

599

ENGINEERS'

LEVEL BOOK

NO. 410

300 -- AVE

Dist 51

F.B. 599

BLITZGEN  
TRADE MARK

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 Feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

**Example**—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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421.5  
44.5  
Valve 3+7 7.0  
No. 5 of N. Line = 5.4

599

599

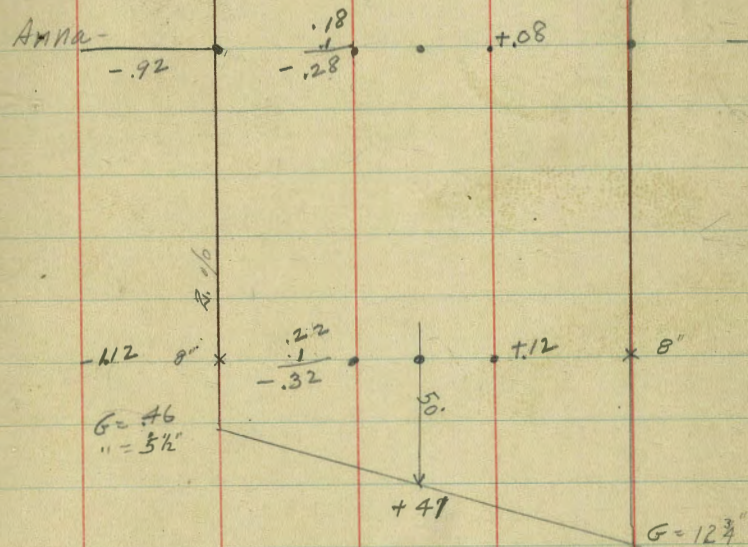
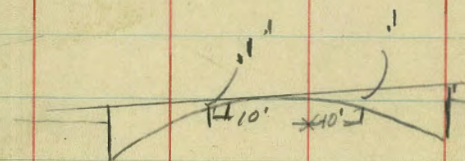
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Intersections on D-67

4/22/24

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intersection at Orange & Chamouni	4
" " Anna "	5
" " Cabillot Klüber	6

21 D



✓

Apna

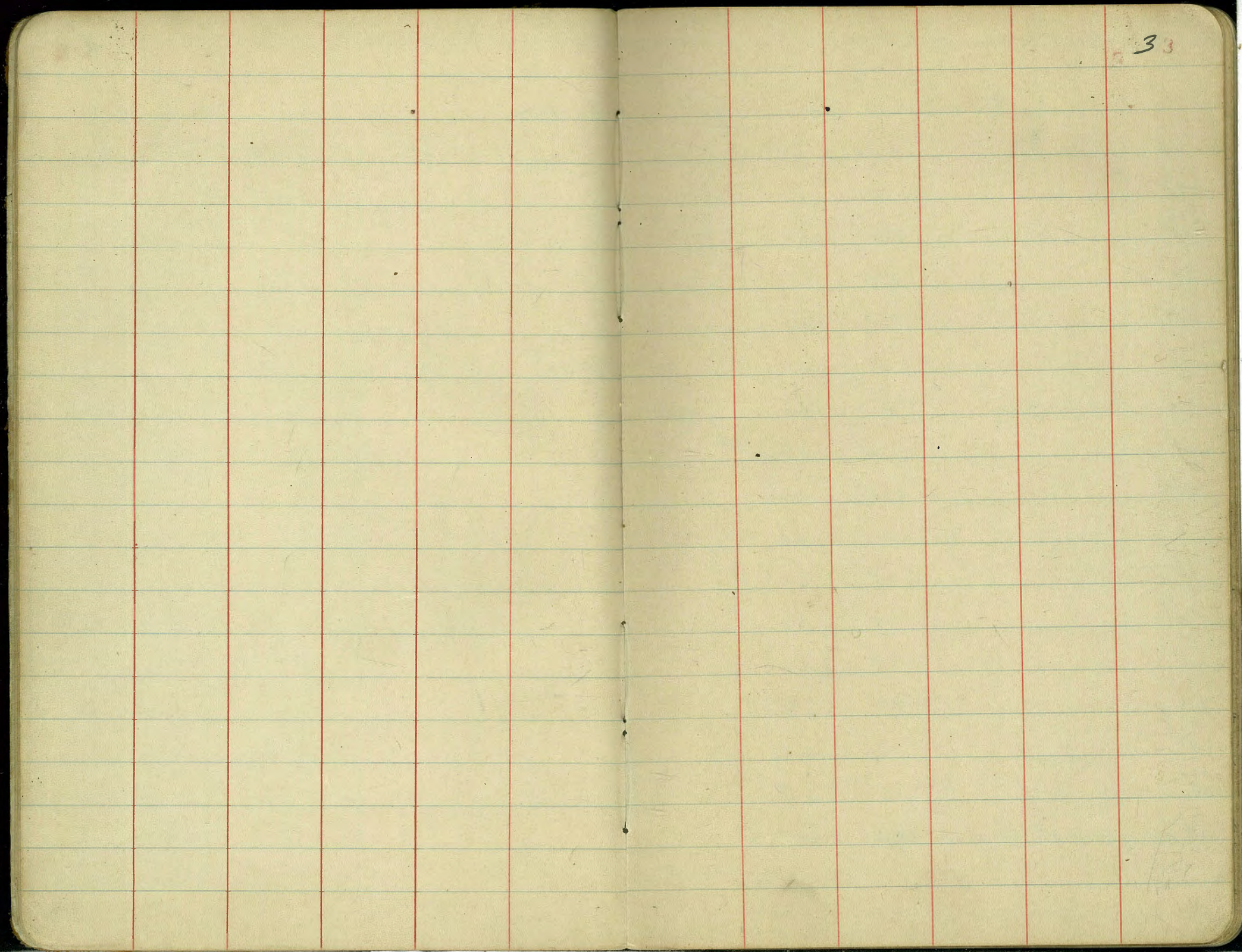
$$\begin{array}{r} .12 \\ 1 \\ \hline -63 \\ -22 \end{array}$$

+ .02

-78  
Orange

$$\begin{array}{r} .15 \\ 1 \\ \hline -12 \end{array}$$

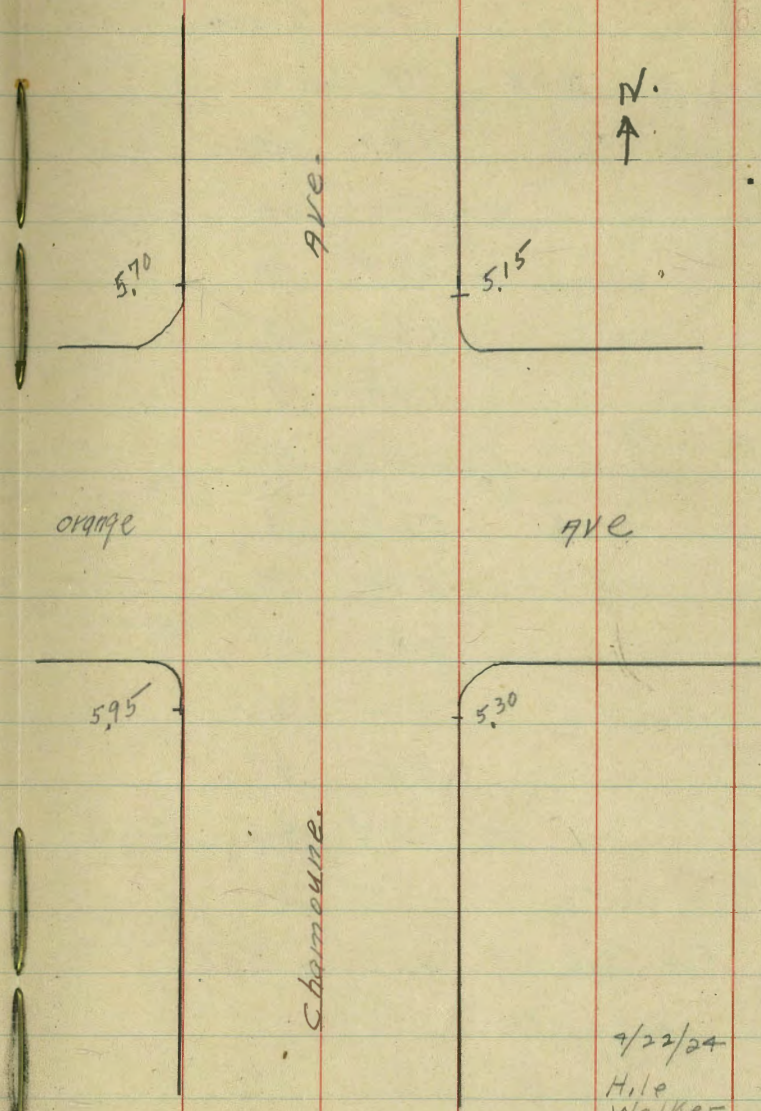
+ .05



West gutter Chamounne + Orange.  
 Rod Grade

5.95 S.W. Cor.

05	588	.07
10	587	.13
15	587	.13
20	579	.16
25	573	.22
30	"	.22
35	"	.22
40	570	.25
45	573	.22
50	"	.22
55	.75	.20
60	.73	.22
65	.75	.20
70	.77	.18
75	.73	.22
80	.70	.25



See page 9 for East gutter

7/22/24  
 Hile  
 Walker  
 Preston  
 Hartigan



North Gut Line.

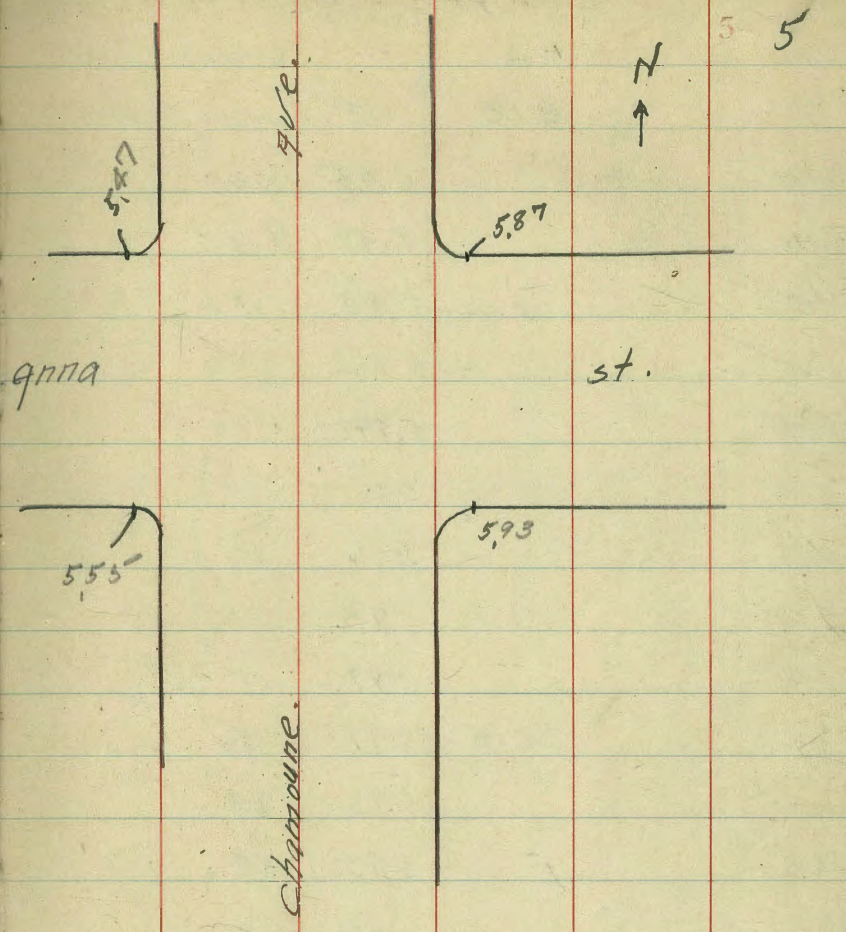
H.I. - Grade

5.47 N.E. Corner.

+05	5.53	.06
10	5.53	.06
15	5.55	.08
20	5.64	.17
25	5.64	.17
30	5.68	.21
35	5.68	.21
40	5.74	.27
45	5.78	.31
50	5.84	.37
55	5.87	.40
60	5.87	.40

OK

For South Gutter line see  
Page. 7.



East Gutter - Cabrillo + Klauber

H.I.

+ grade.

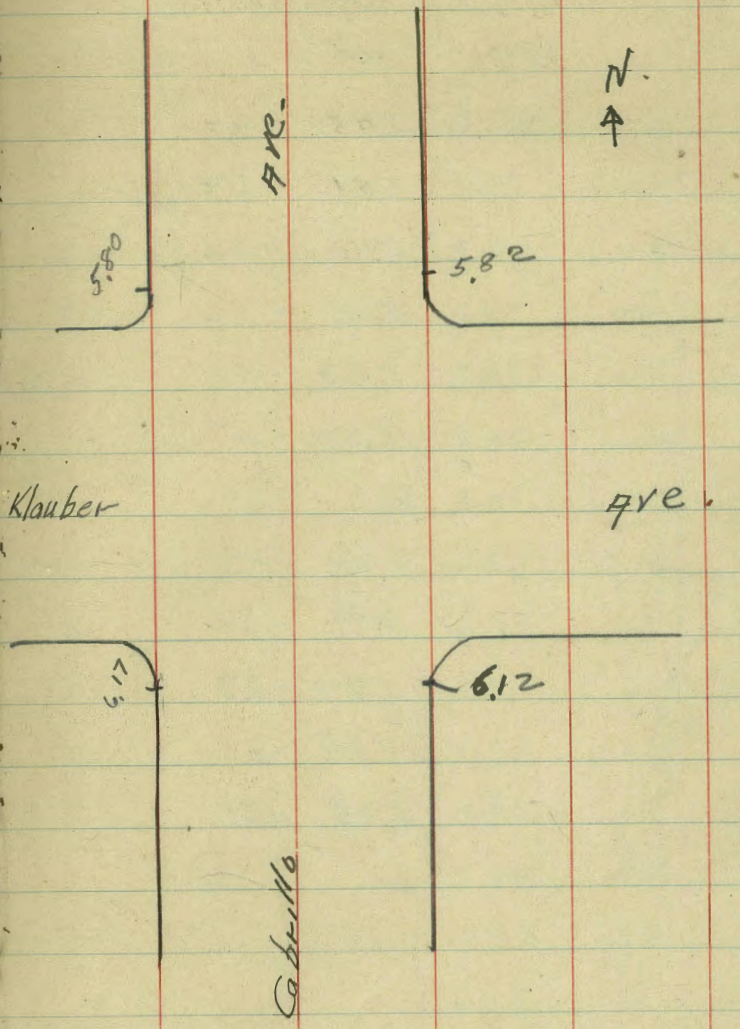
6.12

SE. Cor of gutter

6 6

0+05	6.05	.07
0+10	5.97	.15
+15	5.96	.16
+20	5.96	.16
+25	5.94	.18
+30	5.96	.16
+35	5.96	.16
+40	5.98	.14
+45	5.97	.15
+50	5.97	.15
+55	5.93	.19
+60	5.93	.19
+65	5.90	.22
+70	5.80	.30
75	5.80	.30
80	5.82	.30

low



See page 8 for West Gutter

7.

South gutter line  
711.9 + Chamoune  
5.55

Sta.	Rod	Grade
05	5.49	+0.06
10	5.51	+0.04
15	5.53	+0.02
20	5.53	+0.02
25	5.60	-0.05
30	5.67	-0.07
35	5.66	-0.11
40	5.70	-0.15
45	5.77	-0.22
50	5.84	-0.29
55	5.84	-0.29
60	5.93	-0.38

ti

West gutter Cabrillo + Kpauber.

8 8

Sta	HI	Rod	Grade
	5.80	N.W. Cor.	
05		5.82	.02
10		5.85	.05
15		5.87	.07
20		5.92	.12
25		5.95	.15
30		5.96	.16
35		5.95	.15
40		5.92	.12
45		5.93	.13
50		5.92	.12
55		5.92	.12
60		5.95	.15
65		5.94	.14
70		5.99	.19
75		6.09	.29
80		6.17	.37

low.

East Gutter Chamoune + Orange  
(9) Sta. H I Rod Grade

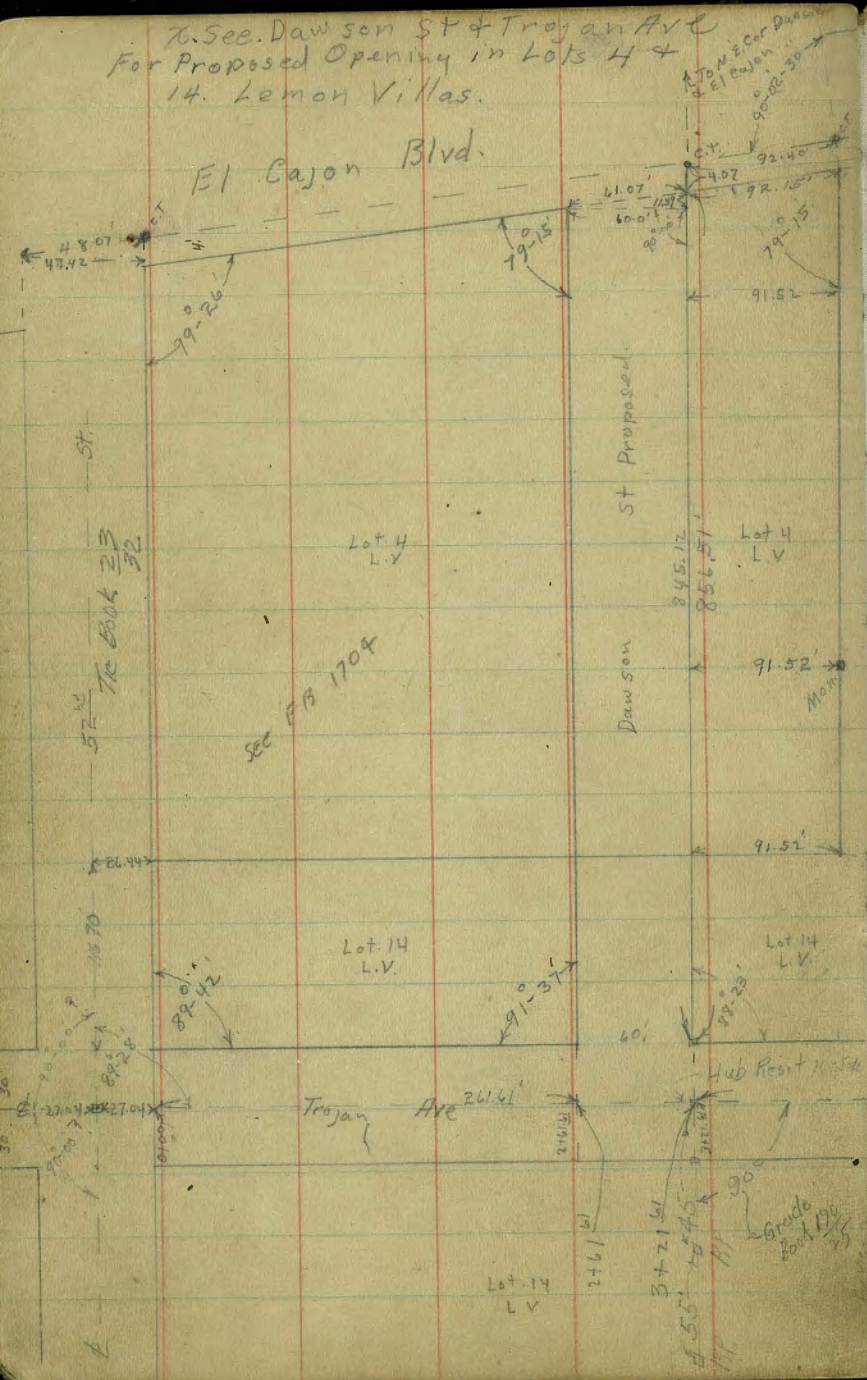
5.15

NE Gutter

.05	5.16	.01
10	5.15	.00
15	5.16	.01
20	5.16	.01
25	5.14	+ .01
30	5.18	.03
35	5.19	.04
40	5.22	.07
45	5.25	.10
50	5.26	.11
55	5.27	.12
60	5.24	.09
65	5.25	.10
70	5.23	.08
75	5.27	.12
80	5.30	.15

low.

X. Sec. Dawson St + Trojan Ave  
 For Proposed Opening in Lots 4 +  
 14. Lemon Villas.



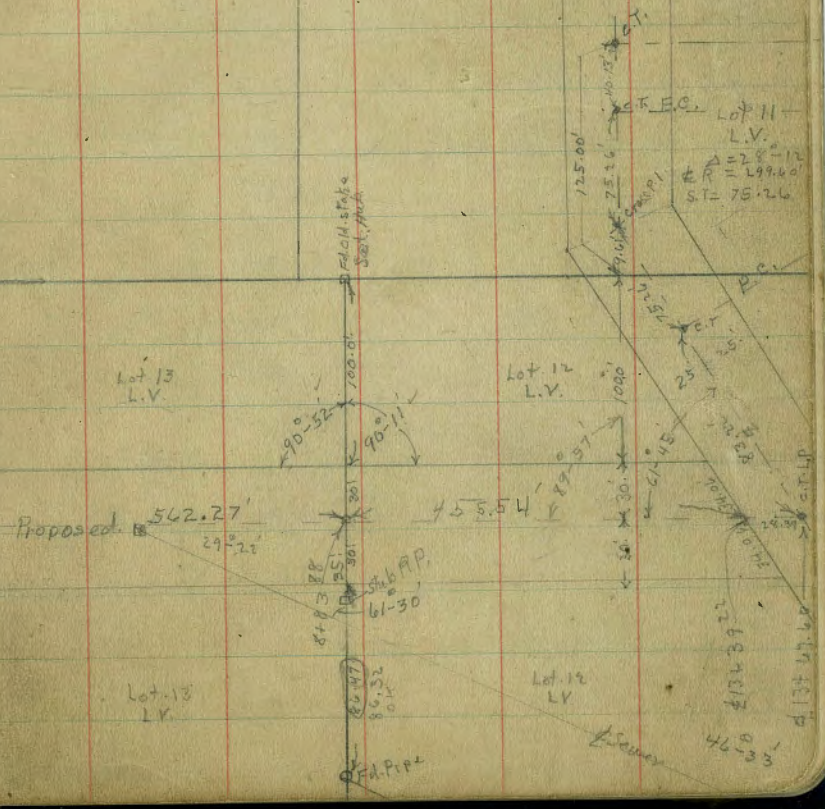
Indexed  
 C-S-K

28-12  
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 90-03

Lot 5  
 L.V.

Lot 6  
 L.V.

Lot 7  
 L.V.



Proposed 542.27  
 29-22

Lot 13  
 L.V.

Lot 12  
 L.V.

Lot 14  
 L.V.

Sewer Line  
 B.M. Mon. 9.49 333.51 323.82

X See Trojan Ave  
 60' wide 10' chs. 10' 1/4 S.

W. Line 52<sup>nd</sup> St.

57' Line Trojan  
 20' E. of W  
 Line 52<sup>nd</sup>  
 This B.M. is  
 0.18' Lower  
 than B.M. S  
 Used for  
 Sewer

333.51

Trojan 11

11

27.04 E. of W  $\phi$ .

S-20	14.0	319.5
S	13.0	320.5
d	11.4	322.1
$\phi$	10.1	323.4
14	7.8	325.7
d	6.2	327.3
N	5.2	328.3
10' E = W. d		
N	5.0	328.5
d	6.0	327.5
14	7.3	326.2
$\phi$	8.2	325.3
14	9.7	323.8
d	8.6	323.9
S	10.8	322.7
+10	11.0	322.5

-10	10.7	322.8
S	10.1	323.4
d	9.5	324.0
$\phi$ stab	7.93	325.58
d	6.4	327.1
N	5.3	328.2
17.04 E of $\phi$ = E d		
N-10	5.7	327.8
N	6.6	326.9
d	7.7	325.8
$\phi$	9.1	324.4
d	10.8	322.7
S	11.5	322.0
+20	12.5	321.0
0+00 = 27.04 E of $\phi$ = E. Line 52 <sup>nd</sup>		
-20	12.2	321.3
S	11.2	322.3
d	10.4	323.1
$\phi$	8.9	324.6

333.51

0+00 (con)

db	7.3	326.2
N	6.2	327.3
+10	5.2	328.3

0+50

-10	8.0	325.5
N	9.5	324.0
d	10.0	323.5
φ	11.0	322.5
db	11.8	321.7
S	11.8	321.7
+20	12.6	320.9

T.P.	2.72	336.04	0.19	333.32
------	------	--------	------	--------

1+00

-20	14.0	322.0
S	13.8	322.2
db	13.5	322.5
φ	12.2	323.8

336.04

Trojan 12

db	11.8	324.2
N	11.3	324.7
+10	11.0	325.0

1+50

-10	10.7	325.3
N	10.9	325.1
db	11.4	324.6
φ	12.2	323.8
d	12.8	323.2
S	13.1	322.9
+15	13.6	322.4

2+00

-15	12.7	323.3
S	12.1	323.9
d	11.5	324.5
φ	10.8	325.2
d	10.2	325.8
N	10.0	326.0
+10	9.9	326.1

336.04

2+35

N	8.5	327.5
cl	9.2	326.8
⊕	9.9	326.1
cl	10.2	325.8
S	12.0	324.0
+7	14.0	322.0
+12 = ⊕ wash	14.3	321.7
+20	13.1	322.9

2+46

-20	13.0	323.0
S wash	14.0	322.0
cl "	14.0	322.0
14 "	13.9	322.1
⊕	9.4	326.6
cl	9.0	327.0
N	8.2	327.8

2+61 <sup>61</sup> W. line Dawson St

N	8.1	327.9
cl	8.3	327.7
+15	8.5	327.5
⊕	12.6	323.4

336.04

Tujan 13

+5 = ⊕ wash	13.7	322.3	13
cl	12.8	323.2	
S	12.8	323.2	
+20	12.8	323.2	

2+91 <sup>61</sup> ⊕

-20	12.6	323.4
S	12.8	323.2
cl	13.0	322.6
+30 = ⊕ wash	13.6	322.4
+8	13.2	322.8

⊕	8.0	328.0
cl	7.4	328.6
N	7.3	328.7

3+21 <sup>61</sup> E. line Dawson

N	6.8	329.2
cl	6.9	329.1
+15	8.0	328.0

⊕ Hub	9.45	326.59
-------	------	--------

+3	13.3	322.7
+6 = ⊕ wash	13.6	322.4
cl	12.3	323.7
S	11.9	324.1
+20	11.8	324.2



336.04

3+40

-20 11.6 324.4

S 11.8 324.2

cl 11.8 324.2

+16 = cl wash

13.3 322.7

cl 13.0 323.0

+7 8.9 327.1

cl 7.4 328.6

N 6.8 329.2

4+00

N 5.6 330.4

cl 6.2 329.8

cl 10.0 326.0

+15 = cl wash 12.5 323.5

cl 11.2 324.8

S 10.8 325.2

+20 10.6 325.4

4+29.8 N + S. Barbed wire Fence

4+50

-15 10.6 325.4

S - 10 = wash.

S - 5. 11.0 325.0

336.04

Trojan 14

14

13.2 322.8

10.6 325.4

8.5 327.5

5.0 331.0

4.1 331.9

5+00

2.7 333.3

3.4 332.6

6.3 329.7

9.4 326.6

11.5 324.5

10.4 325.6

9.6 326.4

5+50

S-20 10.0 326.0

-10 cl wash 10.4 325.6

S 7.9 328.1

cl 7.7 328.3

cl 5.6 330.4

cl 2.6 333.4

N 1.7 334.3

336.04

6+00

N	0.5	335.5
cl	1.2	334.8
φ	2.6	333.4
cl	5.0	331.0
S	6.4	329.6
+10	8.0	328.0
+20	8.0	328.0

6+35

- 23 = wash  
- 15

- 23 = wash	7.3	328.7
- 15	5.2	330.8
S	3.8	332.2
cl	2.0	334.0

T.P.	10.63	343.95	2.72	333.32
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cl	8.9	335.0
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N	8.4	335.5
---	-----	-------

343.95

Trojan 15

6+60

3

15

N	9.0	334.9
cl	9.6	334.3
φ	10.4	333.1
cl	12.3	331.6
S	13.7	330.2
+15	15.0	328.9
+20 = φ wash	17.5	326.4

7+00

- 20	17.0	326.3
- 15	15.2	328.7
S	14.2	329.7
cl	13.6	330.3
φ	12.3	331.0
cl	11.2	332.7
N	10.4	333.1
+10	10.1	333.8

343.95

7+35

-10	10.0	333.9
N	11.0	332.9
cl	11.7	332.2
¢	12.5	331.4
cl	13.5	330.4
S	14.6	329.3
+5 = ¢ wash	15.2	328.7
+20	14.6	329.3

7+50

-20	14.2	329.7
S	14.6	329.3
+6 = ¢ wash	16.4	327.5
cl	14.3	329.5
+5	12.5	331.4
¢	11.5	332.4
cl	10.7	333.2
N	10.7	333.2
+10	10.4	333.5

343.95

7+80

Trojan 16

-10	7.9	336.0	16
N	8.1	335.8	
cl	8.7	335.2	
¢	11.4	332.5	
cl	13.4	330.5	
S	14.0	329.9	
+5 = ¢ wash	14.8	329.1	
+20	14.7	329.2	

8+10

-20	13.0	330.9
S	12.6	331.3
cl	12.2	331.7
¢	10.2	333.7
cl	7.3	336.6
N	6.0	337.9
+10	5.6	338.3

8+40

-10	3.8	340.1
N	3.8	340.1
cl	4.3	339.6

343.95

8+40 con

4		5.4	338.5
cb		7.0	336.9
S		8.1	335.8
+15		9.6	334.3

8+70

-		6.6	337.3
S		4.3	339.6
cb		3.6	340.3
4		3.3	340.6
cb		2.8	341.1
N		2.5	341.4

8+83<sup>85</sup> W. line Lot. 12 - W. End. Partially graded. St. from N. line to S. cb.

9+00

N	grading	2.8	341.1
cb	"	2.8	341.1
4	"	2.9	341.0
+18	"	2.6	341.3
cb	Nat. ground	3.1	340.8
S	"	3.4	340.5
+10	"	4.1	339.8

343.95

9+50

-10	Nat. Ground	4.6	339.3	17
S	"	4.0	339.9	
cb	"	3.2	340.7	
+4	grading	2.2	341.7	
4	"	2.3	341.6	
cb	"	2.4	341.5	
N	"	1.8	342.1	

10+00

N-5	Nat. ground	1.7	342.2	
N	grading	1.3	342.6	
cb	"	1.4	342.5	
4	"	1.5	342.4	
+17	"	1.1	342.8	
cb	"	2.5	341.4	
+3	Nat. ground	4.0	339.9	
S	"	4.5	339.4	
+15	"	5.3	338.6	

Troyan 17

		343.95	10+50	
S-15	Nat ground.		4.9	339.0
S	" "		4.5	339.4
+4	" "		4.4	339.5
cl	grading		1.0	342.9
+2	" "		0.0	343.9
+11	" "		70.4	344.0
+12	" "		0.1	343.8
±	" "		0.2	343.7
cl	" "		0.1	343.8
+7	" "		0.1	343.8
N	Nat. ground		1.7	342.2
+5	" "		1.5	342.4
T.P.	12.88	356.59	0.24	343.71

Culvert.

10+56 - 18' S. of ± = S. End. Outlet Old Rustad

20" Iron Pipe P.L. 17.7 338.9

11+08 - 30' N of ± = N End. Inlet. above Pipe

FL. 15.2 341.4

		356.59	11+00	
N-10	Nat. ground		14.0	342.6
N	" "		14.0	342.6
+3	grading		11.0	345.6
cl	" "		11.0	345.6
±	" "		11.1	345.5
cl	" "		11.0	345.6
+5	Nat ground		13.7	342.9
S	" "		14.5	342.1
+15	" "		14.8	341.8

11+50

-5	Nat ground.	9.5	347.1
S	" "	9.5	347.1
cl	grading	8.6	348.0
±	" "	8.8	347.8
cl	" "	8.6	348.0
+7	" "	8.4	348.2
N	" "	9.6	347.0
+5	Nat. ground.	10.6	346.0

		356.59	
-5	Nat ground.	8.3	348.3
N	grading	7.3	349.3
d	"	7.5	349.1
±	"	7.7	348.9
+14	"	7.6	349.0
d	Nat ground	6.4	350.2
S	" "	6.3	350.3
		12+00	
S	Nat ground	3.1	353.5
+9	" "	5.0	351.6
d	grading	6.5	350.1
±	"	6.8	349.8
d	"	6.8	349.8
+5	Nat ground.	5.8	350.8
N	" "	5.8	350.8
		12+35	
N	Nat. ground.	2.3	354.3
+1	grading	4.8	351.8
d	"	5.5	351.1
±	"	5.5	351.1

		356.59		Trojan 19
d	grading	5.2	351.4	19
+1	"	1.6	355.0	
S	Nat. ground	1.0	355.6	
		12+50		
S	Nat. ground	+1.1	357.7	
+9	" "	+1.1	357.7	
d	grading	5.0	351.6	
±	"	5.1	351.5	
d	"	4.9	351.7	
N	"	4.7	351.9	
		13+00		
N	grading	3.4	353.2	
d	"	4.0	352.6	
±	"	4.2	352.4	
+18	"	3.8	352.8	
+19	Nat ground	+3.3	359.9	
d	" "	+3.3	359.9	
S	" "	+3.3	359.9	

356.59

13+35  $\phi$  (on Diagonal) parallel to W. Line 54<sup>th</sup> St

S	Nat. ground	+2.7	359.3
cb	" "	+2.7	359.3
+4	grading	5.2	351.4
$\phi$	"	4.9	351.7
cb	"	4.3	352.3
N	"	4.0	352.6

13+39<sup>22</sup>  $\phi$  (on diagonal) = W. Line 54<sup>th</sup> St

N		4.0	352.6
cb		4.4	352.2
$\phi$		5.0	351.6
cb		5.5	351.1
S		5.8	350.8

 $\phi$  = W. edge Ext. 20' Pav.

S-100'		6.91	349.68
S		5.63	350.96
cb		5.35	351.24
$\phi$		4.91	351.68
cb		4.42	352.17
N.		4.23	352.36
+44		3.18	353.41

356.59

13+67<sup>60</sup> =  $\phi$  54<sup>th</sup> St.  
=  $\phi$  20' Pav.

Trojan 20

20

N-49.10 = RC. Pav. on c.T. = 5/8 10+21 <sup>80</sup>		3.34	353.25
N		4.24	352.31
cb		4.44	352.15
$\phi$ on c.T.		4.92	351.67
cb		5.35	351.24
S		5.59	351.00
+100		6.86	349.73

T.P. 12.04 366.99 1.64 354.95

BN B.P. Headwall 54<sup>th</sup> + Orange 3.24 363.75 = 363.75

2-14-39 Dawson Ave (Proposed) X Sec. El Cajon to Trojan Ave  
 Miller  
 Walker  
 Blais  
 60' wide, 10' chs. 10' hys

394.58

21

Direction	Distance	Station	Elevation	Notes	Direction	Distance	Station	Elevation
	0.70	394.58			W	16.4	378.22	
R.M. B.P.				S.W. 53' + El Cajon.	ch	15.6	379.0	
E. S. 4' Line El Cajon + E. Line Dawson	8.51	386.07			±	14.3	380.3	
10' N of S. = S. ch El Cajon (on diagonal)					ch	12.8	381.8	
E -	6.53	388.05			E	10.4	384.2	
E -	7.25	387.33						
E. Line	9.18	385.40						
" "	8.47	386.09			T.P.	0.59	382.82	12.35
W "	11.92	382.66						1+00
W "	12.54	382.04			E	5.7	377.1	
10' N of S = S. edge score walk					ch	7.0	375.8	
W. Line	11.90	382.68			±	7.4	375.4	
E. "	8.58	386.00			ch	8.3	374.5	
S. Line El Cajon (on Diagonal)					W	8.5	374.3	
E	9.1	385.5			+10	8.6	374.2	
ch	9.3	385.3						1+50
±	10.4	384.2			-10	11.5	371.3	
ch	11.6	383.0			W	11.1	371.7	
W	12.0	382.6			ch	11.1	371.7	
					±	11.1	371.7	
W - 10	17.5	377.1			ch	11.2	371.6	
From S. Line El Cajon to 1+95 Ground is being leveled off					E	10.7	372.1	



382.82

1+95 on New Fill Bank

E	12.8	370.0
cl	13.0	369.8
φ	13.2	369.6
cl	12.8	370.0
W	13.0	369.8

T.P.	0.09	369.99	12.92	369.90
------	------	--------	-------	--------

2+12 Nat. ground from Here South

-10	3.2	366.8
W	3.5	366.5
cl	4.2	365.8
φ	4.6	365.4
cl	5.3	364.7
E	5.2	364.8
+10	5.2	364.8

2+40

-10	6.4	363.6
E	6.5	363.5

369.99

Dawson. 22

cl	6.6	363.4
φ	7.0	363.0
cl	6.4	363.6
W	5.8	364.2
+10	4.8	365.2

2+70

-10	6.1	363.9
W	7.5	362.5
cl	8.7	361.3
φ	10.0	360.0
cl	10.3	359.7
E	10.7	359.3
+10	10.6	359.4

3+00

-10	13.3	356.7
E	13.2	356.8
cl	12.7	357.3
φ	11.7	358.3
cl	9.8	360.2
W	8.6	361.4
+10	7.1	362.7

369.99

3+50

-10		9.5	360.5
w		11.5	358.5
d		13.0	357.0

T.P.	0.37	357.57	12.79	357.20
------	------	--------	-------	--------

ϕ		2.7	354.9
---	--	-----	-------

E d		3.7	353.9
-----	--	-----	-------

E		3.8	353.8
---	--	-----	-------

+10		3.8	353.8
-----	--	-----	-------

3+70

-10		4.0	351.6
-----	--	-----	-------

E		6.0	351.6
---	--	-----	-------

d		5.7	351.9
---	--	-----	-------

ϕ		4.2	353.4
---	--	-----	-------

d		1.5	356.1
---	--	-----	-------

w		0.6	357.0
---	--	-----	-------

357.57

4+00

w		3.3	354.3
---	--	-----	-------

d		4.0	353.6
---	--	-----	-------

ϕ		6.3	351.3
---	--	-----	-------

d		7.6	350.0
---	--	-----	-------

E		8.3	349.3
---	--	-----	-------

+10		8.6	349.0
-----	--	-----	-------

4+50

-10		12.1	345.5
-----	--	------	-------

E		11.8	345.8
---	--	------	-------

d		11.0	346.6
---	--	------	-------

ϕ		9.9	347.7
---	--	-----	-------

d		8.1	349.5
---	--	-----	-------

w		7.4	350.2
---	--	-----	-------

5+00

w		11.9	345.7
---	--	------	-------

d		12.5	345.1
---	--	------	-------

T.P.	0.44	345.11	12.90	344.67
------	------	--------	-------	--------

Dawson 23

23

345.11

5+00 (con)

±	1.0	344.1
dr	2.1	343.0
E	2.4	342.7
+10	2.6	342.5

5+50

-10	5.3	339.8
E	5.8	339.6
dr	5.1	340.0
±	4.6	340.5
d	3.7	341.4
W	3.1	342.0

6+00

W	7.7	337.4
dr	7.5	337.6
±	7.5	337.5
dr	8.0	337.1
E	8.0	337.1
+10	7.8	337.3

345.11

Dawson 24

6+50

24

E-10	10.2	334.9
E	10.4	334.7
dr	10.7	334.4
±	11.0	334.1
dr	11.5	333.06
W	11.6	333.5
+10	11.6	333.5

7+00

W	12.8	332.3
d	12.6	332.5
±	12.2	332.9
dr	11.9	333.2
E	11.8	333.3

T.P.	3.24	335.49	12.86	332.25
------	------	--------	-------	--------

7+50

E	3.6	331.9
dr	3.7	331.8

335.49

7450 (con)

£	4.1	331.4
d	4.4	331.1
w	4.7	330.8

8+00

w	6.1	329.4
d	5.7	329.8
£	5.3	330.2
d	4.7	330.8
E	4.6	330.9

8+45<sup>12</sup> on E. = N.E. Cor. Trojan & Dawson.

E. stub	6.10	329.39
d	6.3	329.2
£	6.7	328.8
d	7.2	328.3
w	7.5	328.0

Hub.  $\frac{1}{2}$  Trojan  
E. Line Dawson

8.90	326.59 = 326.59
	page 13

Dawson. 25

25

Levels on R.O.W. Limes Wash. St Ext.

7th to 9th

SETOP FH. 474 289.15 284.41 8TH Wash

7+50 S.L. ROW 7.9 281.3

8 " " 5.8 283.4

+50 " " 4.9 284.3

+84 " LOT grade 4.5 284.7 = approx. W. 8th St.

+84 " Top 10" <sup>CONC.</sup> Wall 3.5 285.7

+84 " St. grade 7.2 287.0

BM 359 288.00 284.41

11+50 N.L. ROW. 4.1 283.9

12 " " 5.4 287.4

+50 " " 6.0 287.0

T.P. 446 287.07 5.41 287.59

13 N.L. ROW 6.4 280.8

approx. W. L. Burkholder Prop.

T.P. 315 285.15 5.07 284.00

+50 N.L. ROW 3.9 281.3

Indexed  
C.S.K.

Moore 26  
6-7-39  
26

14	N.L. ROW	6.2	279.0
	El. of Cent. porch		
+ 20	of Small Frame Porch	5.82	279.33
+ 56	ground	6.8	278.4
+ 50		11.8	273.4
15	30' lower approx. than 14+50		243.4

Porch is over N. ROW line approx. 4'

X520 for Paving of N 45 alley

BIK 3 Hartloys North Park

SIN BR	8.15	354.55		346.40	Wrightman 32 m d.
T P NAIL PAV	4.57	357.35	3.77	350.78	N 45 E alley

0-10 of 6 Wrightman

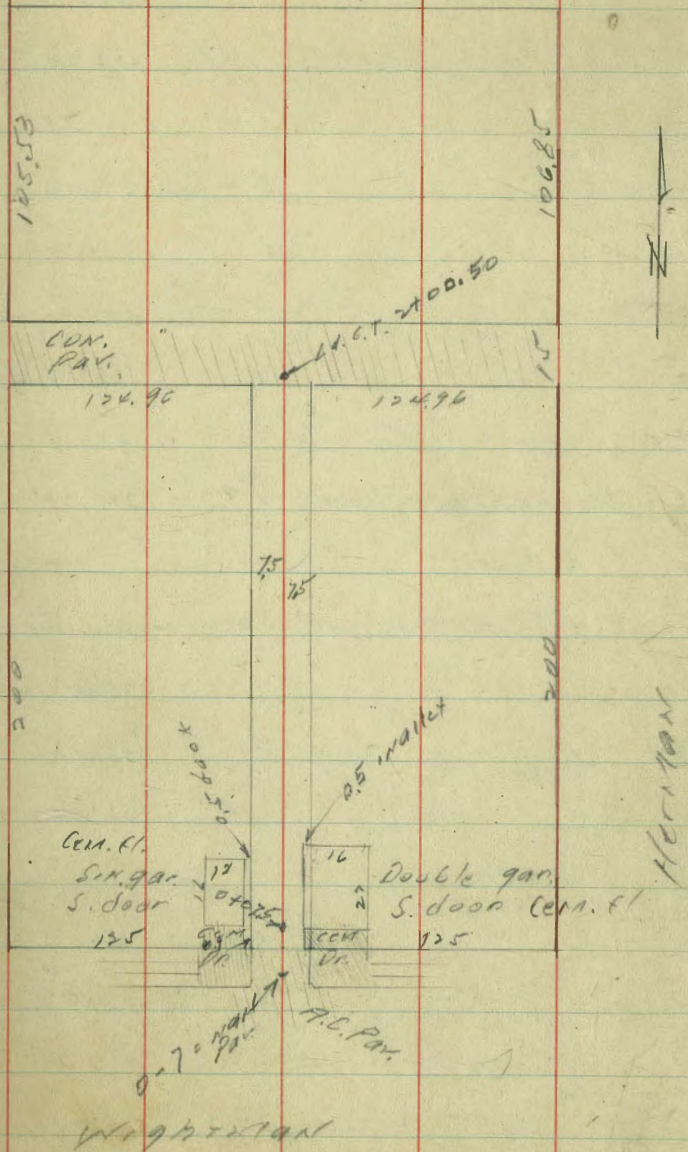
E PAV		6.76		350.69	
W "		4.58		350.77	
00 = NL	"				
W 06		5.94		351.43	
W PAV		6.01		351.34	
C "		6.33		351.02	
# 6.7 TOP		5.83		351.52	
E PAV		6.10		351.25	
E 06		5.78		351.57	
0 + 7.5					
E TOP CEM DR		4.76		352.59	
E top " " "		4.76		352.59	
C		5.4		352.0	
tot		5.4		351.8	

INDEXED  
C.S.K.

MOORE  
6-13-39.

UNIV. AVE.

28



357.35

W		4.7	352.7
+ 0.9		4.7	352.88
0 + 23.5			
W - 0.5		3.4	354.0
W		3.4	354.0
+ 5		4.4	353.0
c		4.4	353.0
+ 4		4.5	352.9
+ 07.0 against gap		3.9	353.5
0 + 29.5			
E + 0.5 NW Cor gap		3.9	353.5
c		4.1	353.3
+ 3		4.0	353.4
W		3.4	354.0
0 + 50			
W		3.2	354.2
c		3.4	354.0
E + 7.1 beg. Bd. fence		3.4	354.0
T.P.	519	359.32	3.22

2. in alley  
23' long

359.32

20

0 + 79			
- 1.5 E SIN. gap	cent. fl.	5.14	354.16
E		5.2	354.1
c		5.0	354.3
W		4.8	354.5
1 + 04			
W		4.8	354.5
c		5.0	354.3
E		5.1	354.2
+ 2.5 SIN. gap	cent.	4.80	354.52
1 + 14			
E - 2.5 2' cent. walk		4.8	354.50
1 + 50			
E TOP cent. rd. of	SMALL STUCCO 5129	4.8	354.5
c		4.4	354.7
W		4.3	355.0
1 + 75			
W		4.0	355.3
c		4.5	354.8
E		4.8	354.5

04 back



359.32

1+94

E -1.7 Top W. edge apron <sup>Cent.</sup> 4.78 354.54

E 4.9 354.4

C 4.5 354.8

W 4.1 355.2

2+00.20

W Pav 4.97 354.35

C 5.04 354.26

E " 5.04 354.28

LEVELS ON CENT. FTW ailer

2+00.20  
T.P. <sup>102</sup> C.7 5.35 359.59 5.08 354.24  
00 = E.L. 3151

S 4.22 355.35

C 4.41 355.18

N 4.09 355.50

0+50

N 4.46 355.13

C 4.80 354.79

S 4.76 354.83

359.59

1+00

S 4.92 354.67

C 5.09 354.50

N 4.85 354.74

1+24.90 MC 5 ailer

N 5.03 354.56

C 5.32 354.27

1+39.96 EL 5 ailer

C 5.47 354.12

N 5.21 354.38

1+70

N 5.26 354.33

C 5.50 354.09

S 5.34 354.23

2+00

S 5.49 354.16

C 5.56 354.03

N 5.39 354.20

2+35

N 5.91 353.68

359.59

31

C 6.08 353.51

S 6.02 353.55

W & HEURNAN

S 6.19 353.40

C 6.19 353.40

N 6.13 353.46

TP. 6.04 362.89 2.72 356.87

check to MW UNIV. 4122 4.88 35801.357.98

ox Lead.  
Br. Plug out.

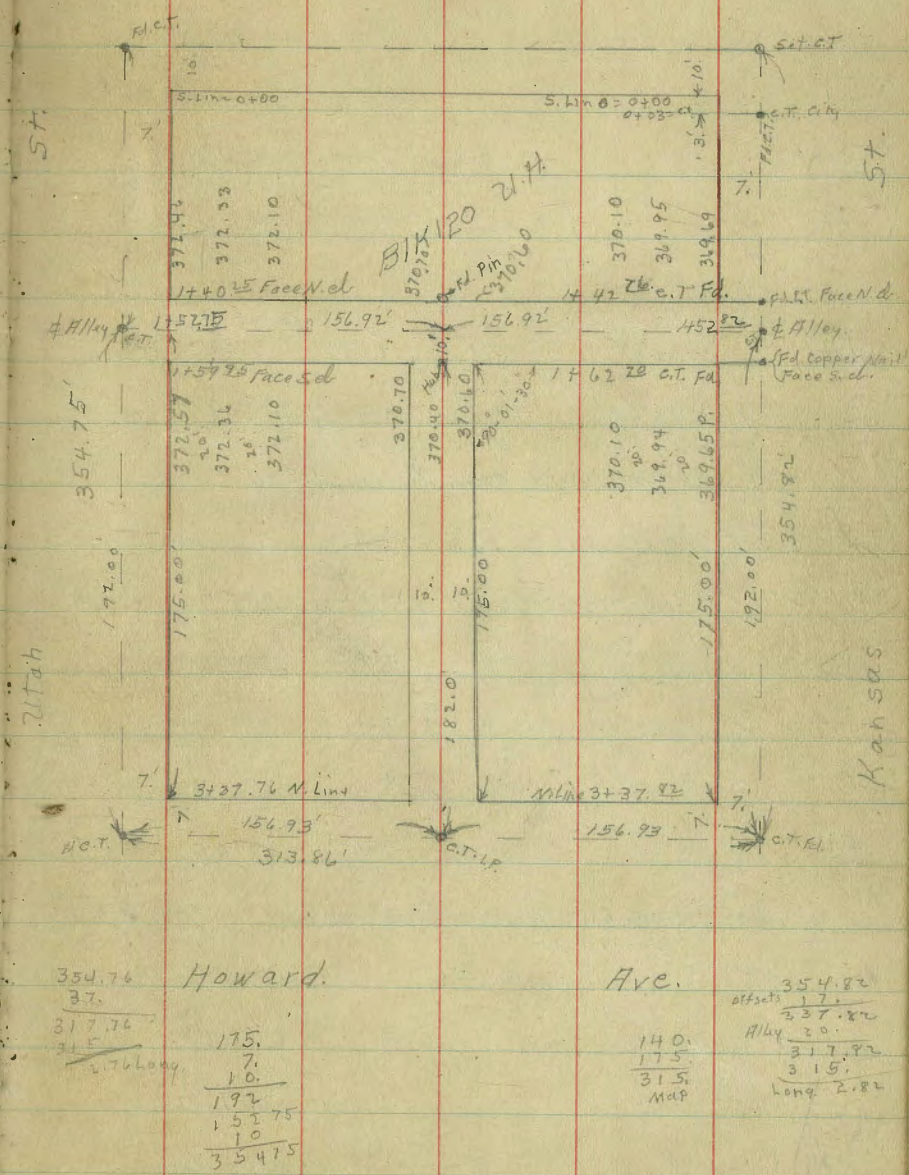
6-22-39  
Miller  
Walker  
Bliss

X Sec. Allegs BIK 120 U.H.

indexed  
c.s.k.

BM. B.P.	5.23	373.58		368.35	N. e. El Cajon + Hamilton
T.P.	6.45	380.26	0.17	373.41	
T.P.	2.50	378.63	4.13	376.13	
(Posted c.s.k.) set BM	S.E.T. c.T.		3.20	375.43	Idaho + El Cajon
T.P. BM. B.P.	5.58	378.59	5.55	(from El Cajon) 373.08 = 373.07	S.W. Utah
T.P. BM. B.P. (Posted c.s.k.)	2.90	376.85	4.64	373.95	+ Howard
set BM. B.P. (Posted c.s.k.)			6.14	370.69	S.W. Kansas + Howard
14' S. of 0+00 = N. d. Howard.					
E. = cb			5.13	371.72	
E. gutter pav			5.60	371.25	
4 " "			5.44	371.41	
W " "			5.43	371.42	
W d			4.95	371.90	
W + 30	gutter		5.17	371.68	
0+00 = N. Line Howard.					
u cone.d N. end			4.83	372.02	
3 pav " "			5.28	371.57	
4 " " "			5.38	371.47	
" " " "			5.45	371.40	
? cone.d " "			4.96	371.89	

El Cajon Blvd 30



Howard Ave.

354.76		354.82
37.		17.
317.76		337.82
31.5		30.
	175.	317.92
	7.	315.
	10.	Long 2.82
	192	
	152.75	
	10	
	354.75	

MAP

376.85

0+05 N.

E		5.0	371.9
+1		5.5	371.4
±		5.1	371.8
W		4.8	372.1

T.P.	3.89	376.01	4.73	372.12
------	------	--------	------	--------

0+41 S. End Lattice Fence on E 0.514 Alley

0+49 7.92' of ± = W. edge Elec Pole R. 3750T

0+55 garage on W. conc. floor 9.3 Back

W-9.3 = floor		3.91	372.10
W-5.7 = E. End conc apron		4.22	371.79
W		4.0	372.0
±		4.1	371.9
E		4.7	371.3
+5 yard		4.5	371.5

0+79 = N. End above Fence on E 0.414 Alley

Garage on E conc. floor 16.1 Back

0+85 " " W " " 8.8 "

E-16.1 floor		4.74	371.27
E		4.3	371.7
±		4.0	372.0

376.01

W

		4.1	371.9	33
+3.5 = E. End. conc e. apron		3.96	372.05	
+8.8 = floor		3.85	372.16	

1+03

W-5. yard		4.8	371.2
W		4.9	371.1
±		4.7	371.3
E		4.9	371.1
+10 = yard.		4.9	371.1

1+38

E-10 yard		4.5	371.5
E		5.0	371.0
±		5.0	371.0
W		5.0	371.0
+2. = yard		4.8	371.2

1+70 Elec Co. Dead Man for cable guy 8.9' E. of ±

1+75 S. Line E+W Alley

W		4.9	371.1	
±		5.28	370.73	
E		4.9	371.1	
T.P.	5.82	376.55	5.24	370.73

376.55  
X sec. E+W Alley

14' E of W Line = W. ch. of Kansas St.		
10.0 S of $\Phi$ = S. ch Ret.	6.81	369.74
" " " = pav	7.37	369.18
$\Phi$ = "	7.39	369.16
10.0' N of $\Phi$ = "	7.43	369.12
" N of $\Phi$ = N. ch Ret.	6.90	369.65
0+00 = W. Line Kansas		
10.6 N of $\Phi$ = S.W. cor. Cor. Iron Bldg.		
10.0 N of $\Phi$ = ch. W. End.	6.61	369.94
10.0 " " " pay " "	6.86	369.69
$\Phi$ " " "	7.03	369.52
9.8 S of $\Phi$ " " "	6.90	369.65
9.8 S of $\Phi$ ch " " = E. End Fence	6.57	369.98
0+25 W		
9.8 S of $\Phi$ = Fence.	5.9	370.7
$\Phi$	5.8	370.8
10.8' N of $\Phi$ = S.W. Cor. Cor. Iron Bldg	6.0	370.6
0+25.5		
11.0' N of $\Phi$ = S.E. Cor. Wooden Bldg.		

376.55

0+41.2

34

11.0' N of $\Phi$ = S.W. Cor. Wooden Bldg	5.8	370.8
$\Phi$	5.6	371.0
9.8 S of $\Phi$ = Fence.	5.9	370.7
0+69		
9.5 S of $\Phi$ = Fence	5.6	371.0
$\Phi$	5.6	371.0
10.3' N of $\Phi$ = E. End Fence	5.6	371.0
0+80		
8.0 S of $\Phi$ = N. edge elec pole		
1+00		
10.1' N of $\Phi$ = W. end above Fence	5.6	371.0
$\Phi$	5.7	370.9
9.8 S of $\Phi$ = Fence line	5.4	371.2
12.5' " " " E+W. concrete walk	5.23	371.32
1+40 = E. Line N+S. Alley.		
9.8 S of $\Phi$ = W. End Fence	5.4	371.2
$\Phi$	5.4	371.2
+10 = N.	5.8	370.8
1+49		
8.4' N of $\Phi$ = S. side Tel Pole		

376.55

1+50 =  $\phi$  N + S Alley

N	5.5	371.1
$\phi$	5.3	371.3
S	5.8	370.7

1+60 = W. Line N + S Alley

S	5.4	371.2
$\phi$	5.4	371.2
N	5.5	371.1

1+61

7.0 S of  $\phi$  = N. side Elc Pole

2+00

N	5.3	371.3
$\phi$	5.7	371.5
S	5.2	371.4

2+08 garage on N. conc. floor 14.5' Back

N-14.5 = floor 4.67 371.88

N-11.5 = S. end conc. apron 4.76 371.79

2+12 garage on S. dirt floor 0.2 Back

S-0.2 = floor 4.9 371.7

2+40 = E. End Flower Bed on S. 7.5 S. of  $\phi$ 

376.55

2+50

S	4.3	372.3
+2.5	4.8	371.8
$\phi$	4.4	372.2
N	4.5	372.1

T.P. 6.60 379.11 4.04 372.51

2+99<sup>84</sup> = E. Line Utah12.6' N of  $\phi$  =  $\phi$  E End 6.55 372.56

" " " pav " " 6.65 372.46

 $\phi$  " " " 6.67 372.447.2' S of  $\phi$  = " " " 6.54 372.577.2' S of  $\phi$  =  $\phi$  " " 6.43 372.6814. W of E = e.  $\phi$  Line7.2' S of  $\phi$  =  $\phi$  6.64 372.47

" " " pav. 7.14 371.97

 $\phi$  " " 7.12 371.9912.5' N of  $\phi$  = " 7.23 371.88" " " "  $\phi$  6.78 372.33

B.M. 6.10 373.01

s. e Idaho  
+ Howard

Grades E+W Alley BIK 120 UH.

See Page 37

(B.M. Hub	S. Line	E+W. Alley	E N+S Alley	see Page
BM "	5.17	375.90		370.73

N. Line E+W. Alley

0+00 = W. Line	Kansas.			369.69
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Brk	0+20 W.			369.95
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Brk	0+40 W			370.10
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1+00 W = E. side New Bldg	5.00	370.90	370.40	+0.50' = 0'-6"
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1+40 W = E. Line N+S Alley	5.11	370.79	370.60	+0.19' = 0'-2 1/4"
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1+50 W = { E N+S Alley W. side New Bldg }	4.83	371.07	370.65	+0.42' = 0'-5"
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1+60 W = W. Line N+S Alley				370.70
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W. End. Bldg	Top wood sill	4.07	371.53	370.65	0.88 = 0'-10 3/4 above Alley Grade
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E " "	" "	4.34	371.52	370.40	1.12 = 1'-1 1/2 " " "
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N. Line

S. Line

Station	N. Line	S. Line
0+00 = W. Line Kansas	Exp 369.69 6.33	376.02 3.87 372.15 4.76 376.91
0+20 B	369.95 6.07 4.07 +2.00	369.94 6.08 4.08 +2.00
0+40 B	370.10 5.92 3.92 +2.00	370.10 5.92 3.92 +2.00
0+90	370.35 5.67 5.50 +0.17	370.35 5.67 3.62 +2.00
1+40 B. Line Alley B	370.60 5.42 5.18 +0.24	370.60 5.42 4.42 +1.00
1+50 4 "		375.88 370.40 5.48 5.00 +0.40
1+60 W. Line Alley B	370.70 5.32 4.96 +0.36	370.70 5.32 4.96 +0.36
2+10	371.40 4.62 4.70 -0.08	371.40 4.62 4.62 0.00
2+60 B	372.10 4.81 4.71 +0.10	372.10 4.81 4.73 +0.08
2+80 B	372.35 4.56 4.70 -0.14	372.36 4.55 4.41 +0.14
3+00 C. Line Utah	Pay 372.46 4.45	Pay 372.57 4.34 4.34 0.00





6-27-39  
mills  
Walker  
Benn

X See Streets for Grade

Establishment in Buena Vista Tract.

C. St 125<sup>th</sup> W of 41<sup>st</sup> to 42<sup>nd</sup>  
41<sup>st</sup> Hill Top to C. St  
42<sup>nd</sup> " " " "  
Broadway 40<sup>th</sup> to 42<sup>nd</sup>  
Hill Top 41<sup>st</sup> to 42<sup>nd</sup>

Indexed  
C.S.K.

166.13

1/4 10.6 155.5  
+5 11.7 154.4  
± 11.7 154.4  
1/4 11.8 154.3  
cl 11.9 154.2  
N 11.5 154.6

± 42<sup>nd</sup> St

Hill Top Drive

B.M. Nails in Pole 2.93 168.80 165.87

41<sup>st</sup> + Hill Top  
Box 1377  
Page 58.

N 11.0 155.1  
cl 11.4 154.7

Set B.M. S. E. Cor. small concrete  
Porch. S. Side caretakers Cottage  
Catholic Cemetery. 0.25 168.55

1/4 11.6 154.5  
± 11.6 154.5

T.P. 7.18 175.19 0.79 168.01

+5 11.6 154.5

P.I. Mon  
S. E. Cor  
Lot 25 HP  
Pipe NW  
Cor 42<sup>nd</sup>  
+ Hill Top

B.M. T.P. 0.79 166.04 9.94 165.25

1/4 11.0 155.1

B.M. T.P. 10.94 166.13 10.85 155.19

cl 11.7 154.4

150 E. of E. line 42<sup>nd</sup> ± Hill Top 11.8 154.3

S 12.0 154.1

100 " " " " ± " 12.2 153.9

50. " " " " ± " 12.3 153.8

+5 12.2 153.9

E. Line 42<sup>nd</sup> St.

0+00 = W. Line 42<sup>nd</sup> St.

S-5 12.7 153.4

-5 12.4 153.7

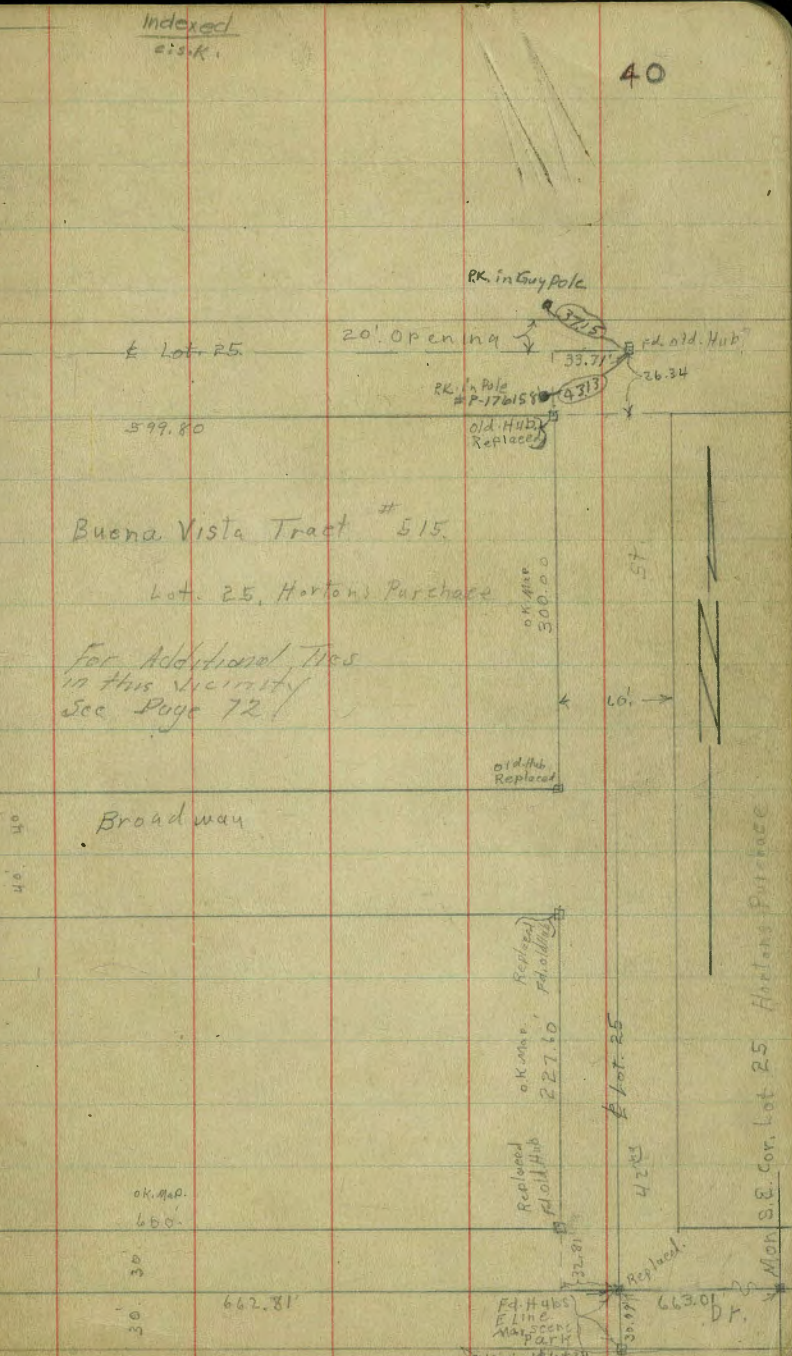
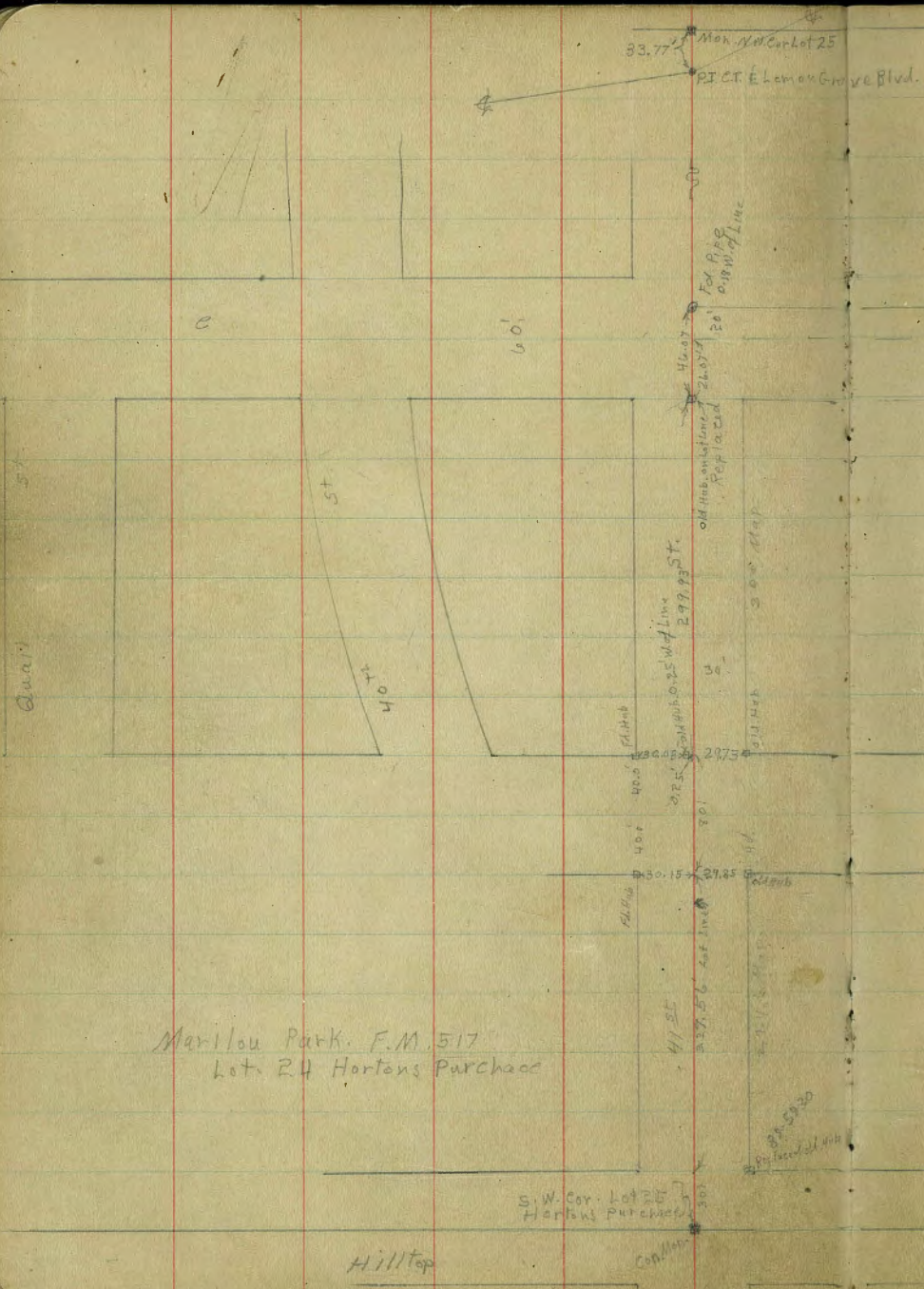
S 11.9 154.2

S 12.3 153.8

cl 11.2 154.9

cl 12.0 154.1

Indexed  
as K.



166.13

0+00 con

14	11.5	154.6
ϕ	11.8	154.3
14	11.8	154.3
el	11.5	154.6
N	11.0	155.1

0+50: 3.8 ϕ 42<sup>nd</sup> st. to South

- 5	11.4	154.7
N	11.4	154.7
el	11.5	154.6
14	11.3	154.8
ϕ	11.2	154.9
14	11.9	154.2
el	12.5	153.6
S	13.1	153.0
+100's	14.5	151.6
+200's	14.9	151.2

1+00

- 5.	11.2	154.9
S.	11.2	154.9
el	10.6	155.5
14	9.7	156.4

166.13

Hill Top

+5	10.4	155.3
ϕ	10.7	155.4
14	10.6	155.5
+7	10.5	155.6
el	10.0	156.1
N	10.6	155.5
+5	10.7	155.4

1+50

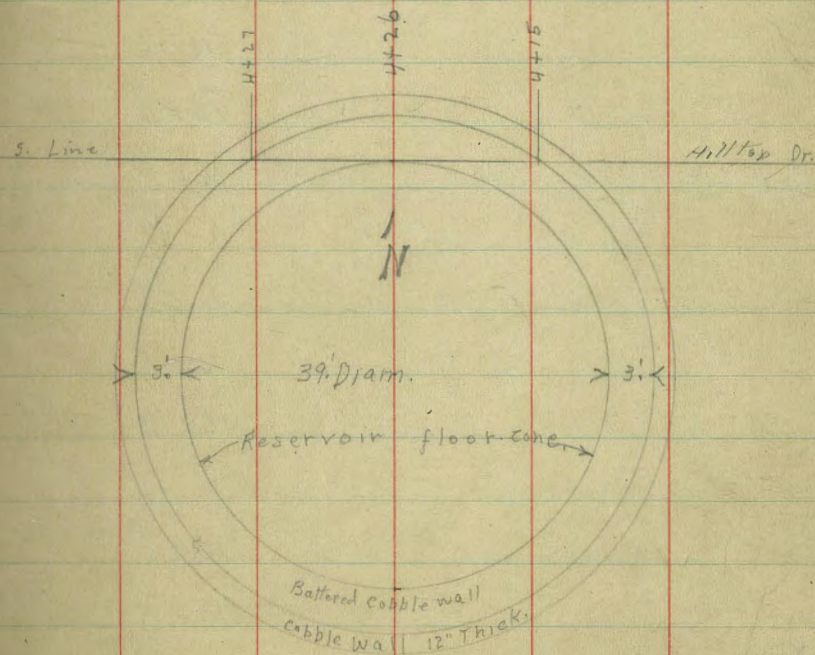
N	8.8	157.3
el	8.7	157.4
+4	9.1	157.0
+6	9.8	156.3
14	9.8	156.3
ϕ	10.1	156.0
+7	10.1	156.0
14	9.3	156.8
el	10.2	155.9
S	11.1	155.0
+5	11.2	154.9

	166.13		
	2+00		
-10	11.6	154.5	
S	11.0	155.1	
cl	10.1	156.0	
+3	8.8	157.3	
1/4	9.0	157.1	
+5	9.4	156.7	
cl	9.4	156.7	
1/4	9.3	156.8	
cl	8.6	157.5	
N	8.6	157.5	
	2+50		
N.	8.1	158.0	
cl.	8.6	157.5	
1/4	9.0	157.1	
cl	9.2	156.9	
+5	9.2	156.9	
1/4	8.8	157.3	
+5	8.5	157.6	
cl	9.7	156.4	
S	10.9	155.2	
+10	11.1	155.0	

	166.13	Hilltop	
	3+00		
-10	10.2	155.9	42
S	9.7	156.4	
cl	8.3	157.8	
1/4	7.4	158.7	
+3	7.4	158.7	
+5	8.2	157.9	
cl	8.1	158.0	
1/4	8.1	158.0	
+4	8.1	158.0	
+5	7.3	158.8	
cl	7.5	158.6	
N.	7.1	159.0	
	ground same as cl		
	3+50 = 11. W. of cl Morrison St.		
N	5.0	161.1	
cl	5.4	160.3	
+6	6.0	160.1	
+7	7.0	159.1	
1/4	7.0	159.1	
cl	6.7	159.4	
1/4	7.0	159.1	
cl	7.6	158.5	
S	8.4	157.7	
0+50 S	10.8	155.3	

	166.13 <sup>v</sup>	
	3+50 (e.w)	
1+00 S	14.5	151.6
1+50 S	17.4	148.7
2+00 S	21.0	145.1
	3+77	
20' N. of S. Line Air Blowoff Valve 4"		
Top of valve	3.5	162.6
	3+90	
S-10	7.6	158.5
S	7.3	158.8
+5	6.7	159.4
cl	5.5	160.6
1/4	5.3	160.8
cl	5.7	160.4
1/4	5.7	160.4
+3	5.7	160.4
+4	4.8	161.3
cl	4.5	161.6
N	3.8	162.3
	4+15	
N	3.2	162.9
cl	4.3	161.8

	166.13 <sup>v</sup>	Hill Top 43
+7	5.0	161.1
1/4	6.0	160.1
cl	5.7	160.4
1/4	5.5	160.6
cl	5.0	161.1
+8 ground N. of wall Reservoir	5.0	161.1
S = Inside Top of cobble wall	4.47	161.66
+4 cone floor	13.4	152.7



166.13'		
4+26.		
S-39. Conc. floor s. sid.	11.40	154.73
S. Line " " foot of wall	11.40	154.73
+3. Top wall inside	4.47	161.66
+5 ground,	5.1	161.0
d.	5.1	161.0
1/4	5.1	161.0
d.	5.9	160.2
1/4	6.3	159.8
+3	6.3	159.8
+5	5.5	160.6
d.	4.3	161.8
N	3.6	162.5
4+37		
N	4.0	162.1
d.	4.6	161.5
+7	5.9	160.2
1/4	6.9	159.2
d.	6.7	159.4
+6	6.3	159.8

166.13'		4+26.
1/4	5.7	160.4 <sup>44</sup>
d.	5.6	160.5
+8 ground	5.0	161.1
S. = inside Top. wall	4.60	161.53
+4 floor of reservoir	11.40	154.73
T		
(T.P. Nail S.W. Guard Post. of Air Valve Sta 3477 T.P. 0.72 163.53)		
	3.32	162.81
4+50		
S	3.8	159.7
d.	3.7	159.8
1/4	3.7	159.8
+2	4.3	159.2
d.	4.4	159.1
1/4	4.8	158.7
+2	4.8	158.7
+7	2.0	161.5
d.	1.9	161.6
N	1.1	162.4

163.53

4+75

N	3.2	160.3
d	3.7	159.8
+5	4.0	159.5
+7	6.3	157.2
14	6.3	157.2
⊕	6.0	157.5
14	6.0	157.5
d	6.3	157.2
S	8.0	155.5
	5+15	
-10	11.2	152.3
S	10.9	152.6
d	9.4	154.1
14	8.6	154.9
⊕	8.4	155.1
14	8.4	155.1
d	8.0	155.5
N	7.5	156.0
+5	7.0	156.5

163.53

5+50

Hilltop

45

-5	8.0	155.5
N	8.4	155.1
d	9.3	154.2
14	9.8	153.7
⊕	9.7	153.8
14	10.1	153.4
+3	10.4	152.7
⊕	11.5	152.0
+5	11.7	151.8
S	13.0	150.5
+10	13.0	150.5
	6+00 = E. Line	41 <sup>st</sup> St.
S-100	20.0	143.5
S-50	17.4	146.1
S	13.4	150.1
+3	12.4	151.1
d	12.0	151.5
14	10.9	152.6
⊕	10.4	153.1



163.53

6 + odcow)

1/4	10.0	153.5
cb	8.8	154.7
N	7.7	155.8
± 41 <sup>st</sup> St.		
N.	6.5	157.0
d	8.6	154.9
1/4	9.7	153.8
±	10.2	153.3
1/4	11.2	152.3
d	12.4	151.1
S	13.6	149.9
+ 50.0	17.7	145.8
+ 100.0	19.7	143.8
W. Line 41 <sup>st</sup>		
S-100.	19.7	143.8
S-50.	17.0	146.5
S	12.6	150.9
cb	11.2	152.3
1/4	10.4	153.1
±	9.8	153.7

163.53

Hilltop

MON. 10.54

1/4	9.6	153.9
cb	8.4	155.1
N	7.8	155.7
± Hilltop Dr.		
50' W. of W. Line 41 <sup>st</sup>	8.3	155.2
100' " " " "	5.7	157.8
Set. B.M. ± Men	10.54	152.99
41 <sup>st</sup> St. X Sec.		
0+00 = N. Line Hilltop Dr		
E	7.7	155.8
d	7.1	156.4
1/4	6.7	156.8
±	6.5	157.0
1/4	6.6	156.9
cb	7.1	156.4
W.	7.8	155.7
+10	7.8	155.7

41<sup>st</sup> + Hilltop  
SW. Cor. Lot. 25

		163.53		
	0750	North.		
W			2.4	161.1
d			2.8	160.7
1/4			3.0	160.5
⊕			2.3	161.2
1/4			2.4	161.1
d			2.7	160.8
E			2.8	160.7
T.P.	12.92	174.63	1.82	161.71 <sup>✓</sup>
		1700		
E			11.0	163.6
d			11.0	163.6
1/4			11.0	163.6
⊕			10.6	164.0
1/4			10.8	163.8
d			10.4	164.2
W			10.6	164.0
		1450		
W			7.4	167.2
d			8.0	166.6
1/4			8.3	166.3

		B.M. chK			41 <sup>st</sup> St
B.M. B.P.	13.08	132.47 <sup>v</sup>		125.39 <sup>✓</sup>	N. 2. 41 <sup>st</sup> Market.
T.P.	12.51	150.21	0.77	137.70 <sup>✓</sup>	
T.P.	7.03	156.54	0.70	149.51	
B.M. E Mon				3.55	Hill Top 41 <sup>st</sup> St. P <sub>47</sub> + 46
				174.63	
⊕				8.1	166.5
1/4				8.3	166.3
⊕				8.6	166.0
E				8.6	166.0
				1775	
E				6.3	168.3
d				6.9	167.7
1/4				6.7	167.9
⊕				6.0	168.6
1/4				5.8	168.8
d				5.7	168.9
W				5.6	169.0

174.63

2+27 ~~st~~ = S. Line Bdw.

w	2.0	172.6
d	2.8	171.8
ly	3.4	171.2
ϕ	3.6	171.0
ly	4.1	170.5
cl	4.2	170.4
E	4.5	170.1

0+00 = N. Line Bdw

E	0.1	174.5
cl	1.5	173.1
ly	1.9	172.7
ϕ	1.9	172.7
ly	2.7	171.9
cl	2.9	171.7
W = B.M. Cor. Hdb	2.93	171.70

0+25 N

-15	5.6	169.0
w	4.8	169.8
cl	3.7	170.9

174.63

41<sup>st</sup> St.

48

ly	3.0	171.6
ϕ	1.2	173.4
ly	2.5	173.1
cl	1.9	172.7
E	1.5	173.1

T.P.	2.07	180.77	2.93	171.70
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0+50 N

E	7.1	173.7
cl	7.0	173.8
ly	7.8	173.0
ϕ	8.7	172.1
+6	10.5	170.3
ly	10.6	170.2
cl	11.3	169.5
w	12.4	168.4
+15	13.4	167.0

N.W. Cor  
41<sup>st</sup> + Bdw

180.77

0+75

W-20	16.0	164.8
W.	13.3	167.5
eb	11.5	169.3
1/4	10.8	170.0
ϕ	9.8	171.0
1/4	8.8	172.0
eb	7.7	173.1
E	6.8	174.0

1+00

E	5.4	175.4
eb	6.6	174.2
1/4	7.3	173.5
ϕ	8.1	172.7
1/4	9.5	171.3
eb	10.3	170.5
W	11.1	169.7
+20	12.8	168.0

1+25

-15	8.2	172.6
-----	-----	-------

180.77

41.25

W	8.2	172.6	49
eb	7.7	173.1	
1/4	6.6	174.2	
ϕ	5.8	175.5	
1/4	4.0	176.8	
eb	4.0	176.8	
E	3.5	177.3	

1+50

E	0.9	179.9
eb	0.9	179.9
1/4	1.0	179.8
ϕ	2.2	178.6
1/4	3.5	177.3
eb	4.3	176.5
W	4.8	176.0
+15	4.8	176.0

1+75

W	1.6	179.2		
eb	1.3	179.5		
T.P.	9.78	189.92	0.63	180.14

189.92

2+75 corr

1/4	9.4	180.1
Φ	8.8	181.1
1/4	8.6	181.3
d	8.3	181.6
E	7.9	182.0

2+00

e	5.7	184.2
cl	6.4	183.5
1/4	6.7	183.2
Φ	7.0	182.9
1/4	7.2	182.7
d	7.5	182.4
w	8.0	181.9

2+25

w	6.6	183.3
cl	6.3	183.6
1/4	6.0	183.9
Φ	5.2	184.7
1/4	5.2	184.7

189.92

41st st

d	5.0	184.9
---	-----	-------

E	4.3	185.6
---	-----	-------

2+50

e	4.0	185.9
---	-----	-------

cl	4.4	185.5
----	-----	-------

1/4	4.8	185.1
-----	-----	-------

Φ	4.8	185.1
---	-----	-------

1/4	4.3	185.6
-----	-----	-------

cl	4.2	185.7
----	-----	-------

w	4.3	185.6
---	-----	-------

2+75

w	5.0	184.9
---	-----	-------

cl	4.9	185.0
----	-----	-------

1/4	4.8	185.1
-----	-----	-------

Φ	4.5	185.4
---	-----	-------

1/4	4.3	185.6
-----	-----	-------

cl	3.6	186.3
----	-----	-------

E	2.8	187.1
---	-----	-------

189.92

3+00 = S. Line C. St

E	3.1	186.8
el	2.5	187.4
1/4	2.7	187.2
ϕ	4.1	185.8
1/4	4.8	185.1
el	5.0	184.9
W	5.1	184.8

E. St. 7 sec. 60' wide W. of ϕ 41<sup>st</sup>0+00 = W. Line 41<sup>st</sup> St.

N	5.3	184.6
+10 = el	5.0	184.9
+20 = 1/4	4.2	185.7
+30 = ϕ	3.7	186.2
+40 = 1/4	4.1	185.8
+50 = el	4.9	185.0
+60 = S	5.0	184.9

189.92

0+30 west.

C. St

51

S	5.5	184.4
el	5.6	184.3
1/4	5.5	184.4
ϕ	5.8	184.1
1/4	6.1	183.8
el	6.3	183.6
N	6.6	183.3

0+65 W

N	2.0	181.9
el	2.5	182.4
1/4	6.6	183.3
ϕ	6.6	183.3
1/4	6.9	183.5
el	5.9	184.0
S	5.5	184.4

189.92

1+00 W

S	8.1	181.8
cb	8.1	181.8
1/4	8.1	181.8
1/4	8.1	181.8
1/4	8.1	181.8
cb	7.8	182.1
N.	8.4	181.5

1+25 Top canyon

N	11.1	178.8
cb	11.1	178.8
1/4	11.1	178.8
1/4	11.1	178.8
1/4	11.7	178.2
cb	11.9	178.0
S.	12.0	177.9

T.P. B.M. Pipe 3.17 188.89 4.20 185.72

S.W. Cor. of  
N.W. 1/4 of  
Lot 25.E. 5th X Sec. 41<sup>st</sup> East.

188.89

E. 5th

50.

41<sup>st</sup> St = W. line Lot 25.

S	3.0	185.9
+10 N	2.1	185.8
+20	3.3	185.6
+30 1/2 to W.	3.5	185.4
+40	3.7	185.2
+46 <sup>07</sup> N line to E.	3.2	185.7
+50	3.4	185.5
+60 = N. Line to W.	3.5	185.4

70' E of 1/4

8+46 N	3.4	185.5
+40	3.4	185.5
+30	3.0	185.9
+20	2.7	186.2
+10	2.6	186.3
S.	1.5	187.4

30' E. of 1/4 = E Line 41<sup>st</sup>

S	2.2	186.7
+10 N	2.6	186.3

188.89		8. Line (e.w.)	
st 20 N	2.6	186.3	
+30	2.7	186.2	
+40	2.8	186.1	
+46 = N = Gate to yard	2.8	186.1	
	0+50 E		
+50	3.2	183.7	
5 +46 N = N Line	5.0	183.9	
+40	4.4	184.1	
+30	4.4	184.5	
+20	3.7	185.2	
+10	3.5	185.4	
S	2.7	186.2	
	0+75		
S	2.2	186.7	
+8	3.3	185.6	
+10	4.6	184.3	
+20	4.4	184.1	
+30	5.8	183.1	
+40	6.5	182.4	
+46 <sup>1</sup> = N. Line	2.0	181.9	
+50 N			

188.89		e. st.	
	1+00		33
+60	9.5	179.4	
+46	9.0	179.9	
+40	8.3	180.6	
+30	7.2	181.7	
+20	6.3	182.6	
+10	6.3	182.6	
+4.6 = Elev. Pole			
S	5.5	183.4	
	1+30		
S	7.2	181.7	
+10	8.5	180.4	
+20	8.5	180.4	
+30	8.3	180.6	
+40	9.1	179.8	
+46	10.0	178.9	
+60	11.8	177.1	
	1+50		
st 60	14.6	174.3	
+46	12.6	176.3	



	188.89		
+40	11.8	177.1	
+30	11.0	177.9	
+20	10.0	178.9	
+10	9.3	179.6	
+7	8.5	180.4	
S	6.0	182.9	
	1+85		
S	10.1	178.8	
+10	11.4	177.5	
+20	12.3	176.6	
+30	13.4	175.5	
+40	15.0	173.9	
+46	15.4	173.5	
S+40 N	17.0	171.9	
	2+05		
S+40 N	12.7	169.2	
+46 N = N line	17.2	171.7	
+40	16.2	172.7	
+30	14.5	174.4	
+20	12.7	176.2	
+10	11.4	177.5	

	188.89		C. 95.1
+5	10.7	178.2	54
S	9.1	179.8	
	2+20		
S	9.0	179.9	
+6	11.0	177.9	
+10	11.2	177.7	
+20	12.7	176.2	
T.P.	0.86	177.10	
	12.65	176.24	
+30	3.0	174.1	
+40	4.4	172.7	
+46 <sup>2</sup> = N line	5.3	171.8	
+40 N	7.4	169.7	
	2+40		
+40 N	6.5	170.6	
+46 <sup>2</sup> N	4.8	172.3	
+40	4.5	172.6	
+30	3.6	173.5	
+20	2.9	174.2	
+10	1.1	176.0	
S	0.5	176.6	

	177.10			
S	0.5	176.6		
+10	1.2	175.9		
+20	1.9	175.2		
+30	3.9	173.2		
+40	4.6	172.5		
+46 <sup>2</sup> = N. Line	5.9	171.2		
+47 <sup>5</sup> = S. End entrance Garage	5.9	171.2	dirt floor	
2+80 Eucalyptus Tree 12" Diam	S+41.1			
2+86 " " " 6" " "	S+41			
2+96 Tel Co Dead man	S+41			
2+99 Elec Pole	S+45			
3+03 Euc. Tr. 12" Diam	S+41			
3+05 Meter Box	S+38			
3+14 Tel Pole	S+39			
3+28 Acacia 3" Diam	S+40			
3+40 " " "	S+40			
3+48 Meter Box	S+37			
3+50 Pepper 2" "	S+48			
	3+00			
+60	6.1	171.0		
S+46 <sup>2</sup> = N. Line	5.2	171.9		
+40	4.9	172.2		
+30	4.5	172.6		
+20	3.8	173.3		

	177.10			
+10	3.3	173.8		53
+5	3.1	174.0		
S	1.7	175.4		
	3+13			
S	3.6	173.5		
+10	4.0	173.1		
+20	4.1	173.0		
+30	4.6	172.5		
+40	5.1	172.0		
+46 <sup>3</sup> = N. Line	5.4	171.7		
+60	6.4	170.7		
	3+25			
+56 <sup>5</sup> porch	6.0	171.1		
+56 ground.	6.6	170.5		
+46	6.7	170.4		
+40	6.5	170.6		
+30	5.4	171.7		
+20	4.5	172.6		
+10	4.3	172.8		
S.	4.0	173.1		

172.10

3+52

S	6.6	170.5
+10	8.1	169.0
+20	8.4	168.7
+30	9.0	168.1
+40	9.3	167.8
+46 <sup>2</sup> = N. Line	8.9	168.2
+60	9.0	168.1

3+60

S+49 = Single garage dirt floor	12.2	164.9
+46 <sup>2</sup>	12.2	164.9
+40	11.2	165.9
+30	10.5	166.6
+20	9.3	167.8
+10	9.1	168.0
S	8.4	168.7

3+75

S	10.2	166.9
+10	11.2	165.9
+20	11.5	165.6
+30	13.0	164.1
T.P.	0.30	164.48
	12.92	164.18

164.48

c.st

+40	2.0	162.5
+46 <sup>3</sup> = N	2.5	162.0
+60	3.2	161.3
+90 <sup>3</sup> N	14.7	149.8
+60 N	11.4	152.9
+46 <sup>3</sup> N = N. Line	9.5	155.0

4+13

+40	8.6	155.9
+30	8.0	156.5
+20	7.0	157.5
+10	6.0	158.5
S	4.4	160.1
+20 S	2.0	162.5

4+38 o.k. for Culvert.

S-30' S	4.5	160.0
S	7.1	157.4
+10	7.3	157.2
+20	7.3	157.2
+30	8.1	156.4
+40	10.0	154.5
+46 <sup>3</sup> = N	10.6	153.9

	164.48		
+60' N.	4+34 (con)	11.5	
5+100' N		14.7	149.8
	4+55		
5+80' N.		8.8	155.7
+60		7.1	157.4
+46 <sup>2</sup>		6.6	157.9
+40		6.2	158.3
+30		5.5	159.0
+20		5.3	159.2
+10		5.3	159.2
S		5.0	159.5
+25' S.		3.8	160.7
	4+75		
-25' S		1.5	163.0
S		1.9	162.6
+10' N		1.5	163.0
+20		0.9	163.6
+30		0.7	163.8
+40		0.3	164.2
+46 <sup>3</sup> = N. Line		1.0	163.5
5+80' N		2.9	161.6

		164.48			8.5+
T.P.	12.40	176.47	5+00	0.41	164.07
5+60' N				6.2	170.3
5+46 <sup>2</sup> = N. Line				6.2	170.3
+40				6.3	170.2
+30				7.4	169.1
+20				8.3	168.2
+10				9.3	167.2
S				9.3	167.2
+25' S.				9.9	166.6
			5+25		
-10				5.1	171.4
S				4.9	171.6
+10				4.4	172.1
+20				3.5	173.0
+30				3.2	173.3
+40				2.8	173.7
+46 <sup>3</sup>				2.1	174.4
+40				2.2	174.3
T.P.	12.77	188.91		0.33	176.14

	188.91	
	5+50	
+60N	12.3	176.6
+46 <sup>3</sup> = N Line	11.6	177.3
+40	11.7	177.2
+30	11.6	177.3
+20	11.7	177.2
+10	12.0	176.9
S	12.4	176.5
+10	13.0	175.9
	5+75	
S	8.0	180.9
+10	7.7	181.2
+20	7.0	181.9
+30	7.4	181.5
+40	8.1	180.8
+46 <sup>2</sup> = N Line	8.3	180.6
+60N	9.2	179.7
5+97	4.5 N of S. line = Elec Pole	176.58
	5+99.80 = W. Line 42 <sup>nd</sup> St.	
+60N	4.9	184.0
+46 <sup>2</sup> = N Line	4.8	184.1
+40	4.8	184.1
+30	4.8	184.1

	188.91	
+20	4.1	184.8
+10	4.6	184.3
S	4.6	184.3
Set B.M.	4.57	184.34 = 184.32
		RR Spk. Elec. Pole 217 W 59 S.W. Cor 42 <sup>nd</sup> + C. St. Page 62
		42 <sup>nd</sup> St. X Sec. 60. wide
B.M. Pipe	12.18	167.37
		N.W. cor. 42 <sup>nd</sup> + Hill Top Page 39
		155.19
		0+00 = N. Line Hill Top Dr.
W	12.3	155.1
el	12.0	155.4
114	12.1	155.3
⊕	12.2	155.2
114	12.2	155.2
el	12.2	155.2
E	12.8	154.6
+20	12.8	154.6
	0+20 North	
E-10	12.5	154.9
E	12.3	155.1

	167.37		
cl	12.0	155.4	
ly	11.7	155.7	
cl	11.6	155.8	
ly	11.3	156.1	
cl	10.8	156.6	
W	10.5	156.9	
	0750 N		
W	10.2	156.8	
cl	10.5	156.9	
ly	10.4	157.0	
cl	10.6	156.8	
ly	10.7	156.7	
cl	11.0	156.4	
E	11.7	155.7	
ly	11.7	155.7	
	1400		
-10	10.9	156.5	
E	10.7	156.7	
cl	10.4	157.0	
ly	9.2	158.2	

	167.37	424 ST
cl	9.3	158.1
ly	9.6	157.8
cl	9.5	157.9
W	9.5	157.9
+10	9.5	157.9
	1750 N	
-10	8.1	159.3
W	7.9	159.5
cl	8.1	159.3
ly	7.4	159.6
cl	7.7	159.7
ly	7.7	159.7
cl	8.0	159.4
E	8.3	159.1
+10	8.5	158.9
	2400	
E	5.0	162.4
cl	5.2	162.2
ly	5.6	161.8
cl	5.5	161.9

	167.37		
1/4	4.0	161.4	
cl	6.1	161.3	
W	5.8	161.6	
+10	5.8	161.6	
	2+27 <sup>6</sup> = S. Line Bdw. 80' wide		
RM W. on Hub	4.63	162.74	
cl	4.8	162.6	
1/4	4.7	162.7	
±	4.3	163.1	
1/4	4.3	163.1	
cl	4.0	163.4	
±	3.6	163.8	
	± Bdw.		
±	1.0	166.4	
cl	1.5	165.9	
1/4	2.2	165.2	
±	2.3	165.1	
1/4	2.7	165.7	
cl	2.6	164.8	
W	2.7	164.7	

	167.37		
	0+00 = N. Line Bdw.		
W.	0.9	166.5	
cl	0.7	166.7	
1/4	9.5	166.9	
±	0.2	167.2	
T.P.	12.96	180.11	0.22 167.15
1/4			13.0 167.1
cl			12.7 167.4
±			12.4 167.7
	0+50		
±			9.0 171.1
cl			9.2 170.9
1/4			9.8 170.3
±			9.8 170.3
1/4			10.4 169.7
cl			11.0 169.1
W			11.4 168.7
+10			11.5 168.6

42.55

F11

	180.11	1400		
-10			9.0	171.1
w			9.0	171.1
el			8.1	172.0
1/4			7.6	172.5
±			6.9	173.2
1/4			6.8	173.3
el			6.0	174.1
E			5.7	174.4

	1750			
E			3.1	177.0
el			3.4	176.7
1/4			4.4	175.7
±			4.6	175.5
1/4			5.4	174.7
el			6.0	174.1
w.			6.3	173.8
+10			6.5	173.6

	1785			
w. -10			4.8	175.3
w.			4.7	175.4

	180.11			
d			4.5	175.6
1/4			3.9	176.2
±			3.1	177.0
1/4			2.9	177.2
el			1.8	178.3
E			1.2	178.9
T.P.	12.83	192.41	0.53	179.58
		2+25		

E			10.5	181.9
d			10.8	181.6
1/4			11.3	181.1
±			11.3	181.1
1/4			11.9	180.5
el			12.4	180.0
w			12.7	179.7
+10			13.6	178.8

	2+50			
-10			10.9	181.5
w			10.6	181.8
d			10.0	182.4

42st.

62



192.41

2+50 (con)

1/4	9.1	183.3
±	8.5	183.9
1/4	8.5	183.9
el	8.0	184.4
E.	7.6	184.8

2+75

E.	4.3	188.1
el	4.3	188.1
+5	4.6	187.8
+7	5.8	186.6
1/4	6.1	186.3
±	6.3	186.1
1/4	7.0	185.4
el	8.0	184.4
W	9.2	183.2
+10	10.5	181.9

3+00 = S. line C. st

W	8.1	184.3
el	7.0	185.4
1/4	5.9	186.5
chk. BM. SpK. P.de	8.09	184.32

S.W. 42<sup>nd</sup>  
+ C. Sts

192.41

42<sup>nd</sup> St.

62

±	5.0	187.4
1/4	4.6	187.8
d	3.3	189.1
E	2.8	189.6
+50	1.1	181.3

26.34 N of S = ± lot 25

E-50	+1.3	193.7
E	0.7	191.7
el	1.9	190.5
1/4	3.2	189.2
±	4.5	187.9
1/4	5.4	187.0
el	6.5	185.9
W	8.0	184.4

46<sup>34</sup>

W	8.3	184.1
el	7.2	185.2
1/4	6.1	186.3
±	5.1	187.3
1/4	4.0	188.4

	192.41		42 <sup>nd</sup>
dr	2.3	190.1	
E	0.9	191.5	
+ 20	40.5	192.9	
+ 50	+ 3.5	195.9	

Broadway X. Sec.

80' wide 14' chs. - 13' 1/4"

B.M. Hub 12.30 175.04 162.74 S.W. Bdw +42<sup>nd</sup>

0+00 = W. Line 42<sup>nd</sup> St

S	12.3	162.7
el	11.9	163.1
1/4	11.2	163.8
⊕	10.4	164.6
1/4	10.2	164.8
+ 2	9.4	165.6
el	8.9	166.1
N	8.6	166.4
	0+50 W	
N	8.7	166.3
dr	9.6	165.4

	175.04	Bdw
1/4	10.2	164.8
+ 1	10.7	164.3
⊕	10.8	164.2
1/4	11.4	163.6
el	11.9	163.1
S	12.0	163.0
+ 5	12.0	163.0
	0+85	
- 10	13.4	161.6
S	12.3	162.7
dr	11.0	164.0
1/4	10.6	164.4
⊕	10.6	164.4
+ 12	10.5	164.5
1/4	9.6	165.4
el	8.5	166.5
N	7.7	167.3

	175.04	
	+10	
N	6.9	168.1
cl	7.8	167.2
14	9.0	166.0
+2	10.2	164.8
±	10.6	164.4
14	11.5	163.5
cl	12.2	162.8
S	13.2	161.8
+10	13.6	161.4
	+25	
-10	13.6	161.4
S	13.2	161.8
cl	12.6	162.4
14	11.9	163.1
±	10.6	164.4
14	10.1	164.9
cl	9.2	165.8
N.	7.8	167.2

	175.04		Bdw.
	+50		
N	7.8	167.2	64
cl	8.3	166.7	
14	8.8	166.2	
+2	10.1	164.9	
±	10.3	164.7	
14	11.0	164.0	
cl	12.5	162.5	
S	12.9	162.1	
+10	13.6	161.4	
	+85		
	12.1	162.9	
S	11.6	163.4	
cl	11.1	163.9	
14	10.6	164.4	
±	9.6	165.4	
14	9.6	165.4	
d	9.1	165.1	
N	8.1	166.9	
+5	7.7	167.3	

175.04

2+25

-5	6.9	168.1
N	7.1	167.9
d	7.5	167.5
1/4	7.7	167.3
+	7.4	167.6
1/4	7.7	167.3
d	8.6	166.4
S	9.0	166.0
+10	9.0	166.0

2+50

-10	6.6	168.4
S	6.3	168.7
d	6.0	169.0
1/4	5.0	170.0
+	4.9	170.1
1/4	4.8	170.2
d	5.6	169.4
N	5.7	169.3
+10	5.2	169.8

175.04

2+75

-10	3.5	171.5
N	3.1	171.9
d	3.0	172.0
1/4	2.7	172.3
+	2.6	172.4
1/4	3.2	171.8
d	4.0	171.0
S	4.5	170.5
+10	4.8	170.2

3+00

S	2.2	172.8
T.P.	8.05	181.58
d	1.51	173.53
1/4	8.0	173.6
1/4	7.4	174.2
+	7.0	174.6
+11	7.1	174.5
1/4	6.1	175.5
d	5.5	176.1
N	5.3	176.3

Bdw.

lot stake  
S Line 3+00

181.58  
3+25

N	2.7	178.9
d	2.9	178.7
14	4.2	177.4
+2	5.2	176.4
d	5.2	176.4
4	6.0	175.6
d	7.1	174.5
S	8.1	173.5
+10	9.0	172.6

3+50

-10	9.5	172.1
S	8.5	173.1
d	7.3	174.3
4	5.8	175.8
d	4.5	177.1
+11	4.7	176.9
14	3.3	178.3
d	2.0	179.6
N	1.3	180.3

181.58  
3+75

N	0.0	181.6
d	1.0	180.6
14	2.6	179.0
+3	4.5	177.1
d	4.4	177.2
+10	5.0	176.6
14	6.1	175.5
d	7.5	174.1
S	8.9	172.7
+10	9.7	171.9

4+10

-10	10.1	171.5
S	9.0	172.6
d	7.5	174.1
14	5.6	176.0
+3	5.0	176.6
d	4.7	176.9
+10	4.7	176.9
14	3.6	178.0
d	2.0	179.6
N	0.8	180.8

Bdw.  
68

181.58

4+35

N	0.4	181.2
ch	1.7	179.9
1/4	3.2	178.4
+3	4.7	176.9
±	5.0	176.6
+8	5.5	176.1
1/4	6.6	175.0
ch	7.9	173.7
5	9.1	172.5
+10	9.8	171.8

4+75

-10	10.0	171.6
5	9.6	172.0
ch	8.6	173.0
1/4	7.4	174.2
+5	6.2	175.4
±	5.8	175.8
+11	5.8	175.8
1/4	4.3	177.3
ch	2.9	178.7
N	2.2	179.4

181.58

5+00

N	3.7	177.9
ch	4.7	176.9
1/4	5.3	176.3
+1	6.6	175.0
±	6.6	175.0
+6	7.1	174.5
1/4	8.0	173.6
ch	8.7	172.9
5	10.0	171.6
+10	11.1	170.5

5+50

-10	12.0	169.6
5	11.4	170.2
ch	9.2	172.4
1/4	8.1	173.5
±	7.8	173.8
+12	7.8	173.8
1/4	7.0	174.6
ch	7.1	174.5
N	6.2	175.4

Bdu.

67

181.58

5+75

N	5.7	175.9
el	6.9	174.7
1/4	8.4	173.2
⊕	8.5	173.1
+7	8.5	173.1
1/4	9.7	171.9
dr	10.3	171.3
s	11.3	170.3
+10	11.7	169.9
6+00 = 2 lines 41 <sup>st</sup> st.		
s	11.4	170.2
el	10.8	170.8
1/4	10.0	171.6
+5	9.0	172.6
⊕	8.9	172.7
1/4	8.8	172.8
el	7.8	173.8
N	7.2	174.4

181.54

E. el

Bdo

N	8.5	173.1	68
el	8.1	173.5	
1/4	8.8	172.8	
⊕	8.9	172.7	
1/4	9.5	172.1	
el	10.7	170.9	
s	11.3	170.3	
⊕ 41 <sup>st</sup> st			
s	10.6	171.0	
el	10.2	171.4	
1/4	9.6	172.0	
⊕	9.1	172.5	
1/4	8.7	172.9	
el	8.0	173.6	
N	9.0	172.6	
W. el. 41 <sup>st</sup> st			
N	9.9	171.7	
di	9.6	172.0	
1/4	9.2	172.4	
⊕	9.1	172.5	

	181.58	W. d. (Leon)		
S. 1/4		8.9	172.7	
el		9.4	172.2	
S		9.8	171.8	
0+00 = W Line Bdw.				
S		9.0	172.6	
el		8.8	172.8	
1/4		8.9	172.7	
el		9.2	172.4	
1/4		9.6	172.0	
el		9.7	171.9	
N Hub.		9.88	171.70	

T.P. Hub 7.28 ✓ 178.98 ✓ 9.88 171.70 ✓ Page 48

	0+35 W.			
N-10		8.8	170.2	
N		8.6	170.4	
el		7.5	171.2	
1/4		6.3	172.7	
el		5.3	173.7	

	178.98	Bdw.	
1/4		4.0	175.0 69
el		4.2	174.8
S		5.0	174.0
0+70 W			
S		3.4	175.6
el		3.5	175.5
1/4		4.2	174.8
el		5.6	173.4
1/4		6.4	172.2
el		8.5	170.5
N		9.9	169.1
1/4		10.6	168.4

	1+00		
-10		12.5	166.5
N		11.2	167.8
el		9.2	169.8
1/4		7.2	171.8
el		5.3	173.7
1/4		3.0	176.0
el		1.7	177.3
S		2.1	176.9



178.98

1+30

S	1.5	177.5
dr	1.3	177.7
+6	2.5	176.5
14	3.9	175.1
±	6.7	172.3
14	8.1	170.9
d	9.8	169.2
N	11.3	167.7
+10	12.0	167.0

1+45

-10	13.6	165.4
N	12.0	167.0
el	9.7	169.3
14	8.9	170.1
±	7.5	171.5
14	4.8	174.2
el	2.6	176.4
S	1.2	177.8

178.98

1+70

Bdw.

S	1.9	177.1
+10	2.4	176.6
el	3.1	175.9
14	6.5	172.5
±	8.8	170.2
14	10.2	168.8
d	11.7	167.3
N	12.9	166.1
+10	14.0	165.0

1+95

-10	15.2	163.8
N	14.4	164.6
el	13.0	166.0
14	11.1	167.9
±	10.0	169.0
14	7.3	171.7
el	5.3	173.7
S	4.2	174.8

	178.98		
S	2+15	4.8	174.2
dr		6.1	172.9
1/4		8.7	170.3
±		11.4	167.6
1/4		12.3	166.7
dr		13.8	165.2
N		15.4	163.6
+10		16.6	162.4

	2+35		
-10		17.2	161.8
N		15.7	163.3
dr		13.2	165.8
1/4		11.7	167.3
±		11.4	167.6
1/4		11.1	167.9
dr		9.3	169.7
S.		8.2	170.8

	178.98		Bdw
S	2+55	10.8	168.2
dr		11.6	167.4
1/4		13.2	165.8
±		12.6	166.4
1/4		13.8	165.2
dr		15.7	163.3
N		18.2	160.8
+15		20.4	158.6



60' wide - 10' els - 10' 1/4's

BM Pipe 6.10 161.29<sup>v</sup> 155.19 N.W. cor  
42<sup>nd</sup> + H. 11<sup>th</sup> St

0+00 = E. line 42<sup>nd</sup> Page 39.

0+50 E

- 5	7.4	153.9
N	7.6	153.7
el	7.4	153.9
1/4	7.4	153.9
⊕	7.5	153.8
1/4	7.4	153.9
el	8.2	153.1
+ 4 = BM Fence	8.6	152.7
S	8.6	152.7
+ 10	8.8	152.7
1+00 E.		
- 10	9.4	151.9
S	8.9	152.4
+ 9' = BM Fence	8.2	153.1
el	7.5	153.8
1/4	7.4	153.9
⊕	7.4	153.9
1/4	7.2	154.1
el	7.4	153.9

161.29<sup>v</sup>

6.8 154.5 73

6.8 154.5

1+50 E

- 5	6.0	155.3
N	6.3	155.0
el	6.6	154.7
1/4	7.0	154.3
⊕	7.0	154.3
1/4	7.2	154.1
el	8.2	153.1
S	8.6	152.7
+ 10	9.0	152.3
2+00		
- 10	8.3	153.0
S	7.7	153.6
el	7.1	154.2
1/4	6.4	154.9
⊕	6.3	155.0
1/4	6.3	155.0
el	5.4	155.5

161.29

N	5.0	156.3
+5	4.7	156.6
	2+50	
-5	4.1	157.2
N	4.5	156.8
cl	4.7	156.6
14	5.3	156.0
♀	5.3	156.0
14	5.3	156.0
cl	6.9	154.4
S	7.1	154.2
+10	7.4	153.9
	3+00 E	
-10	6.4	154.9
S	6.2	155.1
cl	5.5	155.8
14	4.3	157.0
♀	4.4	156.9
14	4.3	157.0
cl.	3.4	157.9

161.29

Hill top

N	2.7	158.6	74
+5	2.6	158.7	
	3+50 E		
-5	1.5	159.8	
N	1.6	159.7	
cl	2.4	158.9	
14	3.0	158.3	
♀	3.2	158.1	
14	2.8	158.5	
cl	4.2	157.1	
S	4.8	156.5	
+10	5.1	156.2	
	3+53	21. S. of E. end. B. W. Fence	
	4+00		
-10	3.3	158.0	
S	3.2	158.1	
cl	2.9	158.4	
14	1.4	159.9	
♀	1.6	159.7	
14	1.7	159.6	
cl	0.8	160.5	
N	+0.2	161.5	

161.29

170.57

Hilltop Dr.

T.P.

10.91

170.57

1163

159.66

114

7.0

163.6

4+10 - 19' N of  $\phi$  Pepper Tree 5 Trunks

+5

7.0

163.6

4+50E

 $\phi$ 

6.3

164.3

N

7.3

163.6

+5.3

 $\phi$  S. edge bottom step

5.33

165.24

+5

8.2

162.4

+6.3

 $\phi$  S. edge Top step  
S. End. Conc. walk

4.77

165.80

 $\phi$ 

8.4

162.2

N

and walk.

4.54

166.03

+5

9.1

161.5

5+27<sup>28</sup> W Line 43<sup>rd</sup> St 50' wide

114

9.1

161.5

N

4.2

166.4

 $\phi$ 

8.9

161.7

 $\phi$ 

6.0

164.6

114

8.7

161.9

44

5.7

164.9

 $\phi$ 

9.4

161.2

 $\phi$ 

6.0

164.6

S

10.1

160.5

114

6.30

164.3

+10

10.4

160.2

 $\phi$ 

N side yard.

6.4

164.2

Lawn

4+70 21.75 of  $\phi$  = Pepper Tree 16" Diameter

S

6.8

163.8

"

5+05

+10

7.0

163.6

"

-10

7.5

163.1

Lawn

25' E. of W. Line =  $\phi$  43<sup>rd</sup>

6.5

164.1

Lawn

S

7.2

163.4

-10

6.4

164.2

"

 $\phi$ 

= N. edge of yard.

7.0

163.6

S

6.4

164.2

"

114

7.0

163.6

 $\phi$ 

N. edge yard.

5.7

164.9

"

 $\phi$ 

7.0

163.6

114

5.6

165.0

170.57  
#43rd

±	5.3	165.4
1/4	5.0	165.6
cb	4.5	166.1
N	3.7	166.9
+65' N.	0.2	170.4

0+00 = E. line 43rd st.

N	3.0	167.6	
+8	3.5	167.1	
cb	4.5	166.1	
1/4	4.5	166.1	
±	4.9	165.7	
1/4	5.4	165.2	
cb	5.8	164.8	Flowers
S	6.0	164.6	"
+10	6.2	164.4	"

0+10 = W. side Brick incinerator 3.4 ESW.  
4.4 N+S. N. Edge 21.2 S. of c.

0+21 - 21' S. of c Pepper Tree 48" Diam

170.57  
0+50. E Hilltop Dr

-10	6.7	163.9	
S.	6.3	163.3	
cb	6.0	164.6	
1/4	5.6	165.0	
±	4.8	165.8	
1/4	4.5	166.1	
cb	4.5	166.1	
+3	3.4	167.2	
N	2.0	167.6	
			1+00 E
N	3.5	167.1	
cb	4.5	166.1	
1/4	4.5	166.1	
±	4.9	165.7	
1/4	5.7	164.9	
cb	5.9	164.7	
+5. = fence	7.0	163.6	
S			
+10	7.5	163.1	
+42	26' S of c	Pepper	12" Diam
+45	26' S of c	"	" "
+48	26' S of c	"	" "

170.57

1444<sup>S</sup> 10' S of #4 Air Valve

1450.0

S-10	6.5	164.1
S	6.2	164.4
P5	5.2	165.4
cl	5.2	165.4
1/4	5.2	165.4
±	4.9	165.7
1/4	4.7	165.9
cl	4.7	165.9
N	3.5	167.1

1487 Pepper Tree.

2400

N	4.2	166.4
cl	5.3	165.3
1/4	5.3	165.3
±	5.1	165.5
1/4	5.3	165.3
cl	4.9	165.7
S	6.0	164.6
+10	6.1	164.5

170.57

T.P. Man 8.72

173.97

5.32

165.25

250

-10	10.7	163.3
S	11.0	163.0
cl	9.7	164.3
1/4	9.7	164.3
±	9.9	164.1
1/4	9.8	164.2
cl	9.8	164.2
N	8.6	165.4
+5	8.6	165.4

2470

-20	8.8	165.2
N	9.3	164.7
cl	10.0	164.0
1/4	10.0	164.0
±	10.2	163.8
1/4	10.6	163.4
cl	11.4	162.6
+5 = Fence		

4.11 Top.

77

Lot. Cor  
145.25



173.97

2+70 con

S 12.5 161.5

+40 13.3 160.7

2+85 Eucalyptus 3 Trunks. 36" Diam 25' S. of  $\phi$ 

3+10

S-10 10.3 163.7

S 10.4 163.2

 $\phi$  9.7 164.3

14 9.6 164.4

 $\phi$  9.3 164.7

14 9.7 164.7

 $\phi$  9.3 164.7

N 8.8 165.2

+10 8.4 165.2

3+50

-10 7.3 166.7

N 7.4 166.6

 $\phi$  8.1 165.9

14 8.2 165.8

 $\phi$  7.8 166.2

14 8.2 165.8

173.97

Hilltop  
78 $\phi$  8.4 165.6

+5 = Fence.

S 8.7 165.3

+10 8.7 165.3

3+61 Pepper 14" Diam 25' S. of  $\phi$ 3+85 Eucalyptus 24" Diam. on  $\phi$ 

4+00

-10 6.5 167.5

S 6.2 167.8

 $\phi$  5.7 168.3

14 5.8 168.2

 $\phi$  5.3 168.7

14 6.1 167.9

 $\phi$  6.1 167.9

N 5.3 168.7

+10 5.3 168.7

4+08 1.5 N. of  $\phi$  Eucalyptus 24" Diam

Continued F.B. 598 - P. 40.

00895  
140  
35800  
895  
1253  
157  
2.82V

315  
00895  
175  
4475  
6265  
995  
1.56625

00895  
7.820  
2520  
3000  
2835  
1650  
1575

152.82  
142.78  
86.98  
52.78  
142.76  
19.98  
127.0

354  
17  
397.78  
20  
317.78  
140  
177.78

offsets  
Allen  
51.25  
42.76  
8.49

223  
446  
0.01625  
1625  
20  
32500  
16  
2.6  
7.6  
100  
96  
40  
340

BM Mon 52N Trojona = 323.82  
C.T. A line Bl/comp & Dawson = 386.00  
Top M.H. Trojona & Dawson = 327.43

Table gives an idea of the value of the various factors and their contribution to the total value of the property. The value of the property is determined by the value of the land, the value of the buildings, and the value of the improvements. The value of the land is determined by the location, the size, and the quality of the land. The value of the buildings is determined by the age, the condition, and the quality of the buildings. The value of the improvements is determined by the nature and extent of the improvements. The total value of the property is the sum of the value of the land, the value of the buildings, and the value of the improvements.

CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.66	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if  $w = 16.2$  and  $h = 5.3$ , cu. yds. =  $1.48 + .028 + .089 = 1.597$  cu. yds. or practically 160 cu. yds. per 100 ft. If  $w$  exceeds 40 ft., use one half and multiply result by 2, if both  $w$  and  $h$  are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =  $h$ , and  $\frac{1}{2}$  the roadbed =  $w$ , add the triangles formed by taking the distance out to each break in turn ( =  $w$ 's) by the difference between the cuts (or fills) on each side of it ( =  $h$ 's) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.