

ENGINEERS'

FIELD BOOK

NO. 410

MEER

FB 598

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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9° 02' 30"

F.B. 598

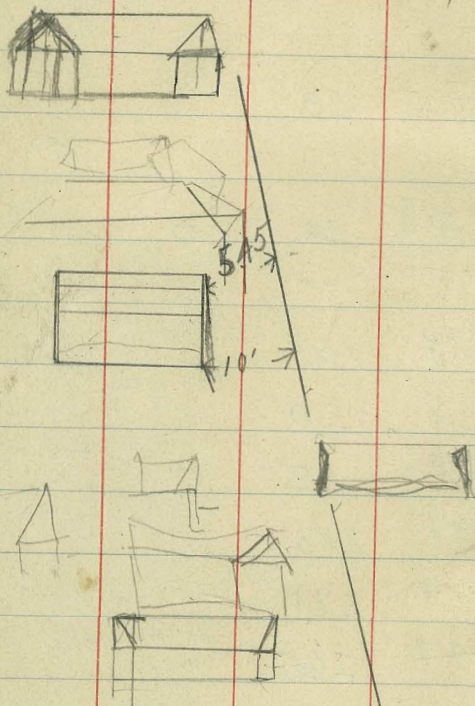
Ford Mileage.

City Ford License #

Eng #

Date	Day	Speedometer Reading	Gas.	Oil-
April				
29		58		
May				
1	28	86	8	
2		—		
3	19	105		
4	15	120		
5	62	182	8	
6	31	213		
7	8	221		
8	47	268		
9	34	302	5	
10	25	327		
11	13	340	9	
12	33	373		

Sta	+	HI	-	EL. SUR.
5.78		79.93		74.15
			135	78.58
			5.2	74.73
			6.7	73.23



Date	Hubometer Record		Gas	Oil
	A.M. Hubometer	P.M.		
1001	09	9		
2	9	35		
3	41	67		
5	75	97		
6	99	147		
7	149	193		
8	199	233		
9	243	—		
10	287	312		To Police 2:00 P.M.
12	343	368		
13	368	397		
14	406	427		
15	433	467		Election
16	473	517		✓
17	522	553		To Police 2:00 P.M.
19	575	625		Election.
20	625	647		
21	650	671		
22	697	716		
23	720	741		

Hubometer
Record-

Date A.M. P.M.

June

24 766 795

26 831 889

27 895 934

28 941 967

29 980

5:00 P.M.
Police

July

July A.M. P.M. Gas Oil

1

2

3

4

5

6

7

8

9

10

11

12

13

14

15

16

17

18

19

July	A.M.	P.M.	Gas	Oil.
------	------	------	-----	------

20

21

1qt

22

23

9038

24

2150

129

~~77.48~~

25

12900

Hubometer
Record
August A.M. - P.M.

6

1		
2		
3		
4		
5		
6		
7		
8		
9	1	17
10	17	31
11	31	40
12	40	61
13		
14	61	78
15	78	93
16	93	101
17	101	120
18	120	141
19	141	167

Hubometer
Record
August A.M. P.M.

oil

7

20

21 167 175

22 175 196

23 196 217

24 217 237

25 237 258

26 258 272

27

28 272 290

1 qt.

29 290 308

30 290 308

31 308 328

Hubometer
Record

8

Sept.

1 328 358

2 358 370

3

4

5 370 381

6 381 402

7 402 421

8 421 442

194

9 442 445

10

11 445 464

12 464 484

13 484 502

14 502 521

15 521 536

16 536 558

18 558 578

Hobometer
Record

oil

9

Sept

19	578	601
20	601	622
21	622	638
22	638	656
23	656	672
24	672	676
25	676	702
26	702	720
27	720	738
28	738	753
29	753	772
30	772	791

1 qt.

battery tested
No. 1 dry cells
1/250

October	Hubometer Record		oil
	A.M.	P.M.	
1			
2	791	806	
3	806	830	
4	830	862	
5	862	878	
6	878	892	
7	892	912	
8			
9	912	928	1 qt
10	928	954	
11	954	976	
12	976	992	
13	992	1012	
14	1012	1029	
15	1029	1048	
16	1048	1064	
17	1064	1076	
18	1076	1100	
19	1100	1117	

Battery tested
No. dry others
1225

October	Hobometer Record		oil	Remarks.
	A.M.	P.M.		
20	11.17	1132	1 qt	
21	1132	1154		
22	1154	1167		
23	1167	1182		
24	1182	1197		2 R.C. Tires on Rear at 1182
25	1197	1215		
26	1215	1232		
27	1232	1254		bands tightened
28	1254	1282		
29	1282	1282		Elev
30	1282	1297		Elev Elev
31	1297	1308		ELV
		EI		ELV.

426
194
238

4
2700
16200
9038
1620
810474.8
7418
589

Sta	+ 10 HI	-	EI pipe	EL 11 Surface
	2.24	93.01		90.77
1300	92	760	82.58	85.41
Well	$\frac{6241}{15441}$	10.	82.58	83.01
II	80	8.3		84.71
	70			
	266	880	4.8	88.21
	176.6			
	58000	878	-	81.38
1450	89.56	87.56	3.0	90.01
1400		87.56	2.82	90.19
	4.70	92.32		87.62
			6.57	85.75
30.75	$\frac{18150}{900}$	13.23	6.66	7209
	2200			7193
	6			.6
	13200		90.58	
			13.2	
	91.64		76.18	
	116		80.04	
	13.2		78.44	
84.96	2.89		82.07	
	1240		720.6	

Nov.	Hubometer Record		oil	HT.	+	-	EI.
	A.M.	P.M.					
1	1308	1325		84.96			
2	1325	1337	31.56	82.27	10.27		72.00
3	1337	1354	<u>6</u>			4.86	77.41
4	1354	1376	18.936			7.5	74.77
5			90.38				
6	1376	1399	<u>18.94</u>				
7	1399	1427	51.44				
8	1427	1446	77.41				
9	1446	1462	<u>71.44</u>				
10	1462	1480	5.97				
11	1480	1487					
12	1487	1494					
13	1494	1508					
14	1508	1527					
15	1527	1532					
16	1532	1536					
17	1538	1546					
18	1546	1551					
19	1551	1554					

Nov.	Hubometer Record		oil	H.I.	+	-	EL PIPE	EL
	A.M.	P.M.						13
20	1554			82.27				
21	1563			30+70		2.85	71.96	79.42
22	1581			30+85		1.92	71.87	80.35
23	1595			31+00	37195	0.95	71.78	81.32
24	1604		3070	31+15	37195	1.49	71.69	80.78
25	1621	gas 5 gal	15.20	31+30	356 37195	2.08	71.60	80.19
26			9038	31+45	356.98 356	4.60		77.67
27	1630		18.22 71.96	31+55	3356.98 356.98	2.34		69.93
28	1641		15	T.P.	7.043	1.12	12.96	69.31
29		31.45	0.96	31+65		7.02		63.41
30		6 18.970	9038 18.87	31+75		11.67		58.76
		77.67	77.51	31+85		15.4		55.03
		71.37		32+00		15.8		54.63
		6.16		32+15		16.1		54.33
	3300	90.38		32+30		16.8		53.63
	19800	19.8		32+40		17.6		52.83
		70.58		32+50		12.4		58.03
		12		32+60		9.0		61.43
		48.78		32+70		6.0		64.43
				32+80		3.4		67.03

Dec	Hobometer Record FM		4900 6
1	16.57	29400	
2	16.65	9038 29.4	
3		6098	
4	16.92	5400	
5	17.21	32400	6912
6	17.35	9038 32.4	6098
7	17.52	5798	8.14
8	17.61	5400 8.06	6520 5978
9		32400	5.42
10	17.78	9038 32.4	
11	18.09	5798	4.87
12	18.21	6930	6.47
13	18.39	5798	
14	18.53	11.32	
15	18.60	5100 6	
16	—	30626	
17	18.68	9038 30.6	6427 5978
18	18.74	5798	4.47
19	18.90		

Sta	+	HT	-	EI PPO	E _L Surface
32+90	1770	70.43	0.24		70.19
T.P.	1296	83.15	0.24		70.19
T.D.	933	81.33	11.15		72.00
54+00		76.07	6.70		69.30
			11.80		64.27
			6.95		69.12
51+00		73.40	8.20	59.78	65.20
	9000 6		350	60.38	69.90
	54000		6.35	62.8	67.05
	9038		4.15	62.78	69.25
	54		6.70		
	9800 6		90.38		
58800			5.88		
			31.58		

Dec

20 1914

4450
6

21 1922

26700 75.16

22 1932

~~7038~~
26700 63.68

23 1943

63.68 11.48

24 1958

75.16
4.00

25 —

7094

26 —

63.68

6729

63.28

3.91

27 1964

6846

6338

5.08

75.15 75.15

850 133

66.35 61.85

6318 2.13

3.17 75.16

1020 98

6416 67.35

6398 63.98

.48 3.37

4600 9.38

27660 62.78

7266 8318

6278 7278

9.78 9.53

8.38 62

Sta

+

H.E.

-

7.16 75.16

6.70

7.87

2.85

2.5

3

7.3

15
E1 surface

68.00

68.46

67.29

~~7231~~

7246

71.16

67.86

9800

6

58.800

9038

58.8

3158

10000

6

60000

7500

6

57060

1923

Oct.

H₂O
Reaching.

10

6847

11

6853

12

6859

13

6861

15

6868

16

6885

17

6904

18

6926

19

6946

20

6956

21

6965

Location.
MISSION VALLEY SEWERS

Sta.

16+86 A R 9° 19'

14+83 A L 15° 08'

13+55 A R 14° 43' 30"

12+54.76 O P.O.T.

11+14.81 A L 6° 31' 30"

8+07.66 A R 10° 10' 30"

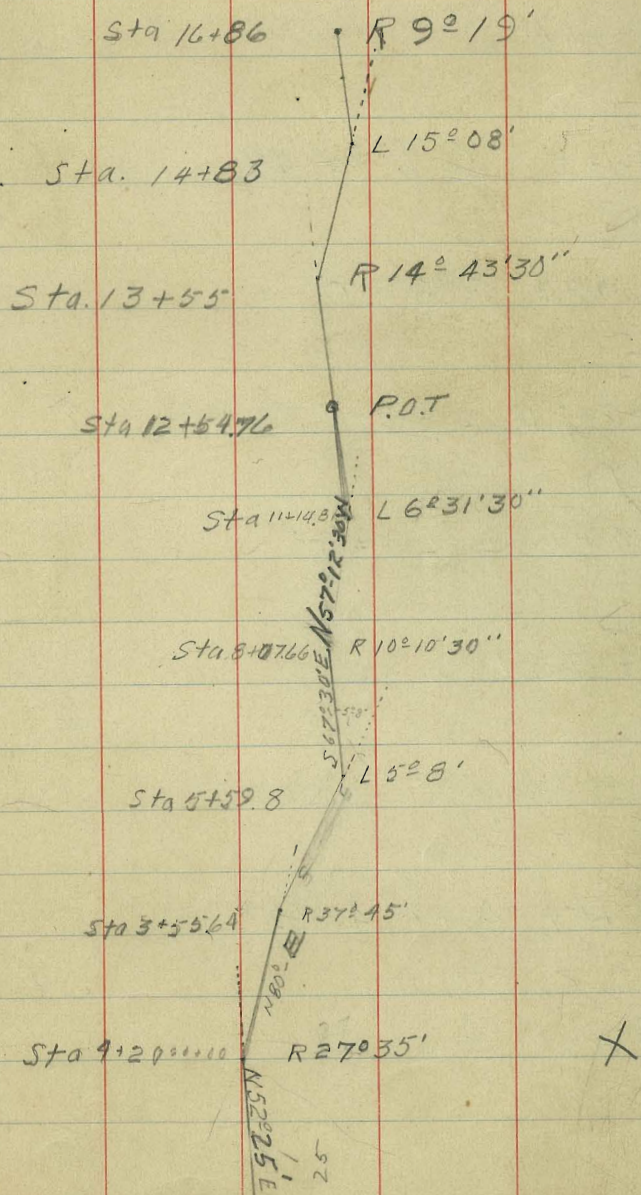
5+59.8 A L 5° 8'

3+55.64 A R 37° 45'

Sta 4+20=

0+00 A R 25° 35'

21



Sta

31+46 Δ R 76°3'

30+56 Δ L 74°49'

30+01.1 ○ P.O.T

27+20 Δ R 9°8'30"

24+90 Δ L 9°2'

23+45.51 ○ P.O.T

21+02.45 Δ L 9°36'30"

19+54 Δ L 40°22'

18+20 Δ L 17°10'30"

Sta. 31+46 R 76°3'

Sta. 30+56 L 74°49'

Sta. 30+01.1 ○ P.O.T

Sta 27+20

R 9°8'30"

Sta. 24+90

L 9°02'00"

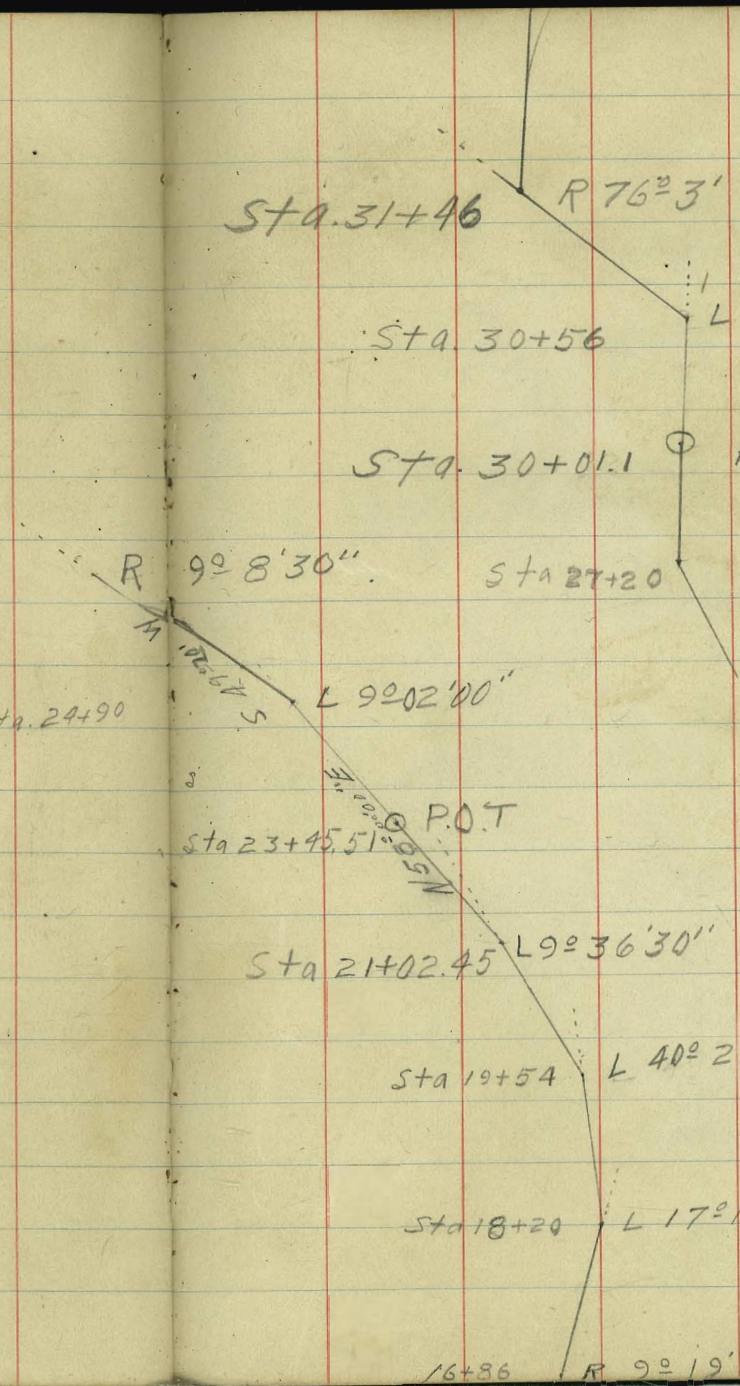
Sta 23+45.51 ○ P.O.T

Sta 21+02.45 L 9°36'30"

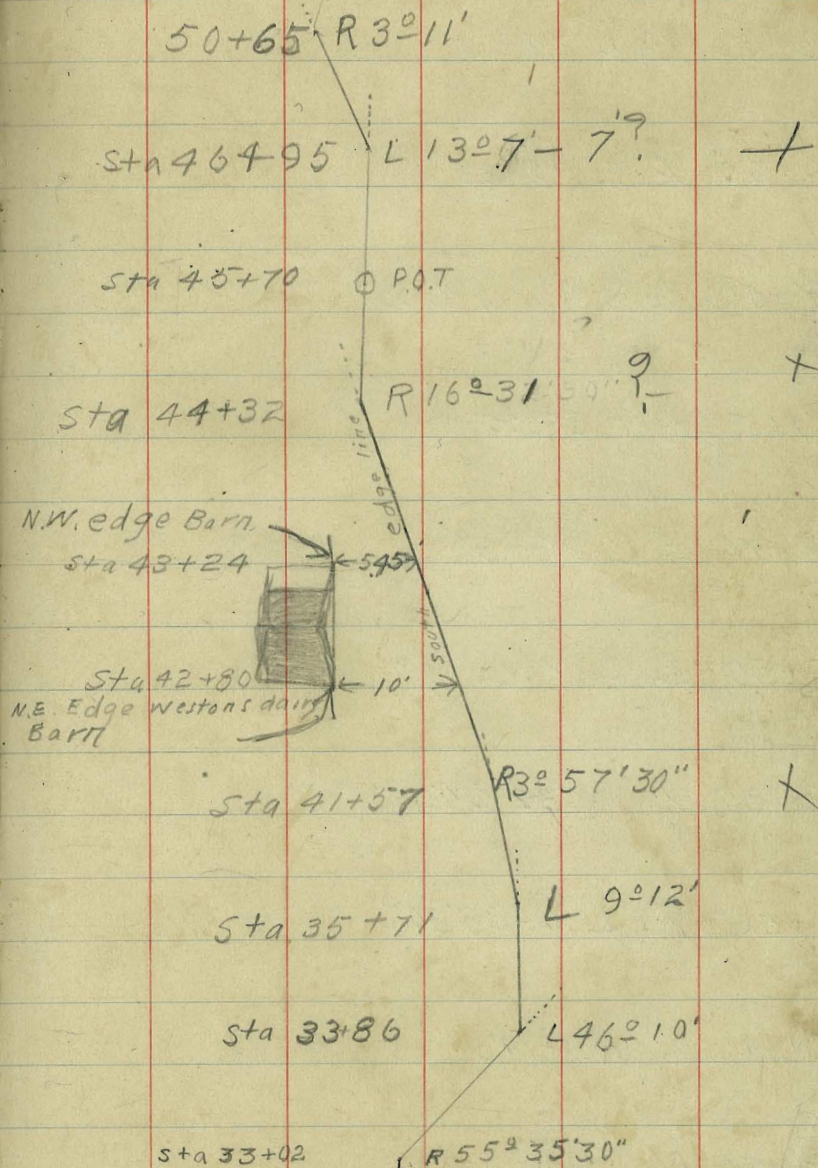
Sta 19+54 L 40°22'

Sta 18+20 L 17°10'30"

16+86 R 9°19'



sta
 50+65 Δ R $3^{\circ}11'$
 46+95 Δ L $13^{\circ}7'$
 45+70 \odot P.O.T
 44+32 Δ R $16^{\circ}31'$
 41+57 Δ R $3^{\circ}57'30''$
 35+71 Δ L $9^{\circ}12'$
 33+86 Δ L $46^{\circ}10'$
 33+02 Δ R $55^{\circ}35'30''$



85+50 Δ L $24^{\circ}21'$ 79+60 Δ L $49^{\circ}33'$ 77+00 Δ R $46^{\circ}54'30''$ 74+15 Δ R $39^{\circ}55'$ 70+70 Δ L $23^{\circ}9'$ 65+50 Δ L $18^{\circ}12'30''$ 62+85 Δ R $32^{\circ}56'30''$ 60+50 Δ L $6^{\circ}38'30''$ 57+00 Δ R $10^{\circ}14'30''$ 53+70 Δ L $9^{\circ}56'30''$

Sta 85+50

L $24^{\circ}21'$

Sta 79+60

L $49^{\circ}33'$

Sta 77+00

R $46^{\circ}54'30''$

Sta 74+15

R $39^{\circ}55'$

Sta 70+70

L $23^{\circ}9'$

65+50

L $18^{\circ}12'30''$

Sta 62+85

R $32^{\circ}56'30''$

Sta 60+50

Sta 60+50

L $6^{\circ}38'30''$

57+00

R $10^{\circ}14'30''$

53+70

L $9^{\circ}56'30''$

111+10 $\Delta L 4^{\circ} 8'$

108+40 ΔR

105+30 $\Delta L 14^{\circ} 34' 30''$

103+20 $\Delta R 13^{\circ} 24' 30''$

100+15 $\Delta L 12^{\circ} 42' 30''$

97+00 $\Delta R 12^{\circ} 58'$

94+55 $\Delta L 7^{\circ} 37'$

92+62.41 $\Delta L 5^{\circ}$

89+76.6 $\odot P.O.T$

88+80 $\Delta R 13^{\circ} 9'$

Sta 111+10 $L 4^{\circ} 8'$

Sta 108+40 $R 37^{\circ} 28'$

105+30 $L 14^{\circ} 34' 30''$

103+20 $R 13^{\circ} 24' 30''$

Sta 100+15 $L 12^{\circ} 42' 30''$

97+00 $R 12^{\circ} 58'$

Sta 94+55 $L 7^{\circ} 37'$

92+62.41 $L 5^{\circ}$

89+76.6 $\odot P.O.T$

Sta 88+80 $R 13^{\circ} 9'$

125+69.7 ⊙ P.O.T

124+30 Δ L 12° 58'

121+90 Δ L 5° 42'

119+62 Δ L 46° 37' 30"

118+50 ⊙ P.O.T

116+63 Δ R 142° 11'

114+62 Δ L 86° 14'

114+45 ⊙ P.O.T

112+98 Δ L 20° 52'

112+59.19 ⊙ P.O.T

127+44.50 nail on edge of road

127+00 End of line

125+69.7 ⊙ P.O.T

124+30 L 12° 58'

121+90 L 5° 42'

119+62 L 46° 37' 30"

118+50 ⊙ P.O.T

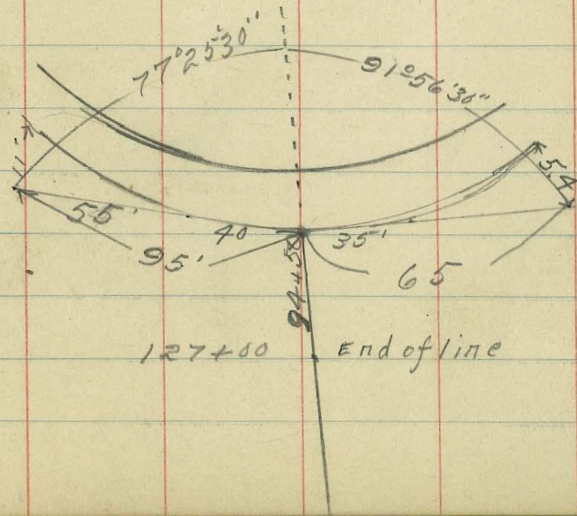
116+63 R 142° 11'

114+62 L 86° 14'

114+45 ⊙ P.O.T

Sta 112+98 L 20° 52'

112+59.19 ⊙ P.O.T



2704

~~1822~~

882

4590

4368

~~222~~

Sta	+	H1	-	E1
B.M. ^{road} on huben	6.37	50.05		43.68
T.P.	1.78	51.62	0.21	49.84
T.P.	2.70	42.60	11.72	39.90
T.P.	3.54	39.54	6.60	36.00
T.P.	3.17	36.50	6.21	33.33
			8.37	28.13
T.P.	7.57	36.20	7.87	28.63
T.P.	6.68	31.46	11.42	24.78
T.P.	7.11	27.04	11.53	19.93
	450	48.18		43.68
			4.84	43.34
	3.68	51.15	0.71	47.47
	6.93	50.61		43.68
			4.69	45.92

23
allens
Dairy
on rock
North of
chicken houses
on hub
west of 2nd
old house
at sta
100+15

on top
of house
by cor of house
at sta 114+62
at sta
119+62

Indexed
C.S.K.

XSEC Alley 30' wide
Bik & Center Addr. to La Jolla Park

Virginia

Way

Moore
5-29-37
30

SEBR 3.47 118.64 115.17 Pearl & Girard

T.P. 8.23 125.75 117 117.54

0-17 edge corr. gut.

W 5.89 119.86

E 5.07 120.68

0-14 N cb line Pearl

E 5.37 120.38

W 4.14 119.61

0-13 inside edge corr. gut

W TOP cb 5.16 120.59

W 6.04 119.71

C 5.60 120.15

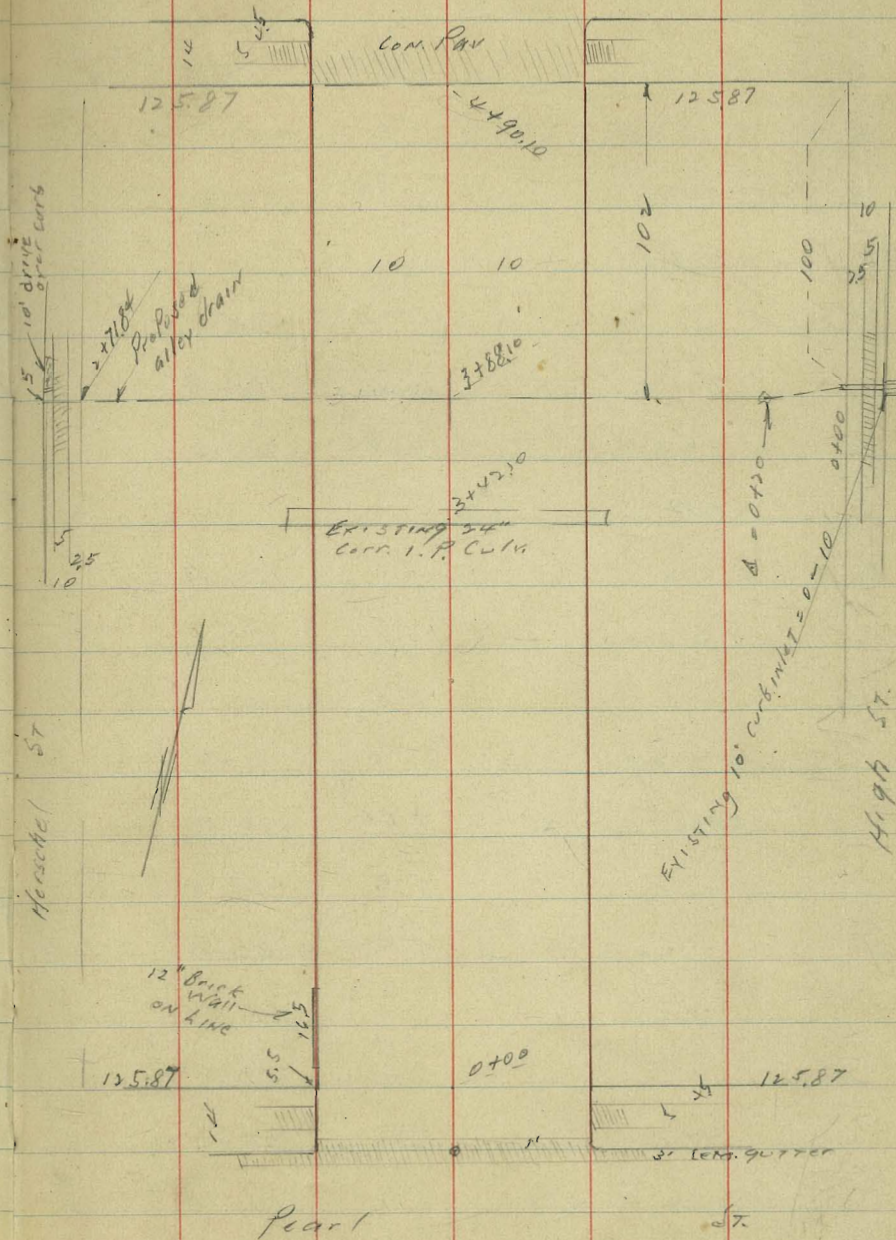
E 5.22 120.53

E TOP cb 4.34 121.41

0+00

E TOP alley cb return 4.16 121.59

E dirt 4.9 120.9



125.75

C	dirt	5.3	120.5
W		5.1	120.7
W	TOP curb	4.90	120.85
	0+05.5		
W		5.0	120.8
C		5.2	120.6
E		4.8	121.0
	0+12.5		
E		5.1	120.7
C		5.3	120.5
W		5.5	120.3
	0+26		
W	S. edge Cem. apron	5.66	120.09
C		5.3	120.5
E		5.4	120.4
	0+39		
E		5.6	120.2
C		5.8	120.0
W	N edge Cem apron	5.91	119.84
	+2.5' Sin 90° Cem.	5.70	120.05

125.75

	0+45		
W	E 5' Cem. walk	6.94	118.81
C		7.1	118.7
E		6.8	119.0
	1+05		
	-10 E Sin 90° Cem.	7.65	118.10
	-7 " Cem apron	7.92	117.83
E		8.8	117.0
C		9.1	116.7
W		9.2	116.6
	T.P.	3.07	118.99
		9.83	115.94
	1+60		
	-7.5 S. end do. 90° Cem.	4.02	114.97
W		3.8	115.2
C		3.9	115.1
E		3.7	115.3

118.99

1+67

E	4.1	114.9
+8	4.6	114.4
C	4.6	114.4

+7.4	Con. gus of Per wall	4.4	114.53
------	----------------------	-----	--------

+7.2	Top end wall	3.7	115.27
------	--------------	-----	--------

W	gus	4.3	114.56
+7.5	"	4.35	114.64
+7.5	N end do. gar cem	4.11	114.88

1+75

W 10' Larch fence 1.3 in alley

1+85

W	5.5	113.5
---	-----	-------

C	5.5	113.5
---	-----	-------

E	fence .3 in alley	5.4	113.6
---	-------------------	-----	-------

2+00

E	5.5	113.5
---	-----	-------

+4	6.0	113.0
----	-----	-------

C	6.0	113.0
---	-----	-------

W	4.3	112.7
---	-----	-------

118.99

2+45

W	7.4	111.6
---	-----	-------

C	7.3	111.7
---	-----	-------

E	7.3	111.7
---	-----	-------

+8.5	S.W. gar. dirt	7.2	111.8
------	----------------	-----	-------

2+54

-8.5	S.W. gar. dirt	7.4	111.4
------	----------------	-----	-------

E	7.8	111.2
---	-----	-------

C	7.8	111.2
---	-----	-------

W	7.9	111.1
---	-----	-------

2+90

-10	9.8	109.2
-----	-----	-------

W	9.4	109.4
---	-----	-------

C	S.M.H. P.M.	9.4	109.57
---	-------------	-----	--------

+8	9.4	109.6
----	-----	-------

E	8.4	110.6
---	-----	-------

+10	8.0	111.0
-----	-----	-------

T.P.	8.04	117.62	9.41	109.58
------	------	--------	------	--------

		117.64	
3+42			
-10		10.2	107.4
-3	F.L. 24" I.P. CULV.	10.58	107.04
-3	TOP PIPE	8.58	109.04
E		8.6	109.0
C		8.7	108.9
+3		8.8	108.8
+7.5	F.L. OUTLET 24" PIPE	11.42	106.20
W		11.5	106.1
+10		11.7	106.4
3+60			
-10		11.8	105.8
W		11.6	106.0
+3		11.3	106.3
+7		8.8	108.8
C		8.6	109.0
E		8.3	109.3
+5		9.8	107.8
+10		9.8	107.8

		117.62		
3+8810 for drain levels				
0+10	W. CB High St.	2.99	114.63	E. INLET 10' curb inlet.
	gUT ON IRON GRATE	3.99	113.63	
	Bot. Box F.L.	7.50	110.12	
0+00	W.L. High St.	7.78	109.84	Ft. 24" CON. PIPE OUTLET
0+3		6.5	111.1	
0+20	= Δ Pt. CULV.	2.3	115.3	
0+50		2.6	115.0	
0+60		4.7	112.9	
0+90		6.0	111.6	
1+25.87	= EL. Alley	7.9	109.7	
1+35.87	E "	8.2	109.2	
1+41		8.4	109.2	
1+45.87	W.L. "	9.5	108.1	
1+75		12.3	105.3	
2+00		13.0	104.6	
2+40		12.9	104.7	
2+71.84	EL. Herschel	12.9	104.7	
2+81.84	TOP curb	12.81	104.81	E. curb Herschel
" "	gUT. Pav.	13.32	104.28	

117.62

	4+10		
- 10		9.4	108.0
W		8.4	109.2
C		8.0	109.6
E		7.4	110.0
+5		5.8	111.8

4+50

- 5		5.2	112.4
E		7.5	110.1
C		7.4	110.0
+4		7.9	109.7
+6		7.0	110.6
W		7.4	110.2
+5		8.0	109.6

4+75

W		7.8	109.8
+4		8.0	109.6
C		7.8	109.8
E		7.4	110.4

117.62

E +5		5.3	112.3
4+90.1	S.L. Virginia Way		
E TOP curb		7.10	110.52
E Pav		7.43	110.19
C "		8.14	109.48
W "		8.34	109.28
W cb TOP		8.24	109.36

S.L. +14 = S. cb. Virginia Way

W Pav cur		8.88	108.74	
E " "		7.87	109.75	
T.P.	861	119.19	7.04	110.58
check to orig. B.M.	401		115.18	115.17

6-26-39
Miller
Walker
Blinn

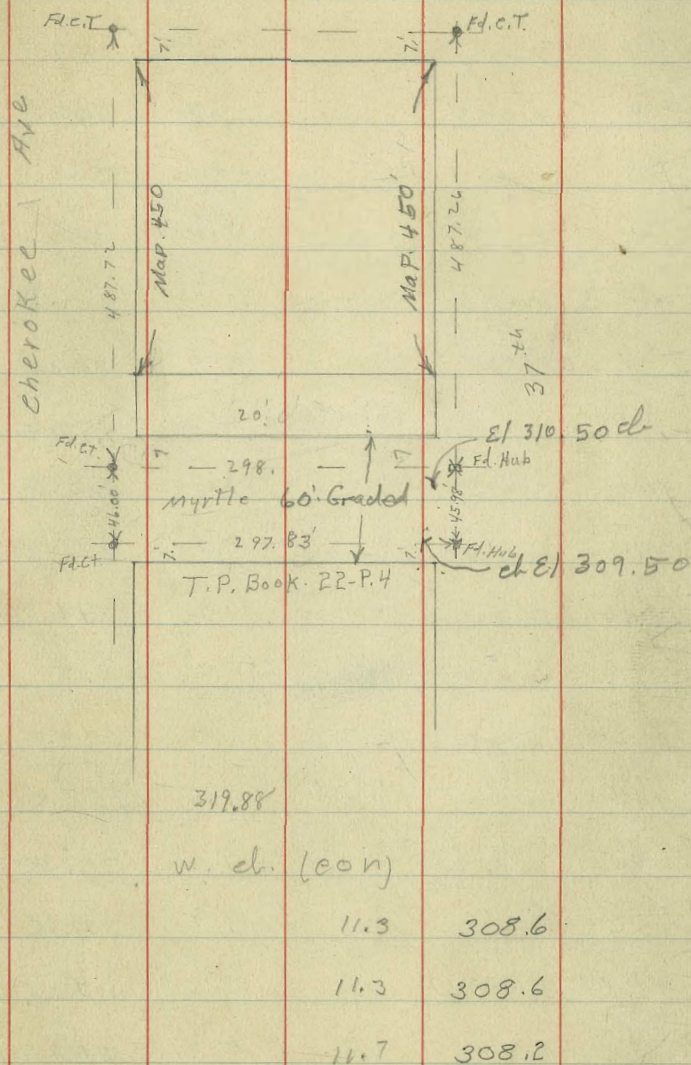
X. Sec. Myrtle Ave Cherokee to 37th
Graded 60' wide from S. line
60' wide 10' elev. 10' 11/2

B.M.	0.40	320.39		319.99	N.W. Dwight + 37 th
T.P. B.M. BP	9.13	319.88	9.64	310.75	N.W. 37 th + Myrtle 310.74 B.M. Book
					80' N. of S. Line Myrtle
W. conc. db.	37 th		8.91	310.97	
E " " 37 th			9.30	310.58	
					60' N. of S. Line Myrtle
C. conc. db.	S. End.		9.68	310.20	
gutter	par " "		10.28	309.60	
+13 W = 1/4 " " "			9.63	310.25	
+24 = 1/4 " " "			9.35	310.53	
+39 = 1/4 " " "			9.40	310.48	
+52 = gutter " "			10.00	309.88	
concd " "			9.33	310.55	
14' E. of W. line = W. db. line 37 th					
N - 20. Top. db			8.91	310.97	
N. " "			9.33	310.55	
db			10.5	309.4	
1/4			11.2	308.7	
1/4			11.3	308.6	

Indexed
c.s.R.

35

Dwight



319.88

w. db. (con)

114	11.3	308.6
db	11.3	308.6
S	11.7	308.2

319.88

0+00 = W. line 37th

S	10.7	309.2
el	10.4	309.5
+4	10.2	309.7
+5	10.9	309.0
14	10.8	309.1
⊕	10.2	309.7
14	10.0	309.9
+8	10.0	309.9
el	9.4	310.5
N	8.7	311.2
+20	8.2	311.7
0+05. West:		
-20	6.3	313.6
N	7.5	312.4
el	9.0	310.9
+2	9.9	310.0
14	9.8	310.1
⊕	10.0	309.9
14	10.4	309.3

319.88

Myrtle

36

+3	10.9	309.0
+5	10.2	309.7
el	10.3	309.6
S	10.5	309.4
0+50 W.		
S	10.2	309.7
el	9.5	310.4
+5	9.4	310.5
+7	10.0	309.9
14	9.8	310.1
⊕	9.5	310.4
14	9.0	310.9
el	9.0	310.9
+2	8.3	311.6
N	7.9	312.0
+20	6.5	313.4
1+00		
-20	5.8	314.1
N	7.0	312.9
+8	7.5	312.4

319.88

+100 con

el	8.3	311.6
1/4	8.2	311.7
1/2	8.4	311.5
3/4	8.7	311.2
+3	9.0	310.9
+5	8.5	311.4
el	8.5	311.4
S	9.1	310.8
	+59' W. = E. End. Conc. Walk. on S.	
S	7.2	312.7
+3.5 = S. edge conc. walk. E. End.	6.98	312.90
+8.5 = N " " " "	7.02	312.86
el	7.0	312.9
+4 = {N. edge } Edge pole	7.0	312.9
+6	7.5	312.4
1/4	7.2	312.7
1/2	6.9	313.0
3/4	6.8	313.1
el	7.1	312.8

319.88

Myrtle

37

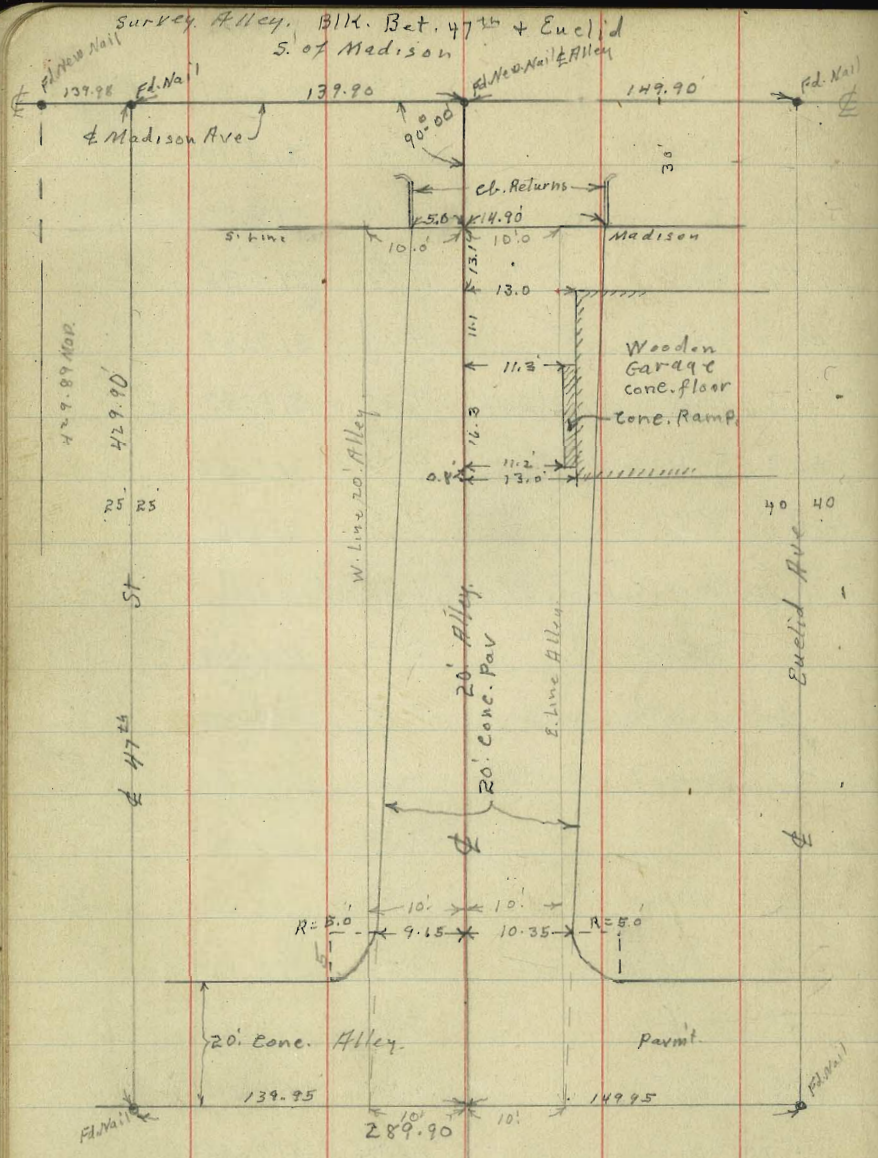
+1	6.6	313.3
N	6.1	313.8
+20	5.0	314.9
	+92' = E. Edge Conc. Drive North of line	
N-20' E. edge drive	3.90	315.98
N-4.0 " " " S. End.	4.37	315.51
	+01' = W. edge above drive	
N-20' W. edge drive	3.92	315.96
N-4.0 " " " S. End.	4.35	315.53
N	5.2	314.7
+9	5.6	314.3
el	6.2	313.7
1/4	6.0	313.9
1/2	6.0	313.9
3/4	6.4	313.5
+8	6.6	313.3
el	6.3	313.6
+1.5 = N. Edge conc. walk	6.32	313.56
+6.5 = S " " "	6.26	313.62
S	5.8	314.1

	319.88		
	2+50 W		
S	5.1	314.8	
+3.5 = S. edge conc. walk.	5.30	314.58	
+8.5 = N " " "	5.31	314.57	
cl	5.4	314.5	
"4	5.2	314.7	
cl	4.8	315.1	
"4	4.7	315.2	
cl	4.7	315.2	
+2	4.0	315.9	
+8	3.8	316.1	
N.	3.2	316.7	
+20	2.1	317.8	
	2+97 ⁸³ W. on S. 7. Line = { E. End. Returns E. Line Cherokee		
N-20	1.8	318.1	
N.	2.7	317.2	
+2.5 = N. Edge conc. walk. E. End.	2.82	317.06	
+7.5 = S. " " " "	3.13	316.75	
cl = E. End. conc. cl	3.26	316.62	
gutter pav. E. End	3.86	316.02	

	319.88	Myrtle	
"4 pav E. End	3.67	316.21	
cl " " "	3.78	316.10	
"4 " " "	4.16	315.72	
gutter " " "	4.93	314.95	
cl = conc. cl. " "	4.34	315.54	
+1.5 = N. Edge conc. walk.	4.35	315.53	
+6.5 = S " " "	4.38	315.50	
E	4.3	315.6	
14' W of E. Line = E. cl. Line Cherokee			
S. pav	5.07	314.81	
cl "	4.74	315.14	
"4 "	4.18	315.70	
cl "	3.86	316.02	
"4 "	3.73	316.15	
cl "	3.58	316.30	
N "	3.45	316.43	
N. cl	2.84	317.04	
+20 cl.	2.42	317.46	
B.M. B.P.	2.65	317.23	N.W Myrtle + Cherokee

7-13-39
miller
Walker

Indexed
C.S.K



X sec. Hilltop Drive
Continued from F.B. 599-P.78.

173.97✓

4+46 = W. Line 44th St. to North

N-100'	2.6	171.4
N.	2.6	171.4
+5	3.9	170.1
eb	3.8	170.2
1/4	3.7	170.3
1/2	2.6	171.4
1/4	3.0	171.0
eb	2.6	171.4
S.	3.3	170.7
+10	3.8	170.2

25' E. of W. = 1/2 44th St

-5	3.2	170.8
S.	2.8	171.2
eb	1.8	172.2
1/4	1.8	172.2
1/2	1.7	172.3
1/4	2.3	171.7

173.97✓

40

eb	2.2	171.5
N	1.3	172.7
+100' N	2.0	172.0
13' E. of 1/2 44 th St. - 24' S. of Hilltop Eucalyptus 4 Trunks 30" Diam		
0+00 = E. Line 44 th St. = 50' E. of W. Line		

N-100	0.8	173.2
N.	0.0	174.0
+3.5 = W. End. Wire Fence.	1.0	173.6
eb.	1.2	172.8
1/4	1.2	172.8
1/2	1.0	173.6
1/4	1.4	172.6
eb	1.4	172.6
+5 = Fence		

S	2.4	171.6
+5	2.4	171.6

0+12 Pepper Tree 4 Trunks 30" Diam 1/2 N. of 1/2.

T.P.	4.73	178.37	0.33	173.64
------	------	--------	------	--------

178.37

0+50 E

S	5.7	172.7
cl	4.8	173.6
"4	4.6	173.8
⊕	4.4	174.0
"4	4.5	173.9
cl	4.3	174.1
+5	4.3	174.1
+6	2.3	176.1
N	2.3	176.1

0+70 - 25' S. of ⊕ Eucalyptus 12" Diam

0+94 10' S of ⊕ 4" Air Valve

1+00

N	2.0	176.4
+4 = Fence	2.0	176.4
+7	4.0	174.4
cl	4.0	174.4
"4	4.2	174.2
⊕	4.0	174.4

178.37

Hill Top Dr

41

"4	4.2	174.2
cl	4.0	174.4
S	4.6	173.8
+5	4.7	173.7

1+08 - 25' S of ⊕ Eucalyptus stump, with 3. Trunks
30" Diam

1+40

-5	4.8	173.6
S	4.7	173.7
cl	4.5	173.9
"4	4.4	174.0
⊕	4.3	174.1
+5	5.1	173.3
"4	5.0	173.4
cl	4.8	173.6
+3	4.8	173.6
+6	2.8	175.6
N	2.8	175.6

1+48 Garage 25' S. of ⊕ dirt floor

floor	5.0	173.4
-------	-----	-------

178.37

1+70

N	5.0	173.4
+4	5.0	173.4
+8	6.4	172.2
cl	6.8	171.6
1/4	7.0	171.4
+7	7.1	171.3
cl	5.8	172.6
1/4	5.5	172.9
cl	5.5	172.9
S	6.2	172.2
	2+00	
S	9.0	169.4
cl	8.0	170.4
1/4	8.1	170.3
cl	8.5	169.9
+3	10.0	168.4
1/4	9.7	168.7
cl	9.6	168.8
+3	9.6	168.8

178.37

Hilltop

42

+7	8.0	170.4
N	8.0	170.4
	2+26 = W. Line Catholic Cemetery	
N	10.2	168.2
+3 = Fence to W	10.2	168.2
+5 " " E	10.6	167.8
+7	11.4	167.0
cl	11.4	167.0
1/4	11.6	166.8
+7	11.6	166.8
cl	10.6	167.8
1/4	10.8	167.6
cl	11.3	167.1
S	11.2	167.2
T.P.	2.06	168.85
	2+65	
-10	6.0	162.9
S	5.5	163.4
cl	4.8	164.1
1/4	4.6	164.3

	168.85		
±		4.2	164.7
1/4		4.2	164.7
cl		4.2	164.7
+5 = Fence	Lawn	3.6	165.3
N	"	3.5	165.4
	3+00		
N	Lawn	5.2	163.7
+5	Fence	5.2	163.7
cl		5.8	163.1
1/4		5.8	163.1
±		5.8	163.1
1/4		6.1	162.8
cl		6.9	162.0
S		7.9	161.0
+10		8.3	160.6
	3+40		
-10		10.5	158.4
S		10.2	158.7
cl		9.2	159.7
1/4		7.5	161.4
±		6.9	162.0

	168.85	Hilltop Dr	43
44		6.8	160.1
cl		6.8	160.1
+5 Fence Line		6.6	160.3
N			
	3+70		
N-10 = Drive Catholic Cemetery		5.8	163.1
N	" " "	6.2	162.7
cl		6.9	162.0
1/4		7.1	161.8
±		7.3	161.6
1/4		7.3	161.6
cl		9.0	159.9
+5 = Fence		11.1	157.8
S		11.5	157.4
+10		12.4	156.5
+60		15.0	153.9
chk. B.M. Porch in Cemetery } See F.B. 599 - P 39		0.30	168.55 = 168.55

X sec. C. St. 42nd to 44th St.
 50' wide - 10' elev. 7.5' 1/4s
 B.M. SPK Pd. 12.50 196.82 184.32

S.W. 42nd
 & C. St.

196.82

44

0+00 = E. Line 42nd St

S	7.8	189.0
dr	6.8	190.0
1/4	5.9	190.9
1/2	5.3	191.5
3/4	5.1	191.7
dr	5.6	191.2
N	5.6	191.2

0+25

N	3.4	193.4
dr	4.1	192.7
1/4	4.1	192.7
1/2	4.3	192.5
3/4	4.8	192.0
dr	6.1	192.7
S	7.5	189.3

0+50

S	6.1	190.7
dr	4.6	192.2

1/4

1/2

3/4

dr

+3

N

T.P.

5.32

200.12

2.02

194.80

1+05

N

+7

dr

1/4

1/2

3/4

dr

S

1.1

199.0

2.0

198.1

3.7

196.4

4.2

195.9

4.6

195.5

5.5

194.6

6.3

193.8

8.2

191.9

200.12

1+50

S	10.5	189.6
+7	9.5	190.6
cl	8.0	192.1
14	7.1	193.0
cl	6.2	193.9
14	5.6	194.5
cl	4.5	195.6
+3	3.0	197.1
N.	1.7	198.4

2+00

N	6.6	193.5
+8	7.7	192.4
cl	8.8	191.3
14	9.3	190.8
cl	9.6	190.5
14	10.6	189.5
cl	12.3	187.8
S	13.8	186.3
+10	14.2	185.9

200.12

2+40

S-10	12.5	187.6
S	11.6	188.5
cl	11.2	188.9
14	13.5	186.6
cl	12.6	187.5
14	12.5	187.6
cl	11.5	188.6
N	10.4	189.7
T.P.	7.96	196.39
11.69		188.43

3+00

N	7.6	188.8
cl	8.5	187.9
14	8.6	187.8
cl	8.9	187.5
14	9.2	187.2
cl	10.0	186.4
S	10.2	186.2
+10	11.1	185.3

e. st.

45

196.39

3+50

-10	11.3	185.1
S	10.6	185.8
cb	10.2	186.2
ly	9.3	187.1
±	9.0	187.4
ly	8.5	187.9
cb	8.2	188.2
N	7.3	189.1

4+00

N	6.9	189.5
cb	7.8	188.6
ly	8.0	188.4
±	8.3	188.1
ly	8.6	187.8
cb	9.2	187.2
S	9.4	187.0
+10	9.8	186.6

4+20 Double Garage on S. conc. Floor 21. Back

S-21 = floor 9.60 186.79

4+40 Double Garage on N. conc. Floor 15.7 Back

N-15.7 floor 4.80 191.59

196.39

4+50

-5	8.3	188.1
S	8.2	188.2
cb	7.8	188.6
ly	7.2	189.2
±	6.8	189.6
ly	6.7	189.7
cb	6.6	189.8
N	6.0	190.4

5+00

N-5	4.4	192.0
N	5.1	191.3
cb	5.4	191.6
ly	5.6	190.8
±	5.8	190.6
ly	6.1	190.3
cb	6.6	189.8
S	7.0	189.4
+5	7.0	189.4

e. st-

46

	5+28	196.39 = W Line	43 rd St. 50' wide	
S-50			9.0 188.4	
S			6.3 190.1	-100'
d			6.0 190.4	S
1/4			5.5 190.9	d
1/4			5.0 191.4	1/4
1/4			4.7 191.7	1/4
d			4.0 192.4	1/4
N			3.7 192.7	d
+15			3.0 193.4	N
		25' E. of W. = E 43 rd St.		
-100'			+1.5 192.9	+15
N			3.4 193.0	
d			4.0 192.4	N
1/4			4.3 192.1	d
1/4			4.8 191.6	1/4
1/4			5.1 191.3	1/4
d			5.5 190.9	1/4
S			5.9 190.5	d
+100			10.3 186.1	S

		196.39	C. St
	0+00 = E. Line 43 rd St.		47
		9.8	186.6
		5.1	191.3
		5.0	191.4
		4.6	191.8
		4.2	192.2
		3.9	192.5
		3.5	192.9
		2.7	193.7
		2.2	194.2
	0+50		
		2.0	194.4
		2.6	193.8
		3.0	193.4
		3.0	193.4
		3.1	193.3
		3.6	192.8
		3.7	192.7

		196.39		
		1+00		
S			3.0	193.4
cl			2.6	193.8
ly			2.3	194.1
ϕ			2.1	194.3
ly			2.1	194.3
cl			1.7	194.7
N			1.1	195.3
set B.M. Spl. Elec. Pole			5.88	190.51
				S.W. 43 ^m + C. Sts
T.P.	1.30	195.58	2.11	194.28
		1+50		
N.			1.2	194.4
cl			1.5	194.1
ly			1.6	194.0
ϕ			1.4	194.2
ly			1.6	194.0
cl			1.9	193.7
S.			1.9	193.2

		195.58		C. St.
		2+00		48
S			2.2	193.4
cl			2.2	193.4
ly			2.1	193.5
ϕ			2.3	193.3
ly			2.6	193.0
cl			2.5	193.1
N			2.3	193.3
		2+50		
N.			4.0	191.6
cl			4.2	191.4
ly			4.2	191.4
ϕ			4.0	191.6
ly			4.0	191.6
d			4.3	191.3
S			4.2	191.4
		2+52		
N.	= S. end RH cone walk		4.04	191.54

		195.58	
		3+00	
S	6.3	189.3	
cl	6.4	189.2	
¹ / ₄	6.0	189.6	
±	6.0	189.6	
¹ / ₄	5.8	189.8	
cl	5.8	189.8	
N	5.6	190.0	

		3+50	
N	7.2'	188.4	
cl	7.6	188.0	
¹ / ₄	8.0	187.6	
±	8.1	182.5	
¹ / ₄	8.1	187.5	
cl	8.3	187.3	
S.	8.6	187.0	

		4+00	
S.	10.4	185.2	
cl	10.2	185.4	
¹ / ₄	9.6	186.0	

		195.58	C. ST.
±	9.5	186.1	49
¹ / ₄	9.5	186.1	
cl	9.1	186.5	
N	8.5	187.1	
		4+45 ² = W. Line 44 th St.	50' wide
-100'	5.4	190.2	
N	9.1	186.5	
cl	9.8	185.8	
¹ / ₄	10.0	185.6	
±	10.3	185.3	
¹ / ₄	10.6	185.0	
cl	11.0	184.6	
S	11.6	184.0	
+50	14.4	180.8	
+100	15.7	179.9	

		25' E = ± 44 th	
S-100'	17.2	178.4	
-50	14.8	180.8	
S	11.8	183.8	
cl	11.1	184.5	
¹ / ₄	10.7	184.9	
±	10.2	185.4	

195.58^v

E. St

± 44th (con)182.96^v

50

1/4	10.1	185.5
cb	9.5	186.2
N	9.0	186.6
+70'	5.4	190.2
+100'	4.8	190.8
E. Line 44 th St.		
-100.	4.7	190.9
N.	8.0	187.4
cb	8.5	187.1
1/4	8.9	186.7
±	9.3	186.3
1/4	9.6	186.0
cb	10.0	185.6
S	10.5	185.1
+50	13.4	182.2
+100	15.0	180.6
B.M. Blk. Cor Hub	9.26	186.32
T.P.	0.08	182.96

N.W. Cor.
44th & E St

182.88

T.P.

2.97

176.54

9.39

173.57

T.P. Page 40 for chK.

2.90

173.64

=173.64^v

$$\begin{array}{r} 86 \\ 6 \\ \hline 576 \\ 88 \\ \hline 604 \end{array}$$

Hilltop to C. Map.

7-21-39

43rd St X Sec.

Hilltop to C.

50' wide 10-0
75' +

B.M. Spk. Pole

190.51

S.W. Cor 43rd
+ C. - Page 48

B.M. Man

11.02

176.27

165.25

S.E. Cor Lot 25
Hortons Purchase

+100 = N. Line Hilltop

N.

9.8

166.5

cb

10.8

165.5

1/4

9.9

166.4

±

9.5

166.8

1/4

9.6

166.2

cb

9.8

166.5

+1

8.6

167.7

E

8.8

167.5

176.27

0+50 N

6.5 169.8

+7 6.5 169.8

el 7.1 169.2

14 6.8 169.5

E 7.0 169.3

14 7.1 169.2

el 6.9 169.4

W 7.4 168.9

out of place for +27 - 16.5' W of E = Pepper Tree 5" Diam

0+48 - 16.5 " " " " 8" "

0+70 16.5 " " " " " "

0+72 Garage on E. conc. floor 15' Back

E. ground 4.9 171.4

E-15 " 5.0 171.3

E-15 floor 4.62 171.65

0+80 = Conc. strip Drive on W.

W. Line 5.83 170.44

10' E. of W. Line = E. End strips 5.60 170.67

0+86 S. End. Picket Fence on W. 4.0 in ST.

0+90 - 16.5' W. of E. Avocado Tree

176.27

1+00 N.

W 4.9 171.4

el 4.6 171.7

14 4.7 171.6

E 4.4 171.9

14 4.1 172.2

el 4.4 171.9

+3 3.2 173.1

E 3.2 173.1

1+15 - 16.5' W. of E = Avocado Tree

E+27 " " " " " "

1+40 " " " " " "

1+50 N

E 1.3 175.0

+7 1.3 175.0

el 2.1 174.2

14 2.1 174.2

E 2.2 174.1

14 2.5 173.8

el 2.5 173.5

W 2.2 174.1

43rd ST.

51

1+55 - 16.5' W of ϕ = Avocado Tree

1+66 - " " " " = " "

2+00 w

w .08 175.5

cb 0.6 175.7

1/4 0.6 175.7

 ϕ 0.3 176.0

1/4 0.2 176.1

cb 0.3 176.0

+1 +0.2 176.5

E +0.3 176.6

T.P. 9.85 185.85 0.27 176.00

2+05 - 16.5' W of ϕ = Avocado Tree

2+22 " " " " " "

2+41 " " " " " "

2+50

E1 8.2 177.7

cb 8.3 177.6

1/4 8.3 177.6

 ϕ 8.4 177.5

1/4 8.7 177.2

cb 8.4 177.3

w 8.6 177.3

2+58 - 16.5' W of ϕ = Avocado Tree

2+70 - " " " " " "

2+84 " " " " " "

2+98 " " " " " "

(N. End Picket Fence on W. 4.0' E. of W. Line
3+00 S. " Eugenia Hedge 18.0' W of ϕ)

w 7.4 178.5

cb 7.1 178.8

1/4 7.0 178.9

 ϕ 6.9 179.0

1/4 6.8 179.1

cb 6.8 179.1

+1 6.3 179.4

E 6.3 179.6

3+28 - N. End above Eugenia Hedge 18.0' W of ϕ 3+44 18.0' W of ϕ Avocado Tree

185.85

3+50 N.

E	4.6	181.3
+9	4.5	181.4
d	5.2	180.7
1/4	5.1	180.8
E	5.3	180.6
1/4	5.2	180.7
d	5.4	180.5
W	5.4	180.5
+5	5.6	180.3

3+61 - 18' W. = Avocado Tree

3+78 - " " = " "

3+95 " " = " "

4+00

W	3.7	182.2
d	3.7	182.2
1/4	3.6	182.3
E	3.6	182.3
1/4	3.5	182.4
d	3.2	182.7
E	2.7	183.2

185.85

43rd St

53

4+12 - 18' W. of E = Avocado Tree

4+50

E	1.1	184.8
d	1.2	184.7
+3	1.9	184.0
1/4	1.8	184.1
E	1.9	184.0
1/4	2.1	183.8
d	2.2	183.7
W	2.3	183.6
+5 in yard	2.4	183.5

T.P. 10.77 195.97 0.65 185.20

5+00

W	10.4	185.6
d	10.3	185.7
1/4	10.2	185.8
E	10.0	186.0
1/4	10.1	185.9
d	9.8	186.2
E	9.4	186.4

195.97

5+50

E	7.2	177.8
ch	7.5	188.5
+3	8.0	188.0
14	7.8	188.2
⊕	7.7	188.3
14	7.9	188.1
ch	8.0	188.0
W	8.0	188.0

5+26 ⊕ 2.8' Walk on W.

7.0' E. of W. Line = E. End. walk. 4.62 189.35

6+04 = S. Line C. St. 50' wide

N	5.8	190.2
ch	5.8	190.2
14	5.6	190.4
⊕	5.4	190.6
14	5.5	190.5
ch	4.6	191.4
E.	4.6	191.4

chk. B.M.

5.46

190.51

S.W. 4/3rd
+ C.

195.97

43 rods

54

5+60 - 17.5' E. of ⊕ Heacia Tree 12" Diam

5+82 - " " " " " 10" "

6+03 - " " " " " 8" "

0+00 = N. Line C. St

⊕	2.2	193.8
ch	2.7	193.3
14	3.1	192.9
⊕	3.0	193.0
14	3.1	192.9
ch	3.1	192.9
W	3.2	192.8

0+13 N - 17.5' E. of ⊕ = Olive Tree

0+29 N - " " " " " "

0+44 N - " " " " " "

0+74 N - " " " " " "

0+37 E.N. - W. of ⊕ = E. End.
conc walk 2.8' wide 1.43 194.54

0+50 N.

W	1.1	194.9
ch	0.6	195.4
14	0.5	195.5
⊕	0.6	195.4
14	0.7	195.3

	195.97		
E. cl	0.6	195.4	
E.	0.3	195.2	
	1+00 N		
E	+1.7	197.6	
cl	+1.6	197.6	
ly	+1.6	197.6	
ϕ	+1.9	197.9	
ly	+2.1	198.1	
cl	+2.0	198.0	
W	+1.5'	197.5	

43rd St 7-21-39 44th St. X Sec. Hill Top 15 E. St. 44th d
 B.M. N. W. B. H. Cor. 5.45 191.77 186.32 e. st/s 55

			100' N. of N. Line - C. St.
W			1.5 190.3
cl			1.4 190.4
ly			1.2 190.6
ϕ			1.0 190.8
ly			1.0 190.8
cl			0.9 190.9
E			0.9 190.9

from 0785 N. of N. Line E. St. to 3+50 S. of

S. Line C. St. = Row Black. Roacia Trees. 17.5' E. of ϕ.

0+50 N. of N. Line - C St

E			2.1 189.7
cl			2.1 189.7
ly			2.5 189.3
ϕ			2.5 189.3
ly			2.8 189.0
cl			3.1 188.7
W			2.8 189.0

191.77	
N. Line	E. St
W	5.4 186.4
cl	5.4 186.4
1/4	5.3 186.5
cl	5.1 186.0
1/4	5.0 186.8
cl	4.1 187.2
E	4.0 187.8

25' S. of N = cl E. St

E	5.3 186.5
cl	5.4 186.0
+3	6.5 185.3
1/4	6.5 185.3
cl	6.4 185.4
1/4	6.5 185.3
cl	6.6 185.2
W	6.5 185.3

0+00 = S. Line E. St

W	7.8 184.0
cl	7.8 184.0

191.77	
1/4	8.2 183.6
cl	7.9 183.9
1/4	7.9 183.9
1/4	7.9 183.9
cl	7.0 184.8
E	6.9 185.0

0+50 S.

E	9.2 182.6
cl	9.5 182.3
+3	10.5 181.3
1/4	10.7 181.1
cl	10.4 181.0
1/4	10.4 181.0
cl	10.8 181.0
W	10.8 181.0

0+98 S.

W = S. edge 9' conc. Drive	ground	11.80	179.97	E. End.
W = N End. cond Wall on W Line		11.60	180.27	

44th St

56

191.77

1500

W		11.9	179.9
ch		12.6	179.2
1/4		13.1	178.2
⊕		13.2	178.6
1/4		13.3	178.5

T.P.	1.95	180.81	12.91	178.86
------	------	--------	-------	--------

+3		2.3	178.5
----	--	-----	-------

ch		1.9	178.9
----	--	-----	-------

E		1.8	179.0
---	--	-----	-------

1+16	- 15.8'	W. of ⊕ = Black. Acacia Tree
------	---------	------------------------------

1+27	" " " "	" " "
------	---------	-------

1+37	S. End.	above wall on wall line
------	---------	-------------------------

W. ground		3.0	177.8
-----------	--	-----	-------

W Top. wall		0.57	180.24
-------------	--	------	--------

1+40	15.8'	W. of ⊕ = Black. Acacia Tree
------	-------	------------------------------

1+52	" " " "	" " "
------	---------	-------

1+67	" " " "	" " "
------	---------	-------

180.81

1+50

E.		4.0	176.8
ch		3.9	176.9
1/4		4.2	176.6
⊕		4.2	176.6
1/4		4.0	176.8
ch		3.9	176.9
W		3.8	177.0
+5		3.8	177.0

2+00

-5		5.3	175.5
----	--	-----	-------

W		5.3	175.5
---	--	-----	-------

ch		5.7	175.1
----	--	-----	-------

1/4		5.8	175.0
-----	--	-----	-------

⊕		5.9	174.9
---	--	-----	-------

1/4		5.7	175.1
-----	--	-----	-------

ch		5.3	175.5
----	--	-----	-------

E.		5.3	175.5
----	--	-----	-------

44th ST

57

180.81

2+50

E	6.5	174.3
cl	6.5	174.3
1/4	6.7	174.1
cl	6.8	174.0
1/4	6.9	173.9
cl	6.8	174.0
W	6.5	174.3
+5	6.5	174.3

3+00

-25	8.4	172.4
W	7.7	173.1
cl	7.4	173.4
1/4	7.3	173.5
cl	7.3	173.5
1/4	7.0	173.8
cl	6.7	174.1
E	6.6	174.2

180.81

3+50 S₁ = S. End. Row. #excels on E44th ST

58

E	7.0	173.8
cl	7.1	173.7
1/4	7.7	173.1
cl	7.7	173.1
1/4	7.9	172.9
cl	8.2	172.6
W	8.2	172.6
+5	8.2	172.6

4+00

-5	8.8	172.0
W	8.8	172.0
cl	8.8	172.0
1/4	8.6	172.2
cl	8.7	172.1
1/4	8.6	172.2
cl	8.4	172.7
E	8.0	172.8

T.P.	3.63	176.34	8.10	172.71
------	------	--------	------	--------

176.34

4+50 S

e	3.5	172.8
+8	3.8	172.8
el	4.6	171.7
ly	4.6	171.7
⊕	4.6	171.7
ly	4.7	171.6
el	4.8	171.5
w	5.0	171.3
+5	5.2	171.1

5+00

-5	5.2	171.1
w	5.1	171.2
el	4.7	171.6
ly	4.8	171.5
⊕	4.7	171.6
ly	4.5	171.8
el	4.2	172.1
+2	3.6	172.7
E	3.1	173.3

176.34

5+50

E	2.3	174.0
+8	2.8	173.5
el	3.6	172.7
ly	3.6	172.7
⊕	3.9	172.7
ly	4.3	172.0
el	4.8	171.5
w	5.2	171.1
+5	5.6	170.7

6+04 N. line Hill Top

w	4.8	171.5
el	4.8	171.5
ly	4.3	172.0
⊕	3.6	172.7
ly	3.5	172.8
el	3.2	173.1
E	2.2	174.1

CHK. T.P. Page 40

2.70 173.64 = 173.64

44. 44

59

7-22-39 X Sec. 41st St. HN/top to J. St.
 Miller
 Walker.

60' W. of
 10' obs
 10' 1/2

indexed
 C.S.M.

109.95

60

B.M. B.P. 8.20 133.57⁹ 125.39

T.P. 1.88 122.58⁶⁰ 12.87 120.70²

0.41 109.95⁷ 13.04 108.54⁶

60' S of N line J. St = 20' S. of S. line

W-40 12.5 92.5

W 12.1 92.9

cl 12.2 92.8

114 11.8 98.2

cl 11.6 98.4

114 11.5 98.5

cl 10.8 99.2

E 9.7 100.3

+30 8.4 101.6

7.5' S. of S. line J. St.

1.5' W of E = N.E. cor small House 8' x 12'

9.5' " " " = N.W. " above "

40' S. of N = S. line J. St.

E-30 8.4 101.6

E 8.6 101.4

N.W. 41st St

Market St

cl

114

cl

114

cl

W

+40

-40

W

cl

114

cl

114

cl

E

+30

E-155

9.2 100.8

9.6 100.4

10.4 99.6

11.4 98.6

11.5 98.5

12.0 98.0

12.6 97.4

30' S. of N. Line J. St

12.8 97.2

11.5 98.5

10.6 99.4

10.0 100.0

8.6 101.4

7.5 102.5

6.6 103.4

6.4 103.4

7.0 103.0

20' S. of N. line J. St.

6.0 104.0

	109.95	
E - 115	7.0	103.0
E - 85	8.8	101.2
E - 3.0	6.4	103.6
E	6.1	103.9
cl	6.4	103.6
14	6.8	103.2
±	7.4	102.6
114	6.3	101.7
cl	9.5	100.5
W	10.8	99.2
+ 20.	12.5	97.5
+ 100.	13.5	96.5
	10' S. of N.	
- 100	13.5	96.5
- 30.	12.8	97.2
W	7.5	102.5
cl	5.5	104.5
114	4.2	105.8
±	3.7	106.3
114	3.0	108.0

	109.95	41 st St
cl	4.6	105.4
E	5.1	104.9
+ 30.	4.8	105.2
	0 + 00 = N. Line J. St	
- 30.	0.7	109.3
E	1.0	109.0
cl	0.0	110.0
14	+ 0.7	110.7
±	0.0	110.0
14	0.9	109.1
cl	2.5	107.5
W	4.5	105.5
+ 20	11.0	99.0
	0 + 10 N	
- 30	7.8	102.2
W	2.0	108.0
T.P.	12.86	122.40
cl	0.41	109.54
cl	11.6	110.8
14	9.2	113.2
±	7.8	114.6

1224x
2

1/4	8.7	113.7
el	9.1	113.3
E	10.2	112.2
+20	10.8	111.6

+22 - 8' W. of E. Line = Elec Pole
0+24

E	5.3	117.1
el	5.2	117.0
1/4	6.0	116.4
⊕	6.2	116.2
1/4	5.7	116.7
el	7.0	115.4
W	9.6	112.8
+10	10.7	111.7

0+50

W	4.8	117.6
el	4.7	117.7
1/4	5.1	117.3
⊕	5.1	117.3
1/4	5.0	117.4
el	4.8	117.6
E	5.0	117.4

+54 - 8' W of C Line = Elec. Co. Guy Wire - D.M.

1224x
3+75

41st St

62

E	4.4	118.0
el	3.8	118.6
1/4	4.1	118.3
⊕	4.6	117.8
1/4	4.8	117.6
el	4.2	118.2
W	4.0	118.4

1+00

W	4.4	118.0
el	4.0	118.4
1/4	3.6	118.8
⊕	3.8	118.6
1/4	3.7	118.7
el	3.6	118.8
⊖	3.5	118.9

1+25

E	3.3	119.1
el	3.0	119.4
1/4	2.9	119.5
⊕	3.1	118.7

		122.40 ²		
		1+25 con		
114		3.8	118.6	
d		4.1	118.3	
w		3.7	118.7	
		1+45		
w		3.7	118.7	
d		3.4	119.0	
114		2.8	119.6	
e		2.8	119.6	
114		2.5	119.9	
d		2.7	119.7	
E		2.7	119.7	
T.P.	12.80	133.58 ²	1.70	120.70 ²
		1+70		
E		11.4	122.1	
d		11.5	122.0	
114		12.5	121.6	
e		12.6	120.9	
114		12.3	121.2	
d		12.1	121.4	
w		12.4	121.1	

		133.58 ²		41 st 8+
		1+90		63
w		12.7	120.8	
d		12.5	121.0	
114		12.3	121.2	
e		12.0	121.5	
114		11.8	121.7	
d		11.3	121.2	
E		11.6	120.9	
		2+25		
E		10.5	123.0	
d		10.2	123.3	
114		10.2	123.3	
e		9.6	123.9	
114		8.6	124.9	
d		9.2	124.3	
w		10.7	122.8	
		2+50		
w		9.1	124.4	
d		9.2	124.3	
114		9.1	124.9	
e		8.7	124.8	

133.50₂

14	8.8	125.7
d	8.6	125.9
e	8.6	125.9

2+75

e	6.4	127.1
d	6.3	127.2
14	6.5	127.0
e	6.2	127.3
14	5.8	127.7
d	5.8	127.7
w	6.4	127.1

3+00

w	5.6	127.9
el	5.1	128.4
14	4.8	128.7
e	4.2	129.3
14	3.9	129.6
d	3.6	129.9
e	4.5	129.0

3+23.5 - u 8.5' W. of e. line = Elec Pole

133.50₂ 3+25

41st St

64

e	4.5	129.0
el	3.2	130.3
14	3.3	130.2
e	3.8	129.7

14	4.5	129.0
el	4.9	128.6
w	5.2	128.3

3+60

w	2.3	131.2
el	3.3	130.2
14	3.9	129.6
e	3.5	130.0
14	3.4	130.1
d	3.4	130.1
e	4.1	129.4

3+90

e	3.0	130.5
el	1.8	131.7
14	2.0	131.5
e	2.4	131.1

133.52

1/4	3+90 con	3.1	130.4
d		3.3	130.2
w		3.5	130.0
4+18			
w		2.4	131.1
cb		1.9	131.6
1/4		1.1	132.4
⊕		1.0	132.5
+3		1.7	131.8
1/4		1.9	131.6
d		2.4	131.1
E		3.9	129.6
4+37 Next Page			
4+55			
E		4.0	129.5
d		3.4	130.1
1/4		3.2	130.3
⊕		3.1	130.4
1/4		3.8	129.7
d		3.8	129.7
w		3.8	129.7

133.52

out of place 4+37.

41st St. 65

w		1.6	131.9
d		2.0	131.5
1/4		2.2	131.3
⊕		2.3	131.2
1/4		2.6	130.9
d		2.7	130.8
E		3.9	130.6
4+70			
E		4.9	128.6
d		3.8	129.7
1/4		3.8	129.7
⊕		3.7	129.8
1/4		4.4	129.1
d		4.3	129.2
w		4.4	129.1
4+85			
w		3.8	129.7
d		3.7	129.8
1/4		4.7	128.9
1/6		5.3	128.2

	133.52	4+85 (con)		
⊕		5.1	128.4	
1/4		5.1	128.4	
el		4.8	128.2	
E		5.5	128.0	

5+01. - 8' W of E = Elec. Pole

5+01. - 31' W of E = Elec. Guy. Pole

		5+15		
- 10		8.7	124.8	
E		9.3	124.2	
d		8.7	124.8	
1/4		8.7	124.8	
⊕		9.0	124.5	
1/4		8.7	124.8	
el		8.2	125.3	
W		7.7	125.8	
+10.		7.5	126.0	
T.P.	5.35	131.6 ³	7.24	126.2 ⁵

	131.63	5+55		41 st St
W		6.4	125.2	66
d		6.6	125.0	
1/4		7.0	124.6	
⊕		7.8	123.8	

1/4		8.0	123.6	
d		8.2	123.4	
E		8.5	123.1	
+10		9.1	122.5	

5+97

E		8.8	122.8	
el		8.7	122.9	
1/4		8.6	123.0	
⊕		8.4	123.2	
1/4		7.3	124.3	
el		6.2	125.4	
W		6.2	125.4	

6+00 = S. Line Market.

W		7.5	124.1	
+ 2.5	= W. edge S. End walk	7.73	123.90	
+ 7.5	= E " " " "	7.75	123.88	

131.63
6+00 edn

W. cl	S. End.	7.82	123.81
G pav	" "	8.40	123.23
W "	" "	8.46	123.17
cl "	" "	8.51	123.12
W "	" "	8.77	122.86
G "	" "	9.21	122.42
E. cl	" "	8.64	122.99
+2.5 = W. edge & S. end walk		8.59	123.04
+7.5 = E " " " "		8.51	123.12
E		8.6	123.0
20' N of S. = S. cl. Market			
E-10. B.C. 20' R cl. Ret.		8.96	122.67
" " G		9.50	122.13
E		9.32	122.31
cl		9.08	122.55
W		8.82	122.81
cl		8.58	123.05
W		8.41	123.22
cl		8.22	123.41
W		7.99	123.64

131.63

71st

67

+10. = E.C. 20' Rad. Return prev.	7.68	123.98
" = " " " " cl.	7.16	124.47
chk. BM	6.22	125.34
20.5 of N = N. cl. of Market		
W-10. = E.C. 20' Rad. Ret.	6.28	125.35
" " " " " G	6.82	124.81
W	7.14	124.49
cl	7.40	124.23
W	7.56	124.07
cl	7.73	123.90
W	7.90	123.73
cl	8.12	123.51
E	8.33	123.30
+10. E.C. 20' Rad. Ret. G	8.50	123.13
" " " " " cl	7.92	123.71
0+00 = N. Line Market		
E	7.5	124.1
+2.5 = E. edge N. End. walk.	7.44	124.19
+7.5 = W " " " "	7.47	124.16
cl. N. End.	7.50	124.13

N.W. 1/4 of Market = 125.39

		131.63 N. Line Market St.	0+00 (con).		135.82		41 st		
G. pay	N. End		8.10	123.53	el		10.9	124.9	68
1/4 "	" "		7.68	123.95	1/4		11.1	124.7	
1/2 "	" "		7.43	124.20	1/2		10.8	125.0	
1/4 "	" "		7.34	124.29	1/4		9.7	126.1	
G "	" "		7.37	124.26	el		9.4	126.4	
Web	" "		6.78	124.85	W		9.0	126.8	
+2.5 =	E. edge N. end. walk		6.81	124.82		1+00			
+7.5 =	W " " " "		6.75	124.88	W		8.5	127.3	
W			6.4	125.2	el		8.8	127.0	
T.P. B.M. R.P.	10.43	135.82	6.22	125.39	1/4		9.4	126.4	
		0+16			1/4		10.1	125.7	
W			9.1	126.2	1/4		10.5	125.3	
el			10.0	125.8	el		10.7	125.1	
1/4			10.8	125.0	E		11.5	124.3	
1/2			11.5	124.3	+10		11.9	123.9	
1/4			11.8	124.0			1+50		
el			11.5	124.3	-10		8.9	125.9	
E			11.5	124.3	E		9.8	126.0	
		0+50			el		9.6	126.2	
-5			10.6	125.2	1/4		9.5	126.3	
E			10.6	125.2	1/2		9.4	126.4	

N.W. 41st
+ Market

	135.82 1+50 con		
14		8.6	127.2
ch		8.3	127.5
w		7.9	127.9
	1+67		
w		7.7	128.1
ch		7.7	128.1
14		8.0	127.8
⊕		8.5	127.3
14		8.8	127.0
ch		8.7	127.1
⊕		8.5	127.3
+10		8.9	126.9
	1+80		
-10		8.8	127.0
⊕		8.4	127.4
ch		8.2	127.6
14		8.2	127.6
⊕		7.6	128.2
14		6.8	129.0
ch		6.2	129.6
w		6.6	129.2

	135.82 2+40		41st
w		4.7	131.1
ch		4.9	130.9
14		5.1	130.7
⊕		5.0	130.8
+5		5.6	130.2
14		5.9	129.9
ch		6.2	129.6
⊕		7.1	128.7
+10		7.6	128.2
	2+70		
-10		6.0	129.8
⊕		6.3	129.5
ch		6.0	129.8
14		5.8	130.0
⊕		5.5	130.3
+7		4.1	131.7
14		3.3	132.5
ch		3.2	132.6
w		3.5	132.3
	2+84		
w		3.3	132.5
ch		3.9	131.9

	135.82	2+88 (com)	
14	4.8	131.0	
⊕	5.3	130.5	
14	5.5	130.3	
d	5.6	130.2	
⊕	5.6	130.2	
+10	5.4	130.4	
	3+15		
-10	5.3	130.5	
⊕	5.2	130.6	
d	4.7	131.1	
14	4.8	131.0	
⊕	4.7	131.1	
14	4.6	131.2	
d	4.2	131.6	
w	3.7	132.1	
	3+44		
w	2.2	133.6	
d	2.6	133.2	
14	3.1	132.9	
⊕	3.0	132.8	
+3	4.0	131.8	
14	3.8	132.0	

	135.82		41.5
d	3.9	131.9	70
⊕	4.0	131.8	
	3+75		
⊕ -10	6.4	129.4	
⊕	5.5	130.3	
⊕	4.6	131.2	
+5	4.7	131.1	
14	4.4	131.4	
⊕	4.1	131.7	
+7	3.3	132.5	
14	3.0	132.8	
d	2.7	133.1	
w	2.5	133.5	
	4+00		
w	2.0	133.8	
d	2.3	133.5	
14	2.9	132.9	
⊕	3.0	132.8	
+3	4.1	131.7	
14	4.8	131.0	
d	5.4	130.4	

135.82
4+100 con

E	5.9	129.9
+10	7.4	128.4
4+30		
-10	8.4	127.4
E	7.0	128.8
+5	6.1	129.7
cl	6.2	129.6
1/4	6.0	129.8
+5	5.7	130.1
E	3.7	132.1
1/4	1.9	133.9
cl	1.7	134.1
W	1.5	134.3
4+55		
W	3.4	132.4
cl	4.2	131.6
1/4	5.6	130.2
E	6.1	129.7
1/4	6.4	129.4
cl	6.6	129.2
E	7.1	128.7
+10	7.7	128.1

135.82
4+75

-10	7.7	128.1
E	7.0	128.8
cl	6.5	129.3
1/4	6.3	129.5
E	6.0	129.8
1/4	5.6	130.2
cl	5.0	130.8
W	4.3	131.5
5+10		
W	3.2	133.6
cl	3.3	132.5
1/4	3.5	132.3
E	4.3	131.5
+5	5.6	130.2
1/4	5.9	129.9
cl	6.2	129.6
E	6.7	129.1
+10	7.2	128.6
5+35		
-10	6.3	129.5
E	5.9	129.9

41 21

71

135.82
5+35 con

cl	5.7	130.1
h4	5.5	130.3
±	4.9	130.9
h4	4.5	131.3
cl	3.9	131.9
w	3.3	132.5

5+60

w	1.1	134.7
cl	2.0	133.8
h4	3.2	132.6
±	4.0	131.7
h4	4.5	131.3
cl	4.8	131.0
E	5.2	130.4
h10	6.0	129.8

5+90

-10	5.5	130.3
E	4.6	131.2
cl	4.2	131.6
h4	3.8	132.0
h7	3.3	132.5
±	2.0	133.8

135.82
41 st.

h4	2.4	133.4
cl	3.3	132.5
w	3.2	132.6
6+10		
w	3.1	132.7
cl	3.3	132.5
h4	3.8	132.0
±	3.8	132.0
h4	4.0	131.8
cl	4.0	131.8
E	4.6	131.2
h10	5.1	130.7
T.P.	11.60	144.36
	3.66	132.76

6+40 = s. line - F. St. 50' wide

-50	13.6	130.8
E	12.4	132.0
cl	12.4	132.0
h4	12.3	132.1
±	12.1	132.3
h4	11.5	132.9
cl	11.1	133.3
w	10.5	133.9
±	8.6	135.8

72

144.36
25' N of S = ϕ F. ST

W - 40		9.0	
W		10.8	133.6
cl		11.1	133.3
ly		11.6	132.8
ϕ	Rim M.H.	11.50	132.86
ly		11.9	132.5
cl		12.1	132.3
E		12.1	132.3
+ 50		13.0	131.4

0400 = 50' N of S. = N. line F. ST.

-50.		13.8	130.6
E		12.4	132.0
cl		11.9	132.5
ly		11.7	132.2
ϕ		11.2	133.2
ly		11.3	133.1
cl		11.0	134.4
W		10.6	133.8
+ 30		9.5	134.9

144.36
0450

41¹⁵ ST

73

W		10.9	133.5
cl		11.1	133.3
ly		11.1	133.3
ϕ		11.3	133.1
ly		11.7	132.7
cl		11.7	132.7
E		12.1	132.3
+ 10		12.4	132.0

0478

W. Line = E End conc. walk

10.60 133.76

1200

-10		12.3	132.1
E.		11.8	132.6
cl		11.5	132.9
ly		11.2	133.2
ϕ		11.3	133.1
ly		11.0	133.4
cl		11.0	133.4
W		10.9	133.5

	144.36 1+50	
-5	9.8	134.6
w	9.8	134.6
cb	9.6	134.8
14	9.8	134.6
±	10.4	134.0
14	10.4	134.0
cb	10.5	133.9
0	10.3	134.1
+10	10.4	134.0

	2+00	
-80	6.9	137.5
+5	8.2	136.2
cb	8.1	136.3
14	8.1	136.3
±	8.4	136.0
14	8.4	136.0
cb	8.2	136.2
w	8.4	136.0
+10	9.3	135.1

	144.36 2+50	41 or 51 74
-40	7.1	137.3
w	7.2	137.2
cb	6.6	137.8
14	6.5	137.9
±	5.8	138.6
+15	4.4	140.0
14	4.7	139.7
cb	5.1	139.3
+2	5.2	139.2
±	4.4	140.0

	3+00	
±	3.3	141.1
+3	3.5	140.9
cb	3.6	140.8
14	3.6	140.8
±	4.6	139.8
14	4.9	139.5
cb	5.0	139.4
w	5.6	138.8
+10	5.6	138.8

144.36 3+50

-10	4.5	139.9
W.	4.4	140.0
eb	3.7	140.7
1/4	3.7	140.7
⊕	3.3	141.1
1/4	3.0	141.4
eb	3.0	141.4
⊕	2.7	141.7

4+00

-10	2.0	142.4
⊕	2.1	142.3
eb	2.3	142.1
1/4	2.2	142.2
⊕	2.5	141.9
1/4	2.7	141.7
⊕	2.4	142.0
W	2.5	141.9
+10	2.5	141.9

4+50

-10	0.6	143.8
W	0.8	143.6
eb	0.6	143.8

144.36

1/4	1.3	143.1
⊕	0.9	143.5
1/4	1.0	143.4
eb	1.1	143.3
⊕	0.6	143.8
+10	0.4	144.0
T.R.	11.78	155.09

5+00

-10	9.0	146.1
⊕	9.2	145.9
eb	9.6	145.5
1/4	9.8	145.3
⊕	10.0	145.1
1/4	9.2	145.9
eb	8.7	146.4
W ground,	8.4	146.2
W = E. End, concwalk.	7.98	147.11

41st St.

75

15509

5+30

W-10

6.4

148.7

W

6.5

148.6

d

6.8

148.3

14

6.8

148.3

E

7.8

147.3

14

8.0

147.1

+7

8.0

147.1

d

7.1

148.0

E

6.9

148.2

+10

6.8

148.3

5+61 = S. Line Hill Top

E

5.0

150.1

d

4.8

150.3

+5

5.6

149.5

14

5.5

149.6

E

5.3

149.8

14

5.7

149.4

+2

4.5

150.6

d

4.6

150.5

W

4.2

150.9

155.09

41st 54

76

chk. B.M.

E Mon 41st Hill Top

2.16

152.93 = 152.99

FINAL MEAS. ALLEY
 BK 1 CITY HTS. ANNEX #1

BET. UNIV. AVE + POLK
 FAIRMONT + 44TH

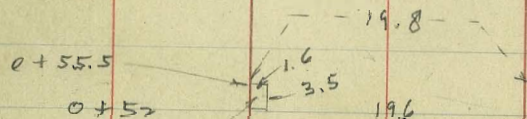
3 + 00 20

2 + 50 20

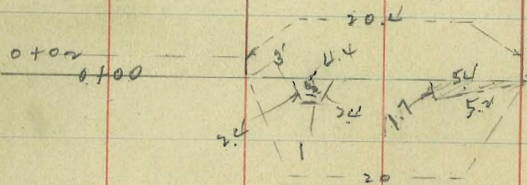
2 + 00 19.9

1 + 50 19.9

1 + 09 19.9



Plaster
 Excepted



UNIV. AVE

Moore

77

8-3-40

Polk

5 + 99.3

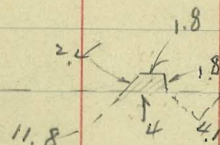
5 + 00 19.9
 5 + 50 19.8

5 + 00 19.9

4 + 50 20

4 + 00 20

3 + 50 20



19.9
 19.8

19.9

20

20

20

6+03 Aca 487.26
 5+22 Aca 14
 5460 Aca 73.26

4+12 Aca
 18'W

3+95 Aca
 18'W

3+78 Aca
 18'W

3+61
 18'W

3+44
 18'W

328 N End
 Eap Hedge

3700 S end N End Latic
 18' Hedge 4' in St.

2+98 Aca
 16.5'W

2+84 Aca

2+70 Aca

2+58 Aca

2+41 Aca

2+22 Aca

2+06 Aca
 16.5'W

1+44 Aca

1+55 Aca of 76 S End
 11'W

1+40 Aca of 70 conc Dr 14.7W

1+27 Aca of 70 Pepper

1+15 Aca of 48 "

0+70 Aca of 27 "

N End wall
 of 98 S edge Drive

1+76 Aca

1+27 "

1+37 S End wall

1+40 Aca

1+50 "

1+74 "

15.8'W

of 72 gavel
 15. Buck.

CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.69	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w=16.2$ and $h=5.3$, cu. yds. $=1.48 \times .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $=h$, and $\frac{1}{2}$ the roadbed $=w$, add the triangles formed by taking the distance out to each break in turn ($=w$'s) by the difference between the cuts (or fills) on each side of it ($=h$'s) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 $\frac{1}{2}$.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.