F.B.
854

FIELD BOOK
360

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

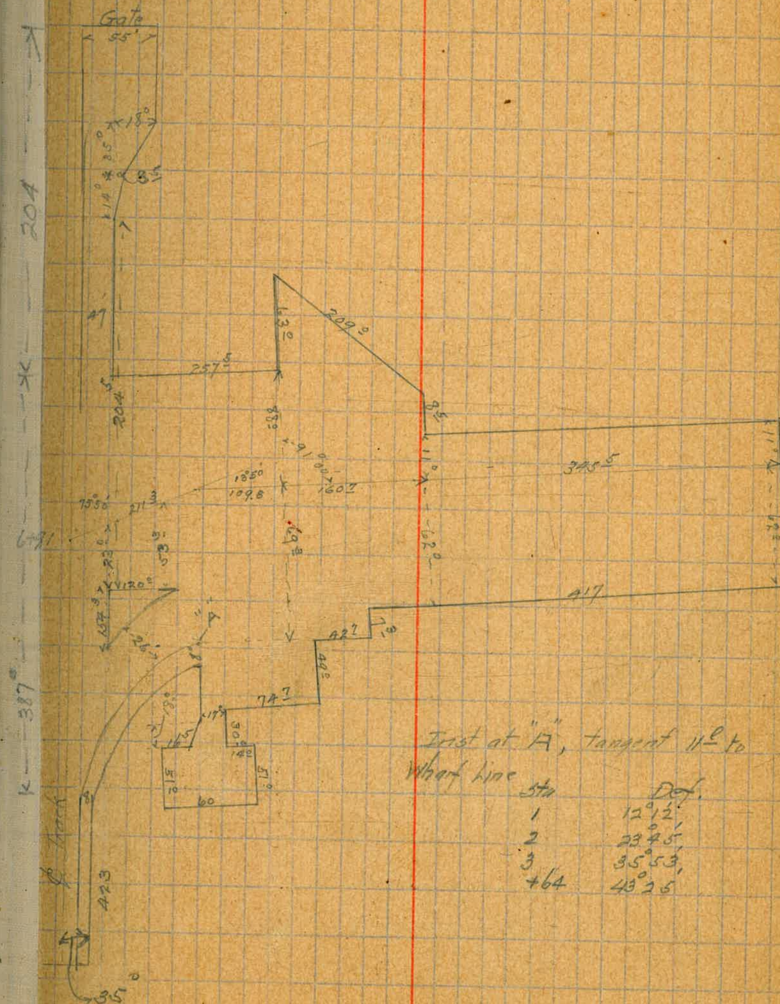
Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tabels see end of book.

I

11/12 Hotel. where wall

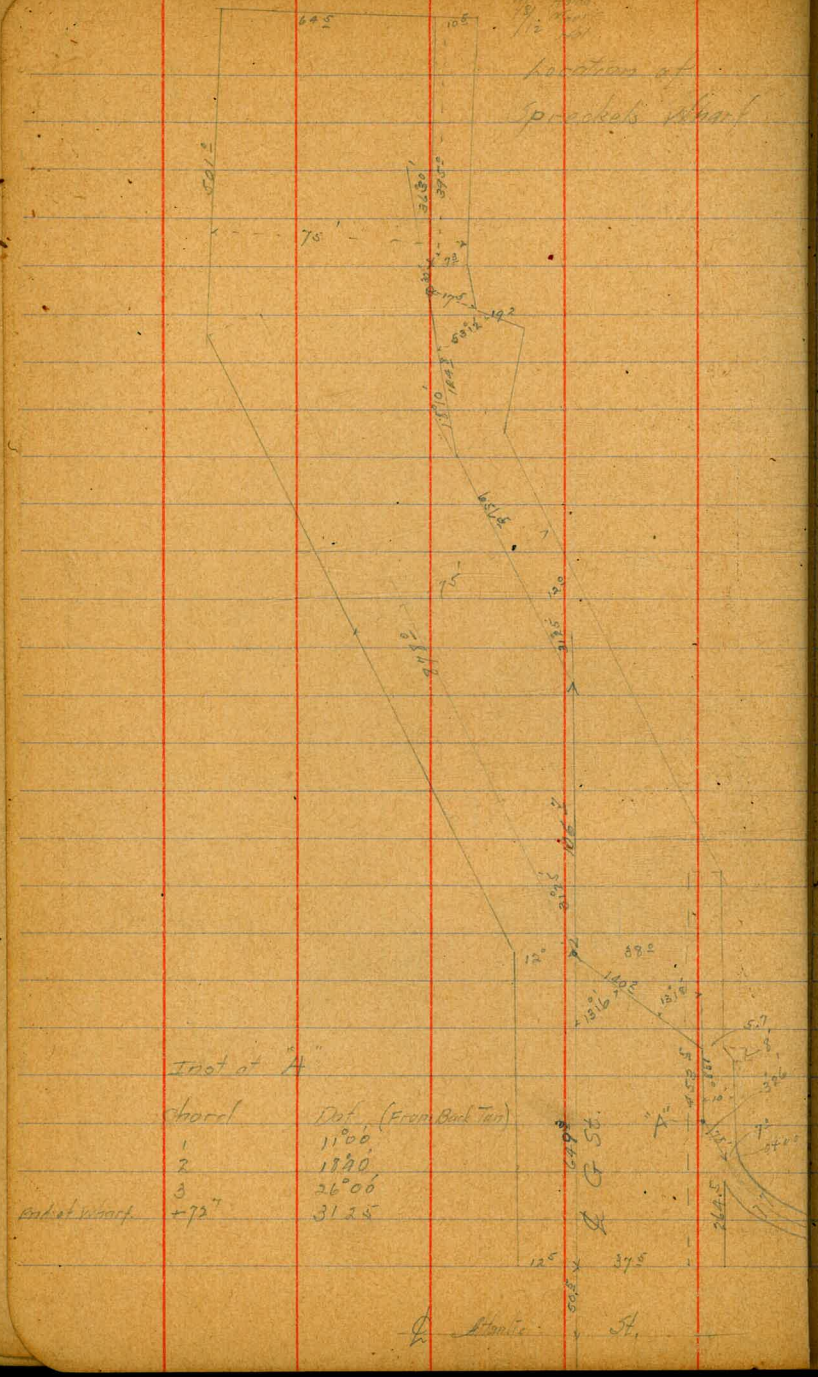
Location of Santa Fe Wharf



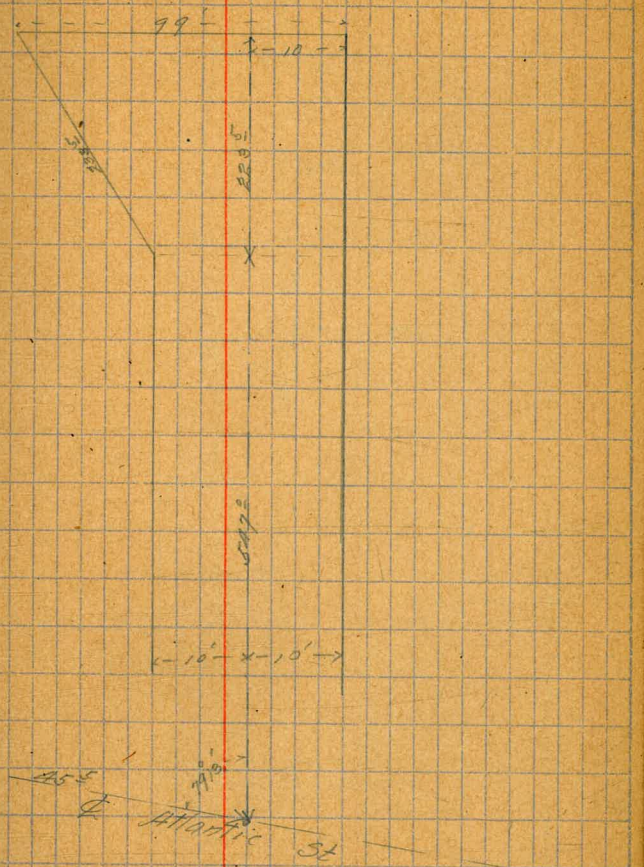
Inst at "A", tangent 11° to Wharf Line

Sta	Def.
1	12°12'
2	23°45'
3	35°53'
+64	43°25'

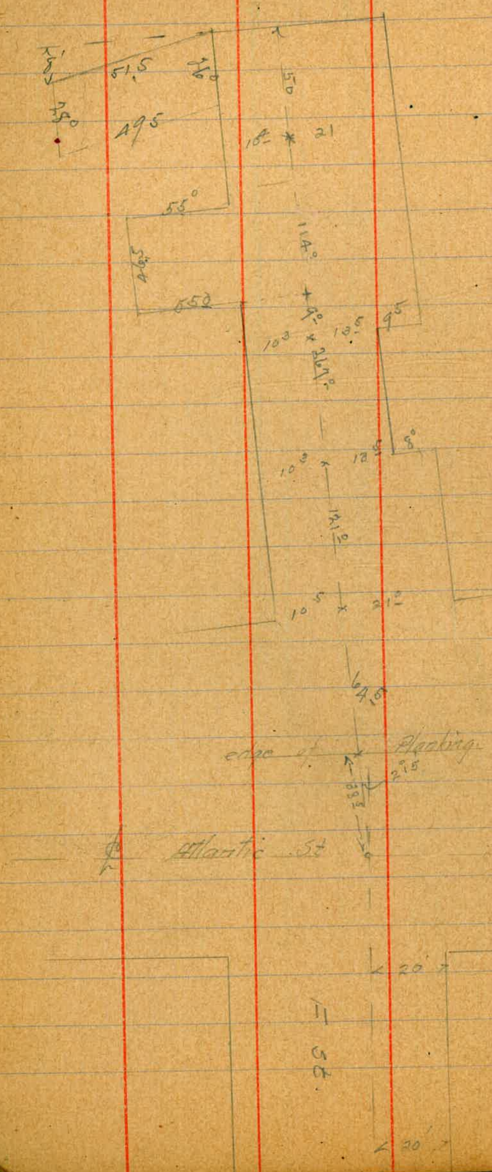
Location of Peckels Wharf



Location of Pt Loma Wharf

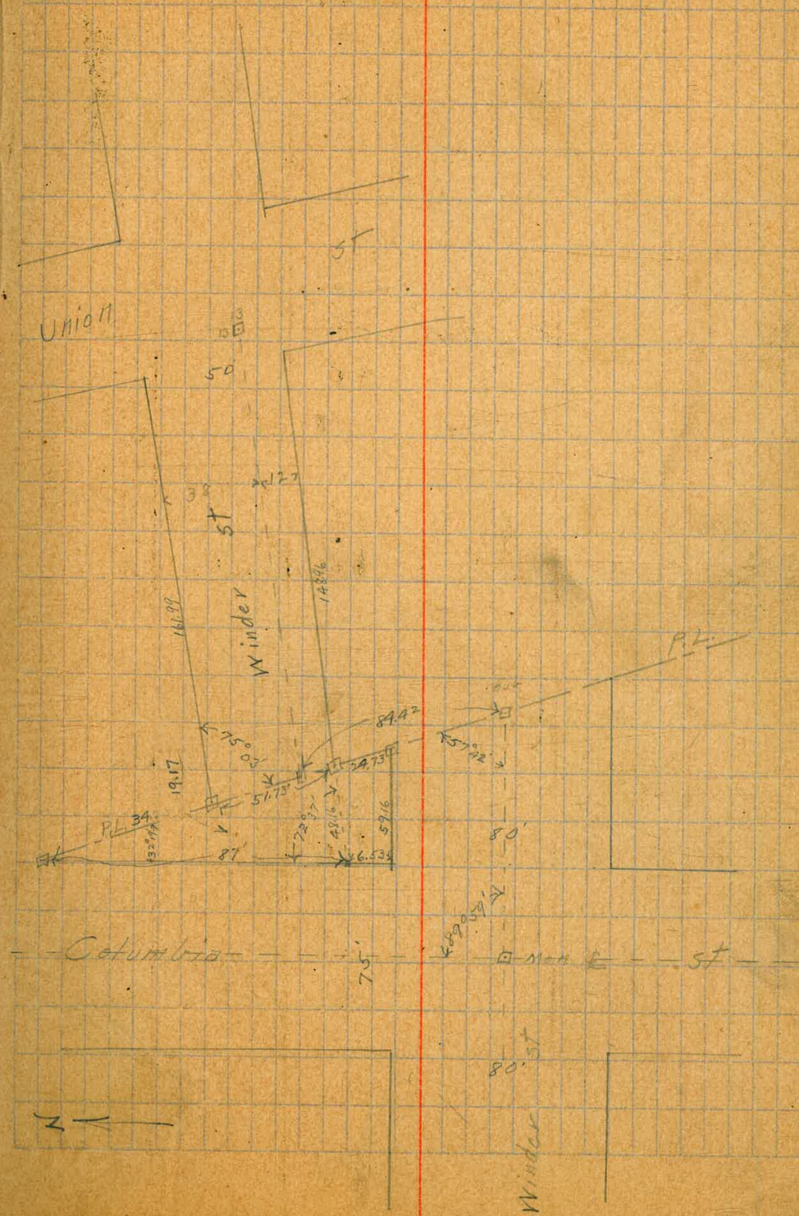


11/8/17 Hatch Moore Hall Location of Torres Wharf.



3/18/13 [illegible]
Evans
Kerr

survey for opening of Winder & Columbia st,



Cross-Section of Tenth St S.L. UNIVERSITY
South End. Various width St. 16' S/W.

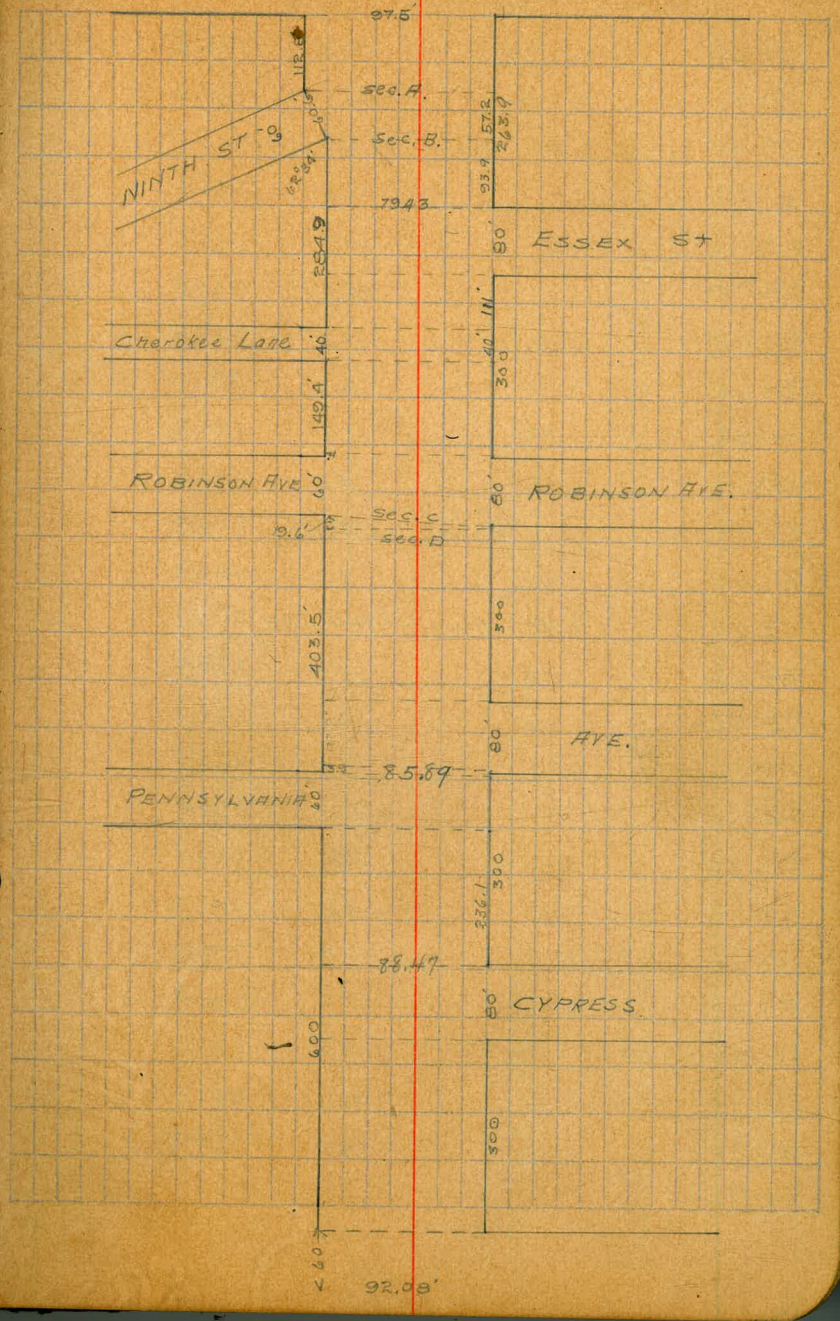
B.M.	2.06	284.15	282.09	S.W. cor 10th & Virginia B.P.

S.L. UNIVERSITY (97.5 WIDE)

W.		2.0	282.2
ob		2.2	282.0
1/4		1.9	282.3
C		1.6	282.6
1/4		1.4	282.8
ob		5.2	279.0
E		4.1	280.1
	25' So.	(97.65 WIDE)	
E		15.6	268.6
+6		14.9	269.3
ob		9.4	274.8
1/4		11.6	279.6
C		0.9	283.3
1/4		0.8	283.4
ob		5.1	279.1
W		3.5	280.7
	50' So.	(97.87 WIDE)	
W		4.5	279.7
ob		7.5	276.7
+11		8.1	276.1
1/4		5.7	278.5
C		2.2	282.0
1/4		2.8	281.4

Grade book 71

7



284.15

	284.15	
cl	11.3	272.9
E	21.1	263.1
75' So. (98.05 WIDE)		
E	23.2	261.0
+8	21.7	262.5
cl	16.4	267.8
C 1/4	6.2	278.0
C	4.0	280.2
1/4	12.2	272.0
+5	13.6	270.6
cl	11.2	273.0
W	5.0	279.2
100' So. (98.23 WIDE)		
W	16.5	267.7
cl	19.5	264.7
+10	21.3	262.9
1/4	20.3	263.9
C	10.5	273.7
+6	6.9	277.3
1/4	6.9	277.3
+3	7.4	276.8
cl	16.6	267.6
+11	22.3	261.9
E	24.9	259.3

284.15

112.8' So = Sec. A (95.32 WIDE)

E	17.9	266.3
+5	20.1	264.1
cl	14.6	269.6
+12	7.7	276.5
1/4	8.5	275.7
+5	8.9	275.3
C	15.0	269.2
1/4	23.3	260.9
cl	23.3	260.9
W	22.0	262.2
122.33 = No 1/4 (95.05' WIDE)		
W	24.0	260.2
cl	25.8	258.4
+12	26.4	257.6
1/4	25.3	258.9
C	16.5	267.7
1/4	9.8	274.4
+7	8.3	275.9
cl	13.9	270.3
+5	18.2	266.0
E	16.3	267.9
131.86 So = No 1/4 (91.99 WIDE)		
E	13.9	270.3
+12	16.0	268.2
cl	14.0	270.2

		284.15		
+6			10.4	273.8
1/4			12.6	271.6
T.P.	3.01	274.05	13.4	271.04
C			9.8	2643
1/4			19.3	254.8
ch			18.2	255.9
W			16.6	257.5
	141.39' So = Center (88.52' WIDE)			
W			19.4	254.7
ch			19.7	254.4
1/4			16.2	257.9
C			11.4	262.7
1/4			4.8	269.3
+8			2.7	271.4
ch			3.1	271.0
+6			5.2	268.9
E			3.3	270.8
	150.93' So. = So 1/4 (85.26' WIDE)			
E			2.9	271.2
ch			3.3	270.8
1/4			6.5	267.6
C			7.2	266.9
1/4			10.4	2637
ch			13.7	260.4
W			18.6	255.5

274.05

160.47' So = So. Curb. (82.00 WIDE)

W		11.7	262.4
ch		9.0	265.1
1/4		6.7	267.4
C		5.1	269.0
1/4		4.4	269.7
ch		3.3	270.8
E		0.9	273.2
	170' So = So. L of Sec 8. (78.74' WIDE)		
E		+0.4 (278.6)	274.5
ch		1.3	272.8
1/4		1.1	273.0
C		1.0	273.1
1/4		2.9	271.2
ch		5.3	268.8
W		7.7	266.4
B.M.	6.86	288.95	282.09
	25' So. (78.92' WIDE)		
W		14.1	274.9
ch		9.5	279.5
1/4		9.5	279.5
C		9.9	279.1
1/4		10.2	278.8
ch		11.8	277.2
E		11.2	277.8

28895

50' So. (79.10) WIDE

E	8.2	280.8
cb	7.8	281.2
1/4	7.4	281.6
C	7.4	281.6
1/4	7.7	281.3
cb	8.2	280.8
W	7.9	281.1

75' So. (79.29 WIDE)

W	6.8	282.2
cb	7.3	281.7
1/4	7.1	281.9
C	6.6	282.4
1/4	6.8	282.2
cb	7.0	282.0
E	6.8	282.2

93.9' So. = N.L ESSEX ST (SECTION = 79.13 W.)

E	6.6	282.4
cb	6.8	282.2
1/4	6.2	282.8
C	6.3	282.7
1/4	6.3	282.7
cb	6.6	282.4
W	6.5	282.5

NO. CURB

W	6.3	282.7

28895

cb	6.1	282.9
1/4	5.9	283.1
C	5.8	283.2
1/4	5.7	283.3
cb	6.4	282.6
E	7.4	281.6

NO. 1/4

E	7.0	282.0
cb	6.1	282.9
1/4	5.5	283.5
C	5.4	283.6
1/4	5.4	283.6
cb	5.6	283.4
W	5.7	283.3

CENTER

W	5.5	283.5
cb	5.4	283.6
1/4	5.4	283.6
C	5.2	283.8
1/4	5.3	283.7
cb	5.8	283.2
E	6.9	282.1

288.95

So. 1/4

E	6.9	282.1
cb	5.7	283.3
1/4	5.2	283.8
C	5.0	284.0
1/4	5.0	284.0
cb	5.3	283.7
W	5.3	283.7

So Curb

W	5.3	2837
cb	5.2	2838
1/4	5.0	284.0
C	4.9	284.1
1/4	4.9	284.1
cb	5.3	283.7
E	6.9	282.1

So. Line (80.01 wide)

E	5.6	283.4
cb	5.4	283.6
1/4	5.0	284.0
C	4.9	284.1
1/4	4.9	284.1
cb	5.1	283.9
W	5.3	283.7

288.95

25' So. C

W	5.2	283.8
cb	5.2	283.8
1/4	5.1	283.9
C	5.0	284.0
1/4	4.7	284.3
cb	5.3	283.7
E	4.9	284.1

50' So.

E	4.9	2841
cb	5.2	283.8
1/4	4.6	284.4
C	5.0	284.0
1/4	5.4	283.6
cb	5.2	2838
W	5.3	283.7

75' So

W	5.5	283.5
cb	5.5	283.5
1/4	5.5	283.5
C	5.1	283.9
1/4	4.9	284.1
cb	5.4	283.6
E	4.9	284.1

288.95

111' So = N.L. Cherokee Lane

E	5.1	283.9
cb	5.9	283.1
1/4	5.4	283.6
C	5.6	283.4
1/4	5.7	283.3
cb	5.8	283.2
W	5.3	283.7

No. CURB.

W	5.6	283.4
cb	5.6	283.4
1/4	5.6	283.4
C	5.4	283.6
1/4	5.4	283.6
cb	5.9	283.1
E	5.1	283.9

No 1/4

E	5.0	284.0
cb	5.9	283.1
1/4	5.4	283.6
C	5.5	283.5
1/4	5.6	283.4
cb	5.8	283.2
W	5.6	283.4

288.91

CENTER.

W	5.8	283.2
cb	5.9	283.1
1/4	5.6	283.4
C	5.7	283.3
1/4	5.4	283.6
cb	6.1	282.9
E	4.9	284.1

So. 1/4

E	4.9	284.1
cb	6.0	283.0
1/4	5.5	283.5
C	5.5	283.5
1/4	5.7	283.3
cb	6.0	283.0
W	5.9	283.1

So. CURB

W	6.2	282.8
cb	6.0	283.0
1/4	5.7	283.3
C	5.6	283.4
1/4	5.6	283.4
cb	6.1	282.9
E	4.9	284.1

288.95

50. LINE.

E	5.7	283.3
ch	5.9	283.1
1/4	5.6	283.4
C	5.4	283.6
1/4	5.7	283.3
ch	6.2	282.8
W	6.5	282.5

25' So.

W	6.5	282.5
ch	6.8	282.2
1/4	5.9	283.1
C	5.6	283.4
1/4	5.8	283.2
ch	6.1	282.9
E	5.3	283.7

50' So.

E	5.6	283.4
ch	6.4	282.6
1/4	5.9	283.1
C	6.0	283.0
1/4	6.3	282.7
ch	6.8	282.2
W	6.8	282.2

288.95

75' So.

W	7.2	281.8
ch	7.0	282.0
1/4	6.5	282.5
C	6.2	282.8
1/4	6.0	283.0
ch	6.3	282.7
E	5.8	283.2

100' So.

E	5.9	283.1
ch	6.1	282.9
1/4	6.1	282.9
C	6.5	282.5
1/4	6.9	282.1
ch	7.4	281.6
W	7.6	281.4

125' So.

W	7.8	281.2
ch	7.7	281.3
1/4	7.0	282.0
C	6.3	282.7
1/4	6.3	282.7
ch	6.6	282.4
E	5.9	283.1

288.95

149.0' ON WEST (EAST) } = N. L. ROBINSON
149.4 - EAST (WEST) }

E	6.2	282.8
cb	7.1	281.9
1/4	6.5	282.5
C	6.7	282.3
1/4	7.3	281.7
cb	8.4	280.6
W	8.5	280.5

NO. CURB.

W	8.3	280.7
cb	8.2	280.8
1/4	7.5	281.5
C	6.9	282.1
1/4	6.7	282.3
cb	7.2	281.8
E	6.6	282.4

NO. 1/4

E	6.7	282.3
cb	7.0	282.0
1/4	6.8	282.2
C	6.9	282.1
1/4	7.6	281.4
cb	8.3	280.7
W	8.8	280.2

288.95

CENTER

W	8.7	280.3
cb	8.3	280.7
1/4	7.7	281.3
C	7.0	282.0
1/4	6.7	282.3
cb	7.1	281.9
E	6.7	282.3

SO. 1/4

E	6.6	282.4
cb	7.3	281.7
1/4	7.1	281.9
C	7.2	281.8
1/4	7.9	281.1
cb	8.4	280.6
W	8.6	280.4

SO. CURB

W	8.9	280.1
cb	8.6	280.4
1/4	7.9	281.1
C	7.2	281.8
1/4	7.4	281.6
cb	7.4	281.6
E	7.0	282.0

288.95

SECTION C

E			6.7	282.3
cb			7.6	281.4
1/4			7.4	281.6
C			7.2	281.8
1/4			7.9	281.1
cb			8.7	280.3
W			8.7	280.3
T.P.	4.86	285.27 ✓	8.54	280.41

SECTION D (82.93 WIDE).

W		4.9	280.4
cb		5.0	280.3
1/4		4.3	281.0
C		3.8	281.5
1/4		3.8	281.5
cb		4.0	281.3
E		3.6	282.3

25' So.

E		3.0	282.3
cb		4.2	281.1
1/4		3.7	281.6
C		3.7	281.6
1/4		4.3	281.0
cb		4.8	280.5
W		4.7	280.6

285.27

50' So.

W		4.3	281.0
cb		4.6	280.7
1/4		4.1	281.2
C		3.3	282.0
1/4		3.6	281.7
cb		3.7	281.6
E		3.1	282.2

75' So.

E		3.1	282.2
cb		4.2	281.1
1/4		3.7	281.6
C		3.4	281.9
1/4		3.7	281.6
cb		4.3	281.0
W		3.9	281.4

100' So.

W		3.6	281.7
cb		4.3	281.0
1/4		3.9	281.4
C		3.2	282.1
1/4		3.4	281.9
cb		3.9	281.4
E		3.1	282.2

285.27

125' So. of Robinson

E	3.2	282.1
cb	4.7	280.6
1/4	3.6	281.7
c	3.2	282.1
1/4	3.9	281.4
ob	4.2	281.1
W	3.7	281.6

150' So.

W	3.7	281.6
cb	4.3	281.0
1/4	4.1	281.2
c	3.5	281.8
1/4	3.8	281.5
ob	4.3	281.0
E	3.6	281.7

175' So.

E	4.5	280.8
cb	5.0	280.3
1/4	4.5	280.8
c	4.0	281.3
1/4	4.2	281.1
ob	4.4	280.9
W	3.7	281.6

200' So.

W	4.1	281.2
cb	4.9	280.4
1/4	4.5	280.8
c	4.2	281.1
1/4	4.9	280.4
ob	5.5	279.8
E	5.0	280.3

225' So

E	5.9	279.4
cb	6.2	279.1
1/4	5.5	279.8
c	4.9	280.4
1/4	4.9	280.4
ob	5.1	280.2
W	4.6	280.7

250' So.

W	5.1	280.2
cb	5.7	279.6
1/4	5.7	279.6
c	6.1	279.2
1/4	6.7	278.6
ob	7.6	277.7
	9.4	275.9
E	11.4	273.9

285.27

275' 50. (85.08 WIDE)

-10	19.0	266.3
E	20.0	265.3
cb	15.5	269.8
1/4	10.5	274.8
+2	8.8	276.5
C	7.1	278.2
1/4	6.5	278.8
cb	6.2	279.1
W	5.6	279.7

297' 50.

W	6.9	278.4
cb	6.9	278.4
1/4	7.4	277.9
C	9.4	275.9
+5	10.2	275.1
1/4	14.4	270.9
cb	18.5	266.8
E	25.8	259.5
+15	27.4	257.9

300' 50. = N.L. PENNSYL. ON EAST

-15	28.4	256.9
E	26.7	258.6
cb	19.8	266.1
1/4	15.3	270.3
C	10.9	274.7
+10	8.2	277.1
1/4	8.7	276.6
cb	8.8	276.5
W	10.0	275.3

T.P. 0.26 272.58 13.01 272.26

NO. CURB

W	3.3	269.2
cb	2.5	270.0
1/4	2.2	270.3
C	4.1	268.4
1/4	6.8	265.7
cb	11.6	260.9
E	16.4	256.1
+20	21.3	251.2
+30	20.0	252.5

NO. 1/4

	25.2	247.3
-20	25.7	246.8
E	20.1	252.4
cb	16.4	256.1
1/4	13.1	259.4
C	10.3	262.2
1/4	8.6	263.9
cb	8.7	263.8
W	7.9	264.6

CENTER

W	13.4	259.1
cb	14.8	257.7
1/4	15.0	257.5
C	16.4	256.1

1/4		272.52		
cb			18.5	254.0
E			21.2	251.3
+30			24.4	248.1
T.P.	0.63	260.20	29.6	242.9
-30	So.	1/4	12.95	259.57
-20			22.0 22.5	238.7 238.2
E			19.1	241.1
cb			15.4	244.8
1/4			13.6	246.6
C			11.7	248.5
1/4			9.9	250.3
cb			8.5	251.7
W			7.8	252.4
			6.5	253.7
	So. CURB			
W			11.2	249.0
cb			12.4	247.8
1/4			13.2	247.0
C			14.9	245.3
1/4			15.8	244.4
cb			16.0	244.2
E			17.2	243.0
+15			18.8	241.4
+30			22.5	237.7
+35			20.6	239.6
T.P.	0.25	248.08	12.37	247.53

248.08

18

So. LINE ON EAST.

+30	8.7	239.4
-30	12.5	235.6
E	10.1	238.0
cb	8.9	239.2
1/4	8.0	240.1
C	7.2	240.9
1/4	6.2	241.9
cb	5.3	242.8
W	4.3	243.8
	3.9 So. = N.L. on WEST.	
W	5.9	242.2
cb	6.7	241.4
1/4	7.6	240.5
C	8.4	239.7
1/4	9.0	239.1
cb	10.3	237.8
E	11.7	236.4
+20	12.4	235.7
+30	7.8	240.3
	No CURB	
-30	6.9	241.2
-20	11.0	237.1
E	13.2	234.9
cb	13.7	234.4
1/4	12.7	235.4
C	12.9	235.2

		248.05		
1/4			10.4	237.7
cb			9.8	238.3
W			9.2	238.9
T.P.	0.22	248.05	0.25	247.83
	No. 1/4			
W			12.8	235.3
cb			14.3	233.8
1/4			15.4	232.7
C			16.4	231.7
1/4			15.3	232.8
cb			12.9	235.2
E			8.8	239.3
	CENTER			
E			5.4	242.7
cb			8.6	239.5
1/4			11.4	236.7
C			13.0	235.1
1/4			16.2	231.9
cb			18.1	230.0
W			19.2	228.9
+20			15.0	233.1
	So 1/4			
−35			18.0	230.1
−20			20.1	228.0
W			17.1	231.0

248.05

cb			15.0	233.1
1/4			12.5	235.6
C			9.8	238.3
1/4			7.8	240.3
cb			4.9	243.2
E			2.8	245.3
	So. CURB			
E		+0.3	248.4	
cb			2.2	245.9
1/4			5.0	243.1
C			7.0	241.1
1/4			9.4	238.7
cb			12.1	236.0
W			14.2	233.9
+18			16.2	231.9
+45			22.1	226.0
+55			18.0	230.1
T.P.	12.33	259.91	0.47	247.58
	So. LINE			
−65			29.8	230.1
−52			34.4	225.5
−33			26.2	233.7
W			22.9	237.0
cb			19.7	240.2
1/4			17.2	242.7
C			15.0	244.9

1/4		259.41	12.6	247.3
ab			9.2	250.7
E			7.2	252.7
T.P.	12.52	272.40	0.03	259.88
	25' SO.			
E			9.0	263.4
ab			12.1	260.3
1/4			14.0	258.4
C			16.8	255.6
1/4			20.5	251.9
ab			23.6	248.8
W			26.3	246.1
SAME SLOPE				
	50' SO.			
W			19.6	252.8
ab			15.7	256.7
1/4			11.9	260.5
C			9.3	263.1
1/4			6.3	266.1
ab			2.7	269.7
T.P.	11.63	283.80	0.23	272.17
E			9.0	274.8
	75' SO.			
E			5.5	278.3
ab			6.4	277.4
1/4			9.0	274.8

283.80

C		12.5	271.3
1/4		15.3	268.5
ab		17.8	266.0
W		21.4	262.4
	100' SO.		
W		14.2	269.6
ab		8.0	275.8
1/4		6.8	277.0
C		6.3	277.5
1/4		3.8	278.0
ab		4.9	278.9
E		5.2	278.6
	125' SO.		
E		4.1	279.7
ab		5.7	278.1
1/4		5.6	278.2
C		5.6	278.2
1/4		6.3	277.5
ab		7.2	276.6
W		8.5	275.3

R83.50

150' So.

W	8.0	275.8
cb	6.3	277.5
1/4	6.1	277.7
C	5.5	278.3
1/4	5.0	278.8
ab	4.7	279.1
E	3.4	280.4

175' So

E	4.0	279.8
cb	4.1	279.7
1/4	5.2	278.6
C	4.7	279.1
1/4	5.1	278.7
ab	6.6	277.2
W	7.7	276.1

200' So

W	7.0	276.8
cb	6.5	277.3
1/4	5.2	278.6
C	4.6	279.2
1/4	4.7	279.1
ab	4.4	279.4
E	4.0	279.8

283.80

R36.1 So = N.L Cypress

E	3.6	280.2
cb	4.2	279.6
1/4	4.5	279.3
C	4.4	279.4
1/4	5.2	278.6
ab	5.7	278.1
W	6.3	277.5

No. curb

W	5.6	278.2
cb	5.6	278.2
1/4	5.2	278.6
C	4.1	279.7
1/4	4.1	279.7
cb	4.2	279.6
E	3.6	280.2

No. 1/4

E	4.0	279.8
cb	4.3	279.5
1/4	4.0	279.8
C	4.2	279.6
1/4	4.5	279.3
ab	5.5	278.3
W	5.7	278.1

283.80

CENTER

W	5.9	277.9
cb	5.0	278.8
1/4	4.3	279.5
C	4.5	279.3
1/4	4.5	279.3
ct	4.5	279.3
E	4.4	279.4

SO. 1/4

E	4.4	279.4
cb	4.6	279.2
1/4	4.4	279.4
C	4.8	279.0
1/4	4.2	279.6
ct	4.9	278.9
W	5.8	278.0

SO. CURB

W	5.8	278.0
cb	5.4	278.4
1/4	5.1	278.7
C	5.0	278.8
1/4	5.0	278.8
ct	5.0	278.8
E	4.4	279.4

283.80

SO. LINE

E	5.4	278.4
cb	4.2	279.6
1/4	5.6	278.2
C	5.3	278.5
1/4	5.1	278.7
ct	4.9	278.9
W	5.8	278.0

25' SO.

W	5.2	278.6
cb	5.8	278.0
1/4	6.2	277.6
C	6.4	277.4
1/4	6.0	277.8
ct	5.8	278.0
E	5.4	278.4

50' SO.

E	5.5	278.3
cb	6.2	277.6
1/4	6.2	277.6
C	6.9	276.9
1/4	7.3	276.5
ct	7.0	276.8
W	6.5	277.3

		283.80		
		75' SO.		
W			11.0	272.8
ab			11.2	272.6
1/4			9.7	274.1
C			7.8	276.0
1/4			7.2	276.6
ab			6.6	277.2
E			6.1	277.7
		100' SO		
E			6.3	277.5
ab			6.6	277.2
+5			7.6	276.2
1/4			8.5	275.3
+10			9.7	274.1
C			12.9	270.9
1/4			23.5	260.3
+10			24.2	259.6
ab			22.8	261.0
W			15.7	268.1
+3			13.7	270.1
+13			13.5	270.3
		110' SO.		
-16			14.3	269.5
-6			14.4	269.4
W			18.7	265.1
ab			26.4	257.4

283.80

+10				25.5	258.0
1/4				24.6	259.2
C				13.7	270.1
1/4				12.0	271.8
ab				8.3	275.5
E				7.0	276.8
T.P.	0.21	271.14 ✓		12.87	270.93
		125' SO			
E				4.3	266.8
ab				2.6	268.5
1/4				4.2	266.9
C				6.7	264.4
+5				7.7	263.4
1/4				13.7	257.4
ab				17.6	253.5
W				9.3	261.8
+9				3.3	267.8
+20				2.8	268.3
		150'			
-20				5.3	265.8
-4				5.8	265.3
W				9.0	262.1
ab				20.7	250.4
+5				24.0	247.1
1/4				22.7	248.4

13		271.14		
C			18.2	252.9
1/4			14.0	257.1
ob			14.9	256.2
~~#~~ 10			16.2	254.9
E			14.4	256.7
+10			10.3	260.8
T.P.	4.38	262.50 ✓	13.02	258.12
		175' SO		
-10			1.1	261.4
E			6.5	256.0
ob			15.2	247.3
1/4			19.5	243.0
+7			19.6	242.9
C			20.8	241.7
+7			21.6	240.9
1/4			18.0	242.5
ob			6.6	255.9
+6			1.1	261.4
W			0.5	262.0
+9			0.6	262.0
		200' SO		
-10			+1.2	263.7
-4			4.5	258.0
W			4.7	257.8
+8			4.0	258.5

262.50

ob			8.5	254.0
1/4			16.9	245.6
C			25.0	237.5
1/4			21.8	240.7
ob			12.6	249.9
E			4.9	257.6
		325' SO		
E			8.3	254.2
ob			15.4	247.1
1/4			22.1	240.4
C			28.1	234.4
+8			28.1	234.4
1/4			23.4	239.1
ob			14.5	248.0
+8			8.1	254.4
W			8.8	253.7
+10			1.2	261.3
		250' SO		
-10			4.5	258.0
W			12.1	250.4
+10			12.3	250.2
TP	0.73	250.22 ✓	13.01	249.49
ob			4.2	246.0
1/4			12.3	237.9
C			19.3	230.9

		950.22		
1/4			14.8	235.4
ch			9.3	240.9
E			0.9	249.3
		975' So.		
E			10.9	239.3
ch			17.2	233.0
1/4			21.9	228.3
+5			23.5	226.7
C			22.0	228.2
1/4			13.5	236.4
ch			4.6	245.6
+12			5.0	245.2
W			0.0	250.2
		300' So = So END.		
W			00	250.2
+6			4.0	246.2
+10			9.0	241.2
ch			8.8	241.4
+8			9.0	241.2
1/4			13.3	236.9
C			21.0	229.2
1/4			26.3	223.9
ch			22.6	227.6
E			18.0	232.2

Cross section of B St from W. L 28th to west

B.M.	1.43	198.39	196.96	B.P. SE 28th & B
	W L 28TH ST			
-20 -12		14.2 7.8		
S		3.6		
+4		1.4		
cb		1.9		
1/4		1.0		
C		1.1		
1/4		1.0		
cb		0.8		
N		0.5		
	25' W			
N		0.5		
cb		0.8		
1/4		1.0		
C		1.1		
1/4		1.2		
cb		1.6		
+12		1.8		
S		3.6		
+10		12.1		
	50' W			
S		2.8		
cb		1.2		
1/4		1.1		
C		1.0		
1/4		0.9		
cb		0.7		
N		1.1		
	75' W			
+25		17.3		
-18		15.5		
N		5.0		
+4		1.0		
cb		0.6		
+8		1.8		
1/4		5.4		
C		6.5		
1/4		4.1		
+5		1.6		
cb		7.3		
+5		4.0		
S		4.0		
	90' W			
+25		22.7		
-15		21.2		
S		11.3		
+6		5.8		
cb		4.7		
1/4		3.5		
C		6.7		

198.39

+7		10.7
1/4		8.2
+7		1.1
cb		1.2
+4		1.4
N		9.4
+13		17.3
+25		21.3
	100' W.	
-35		24.0
-25		24.7
N		13.1
+10		5.9
cb		6.3
1/4		9.9
+7		12.4
C		10.9
1/4		5.1
cb		5.7
+8		7.6
S		11.2
+21		23.1
+35		24.5
	110' W	
-40		31.0
-25		24.2

S	16.1
cb	8.7
+8	3.1
1/4	5.0
C	10.4
+6	11.4
1/4	15.5
+5	11.3
cb	12.0
+8	13.2
N	16.8
+13	24.1
+35	26.2
	135' W
-25	26.4
-10	29.0
N	25.9
cb	22.9
1/4	23.4
C	16.6
1/4	6.5
+5	4.8
cb	9.5
S	19.3
+13	28.1

		1983			
+35			35.9		
+45			34.4		
		150' W			
-50			39.8		
-25			36.6		
S			21.1		
cb			11.9		
+8			7.2		
1/4			10.2		
T.P.	0.68	186.96	12.11	186.28	
C			6.0		
1/4			11.6		
T.P.	0.73	175.06	12.63	174.33	
cb			6.9		
N			6.3		
+20			3.0		
		175' W			
-20			8.3		
N			10.2		
cb			10.6		
1/4			8.7		
C			4.0		
1/4			+4.4	179.5	
cb			+3.0	178.1	
S			5.4		
+18			14.4		

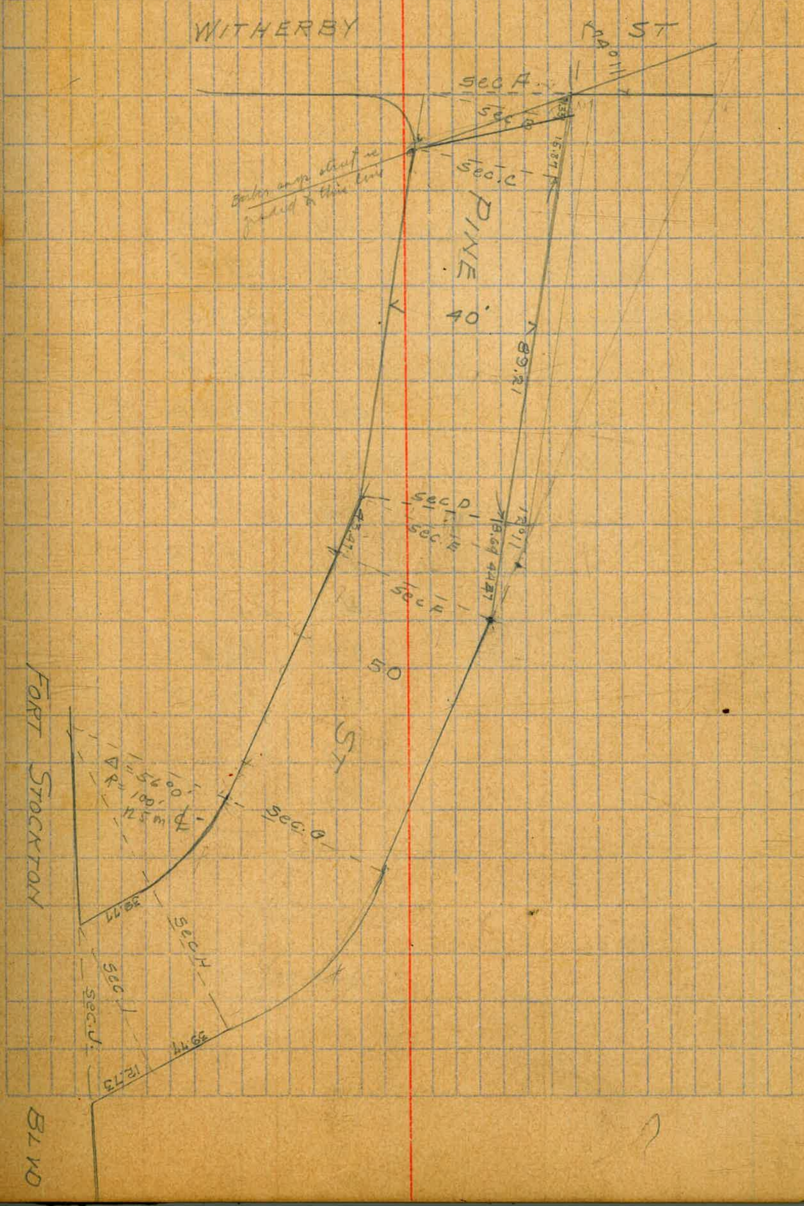
+55			16.4		
		300' W			
-30			8.9		
-15			11.8		
S			11.2		
cb			11.0		
1/4			9.6		
C			9.7		
1/4			8.9		
cb			10.0		
N			12.0		
+25			12.8		
+35			10.7		
+47			10.7		
		225' W			
-40			9.8		
-27			11.7		
-5			2.2		
N			2.9		
cb			3.0		
T.P.	8.95	182.90	1.11	173.95	
1/4			8.4		
C			8.5		
1/4			9.3		
cb			6.8		

		182.90		
S			6.8	
+13			7.0	
+20			11.0	
+30			7.2	
		250' W		
-25			2.4	
-15			1.1	
T.P.	12.64	194.58	0.76	182.14
S			4.3	
T.P.	10.92	201.43	4.07	190.51
+4			8.6	
cb			8.6	
1/4			10.1	
C			13.6	
1/4			9.5	
cb			9.3	
+4			9.5	
N			15.6	
+26			30.3	
+39			33.4	
		275' W		
-40			2.6	
-25			23.4	
N			7.3	
+4			4.1	
cb			3.8	

1/4			4.0
C			4.4
1/4			4.4
cb			4.7
S			5.0
		300' W	
S			4.5
cb			4.7
1/4			4.5
C			4.3
1/4			4.3
cb			3.9
N			4.1

3/3/13. Gregory, Belford, Bunker — Cross Section of Pine St (40' & 50' wide) from E.L. Witherby.

B.M.	2.80	270.23 ✓		267.43	NE Stockton & Sierra Vista
T.P.	0.73	262.08 ✓	8.88	261.35 ✓	
		E. LINE WITHERBY (SEC A.)			
S			7.8	254.3	
+6			9.4	252.7	
cb			9.1	253.0	
1/4			9.0	253.1	
C			8.8	253.3	
1/4			9.1	253.0	
cb			9.3	252.8	
+3			9.4	252.7	
N			11.2	250.9	
		(Sec B.)			
-48			34.0	228.1	
-39			32.2	229.9	
-19			22.5	239.6	
N			14.9	247.2	
+8			14.3	247.8	
cb			9.9	252.2	
1/4			8.8	253.3	
C			8.6	253.5	
1/4			8.9	253.2	
cb			9.1	253.0	
S			7.8	254.3	



Sec. C

S	8.1	254.0
cl-	8.5	253.6
1/4	8.1	254.0
C	8.7	253.4
1/4	14.8	247.3
cl-	15.3	246.8
+3	16.0	246.1
N	21.3	240.8
+15	30.9	231.2
+41	40.8	221.3
+60	42.1	220.0

25' EAST OF C.

-75	54.1	208.0
-64	55.7	206.4
-37	41.9	220.2
-25	38.7	223.4
N	23.6	238.5
cl-	16.6	245.5
1/4	13.3	248.8
C	10.8	251.3
1/4	9.6	252.5
cl-	7.4	254.7
S	7.5	254.6

50' EAST

S	6.7	255.4
cl-	6.5	255.6
1/4	6.9	255.2
C	7.7	254.4
1/4	10.9	251.2
cl-	12.7	249.4
N	17.8	244.3
+10	23.1	240.0
+38	33.7	228.4
+45	39.5	222.6
+70	50.6	211.5

75' EAST

-70	40.7	221.4
+48	33.7	228.4
N	8.7	253.4
+5	6.2	255.9
cl-	6.1	256.0
1/4	5.6	256.5
C	5.3	256.8
1/4	5.2	256.9
cl-	5.9	256.2
S	6.7	255.4

262.08

89.21' East = Sec D.

S	6.2	255.9
eb	5.6	256.5
1/4	6.1	256.0
C	5.6	256.5
1/4	5.8	256.3
eb	6.3	255.8
+5	5.8	256.3
N	6.3	255.8
+17	10.7	251.4

Sec. E

-15	7.5	254.6
N	6.6	255.5
eb	6.2	255.9
1/4	6.1	256.0
C	5.9	256.2
1/4	6.1	256.0
eb	6.1	256.0
S	6.2	255.9

21.73' EAST OF Sec E

S	5.9	256.2
eb	5.7	256.4
1/4	5.7	256.4
C	5.6	256.5
1/4	5.3	256.8
eb	6.1	256.0
N	5.9	256.2

262.08

43.47' EAST = Sec. F (ST = 50' WIDE)

N	5.0	257.1
eb	5.8	256.3
1/4	5.6	256.6
C	5.0	257.1
1/4	5.2	256.9
eb	5.6	256.5
S	4.6	257.5

25' EAST OF Sec F

S	4.0	258.1
eb	4.4	257.7
1/4	4.0	258.1
C	3.6	258.5
1/4	4.0	258.1
eb	4.0	258.1
N	3.8	258.3

50' EAST

N	3.4	258.7
eb	2.9	259.2
1/4	3.0	259.1
C	3.4	258.7
1/4	2.7	259.4
eb	3.0	259.1
S	2.5	259.6

262.05

75' EAST

S			0.5	261.6
cb			1.3	260.8
1/4			1.7	260.4
C			1.5	260.6
1/4			1.7	260.4
cb			2.5	259.6
N			2.8	259.3
T.P.	6.04	267.39	0.78	261.35

100' EAST

N			6.6	260.8
cb			6.6	260.8
1/4			6.1	261.3
C			5.8	261.6
1/4			6.2	261.2
cb			6.3	261.1
S			5.9	261.5

125' EAST

S			5.2	262.2
cb			5.6	261.8
1/4			5.3	262.1
C			5.0	262.4
1/4			5.5	261.9
cb			6.4	261.0
N			6.7	260.7

267.39

150' EAST

N			6.6	260.8
cb			6.1	261.3
1/4			5.1	262.3
C			4.3	263.1
1/4			4.7	262.7
cb			4.9	262.5
S			4.2	263.2

By Computation 176.9 E = Sec. G.

S			3.3	264.1
cb			4.1	263.3
1/4			4.2	263.2
C			4.1	263.3
1/4			5.0	262.4
cb			5.5	261.9
N			6.1	261.3

25' EAST OF G = { 30' EAST ON No. L. / 20' " " So. L

N			5.4	262.0
cb			4.7	262.7
1/4			4.5	262.9
C			3.9	263.5
1/4			3.8	263.6
cb			3.7	263.7
S			2.6	264.8

267.39

50' E OF G = { 60' ON No. / 40' ~ So.

S	2.2	265.2
ch	3.6	263.8
1/4	3.6	263.8
C	3.8	263.6
1/4	4.5	262.9
ch	4.6	262.8
N	5.0	262.4

75' EAST = { 90' ON No. / 60' ~ So.

N	4.2	263.2
ch	4.2	263.2
1/4	4.0	263.4
C	3.6	263.8
1/4	3.6	263.8
ch	3.5	263.9
S	2.3	265.1

100' EAST = { 120' ON No. / 80' ~ So.

S	2.41	265.0
ch	3.6	263.8
1/4	3.6	263.8
C	3.4	264.0
1/4	4.1	263.3
ch	4.2	263.2
N	4.4	263.0

267.39

34

122.18' EAST = { 146.6' ON No. / 97.74' ~ So. } = Sec H.

N	4.6	262.8
ch	4.8	262.6
1/4	4.3	263.1
C	3.9	263.5
1/4	3.9	263.5
ch	3.9	263.5
S	2.8	264.6

39.47' EAST = Sec. I

S	3.9	263.5
ch	4.3	263.1
1/4	4.2	263.2
C	4.3	263.1
1/4	4.7	262.7
ch	5.4	262.0
N	4.4	263.0

Sec. J = N.L. FORT STOCKTON

N	5.1	262.3
ch	5.1	262.3
1/4	4.9	262.5
C	4.5	262.9
1/4	4.3	263.1
ch	4.3	263.1
S	3.8	263.6

10/13/24

50' wide
10' s/w
7.5' 1/4s

Cross Section of Sunset Blvd. Witherby to Hortensia

Moore
Earle
Stock
Kelley

NE of Sunset & Witherby

	3.11	264.13	261.02

W.L. Witherby

SL	0.2
cb	0.9
+3	0.8
1/4	1.5
c	2.1
1/4	2.7
cb	3.2
NL	2.8
	25' W
NL	2.5
cb	3.1
1/4	2.8
c	2.4
1/4	1.8
cb	1.6
SL	1.3
	50' W
SL	3.1
cb	3.7
1/4	4.2
c	4.5
1/4	5.4
cb	5.5
	264.13
NL	5.6
	66' W
NL	6.5
cb	6.7
1/4	6.0
c	5.8
1/4	5.5
cb	5.3
SL	3.7
	68' W
SL	4.1
cb	5.4
1/4	5.6
c	5.9
+2	7.7
1/4	7.7
+2	6.6
cb	6.9
NL	6.7
	75' W
NL	7.0
cb	7.3
+3	7.2
+5	8.3
1/4	8.4
c	7.9

		264.13		
+3			6.1	
1/4			6.1	
cb			6.0	
SL			4.9	
T.P.	3.47	259.53	8.07	256.06
		90' W		
SL			2.2	
cb			2.4	
1/4			2.3	
+2			2.4	
+4			3.6	
C			4.3	
1/4			3.8	
cb			3.9	
N			4.0	
		100' W		
N			5.3	
cb			5.2	
1/4			4.6	
C			4.2	
1/4			3.4	
cb			3.1	
S			3.1	
		125' W		
S			4.7	
cb			5.1	

25453 Sunset Blvd 36

1/4	5.5
C	6.1
1/4	4.6
cb	6.2
N	7.0
+10	7.2
	150' W
-10	9.5
N	8.9
cb	8.7
1/4	8.5
C	8.2
1/4	7.9
cb	7.4
S	6.8
	175' W
S	8.9
cb	9.4
1/4	10.0
C	10.5
1/4	10.8
cb	11.1
N	11.2
+10	11.3
	200' W
+10	12.4

		25953			
N			11.8		
cb			12.1		
1/4			12.1		
C			12.2		
1/4			11.8		
cb			11.5		
S			10.9		
			225' W		
S			12.9		
cb			13.2		
1/4			13.3		
T.P.	1.08	24.68	12.93	24.6.60	
C			1.6		
1/4			1.9		
cb			2.0		
N			2.3		
			250' W		
N			3.1		
cb			2.8		
1/4			3.1		
C			2.8		
1/4			2.6		
cb			2.2		
S			1.9		
			265' W		
S			3.1		

24.7.68 Sunset Blvd

cb	3.1
1/4	3.5
C	3.5
1/4	4.1
cb	4.4
N	4.0
	275' W
+10	6.5
N	6.1
cb	5.1
1/4	4.6
C	3.9
1/4	3.6
cb	3.7
S	3.8
	291' W
S	5.4
cb	5.7
1/4	5.6
C	6.5
1/4	7.6
cb	8.9
N	9.7
+10	12.8
	300' W = W L of Hortensia
-15	18.3

50' wide
10' slur
7.5' 1/4 S

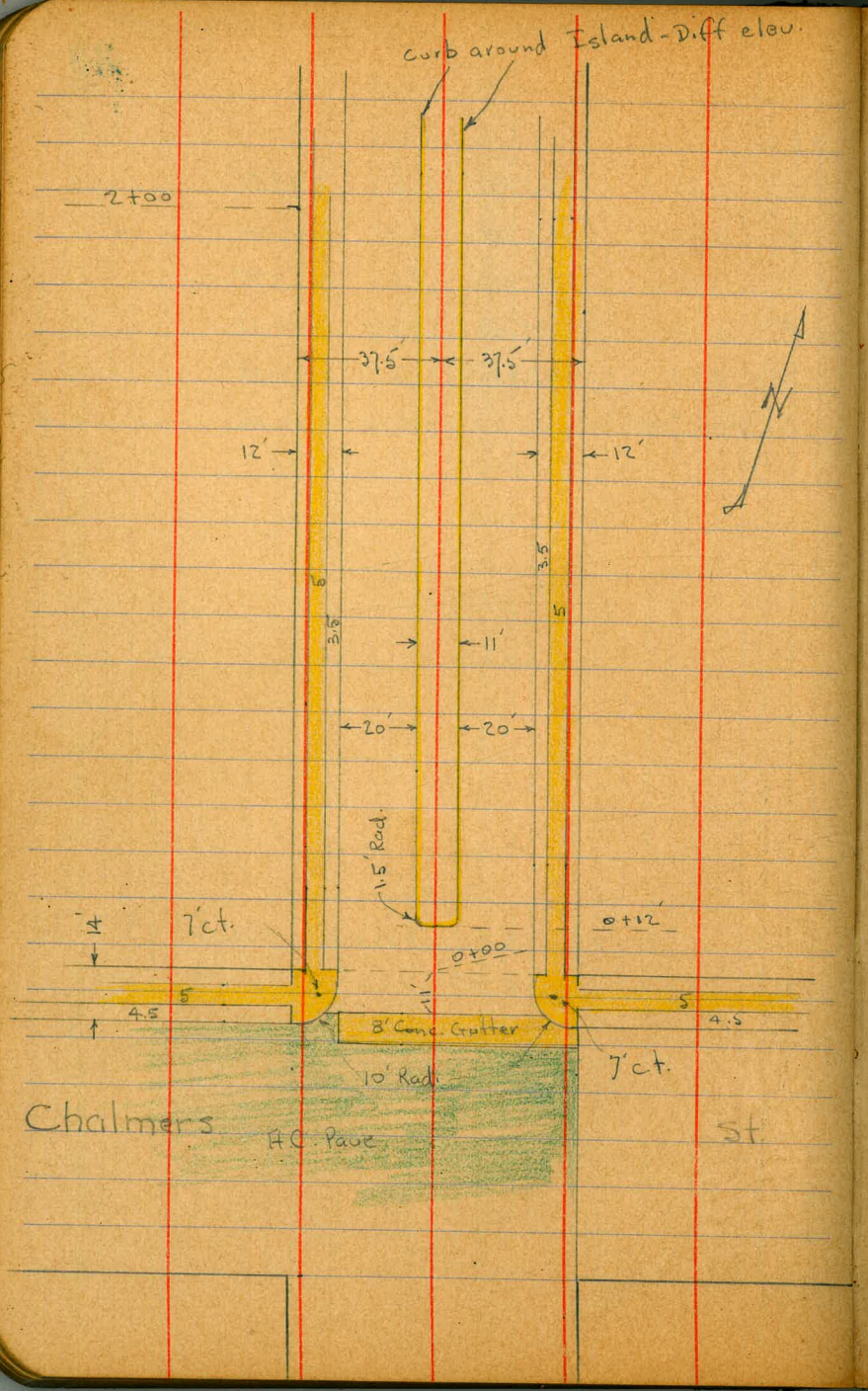
		247.68		
N			14.4	
cb			11.6	
1/4			10.6	
C			9.3	
1/4			8.9	
cb			7.5	
S			6.2	
		E cb		
S			9.2	
cb			11.5	
1/4			12.6	
C			13.3	
T.P.	0.47	235.33	12.82	234.86
1/4			1.4	
cb			2.7	
N			3.3	
+15			8.8	
		E 1/4		
-15			13.4	
N			8.2	
cb			5.5	
1/4			4.2	
C			4.3	
1/4			3.9	
cb			2.5	
S			1.5	

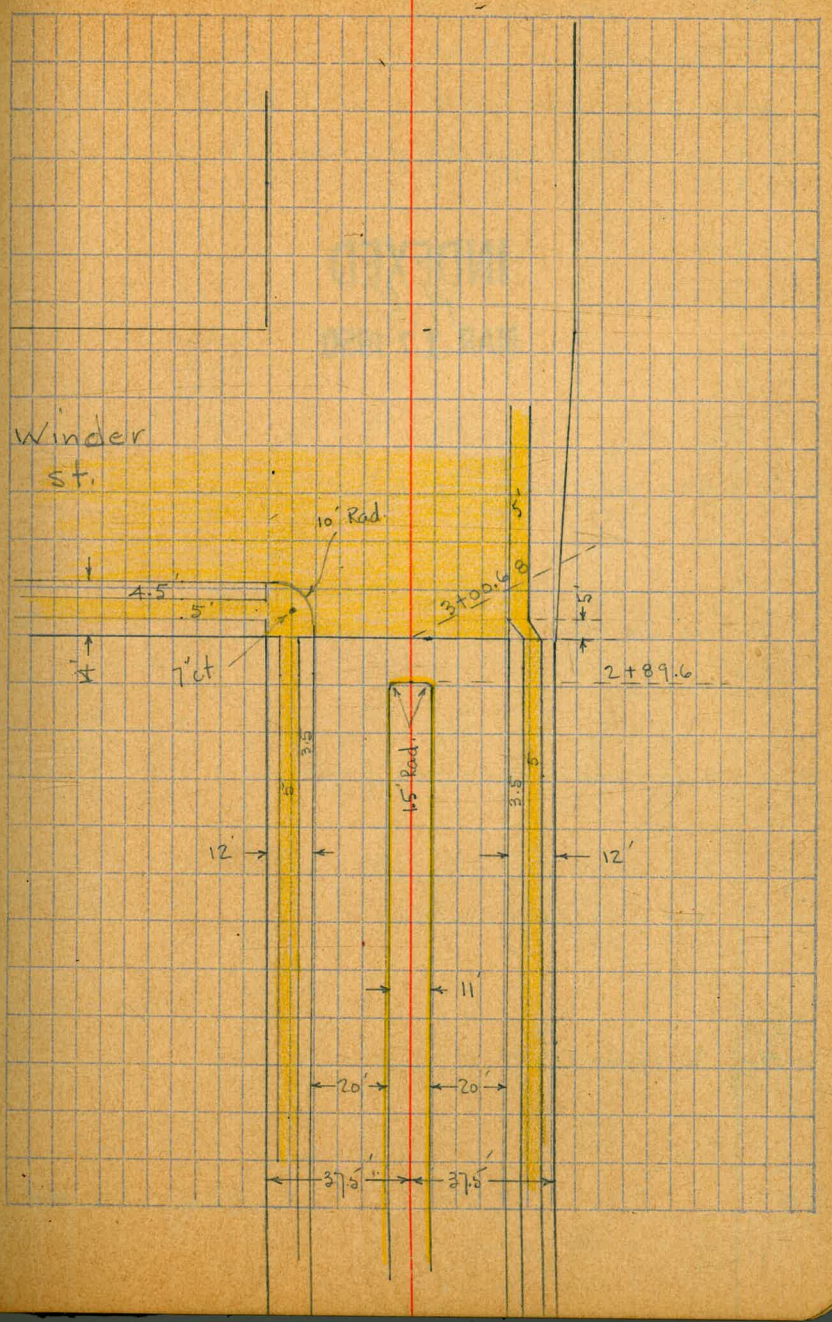
+5			0.4	
		Center		
-10			2.4	
S			5.3	
cb			6.4	
1/4			7.5	
C			8.0	
1/4			8.3	
cb			9.0	
N			10.7	
+15			18.0	
		W 1/4		
-15			21.5	
N			14.8	
cb			13.1	
1/4			13.0	
C			13.2	
1/4			12.3	
cb			11.8	
S			10.7	
+10			8.0	
		W cb		
-15			6.9	
-6			12.4	
T.P.	0.12	222.72	12.73	222.60
S			2.4	

		222.72			
cb			4.2		
1/4			4.8		
C			5.0		
1/4			4.7		
cb			4.4		
N			6.8		
+15			11.8		
			WL of Hortensia		
-20			18.4		
N			12.2		
cb			12.0		
1/4			11.2		
C			11.0		
1/4			10.1		
cb			9.0		
S			6.0		
+10			2.2		
			25' W		
T.P.	0.08	210.16	12.64	210.08	
-15			0.3		
S			15.4		
cb			8.9		
1/4			11.3		
C			13.0		
1/4			13.8		
cb			15.1		

210.16 Sunset

N			1.48		
+20			17.6		
TP	11.91	220.85	1.22	208.94	
TP	12.42	233.10	0.17	220.68	
TP	12.60	245.07	0.63	232.47	
TP	12.78	257.28	0.57	244.50	
TP	9.78	265.86	1.20	256.08	
	Check BM		4.80	261.06	261.02 BM.


Curb around Island - Diff elev.
2+00
37.5'
37.5'
12'
12'
11'
20'
20'
1.5' Rad.
0+12
0+00
7' ct.
7' ct.
8' Conc. Gutter
10' Rad.
Chalmers
AC Pave
St.


Winder
St.
10' Rad.
4.5'
5'
3+00.6
2+89.6
7' ct.
15' Rad.
12'
12'
11'
20'
20'
37.5'
37.5'

X-Sect. Colombia St. - 75' St. - 12' curbs + 11' Parkway in ℄ - curbs on E. side are higher than the West. Will take Levels on each side separately - Use H.I. shown on each side

4203

W.O. 31593

INDEXED
M.K.
MAR 17 1950

2-24-50

Osborne
Hardin
Hatch
Shepard

0-11 = Nly. of Conc. gut.

0-14 = N. cb

0-15 = ℄ of Conc. gut = Low point

0-19 = Sly. of 8' Conc. gutter.

0-40 = ℄ Chalmers = W.C. Pave

BM.	2.81	99.92	97.11 S.E. B.P.

Lt. = W. ℄ = Consider as N. + S. R = E.

Soil Sample - W. ½ - 100' S. of S.L. Winder

		93.97	93.47	93.58	94.27	95.01	95.67	96.51	97.26			
		5.95	6.45	6.34	5.65	4.91	4.25	3.41	2.86			
		28.4	28.4	25.5	13		13	28.4	28.4			
		Top	gut.	end Conc. + AC				gut.	Top			
89.84	89.01	94.11	93.96	93.40	93.04	94.78	95.46	96.13	96.96	97.04	98.62	99.47
10.08	10.91	5.81	6.76	6.52	5.84	5.14	4.46	3.79	3.66	2.88	1.3	0.45
70	70	37.5	37.5	25.5	13		13	25.5	37.5	37.5	8.5	8.5
Top	gut.	Top	gut.						gut.	Top	gut.	Top
	89.07	83.12	83.36	83.97		84.68	85.57	96.09	96.30			
	10.85	6.80	6.56	5.95		5.24	4.53	3.83	3.62			
	70	37.5	25.5	13			13	25.5	37.5			
			end Conc. Beg A.C.						end Conc.			
	89.84	93.14	93.62	92.26		94.91	95.67	96.41	96.56		98.82	
	10.04	6.76	6.30	5.66		5.01	4.25	3.55	3.36		1.1	
	65	37.5	25.5	13			13	25.5	37.5		8.5	
			end Conc. + Beg A.C.						end Conc.			
89.47		92.11	93.24	94.06		95.42	96.51	96.80			99.90	
10.25		7.81	4.70	5.86		4.50	3.41	3.12			0.2	
70		50	37.5	25.5			25.5	37.5			8.5	
		99.92							edge Pave	99.92		

Chalmers & Colombia

Note: H.I. may be diff. for each side of ℄

1+10 = Sly. of Conc Dr. on Rt.

T.P. 8.41 107.08 1.25' 98.67

1+00

0+75

× 0+67 = ℄ 11' Conc. Dr. on Rt.

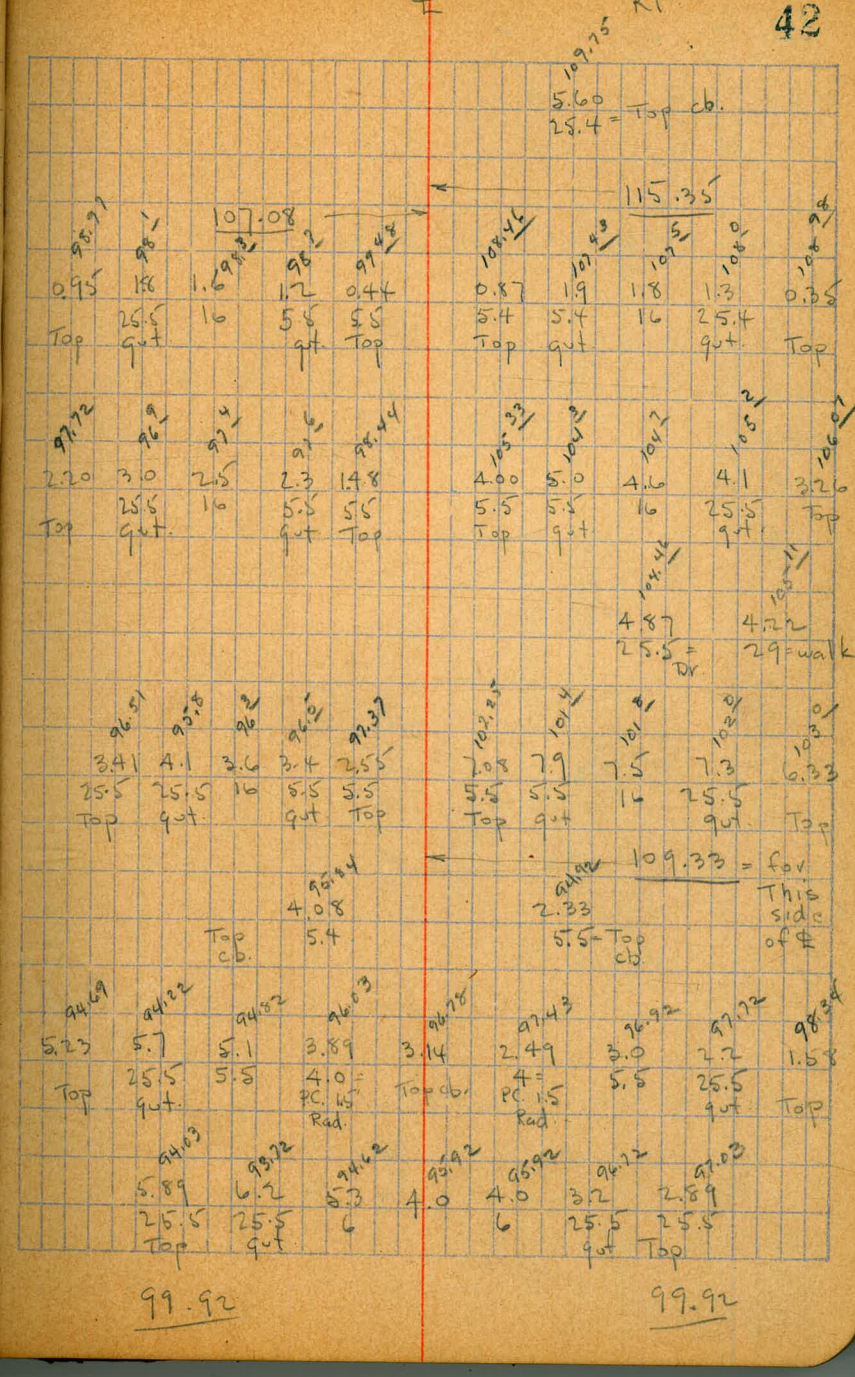
Note: dirt in ℄ is average between cbs.

0+50

0+13.5 = P.C. of 1.5' Rad. on Island cb.

0+12 = Most Sly. of cb. around 11' Island.

0+00 = N.L. Chalmers



2+25

2+18 = Sly. of Conc. Dr. on Rt.

2+00

1+75

1+50

1+52 = Nly. of Dr.

1+44 = ℄ of 15' Conc. Dr. on Lt.

1+25

Lt. | ℄ | Rt.

2+25 Rt.:
109.07 6.26 5.3 Top
108.2 6.7 gut.
108.9 6.5 16
109.07 6.28 25.3 gut = Dr.
109.77 5.58 walk
110.11 5.24 25.4 = Top cb.

2+00 Lt.:
100.04 7.04 Top
99.7 7.4 25.5 gut.
100.01 7.1 16
100.31 6.8 5.5 gut.
100.79 6.29 5.5 Top

2+00 Rt.:
110.27 5.08 5.3 Top
109.8 5.6 gut.
110.4 5.3 16
110.3 5.1 25.4 gut.
110.76 4.59 Top

1+75 Rt.:
110.58 4.77 5.3 Top
110.25 5.1 gut.
110.6 4.8 16
110.81 4.6 25.5 gut
111.13 4.23 Top

1+50 Lt.:
99.54 7.54 Top. (Grade)
99.13 7.95 25.5 in Dr.
99.51 7.6 16
99.61 7.3 5.5 gut
100.21 6.94 5.5 Top

1+50 Rt.:
110.55 4.80 5.4 Top
110.1 5.3 gut.
110.5 4.9 16
110.56 4.79 25.4 gut. = in Dr.
111.25 4.10 28.9 walk
111.09 4.26 25.4 = Top cb.

1+44 Lt.:
7.45 29 walk
7.96 25.4 Dr.

1+25 Lt.:
99.23 7.85 Top
98.9 8.2 25.5 gut
99.0 8.1 16
99.3 7.8 5.5 gut
99.79 7.29 5.5 Top

107.08

1+25 Rt.:
110.32 5.13 5.4 Top
109.4 6.0 gut.
109.6 5.7 16
110.03 5.32 25.5 = gut. in Dr.
29 walk

115.35

T.P. on S.W. 7' ct. 5.82 101.26 - checked by upper levels.

3+14.68 = S. cb. to W.

℄ of S.W. Ret

3+00.68 = S.L. Winder St = edge of Conc. pave

2+89.6 = Nly. of cb. around Island.

2+88.1 = P.C. of 15' Rad. on Island curb

2+75

2+50

2+47 = Nly. of Di

Lt. ℄ Rt.

97 60	96 79	101 01	100 22	100 77	101 76	102 54	102 91	103 08	103 71
9.48	10.29	6.07	6.81	6.31	5.32	4.57	4.17	4.00	3.37
70	70	37.5	37.5	25.5	13		13	25.3	
Top	gut	Top	gut					gut.	Top

6.60	5.93
gut.	Top

101 13	100 47	101 74	102 53	102 97	103 17	103 87
5.95	6.47	5.34	4.55	4.11	3.89	3.21
	25.6	13		13	25.3	
Top	gut.				gut.	Top

101 09	100 81	101 31	101 81	103 15	103 1	103 2	103 9	104 64
6.05	6.3	5.8	5.3	3.93	4.0	3.4	3.2	2.44
	25.6	16	5.7		5.5	16	25.3	
Top.	gut						gut.	Top

102 04	103 89
5.00	3.19
5.7	5.5
Top	Top

105.01	104 2	104 5	105 1	105 28
2.07	2.9	2.6	2.0	1.30
5.5	5.5	16	25.4	
Top	gut.		gut.	Top

107.08

100 63	100 24	100 44	100 8	101 46	107 30	106 45	106 75	106 9	107 75
6.54	6.8	6.6	6.3	5.62	8.05	8.9	8.6	8.4	7.60
	25.5	16	5.6	5.6	5.5		16	25.4	
Top	gut		gut.	Top	Top	gut.		gut.	Top

107 95
7.40
25.4
Top cb.

107.08 ← 115.35

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P.=23° 20′ to the R. at Station 542+72.

Ext. in Tab. IV opposite 23° 20′=120.87
120.87÷12=10.07. Say a 10° Curve.

Tan. in Tab. IV opp. 23° 20′=1183.1
1183.1÷10=118.31.

Tab. V correction for A. 23° 20′ for a 10° Cur.=0.16
118.31+0.16=118.47=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. 23° 20′=23.33°÷10=2.3333=L. C.

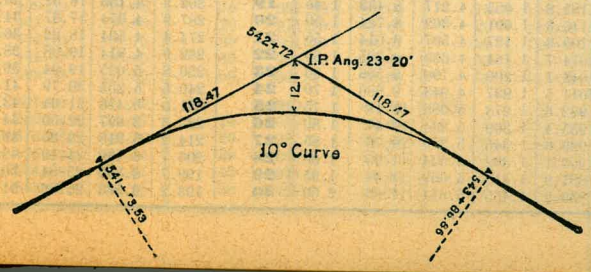
2° 19½′=def. for sta.	542	I. P.=sta.	542+72
4° 49½′= " " "	+50	Tan.=	1.18.47
7° 19½′= " " "	543	B. C.=sta.	541+53.53
9° 49½′= " " "	+50	L. C.=	2.33.33
11° 40′= " " "	543+	E. C.=sta.	543+86.86
	86.86		

100—53.53=46.47×3′(def. for 1 ft. of 10° Cur.)=139.41′=
2° 19½″=def. for sta. 542.

Def. for 50 ft.=2° 30′ for a 10° Curve.

Def. for 36.86 ft.=1° 50½′ for a 10° Curve

(These tables are published in Field Books of
KEUFFEL & ESSER Co., New York, N. Y.)



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.