.1}$
4+00					$\frac{4.8}{368.2}$	$\frac{5.0 \ 6.0 \ 5.7}{368.0 \ 367.0 \ 367.3}$	$\frac{5.0}{368.0}$	$\frac{5.1 \ 5.3 \ 4.4}{367.9 \ 367.7 \ 368.6}$	$\frac{4.7}{368.3}$
4+50					$\frac{4.9}{368.1}$	$\frac{4.9 \ 5.8 \ 5.8}{368.1 \ 367.2 \ 367.4}$	$\frac{4.8}{368.2}$	$\frac{4.4 \ 4.4 \ 4.2}{368.1 \ 368.1 \ 368.8}$	$\frac{4.3}{368.7}$
5+00					$\frac{4.7}{368.3}$	$\frac{4.8 \ 5.6 \ 5.4}{368.2 \ 367.4 \ 367.6}$	$\frac{4.6}{368.4}$	$\frac{4.7 \ 5.1 \ 4.0}{368.3 \ 367.9 \ 369.0}$	$\frac{4.2}{368.8}$
5+50					$\frac{4.1}{368.7}$	$\frac{4.2 \ 5.1 \ 4.8}{368.8 \ 367.9 \ 368.2}$	$\frac{4.2}{368.7}$	$\frac{4.3 \ 4.6 \ 3.7}{368.7 \ 368.4 \ 369.3}$	$\frac{4.0}{369.0}$
6+7	S.P.L. Monroe				$\frac{4.1}{368.9}$	$\frac{4.0 \ 4.5 \ 4.6}{369.0 \ 368.5 \ 368.4}$	$\frac{3.6}{369.4}$	$\frac{4.1 \ 4.2 \ 3.6}{368.9 \ 368.8 \ 369.4}$	$\frac{3.7}{369.3}$



X Sec Central El Cajon to Monroe

Sta	+	-	Elev
			366.05
698			373.03
		3.84	369.19
243			371.62

0+00

$\frac{6.4}{365.2}$      $\frac{4.4}{365.2}$      $\frac{7.0}{365.6}$      $\frac{6.6}{365.8}$      $\frac{6.3}{365.3}$      $\frac{6.5}{365.0}$      $\frac{6.4}{365.7}$      $\frac{6.4}{365.2}$      $\frac{6.5}{365.1}$

365.2

365.1

0+50

$\frac{6.6}{365.0}$      $\frac{6.4}{365.2}$      $\frac{7.1}{365.5}$      $\frac{6.3}{365.7}$      $\frac{6.4}{365.2}$      $\frac{6.7}{364.9}$      $\frac{7.1}{365.5}$      $\frac{6.4}{365.2}$      $\frac{6.5}{365.1}$

1+00

$\frac{6.4}{365.2}$      $\frac{6.3}{365.3}$      $\frac{7.0}{364.6}$      $\frac{6.3}{364.7}$      $\frac{6.2}{365.4}$      $\frac{6.4}{365.2}$      $\frac{6.5}{364.7}$      $\frac{6.2}{365.4}$      $\frac{6.4}{365.2}$

1+50

$\frac{6.0}{365.6}$      $\frac{6.1}{365.5}$      $\frac{6.5}{365.1}$      $\frac{6.3}{365.3}$      $\frac{6.1}{365.0}$      $\frac{6.3}{365.3}$      $\frac{6.6}{365.0}$      $\frac{6.0}{365.6}$      $\frac{6.1}{365.5}$

2+00

$\frac{5.7}{365.8}$      $\frac{5.8}{365.5}$      $\frac{6.3}{365.3}$      $\frac{6.6}{365.6}$      $\frac{5.7}{365.9}$      $\frac{6.0}{365.6}$      $\frac{6.4}{365.2}$      $\frac{5.8}{365.8}$      $\frac{5.5}{365.8}$

2+50

$\frac{5.3}{366.3}$      $\frac{5.4}{366.0}$      $\frac{5.4}{366.0}$      $\frac{5.7}{365.9}$      $\frac{5.2}{366.4}$      $\frac{5.6}{366.0}$      $\frac{5.9}{365.7}$      $\frac{5.5}{366.1}$      $\frac{5.6}{366.0}$

3+00

$\frac{5.3}{366.3}$      $\frac{5.1}{366.0}$      $\frac{5.3}{366.3}$      $\frac{5.7}{366.5}$      $\frac{4.8}{366.8}$      $\frac{5.3}{366.3}$      $\frac{5.6}{366.3}$      $\frac{5.0}{366.6}$      $\frac{5.0}{366.6}$

Ellis Walker  
Preston Pilod  
E.P.L.

33

W.P.L. Carb. Cut  $\frac{1}{4}$  E  $\frac{1}{4}$  Cat. Carb. E.P.L.  
N.W. Co. Stockton + Olive.

X Sec. Central El Cajon to Monroe

Ellis  
Walker  
Preston  
Dibol  
EPL

34

Sta	+	π	-	Elev	W.P.L.	Comb det	φ	Went Comb	EPL
3+50		371.62			$\frac{4.7}{366.9}$	$\frac{4.7}{366.9}$ $\frac{5.3}{366.9}$ $\frac{5.0}{366.9}$	$\frac{4.6}{367.0}$	$\frac{4.9}{366.7}$ $\frac{5.4}{366.7}$ $\frac{5.7}{366.7}$	$\frac{4.8}{366.8}$
4+00					$\frac{4.1}{367.5}$	$\frac{4.3}{367.5}$ $\frac{4.8}{366.8}$ $\frac{4.6}{367.0}$	$\frac{4.3}{367.3}$	$\frac{4.6}{367.0}$ $\frac{5.1}{366.6}$ $\frac{4.7}{366.9}$	$\frac{4.7}{366.9}$
4+50					$\frac{4.0}{367.6}$	$\frac{4.1}{367.5}$ $\frac{4.8}{366.8}$ $\frac{4.6}{367.0}$	$\frac{4.3}{367.3}$	$\frac{4.7}{366.9}$ $\frac{5.3}{366.3}$ $\frac{4.6}{367.0}$	$\frac{4.8}{366.7}$
5+00					$\frac{3.8}{367.8}$	$\frac{3.8}{367.8}$ $\frac{4.0}{367.7}$ $\frac{4.3}{367.3}$	$\frac{4.1}{367.5}$	$\frac{4.6}{367.0}$ $\frac{5.2}{366.2}$ $\frac{4.5}{367.1}$	$\frac{5.2}{366.4}$
5+50					$\frac{3.9}{367.7}$	$\frac{3.8}{367.8}$ $\frac{4.8}{366.8}$ $\frac{4.4}{367.7}$	$\frac{4.2}{367.2}$	$\frac{4.5}{367.1}$ $\frac{5.0}{366.6}$ $\frac{4.3}{367.3}$	$\frac{4.8}{366.8}$
6+07	S.P.L Olive				$\frac{3.4}{368.2}$	$\frac{3.3}{368.3}$ $\frac{4.1}{367.5}$ $\frac{3.9}{367.7}$	$\frac{3.6}{368.0}$	$\frac{3.9}{367.7}$ $\frac{4.5}{367.1}$ $\frac{3.9}{367.7}$	$\frac{4.1}{367.5}$
			243	368.19			368.2		368.1
	4.13	373.32							
0+00	N.P.L Olive				$\frac{4.1}{368.2}$	$\frac{4.1}{368.2}$ $\frac{4.8}{367.5}$ $\frac{4.5}{368.3}$	$\frac{4.2}{368.1}$	$\frac{4.5}{368.8}$ $\frac{5.0}{368.3}$ $\frac{4.4}{368.9}$	$\frac{4.5}{368.8}$
							368.6		368.4
0+50					$\frac{3.5}{369.8}$	$\frac{3.3}{370.0}$ $\frac{4.1}{369.2}$ $\frac{3.7}{369.6}$	$\frac{3.3}{370.0}$	$\frac{3.7}{369.6}$ $\frac{4.3}{369.0}$ $\frac{3.5}{369.7}$	$\frac{3.8}{369.5}$
							368.7		368.5
1+00					$\frac{3.0}{369.7}$	$\frac{4.3}{370.0}$ $\frac{3.3}{369.6}$ $\frac{3.3}{370.0}$	$\frac{2.9}{370.4}$	$\frac{3.2}{370.1}$ $\frac{3.4}{369.7}$ $\frac{2.7}{370.6}$	$\frac{2.6}{370.7}$
							368.8		368.6

X Sec Central El Cajon to Monroe

Sta	+	π	-	Elev
1+50		37332		

2+00

2+50

3+00

3+50

4+00

4+50

5+00

5+50

5+71.37 S.P.L. Monroe

W.P.L.	Cumb cut 1/2	⊕	1/4 cut Cumb	E.P.L.
24 370.9	2.8 3.2 3.3 370.7 370.1 370.8	3.0 370.3	3.4 3.8 3.6 369.9 369.4 369.7	3.8 369.5

368.9 2.8 370.5	3.2 3.9 3.6 370.1 369.4 369.7	3.5 369.8	4.0 4.3 369.3 368.8	4.0 4.4 369.3 368.7
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368.9 3.8 369.5	3.8 4.2 4.5 369.5 368.6 368.8	4.4 368.9	4.8 5.0 4.8 368.4 368.3 368.5	5.2 368.1
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369 4.6 368.7	4.8 5.4 5.4 368.8 367.7 367.1	5.1 368.2	5.8 6.1 5.5 367.5 367.2 367.8	5.9 367.4
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369.1 5.0 368.5	5.6 6.0 5.7 368.3 367.3 367.6	5.5 367.8	6.2 6.7 5.9 367.1 366.6 367.0	6.4 366.9
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369.2 5.7 367.6	5.4 6.5 6.1 367.9 366.8 367.2	5.9 367.4	6.3 6.9 6.2 367.6 366.4 367.1	6.6 366.7
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369.3 5.6 367.7	5.7 6.3 6.7 367.6 367.0 367.0	6.3 367.0	6.3 7.1 6.5 366.8 366.2 366.8	6.8 366.5
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369.4 6.2 367.1	6.5 366.8	6.1 367.2	6.6 7.1 6.5 366.7 366.2 366.8	6.9 366.4
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369.5 6.3 367.1	6.4 366.9	6.3 367.0	6.3 6.8 6.4 367.0 366.5 366.9	6.6 366.7
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369.5 6.2 367.1	5.8 367.4	5.8 367.8	5.9 6.6 6.3 367.4 366.7 367.0	6.3 367.0
-----------------------	--------------	--------------	----------------------------------	--------------

369.6

Ellis  
Walker  
Preston dated

30

368.7

368.7

368.9

369

369.1

369.2

369.3

369.3

369.4

369.4

X Sec 4<sup>th</sup> St E/Cajon to Olive.

Sta + T - Elev  
369.19

0+00 3.24 372.43  
N.P.L. E/Cajon

0+50

1+00

1+50

2+00

2+50

3+00

3+50

W.P.L. Comb. Cont'd & 1/2 Sect Comb. E.P.L.  
T.P.B.M. N.W.C. Olive + Central

$\frac{5.7}{366.7}$   $\frac{6.2}{366.2}$   $\frac{7.0}{365.4}$   $\frac{6.3}{366.1}$   $\frac{6.0}{366.4}$   $\frac{6.1}{366.3}$   $\frac{6.5}{365.9}$   $\frac{5.9}{366.5}$   $\frac{5.8}{366.6}$

$\frac{5.7}{366.7}$   $\frac{6.1}{366.3}$   $\frac{6.8}{365.6}$   $\frac{6.3}{366.1}$   $\frac{5.9}{366.5}$   $\frac{6.1}{366.3}$   $\frac{6.4}{366.7}$   $\frac{5.9}{366.5}$   $\frac{6.8}{365.9}$

$\frac{6.0}{366.4}$   $\frac{6.0}{366.4}$   $\frac{6.6}{365.8}$   $\frac{6.2}{366.2}$   $\frac{5.8}{366.6}$   $\frac{6.0}{366.4}$   $\frac{6.5}{365.9}$   $\frac{5.8}{366.6}$   $\frac{6.2}{366.2}$

$\frac{5.7}{366.7}$   $\frac{5.9}{366.5}$   $\frac{6.2}{365.8}$   $\frac{6.1}{366.3}$   $\frac{5.8}{366.6}$   $\frac{6.0}{366.4}$   $\frac{6.4}{366.0}$   $\frac{5.7}{366.7}$   $\frac{5.9}{366.5}$

$\frac{5.9}{366.8}$   $\frac{5.7}{366.7}$   $\frac{6.4}{366.0}$   $\frac{6.0}{366.4}$   $\frac{5.8}{366.9}$   $\frac{5.9}{366.5}$   $\frac{6.3}{366.1}$   $\frac{5.7}{366.7}$   $\frac{5.9}{366.5}$

$\frac{5.8}{366.9}$   $\frac{5.8}{366.9}$   $\frac{6.2}{366.2}$   $\frac{5.8}{366.4}$   $\frac{5.3}{367.1}$   $\frac{5.7}{366.7}$   $\frac{6.3}{366.1}$   $\frac{6.7}{366.7}$   $\frac{5.7}{366.7}$

$\frac{5.2}{367.2}$   $\frac{5.3}{367.1}$   $\frac{6.1}{366.9}$   $\frac{5.5}{366.9}$   $\frac{5.2}{367.2}$   $\frac{5.7}{366.7}$   $\frac{6.2}{366.7}$   $\frac{5.5}{366.9}$   $\frac{5.6}{366.8}$

$\frac{5.3}{367.1}$   $\frac{5.2}{367.2}$   $\frac{5.9}{366.5}$   $\frac{5.4}{367.2}$   $\frac{4.9}{367.5}$   $\frac{5.5}{366.9}$   $\frac{6.0}{366.4}$   $\frac{5.3}{367.1}$   $\frac{5.5}{366.9}$

10-22-23  
36

X Sec 4<sup>th</sup> St EIC on + Olive

Ellis  
Walker  
Proctor  
37  
1022-23

Sta + X - Elev  
4+00 372.43

W.P.L.	Cont. Cut by	℄	Cont. limb	E.P.L.
$\frac{5.3}{367.1}$	$\frac{4.9 \ 5.7 \ 5.3}{367.5 \ 367.6 \ 367.1}$	$\frac{4.8}{367.6}$	$\frac{5.2 \ 5.8 \ 5.0}{367.2 \ 367.6 \ 367.9}$	$\frac{5.0}{367.4}$

4+50

$\frac{4.7}{367.7}$	$\frac{4.7 \ 5.7 \ 5.1}{367.5 \ 367.7 \ 367.3}$	$\frac{4.6}{367.8}$	$\frac{5.0 \ 5.6 \ 4.8}{367.4 \ 367.8 \ 367.6}$	$\frac{5.0}{367.4}$
---------------------	---	---------------------	---	---------------------

5+00

$\frac{4.3}{368.1}$	$\frac{4.7 \ 5.4 \ 5.0}{367.7 \ 367.9 \ 367.4}$	$\frac{4.5}{367.9}$	$\frac{4.9 \ 5.4 \ 4.6}{367.6 \ 367.8 \ 367.8}$	$\frac{4.6}{367.8}$
---------------------	---	---------------------	---	---------------------

5+50

$\frac{4.0}{368.4}$	$\frac{4.5 \ 5.2 \ 4.8}{367.9 \ 367.7 \ 367.6}$	$\frac{4.3}{368.1}$	$\frac{4.6 \ 5.1 \ 4.4}{367.8 \ 367.3 \ 368.0}$	$\frac{4.3}{368.1}$
---------------------	---	---------------------	---	---------------------

6+? S.P.L Olive

$\frac{4.2}{368.2}$	$\frac{4.4 \ 5.0 \ 4.6}{368.0 \ 367.4 \ 367.8}$	$\frac{4.1}{368.3}$	$\frac{4.3 \ 4.9 \ 4.2}{368.1 \ 368.2 \ 368.2}$	$\frac{3.9}{368.5}$
---------------------	---	---------------------	---	---------------------



Hulse Moore		Levels on Molino Ave		50' wide		289.08			38
DN NE Univ + Molino 65'		289.08	282.57	iron pipe	EL		6.1	283.0	
20' NL of Univ on WL of Molino						215' N = PC		sta. on WL	
WL	10.0	279.08		EL			5.5	283.6	
C	7.0	282.08		C			5.8	283.3	
EL	6.5	282.6		WL			6.8	282.3	
13' N = Opposite NE cor of Univ + Molino						258.2' N		Conv. = 43.24	
EL	6.5	282.6		WL			6.2	282.9	
C	6.8	282.3		C			5.0	284.1	
WL	8.9	280.2		EL			5.0	284.1	
50' N						201.48' N			
WL	7.0	282.1		EL			3.6	285.5	
C	6.2	282.9		C			4.9	284.2	
EL	5.9	283.2		WL			5.2	283.9	
100' N						344.72' N			
EL	5.5	283.6		WL			2.2	286.9	
C	6.1	283.0		C			2.0	287.1	
WL	7.3	281.8		T.P.	130'	300.57	155	287.53	
150' N				EL			11.1	289.5	
WL	7.0	282.1				387.96' N = EC			
C	6.3	282.8		EL			3.0	285.0	
				C			10.5	277.5	
				WL			7.3	279.7	

Levels on Lemona N. of Univ 30w70

305.94

39

Unit  
on BM SW Lemona 0.35

329.79

329.79

5x iron pipe

150' N

NL = 0.000

WL

9.4

320.4

WL

14.7

291.2

EL

10.0

319.8

EL

12.3

293.6

25' N

EL

6.7

299.2

EL

9.2

320.6

WL

2.0

303.9

WL

8.9

320.9

200' N

250' N

T.P.

0.79

317.92

12.66

317.13

WL

1.7

304.2

50' N

T.P.

4.33

309.45

0.82

305.17

WL

6.3

322.5

EL

11.3

294.6

EL

9.9

319.9

300' N

T.P.

0.68

305.94

12.62

305.26

EL

12.2

293.7

100' N

WL

5.6

300.1

EL

12.8

317.0

250' N

WL

13.8

316.0

WL

4.2

301.7

110' N

EL

8.8

297.1

WL

16.2

313.6

400' N

EL

14.0

315.8

EL

1.7

304.2

125' N

WL

1.6

304.3

EL

15.5

311.3

309.45

Lennon, N of  
Univ.

T.P.

8.67

317.04

10.8

308.37

446.53 N = SL of Hill Place

WL

6.2

303.3

EL

6.8

302.7

496.53 N = NW ✓ ✓

EL

5.5

304.0

WL

4.8

304.7

40

Levels on Lemona S of Univ. 55.5' wide				Note Middle 25' graded 338.69			41
on 5" dia. PVC pipe	9x5	338.69	329.44	Univ. + Lemona	EL	4.4	
		SL of Univ. = 0+00				250' S = NL of King Court on W	
WL		9.3	329.4		EL	5.3	332.4
C		13.9	324.8		C	5.2	333.5
EL		13.3	325.4		WL	4.6	334.1
		50' S				300 S = SL	✓ ✓ ✓
EL		8.3	330.4		WL	6.1	333.6
C		9.1	329.6		C	5.6	333.1
WL		5.1	333.6		EL	6.1	332.6
		100' S				350 S	
WL		4.1	334.6		EL	5.5	333.2
C		6.7	331.8		C	5.8	332.9
EL		5.0	333.7		WL	5.8	332.9
		150' S				400' S	
EL		4.3	334.4		WL	6.7	332.0
C		5.3	333.4		C	5.7	333.0
WL		4.6	334.1		EL	5.5	333.2
		200' S				450' S	
WL		4.9	333.8		EL	5.5	333.2
C		5.2	333.4		C	6.3	332.4

338.69

WL

7.0

331.7

500 S - WL of Carland (West)

WL

7.7

331.0

C

6.7

332.0

EV

6.1

332.6

42

11/6/75  
Moore

Levels on Skiloh St of Univ. 50' wide

338.37

43

Lemon Villa  
SE Blk 2nd

12.93

325.96

31303

iron pipe

EL

3.1

335.3

SL of Univ. = 0+00

WL

3.1

335.3

EL 2nd hole P

3.4

322.6

T.P

11.84

349.81

0.40

337.97

e

5.1

320.9

250 S

WL

6.7

319.3

WL

12.5

337.3

50' S

C

10.9

338.9

WL

4.5

321.5

EV

10.0

339.8

C

3.3

323.7

? 270.4' S = N.E. of Arnett Ave  
280.4'

EV

1.4

324.6

EL

8.2

341.6

100' S

C

10.0

339.8

EV

0.2

325.8

WL

11.9

337.9

C

0.9

325.1

0+00 = SL of Arnett 40' wide

WL

1.1

324.9

WL

8.0

341.8

T.P

12.83

338.37

0.42

325.51

C

6.7

343.1

150' S

EV

4.0

345.8

WL

8.0

330

T.P

10.86

358.46

2.21

347.60

e

8.5

329.9

50' S

EV

9.5

328.9

EL

9.9

348.6

200' S

C

11.3

347.2

358.46

WL 12.5 346.0

100'S

WL 8.9 349.6

C 8.7 349.8

L.EV 7.6 350.7

150'S

EV 6.8 351.7

C 6.1 352.4

WL 7.0 351.5

200'S

WL 6.9 351.6

C 6.7 351.8

EV 5.2 353.3

250'S

EV 6.2 352.3

C 5.9 352.6

WL 5.8 352.7

280'S = WL of Beverly

WL 6.9 351.6

C 6.4 352.1

Shiloh

44

EL 6.0 352.5

SL of Beverly How wide

EL 4.0 354.5

C 5.8 352.7

WL 6.2 352.3

Levels on Douglas S of Univ 50 wide

Univ &  
SW Radio Road  
Douglas

648 370.30 313.87 Iron pipe

EL

11.9 308.4

45

SL of Univ 0 to 0

250 S

WL 6.5 313.8

EL

11.9 308.4

C 7.0 313.9

C

8.3 312.0

EL 7.2 313.1

WL

4.0 316.3

50' S

280.4 = NL of Arrott 40' wide

EL 12.8 307.5

WL

3.7 316.6

C 10.5 309.8

C

7.8 312.5

WL 10.6 309.7

EL

12.2 308.1

100' S

SL Arrott

WL 8.4 311.9

EL

12.2 308.1

C 11.2 309.7

C

7.1 313.2

EL 14.3 306.0

WL

2.8 317.5

150' S

EL 12.5 307.8

C 9.8 310.5

WL 6.3 314.0

200' S

WL 5.4 314.9

C 8.7 311.6



Levels on Douglas No. Univ. 50' wide

Univ. + Radio Road 13.21 327.03 313.82 iron pipe

0+00 = N.L. of Univ. = 60' N of iron pipe?

wL 6.7 320.3  
 c 7.0 320.0  
 EV 7.4 319.6

50' N

EV 3.0 324.0  
 c 2.1 326.9  
 wL 0.4 326.6

T.P. 898 336.00 0.2' 327.02

100' N

wL 5.0 322.0  
 c 5.0 322.0  
 EV 6.3 320.7

150' N

EV 5.1 321.9  
 c 2.2 324.8  
 wL 2.3 324.7

Chas Moore  
 July 5<sup>th</sup> 1939  
 DEM. Curb Levels on  
 10' Sidw. & Curbs in  
 Nashville, Causeway Nely to Lapwai

BM B.P. HOWAY  
 CUM. PT. R.R.  
 Causeway

430	7.30	3.00
Nly Causeway = 00		
E NEW cb	5.62	1.68
" 90T	6.22	1.06
C Pav.	6.07	1.23
W 90T	6.26	1.06
W NEW cb	6.05	1.26
0 + 01		
W TOP old cb	7.06	0.24
E	7.10	0.20

S.L. Jupiter

E	7.23	0.07
W	7.23	0.07
400 E Nashville	7.55	-0.25
480 W "	8.75	-1.45

Indexed  
 C.S.K. 7.30

N.L. Jupiter

E	cb	7.30	0.00	
W	cb	7.30	0.00	
400 E Nashville		7.66	-0.34	
480 W "		8.85	-1.55	
T.P.	4.73	4.52	7.51	-0.21
S.L. La Salle				
E	cb	4.81	-0.29	
W	"	4.75	-0.23	
400 E Nashville		3.92	+0.60	
480 W "		6.01	-1.49	
N.L. La Salle				
E	cb	4.75	-0.23	
W	cb	4.75	-0.23	
400 E Nashville		3.95	+0.57	
480 W "		6.05	-1.53	
T.P.	4.71	4.46	4.97	-0.45

426

## S L Western

W cb 5.04 -0.76

E cb 5.00 -0.74

400 " E Nashville 4.97 -0.71

480 W " 5.91 -1.65

## N W Western

E cb 5.13 -0.87

W cb 5.10 -0.74

400 E Nashville 5.17 -0.91

480 W " 5.95 -1.69

T.P. 5.45 4.30 5.41 -1.15

## S L Lapwai

W cb 5.45 -1.15

E " 5.50 -1.20

120 " E of Nashville 5.10 -0.80 Top cb

483 W " 6.14 -1.84 " "

430

levels for Prop  
Sly Ditch  
48

## S cb Lapwai

W L Nashville 000

00 dirt 5.2 -0.9

0 150 E L Nashville 4.8 -0.5 dirt

1 S E 1/4 4.5 -0.2 "

+70 4.1 +0.2 "

" ON CB 5.10 -0.7

✓ 4.3 00 "

+50 4.0 +0.3 "

3 3.7 +0.6 "

+18 end cb 4.65 -0.35 Top curb

" dirt 3.7 +0.6 dirt

T.P. 6.65 5.49 5.45 -1.15 Top cb  
S L Lapwai  
W cb  
Nashville

3450 5.1 +0.4 dirt

4 4.0 +1.5 "

+35 4.5 +1.0

+75 3.0 +2.5

5 5.0 +0.5

5 + 50	5.6	+0.9
6	4.7	+0.8
+ 50	4.8	+0.7
7	5.6	+0.9
+ 50	4.3	+1.2
8	4.4	+3.1
+ 30	3.0	+1.9
+ 65	7.0	-1.5
9	7.0	-1.5
+ 30 old river channel	7.7	-2.2 ✓
+ 60	4.0	+1.5

49

roads for prop ditch Nly

Nly Ext of Nashville + road

Pac. View.

along Wly curb Nashville

11.1 996 -1.15 top cb.

SW Cor Nashville + Lapwai = 0.0

00	11.1	-1.1	dir T
0 + 10	10.8	-0.8	"
0 + 50 Nly Lapwai	10.2	-0.2	"
1	9.8	+0.2	"
✓	9.3	+0.7	"
3	9.1	+0.9	"
+ 50 E King	9.3	+0.7	"
4	9.4	+0.6	"
+ 60	9.1	+0.9	"
5	6.0	+4.0	"
+ 50	3.5	+6.5	"
6	1.8	+8.2	"
11 + 65 Sly	3.4	+6.4	"
7	4.2	+3.8	"

9.96

7+35 10.5 -0.5

8 8.4 +1.4

+15 8.6 +1.4

+30 old channel 11.4 -1.6

7+35  $\Delta$  90° RT 10.5 -0.5

8 10.4 -0.6

+40 11.0 -1.0

+50 old overflow 12.3 -2.3

channel of river

Levels for ditch

514 curb Lapwai

Nashville Wly

50

6.00 4.85 -1.15 curb

00 + W/L Nashville 6.00 -1.15 "

" " 5.80 -0.95 ground

1 +00 cb 6.25 -1.40

" ground 6.0 -1.15

" cb 6.35 -1.50

" ground 5.9 -1.05

3 cb 6.47 -1.62

" ground 5.0 -0.15

+15 " 5.0 -0.15

+35 " 4.8 +0.05

+50 " 5.4 -0.5

" cb 6.67 -1.82

" ground 6.0 -1.15

4+83.85 Wly Druckers 6.69 -1.74 cb

" " 5.4 -0.5 ground

5 make angle bene 5.2 -0.7

See next Page

6	5.4	-0.3
7	5.6	-0.7
8	6.1	-1.3

Too far to go w/ly

5+00 Δ 60°43' LT.	5.7	-0.3
-------------------	-----	------

6	5.5	-0.6
---	-----	------

7	6.4	-0.5
---	-----	------

+50	6.6	-0.7
-----	-----	------

+75 Top Emb.	5.1	-0.2
--------------	-----	------

+87 int. of dug	7.8	-2.9
-----------------	-----	------

ditch on Nly curb line of  
Western St.

See P 47

8-3-39  
Miller  
Walker  
Bliss

X Sec. National Hwy E. of 41<sup>st</sup>  
For Bridge

36.7  
216.8  
253.5

4+14  
25'  
3+89

conc. prev  
30' 10'

Indexed  
C.S.K.

52

B.M. B.P.

35.25

N.W. National  
+ 41<sup>st</sup>

channel location  
240' N. of & 20' strip

3+90 = W. Bank. of Wash. overall

3+98 W side of wash

5+40 W Bank. Main wash

5+80 W side " "

6+08 E " " "

6+18 E Bank of Wash overall

240' S. of & 20' strip

2+00 W Bank Wash overall

2+10 W side " "

2+40 = W. Bank. Main wash.

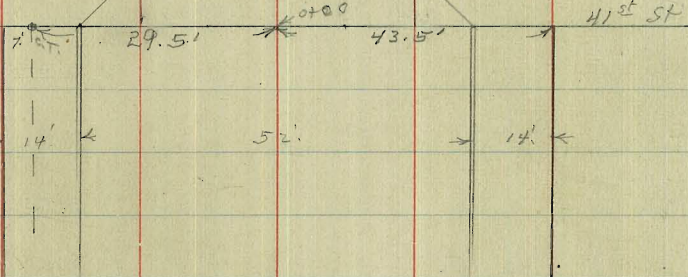
2+50 = W side " "

2+75 = E. " " "

3+05 = E " Wash overall

3+20 = E Bank " "

W. Line



e. end. Bridge

W. End. Bridge

41<sup>st</sup> St

				N. W. 41 <sup>st</sup> + National			National	53
BM. B.P.	1.39	36.64	35.25		18. LT	2.9	28.7	
T.P.	5.00	31.62	10.02	26.62	10. LT = N. Pav	3.14	28.48	
	0+00 = W. Line 41 <sup>st</sup> St.				£ "	3.17	28.45	
	2+00 E.							
60. Rt		6.1	25.5		10. Rt = S. "	3.32	28.30	
40. Rt.		5.5	26.1		18. "	3.4	28.2	
20. "		4.0	27.6		20. "	4.6	27.0	
17. "		2.7	28.9		40. "	5.9	25.7	
10. " = S. Pav		2.79	28.83		60. " w. bank. overall	6.6	25.0	
£ "		2.58	29.04					
10. LT = N. "		2.47	29.15					
16. "		2.4	29.2		2+60			
20. "		4.5	27.7		60. Rt	9.0	22.6	
25. "		5.6	26.0		40. " w. Bank. overall	5.6	26.0	
40. "		4.2	25.4		20. "	5.2	26.4	
60. "		6.0	25.6		17. "	3.5	28.1	
					10. " = S. Pav	3.41	28.21	
					£ "	3.30	28.32	
					10. LT = N. "	3.34	28.28	
	2+45 E				17. "	3.2	28.4	
60. LT		6.1	25.5		20. "	4.6	27.0	
40. "		6.4	25.2		40. "	4.5	27.1	
30. "		6.0	25.6		42. "	6.8	24.8	
20. "		4.4	27.2		60. "	6.3	25.3	



31.62  
2+700.

60' Lt		7.5	24.1
47. "		8.0	23.6
40. "		5.5	26.1
20. "		4.3	27.3
18. "		3.3	28.3
10. "	N. Pav	3.50	28.12
⊕	"	3.45	28.17
10. RT- S	"	3.47	28.15
16. "		3.6	28.0
28. "		8.4	23.2
40. "		9.0	22.6
60. "		10.8	20.8
2+92			
60. RT.	W. side main wash	13.1	18.5
45. "	" " " "	13.0	18.6
40. "	" Bank " "	10.6	21.0
25. "		9.4	22.2
16. "		3.2	28.4
10. "	S. Pav.	3.73	27.89
⊕	"	3.71	27.91
10. Lt.	N "	3.78	27.84

31.62

National 54

17. Lt		4.2	27.4
22. "		6.4	25.2
30. "	Wash from NW.	10.4	21.2
40. "	" " "	10.2	21.4
50. "	" " "	10.2	21.4
60. "	Nat ground.	4.1	27.5
3+05 W. Abutment of Bridge			
60. Lt	Nat. gr.	5.2	26.4
50. "	" "	5.4	26.2
40. "	Wash from NW.	8.3	23.3
27. "	W. Banks. Main wash	10.0	21.6
20. "		9.0	22.6
11. "	ground. below	8.8	22.8
10. "	pav at W End. Bridge	3.72	27.90
⊕	" " " " "	3.70	27.92 ✓
10. RT	" " " " "	3.70	27.92
11. "	ground. below	10.0	21.6
20. "		11.1	20.5
25. "	W. side Main wash	12.8	18.8
40. "	W side " "	13.0	18.6
60. "	W " " "	13.3	18.3

31.62  
3+13

60' RT		14.0	17.6
40' "		13.8	17.8
10' " W. side Main wash		13.8	17.8
ϕ " " " "		14.0	17.6
10' LT " " " "		14.0	17.6
40' " " Bank " "		9.0	22.6
50' "		8.3	23.3
60' " = W. Bank overall		5.4	26.2

3+35

60' LT		9.1	22.5
34' LT NW. Bank main wash		9.4	22.2
30' " " side " "		12.5	19.7
10' " " " " " "		12.5	19.1
ϕ		12.6	19.0
10' RT		12.8	18.8
40' RT		12.7	18.9
60' "		13.0	18.6

3+45

60' RT E. side Main wash	13.0	18.6
40' " " " " " "	13.2	18.4

31.62

National 55

70' RT		12.4	19.2
ϕ		13.2	18.4
10' LT		13.0	18.6
30' " N.W. side Main wash		12.2	19.4
40' " " Bank " "		9.2	22.4
60' " " wash		8.8	22.8

3+60

60' LT " wash	9.2	22.4	
40' " NW. Bank Main Wash	10.1	21.5	
35' " NW side " "	12.0	19.6	
10' " " " " " "	13.0	18.6	
ϕ		13.0	18.6
10' RT E. side Main wash	12.0	19.6	
30' " " " " " "	12.1	19.5	
40' " " Bank " "	10.4	21.2	
60' " " " " " "	9.7	21.9	

3+89 E. Apartment

60' RT	10.0	21.6
40' "	9.8	21.8
11' "	9.3	22.3

31.62  
3+89 (cont)

10' Rt.	s. pav. W. End	3.72	27.90
♀	" " "	3.73	27.89
♀	under Bridge		
10' Lt	N " " 4?	3.70	27.92
11' Lt.		10.2	21.4
14' "	s.e. side Main wash	12.2	19.4
40' "	in " "	12.0	19.6
45' "	NW side " "	10.4	21.2
60' "	NW Banks, " "	8.0	23.6
		4+00	
60' Lt.	N.W. side Main wash,	12.0	19.6
40' "		12.2	19.4
25' "	s.e. side Main wash	13.2	18.4
15' "	wooden Bulkhead	9.3	22.3
14' "		4.1	27.5
10' "	1 pav	3.82	27.80
♀	" "	3.70	27.92
10' Rt		3.73	27.89
16' "		3.2	28.4
25' "		9.3	22.3
40' "	E. side wash overall	9.8	21.8
60' "	" " " "	10.3	21.3

31.62

4+14

60' Rt	E. Bank. overall	4.4	27.2
40' "	" "	4.2	27.4
35' "	" side "	8.8	22.8
25' "	" "	8.6	23.0
16' "		3.3	28.3
10' "	S. Pav	3.67	27.94
♀		3.70	27.92
10' Lt		3.82	27.80
15' "		4.2	27.4
16' "	wooden Bulkhead,	6.9	24.7
25' "		12.0	19.6
30' "	s.e. side main wash	12.4	19.2
40' "	in " "	12.4	19.2
60' "	N.W. side " "	12.4	19.2
		4+25	
60' Lt.		12.4	19.2
40' "		12.2	19.4
35' "	s.e. side	11.0	20.6
25' "		11.0	20.6

National

56

31.62  
4+25 con.

10' Lt	= N Pav	3.73	27.89
4'	"	3.58	28.04
10' Rt.	S "	3.61	28.01
16'	"	3.2	28.4
20'	" S.E. side wash overall	6.0	25.6
27'	"	6.0	25.6
30'	"	4.1	27.5
40'	"	4.1	27.5
60'	"	4.3	27.3
		4+57	
60' Rt		4.6	27.0
40'	"	4.8	26.8
18'	"	3.4	27.8
15'	"	2.5	29.1
10' Rt	S. Pav	3.04	28.54
4'	"	2.99	28.63
10' Lt.	N. "	3.10	28.52
15'	"	3.0	28.6
16'	"	4.0	27.6
25'	S.E. side wash overall	8.0	23.6

31.62

National  
57

40' Lt		8.7	22.9
60'	S.E. Bank. Main wash	10.0	21.6
T.P.	12.32	34.31	9.63
		4+75	
60' Lt		11.6	22.7
40'	E. side Wash overall	9.5	24.8
30'	"	6.7	27.6
20'	"	6.0	28.3
17'	"	4.7	29.6
10'	" N Pav	5.14	29.17
4'	"	5.07	29.24
10' Rt.	S "	5.14	29.17
17'	"	4.5	29.8
23'	"	5.8	28.5
40'	"	6.7	27.6
60'	"	7.1	27.2

34.31

4+90

60' RT		7.2	27.1
40' "		6.6	27.7
23' "		5.3	29.0
19' "		4.2	30.1
10' RT	S. Pav	4.56	29.75
ϕ	"	4.46	29.85
10' Lt.	N "	4.55	29.76
18' "		4.3	30.0
25' "		5.8	28.5
35' "		8.8	25.5
40' "		6.3	28.0
55' "	E. Bank wash overall	6.3	28.0
60' "	E. side wash overall	9.3	25.0
		4+95	
60' Lt.	E. Bank wash overall	6.8	28.3
40' "		6.1	28.2
35' "		8.9	25.4
30' "		5.6	28.7
22' "			
18' "		4.0	30.3

34.31

National

58

10' Lt	N. Pav	4.30	30.01
ϕ	"	4.26	30.05
10' RT	S "	4.37	29.94
18' "		4.1	30.2
21' "		5.3	29.0
40' "		6.3	28.0
60' "		6.3	28.0
		5+30	
60' RT		6.6	27.7
40' "		5.9	28.4
25' "		5.0	29.3
20' "		2.9	31.4
10' "	S. Pav	2.72	31.59
ϕ	"	2.59	31.72
10' Lt	N. "	2.66	31.65
18' "		2.6	31.7
20' "		4.2	30.1
40' "		4.8	29.5
60' "		5.0	29.3
T.P.	9.09	35.72	7.68
Orig BM			0.48
			35.24 = 35.25

Cross Section San Jose Place  
Ocean Front Walk to Bayside Walk  
Stationing

Indexed  
c.s.k.

24' Wide

July 24-40  
S. 18507  
North 1877  
W. 110080 59

BM 4.24 11.32 7.68

S.N.B.P.  
San Jose +  
Seawall

0+54

0-12 = Fly Ocean Front Walk Conc.

S-0.2 = 1/4" Conc Slab 4.61 6.71

S on Conc Walk 6.67 4.65

0+79

S " " " 6.70 4.62

S-0.3 = Fly Conc Slab 4.87 6.95

H " " " 6.70 4.62

0+80 = 1/2" Strand W/ly

0+0 = F. Line Ocean Front Walk

H 5.0 6.3

H 6.9 4.9

S 4.8 6.5

S 6.6 4.7

S 4.5 6.8

S 6.7 4.6

0+0 = F. L. Strand W/ly

0+23

S 4.6 6.7

S-0.3 = 1/2" Conc Walk 5.91 5.91

S 4.8 6.5

0+25

H 5.2 6.1

H-1.0 = 1/2" Plank Walk 6.60 4.72

0+12

0+40

H-1.4 = 1/2" Conc Walk 5.42 5.90

S 5.0 6.3

0+24

S 5.0 6.3

H-1.7 = 1/2" Conc Walk 6.02 5.30

H 5.2 6.1

H 6.2 5.1

0+52

S 6.0 5.3

H-0.9 = 1/2" Plank Walk 4.72 6.60

S 6.0 5.3

S-0.3 = 1/2" Conc Walk 4.63 6.69

Levels Reduced  
86-7127/40

San Jose

11.32

0+50

S	7.1	2.2
L	7.2	2.1
H	7.1	2.2

0+84

-1.0 = 5' Conc Walk	8.22	3.10
H	8.8	2.5
L	8.7	2.6
S	8.6	2.7

0+78

S - 0.2 = 2.5' Conc Walk	8.07	3.25
--------------------------	------	------

1+03

-0.2 = 3.7' Plank Walk	8.95	2.37
S	9.4	1.9
L	9.4	1.9
H	9.5	1.8

1+35

H	10.5	0.8
L	10.5	0.8

60

11.32

S	10.4	+0.9
TP	3.62	4.40
	10.54	0.78

1+60.4 = Wly Edge Paving Mission Blvd

S cb Top Ground	4.26	+0.19
S Paving	4.23	+0.17
L "	4.12	+0.28
H " + Top Cb Ground	4.20	+0.20

1+70.4 = NCB Mission Blvd

H on Paving	4.74	-0.34
L " "	4.73	-0.33
S " "	4.78	-0.38

FC6 Mission Blvd

S on Paving	5.07	-0.67
L " "	4.95	-0.53
H " "	5.05	-0.65

0+0 = FL Mission Blvd

H cb Top	4.55	-0.15
H on Paving	4.64	-0.29
11.8 = Wly Conc Walk	4.56	-0.16

4.40

♂ on Pav 129	4.57	-0.17
+11.1 = H Fly 2 Conc Walk	4.70	-0.30
S on Pav 129	4.66	-0.26
S c6 Top	4.58	-0.28

0+39

S -0.5 = ♀ 3' Conc Door Way	4.58	-0.18
H = ♀ 3' Conc " "	4.30	+0.10

0+46

S on 2 Conc Walk	4.68	-0.28
+2 = H Fly " "	4.84	-0.94
♂	5.0	-0.6
+10	4.8	-0.2
+10.1 = S Fly 2 (Conc) Walk	4.54	-0.14
H on 2 Conc Walk	4.51	-0.11

0+51

S +1.8 = H Fly 2 Conc Walk	4.86	-0.96
S = Fly 2 Conc Walk	4.72	-0.32

0+52

H +0.6 = ♀ 2.5 Conc Walk	4.66	-0.26
--------------------------	------	-------

4.40

0+93

H +0.9 = ♀ 2' Tile Walk	5.00	-0.6
	1+0	

H	5.1	-0.7
♂	5.3	-0.9
S	5.2	-0.8

1+12

H +0.9 = ♀ 3' Tile Walk	5.18	-0.78
-------------------------	------	-------

1+27

H = ♀ 2.6 Conc Walk	5.05	-0.65
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TP	4.89	3.89	5.40	-1.00 ✓
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1+31

S +0.1 = ♀ 3.9 <sup>Conc</sup> Bot on Strip	4.35	-0.96
---	------	-------

1+50

S = ♀ 1.7 Conc Walk	4.62	-0.73
---------------------	------	-------

S	4.8	-0.9
---	-----	------

♂	4.9	-1.0
---	-----	------

H	5.0	-1.1
---	-----	------

61



3.89

3.89

1+90.11 = N.L. Bayside Lane

0+49

H	4.9	-1.0
L	5.0	-1.1
S	4.9	-1.0

H-0.7 = 4.5' Plank Walk	4.87	-0.98
0+53		
H-0.8 = 3' Conc Walk	4.44	-0.55

0+0 = E.L. Bayside Lane

0+56

S	4.9	-1.0
L	5.0	-1.1
H	5.0	-1.1

-2' = Fly Conc Apron	4.28	-0.39
S = Fly " "	4.31	-0.42
S	4.5	-0.6
L	4.5	-0.6
H	4.6	-0.7

0+10

S-6.7 = Fly Du Garage Dirt Floor	4.9	-1.0
----------------------------------	-----	------

0+23

0+67

H-0.6 = 4' Conc Walk	4.73	-0.87
----------------------	------	-------

H-0.5 = 3.4' Conc Walk	4.30	-0.41
------------------------	------	-------

0+24

0+78

S-3.4 = Fly Du Garage Dirt Floor	4.8	-0.9
----------------------------------	-----	------

H	4.1	-0.2
L	4.1	-0.2
S	4.2	-0.3

0+30

H	5.0	-1.1
---	-----	------

L	4.9	-1.0
---	-----	------

S = Fly Conc Apron	4.54	-0.65
--------------------	------	-------

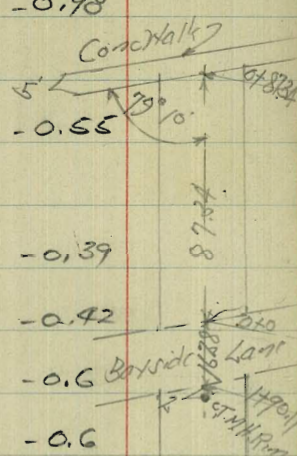
S = Fly Conc Walk	4.25	-0.32
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+5 = 07 " "	4.24	-0.45
-------------	------	-------

L = " " "	4.26	-0.37
-----------	------	-------

N Line Garage

H " " "	4.25	-0.36
---------	------	-------



12x12

12x12

0.50

87.84  
0+87.84 = Fly Conc Walk Bayside Walk

Cross Section Santa Clara Place  
 Ocean Front Walk to Boardwalk  
 & Stationing

Indexed  
 c.s.k.

24' Wide

July 26-40 63  
 S. McCoy  
 H. L. Berger  
 W. Moore

11.57

BM	Stationing	Index	Notes	Value 1	Value 2
BM	4.38	11.57	7.19	4.3	7.3
	0+12 = Fly Conc Walk		Ocean Front Walk	4.6	7.0
S	0+12 Conc Walk	6.84	9.73		
⊘	" " "	6.92	4.65		
H	" " "	6.94	4.63		
	0+20 = E Line		Ocean Front Walk	4.7	6.9
H		6.8	4.8		
⊘		6.8	4.8	0+10	
S		6.7	4.9		
	0+20			0+38	
S		6.0	5.6		
⊘		6.2	5.4		
H		6.4	5.2		
	0+40			0+59	
H		5.9	5.7		
⊘		5.2	6.9		
S		5.3	6.3		
	0+80 = W. Strand				
S		4.4	7.2		

Six BP  
 Santa Clara  
 & Boardwalk

0+10 = E. L. Strand

H = 23 Conc Walk

0+38

-1.0 = 23 Conc Walk

0+59

H - 0.8 = 25 Conc Walk

Notes Reduced - 7-29-40

11.57

4.31

1+0

-10	9.8	1.8
S	9.2	2.9
f	9.2	2.9
H	9.4	2.9
+10	9.6	2.2

S on Paving	4.02	0.29
f " "	4.02	0.29
H " "	4.00	0.31
H cbTop	3.95	+0.36

1+03

S-0.5 = f 2.6 (Cone) Walk 9.13 2.09

1+84.6: Wcb Mission Blvd

H on Paving	4.66	-0.35
f " "	4.62	-0.31
S " "	4.63	-0.32

1+12

S-0.5 = f 3.7 Cone Walk 9.30 2.37

Ecb Mission Blvd

S on Paving	4.93	-0.62
f " "	4.91	-0.60
H " "	4.97	-0.66

1+35

-10	11.1	0.5
H	10.4	1.2
f	10.1	1.5
S	10.2	1.9
+10	10.5	1.1

0+0: E.L. Mission Blvd

H cbTop	4.64	-0.33
H on Paving	4.67	-0.36
f " "	4.56	-0.25
S " "	4.61	-0.30
S cbTop	4.61	-0.30

TP 3.21 4.31 10.47 1.10

1+74.6 = H.L. Mission Blvd Paving

S cbTop 3.97 0.39

431

0+50

S	5.0	-0.7
L	5.0	-0.7
H	5.0	-0.7

0+76

S-0.6 = 2' 3" Conc Walk	5.19	-0.88
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0+90

H-0.3 = 2' 3" Conc Walk	4.98	-0.67
-------------------------	------	-------

1+0

H	5.0	-0.7
L	5.1	-0.8
S	4.9	-0.6
+5	5.2	-0.9

1+21

S-1.0 = 2' 4" Conc Walk	5.21	-0.90
-------------------------	------	-------

1+27

H-0.1 = 2' 3.5" Conc Walk	4.79	-0.98
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1+32

S-1.1 = 2' 8" Conc Walk	5.20	-0.89
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S-19.7 = 2' Garage Conc Floor	5.05	-0.79
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431

1+49

-10	5.8	-1.5
S	5.3	-1.0
L	5.3	-1.0
H	5.2	-0.9

+0.1 = 2' 3" Conc Walk	5.36	-1.05
------------------------	------	-------

1+68 = W End 4' Conc Walk on H

H-0.1 = W End 4' Conc Walk	4.98	-0.67
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1+95

S-0.9 = W 1/4 Conc Slab	5.57	-1.26
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2+0

-0.1 = S 1/4 Conc Walk	5.03	-0.72
------------------------	------	-------

H	5.5	-1.2
---	-----	------

L	5.1	-0.8
---	-----	------

S	5.6	-1.3
---	-----	------

+0.9 = W 1/4 Conc Slab	5.56	-1.25
------------------------	------	-------

2+23

-0.8 = E 1/4 Conc Slab	5.56	-1.25
------------------------	------	-------

S	5.6	-1.3
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431

433

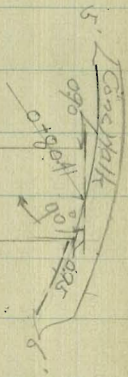
Z	5.2	-0.9
H	5.3	-1.0
+0.2 - 5/4 Conc Walk	5.09	-0.78
2 + <sup>57.90</sup> 59.02 = H.L. Bayside Lane		
-0.2 - 5/4 Conc Walk	5.10	-0.79
H	5.4	-1.1
Z	5.2	-0.9
S	5.2	-0.9
0+0 FL Bayside Lane		
S	5.1	-0.8
Z	5.1	-0.8
H	5.3	-1.0
0+02		
S -0.5 = 1/2 4' Conc Walk	4.98	-0.67
TP	5.20	4.33
5.18	-0.87	
0+34		
H	5.2	-0.9
Z	5.0	-0.7
S	5.3	-1.0

+0.7 - 1/10 Conc Drive Solid	5.35	-1.02
+7.2 07 " "	5.46	-1.13
0+60		
S	4.9	-0.6
Z	4.8	-0.5
H	5.0	-0.7
0+ <sup>80.41</sup> 79.3 = H.L. 5' Conc Walk Bayside Walk		
H = H.L. Conc Walk	4.81	-0.98
Z 0.7 " "	4.78	-0.95
S " " "	4.78	-0.45

Mission Blvd

Santa Clara

Bayside Lane



NWly Curb Line Levels on  
Nashville NE ly to SD River

67

Moore  
2-1-41

5.65

				Nashville	T.P.	6.56	4.84	5.37	0.28
Sw 66	6.80	5.45	-1.15	Lapwai	7+50			7.1	-0.3
				Sec P 48	8			5.2	1.6
10 + 0					+15	old river overflow		8.3	-1.46
+50			6.0		+25	Channel		8.2	-1.4
1			5.7		+50			6.6	0.2
+50			5.9		9			5.0	1.8
2			5.6		+50			5.3	1.5
+50			5.6		10			5.3	1.5
3			5.3		+50			5.2	1.6
+35 = sly Curb on King +50			4.9		11			4.8	2.0
4			5.1		+50			5.1	1.7
+50			4.1		12			4.9	1.9
5			3.1		+50			5.3	1.5
+50			2.8		+65	overflow		7.6	-0.8
6			2.6		+70	Channel		7.4	-0.6
+50			2.5		13			5.1	1.7
+80			0.0		T.P.	5.00	6.94	4.90	1.94
7			2.9		+50			5.0	1.9

69v

14		5.3	1.6
+50		5.0	1.9
15		4.8	2.1
+50		5.0	1.9
16	overflow	6.0	0.9
+10	channel	6.0	0.9
+50		5.2	1.7
17		5.5	1.4
+50		5.1	1.8
18		5.5	1.4
+50		5.2	1.7
19		5.5	1.4
+25		6.8	0.1
+40		9.8	-2.9
+75		9.2	-2.3
+85	Swly S.D. River BANK	12.2	-5.26

Highest Tide mark

8.1

-1.14

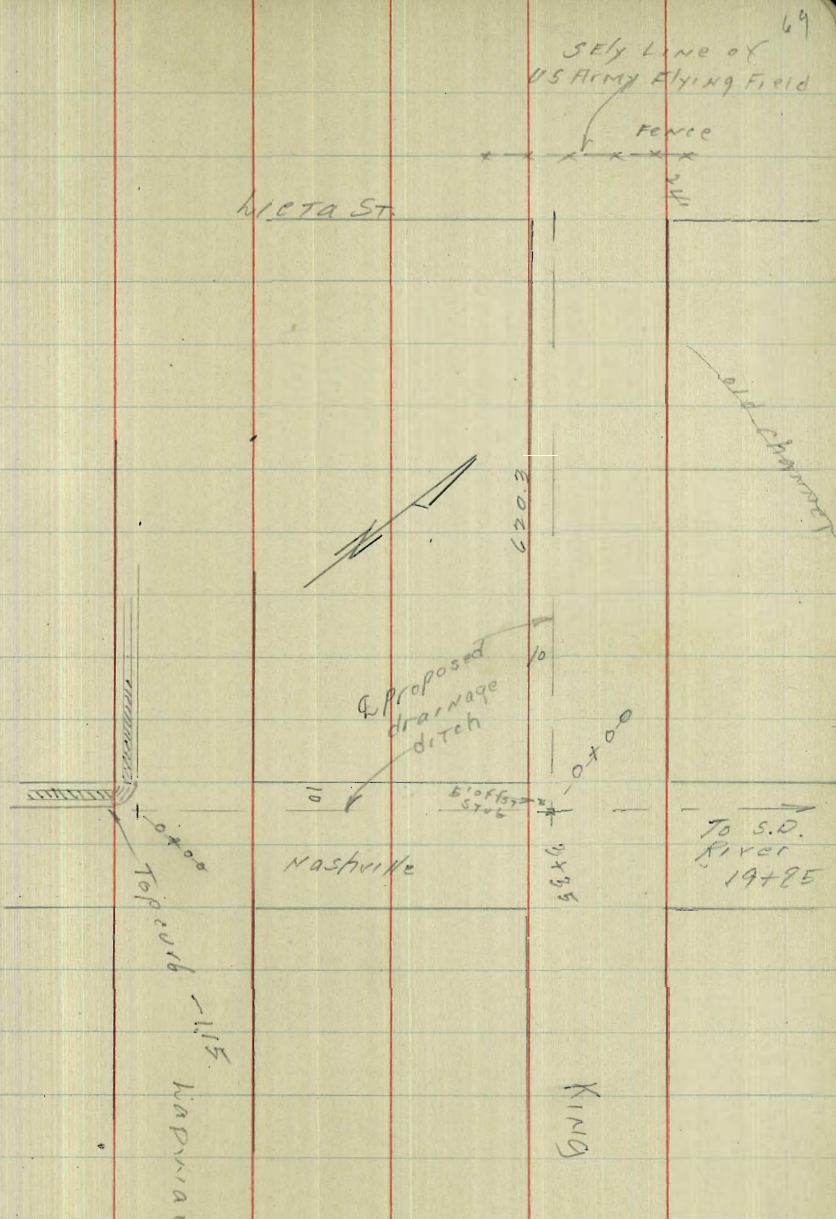
$$\begin{array}{r} 9.01 \\ -1.16 \\ \hline 7.85 \end{array}$$

Tide Book

68

Levels on Sly curb line  
King St to Lieta  
Prop.

Top curb	6.33	5.18	-1.15	Nashville Lapwai
0 + 00 on 5' offset stub	4.66	0.52		
+ 65 "	4.19	1.99		
1 + 15 "	4.16	1.02		
+ 65 "	4.39	0.79		
2 + 15 "	4.60	0.58		
+ 65 "	4.65	0.53		
3 + 15 "	4.40	0.78		
+ 65 "	4.78	0.40		
4 + 15 "	4.91	0.27		
+ 65 "	4.62	0.56		
5 + 15 "	5.30	-0.12		
+ 65 "	5.27	-0.09		
6 + 30.3 S.E. corner Lieta St.	5.08	0.10		
6 + 55.3 Pueblo levee	5.3	-0.12		
7 + 55.3 on Fly Field	5.7	-0.52		
70' RT of 5+15 old overflow channel	6.7	-1.52		





The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page is divided into two columns by a vertical red margin line. The right page has the number '70' written in the top right corner. The notebook is placed on a white surface, and the binding is visible in the center crease.





201.11  
140.00  
341.12  
338.12

259.02  
79.3  
16.3  
354.2

CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.23
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if  $w = 16.2$  and  $h = 5.3$ , cu. yds.  $= 1.48 + .028 + .089 = 1.597$  cu. yds. or practically 160 cu. yds. per 100 ft. If  $w$  exceeds 40 ft., use one half and multiply result by 2, if both  $w$  and  $h$  are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills)  $= h$ , and  $\frac{1}{2}$  the roadbed  $= w$ , add the triangles formed by taking the distance out to each break in turn ( $= w$ 's) by the difference between the cuts (or fills) on each side of it ( $= h$ 's) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

29.5  
36.5  
43.5  
50

485  
9.01  
1386  
6.86  
7.86  
39

1125

3