

564

F.B. 864

380

FIELD

Cooper







1313  
Hitch  
Moore  
Hall

1600 Fern St  
N. h South Park To Fir St

1

237.30 - Date 579 242.35 236.56

30 236.35 912 233.25

N. h South Park

W 87 227.7

cb 82 228.2

1/2 83 228.1

c 85 227.9

+2 78 228.6

1/2 76 228.8

cb 75 228.9

E 76 228.8

25 W

E 76 228.8

cb 76 228.8

1/2 75 228.9

c 81 228.3

1/2 83 228.1

cb 85 227.9

W 83 228.1

50 W

W 68 229.6

cb 70 229.4

1/2 79 229.0

c 75 228.9

1/2 75 228.9

cb 75 228.9

E 81 228.3



236.35

75' N

E	7.4	229.0
cb	6.9	229.5
fo	7.0	229.4
c	6.8	230.4
fo	6.0	230.4
cb	5.4	231.0
W.	4.9	231.5

100' N

W	2.8	233.6
cb	3.2	233.2
+4	3.3	233.1
1/2	4.4	232.0
c	4.6	231.8
1/2	5.5	230.9
cb	5.7	230.7
E	5.9	230.5

127' N = 5h Date

E	4.1	232.3
cb	4.2	232.2
1/2	3.5	232.9
c	3.1	233.3
1/2	2.8	233.6
+4	2.7	233.7
cb	1.7	234.7
W	1.1	235.3

236.35

5cb Date

W	1.8	234.6
cb	2.3	234.1
fo	2.4	234.0
c	2.4	234.0
fo	3.1	233.3
cb	3.8	232.6
E	3.9	232.5

5 1/2

E	3.4	233.0
cb	3.1	233.3
1/2	2.3	234.1
c	1.8	234.6
1/2	1.8	234.6
cb	1.8	234.6
W	1.4	235.0

cr.

W	1.3	235.1
cb	1.7	234.7
1/2	1.5	234.9
c	1.1	235.3
1/2	1.8	234.6
cb	2.6	233.8
E	2.5	233.9



236.35

N 1/4

E	1.9	234.5
cb	2.0	234.4
1/2	1.0	235.4
c	0.3	236.1
1/2	0.8	235.6
cb	1.6	234.8
W	1.4	235.0

1/2 cb.

W	0.9	235.5
cb	0.7	235.7
TP	8.93	245.07
1/2	8.21	236.14
1/2	8.3	236.8
c	8.2	236.9
1/2	9.1	236.0
cb	10.1	235.0
E	10.3	234.8

N 1/2

E	9.9	235.2
cb	9.7	235.4
1/2	8.9	236.2
c	7.5	237.6
1/2	7.4	237.7
cb	7.2	237.9
W	9.0	236.1

245.07

4' N

W	4.6	240.5
cb	6.2	238.9
1/2	7.0	238.1
c	7.2	237.9
1/2	11.6	236.5
cb	9.2	235.9
E	9.7	235.4

25' N

E	9.1	235.0
cb	8.7	236.4
1/2	7.4	237.7
c	6.3	238.8
1/2	5.9	239.2
cb	4.7	240.4
W	3.0	242.1

30' N

W	2.8	242.8
cb	3.7	241.2
1/2	5.0	240.1
c	5.5	239.6
1/2	6.7	238.5
cb	7.7	237.4
E	8.2	236.9

3  
3



245.07  
75' N

E	7.1	238.0
cb	7.0	238.1
1/4	5.7	239.4
0	4.7	240.7
1/4	4.1	241.0
cb	2.9	242.2
W	0.7	244.4

100' N

W	0.5	244.6
cb	2.1	243.0
1/4	3.1	242.0
0	3.9	241.2
1/4	5.0	240.1
cb	6.2	238.9
E	6.8	238.3

135' N

E	6.2	238.9
cb	5.7	239.4
+5	5.2	239.9
1/4	4.2	240.9
0	3.2	241.9
1/4	2.1	243.0
+4	1.8	243.3
cb	0.6	244.5

8.26

25195

1.38 243.69

W	6.3	245.7
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25195  
130' N

W	5.5	246.5
cb	7.3	244.7
1/4	8.3	243.7
0	9.2	242.8
1/4	10.4	241.2
+4	11.5	240.5
cb	11.7	240.3
E	12.2	239.8

175' N

E	11.4	240.6
cb	10.3	241.7
1/4	9.3	242.7
0	7.7	244.3
1/4	7.1	244.9
cb	6.1	245.9
W	4.6	247.4

200' N

W	3.9	248.1
cb	5.6	246.4
1/4	6.2	245.8
0	6.5	245.5
1/4	7.8	244.2
cb	8.6	243.4
E	9.1	242.9



251.95

225' N

E	7.8	244.2
S	6.9	245.1
1/4	6.7	245.3
C	5.3	246.7
1/4	5.2	246.8
cb	4.0	248.0
W	2.4	249.6

260' N

W	1.4	250.6
cb	3.2	248.8
1/4	4.3	247.7
C	4.6	247.4
1/4	5.6	246.4
cb	6.5	245.5
E	7.1	244.9

275' N

E	7.7	244.3
cb	6.3	245.7
1/4	5.3	246.7
C	4.2	247.8
1/4	3.8	248.2
cb	2.8	249.2
W	1.0	251.0

251.95

300' N

W	0.7	251.3
cb	3.0	249.0
1/4	4.0	248.0
C	4.6	247.4
1/4	5.2	246.8
1/4	4.6	247.4
cb	7.4	244.6
E	9.1	242.9

321.5' N = 56' E/H

E	10.9	241.05
cb	9.0	242.0
1/4	5.6	246.4
C	4.6	247.4
1/4	4.2	247.8
cb	3.5	248.5
W	1.7	250.2

300'

W	1.8	250.2
cb	3.9	248.1
1/4	4.6	247.4
C	4.5	247.5
1/4	5.6	246.4
cb	9.6	244.4
E	12.4	242.6



25795  
5/4

E	14.9	227.1
cb	10.0	242.0
1/4	6.5	245.5
+3	4.8	247.2
c	4.9	247.1
1/6	4.9	247.1
cb	4.2	247.8
w	2.3	249.7
cr		
w	2.2	249.8
cb	2.3	247.7
1/6	5.1	246.9
c	5.3	246.7
+5	5.4	246.6
1/6	6.9	246.1
cb	11.0	241.0
E	15.0	237.0
N 1/2		
E	13.8	236.2
cb	11.7	240.3
1/6	7.2	244.8
+2	5.6	246.4
c	5.5	246.5
1/6	5.2	244.8
cb	4.7	247.3
w	2.4	249.6

25795  
web

w	2.4	249.6
cb	4.9	247.1
1/6	5.4	246.6
c	5.6	246.4
+6	5.9	246.1
1/6	7.6	244.4
cb	12.0	240.0
N 1/2		
cb	12.1	239.9
1/6	6.7	245.3
c	5.7	246.3
1/6	5.4	246.6
cb	5.1	246.9
w	2.4	249.6
25 W		
w	17	237.3
cb	4.9	247.1
1/6	5.3	246.7
c	5.7	246.3
+7	6.4	245.6
1/6	7.5	244.2
cb	11.9	240.1
+5	12.0	238.0
E	11.9	240.55
7E	6.6	245.4



25195

30 N

6'E	7.0	245.0
E	11.3	240.7
+4	12.8	239.2
cb	11.2	240.9
+3	10.6	241.4
1/4	7.4	244.6
+2	5.9	246.1
c	5.7	246.3
1/6	5.0	247.0
cb	4.7	247.3
W	2.1	249.9

75 N

W	1.7	250.3
cb	4.4	247.6
1/6	5.1	246.9
c	5.6	246.4
+6	6.3	245.7
1/4	8.1	243.9
+5	11.0	241.0
cb	11.9	240.1
+6	11.5	240.5
E	9.1	242.9
5'E	6.3	245.7

83 N

E	6.4	245.6
cb	6.4	245.6
1/4	5.7	246.3

25195

c	5.4	246.6
1/4	4.5	247.5
cb	4.2	247.8
W	1.7	250.3

100 N

W	1.2	250.8
cb	3.8	248.2
1/6	3.9	248.1
c	5.0	247.0
1/6	4.4	247.6
cb	3.2	248.8
E	2.6	249.4

125 N

E	1.6	250.4
cb	3.3	249.7
1/6	3.6	248.4
c	4.2	247.8
1/6	3.3	248.7
cb	3.3	248.7
W	0.6	251.4

150 N

W	0.6	251.4
+5	2.3	249.7
cb	3.6	249.4
1/6	2.6	249.4
c	3.2	248.8
1/4	2.2	249.8



		2519.5	
cb		1.9	250.1
E		1.5	250.5
	195 N		
E		1.0	251.0
cb		1.1	250.9
1/2		1.2	250.8
c		1.7	250.3
1/4		1.8	250.2
cb		1.9	250.1
+4		1.5	250.5
W		+0.6	252.6
T.P	1138	262.35	0.98 250.97
		200 N	
W		8.7	253.7
cb.		11.2	251.2
1/2		11.2	251.2
c		11.2	251.2
1/4		10.4	252.0
cb		10.3	252.1
E		9.9	252.5
	225 N		
E		9.0	253.4
cb		9.3	253.1
1/4		9.6	
c		9.5	
1/4		9.5	
cb.		9.5	

	262.35	
+2		5.0
W		6.6
	200 N	
W		5.2
+8		6.4
cb		7.7
1/4		7.6
c		7.9
1/2		8.6
cb		8.3
E		7.9
	275 N	
E		6.5
cb		7.3
1/2		7.3
c		6.5
1/4		6.2
cb		6.0
W		4.6
	300 N	
W		3.4
cb		4.5
1/4		5.0
c		5.0
1/4		4.6
cb		5.6
E		5.5



262.35  
310' N

E	5.0
ob	5.0
1/2	4.8
c	4.5
1/4	4.3
cb	4.0
W	2.9
310' N on East } = Sh Fir	
320' N " W }	
W	2.7
cb	3.6
1/4	4.2
c	4.5
1/2	4.6
cb	4.9
E	5.0

Intersection of Fir not taken as contractor is filling in with excess dirt -

0.18 241.23 241.05

Sh Elm -	
15' E of line	1.6
scb.	
25' E of line	13.5
5/4	
25' E of line	16.8
cr	
15' E of line	9.5

25' E	9.9
N 1/4	
10' E	8.6
20' E	8.8
Nob.	
EL.	9.3
6' E	11.2
15' E	9.9
25' E	7.1
N.L.	
EL.	8.5
20' E	3.6



3/11/31  
 113 N. 2000 ft  
 Hall

Köcc Wall St (to Jolla)  
 from Girard to Icterus

8.07 99.33  
 BM Wear Prospect and Jenner 9126

1002 109.58 027 99.06

N. Girard

w	8.3	100.8
cb	8.3	100.8
1/2	7.7	101.4
c	7.1	102.0
1/4	6.9	102.2
gutter	6.9	102.2
cement	6.60	102.48

25' N

E cb	6.27	102.8
gutter	5.8	103.3
1/2	6.5	102.6
c	6.8	102.3
1/2	7.3	101.8
cb	7.5	101.6
w	8.0	101.1

50' N

w	7.7	101.4
cb	7.2	101.9
1/2	7.0	102.1
c	6.3	102.8
1/2	6.0	103.1
gutter	6.1	103.0
cement	5.97	103.2

10908

75' N

E cb	5.76	103.3
gutter	5.3	103.8
1/2	5.8	103.3
c	6.2	102.9
1/2	6.7	102.4
cb	6.9	102.2
w	7.2	101.9

100' N

w	6.7	102.4
cb	6.5	102.6
1/2	6.3	102.8
c	5.9	103.2
1/2	5.4	103.7
gutter	5.3	103.8
cement	5.48	103.6

125' N

cement	5.75	103.9
gutter	4.9	104.2
1/2	5.1	104.0
c	5.6	103.5
1/2	5.9	103.2
cb	6.0	103.1
w	6.3	102.8



109.08

150' N

W	5.9	103.2
cb	5.6	103.5
1/2	5.5	103.6
c	5.1	104.0
1/2	4.7	104.4
cb	4.3	104.8
E	4.1	105.0

175' N

E	3.9	105.2
cb	4.1	105.0
1/2	4.6	104.5
c	4.9	104.2
1/2	5.2	103.9
cb	5.3	103.8
W	5.5	103.6

200' N

W	5.1	104.0
cb	4.9	104.2
1/2	4.9	104.2
c	4.6	104.6
1/2	4.3	104.8
cb	3.9	105.2
E	3.9	105.2

109.08

225' N

E	3.8	104.3
cb	3.8	104.3
1/2	4.2	104.9
c	4.5	104.6
1/2	4.6	104.5
cb	4.6	104.5
W	4.7	104.4

250' N

W	4.5	104.6
cb	4.2	104.9
1/2	4.2	104.9
c	4.4	104.7
1/2	4.0	105.1

270

141.38

4.40

104.68

cb	5.6	105.8
E	5.8	105.6

275' N

E	5.5	105.9
cb	5.8	105.6
1/2	6.3	105.1
c	6.5	104.9
1/2	6.6	104.8
cb	6.4	105.0
W	6.6	104.8



11138

300' N. St. Herschel

W	6.3	105.1
cb	6.3	105.1
1/2	6.3	105.1
0	6.2	105.2
1/4	6.0	105.4
cb	5.8	105.6
E	5.7	105.7

S. cb.

E	5.8	105.6
cb	5.9	105.5
1/2	6.1	105.3
0	6.0	105.4
1/4	6.0	105.4
cb	6.4	105.0
E	6.2	105.2

S 1/4

W	6.4	105.0
cb	6.2	105.2
1/2	6.1	105.3
0	5.9	105.5
1/4	6.0	105.4
cb	5.8	105.6
E	5.7	105.7

11138

cr

E	5.7	105.7
cb	5.8	105.6
1/2	5.9	105.5
0	6.0	105.4
1/4	6.1	105.3
cb	6.1	105.3
W	6.3	105.1

N 1/4

W	6.3	105.1
cb	6.1	105.3
1/2	5.9	105.5
0	6.0	105.4
1/4	5.8	105.6
cb	5.6	105.8
E	5.4	106.0

N. cb.

E	5.1	106.3
cb	5.6	105.8
1/2	5.7	105.7
0	6.0	105.4
1/4	6.0	105.4
cb	6.2	105.2
W	6.1	105.3



11138

12h Herchel

W	6.1	105.3
cb	5.9	105.5
1/2	6.0	105.4
c	5.8	105.6
1/2	5.8	105.6
cb	5.3	106.1
E	5.2	106.2

25 N

E	5.1	106.3
cb	5.2	106.2
1/2	5.5	105.9
c	5.6	105.8
1/2	5.5	105.9
cb	5.7	105.7
W	5.9	105.5

30 N

W	5.8	105.6
cb	5.6	105.8
1/2	5.4	106.0
c	5.5	105.9
1/2	5.4	106.0
cb	5.2	106.2
E	4.9	106.5

11138

75 N

E	5.1	106.3
cb	5.0	106.4
1/2	5.3	106.1
c	5.4	106.0
1/2	5.3	106.1
cb	5.3	106.1
W	5.5	105.9

100 N

W	5.3	106.1
cb	5.3	106.1
1/2	5.1	106.3
c	5.0	106.4
1/2	5.2	106.2
cb	4.8	106.6
E	4.8	106.6

125 N

E	4.6	106.8
cb	4.8	106.6
1/2	5.0	106.4
c	5.0	106.4
1/2	5.1	106.3
cb	5.0	106.4
W	5.3	106.1

13<sup>13</sup>



11.3.8

150' N

W	5.1	106.3
cb	4.9	106.5
1/2	4.9	106.5
c	4.8	106.6
1/2	4.8	106.6
cb	4.6	106.8
E	4.4	107.0

175' N

E	4.2	107.2
cb	4.4	107.0
1/2	4.5	106.9
c	4.7	106.7
1/2	4.7	106.7
cb	4.6	106.8
W	4.7	106.5

200' N

W	4.6	106.8
cb	4.3	107.1
1/2	4.4	107.0
c	4.5	106.9
1/2	4.1	107.3
cb	4.2	107.2
E	4.0	107.4

11.3.8

225' N

E	3.7	107.7
cb	3.8	107.6
1/2	3.8	107.6
c	4.1	107.3
1/2	4.2	107.2
cb	4.2	107.2
W	4.3	107.1

250' N

W	4.0	107.4
cb	3.8	107.6
1/2	4.0	107.4
c	3.8	107.6
1/2	3.7	107.7
cb	3.6	107.8
E	3.4	108.0

275' N

E	3.2	108.2
cb	3.3	108.1
1/2	3.6	107.8
c	3.6	107.8
1/2	3.8	107.6
cb	3.7	107.7
W	3.7	107.7

1414



11138  
 300' N-Sk Ictinus

W	37	107.7
cb	34	108.0
1/2	36	107.8
c	32	108.2
1/2	32	108.2
cb	29	108.5
E	28	108.6
TP	918 11523 533	10605
check	BM Herschel Mt Connecticut	216 113.07 113,033

13<sup>1/2</sup> m<sup>2</sup> water  
 1/3 m<sup>2</sup> wall  
 sec Herschel St (La Jolla)  
 from Wall to Prospect

110.18

NE Arch Grand-Mall

10245

Wk Wall

s	5.1	105.1
cb	5.0	105.2
1/2	5.2	105.0
c	5.1	105.1
1/2	5.1	105.1
cb	4.9	105.3
N	4.9	105.3

25' W

N	4.8	105.4
cb	5.0	105.2
1/2	5.3	104.9
c	5.1	105.1
1/2	5.3	104.9
cb	5.2	105.0
s	5.3	104.9

50' N

s	5.5	104.7
cb	5.2	105.0
1/2	5.3	104.9
c	5.3	104.9
1/2	5.1	105.1
cb	4.8	105.4
N	4.4	105.8



110.18

75' W

N	4.9	105.3
cb	5.0	105.2
1/2	5.2	105.0
c	5.3	104.9
1/2	5.3	104.9
cb	5.4	104.8
S	5.4	104.8

100' W

S	5.6	104.6
cb	5.3	104.9
1/2	5.3	104.9
c	5.3	104.9
1/2	5.1	105.1
cb	4.8	105.4
N	4.7	105.5

125' W

N	4.6	105.6
cb	4.8	105.4
1/2	5.0	105.2
c	5.2	105.0
1/2	5.3	104.9
cb	5.3	104.9
S	5.5	104.7

110.18

100' W

S	5.8	104.4
cb	5.5	104.7
1/2	5.4	104.8
c	5.2	105.0
1/2	5.1	105.1
cb	4.7	105.5
N	4.5	105.7

175' W

N	4.7	105.5
cb	4.8	105.4
1/2	5.1	105.1
c	5.2	105.0
1/2	5.5	104.7
cb	5.4	104.8
S	5.9	104.3

500' W

S	6.0	104.2
cb	5.6	104.6
1/2	5.5	104.7
c	5.4	104.8
1/2	5.1	105.1
cb	4.9	105.3
N	4.7	105.5



11018

225' W

N	4.7	105.5
cb	5.3	104.9
1/2	5.8	104.4
c	5.7	104.5
1/2	5.8	104.4
cb	5.9	104.3
s	6.3	103.9

250' W

s	6.5	103.7
cb	5.9	104.3
1/2	5.8	104.4
c	5.9	104.3
1/2	5.8	104.4
cb	5.7	105.0
N	4.8	105.4

203

107.50

275' W

TP	4.71	105.47
N	2.2	105.3
cb	2.8	104.7
1/2	3.6	103.9
c	3.5	104.0
1/2	3.6	103.9
cb	3.8	103.7
s	4.2	103.3

107.50

300' W

s	4.8	102.7
cb	4.3	103.2
1/2	3.9	103.6
c	3.6	103.9
1/2	3.6	103.9
cb	3.1	104.4
N	2.5	105.0

325' W

N	2.7	104.8
cb	3.4	104.1
1/2	4.1	103.4
c	4.2	103.3
1/2	4.4	103.1
cb	4.8	102.7
s	5.0	102.5

350' W

s	6.0	101.5
cb	5.3	102.2
1/2	5.0	102.5
c	4.6	102.9
1/2	4.5	103.0
cb	3.7	103.8
N	3.2	104.3



107.50

375' W

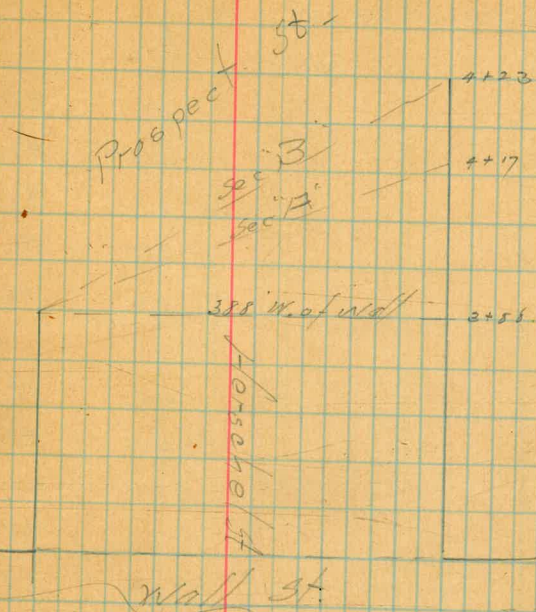
N	3.3	104.2
sb	52.8	103.7
1/2c	25.2	102.3
c	4.9	102.6
1/2c	5.2	102.3
sb	6.0	101.5
s	6.0	101.5
	6.8	100.7

388' W

s	8.3	99.20
sb	8.1	99.4
1/2c	7.1	100.4
c	6.2	101.3
1/2c	5.9	101.6
sb	55.5	102.0
	2.3	103.2
N	3.6	103.9

50c A

N	4.4	103.1
sb	55.1	102.4
1/2c	6.4	101.1
c	6.8	100.7
1/2c	7.2	100.3
1/2c	7.7	99.8
sb	8.4	99.1
Cement curb	8.50	99.0



Sec "B"		
1/2c	8.3	99.2
c	7.4	100.1
1/2c	7.1	100.4
sb	7.1	100.4
N	6.3	101.2
Cement curb	6.42	101.1



Levels for culverts I bet 27th & 28th & Haitt & 29th  
 " " " 28th " J " 8 " K  
 Elevations N.W. cor 28th & "I"  
 1/4 section  
 1/4 Haitt

Levels for Culvert bet 27th & 28th  
 102.78

0+0	4.8	98.0
+25 South	5.0	97.8
+50 "	6.2	96.6
+75 "	6.4	96.4
+90	6.6	96.2

0+0	4.8	98.0
+25 N	4.5	98.3
+50 N	3.3	99.5
+75 N	3.1	99.7
+100 N	3.2	99.6
+125	2.7	100.1
+150	1.5	101.3

Levels for Culvert bet Haitt & 29th  
 108.11

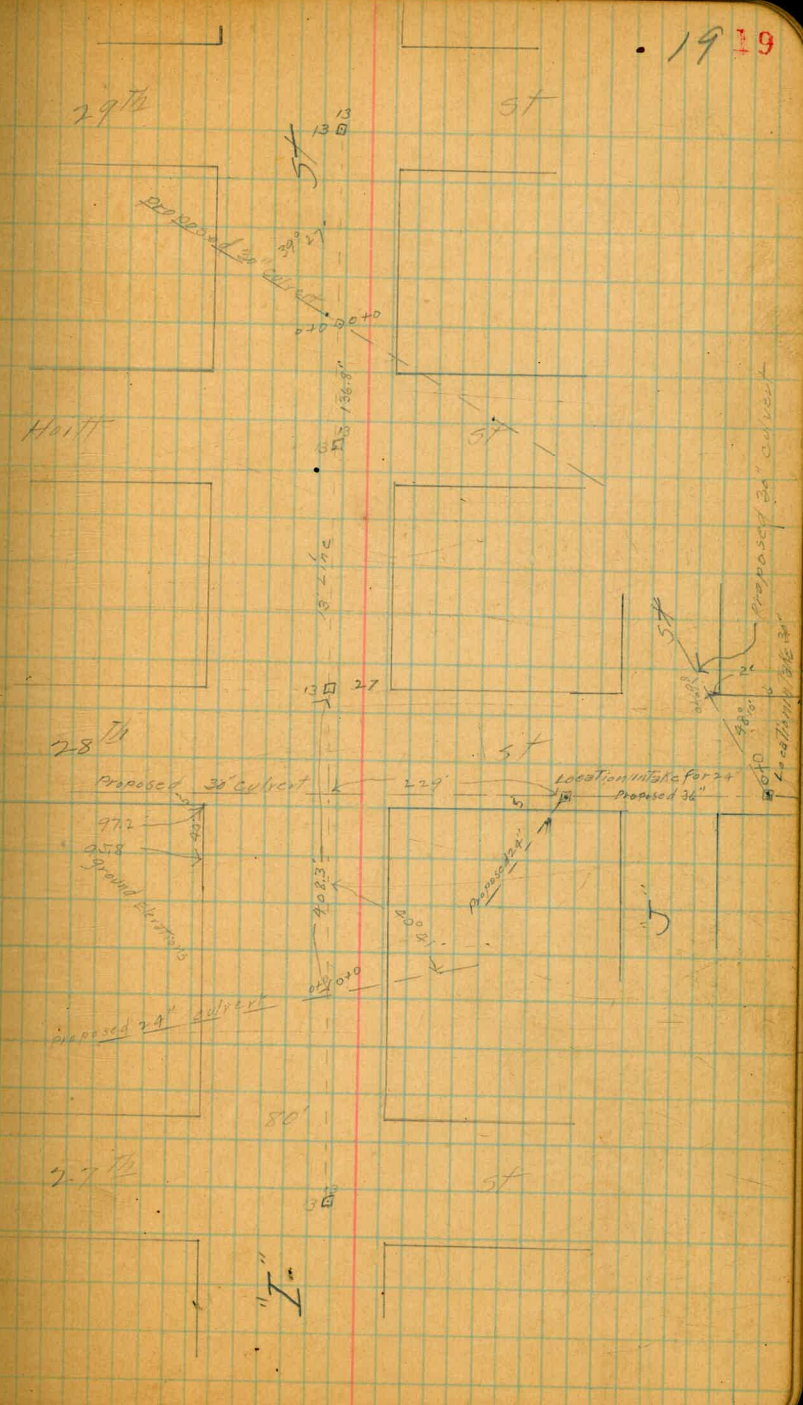
0+0	10.0	98.1
0+06 - water of N. End 18" iron pipe culvert	13.6	94.5
+25 south	12.5	95.6
+50	12.2	95.9
+75	10.7	97.7
+90	11.2	96.9
+110	11.5	96.5
+130	11.6	96.5

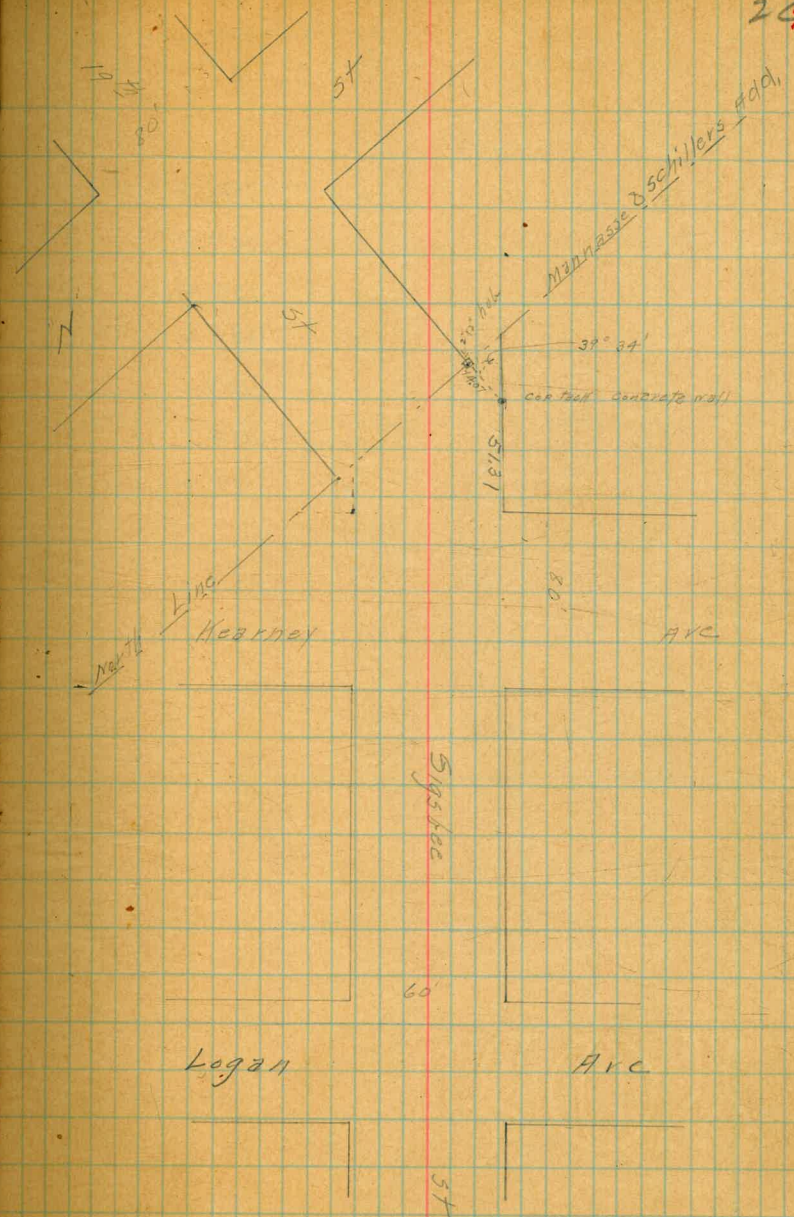
0+0	10.0	98.1
0+25 natural water course filled up	8.9	99.2
0+50	10.6	97.5
0+75	4.0	104.1
+105	3.3	104.3
+120	12.1	96.0
+144 - water S. End 18" iron pipe culvert	13.3	94.6
+160	16.9	91.2
	17.5	90.6

Levels for Culvert 28th St bet J " 8 " K  
 92.37

0+0	7.3	85.1
+25	7.3	85.1
+50	6.9	85.5
+75 = E.L. 28th	5.3	87.1
+85	7.6	84.8
+85	7.6	84.8
+90	5.7	86.7







Survey showing intersection of E.L.N. St & S.L. Sigstec  
with reference to N.L.M. & S. Add.

3/17/13  
Lumpkin  
Kerr.



Location of Proposed 30" culvert with reference to  
 where it leaves 28th st and levels to figure location  
 of where it will leave toe of slope of 28th

HA  
 114.93

2/1/10  
 simple  
 sketch  
 here

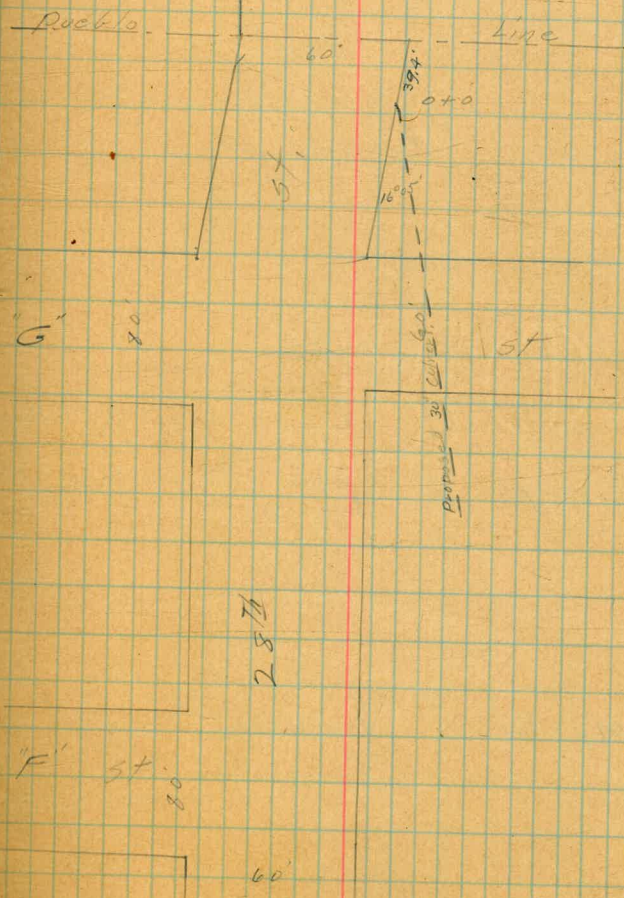
0+0	2.1	106.8
1+25	7.6	107.3
150	6.5	108.1
175	5.7	109.2
1+0	6.4	108.5
1+25	4.2	110.7
1+50	2.9	112.0

Elevations

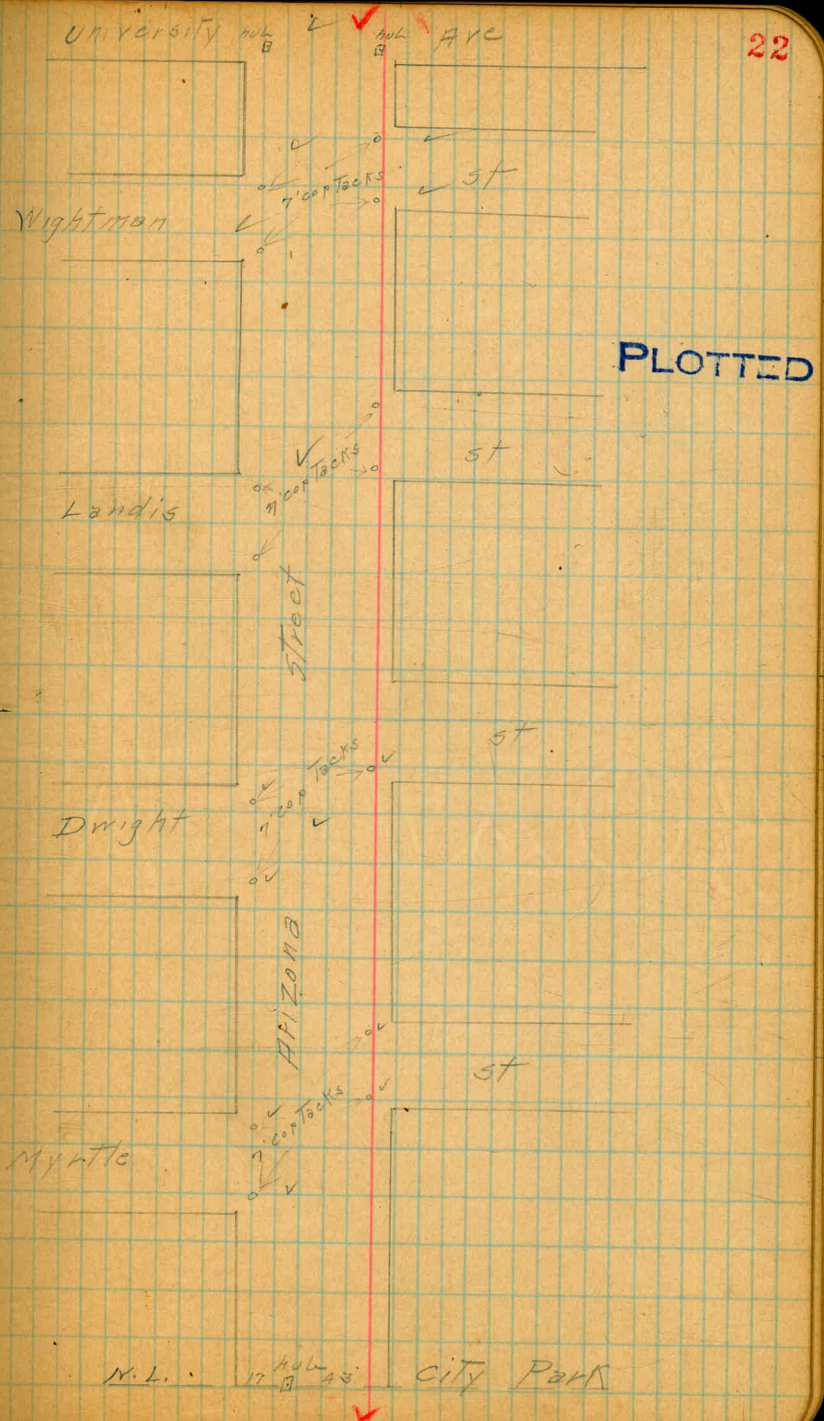
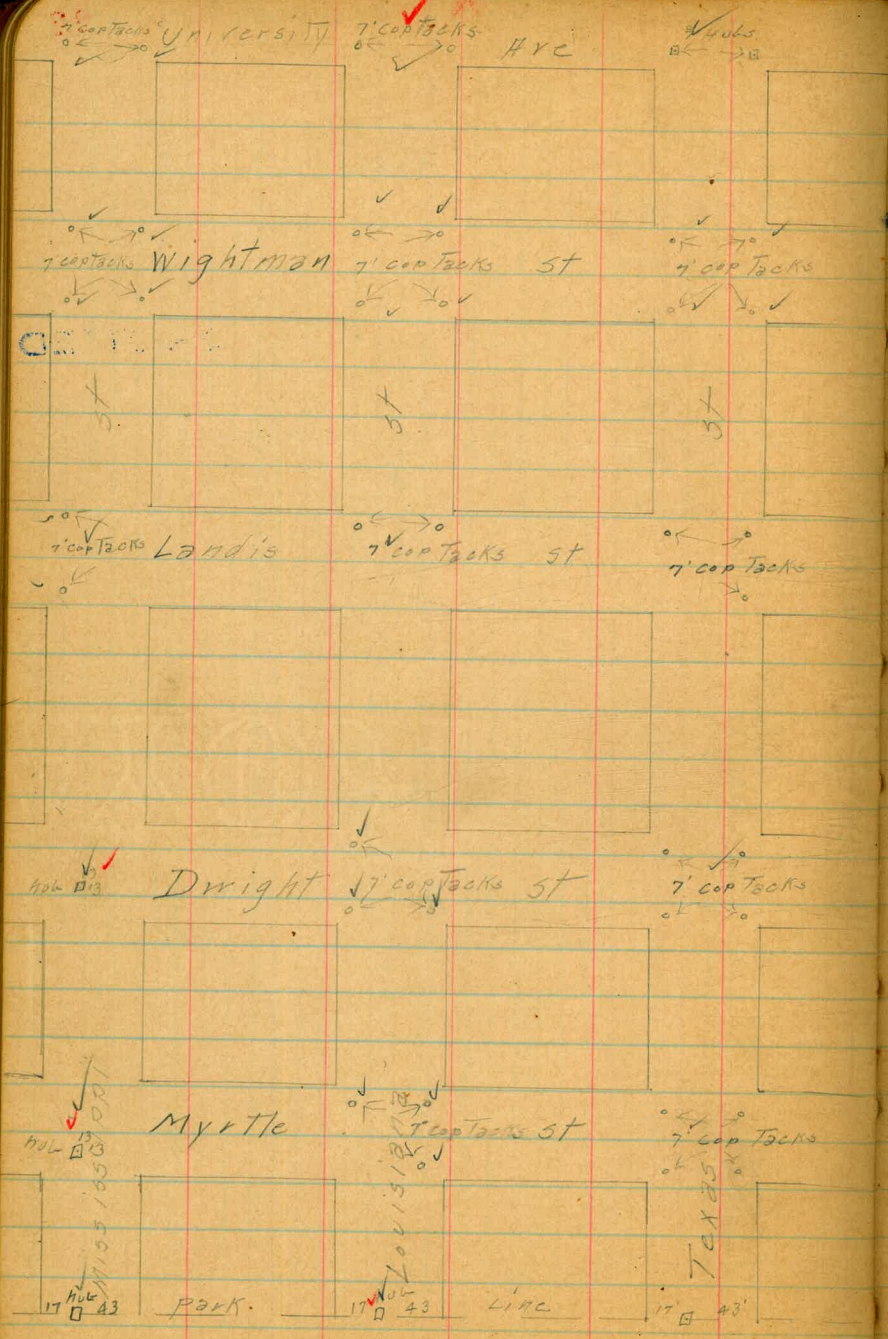
36" culvert under "K" st at 28th st

5' End bottom = 77.88

100' N or S end of 36" pipe = 78.84









Madison

Ave

Monroe

Ave

o-cop tack in walk

PLOTTED

Meade

Ave

street

street

El Cajon

13  
113 Hub

Ave

13  
113

Howard

st

TEXAS

ARIZONA

Dolk

st

Lincoln

st

Mississippi

st

Alabama

13  
113

st

PLOTTED

Ave

Florida

st

o-cop tack in walk

Georgia

st

Park

MISSISSIPPI

bird



University

9' Hubs ✓

Ave

65'

Wightman

7' cap tracks

st

Street

PLOTTED

Landis

7' cap tracks

st

Dwight

7' tracks

st

Arnold

Myrtle

9' Hubs

st

N. L.

1955 455 ✓

City Park

24

Meade

9' cap tracks ✓

Boundary of

El Cajon

13' Hubs

Ave

Street

PLOTTED

Harvard

7' cap tracks

st

Polk

7' cap tracks

st

Lincoln

7' cap tracks

st

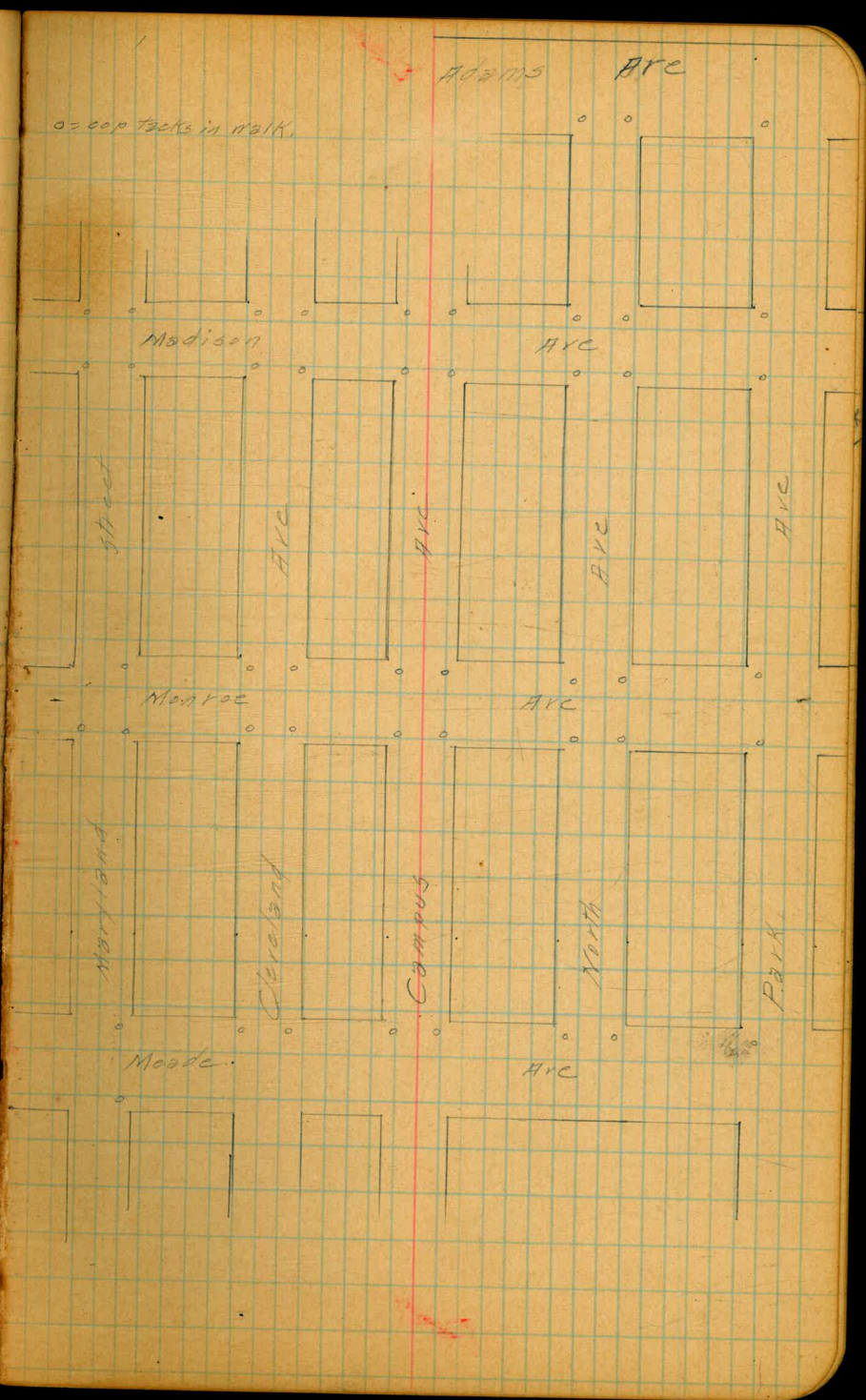
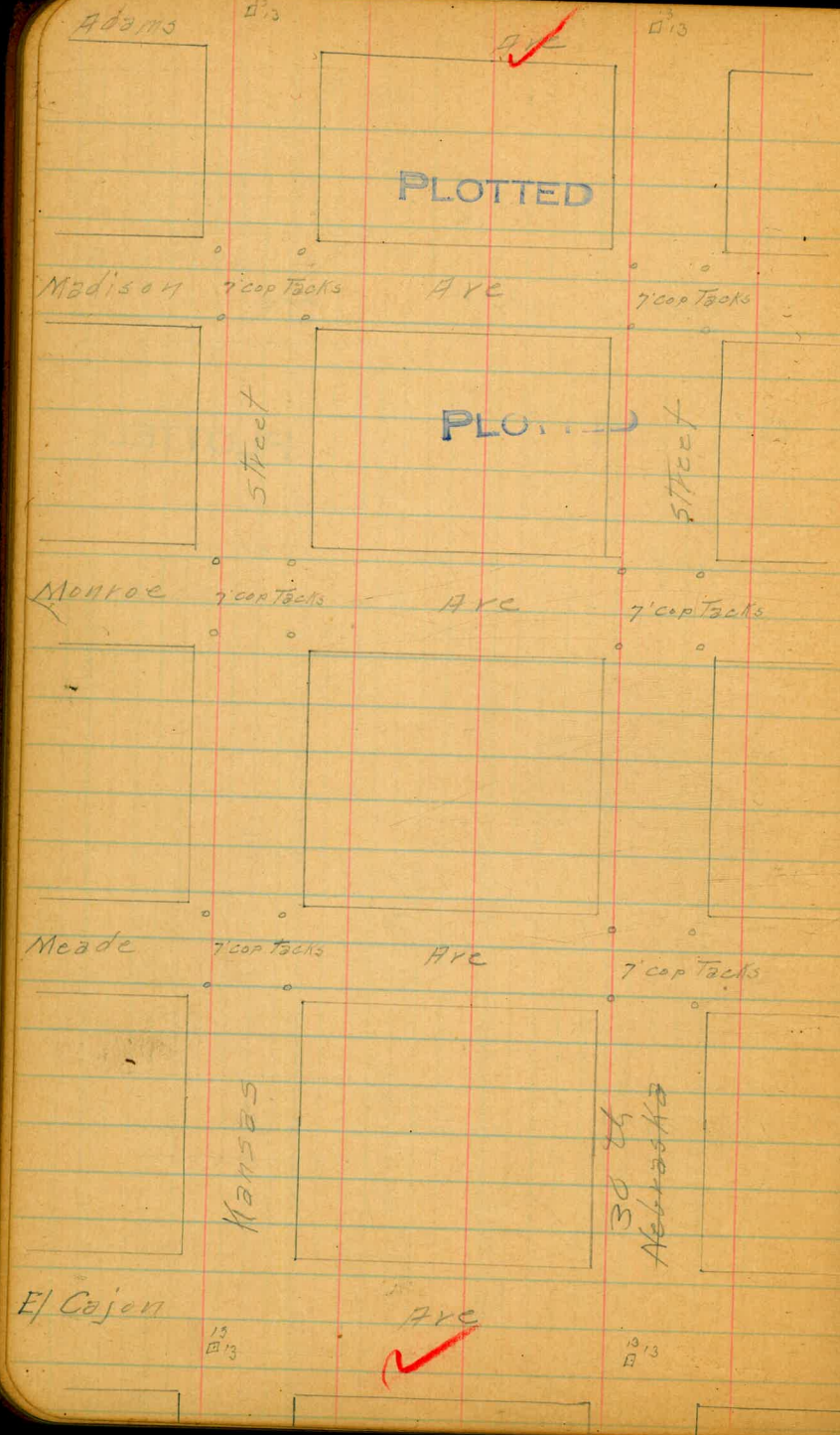
Zona

University

9' Hubs ✓

Ave







Survey for extension of  
1/4 Hutch-Tide St to La Jolla Ave

Tapcock

Hurtz

Wetherby

75

322.88 1/2

567.98

570.11

2315.28

70

49° 08'

Mon.

271.57 La Jolla - Moore

377.12 Moore - Hancock

La Jolla Ave.  
165.80  
Sta 11+64.28

1187.0  
225.1

196.56  
394.6

Sta 5+58.66

74.22  
44.56 1/2

Ryan Curve Sta 8+33.92

133.50  
North

3° 53' Curve  
External Dist 52.16

52.16

138.50  
South

Sta 7+81.47

44.56 1/2  
Sta 7+70.25

1215.24  
North

90°

Man at 515.24

Sta 4+99.25

2° Curve  
External Dist 51.53

51.53

54.17  
21.87

Sta 2+09.25  
48° 06'

51.53  
Sta 2+10.26

49° 08'

Man at 0+00

7

7

7

7

7

La Jolla Ry  
and Moore

South Line Wetherby  
Sta 2+00.42

Man at 308.05  
Sta 100 W/L  
Hurtz

Man at 515.24  
Curtis

Santa Fe

W Line Kurtz St.  
(line taken to Moore on)  
NW Cor Wetherby St

Tide St



Hatch  
14th mo  
Hall

Levels on Extension of  
Fide St.

BM Mon	3.94	14.48 <sup>v</sup>	10.526	Hancock Method
T.P	4.37	6.95 <sup>v</sup>	11.90	2.58
Sta 0+00		0+00		
S		5.8		
cr		5.3	1.6	
N		5.6		
		0+50		
N		6.4		
cr		4.9	2.0	
S		6.0		
		0+60		
S		5.3		
cr		4.9	2.0	
N		8.3		
		1+00		
S		5.6		
cr		5.0	1.9	
N		8.7		
		1+15		
N		8.4		
cr		4.1	2.8	
S		4.4		
		1+45		
S		4.9		
cr		2.7	4.5	
N		6.6		

T.P	11.48	6.95 <sup>v</sup>	16.85	15.8	5.37
			2+00		
N	10.54			10.3	
cr	3.94			8.5	8.3
S	4.37			12.8	
	11.48				
	12.60				
	12.91				
	12.65		2+20		
	12.79				
S	12.81			12.1	
	7.68				
cr	1.23			7.7	9.1
	0.12				
	6.06			7.7	
	11.08				
	6.58				
	4.50		2+50		
N				8.6	
cr				7.2	9.6
S				10.9	
			2+65		
S				5.77	
				6.70	
cr				6.87	9.98
N				3.0	
	11.90				
	1.55				
	7.69		2+85		
	1.15			8.1	
N	0.67			80.3	
	0.11				
cr	0.26			8.4	8.4
	1.13				
S	9.17			6.9	
	1.66				
	11.00				
	8.24		3+00		
	6.58			8.4	
S				8.4	8.1
cr				0.4	
N					



	16.85		
	3+10		
N		0.6	
CV		8.4	8 <sup>2</sup>
S		2.9	
	5+50		
S		4.4	
CV		7.9	8 <sup>2</sup>
N		2.9	
	4+00		
N		4.2	
CV		5.7	11 <sup>2</sup>
S		6.4	
	4+25		
S		9.2	
CV		6.8	10 <sup>2</sup>
N		4.7	
	4+50		
N		4.0	
CV		6.8	10 <sup>2</sup>
S		8.1	
	4+75		
S		9.9	
CV		7.5	9 <sup>2</sup>
N		5.1	
TP	12.60	20.76	7.69
			9.16

	21.76		
	5+00		
N		11.5	
CV		12.6	9 <sup>2</sup>
S		14.1	
	5+20		
S		14.3	
CV		12.4	9 <sup>2</sup>
N		10.6	
	5+50		
N		9.6	
CV		10.6	11 <sup>2</sup>
S		11.9	
	6+00		
S		8.9	
CV		7.8	14 <sup>2</sup>
N		7.5	
	6+50		
N		4.3	
CV		5.3	16 <sup>2</sup>
S		6.5	
	7+00		
S		4.1	
CV		3.6	19 <sup>2</sup>
N		1.9	
TP	12.91	38.52	11.5
			20.61



33.52

7+50

N	10.8	
cr	12.0	21.5
S	13.7	

7+80

S	11.4	
cr	9.7	22.8
N	8.3	

8+00

N	top rail La Jolla line	27.5	
cr		8.4	25.1
S		9.1	

8+12

S	8.6	
cr	7.8	25.7
N	4.1	

8+20

N	5.4	
cr	3.1	30.4
S	7.9	

8+25

S	7.3		
cr	top rail	2.18	31.24
N	5.0		

8+40

N	4.0	29.5
cr	4.5	

33.52

S 2.1

8+65

S 3.8

cr 1.7 31.8

N 0.3

TP 12.65 45.50 0.67 32.85

9+00

N 7.1

cr 8.7 36.8

S 10.9

9+50

S 5.3

cr 2.1 43.4

N 0.0

TP 12.79 58.15 0.11 45.39

10+00

N 5.0

cr 8.8 49.4

S 10.9

10+50

S 3.6

cr 1.5 56.7

TP 12.81 40.73 0.26 57.92

N 11.0

10+70

N = Wh La Jolla Ave 0.5

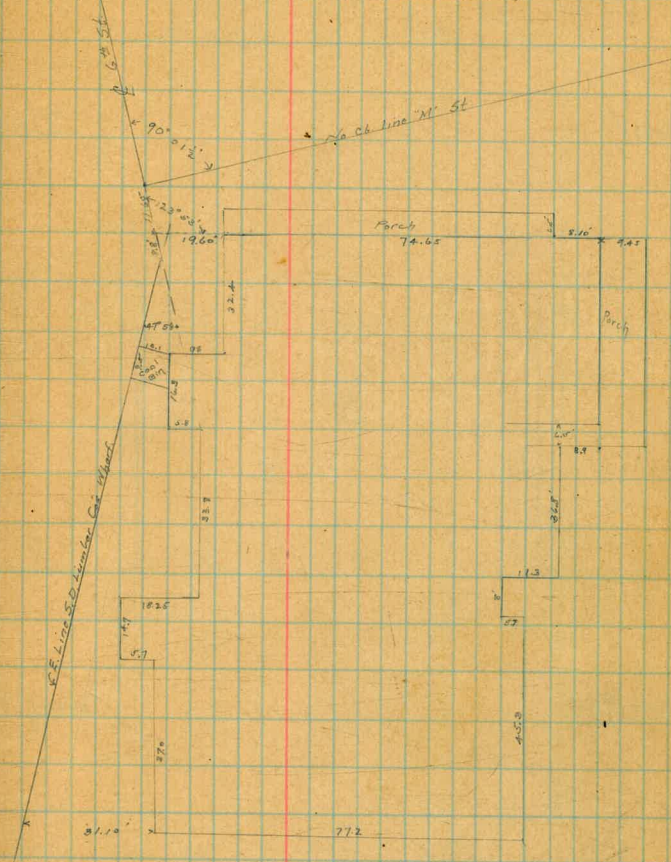
cr 10.4 60.3



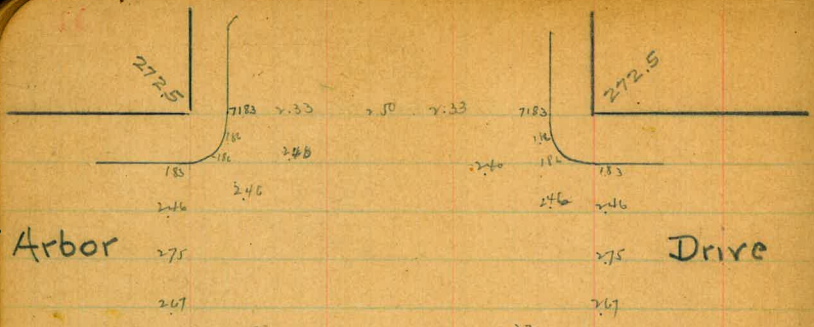
		70.73 ✓		
S			13.5	
		11+00		
S			8.8	
CV			4.5	66 <sup>2</sup>
		11+37		
S			23	
TP	758	77.18 ✓	1.18	69.60 ✓
		11+12		
CV = W Line La Jolla Ave			4.7	72 <sup>5</sup>
		11+50		
S = W Line La Jolla Ave			2.6	
		11+65		
CV on rail			202	7516 ✓
TP	123	69.24 ✓	9.17	68.01
"	0.12	57.70 ✓	11.66	57.58 ✓
"	6.06	52.76 ✓	11.00	46.70 ✓
PM -			826	44.50 ✓



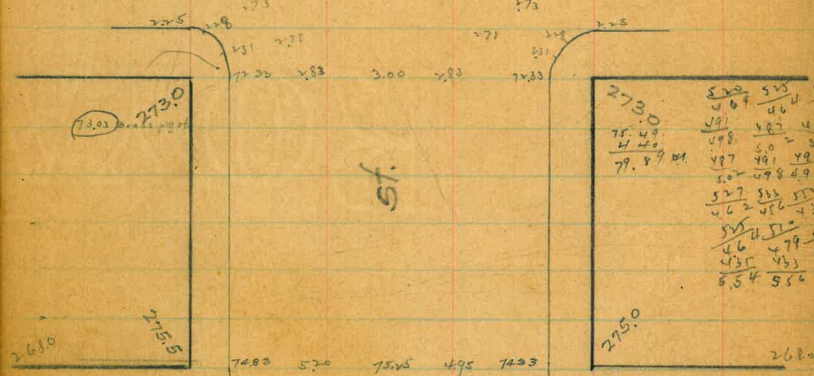
Location of Crookman's Bath House Fort of 6<sup>th</sup> St



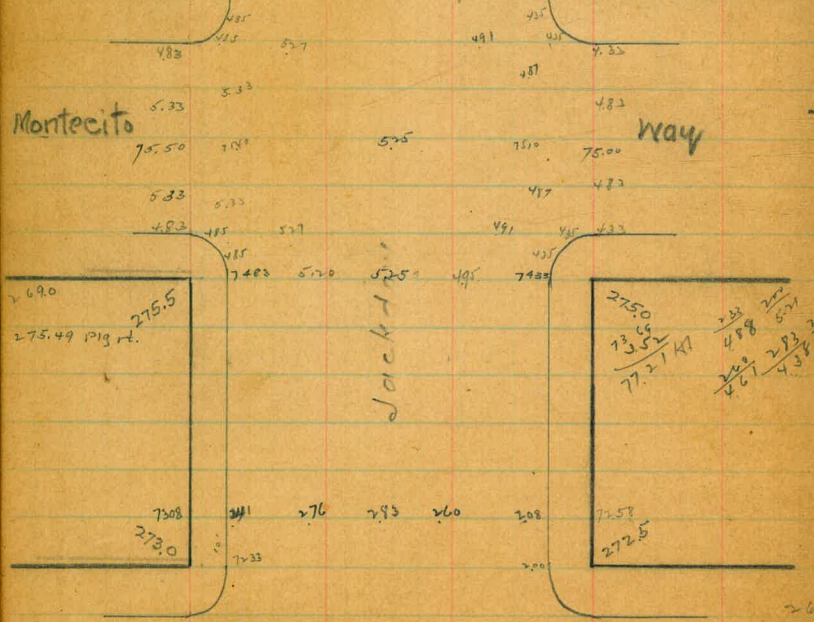




Arbor Drive



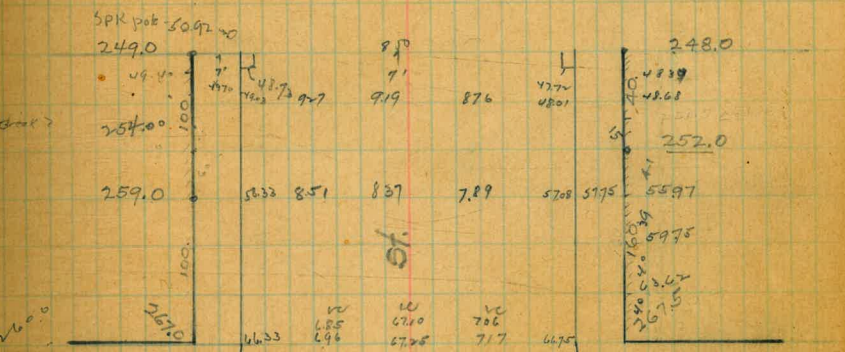
Montecito Way



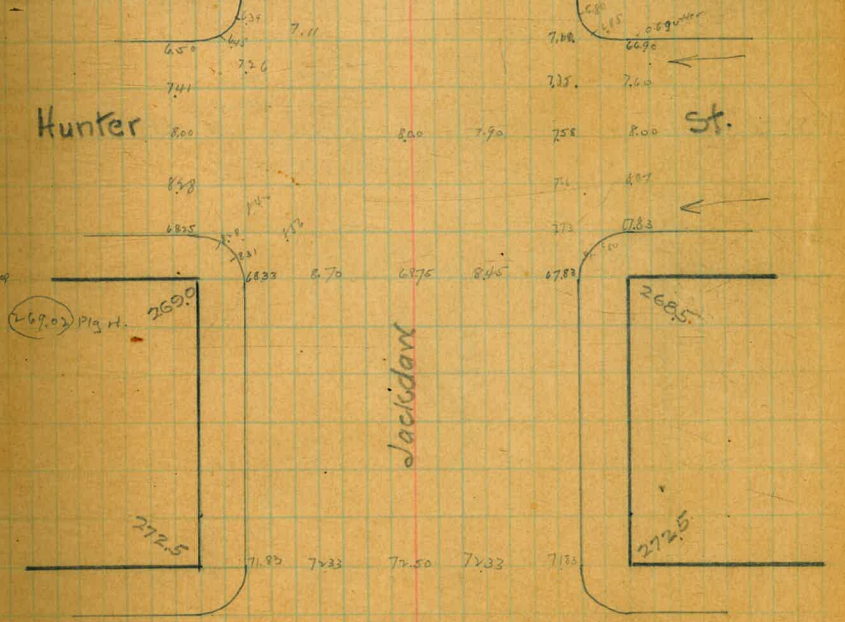
Lewis St. Jack St.

27369 R.R. Spk SW con

269.02	631.2	572.5	559.7	540.2	520.0	490.0	470.0	450.0
27.37	5.09	9.56	13.04	14.11	16.16	17.16	18.16	19.16
69.37 MI	62.62	59.75	55.97	54.00	52.00	49.00	47.00	45.00
57.64 TT	56.8	54.2	52.6	52.3	50.3	48.3	47.2	46.6
58.16 MI	69.02	63.3	67.5	68.3	69.3	70.3	71.3	72.3
69.02	69.35 MI	2.0	2.60	11.0	10.50	11.57	9.33	8.90
69.17 MI	10.31	6.85	7.0	7.0	7.89	8.37	8.51	8.75
10.12	59.75 TT	2.50	2.25	2.24	1.46	10.98	10.84	10.77
59.95 TT	59.79 MI	69.02	69.02	69.02	69.02	69.02	69.02	69.02
59.23 MI	69.02	69.02	69.02	69.02	69.02	69.02	69.02	69.02
69.02	69.02	69.02	69.02	69.02	69.02	69.02	69.02	69.02
69.02	69.02	69.02	69.02	69.02	69.02	69.02	69.02	69.02
57.89 TT	57.89	57.89	57.89	57.89	57.89	57.89	57.89	57.89
58.09 MI	58.09	58.09	58.09	58.09	58.09	58.09	58.09	58.09



Hunter St. Jack St.



Arbor Drive Jack St.



Hawk

Ibis

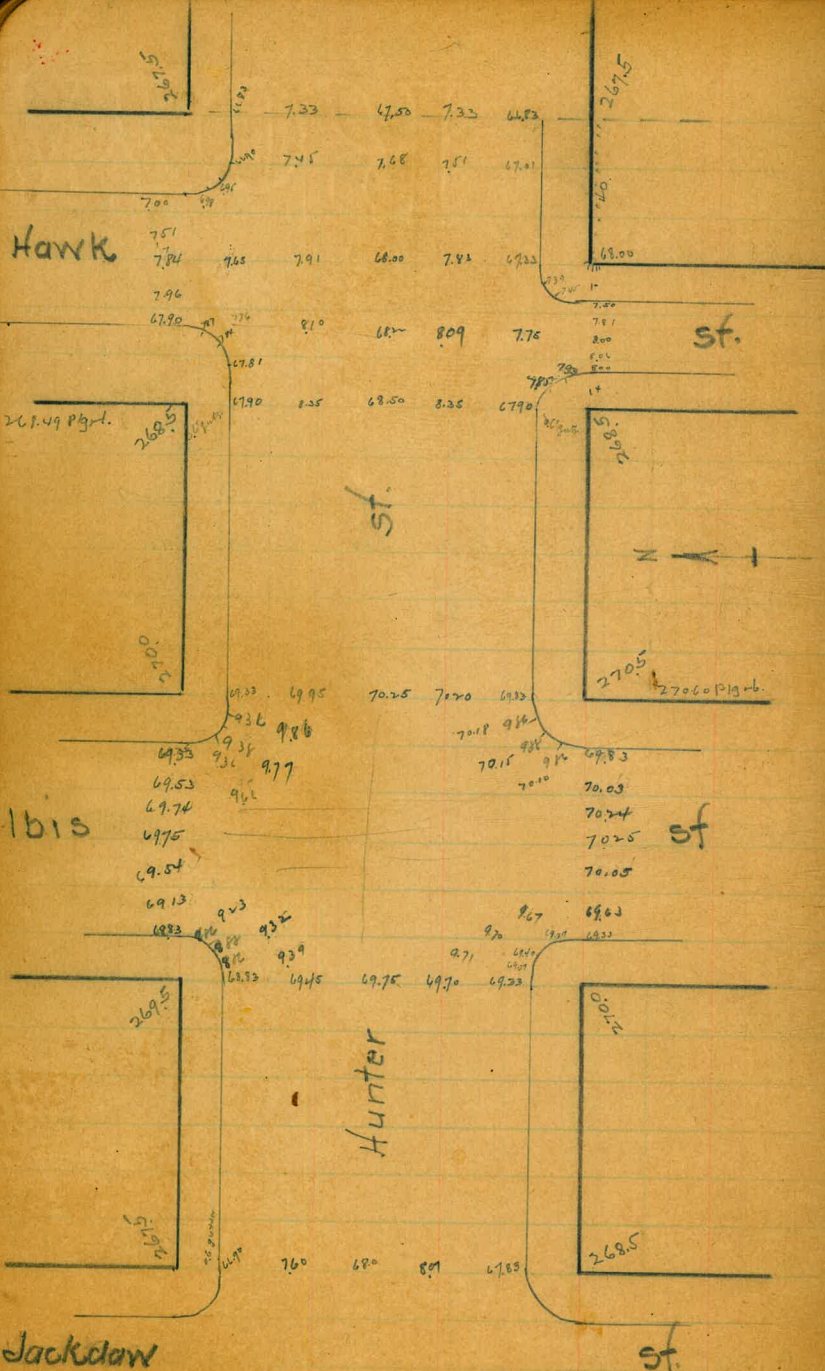
Jackdaw

Hunter

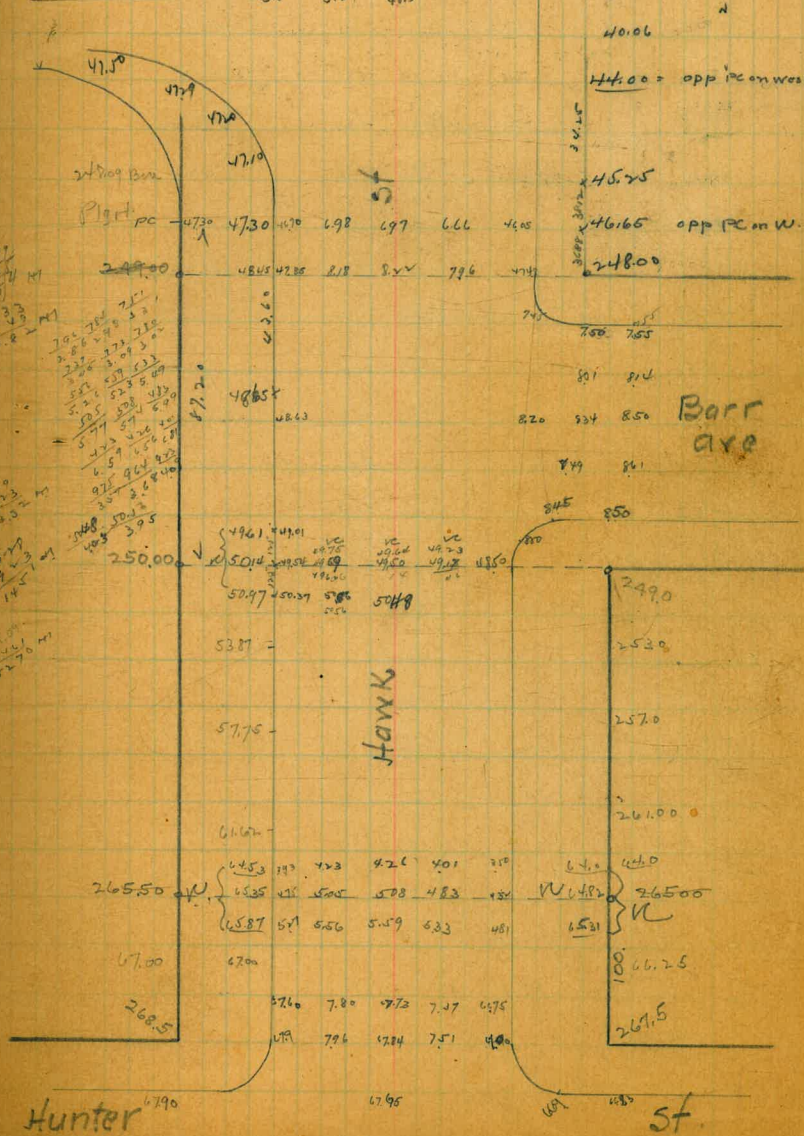
st.

st

st.



4809	4810	4811	4812	4813	4814	4815	4816	4817	4818	4819	4820	4821	4822	4823	4824	4825	4826	4827	4828	4829	4830	4831	4832	4833	4834	4835	4836	4837	4838	4839	4840	4841	4842	4843	4844	4845	4846	4847	4848	4849	4850	4851	4852	4853	4854	4855	4856	4857	4858	4859	4860	4861	4862	4863	4864	4865	4866	4867	4868	4869	4870	4871	4872	4873	4874	4875	4876	4877	4878	4879	4880	4881	4882	4883	4884	4885	4886	4887	4888	4889	4890	4891	4892	4893	4894	4895	4896	4897	4898	4899	4900
------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------



Hunter

st.



Levels over E.C. Hawk. from NE Barr to 6L Franklin Court.

	0.54	269.00		268.49	NW Hawk & Hunter	4.18	H1	252.27	248.09
TP	0.11	257.36	11.78	257.25	EC	4.24		248.0	
			9.27	248.09	B.M.	4.50		248.6	
NE Barr			8.8	248.6	1			248.7	
+50			10.6	246.8	+215 PC			248.7	
T.P	0.39	245.73	12.02	245.34	Sta 1			248.2	
+100			11.5	244.2	2			247.2	
+50			4.1	241.6	3			246.2	
2			8.3	237.4	4 = EL Alley			245.0	
T.P	0.05	233.97	11.81	233.92	with Alley			244.3	
+50			0.5	233.5	1			243.9	
3			4.8	229.2	2			243.1	
+50			9.0	225.0	3 = P.T.			242.3	
+82 Curb			11.55	222.42	PC			240.3	11.1 241.2
4222			15.1	218.87	T.P. 0.07	240.29		240.22	
					Sta 1			239.0	11.1 239.2
					2			237.7	25 237.8
					3			235.9	39 236.4
					4 = PC			234.4	52 235.1
					1			233.4	66 233.7
					2			232.2	76 232.7
					3			231.5	87 231.6
					4 = EC			230.6	97 230.6
					EC			229.8	106 229.9
					T.P. 182	230.31		228.49	



	N1 230.31		Gutter Side	
PC.	1.6	228.1	2.1	227.9
Stal	2.1	228.2	3.0	227.3
γ	2.7	227.6	3.4	226.9
3	3.2	227.1	4.0	226.3
4 EC = P.EC	3.9	226.4	4.5	225.8
PRC + 10	4.2	226.1	6.1	224.4 Topgrate
+20	4.5	225.8		
+21 Top Cl	4.6	225.7		
#0 " "	4.8	225.3		

	N1 253.77			
EC - 44.1K			9.1	44.7
1-6.81			8.9	44.9
2-13.64			8.5	45.3
3 PC G. 30.4			7.9	45.9
1 10.33			7.0	46.4
2 11.91.6			6.0	47.2
3 11.0			6.0	47.8
PC C = 15.17			5.2	48.6
1 11.95			4.7	49.1
EC 11.48			4.2	49.6
2 12.25			3.2	50.6
+ 15.0 PC			2.1	51.7
1 11.0			1.9	51.9
2 10.4			2.0	51.8
3 5.15			1.9	51.9
4 EC + 6.90			1.9	51.9
T.P 4.94	256.81		1.9	
+ 11.4 Ton 11.96			4.9	51.9
PC 15.17			4.8	52.0
1 11.19			4.6	52.2
2			4.7	52.1
3			5.0	51.8
xw End d.			4.7	51.94
4			4.8	51.83
5			5.07	51.74
6 EC 4.89			5.19	51.62

9.75 4.6 49.2  
 PC 3.0 50.8  
 1 2.7 51.1  
 2 2.1 51.2  
 3 1.5 51.3  
 251.87  
 4 EC 5.4 51.4



	5.31	NT 253.40	248.09
PC		4.0	49.1
U		4.7	48.7
L		5.1	48.3
3		5.2	48.2
EC		5.2	48.2
17 <sup>th</sup> P.U		5.2	48.2
Lot 10		5.7	48.4
		44.2	49.00

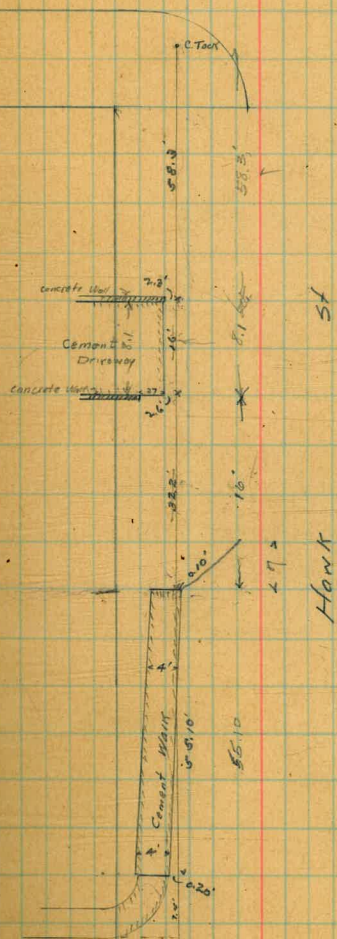


0.66	69.15	262.49	BM. N.W. Hunter.
Top of No. concrete Wall	3.84	265.31	
No. line driveway	6.97	67.18	
So " "	7.17	61.98	
Top So. concrete Wall	8.30	63.85	
N.E. Cor. Sidewalk	8.82	60.83	
N.W. " "	8.75	60.90	
E. Side Sidewalk at PC.	11.90	57.25	
W " " "	11.81	757.34	

Location of Sidewalk on Hawk St. So of Hunter

8 Davis  
16 C Moore  
19 B Moore

Hunter St 50'





270.38 N.E. Redwood Pig ch.

268.90 " Quince "

267.40 " Palm "

70.38

2.33

72.71 M

3.41

69.35

57.75 M

4.10

68.90

73.00 M

69.90

3.68

72.58 M

3.61	2.94	2.72	2.81	2.44	2.6	2.2	4.15	2.78	19.52
69.10	69.87	69.99	69.84	69.77	69.7	69.56	69.43	69.38	3.18
69.35	69.35	69.35	69.35	69.35	69.35	69.35	69.35	69.35	69.35

4.32	6.52	18.53	3.86	4.61	2.67	2.48	6.83	6.71	4.61
68.00	67.22	66.15	66.15	66.15	66.15	66.15	66.15	66.15	66.15

68.09	67.57	67.57	67.57	67.57	67.57	67.57	67.57	67.57	67.57
4.49	4.49	4.49	4.49	4.49	4.49	4.49	4.49	4.49	4.49

69.90	270.38	69.90	69.83	3.61	69.90	69.90	69.90	69.90	69.90
3.68	2.94	3.72	4.37	6.58	4.02	4.02	4.02	4.02	4.02

72.58 M 72.22 M

70.00 62.90

69.17 69.17

69.25

Redwood

69.50 68.82

69.50

69.17 69.17

69.25

69.17 69.17

69.25 68.82

69.20

69.58 69.58

69.09 + 75

69.00

68.75

68.50

68.25

68.00 67.50

68.09

68.35 68.35

68.43 68.51 F TRACK

69.00

Quince

68.00 67.33

68.00

68.35 68.35

67.82

67.67

67.50

67.32

67.17

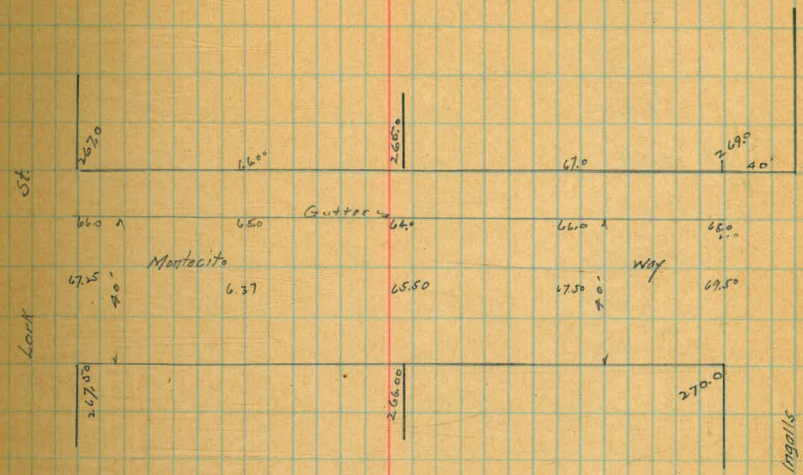
67.00 66.35

67.6

67.10 67.15

Palm





279.00 Cl. S.W. Ingalls  
 1.98  
 271.98 Ht.

6400	6500	6400	6600	6800
598	698	798	698	898
+0.8	+1.0	+2.5	+1.1	+0.7

270.00	Gutter Grades to } Davis										
95	} Camie										
70.95 Ht.	6600	6750	6750	6100	6550	6500	6600	6700	6600	6700	637
	2.95	1.45	2.45	4.95	5.45	5.95	4.95	3.95	4.95	3.70	4.88

270.00  
 96  
 270.96



Levels over  $\phi$  of Alley Block 5 Mission Hills
 $\frac{8}{25}$  Davis  
 $\frac{19}{19}$  Sierra Vista

76.05

	7.38	776.32	2694	2694
EL Sierra K. } S. line on paving		11.52	64.80	
} $\phi$ " "		11.78	64.54	
} No. " "		11.62	64.70	
+04		7.0	69.3	
+25		6.8	69.5	
+50		5.0	71.3	
+88		4.3	72.0	
+88 Garage floor, No side (cliff floor)	3.92		72.40	
1+21	3.4		72.9	
1+21 Concrete Garage floor, N. side	3.23		73.09	
T.P. 519	277.55	3.96	272.36	
1+66	5.2		72.4	
1+66 Concrete Garage floor	4.63		72.92	
2+16	5.6		72.0	
+50	6.0		71.6	
+85	5.4		72.2	
+85 Concrete Garage floor, N. side	5.87		71.68	
3+22.5	5.9		71.9	
3+22.5 Concrete Walk, No side	6.22		71.33	
3+48.5	5.4		72.2	
2+48.5 Concrete Garage floor, No side	5.9		71.7	
4	6.4		71.2	
1+21.5	6.2		71.2	
T.P. 4.90	276.05	6.40	271.15	
1+21.5 Door sill Dwelling, N. line	4.84		71.21	

4+58	4.9	71.2
4+58 Concrete floor Garage on S. line	4.33	71.72
4+67	4.8	71.3
4+67 " " " " "	4.43	71.62
4+75.5	4.8	71.3
	6.2	69.43
5+01.5 S.L. Hormosa } W.L. on Paving	6.8	69.37
	6.28	69.77



Cross-Section of Paring Job. India Y Winder  
to Worthy St & LaBella Ave

84.17

	H.I.		
	7.16	84.17	77.01
S.L. Winder - on Paring			
20' {	W Grate	7.4	76.8
	1/3	6.8	77.4
	2/3	6.35	77.82
	2 W Rail.	6.05	78.12
16' {	2 E "	6.0	78.2
	1/2	6.0	78.2
	E Grate	6.1	78.1

Winder

E. Line	4.0	80.2
" Grate	5.4	78.8
1/2	5.7	78.5
2 E Rail	5.9	78.3
2 W.	6.0	78.2
1/3	6.2	78.0
2/3	6.4	77.8
Grate	6.7	77.5
W.L.	7.7	76.5

W/L Winder

W. Grate	7.7	76.5
1/3	7.2	77.0
2/3	6.6	77.6
2 W R.	6.1	78.1
2 E "	5.9	78.3
1/2	5.7	78.5
E Grate	5.7	78.5

	4.50	
E Grate	5.8	78.4
1/2	5.7	78.5
2 E Rail	5.8	78.4
2 W "	6.2	78.0
1/3	6.5	77.4
2/3	7.3	76.9
W Grate	7.6	76.6
	14.00	
W.G.	7.0	76.6
1/3	7.1	77.1
2/3	6.6	77.6
2 W R	6.3	77.9
2 E "	5.7	78.5
1/2	5.5	78.7
E Grate	5.7	78.5
	14.00	
E "	5.2	79.0
1/2	5.3	78.9
2 E R	5.6	78.6
2 W "	6.0	78.2
1/3	6.5	77.7
2/3	7.0	77.2
W Grate	7.5	76.7



84.17

2900

w guttr	7.3	76.9
$\frac{1}{3}$	6.9	77.3
$\frac{1}{3}$	6.1	77.9
v W Rail	5.9	78.3
v'E'	5.4	78.8
$\frac{1}{2}$	5.3	78.9
E guttr	5.4	78.8

2450

E guttr	5.2	79.0
$\frac{1}{2}$	4.9	79.3
v'E Rail	5.0	79.2
v'W''	5.7	78.5
$\frac{1}{3}$	6.2	78.0
$\frac{1}{3}$	6.7	77.5
w. guttr	7.1	77.1

2100 = St. Pierre

w guttr	6.7	77.5
$\frac{1}{3}$	6.6	77.6
$\frac{1}{3}$	5.8	78.4
v W Rail	5.2	79.0
v'E'	5.0	79.2
$\frac{1}{2}$	4.7	79.5
E guttr	4.8	79.4

84.17

41

E. Pierce

EL	5.3	80.9
guttr	4.9	79.3
E	5.1	79.1
w guttr	6.0	78.2
w.h.	6.5	77.7

No guttr line Pierce

W.h.	7.3	76.9
C	6.0	78.2
EL	3.7	80.5

N.L. Pierce

E guttr	4.4	79.8
C	5.0	78.8
w guttr	6.4	77.8

W.h. India

No guttr	7.4	76.8
$\frac{1}{2}$	6.9	77.3
v' No Rail	6.7	77.5
v' So "	6.5	77.7
$\frac{1}{3}$	7.1	77.1
$\frac{1}{3}$	7.4	76.8
S guttr	6.9	77.3



84.17

Pierca St - 150' West N.L. India

20 guth	10.5	73.7
$\frac{1}{3}$	10.1	74.1
$\frac{2}{3}$	9.9	74.3
2' So Rail	9.7	74.5
2' No "	9.8	74.4
$\frac{1}{2}$	10.1	74.2
No guth	10.1	74.1

7.06

72.73

65.67 194

100' W India

No guth	1.9	70.8
$\frac{1}{2}$	1.7	71.0
2' No Rail	1.6	71.1
2' So "	1.7	71.0
$\frac{1}{2}$	1.8	70.9
$\frac{2}{3}$	1.9	70.8
So guth	2.4	70.3

150 W

So guth	5.6	67.1
$\frac{1}{3}$	5.3	67.5
$\frac{2}{3}$	5.0	67.7
2' So Rail	4.9	67.8
2' No "	4.8	67.9
$\frac{1}{2}$	5.4	67.3
No guth	5.7	67.0

72.73

42

210' W = E L. Arctic No Side

No guth	8.9	63.8
$\frac{1}{2}$	8.6	64.1
2' No	8.4	64.3

200' W = E L. Arctic on So Side

So guth	8.2	64.3
$\frac{1}{3}$	8.0	64.7
$\frac{2}{3}$	7.8	64.9
2' So rail	7.8	64.9

E Arctic

N Line	9.1	63.6
" guth	10.1	62.6
$\frac{1}{2}$	9.5	63.2
2' No Rail	9.2	63.5
2' So "	9.0	63.7
$\frac{1}{3}$	9.3	63.4
$\frac{2}{3}$	9.3	63.4
So guth	9.7	63.0
So line	9.0	63.7

W L. Arctic on So

So guth	11.0	61.7
$\frac{1}{3}$	10.9	61.8
$\frac{2}{3}$	10.8	61.9
2' So Rail	10.3	62.4

W L Arctic on No

2' No rail	9.8	62.9
$\frac{1}{2}$	10.0	62.7
No guth	10.3	62.4



	702	61.19	54.7
		P.C. West Arch. No. 1/2 of St.	
100	No gutter	3.3	57.9
	1/2	3.3	57.9
	2' No Rail	2.9	58.3
	1/2 Curve		
100	2' No "	4.5	56.7
	1/2	5.0	56.2
	No gutter	4.3	56.9
	1/2 Curve		
100	No gutter	4.8	56.4
	1/2	6.1	54.8
	2' No Rail	6.1	55.1
	3/4 Curve 3 rails		
100	No gutter	7.1	54.1
	1/2	7.6	53.6
	2/3	7.5	53.7
	2' No rail	7.2	54.0
	End Curve		
100	2' No rail	8.5	52.7
	1/2	8.6	52.6
	2/3	8.8	52.4
	gutter	7.9	53.3
	1/2 Tan		
100	gutter	9.5	52.7
	1/2	9.2	52.0
	2/3	9.0	52.0
	2' Rail	9.3	51.9

	61.19		
	1/2 Tan		
100	2' Rail	97	51.5
	1/2	97	51.5
	2/3	97	51.5
	gutter	90	52.2
	3/4 Tan		
100	gutter	93	51.9
	1/2	99	51.3
	2/3	99	51.3
	2' Rail	10.1	51.1
	P.C.		
100	2' Rail	10.1	51.1
	1/2	10.0	51.2
	2/3	9.9	51.3
	gutter	9.5	51.7
	1/2 Curve		
100	gutter	9.5	51.9
	1/2	10.1	51.1
	2/3	10.1	51.1
	2' Rail	10.1	51.1
	1/2 Curve		
100	2' Rail	9.9	51.3
	1/2	10.1	51.1
	gutter	9.1	52.1
	3/4 Curve		
100	gutter	8.7	52.5
	1/2	9.6	51.6
	2' Rail	9.6	51.6



6.1.19

End Curve -

15	quatr	89	52.3
	$\frac{1}{2}$	93	51.9
	2' Rail	91	52.1

So Side of St

66.84' Not Arctic = PC - Curve into 10 equal parts 30.81

40	quatr	36	57.6
	$\frac{1}{3}$	33	57.9
	$\frac{2}{3}$	31	58.1
	2' Rail	30	58.2

 $\frac{4}{10}$ 

30.7	quatr	53	55.9
	$\frac{1}{3}$	53	55.9
	$\frac{2}{3}$	47	56.5
	2' Rail	47	56.5

 $\frac{2}{10}$ 

20	quatr	67	54.5
	$\frac{1}{3}$	46	54.6
	$\frac{2}{3}$	62	55.0
	2' Rail	63	54.9

 $\frac{3}{10}$ 

31.2	quatr	79	53.3
	$\frac{1}{3}$	78	53.4
	$\frac{2}{3}$	76	53.6
	2' Rail	77	53.5

6.1.19

44

 $\frac{7}{10}$ 

31.8	quatr	88	52.4
	$\frac{1}{3}$	86	52.6
	$\frac{2}{3}$	86	52.6
	2' Rail	84	52.3

 $\frac{5}{10}$ 

32	quatr	97	51.5
	$\frac{1}{3}$	90	52.2
	$\frac{2}{3}$	94	51.8
	2' Rail	95	51.7

 $\frac{6}{10}$ 

32	quatr	97	51.5
	$\frac{1}{3}$	94	51.8
	$\frac{2}{3}$	98	51.4
	2' Rail	99	51.3

 $\frac{7}{10}$ 

31.2	quatr	104	50.8
	$\frac{1}{3}$	96	51.6
	$\frac{2}{3}$	100	51.2
	2' Rail	101	51.1

 $\frac{8}{10}$ 

30.3	quatr	113	49.9
	$\frac{1}{3}$	98	51.4
	$\frac{2}{3}$	100	51.2
	2' Rail	101	51.1



270

270	qutr	10.4	50.8
	$\frac{1}{3}$	9.8	51.4
	$\frac{2}{3}$	9.8	51.4
	2' Rail	9.6	51.6

End Curve

26.6	qutr	10.3	50.9
	$\frac{1}{3}$	9.8	51.4
	$\frac{2}{3}$	9.6	51.6
	2' Rail	9.1	52.1

9.03

62.44

53.41 Run

End Curve 130' W Side of St. S. Ch. Moore X Sec A see print

Wt	11.6	50.8	
qutr	10.8	51.6	
	$\frac{1}{3}$	10.9	51.5
	$\frac{2}{3}$	10.3	52.1
2' Rail	9.8	52.6	

Sole moore

2' Rail	9.0	53.4
$\frac{1}{3}$	9.5	52.9
$\frac{2}{3}$	10.1	52.3
qutr	10.4	52.0
Wt.	10.6	51.8

E moore

Wt.	9.5	52.9
qutr	9.7	52.7
$\frac{1}{3}$	9.6	52.8
$\frac{2}{3}$	8.7	53.7
2' Rail	8.2	54.2

No 4 moore

2' Rail	73	55.1
$\frac{1}{3}$	81	54.3
$\frac{2}{3}$	89	53.5
qutr	88	53.6
Wt.	86	53.8

No 6 moore

Wt.	75	54.9
qutr	79	54.5
$\frac{1}{3}$	84	54.0
$\frac{2}{3}$	77	54.7
2' Rail	67	55.7

N Line moore

2' Rail	63	56.1
$\frac{1}{3}$	72	55.2
$\frac{2}{3}$	78	54.6
qutr	79	54.5

+50

qutr	71	55.3
$\frac{1}{3}$	72	55.2
$\frac{2}{3}$	64	56.0
2' Rail	57	56.7

+100

2' Rail	49	57.5
$\frac{1}{3}$	57	56.7
$\frac{2}{3}$	64	56.0
qutr	63	55.1



6.44

1449<sup>st</sup> St. Clayton

qutr	55	56.9
$\frac{1}{3}$	55	56.9
$\frac{2}{3}$	46	57.8
2' Rail	38	58.6

## E Clayton

2' Rail	27	59.7
$\frac{1}{3}$	36	58.8
$\frac{2}{3}$	41	58.3
qutr	44	58.0
White	39	58.5

## No. line Clayton

qutr	31	59.3
$\frac{1}{3}$	31	59.3
$\frac{2}{3}$	25	59.9
2' Rail	18	60.6

## 1328 = 100' S of Mc Kee

2' Rail	0.8	61.6
$\frac{1}{3}$	1.5	60.9
$\frac{2}{3}$	2.1	60.3
qutr	2.5	59.9

67.44

46

## E side of St. 150' S of McKee - 30' N of CC

qutr	95	52.9
$\frac{1}{3}$	96	52.8
2' Rail	92	52.8

## 100' S McKee

2' Rail	85	53.9
$\frac{1}{3}$	86	54.0
qutr	87	53.7

## 50' S McKee

qutr	72	55.2
$\frac{1}{3}$	72	55.2
2' Rail	72	55.2

## St. McKee

2' Rail	61	56.3
$\frac{1}{3}$	62	56.2
qutr	66	55.8

## E McKee

Ch.	52	57.2
qutr	58	56.6
$\frac{1}{3}$	57	56.7
2' Rail	57	56.7

## N. of McKee

2' Rail	53	57.1
$\frac{1}{3}$	53	57.1
qutr	55	56.9



6244

60' No marker = 200' S. McNeely

quatr	41	58.3
1/2	40	58.4
2' Rail	42	58.4

200' S.

2' Rail	32	59.2
1/2	30	59.4
quatr	30	59.4

100' S.

quatr	23	60.1
1/2	20	60.4
2' Rail	20	60.4

100' S.

2' Rail	10	61.4
1/2	11	61.3
quatr	14.1	61.4

9.81

70.29

60.48 ran

50' S. McNeely

quatr	7.9	62.4
1/2	7.9	62.4
2' Rail	7.6	62.7

7079

47

W Side of St. or 50' McNeely St.

quatr	81	61.9
1/3	80	61.7
2/3	81	62.2
2' Rail	77	62.6

50' S. McNeely

W quatr	70	63.3
1/3	73	63.0
2/3	69	63.4
2' W Rail	65	63.8
2' E "	64	63.7
1/2	68	63.5
E quatr	69	63.4

♀

E quatr	62	64.2
1/2	61	64.3
2' E Rail	60	64.4
2' W "	59	64.5
1/3	63	64.1
2/3	68	63.5
W quatr	64	63.9

N.L. McNeely

W quatr	65	64.8
1/3	66	63.7
2/3	60	64.3
2' W Rail	55	64.8
2' E "	56	64.7
1/2	58	64.6
quatr	50	64.7



70.29

on dividing Ang at Cal &amp; La Jolla Ave

I3	w/qrtr 1/3	59	64.1
		61	64.2
		55	64.8
	2' Rail	52	65.1
	2' E Rail	52	65.1
22	1/2	51	65.2
		57	65.2

X Sect. Taken from 67' So of Station W to End old Ct on E  
82.45 So Sutherland to 79 gns. mutually

23	w/qrtr 1/3	57	64.6
		59	64.1
		54	64.9
	2' Rail	51	65.2
	2' Rail	51	65.2
29	1/3	52	65.1
		49	65.4
	qrtr	45	65.8

So Line Sutherland St.

17	E L. Lafferman	42	66.1
		46	65.7
10	qrtr 1/2	48	65.5
		46	65.7
	2' W Rail	46	65.7
14	1/3	50	65.3
		53	65.0
		46	65.7

70.29

to Sutherland

w/	41	66.2
qrtr	45	65.8
1/3	47	65.6
2/3	44	65.9
2' W Rail	43	66.0
804	75.69	67.65

No Line Sutherland

E qrtr	89	66.8
1/2	89	66.8
2' E Rail	89	66.8
2' W "	88	66.9
1/2	90	66.7
	2/3	92
qrtr	90	66.7

200 So. Hill

w/qrtr	82	67.5
1/3	82	67.5
2/3	81	67.6
2' W Rail	79	67.8
2' E "	79	67.8
2'	81	67.6
qrtr	82	67.4

200 So. Hill

E qrtr	74	68.3
1/2	71	68.6
2' E Rail	71	68.6
2' W "	70	68.7
1/3	71	68.6
2/3	73	68.2
qrtr	76	68.1

48



75.69

150 So Noell

w quito	71	68.6
$\frac{1}{3}$	65	69.2
$\frac{2}{3}$	62	69.5
v'w Rail	61	69.6
v' E "	62	69.5
$\frac{1}{2}$	63	69.4
Equito	66	69.1

100 So

Equito	56	70.1
$\frac{1}{2}$	56	70.1
v' E Rail	54	70.3
2' W "	53	70.4
$\frac{1}{3}$	53	70.4
$\frac{2}{3}$	57	70.0
quito	62	69.5

50 So

quito	45	70.2
$\frac{1}{3}$	48	70.9
$\frac{2}{3}$	45	71.2
v'w Rail	44	71.3
v' E "	45	71.2
$\frac{1}{2}$	46	71.1
quito	49	70.8

75.69

49

S. Lin Noell

Equito	36	72.1
$\frac{1}{2}$	39	71.8
v' E Rail	36	72.1
v' W "	35	72.2
$\frac{1}{3}$	37	72.0
$\frac{2}{3}$	40	71.7
quito	48	70.9

E

Equito	43	71.4
quito	40	71.7
$\frac{1}{3}$	33	72.4
$\frac{2}{3}$	30	72.7
v'w Rail	29	72.8
v' E "	30	72.7
$\frac{1}{2}$	32	72.5
Equito	29	72.8

Noell Noell

Equito	22	73.5
$\frac{1}{2}$	26	73.1
v' E Rail	25	73.2
v' W "	26	73.3
$\frac{1}{3}$	26	73.1
$\frac{2}{3}$	28	72.9
quito	35	72.2



5.39 8005  
50' No Noed

Wguts	75	74.61
$\frac{1}{3}$	69	72.6
$\frac{2}{3}$	66	73.7
2' W Rail	64	73.5
2' E "	62	73.7
$\frac{1}{3}$	62	73.9
$\frac{2}{3}$	63	73.8
Wguts	65	73.6

100' No Noed

E Wguts	61	74.1
$\frac{1}{3}$	61	74.1
2' E Rail	58	74.3
2' W "	58	74.3
$\frac{1}{3}$	61	74.0
$\frac{2}{3}$	63	73.8
Wguts	71	73.0

150' No

Wguts	66	73.5
$\frac{1}{3}$	59	74.2
$\frac{2}{3}$	56	74.5
2' W Rail	54	74.7
2' E "	53	74.8
$\frac{1}{3}$	55	74.6
Wguts	57	74.4

8005

50

200' No

Wguts	51	75.0
$\frac{1}{3}$	50	75.1
2' E Rail	48	75.3
2' W "	49	75.2
$\frac{1}{3}$	52	74.9
$\frac{2}{3}$	55	74.6
Wguts	61	74.0

250' No

Wguts	56	74.5
$\frac{1}{3}$	51	75.0
$\frac{2}{3}$	47	75.4
2' W Rail	44	75.7
2' E "	43	75.8
$\frac{1}{3}$	45	75.6
Wguts	46	75.5

300' No - St. Estudios

Wguts	39	76.2
$\frac{1}{3}$	40	76.1
2' E Rail	39	76.2
2' W "	40	76.1
$\frac{1}{3}$	43	75.8
$\frac{2}{3}$	46	75.5
Wguts	48	75.3



	83.98	77.38 124
6.60		
♀ Estuero		
w L	83	75.7
queto	81	75.9
$\frac{1}{3}$	83	75.7
$\frac{2}{3}$	78	76.2
v'w Rail	74	76.6
v' E "	73	76.7
$\frac{1}{2}$	74	76.6
E queto	74	76.6
N.L. Estuero		
E queto	65	77.5
$\frac{1}{2}$	68	77.2
v' E Rail	69	77.1
v' w "	70	77.0
$\frac{1}{3}$	74	76.6
$\frac{2}{3}$	77	76.3
w queto	75	76.5
50' No. 200 S. Weight		
w queto	72	76.8
$\frac{1}{3}$	70	77.0
$\frac{2}{3}$	68	77.2
v' w Rail	63	77.7
v' E "	62	77.8
$\frac{1}{2}$	62	77.8
E queto	58	78.2

	200 S. Weight	
E queto	58	78.2
$\frac{1}{2}$	59	78.1
v' E Rail	58	78.2
v' w "	58	78.2
$\frac{1}{3}$	62	77.8
$\frac{2}{3}$	65	77.5
w queto	72	76.8
	100 S.	
w queto	65	77.5
$\frac{1}{3}$	60	78.0
$\frac{2}{3}$	56	78.4
v' w Rail	53	78.7
v' E "	53	78.7
$\frac{1}{2}$	54	78.6
E queto	51	78.9
	100 S.	
E queto	42	79.4
$\frac{1}{2}$	51	78.9
v' E Rail	49	79.1
v' w "	48	79.2
$\frac{1}{3}$	51	78.9
$\frac{2}{3}$	56	78.5
w queto	60	78.0



8398

50' S. Wright

wguts	56	78.4
$\frac{1}{3}$	4.7	79.3
$\frac{2}{3}$	4.5	79.5
v'w Rail	4.3	79.7
v'c "	4.2	79.8
$\frac{1}{2}$	4.3	79.7
Equitr	4.1	79.9

S. L. Wright

Equitr	3.5	80.5
$\frac{1}{2}$	4.0	80.0
v'c Rail	3.8	80.2
v'w Rail	3.9	80.2
$\frac{2}{3}$	4.1	79.9
$\frac{1}{3}$	4.6	79.4
wguts	50	79.0

L. Wright

w'white	4.5	79.5
wguts	4.8	79.7
$\frac{1}{3}$	3.9	80.1
$\frac{2}{3}$	3.6	80.4
v'w Rail	3.4	80.6
v'c "	3.5	80.7
$\frac{1}{2}$	3.4	80.6
Equitr	3.2	80.8

8398

52

Nobin Wright

Equitr	2.8	81.2
$\frac{1}{2}$	3.0	81.0
v'c Rail	2.8	81.2
v'w "	2.9	81.1
$\frac{1}{3}$	3.3	80.7
$\frac{2}{3}$	3.5	80.5
wguts	4.2	79.8
6.10	88.69	82.59

50' No Wright

wguts	8.5	80.6
$\frac{1}{3}$	7.7	81.0
$\frac{2}{3}$	7.4	81.3
v'w Rail	7.0	81.7
v'c "	7.0	81.7
$\frac{1}{2}$	7.1	81.6
Equitr	7.2	81.5

100' No

Equitr	6.0	82.3
$\frac{1}{2}$	6.6	82.1
v'c Rail	6.0	82.3
v'w "	6.5	82.2
$\frac{1}{3}$	6.8	81.9
$\frac{2}{3}$	7.2	81.5
wguts	7.9	80.8



88.69

150' No Wright

Wgutr	73	81.4
$\frac{1}{3}$	68	81.9
$\frac{2}{3}$	63	82.4
2' W Rail	60	82.7
2' E'	59	82.8
$\frac{1}{2}$	58	82.9
Egutr	59	82.8
200' No		
Egutr	56	83.3
$\frac{1}{2}$	54	83.3
2' E Rail	53	83.4
2' W "	54	83.3
$\frac{1}{3}$	58	82.9
$\frac{2}{3}$	61	82.6
Wgutr	61	82.1
250' No		
Wgutr	63	82.4
$\frac{1}{3}$	60	82.7
$\frac{2}{3}$	56	83.3
2' W Rail	50	83.7
2' E'	49	83.8
$\frac{1}{2}$	50	83.7
Egutr	50	83.7

88.69

53

300' No Sh Bandini

Egutr	44	84.3
$\frac{1}{2}$	44	84.3
2' E Rail	44	84.3
2' W "	45	84.2
$\frac{1}{3}$	42	84.1
$\frac{2}{3}$	51	83.6
Wgutr	57	83.0
4 Bandini		
W Line	53	83.4
Wgutr	52	83.5
$\frac{1}{3}$	46	84.1
$\frac{2}{3}$	41	84.6
2' W Rail	40	84.7
2' E Rail	40	84.7
$\frac{1}{2}$	43	84.4
Egutr	39	84.8
No Line Bandini		
Egutr	35	85.2
$\frac{1}{2}$	36	85.1
2' E Rail	34	85.3
2' W "	34	85.3
$\frac{1}{3}$	31	85.1
$\frac{2}{3}$	41	84.6
Wgutr	43	84.4



88.69

50' No. 120' = 250' S. Conto

W qutr	39	84.8
$\frac{1}{3}$	33	85.4
$\frac{2}{3}$	30	85.7
v. E Rail	29	85.8
v. E "	29	85.8
$\frac{1}{2}$	31	85.6
E qutr	32	85.5

220' S. Conto

E qutr	29	85.8
$\frac{1}{2}$	30	85.7
v. E Rail	29	85.8
v. W "	29	85.8
$\frac{1}{3}$	30	85.7
$\frac{2}{3}$	33	85.4
W qutr	40	84.7

200' S.

W qutr	41	84.6
$\frac{1}{3}$	35	85.2
$\frac{2}{3}$	32	85.5
v. W Rail	30	85.7
v. E "	30	85.7
$\frac{1}{2}$	31	85.6
E qutr	31	85.6

88.69

180' S.

E qutr	37	85.0
$\frac{1}{2}$	35	85.2
v. E Rail	32	85.5
v. W "	32	85.5
$\frac{1}{3}$	34	85.3
$\frac{2}{3}$	37	85.0
W qutr	42	84.5

160' S.

W qutr	48	83.9
$\frac{1}{3}$	41	84.6
$\frac{2}{3}$	38	84.9
v. W Rail	36	85.1
v. E "	36	85.1
$\frac{1}{2}$	37	85.0
E qutr	40	84.7

120' S.

E qutr	52	83.5
$\frac{1}{2}$	47	84.0
v. E Rail	46	84.1
v. W "	46	84.1
$\frac{1}{3}$	47	84.0
$\frac{2}{3}$	50	83.7
W qutr	56	83.1

54



8869

80' So. of Courts

Wgutr	7.0	81.7
$\frac{1}{3}$	6.2	82.5
$\frac{2}{3}$	6.0	82.7
v'W Rail	5.8	82.9
v'E "	5.7	82.8
$\frac{1}{2}$	6.1	82.6
Egutr	6.1	82.6
40' So		
Egutr	7.2	81.5
$\frac{1}{2}$	7.1	81.6
v'E Rail	6.9	81.8
v'W "	6.8	81.9
$\frac{1}{2}$	7.2	81.5
$\frac{2}{3}$	7.4	81.3
Wgutr	8.2	80.5
T.P	0-30	80.4

So. line Courts

Wgutr	1.5	79.4
$\frac{1}{3}$	0.7	80.2
$\frac{2}{3}$	0.3	80.6
v'W Rail	0.1	80.8
v'E "	0.2	80.7
$\frac{1}{2}$	0.3	80.6
Egutr	0.1	80.8

8096

55

So. Courts

Egutr	1.1	79.8
$\frac{1}{2}$	1.2	79.7
v'E Rail	1.0	79.9
v'W "	0.9	80.0
$\frac{1}{3}$	1.2	79.7
$\frac{2}{3}$	1.5	79.4
Wgutr	2.7	78.2
W line	2.4	78.5
No line Courts		
Wgutr	3.7	77.2
$\frac{1}{3}$	2.8	78.1
$\frac{2}{3}$	2.3	78.6
v'W Rail	1.7	79.2
v'E "	1.8	79.1
$\frac{1}{2}$	2.0	78.9
Egutr	2.2	78.7

50' No Courts

Egutr	3.9	77.0
$\frac{1}{2}$	3.8	77.1
v'E Rail	3.6	77.3
v'W "	3.6	77.3
$\frac{1}{3}$	4.1	76.8
$\frac{2}{3}$	4.7	76.2
Wgutr	5.2	75.7



80.94

100 No Counts

wgutr	6.8	74.1
$\frac{1}{3}$	6.1	74.8
$\frac{2}{3}$	5.7	75.2
2' w Rail	5.2	75.7
2' E "	5.2	75.7
$\frac{1}{2}$	5.4	75.5
Egutr	5.4	75.5

150 No

Egutr	7.4	73.5
$\frac{1}{2}$	7.0	73.9
2' E Rail	7.0	73.9
2' w "	7.1	73.8
$\frac{1}{3}$	7.5	73.4
$\frac{2}{3}$	8.0	72.9
wgutr	8.7	72.2

200 No

wgutr	10.2	70.7
$\frac{1}{3}$	9.7	71.2
$\frac{2}{3}$	9.3	71.6
2' w Rail	8.9	72.0
2' E "	8.7	72.2
$\frac{1}{2}$	8.8	72.1
Egutr	9.0	71.9

80.94

250 No

Egutr	11.0	69.9
$\frac{1}{3}$	10.7	70.2
2' E Rail	10.7	70.2
2' w "	10.8	70.1
$\frac{1}{3}$	10.6	70.3
$\frac{2}{3}$	11.3	69.6
wgutr	12.0	68.9
T.P. 4th	74.46	107.2

270.4 1/16 = P.C. in Curt on E side

wgutr	5.7	68.8
$\frac{1}{3}$	5.4	69.1
$\frac{2}{3}$	4.6	69.9
2' w Rail	4.7	69.8
2' E Rail	4.6	69.9
Egutr	4.7	69.8

So line withdrawn.

Egutr	4.9	69.6
2' E Rail	5.0	69.5
2' w "	4.9	69.6
$\frac{1}{3}$	4.9	69.6
$\frac{2}{3}$	6.2	68.3
wgutr	6.5	68.0

56

41.5



7446

	Wetherby		
31	Eqtr	61	68.4
	$\frac{1}{3}$	60	68.5
	$\frac{2}{3}$	54	69.1
11	2' W Rail	52	69.3
	2' E Rail	52	69.3
	$\frac{1}{2}$	52	69.3
	Eqtr	5.1	69.4
	N. L. Wetherby		
108	Eqtr	56	68.9
	$\frac{1}{2}$	53	69.2
	2' E Rail	53	69.2
213	2' W.	52	69.3
	$\frac{1}{3}$	58	68.7
	$\frac{2}{3}$	60	68.5
	4 eqtr	6.5	68.0
	1344 N.E. Wetherby	39.6	70.50 / 70.49

S. curb Winder

	5.00	77.01
E		2.6
Eqtr		3.1
$\frac{1}{2}$		3.5
2' E Rail		3.7
2' W of Curve		4.0
$\frac{1}{2}$		4.5
Eqtr		5.3
W		6.0
N. Curb Winder		
W		5.6
Eqtr		5.3
$\frac{1}{2}$		4.7
$\frac{2}{3}$		4.3
2' Rail		3.9
2' E		3.8
$\frac{1}{2}$		3.4
Eqtr		3.1
E		2.1

S. Curb Pierce

	21.5	82.27	80.12
E			1.5
Eqtr			4.5
$\frac{1}{3}$			2.9
$\frac{2}{3}$			3.1
2' E of rail on Curve			3.5
2' W			3.9



191	82.27	
Wgtt	4.9	
W.L.	5.1	
E Cb India		
S.L.	2.9	
S qutr	2.5	
3/4	2.7	
C	2.9	
N 1/4	2.8	
N qutr	2.7	
N.L.	2.4	
W Cb India		
N.L.	4.4	
N qutr	4.9	
1/2	4.3	
2/3	4.1	
N 2' line excurve	4.1	
2' 30' ex rail	4.3	
3 qutr	4.5	
S	4.9	
	5.2	
2.73	68.40	65.67
E Cb Arctic on So.		
S	3.5	
S qutr	4.4	
1/3	4.0	
2/3	3.9	
2' 3' rail	3.5	

E Cb Arctic on N.		
2' N of rail	4.0	
1/2	4.2	
N qutr	4.8	
N	4.0	
W Cb Arctic on S		
N	5.4	
N qutr	<del>5.7</del> 6.3	
1/2	5.6	
N 2' L	5.0	
S 2' L	5.3	
1/3	5.8	
2/3	5.9	
S qutr	6.4	
S	5.7	
S Cb Mc Kee		
5.55	66.03	60.48
E	8.9	
E qutr	10.0	
1/2	9.7	
2' E rail	9.6	
N Cb Mc Kee		
2' E rail	9.1	56.9
1/2	9.0	
E qutr	9.3	
E	8.6	



66.03

## S. Cb. Clayton

2' W of rail	6.9
1/3	7.9
2/3	8.4
W qutr	9.2
W. L.	8.6

## N. Cb Clayton

W. L.	6.5
W qutr	7.6
1/3	6.7
2/3	6.4
2' W. of rail	5.7

## S. Cb. Sutherland

4.85

74.50

67.65

E qutr.	6.5
1/2	6.8
2' E rail	6.7
2' W rail	6.6
1/3	7.0
2/3	7.3
5' E of W qutr	7.6
W qutr	6.7
W. L.	6.6

## N. Cb Sutherland

W. L.	6.2
W qutr	6.2
+3	6.9

72.5

1/3	6.2
2/3	6.1
2' W. rail	5.9
2' E "	6.0
1/2	6.1
E qutr	6.2

## S. Cb NOELL

74.66

E qutr	6.1
3' W	6.9
1/2	6.6
2' E of Rail	6.4
2' W - -	6.3
1/3	6.4
2/3	6.7
W qutr	7.7
W. L.	7.8

## N. Cb NOELL

W. L.	7.0
W qutr	6.9
1/3	6.1
2/3	5.8
2' W	5.7
2' E	5.7
1/2	5.8
W. L. E qutr	5.8
E qutr	5.0



78.66  
S.Cb. Estudillo

Egutr	1.7
3' W of ✓	2.7
1/2	2.5
2' E rail	2.4
2' W ✓	2.5
1/3	2.7
2/3	2.9
5' E of W gutr	3.6
W gutr	3.1
W.L.	3.6

N.Cb. Estudillo

WL	2.8
W gutr	2.4
4' E of ✓	3.1
1/3	2.4
2/3	2.2
2' W rail	1.8
1/2 E ✓	1.7
1/2	1.7
4' W of Egutr	1.9
✓ ✓	0.9

82.74  
S.Cb. Wright

Egutr	2.1
3' W	2.6
1/2	2.6
2' E rail	2.4
2' W ✓	2.4
1/3	2.7
2/3	2.9
W gutr	4.0
WL	3.7

N.Cb. Wright

WL	2.9
W gutr	3.3
1/3	2.5
2/3	2.7
2' W rail	1.8
2' E ✓	1.8
1/2	1.9
Egutr	2.0



11/1/20

Gregory  
Miller  
Shaw.Levels on Hawk St S.  
of Hunter

	2.05	270.54	268.49	NW Hawk & Hunter BR
SE curb H+H.			268.01	no cement
10' S. of Hunter Ecb Hawk			266.7	
25' " " " " " "			68.4	
39' " " " " " " = center garage			63.9	
Floor of garage.			64.2	
50' " " " " " " E. cb Hawk			64.1	
75' " " " " " " " "			59.9	
91.5' " " " " " " " "			55.7	
111.5'			151.5	
proper line 111.5 S:			69.2	
19' S. of Hunter W.L. Hawk			68.9	
" " " " " " Wcbh			66.9	
44' " " " " " " " "			63.6	
50' " " " " " " " "			62.2	
75' " " " " " " " "			60.4	

61



Moore  
Bill  
shaw

Curb Elev. on Hawk St  
N.L. Bush N. to SL of Arnold + Choates Add

62

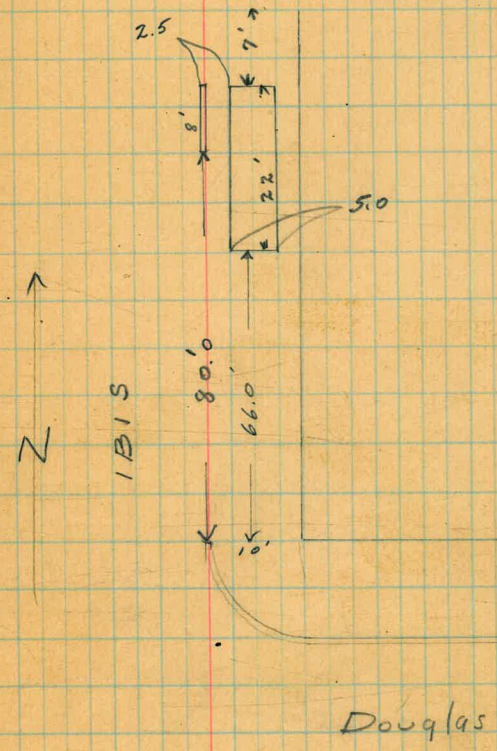
	8.59	27042	261.83	NW Hawk + Bush
NE Hawk + Bush = 0+00 EL				
0 + 38		8.97	261.45	
+ 58		7.34	263.08	
+ 70		6.77	263.65	
+ 90		6.35	264.07	
1 -		5.96	264.46	
+ 30		5.77	264.65	
+ 41		5.43	264.99	
+ 72		5.28	265.14	
+ 85 PC		5.08	265.34	
2 + 04 <sup>2</sup> CC		5.02	265.40	
+ 23 EC		5.0	265.42	
3 + 13 St. Arnold + Choates		4.96	265.46	
NW Hawk + Bush = 0+00 W.L.		5.32	265.10	
+ 38		8.57	261.85	
+ 58		6.87	263.55	
+ 70		6.25	264.17	
+ 90		5.87	264.55	
1 -		5.62	264.80	
+ 32		5.46	264.96	
+ 84		5.08	265.34	
S. return w/ Hawk		4.90	265.52	
2 + 23		4.62	265.80	
N. return w/ Hawk		4.99	265.43	
+ 54		4.72	265.70	
3 + 13		4.96	265.46	
		5.47	264.95	



MOORE 10/18/20 St Arnold + Charts To 95' N of Nk of Douglas  
Elevs shown

	7.01	269.01	262.0	SE. 1/4 S. 1/4 Douglas
SE Return Douglas + Ibis	7.01			
+50 S. of Douglas El Ibis	0.65	268.36		
Nk Ibis Court <sup>0000</sup> Wk	0.43	268.58		
+75 = St Douglas - Wk Ibis	7.55	261.26		
+20	8.10	260.91		
+25 Nk Douglas Wk Ibis	8.18	260.83		
+30	8.45	260.56		
+83	12.44	256.59		
NE Return Douglas + Ibis = 000	7.02	261.99		
+66	11.88	257.13	outside edge of walk	
+88	13.45	255.56	" " "	

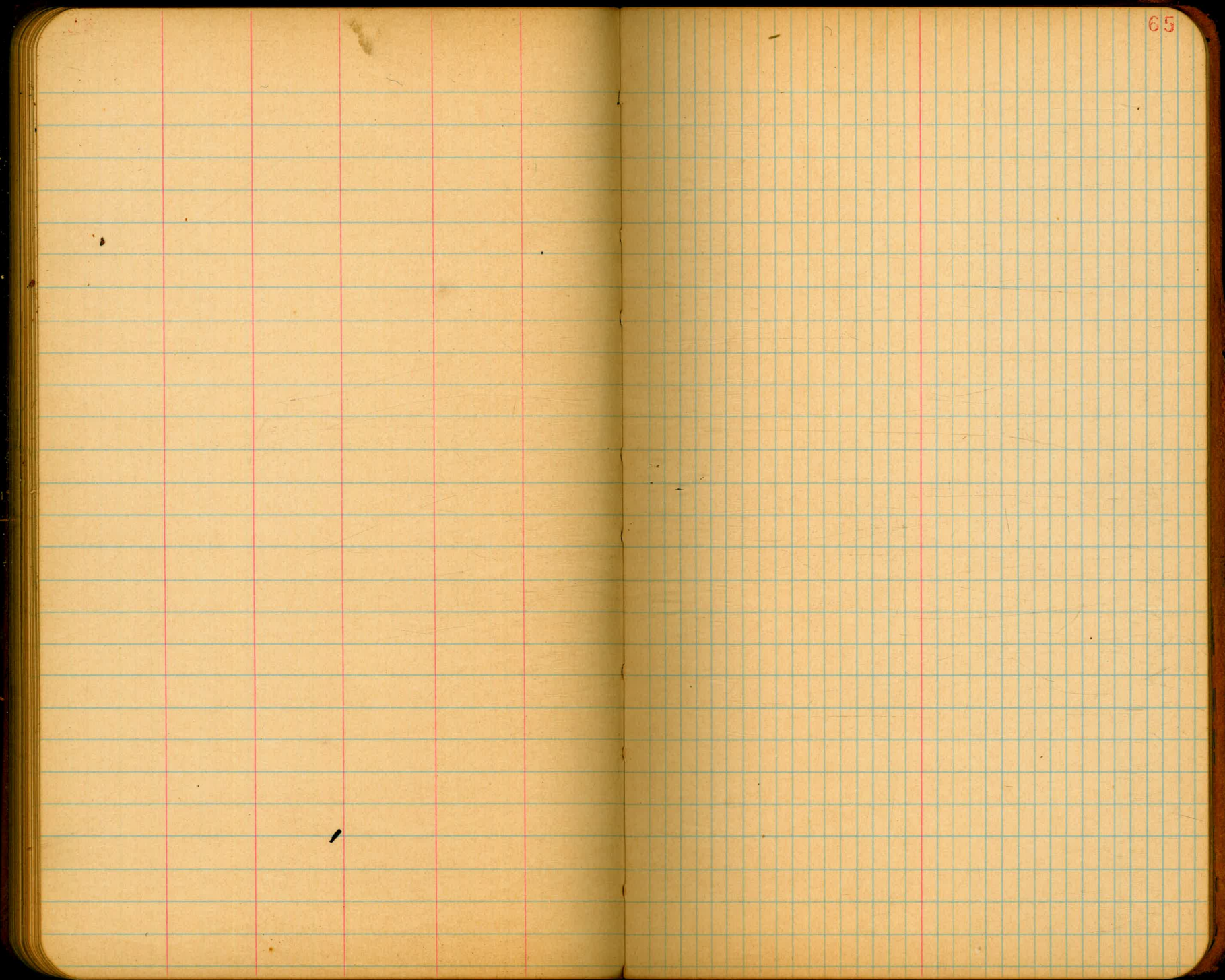
Note: E side of Ibis sidewalk is 5' wide in center  
 W " " " " " " " 3' from curb to outside edge of walk



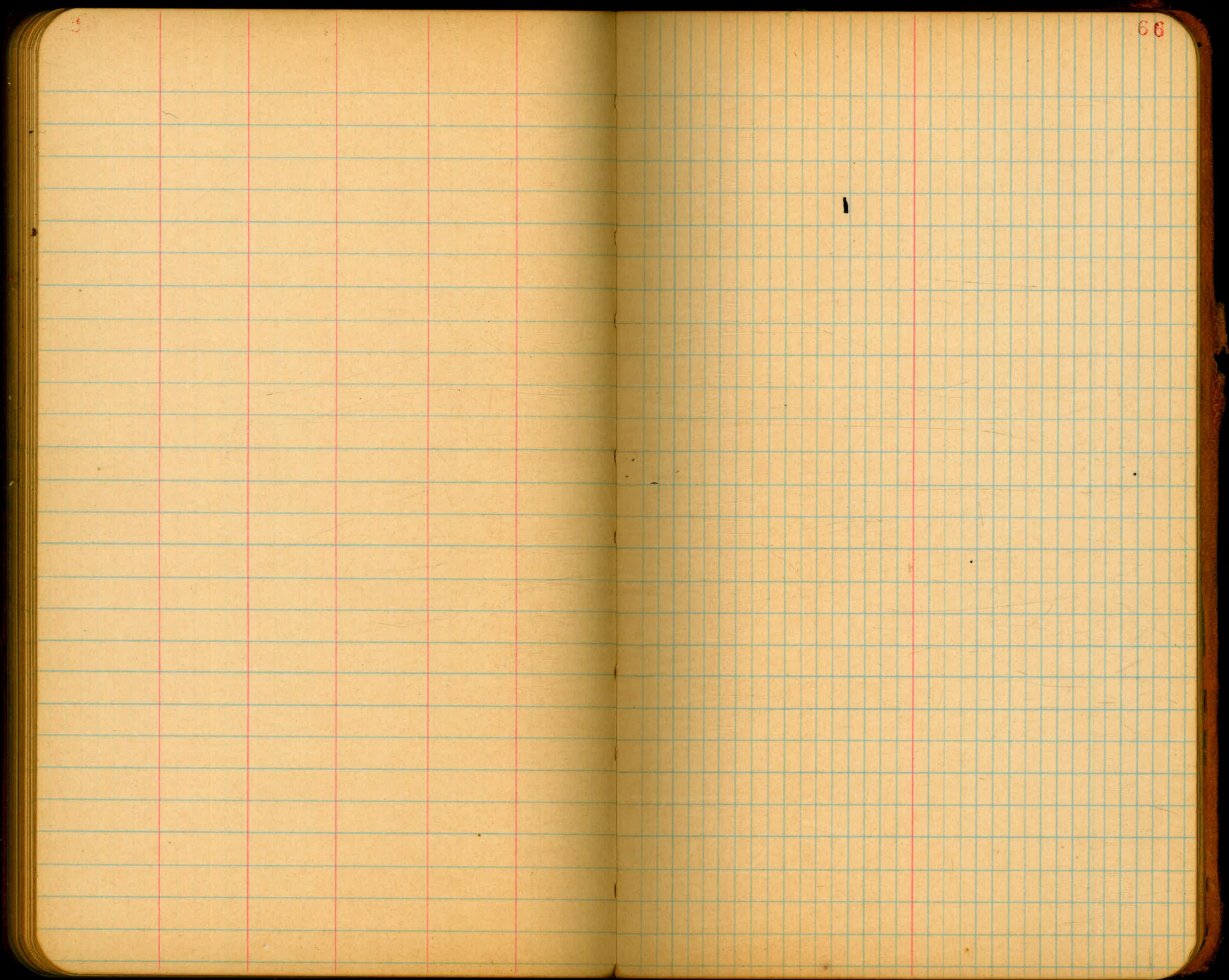








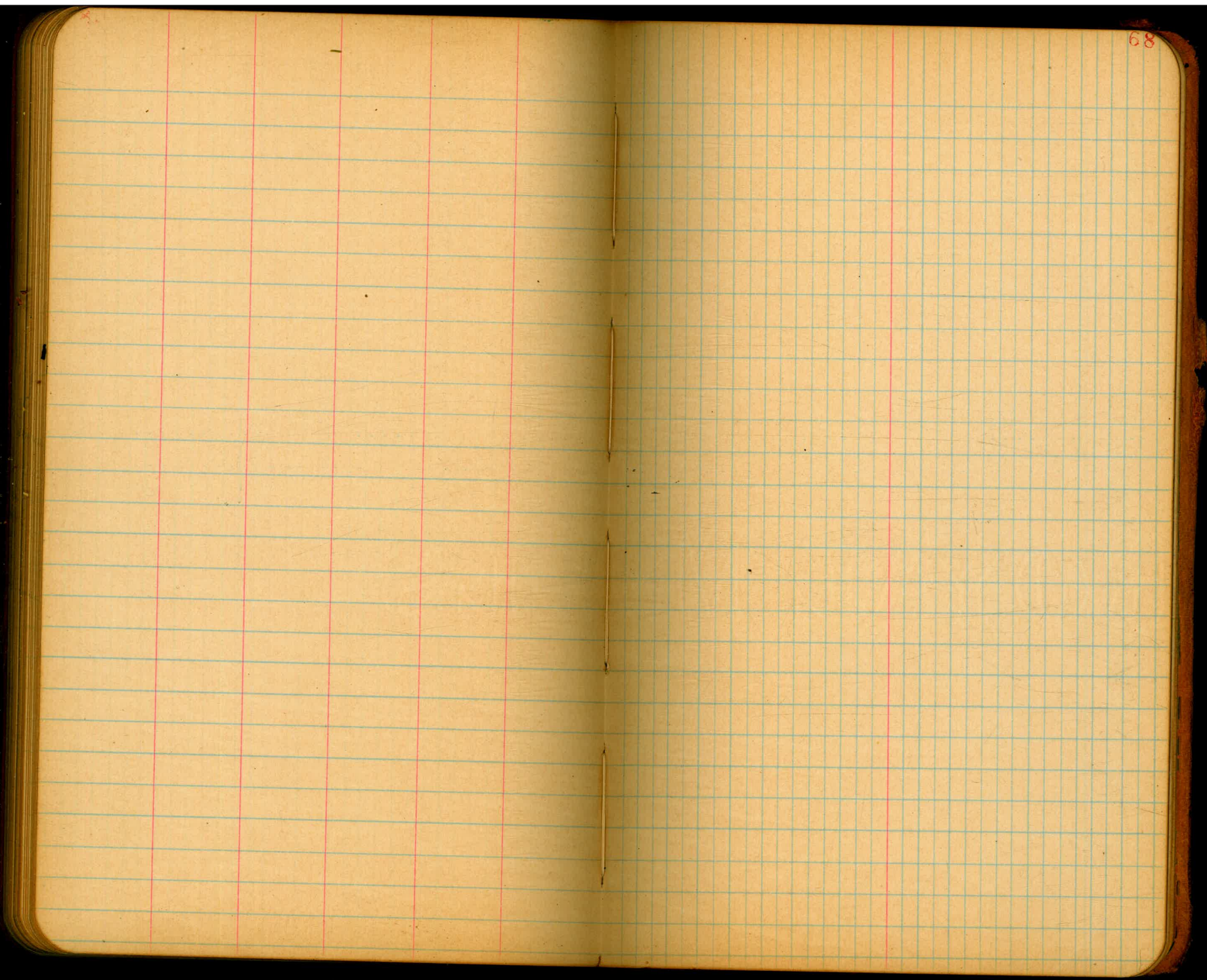
















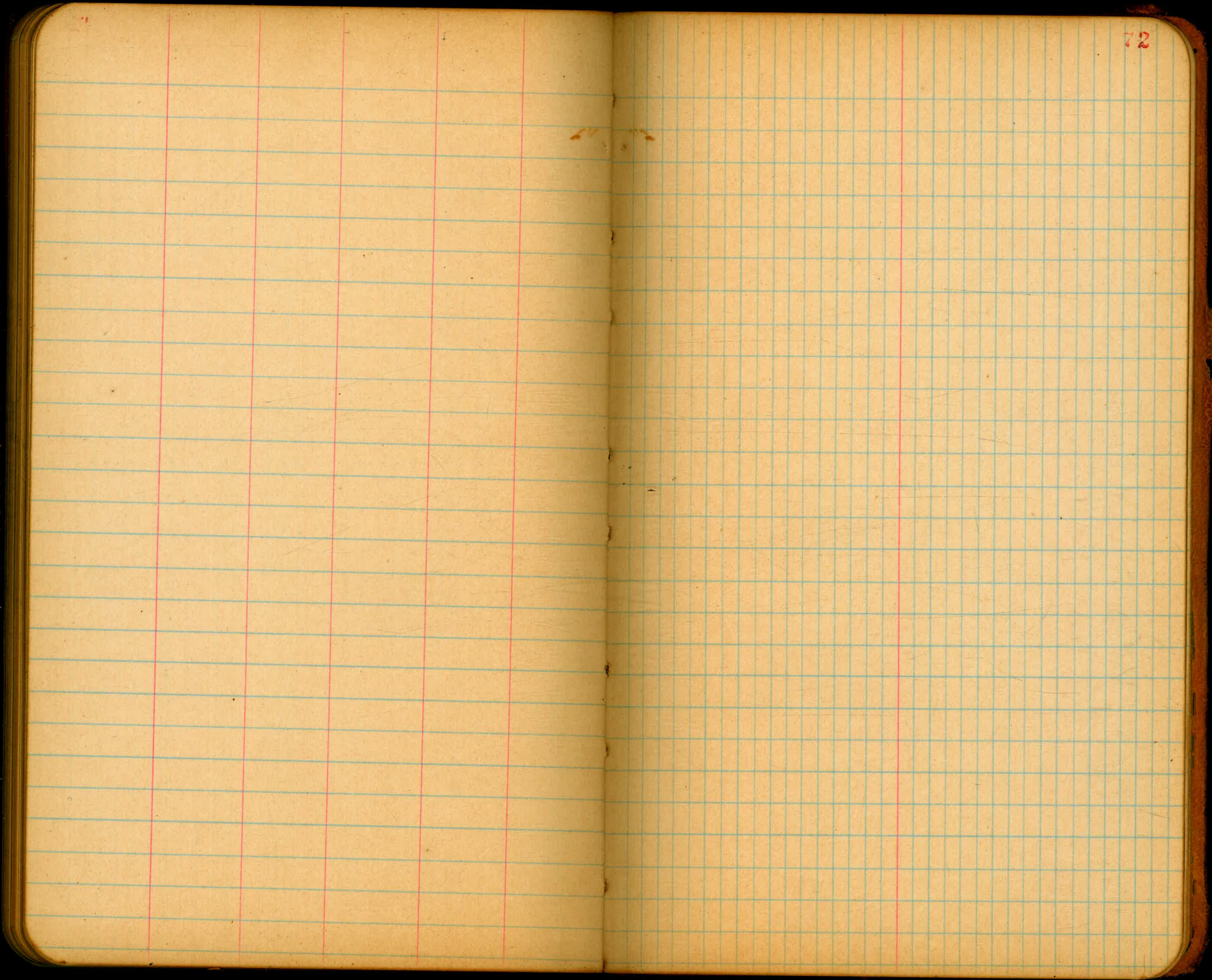






















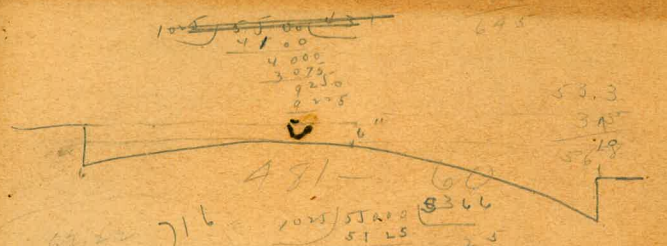








#1400 Lots 1 & 2 3/15



175  
26  
1/2

$$\begin{array}{r} 312 \\ 117 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 57 \\ 37 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 17 \\ 3 \\ \hline 2 \end{array}$$

$$\begin{array}{r} 5366 \\ 2683 \\ \hline 2683 \\ 100 \\ \hline 4683 \\ 100 \\ \hline 4783 \end{array}$$

$$\begin{array}{r} 322.33 \\ 39. \\ \hline 283.33 \end{array}$$

$$\begin{array}{r} 35 \\ 358 \\ \hline 393 \end{array}$$

$$\begin{array}{r} 3255 \\ 1302 \\ \hline 4557 \end{array}$$

$$\begin{array}{r} 1627 \\ 50 \\ \hline 1677 \end{array}$$

$$\begin{array}{r} .0651 \\ 51 \\ \hline 51 \end{array}$$

$$\begin{array}{r} .0651 \\ 6083 \\ 100 \\ \hline 6226 \end{array}$$

$$\begin{array}{r} 60 = 23 \\ 100' = 20'' \\ 309 \\ 10555 \\ 2925 \\ \hline 113 \end{array}$$

$$\begin{array}{r} 73 \\ 20 \\ \hline 113 \end{array}$$

$$\begin{array}{r} 7+8167 \\ 1185 \\ \hline 7+7002 \\ 3934 \end{array}$$

$$\begin{array}{r} 13350 \\ 21571 \\ \hline 34921 \end{array}$$

$$\begin{array}{r} 8050 \\ 3050 \\ \hline 4000 \end{array}$$

$$\begin{array}{r} 2854 \\ 406 \end{array}$$

$$\begin{array}{r} 20800 \\ 239 \\ \hline 21039 \end{array}$$

$$\begin{array}{r} 23626 \\ 197 \\ \hline 23823 \end{array}$$

$$\begin{array}{r} 14367 \\ 71 \\ \hline 14438 \end{array}$$

$$\begin{array}{r} 71.50 \\ 1 \\ \hline 72.50 \end{array}$$

$$\begin{array}{r} 2230 \\ 252 \\ \hline 2482 \end{array}$$

$$\begin{array}{r} 5022 \\ 3942 \\ \hline 8964 \end{array}$$

$$\begin{array}{r} 34904 \\ 34246 \\ \hline 69150 \end{array}$$

$$\begin{array}{r} 40788 \\ 3201 \\ \hline 43989 \end{array}$$

$$\begin{array}{r} 23996 \\ 23 \\ \hline 24019 \end{array}$$

