

872

872  
F.B.

---

LEVEL BOOK.

No. 410 T

---



1995  
19405  
10 4 3  
151  
242  
1215  
142  
36692  
19428  
19505

EUGENE DIETZGEN CO.,  
Drawing Materials and Surveying Instruments.  
NEW YORK. CHICAGO. SAN FRANCISCO.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.  
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
ROADWAY 20 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

Copyright, 1902. No. 39340.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	0
1	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	1
2	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	2
3	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	3
4	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	4
5	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	5
6	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	6
7	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	7
8	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	8
9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	9
10	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	10
11	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	11
12	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	12
13	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	13
14	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	14
15	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	15
16	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	16
17	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	17
18	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	18
19	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	19
20	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	20
21	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	21
22	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	22
23	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	23
24	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	24
25	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	25
26	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	26
27	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	27
28	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	28
29	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	29
30	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	30
31	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	31
32	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	32
33	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	33
34	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	34
35	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	35
36	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	36
37	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	37
38	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	38
39	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	39
40	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	40

Calculated by F. E. Paradis, C. E.

MICROFILMED

DEC 10 1964

596  
8  
88

5829  
5078  
05  
712

712



see Book 474 Page 7  
 ✓ Survey line up campfire to  
 74+00 on back yard campfire

Sta		H.I.	Rod	Ground
J.P.		151.47		
0+00	M.H. Sta.	74+00	12.61	138.86
+25	on main camp line bet. penitentiary		13.5	138.0
+50	Brooks		11.05	140.42
+75			7.93	143.54
1+00	bank cut		0.37	151.12
+25			1.3	150.2
+50			2.73	148.71
+75			2.2	149.3
2+00			2.63	148.7
+25			0.61	150.86
J.P.	10.05	160.91		
+50			8.47	162.41
+75			6.7	154.2
3+00			7.66	153.2
+25			6.3	154.6
+50			5.13	155.7
+60	M.H. E Brant		3.9	157.0
+75			2.6	158.3
J.P.	10.34	170.46		
4+00			0.79	160.12
			9.59	160.5

East from Sta. Mar. 18/13  
 line to alley bet 1st & 2nd  
 H.I. 151.47  
 J.P. 151.47  
 letter

Grade	cut			
134.20	4.7	140.42	151.10	155.78
		6.66	1.46	9.22
134.30	3.7	147.08	152.56	165.00
		134.40	140.00	8.00
		12.68	12.56	157.00
134.40	6.0	148.74	147.50	4.13
		7.07	8.31	160.87
137.20	6.3	155.81	148.75	153.70
		142.50	7.06	2.11
140.00	11.1	143.31	151.25	
		145.00	4.56	
		10.81	153.0	
			2.81	
141.25	9.0			
142.50	6.2			
143.75	5.6			
145.00	3.8			
146.25	4.6			
147.50	4.9			
148.75	5.5			
150.00	3.2			
151.25	3.4			
152.50	3.3			
153.00	4.0			
153.26	5.0			
153.70	7.2			



Mar. 18/13

Childs 2  
Saylor  
Allen

cont. from page 1

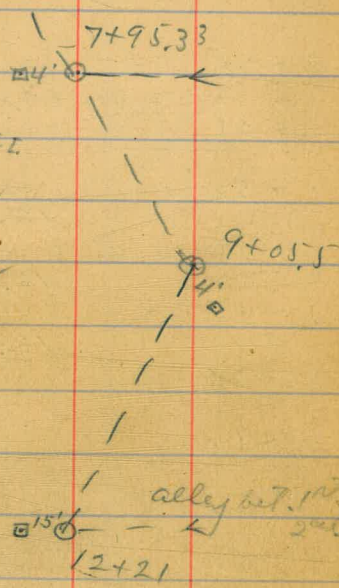
Sta.	H.T.	Red Ground	Grade cut			
	170.46					
4+25	8.80	161.66	154.13	7.5	155.81 H.T. 154.13 1.68 ✓	8.80 158.80 8.32 H.T. 167.12 H.T.
+50	11.66	158.80	154.56	4.2	158.12 ✓ 9.00	155.00 ✓ 12.12
+75	break	12.2	158.3	3.3	161.24 ✓ 5.88 ✓	164.36 ✓ 2.76 ✓
5+00		8.95	161.51	5.0	173.82 4.78	170.60 ✓ 8.00 ✓
+25		5.6	164.9	6.8	178.60 H.T. 167.48 ✓	179.28 ✓ 5.74
+50		7.98	162.48	2.8	171.12 ✓	185.02 H.T. 175.00 ✓
+75		4.8	165.7	4.5	171.91 32 180	10.02 178.00 ✓ 7.02 ✓
6+00		1.55	168.91	6.1		
5 P.	12.33	181.24				
+25		10.6	170.6	6.2		
+50		10.80	170.44	4.5		
+75		8.0	173.2	5.7		
7+00		7.42	173.32	4.8		
+25		4.9	176.3	5.7		
+50		1.96	179.28	7.1		
+75		0.3	180.9	7.2		
+95.3	M.H. center alley	0.45	180.79	5.8		
8+00	bet. 1st + all. trees	2.74	178.50	3.2		



Cont. from page 2

April 11/13 } Childs  
 Jayer 3  
 Allen

Sta.	H.I.	Red Ground	Grade	cut	
8+25	181.24	0.94 180.30	176.89	3.4	
J.P. +50	12.27 192.57	9.11 183.46	178.47	5.0	183.06 4.17
+75		9.6 183.0	180.06	2.9	187.63 H.I. 178.47
9+00		5.88 186.69	181.65	5.0	9.16 182.00
+05.5 m.H.		3.8 188.8	182.00	6.8	5.63 189.40
+25		2.4 190.2	183.11	7.1	6.73 196.13 H.I.
+50		3.17 189.40	184.54	4.9	184.54 71.59
+75		2.4 190.2	185.96	4.2	187.39 8.74
10+00		1.61 190.96	187.39	3.6	189.24 6.89
+25		1.10 191.47	188.81	2.7	193.09 3.04
J.P. +50 break	12.93 204.40	11.60 192.80	189.24	3.6	195.94 0.19
+75		8.8 195.6	191.16	4.4	198.79 8.95
11+00 break		7.39 197.01	193.09	3.9	195.94 11.80
+25		5.0 199.4	194.51	4.9	
+50		2.24 202.16	195.94	6.3	
+75		2.31 202.09	197.36	4.7	
J.P. 12+00	8.43 210.52	6.23 204.29	198.79	5.5	
+21.2 m.H. centrally		5.32 205.20	200.00	5.2	





✓ Server in alley bet. 1st & 2nd  
ditch Brooks + fence to north end

from bottom of canyon  
of trestle.

Sta		H.I.	Red	Ground	Grade	cut
0 + 00	M.H. bottom of Canyon bet. 1st & 2nd	217.12	11.92	205.20	200.00	5.2
+ 25	break		9.25	207.87	202.00	5.9
+ 50			2.83	214.29	209.00	5.3
J.P.	12.13	228.59	0.66	216.46		
+ 75	break		8.74	219.85	216.00	3.9
J.P.	12.95	240.98	0.56	228.03		
1 + 00			9.21	231.77	226.00	5.8
J.P.	12.30	252.65	0.63	240.35		
+ 25	break		11.73	240.92	236.00	4.9
+ 50			1.82	250.83	247.00	3.8

207.54 H.I.  
202  
5.74

219.85

4.51

H.I.

224.36

200.92

216.00

5.98

8.36

246.90 H.I.

236.00

10.90



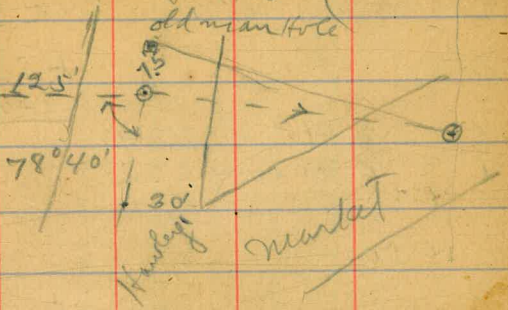
Server of canyon from  
to center alley west of albatross, near

main brickyard canyon

Chields  
Shoe 5  
Bunker

Sta.		H.I.	Red	Ground
J.P.		12.38	178.49	166.11
0+00	M.H. bottom of main canyon & center of market.		12.0	166.5
+25			10.91	167.58
+50			6.31	172.18
+75			2.35	176.14
1+00			3.07	175.42
+25			4.48	174.01
J.P.		10.42	188.20	0.71
+50			6.14	182.06
+59.3	M.H. center		11.9	176.3
2+00	(Hawley) Duran St.		9.61	178.59
+50			6.76	181.45
+84.3	M.H.		4.2	184.0
3+00			2.41	185.79
J.P.		12.97	198.76	9.82
+50			9.82	188.94
+59.3	M.H.		8.4	190.4
4+00			0.47	198.29
J.P.		12.53	210.82	11.94
+42	M.H. center alley west of albatross.		11.94	198.84

Grade	cut
162.28	4.3
163.74	3.8
165.28	6.9
166.82	9.3
168.35	7.0
169.89	4.1
171.43	10.6
172.00	4.3
174.60	4.0
177.80	3.7
180.00	4.0
181.05	4.8
184.38	4.6
185.00	5.4
188.92	9.4
193.00	5.9



172.18	168.35
6.63	10.46
178.81 H.I.	169.89
165.28	8.92
13.53	174.60
178.59	9.58
5.59	
184.18 H.I.	
172.00	177.80
12.18	6.38
180.00	185.79
4.18	8.36
	194.15 H.I.
	181.05
	13.10
184.38	185.00
9.77	9.15
198.29	
2.74	
201.03 H.I.	
188.45	
12.58	
193.00	
8.03	

821 900095  
7443  
5370



Handley Street from M.H.

South to Sta. 2+00

Sta 1+59.3 on center line

Apr 10/13

Childs  
F  
Allen  
Bunker

Sta.	H.I.	Rod	Ground	Grade	cut	
0+00	M.H. Sta. 1+59.3 <u>188.20</u>	11.9	176.3	172.00	4.3	182.16 4.70
+25	on center line	8.5	179.7	172.78	7.0	186.86 H.I. 173.50
+50		6.04	182.16	173.50	8.7	13.36 175.00
1+00		4.91	183.29	175.00	8.3	11.86
+50		3.87	184.33	176.50	7.8	
2+00	dead end	4.14	184.06	178.00	6.1	



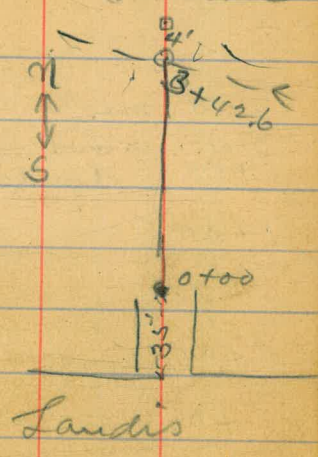
↓ alley west of albatross from bottom of canyon } Lehighs  
 + to Robinson } attery  
 } Bunker  
 April 10/13

Sta.		H.I.	Rod	Ground	Grade	cut		
0+00	M.H. bottom of canyon	210.82	1194	198.88	193.00	5.9	215.62 1.23 216.85 H.I. 211.00 ✓ 5.85 ✓	236.19 2.00 238.24 H.I. 231.00 ✓ 7.24
+25	North of Penh.		3.59	207.23	202.00	5.2	219.62	250.00 ✓
J.P.		12.36	222.55	0.63	210.19		6.34	5.96
+50	break		6.93	215.62	211.00	4.6	255.96 H.I.	257.13
J.P.		12.88	235.21	0.22	222.33		243.67 ✓	6.61
+75			8.40	226.81	221.00	5.8	12.29 ✓	263.74 H.I.
J.P.		11.29	246.01	0.49	234.72			250.89
+100	break		9.82	236.19	231.00	5.2		12.85 ✓
+25			1.68	244.33	237.33	7.0		252.67 ✓
J.P.		12.63	258.35	0.29	245.72			11.07 ✓
+50			8.73	249.62	243.67	6.0		254.44 ✓
+75	break		3.27	255.08	250.00	5.1		9.30
2+00			1.22	257.13	250.89	6.2		256.22 ✓
J.P.		6.90	264.03					7.52 ✓
+50			4.5	259.5	252.67	6.8		3.58.81
3+00			2.50	261.53	254.44	7.1		71.20
+50			1.73	262.30	256.22	6.1		
4+00	F.S. near Robinson		0.82	263.21	258.00	5.2		



✓ Sewer in alley bet. Texas & Ariz. from 35 north of Sandis  
 to main campfire line 20.9 right in Ariz. apr. 9/13  
 Sandis letter  
 Bunker

Sta.		H.I.	Rod	Ground	Grade	cut
0+00	dead end 35	0.94 295.61	3.80	294.67 291.81	287.00	4.8
+50	north of Sandis.		5.7	289.9	285.00	4.9
1+00			8.28	287.33	283.00	4.3
+50			9.6	286.0	281.00	5.0
+75	break		11.44	284.17	280.00	4.2
J.P.		1.14 284.10	12.65	282.96		
2+00			2.10	282.00	276.82	5.2
+50	break		8.27	275.83	270.46	5.3
J.P.		4.97 276.03	13.04	271.06		
+85	break		6.0	270.0	267.30	2.7
3+00			6.36	269.67	267.23	2.4
+426	M.H. in main campfire line		0.0	276.0	267.04	9.0
J.P.		11.55 287.38	14.9	275.83 275.5	272.00	3.5
+50	break		3.11	284.27	281.00	3.3
J.P.		12.72 296.99	7.40	289.59	286.00	3.6
+50	dead end.		2.35	294.64	291.00	3.6



275.83	
156	
277.39 H.I.	270.46
10.35	6.93
267.04	282.00
267.30	7.08
10.09	289.08 H.I.
	276.82
280.00	12.26
9.08	
281.00	283.00
8.08	285.00
291.81	6.08
3.90	4.08
295.71 H.I.	
287.00	
8.71	

501-5



Sever in Texas from 30.3  
400.3 north of Landis.

north of Landis to  
Apr. 9/13

Childs  
attest  
Bunker

Sta.		H.I.	Rod	Ground	Grade	cut	
		6.44 306.75		300.31			300.84 H.I.
0+00	M.H. center of Texas		10.8	296.0	291.0	5.0	291.19
+50	+400.3 north of Landis		10.20	296.55	291.95	4.6	9.65 ✓ 291.95
1+00			9.27	297.48	292.89	4.6	8.89 ✓ 292.89
+50			8.3	298.5	293.84	4.7	7.95 ✓ 293.84
2+00	5		7.32	299.43	294.78	4.7	7.00 ✓ 301.32 294.78
+50			6.3	300.5	295.73	4.8	3.66 ✓ 304.98 H.I. 6.06 ✓ 296.68 295.73 ✓ 8.30 ✓ 5.11 ✓
3+00			5.43	301.32	296.68	4.6	309.20
+50			4.4	302.4	297.63	4.8	297.63 ✓ 11.57
+70	dead end 30.3 north of Landis		3.90	302.85	298.00	4.9	



Valley west of albatross south  
 † of Penn. ave. 150'

of canyon north

apr. 10/13

Lehilds  
 letter 10  
 Boulder

Sta.	H.I.	Rod	Ground	Grade	cut		
0+00 M.H. bottom of	210.82	11.94	198.88	193.00	5.9	201.93	230.53
+25 canyon north						7.88	231.29 H.I.
of Penn.		8.89	201.93	198.45	3.5	209.51 H.I.	224.00
J.P.	7.79	223.41	215.62			198.45	7.29
+55 break		10.72	212.69	205.00	7.7	11.06	
+75		2.13	221.28	213.44	7.8	232.98	212.69
J.P.	13.04	236.26	0.19	223.22		3.45	2.69
1+00 break,		5.73	230.53	224.00	6.5	236.43 H.I.	215.38 H.I.
+25		3.28	232.98	226.50	6.5	229.00	205.00
+50 dead end		-0.3	236.6	229.00	7.6	7.43	10.39
near Penn. ave.							

5



Seiver on Texas from  
South of Wightman to

Sta.	H.I.	Rd Gravel
J.P.	12.15	308.70
0+00	M.H. bottom of	12.7 296.0
+50	Camp bet. Danks & Wightman	11.44 297.26
1+00		9.09 299.61
+50		6.58 302.12
2+00		4.58 304.12
+34.14	M.H. center of	3.8 304.9
+50	Wightman	3.5 305.2
3+00		2.55 306.15
+50		1.66 307.04
J.P.	5.40	312.44
4+00		4.43 308.01
+50		3.5 308.9
5+00		2.56 309.88
+25	dead end near univ. ave	1.8 310.6

325  
234.14  
290.86

Apr. 19/13  
bottom of canyon  
univ. ave.

Chiller  
letter 11  
Bunker

Grade cut		
297.26		38
3.58		
300.84	H.E	291.38
292.92		9.46
7.92		
296.1		
4.05		
303.66	H.I.	
294.84		
8.82		
302.12		
7.08		
309.20	H.I.	
296.76		300.30
12.44		8.90
298.68		301.28
10.52		7.95
300.00		302.19
300.00		7.01
9.20		303.14
304.08		6.06
5.12		
305.03		
4.17		
302.19		
4.9		
303.14		
4.9		
304.08		
4.8		
305.03		
4.9		
305.50		
5.1		



✓ 1/2 mile street from bottom of canyon north of  
 Brookes to Penn. ave.

apr. 14/13  
 Childs  
 letter  
 Box 12

Sta.		H.I.	Red Ground	Grake out				
0	0+00	11.34	167.12	152.9	3.3	154.75	10.42	9.47
	M.H. bottoming		150.00	152.9	3.3	165.17	H.I. 160.00	236.57
	+25			153.00	1.8	153.00	5.17	
	Canyon north of Brookes.		12.37	154.75		12.17		
1	+50		3.39	163.73		180.01		209.48
	J.P.	13.04	179.66	160.00	3.7	5.86	H.I. 181.00	5.81
	+75		0.50	166.62		185.87	4.87	215.29
	J.P.	12.23	191.41	167.00	4.7	174.00		208.00
2	+100		0.48	179.18		11.87		12.29
	J.P.		11.40	180.01		214.68		208.00
	+25 break		4.89	186.52	6.0	3.70		7.29
	J.P.	12.64	203.88	181.00	5.5	228.38	H.I. 383.68	4.35
	+50		0.17	191.24		218.00		238.06
	J.P.	12.71	216.28	192.00	5.6	10.38		226.50
	+75 break		6.24	197.64		6.13		11.56
3	+100		0.31	203.57		240.30		
	J.P.		6.80	209.48	6.5	246.43	H.I. 236.00	
	+150		2.13	214.15		285.00		10.43
	J.P.	12.57	228.63	208.00	6.1	11.43		
	+25		0.22	216.06		235.50		236.10
	+50 break		9.27	219.36	6.4	10.93		10.33
	J.P.	12.80	241.23	218.00	6.7			
5	+300		3.95	224.68				
	J.P.		0.20	228.43				
	+350		7.55	233.68	7.2			
	+50 break		0.93	240.30				
	J.P.	0.74	246.04	235.00	5.3			
	+400		3.83	242.21	6.7			
	+50		4.65	241.39	5.4			
	+60 dead-end		4.8	241.2	5.1			



Server at Hawley from 28'

bet. 44+45 + 22 west of east			
sta. 50.	0.15	184.21	184.00
0 700 dead end		6.88	177.33
+50	75' 20" of +8'		10.75
J.P.	east of line	13.02	171.19
1400	guy wire	1.77	169.57
+50.		5.85	165.49
2400		8.14	163.20
+50 break		11.16	160.78
J.P.	0.08	158.79	12.63
3400 M.H. break		5.3	153.5
+50.5 M.H. main line		11.7	147.15

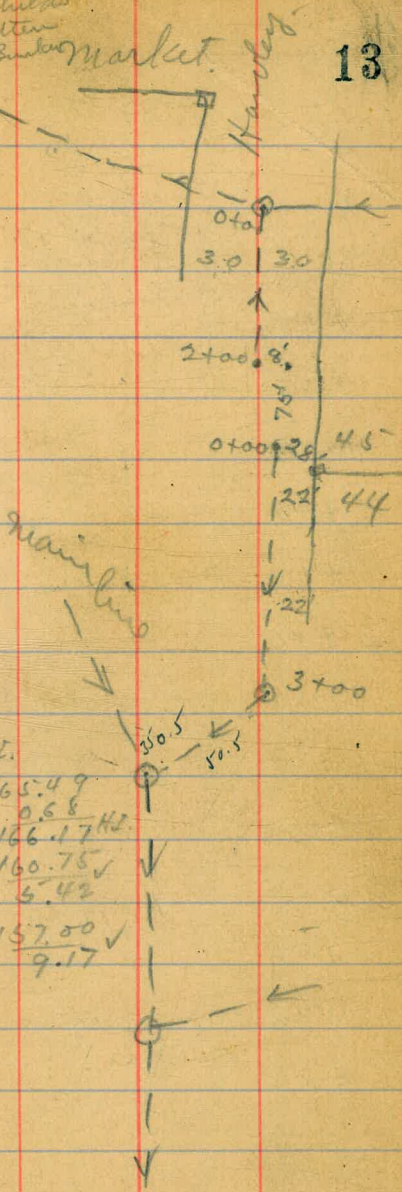
april 13

W.W. of lot line <sup>Habilds</sup> <sup>atten</sup> <sup>Bank</sup> market. 13

line of Hawley

grade of cut	172.00	5.3
	168.25	5.2
	164.50	5.1
	160.75	4.7
	157.00	6.2
	153.25	6.9
	147.00	6.5
	142.7	4.4

173.46	
2.51	
175.97	H.I.
172.00	165.49
3.97	0.68
168.25	166.17
7.72	160.75
164.50	5.42
11.47	157.00
153.25	9.17
12.92	
153.25	
4.49	
157.74	H.I.
147.00	
10.74	





~~12/17~~ Sewer on Granada from old  
to Hawthorn.

F.S. south of Gate  
Apr. 15/13

Childs  
alt 14  
Bunker

Sta.	100 ft S + Date	H.I.	Rod	Ground	Grade	alt.
J.P.	2.91	215.90		212.99		209.13
0+00	old F.S. south of gate.		4.2	211.7	206.00	5.7
+50			5.19	210.71	206.15	4.6
1+00			6.77	209.13	206.30	2.8
+50	170 = E Date		8.22	207.68	206.45	1.2
2+00			7.29	208.61	206.60	2.0
+50			5.9	210.0	206.75	3.3
3+00			4.9	211.0	206.90	4.1
+50	m.H. break 4' east		3.73	212.17	207.05	5.1
4+00			2.6	213.3	207.76	5.5
+50			1.5	214.4	208.48	5.9
5+00			0.40	215.50	209.20	6.3
J.P.	11.18	226.68				
+50			10.6	216.1	209.91	6.2
+55.8	m.H. center of Elm.		10.5	216.2	210.00	6.2
6+00			10.22	216.46	211.04	5.4
+50			9.0	217.7	212.22	5.5
7+00			7.71	218.97	213.40	5.6
+50			6.5	220.2	214.58	5.6

209.13  
 3.43  
 212.56 H.I. 206.60  
 5.96  
 206.30  
 6.26  
 208.61  
 6.80 H.I.  
 215.41  
 206.75  
 8.66  
 215.60  
 5.33  
 206.90  
 8.51  
 9.55  
 206.86  
 220.83 H.I. 207.05  
 8.36  
 206.24  
 207.76  
 13.07  
 210.00  
 212.22  
 208.48  
 10.83  
 9.61  
 12.35  
 211.04  
 213.40  
 209.20  
 9.79  
 7.43  
 11.63  
 210.71  
 214.59  
 4.35  
 215.06 H.I.  
 6.25  
 206.15  
 206.00  
 9.06  
 8.91







cont. from page 15

April 25/13 } Childs  
 After 16  
 Bunker

Sta.	H.I.	Rod	Ground	Grade	cut		
	239.52						236.31
15+50		4.7	234.8	228.36	6.4	235.46	12.05
16+00		4.06	235.46	228.86	6.6	4.59	248.86
+50		3.4	236.1	229.36	6.7	240.05 H.I.	247.87
+62		3.21	236.31	229.48	6.8	228.36	228.86
						11.69	12.15
						235.46	
						5.55 H.I.	
						241.01	
						229.48	
						11.53	
J.P. 0+00	5.71		230.73	99' 20" Grape.			
	236.44	5.9	230.5	223.50	7.0		
6+05		5.96	230.49	223.55	6.9	231.43	
+30		5.01	231.43	223.80	7.6	3.69	
+55		6.4	230.0	224.05	6.0	235.12 H.I.	
1+05		7.67	228.77	224.55	4.2	223.80	
+55		1.35	235.09	225.05	10.0	11.32	
						224.05	
						11.07	
						224.55	
						10.57	

Childs  
 After  
 Bunker

July 1/13

16 62  
 13 14  
 3 48

16 62  
 13 14



✓ Louisiana Street from  
to Landis

5' 20" of Park line  
April 28/13

Childs  
Allen  
17  
Bunker

Sta.	H.I.	Rod Ground	Grade	Cut		H.I.
J.P. center of Little River	281.63	276.74			276.83	
0+00 m.H. & R.O.		3.9 277.7	267.50	10.2	3.95	268.20 ✓
+50 of park line		4.50 277.13	267.85	9.3	280.78	12.58
1+00		4.80 276.83	268.20	8.6	267.85	17
+50		5.21 276.42	268.55	7.9	12.93 ✓	276.13
2+00		5.50 276.13	268.90	7.2	276.13	4.10
+50		5.86 275.77	269.25	6.5	3.69 H.I.	280.23 H.I.
3+00		6.59 275.04	269.60	5.4	279.82 H.I.	268.90 ✓
+16 m.H. center of myrtle.		5.8 275.8	269.70	6.1	268.55	11.33 ✓
+50		5.62 276.01	270.04	6.0	11.27 ✓	
J.P.	6.82 282.83				269.25 ✓	269.70 ✓
4+00		6.34 276.49	270.54	6.0	10.98 ✓	10.53
+50		6.0 276.8	271.04	5.8	270.04	276.49
5+00		5.70 277.13	271.54	5.6	10.19 ✓	5.57
+50		5.4 277.4	272.04	5.4	270.54	282.06 H.I.
6+00		4.91 277.92	272.54	5.4	11.52 ✓	270.54 ✓
+50 m.H.		4.6 278.2	273.04	5.2	271.04 ✓	11.52 ✓
7+00		4.19 278.64	273.37	5.2	11.02 ✓	271.54 ✓
+50		4.0 278.8	273.70	5.1	272.04 ✓	10.52
8+00		3.68 279.15	274.02	5.1	10.02 ✓	272.54 ✓

282.83  
- 3.15  
-----  
279.68

277.92  
- 29.02  
-----  
248.90  
3.29 H.I.  
281.81 H.I.  
273.04  
8.27 ✓  
278.64  
5.35  
283.99 H.I.  
273.37 ✓  
10.62  
273.70  
10.29 ✓  
274.02 ✓  
9.97 ✓



levit. from page 17.

Sta	H.I.	Rod	Ground	Grade	cut
8+50	282.83	3.3	279.5	274.35	5.2
9+00	977 650 327	3.03	279.80	274.68	5.1
+50		2.7	280.1	275.00	5.1
+77		2.4	280.4	275.18	5.2
10+00	6.87 287.33	2.37	280.46	275.36	5.1
J.P. +50		6.4	280.9	275.76	5.1
11+00		5.93	281.40	276.16	5.2
+50		5.7	281.6	276.56	5.0
12+00		5.35	281.98	276.96	5.0
+50		4.9	282.4	277.36	5.0
+80		4.5	282.8	277.60	5.2
13+00		4.40	282.93	277.76	5.1
+50		3.9	283.4	278.16	5.2
14+00		3.56	283.77	278.56	5.2
+50		3.2	284.1	278.96	5.1
15+00		2.84	284.49	279.36	5.1
+50		2.5	284.8	279.76	5.0
+80		2.1	285.2	280.00	5.2

apr. 23/13

leblinds  
utter  
18  
Buller

283.99 H.I.	280.46
274.35 ✓	6.50
9.64 ✓	286.96 H.E.
274.68 ✓	275.36
9.31	11.60 ✓
275.00	275.76 ✓
8.99	11.20
275.18 ✓	276.16 ✓
8.81	10.80
	276.56 ✓
	10.40
	276.96 ✓
	10.00
	277.36 ✓
	9.60
	277.60 ✓
	9.36
	277.76 ✓
	9.20
	278.16 ✓
	8.80
	278.56
	8.40 ✓
	278.96
	8.00 ✓
	279.36 ✓
	7.60
	279.76 ✓
	7.20
	280.00 ✓
	6.96



✓ Sewer in market from Hawley to  
Sheldon.

April 17/13

blinded  
at the  
19  
Bunker  
4.87

Sta.	<del>12.96</del>	H.L.	Rod	Ground	Grade	cut	
	12.96	211.25		198.29			203.53 3.15
0+00	M.H. Hawley + Market.		11.1	200.1	195.60	4.5	206.68 H.L. 196.60 10.08 ✓
+25			7.8	203.4	196.10	7.3	197.60 ✓ 9.08
+50			7.72	203.53	196.60 ✓	6.9	198.60 8.08 ✓
+75			7.6	203.6	197.10	6.5	199.60 ✓ 7.08
1+00			7.33	203.92	197.60 ✓	6.3	
+25			8.40	202.85	198.10	4.8	
+50			8.28	202.97	198.60 ✓	4.4	
+75			5.19	206.06	199.10	7.0	
2+00	dead end		4.45	206.80	199.60 ✓	7.2	



Sewer in alley bet. Robbins  
& Hawley to 1/2 mile.

Sta.	H.I.	Road	Ground
0+00	239.66	11.7	228.00
+25		7.07	232.59
+50		2.19	237.47
+75	252.01	8.72	243.29
1+00 break		4.54	247.47
+25		1.10	250.71
+50	264.55	11.19	253.36
+75		8.63	255.92
2+00		5.99	258.56
+25 dead end		4.63	259.92

Stove from apr. 17/15 } Child  
} Allen  
} Bunker 20

Grade	cut.	H.I.	H.I.
		237.47	247.47
		2.02	1.36
232.70	5.3	239.49	248.83
		230.10	237.50
		9.39	11.33
226.40	6.2	233.36	241.50
		3.21	
230.10	7.4	256.57	248.00
		247.50	8.57
233.80	9.5	12.07	
237.50	10.0		
241.00	9.9		
244.50	8.9		
248.00	7.9		
251.50	7.1		
255.00	4.9		







cont. from page 21

Sta.	H.I.	Red	Ground	Grade	cut
7+00	236.53	6.73	229.82	224.07	5.7
+50		5.6	231.1	224.86	6.2
8+00		4.73	231.82	225.64	6.2
+50		3.8	232.8	226.43	6.4
9+00		3.02	233.53	227.22	6.3
+49.65	M.H. Center 7 Fin. 12.03	2.03	234.53	228.00	6.5
10+00	246.53	10.77	235.78	230.40	5.4
+50		8.2	238.4	232.78	5.6
11+00		5.94	240.61	235.17	5.4
+50		3.4	243.2	237.55	5.7
12+00		0.84	245.71	239.94	5.8
J.P. +50	8.15 253.86	5.8	248.1	242.32	5.8
13+00		3.79	250.07	244.70	5.4
+27.4	M.H. center of J.P. Grape. 12.22	2.81	251.05	246.00	5.1
+50	263.27	11.7	151.6	246.66	4.9
14+00		10.30	252.97	248.11	4.9
+50		8.5	254.8	249.57	5.2

apr. 29/13

Childs  
Allen  
22  
Bunker

233.77 H.I.	
224.07	233.53
9.70 ✓	7.84
224.86	241.37 H.I.
8.91 ✓	228.00
225.64	13.37 ✓
8.13 ✓	230.40
226.43 ✓	10.97 ✓
7.34	
227.22	232.78
6.58 ✓	8.59 ✓
245.71	235.17 ✓
7.22	6.20
252.93 H.I.	237.55 ✓
239.94	3.82
12.99 ✓	
242.32	
10.61 ✓	
244.70	
8.23 ✓	
246.00	
6.93 ✓	
246.66 ✓	
6.27 ✓	
248.11 ✓	
4.82	
249.57 ✓	
3.36	

476  
2  
52



Cont. from page 22

May 1/13

Labills  
Cutter 23  
Bunker

Sta	H.I.	Rod	Ground	Grade	cut		
	263.27					256.21	262.63
15+00		7.06	256.21	251.03	5.2	6.63 262.84 H.I. 251.03	4.57 267.20 H.I. 257.45
+50		5.6	257.7	252.48	5.2	11.81 252.48	9.75 257.58
16+00		4.05	259.22	253.94	5.3	10.36 253.94	9.62 257.78
+50		2.6	260.7	255.40	5.3	8.90 255.40	9.42
17+00		1.36	261.91	256.85	5.1	7.44 257.00	263.24 4.12
+04.83	M.H. center of Hawthorn	1.18	262.09	257.00	5.1	5.84 257.18	267.36 H.I. 258.52
J.P. +50	7.40 269.49	7.1	262.4	257.18	5.2	5.66 257	8.84 258.38
18+00		6.86	262.63	257.38	5.2		8.98 258.18
+50		6.9	262.6	257.58	5.0		9.18 257.98
19+00		7.4	262.1	257.78	4.3		9.38 258.58
+50		6.64	262.85	257.98	4.9		8.78 258.78
20+00		6.3	263.2	258.18	5.0		8.58 258.98
+50		6.8	262.7	258.38	4.3		8.38
+84.7	M.H. center of Joy.	6.0	263.5	258.52	5.0		
27+00		6.25	263.24	258.58	4.7		
+50		7.7	261.8	258.78	3.0		
22+00		5.78	263.71	258.98	4.7		



cont. from page 23

May. 1/13

Childs  
utter 24  
Bunker

Sta.	H.I.	Rod Ground	Grade	cut		
22+50	269.49	5.0 264.5	259.18	5.3	269.5	267.36 H.I.
23+00		4.46 265.03	259.38	5.6	266.8	259.18
+50		4.3 265.2	259.58	5.6	264.8	8.18
+95	F.I. about 30' from juniper	3.7 265.8	259.76	6.0		259.38
						7.98
						259.58
						7.78
						259.76
						7.60



Server in alley bet. Dinglars <sup>and Univ. 2300</sup> fair center of road } behind  
 to Sta. 4+90 east of Brant. } after  
 April 24/13 } Brant 25

Sta.	H.I.	Rod	Ground	Grade	cut		
	235.98					238.40	255.61
0+00		7.2	228.8	224.80	4.0	265 H.I.	201 H.I.
+25	245.00	5.64	230.34	227.90	2.4	241.05	257.62
+50	257.36	6.60	238.40	231.00	7.4	231.00	247.87
+75		7.37	249.99	239.44	10.6	10.05	9.75
1+00		1.75	255.61	247.87	7.7	263.53	3.09
+30	269.96	7.3	262.7	258.00	4.7	250	266.62
+50		6.43	263.53	258.28	5.2	270	258.00
2+00		4.94	265.02	258.98	6.0	265.02	8.62
+50		3.5	266.5	259.67	6.8	5.88	258.28
3+00		2.62	267.34	260.36	7.0	270.90	8.34
+50		3.9	266.1	261.05	5.1	258.98	
4+00		3.26	266.70	261.74	5.0	11.92	
+50		2.4	267.6	262.44	5.2	259.67	
+90 dead end.		2.21	267.75	263.00	4.8	11.23	



Apr. 25/13

Childs  
 26  
 Amherst

Server, in South M. bet alley  
 + Alabama + south gr. miv. ave.  
 Sta.

bet Florida + Alabama

Sta.	Notes	H.I.	Rod	Ground	Grade	Cut	Remarks
0+00	M.H. center alley bet. Florida + Ala.	250.39	4.9	245.5	239.00	6.5	242.63 1.28
+50			7.76	242.63	239.20	3.4	243.91 H.I.
+80			9.1	241.3	239.32	2.0	239.20 4.91
1+00	b		11.90	238.49	239.40	-0.9	239.40 4.87
+50			11.91	238.48	239.60	-1.1	239.60 4.31
J.P.	5.36	257.90	3.85	246.54			257.76
+70			10.37	241.53	239.68	1.8	4.11 253.95 H.I.
2+00	break		3.87	248.03	239.80	8.2	245.00 8.95
+25	dead end		0.14	257.76	245.00	6.8	

31.6 No. of cut  
7+15

257.76  
2.19  
253.95 H.I.  
245.00  
8.95



Section in north st. bet. valley bet Florida + Alabama + Alabama  
 + Alabama + 20. of University ave.  
 Apr. 25/13

Chields  
 27  
 Bunker

Sta.	H.I.	Rod	Ground	Grade	cut
0 + 00	250.39	0.3	250.1	239.60	10.5
+ 25		1.85	248.54	239.70	8.8
+ 50		6.4	244.0	239.80	4.2
1 + 00		9.79	240.60	240.00	0.6
+ 25		9.6	240.8	240.10	0.7
+ 50		5.82	244.57	240.20	4.4
+ 75		5.09	245.30	240.30	5.0
2 + 00	258.60	8.04	250.56	244.30	6.3
+ 25		3.90	254.70	248.30	6.4

M.H. 171 = S<sub>2</sub> of  $\frac{1}{2}$  Univ. ave

Apr 25/13



Sever in Louisiana from  
288.65 north of Landis to 286.5

Sta.	H.I.	Rod	Ground
J.P. 0+00	199 286.48	284.49	
+50	M.H. bottom of camp. 288.05 north of Landis	10.3 276.2	
+100		10.55 275.93	
+150		9.30 277.18	
+200	b	7.1 279.4	
+250		4.96 281.52	
+300		2.8 283.7	
+360	dead end. 286.5 north of Landis.	2.35 284.13	

apr. 26/13  
bottom of canyon  
North of Landis

Grade	cut
284.13	
0.79	
284.92	H.I.
278.58	
6.34	
276.46	
8.46	
274.35	
10.57	
272.23	
12.69	
275.93	
3.63	
279.56	H.I.
270.12	
9.94	
272.23	
7.33	

Rebuilds  
cell 28  
Bunker

81.61  
71.65  
43  
263.42  
11.44



Mississippi street from 5' to Wright.

So. of park line

April 28/13  
Childs  
atten 29  
Bunker

Sta.	H.I.	Rod	Ground	Grade	cut		
J.P.	3.71	276.48	272.77			272.27	
0+00	M.H. center of Mississippi +	3.5	273.0	263.00	10.0	3.38	4.12
+50	5' so. of park line.	4.21	272.27	263.25	9.0	275.65 H.I.	271.53
1+00		4.63	271.85	263.50	8.4	263.25	7.78
+50		4.9	271.6	263.75	7.9	12.40 ✓	271.89
2+00	0.50% b	5.45	271.03	264.00	7.0	263.50 ✓	5.25
+50		5.7	270.8	264.25	6.6	12.15 ✓	277.14 H.I.
3+00		5.86	270.62	264.50	6.1	264.25 ✓	265.35
+1243	M.H. center of Myrtle.	5.3	271.2	264.55	6.6	11.40 ✓	11.79 ✓
+50		4.9	271.6	264.89	6.7	264.50 ✓	265.80 ✓
4+00		4.59	271.89	265.35	6.5	11.15 ✓	11.34 ✓
+50		4.4	272.1	265.80	6.3	264.55 ✓	266.25 ✓
5+00		4.09	272.39	266.25	6.1	11.10 ✓	10.89 ✓
+50		3.6	272.9	266.70	6.2	264.89 ✓	266.70 ✓
6+00		3.47	273.01	267.15	5.9	10.76 ✓	10.44 ✓
+15	M.H.	3.2	273.3	267.29	6.0		267.15 ✓
+50		2.9	273.6	267.60	6.0		9.99 ✓

615.00  
313.63  
301.57



cont. from page 29

Sta.	H.I.	Rod	Ground	Grade cut
7+00	276.48	2.80	273.68	268.06 ✓ 5.6
+50		2.4	274.1	268.51 ✓ 5.6
8+00		2.01	274.47	268.96 ✓ 5.5
+50	915 30	1.6	274.9	269.41 ✓ 5.5
9+00		1.53	274.95	269.87 ✓ 5.1
+15	F.S. near straight	1.5	275.0	270.00 ✓ 5.0

Apr. 28/13

Childs  
Atter 30  
Bunker

277.14 HI	
268.06	✓
9.08	
274.47	
4.89	
279.36 HI	
268.96	✓
10.40	✓
269.41	✓
9.95	
270.00	✓
9.36	
268.51	✓
8.63	✓



Sta.		H.T.	Rod	Ground
0+00	m.H. Camp	286.48	10.3	276.2
+50	bet. Landis & Wightman		8.95	277.53
1+00	ab. 165		6.90	279.58
+50	b		4.5	282.0
2+00			1.99	284.49
J.P.	9.78	296.07	0.19	286.29
+50			9.4	286.7
3+00			7.57	288.56
+45.7	m.H. center of Wightman		6.3	289.8
+50			6.3	289.8
4+00			5.36	290.71
+50			4.3	291.8
5+00			3.33	292.74
+50			2.4	293.7
6+00			1.41	294.66
+35	dead end.		0.5	295.6

bottom of Camp	apr. 30/13	Childs letter Bunker
min. ave.		31
Grade cut	279.58	
	6.55	
	286.13 H.I.	
	272.77	
	13.36	
	275.16	
	10.97 ✓	
	277.54	
	8.59 ✓	
	279.93	
	6.20 ✓	
	282.32 ✓	
	3.81 ✓	
	284.50	
	290.63	
	6.23	
	296.94 H.I.	
	285.63	
	11.31 ✓	
	286.67 ✓	
	10.27 ✓	
	287.70	
	9.24 ✓	
	288.74 ✓	
	8.20 ✓	
	289.77 ✓	
	7.17 ✓	
	290.50	
	6.44 ✓	



Mississippi Street from M.H.  
 + Wightman to right

Sta.	H.I.	Rod	Ground
	4.17	274.91	270.74
0+00	M.H. bottom of canyon bet. Landis	10.4	264.5
+50	Wightman	7.94	266.97
1+00		6.41	268.50
+50		4.8	270.1
+90.4	M.H. center of Landis	4.3	270.6
2+00	278.34	7.60	270.74
+50		7.2	271.1
3+00		6.60	271.74
+50		6.4	271.9
4+00		6.12	272.22
+50		5.6	272.7
+90	M.H.	5.5	272.8
5+00		5.40	272.94
+50		4.9	273.4
6+00		4.65	273.69
+50		4.2	274.1

bottom of canyon bet. Landis  
 May 6/13  
 Lehigh at 32  
 Bunker

Grade	Cut	H.I.	Ground
259.00	5.5	266.97	270.74
260.58	6.4	3.06	4.17
262.15	6.4	270.03	259.00
263.73	6.4	260.58	11.03
265.00	5.6	9.45	272.22
265.08	5.6	270.74	5.23
265.48	5.6	4.95	278.15 H.I.
265.88	5.8	275.69 H.I.	266.68
266.28	5.6	265.00	11.47
266.68	5.5	10.69	267.08
267.08	5.6	265.48	11.07
267.40	5.4	10.21	267.40
267.48	5.4	9.81	267.48
267.88	5.5	266.28	10.67
268.28	5.4	9.41	267.88
268.68	5.4		10.27
			268.28
			9.87
			268.68
			9.47



cont. from page 32

Sta.	H.I.	Rod	Ground	Grade	cut
S.P. 7+00	3.39	278.34	274.95	269.08	5.5
+50			274.8	269.48	5.3
+90 dead end.		3.19	275.15	270.80	5.3

may 7/13

Childs  
alter 33  
Bunker

278.15 H.I.

269.08 ✓

9.07 ✓

269.48

8.67 ✓



✓ 29<sup>th</sup> Street from 60' 20.

320 South of ash.

of ash. To

may 13

Childs letter 34  
Bunker

Sta.	H.I.	Rod	Ground	Grade	cut
0+00	break 60' south	201.80	146	200.34	197.00 3.3
+50	of ash.	3.20	198.60	195.08	3.5
1+00		4.75	197.05	193.16	3.9
+50		6.14	195.66	191.24	4.4
+90		8.42	193.38	189.70	3.7
2+40	break 300' ? 280' Ash.	12.20	189.60	187.40	2.2
		12.88	188.92	185.80	1.92

188.92  
8.13  
197.05 H.I.  
189.70  
7.35  
197.05  
7.11  
204.16 H.I.  
193.16  
11.00  
195.08  
9.08

10.58  
11.28  
185.77  
9.65  
187.40  
6.38  
7.18  
187.0



✓ Sewer in Mississippi Street  
 & South of Wightman to University

from bottom of canyon  
 ave. Childs  
 letter  
 Bunker 35  
 May 7/13

Sta.		H.I.	Rod	Ground	Grade	cut		
		274.91					270.03 H.I.	
0+00	M.H. bottom of canyon 160.4		10.4	264.5	259.00	5.5	260.50 ✓ 9.53 ✓ 262.00 ✓ 8.03 ✓	
+50	north of Fandis		8.18	266.73	260.50	6.2	271.32	277.22 6.30
1+00			6.73	268.18	262.00	6.2	5.57 ✓ 276.89 H.I.	283.52 H.I. 272.50 ✓
+50			5.3	269.6	263.50	6.1	265.00 ✓ 11.89 ✓ 266.50 ✓ 10.39 ✓	11.02 ✓ 273.22 ✓ 10.30 ✓
2+00	b		3.54	271.32	265.00	6.3	268.00 ✓ 8.89 ✓ 269.50 ✓ 7.39 ✓	273.42 ✓ 10.10 ✓ 279.59 4.80
+50			2.2	272.7	266.50	6.2	271.00 ✓ 5.89 ✓	284.39 H.I. 274.22 ✓ 10.17 ✓
3+00		9.73	0.80	274.11	268.00	6.1	283.84	274.62 9.77 ✓
J.P. +50			8.3	275.5	269.50	6.0		275.02 ✓ 9.38 ✓
4+00			6.62	277.22	271.00	6.2		278.42 8.97 ✓
+50			5.5	278.3	272.50	5.8		
+73.7	M.H. Center of Wightman		5.2	278.6	273.22	5.4		
5+00			4.97	278.87	273.42	5.4		
+50			4.6	279.2	273.82	5.4		
6+00		76.5 273.7 291.3	4.25	279.59	274.22	5.4		
+50			4.0	279.8	274.62	5.2		
7+00			3.52	280.32	275.02	5.3		
+50			3.2	280.6	275.42	5.2		
+65	dead end		3.1	280.7	275.54	5.2		



2

Burlingame drive from M.H.  
west of Bridge to Sta. 348.5 east.

bottom of canyon just  
May 13/13

Childs  
letter  
36  
Bunker

Sta.	H.I.	Red	Ground	Grade	cut	
0+00	M.H. 348.5	238.43	0.34	238.09	233.00	5.1 #6
+50	east of M.H. in bottom of canyon		4.8	233.6	227.50	6.1
1+00			10.36	228.07	222.00	6.1
J.P. +50	0.99	226.62	12.80	225.63		
			4.45	222.17	216.50	5.7
2+00	b		9.61	217.01	211.00	6.0
J.P. +50	0.28	213.92	12.98	213.64		
			4.20	209.72	205.50	4.2
3+00	break.		8.02	205.90	200.00	5.9 #1
+48.5	M.H. bottom of canyon west of bridge		8.8	205.1	199.70	5.4 #2

5.4  
199.7



37



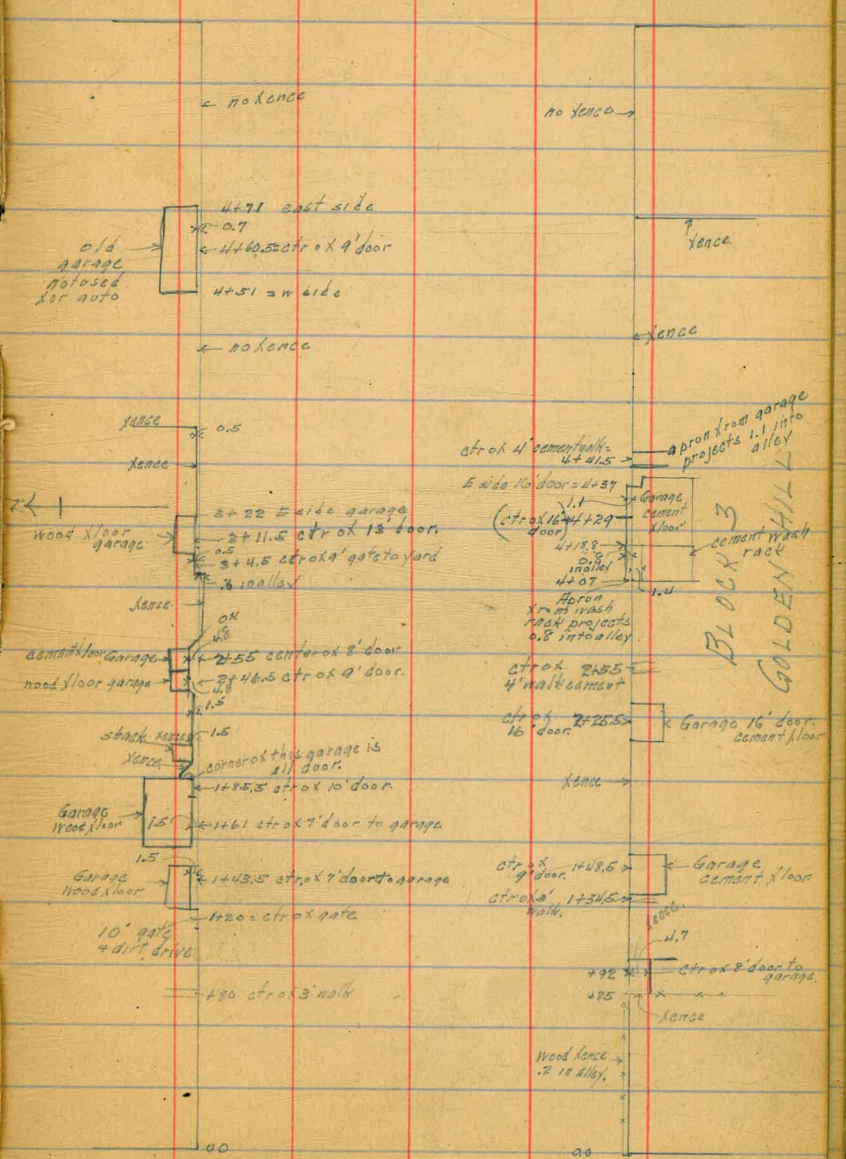
CROSS-SECTION OF ALLEY  
BET. B+C AND 24<sup>TH</sup> STS  
20' wide

Blk 3, Golden Hill Addition

25<sup>TH</sup>

ST

BM.	6.37	185.80	179.43	S+ 24 <sup>TH</sup> C
S		5.13	180.7	on st curb S. Alley produced
N		5.17	180.6	N.L. Alley produced
E.L. 24 <sup>TH</sup> ST.				
N		4.1	181.7	
C		4.3	181.5	
S		4.9	180.9	
3' E				
S		0.3	185.5	
+2		4.0	181.8	
C		4.2	181.6	
+6.5		3.9	181.9	
N		2.3	183.5	
TP.	13.03	14.55	4.28	191.52
50' E				
N		5.0	189.6	
+5		7.9	186.7	
C		8.5	186.1	
+8		7.5	187.1	
S		5.7	188.9	



BLOCK 3 GOLDEN HILL

80' E

24<sup>TH</sup>

ST

N		3.30	191.3	ctr of 3' cement walk to house
---	--	------	-------	--------------------------------



194.55

85' E

S	3.2	191.2	
+2	4.2	190.4	
C	4.5	190.1	
+5	4.3	190.3	
N	2.9	191.7	

92' E

49.50x5L	2.8	191.8	floor of garage
----------	-----	-------	-----------------

115' E

N	1.3	193.3	ctr of dirt drive C
---	-----	-------	---------------------

125' E

N	1.3	193.3	
---	-----	-------	--

+5	2.3	192.3	
----	-----	-------	--

C	2.1	192.5	
---	-----	-------	--

+8	1.9	192.7	
----	-----	-------	--

S	1.4	193.2	
---	-----	-------	--

134.5 E

S	0.9	193.7	ctr. of S walk
---	-----	-------	----------------

T.P.	7.89	202.17	0.27	194.28
------	------	--------	------	--------

39

1+43.5 E

1.5' N of N.L.	7.0	195.2	ctr of door to wood floor garage
----------------	-----	-------	----------------------------------

148.5 E

S	7.9	194.3	ctr of door to cement floor garage
---	-----	-------	------------------------------------

161' E

1.5' N of N.L.	5.3.5	196.8	ctr of door
----------------	-------	-------	-------------

175' E

S	6.9	195.3	
---	-----	-------	--

+2	7.5	194.7	
----	-----	-------	--

+6	7.7	194.5	
----	-----	-------	--

N	7.3	194.9	
---	-----	-------	--

N	6.5	195.7	
---	-----	-------	--

185.5' E

1.5' N of N.L.	5.35	196.8	ctr of corner door to garage
----------------	------	-------	------------------------------

200' E

N	5.9	196.3	
---	-----	-------	--

+5	6.4	195.8	
----	-----	-------	--

C	6.5	195.7	
---	-----	-------	--

+8	6.6	195.6	
----	-----	-------	--

S	6.0	196.2	
---	-----	-------	--







14096  
74  
198.58

441.5' E

3 N. of SL.	3.8	198.4	cement step
0.7 S of SL.	3.4	198.8	main walk

445' E

N	3.8	198.4	
C	4.0	198.2	
S	3.8	198.4	

460.5' E

N	4.7	197.5	on ground ctr door
---	-----	-------	-----------------------

500' E

S	5.0	197.2	
C	5.4	196.8	
+8	5.5	196.7	
N	4.7	197.5	

550' E

N	5.3	196.9	
+2	6.4	195.8	
C	6.4	195.8	
S	6.1	196.1	

41

601' E = N.L. 25 ST

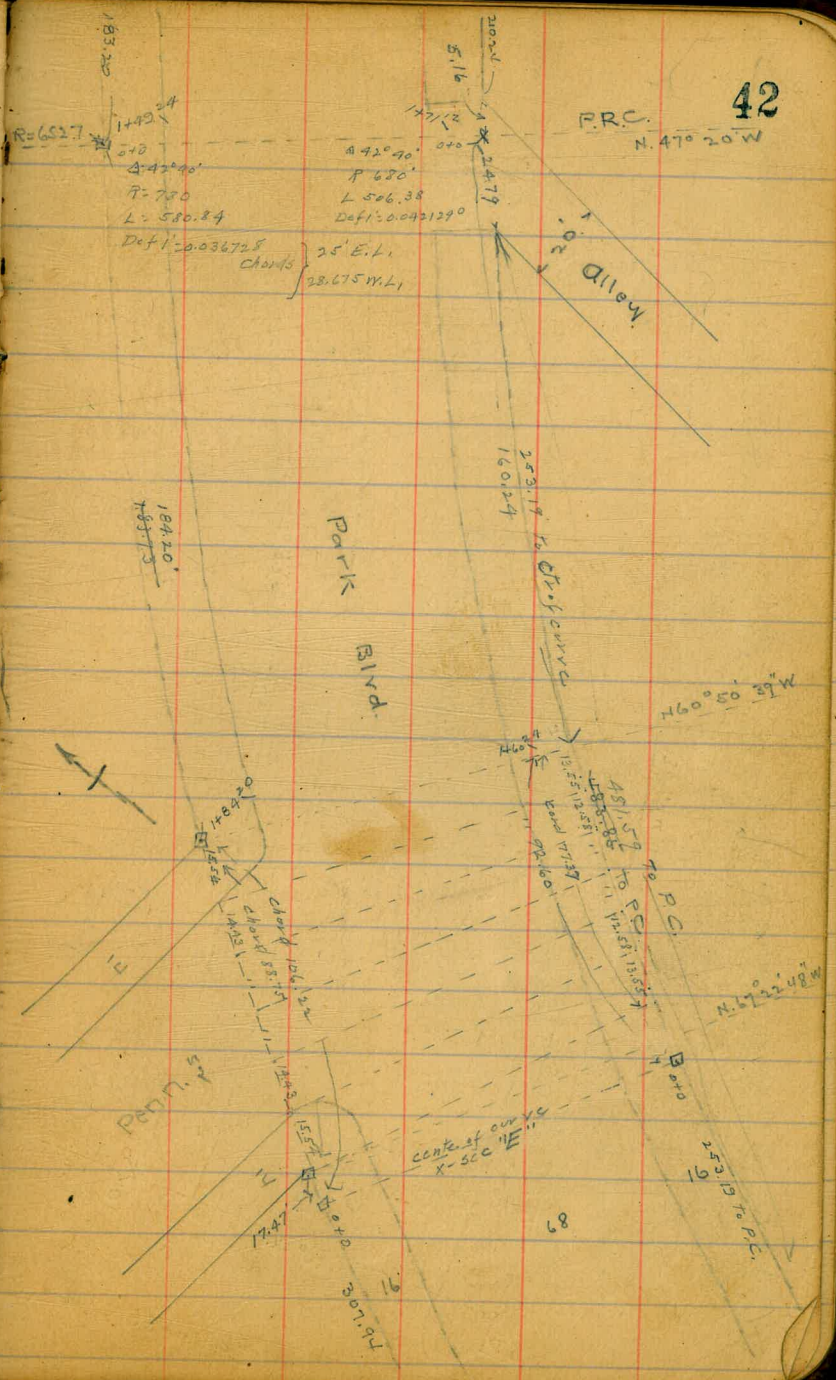
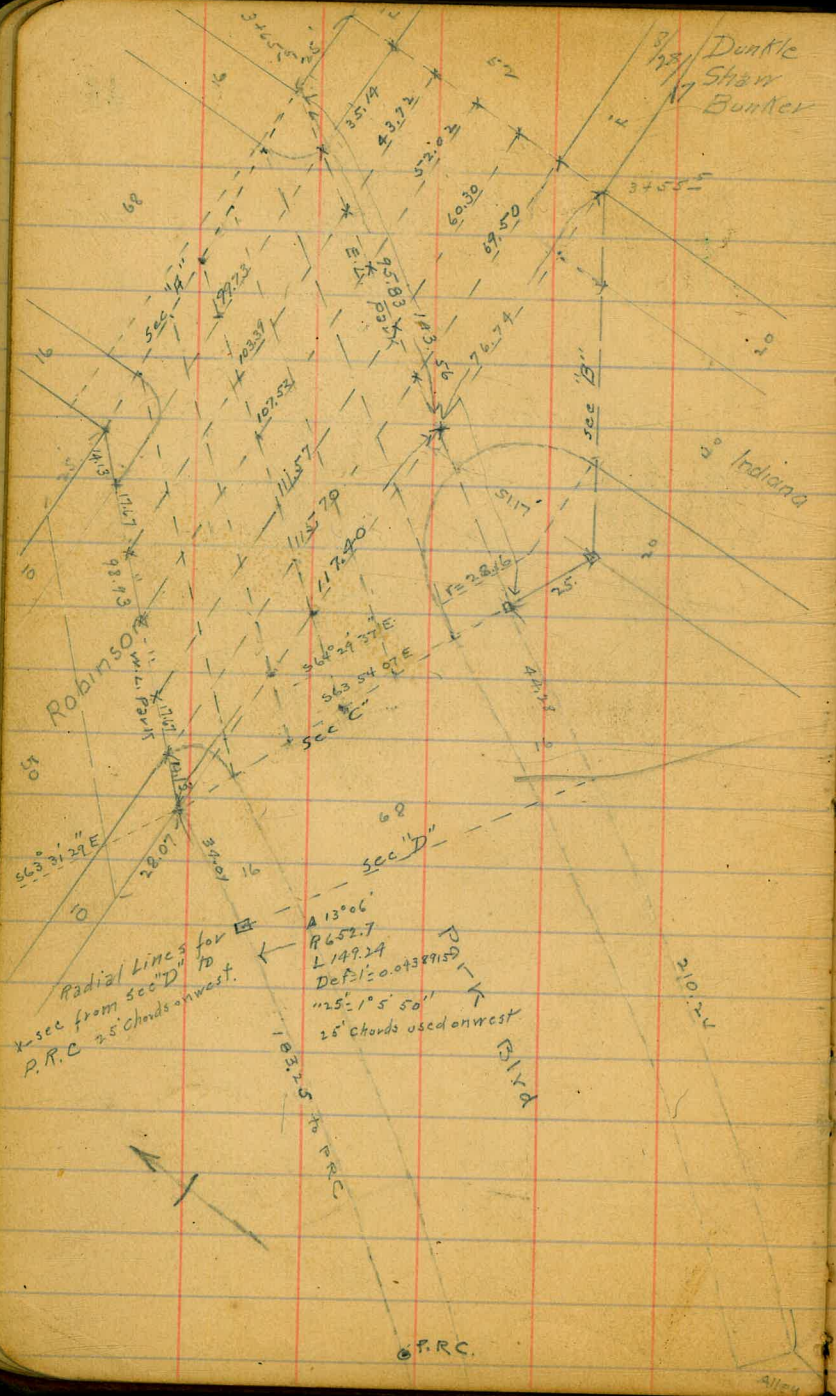
S	8.02	194.2	on cement return
C	8.2	194.0	
N	7.83	194.4	on cement

Returns into alley at 25th St are 20.8' apart  
making the so. one .8' too far south

T.P.	3.87	197.94	8.10	194.07
------	------	--------	------	--------

T.P. on B.M.	6.97	190.97	B.M. 314 25+C = 190.96
--------------	------	--------	---------------------------







Perim.

N 61° 22' 48" W

Park Blvd.

TOP RC

451.59  
453.85

307.94



N. 90° W.

Cypress

x-section Park Blvd from University  
to N.L. Balboa Park  
Park Blvd 100 wide 16 walks & 17 quarters 1/11

43  
Dunkle  
Shaw  
Bunker

B.M. Brass plg. N.W. Corner & University  
11.35 315.26

303.88

T.P. 3.60 317.82 1.04 314.22

0+0 = S.E. University on East

w.L.	3.3	314.5
crk	2.4	315.4
gutter	3.3	314.5
1/4	2.9	314.9
+ 4.8 = 2 west of w. rail	2.6	315.2
crk	2.3	315.5
+ 12.2 = 2' E of E rail	2.3	315.5
1/4	2.3	315.5
crk	2.4	315.4
E.L.	2.9	314.9

0+25 south

E.L.	3.1	314.7
crk	2.6	315.2
1/4	2.8	315.0
+ 4.5 = 2' E of rail	2.8	315.0
M	2.7	315.1
+ 12.2 = 2' W of rail	3.0	314.8
1/4	3.2	314.6
+ 15	3.2	314.2
crk	3.3	314.5
+ 02	2.7	315.1
+ 07	2.7	315.1
w.L.	6.5	311.3

P.C. R=680.

68

16

6

10

10



0+50 west

W.L.	8.2	309.6
+ 4	5.1	312.7
+ 10	3.2	314.6
+ 14	3.2	314.6
Crk	4.0	313.4
"4		
+ 4.8 = 2' W of Rail	3.7	314.1
	3.5	314.3
M	3.2	314.6
+ 12.2 = 2' E of "	3.2	314.6
"4		
	3.3	314.5
Crk	3.0	314.8
E.L.	3.2	314.6

\* 0+75

E.L.	3.3	314.5
Crk	3.3	314.5
"4		
+ 4.8 = 2' E of Rail	3.7	314.1
	3.7	314.1
M	3.8	314.0
+ 12.2 = 2' W of "	4.1	313.7
"4		
	4.3	313.5
Crk	5.1	312.7
+ 4	5.8	312.0
"6		
	7.1	310.7
W.L.	7.6	310.2

1+0

W.L.	6.1	311.7
Crk	5.6	312.2
"4		
	4.6	313.2
+ 4.8 = 2' W of Rail	4.5	313.3
M		
+ 12.2 = 2' E of Rail	4.3	313.5
	4.1	313.7
"4		
	3.9	313.9
Crk		
	3.4	314.4
E.L.		
	3.5	314.3

1+25

E.L.	3.7	314.1
Crk		
	3.7	314.1
"4		
	4.5	313.3
+ 4.8 = 2' E of Rail	4.6	313.2
M	4.8	313.0
+ 12.2 = 2' W of "	4.9	312.9
"4		
	4.9	312.9
Crk		
	5.9	311.9
W.L.		
	7.1	310.7



1450

W.L.	7.3	310.5
crk	6.4	311.4
"4	5.3	312.5
+4.8 = 2W of W. Tail	5.4	312.4
M.	5.3	312.5
+12.2 = 2E of E "	5.1	312.7
"4	4.6	313.2
crk	3.9	313.9
E.L.	4.0	313.8

1475

E.L.	4.3	313.5
crk	4.1	313.7
"4	4.4	313.4
+4.8 = 2E of Tail	5.5	312.3
M.	5.8	312.6
+12.2 = 2W " "	6.0	311.8
+1.5	5.5	312.3
"4	5.9	311.9
crk	6.9	310.9
W.L.	8.1	309.7

2+14 = N.L. Essex St

W.L.	8.5	309.3
crk	8.0	309.8
"4	6.5	311.3
+4.8 = 2W of Tail	6.7	311.1
M	6.5	311.3
+10	6.5	311.3
+12.2 = 2E " "	6.2	311.6
"4	5.4	312.4
+3	4.9	312.9
crk	4.5	313.3
E.L.	4.8	313.0

N. Cuck

E.L.	4.9	312.9
crk	4.7	313.1
+14	5.0	312.8
"4	5.6	312.2
+4.8 = 2E of Tail	6.4	311.4
M	6.8	311.0
	6.7	311.1
+12.2 = 2W " "	6.9	310.9
"4	7.0	310.8
crk	8.3	309.5
W.L.	8.9	308.9



## N 1/4 Essex

W.L.	9.1	308.7
crk	8.4	309.4
1/4	7.4	310.4
+4.8 = 2' W of rail	7.2	310.6
M	6.8	311.0
+10	6.8	311.0
+12.2 = 2' E of rail	6.6	311.2
1/4	5.7	312.1
+3	5.2	312.6
crk	4.8	313.0
E.L.	5.0	312.8

## Center

E.L.	5.0	312.8
crk	5.0	312.8
+13	5.4	312.4
1/4	6.0	311.8
+4.8 = 2' E of rail	6.7	311.1
+7	7.0	310.8
M.	7.0	310.8
+12.2 = 2' W of rail	7.5	310.3
1/4	7.6	310.2
crk	8.6	309.2
W.L.	9.2	308.6

## S 1/4

W.L.	9.6	308.2
crk	8.9	308.9
1/4	7.6	310.2
+4.8 = 2' W of rail	7.6	310.2
M	7.1	310.7
+10	7.1	310.7
+12.2 = 2' E of rail	6.7	311.1
1/4	6.1	311.7
+4	5.4	312.4
crk	5.0	312.8
E.L.	5.1	312.7

## S. curb

E.L.	5.2	312.6
crk	5.1	312.7
+13	5.1	312.7
1/4	6.2	311.6
+4.8 = 2' E of rail	6.9	310.9
+7	7.3	310.5
M	7.3	310.5
+12.2 = 2' W of rail	7.7	310.1
1/4	7.9	309.9
crk	9.2	308.6
W.L.	9.9	307.9



## S.L. Essex

W.L.	10.4	307.4
erb	9.5	308.3
"4	8.1	309.7
+4.8 = 2 w of rail	7.8	310.0
M.	7.5	310.3
+10	7.5	310.3
+12.2 = 2' E. " "	7.1	310.7
"4	6.3	311.5
+4	5.7	312.1
erb	5.3	312.5
E.L.	5.3	312.5

## 0+25 west

E.L.	5.9	311.9
erb	5.7	312.1
+13	6.0	311.8
"4	6.7	311.1
+4.8 = 2' E of rail	7.6	310.2
+7	7.9	309.9
M	8.0	309.8
+12.2 = 2 w. " "	8.4	309.4
"4	8.5	309.3
erb	10.3	307.5
W.L.	11.0	306.8

47

## 0+50

W.L.	11.4	306.4
erb	10.8	307.0
+3	10.3	307.5
"4	9.2	308.6
+4.8 = 2' w of rail	9.0	308.8
M	8.5	309.3
+10	8.4	309.4
+12.2 = 2' E of "	8.1	309.7
"4	7.1	310.7
+4	6.4	311.4
erb	6.0	311.8
E.L.	6.5	311.3

## +75

E.L.	6.7	311.1
erb	6.5	311.3
+13	6.6	311.2
"4	7.6	310.2
+4.8 = 2' E of rail	8.6	309.2
+7	8.9	308.9
M.	9.0	308.8
+12.2 = 2 w of rail	9.4	308.4
"4	9.5	308.3
erb	11.0	306.8
W.L.	11.7	306.1
	12.77	



	140		
W.L.	12.1	305.9	
Crk	11.5	306.3	
"4	10.3	307.5	
+ 4.8 = 2' W of trail	10.0	307.8	
M	9.5	308.3	
+ 10	9.4	308.4	
+ 12.2 = 2' E of 11	9.1	308.7	
"4	8.2	309.6	
+ 5	7.2	310.6	
Crk	7.0	310.8	
E.L.	6.9	310.9	
	142.5		
E.L.	7.0	310.8	
Crk	7.3	310.5	
+ 11	7.6	310.2	
"4	8.5	309.3	
+ 4.8 = 2' E of trail	7.5	308.3	
+ 7	7.9	307.9	
M	9.9	307.9	
+ 12.2 = 2' W of trail	10.5	307.3	
"4	10.8	307.0	
Crk	12.0	305.8	
W.L.	12.6	305.2	

	317.82		
	1450		
W.L.	13.1	304.7	
Crk	12.1	305.7	
"4	11.0	306.8	
+ 4.8 = 2' W of trail	10.9	306.9	
M	10.7	307.1	
+ 10	10.4	307.4	
+ 12.2 = 2' E of 11	10.1	307.7	
"4	9.0	308.8	
+ 6	8.1	309.7	
Crk	7.6	310.2	
E.L.	7.5	310.3	
T.P.	1.97	310.90	8.89
			308.93
	1475		
E.L.	0.5	310.4	
+ 7	1.3	309.6	
Crk	1.3	309.6	
+ 12	1.8	309.1	
"4	2.5	308.4	
+ 4.8 = 2' E of trail	3.7	307.2	
+ 7	4.1	306.8	
M	4.2	306.7	
+ 12.2 = 2' W of 11	4.6	306.3	
"4	4.6	306.3	
Crk	5.6	305.3	
W.L.	6.3	304.6	



310.90

270

W.L.	6.5	304.4
crk	5.5	305.4
"4	4.9	306.0
+ 4.8' = 2' W of rail	5.0	305.9
M.	4.7	306.2
+ 10	4.4	306.5
+ 12.2 = 2' E. "	3.9	307.0
"4	3.4	307.5
+ 4	2.5	308.4
crk	1.9	309.0
+ 9	1.6	309.3
E.L.	+ 0.3	311.2

272.5

E.L.	0.4	310.5
crk	2.4	308.5
+ 11	3.0	307.9
"4	3.8	307.1
+ 4.4 = 2' E of rail	4.9	306.0
M.	5.1	305.8
+ 11.8 = 2' W. "	5.4	305.5
"4	5.2	305.7
crk	5.4	305.5
W.L.	6.3	304.6

49

275.0

W.L.	6.3	304.6
+ 9'	5.4	305.5
crk	5.1	305.8
"4	5.3	305.6
+ 5 = 2' W of rail	5.7	305.2
M.	5.5	305.4
+ 13	5.3	305.6
"4	4.6	306.3
crk	2.7	308.2
E.L.	0.8	310.1

277.5

E.L.	0.4	310.5
+ 7	2.1	308.8
+ 14	2.3	308.6
crk	2.6	308.3
+ 4	4.3	306.6
"4	5.5	305.4
+ 1.8 = 2' E of rail	5.8	305.1
M.	6.1	304.8
+ 6.8 = 2' W of rail	6.3	304.6
"4	5.7	305.2
crk	5.6	305.3
W.L.	6.3	304.6



3+0

w.L.	6.4	304.5
crk	5.6	305.3
"4	6.2	304.7
+6	6.6	304.3
M.	6.7	304.2
"4	6.3	304.6
+1	6.2	304.7
crk	4.5	306.4
E.L.	2.6	308.3

3+25

E.L.	3.5	307.4
crk	5.7	305.2
+12 = 2'E of trail	6.7	304.2
M.	7.1	303.8
+3 = 2' w of trail	6.9	304.0
+7	6.3	304.6
"4	6.4	304.5
crk	6.0	304.9
w.L.	6.7	304.2

3+55<sup>5</sup> = N.L. Robinson on East

w.L.	7.2	303.7
crk	6.5	304.4
"4	6.9	304.0
M.	7.1	303.8
+1.5 = 2' w of trail	7.3	303.6
"4	7.1	303.8
+9.5 = 2' w of trail	7.1	303.8
crk	6.6	304.3
+10	5.6	305.3
E.L.	3.7	307.2
+01	6.2	304.7
+25 = old E.L. Parkaid	6.3	304.6

1-sec H<sub>A</sub> Page 42

E.L.	3.7	307.2
+6	5.6	305.3
crk	6.7	304.2
+7 = 2'E of trail	7.1	303.8
"4	7.2	303.7
+14.5 = 2' w of trail	7.4	303.5
M.	7.1	303.8
"4	7.0	303.9
crk	6.8	304.1
w.L.	7.6	303.3
T.P.	4.42	307.38
	7.94	302.96



## North Creek Robinson

W.L.	4.8	302.6
crk	3.7	303.7
"4	3.7	303.7
M	3.5	303.9
+13 =	3.7	303.7
+15 = 2' w of rail	4.0	303.4
"4	4.1	303.3
crk	3.9	303.5
+6 = 2' E of rail	3.7	303.7
E.L.	3.5	303.9
+15	3.4	304.0
+35 <sup>14</sup> = E.L. Indiana	3.4	304.0

N "4

E.L. Indiana	3.8	303.6
+20	3.7	303.7
+42 = 2' E of rail	3.9	303.5
E.L. Park	3.9	303.5
crk	4.3	303.1
+23.5 from E.L. Park = 2' w of rail	4.2	303.2
"4	3.7	303.7
M	3.6	303.8
"4	3.8	303.6
crk	4.5	302.9
W.L.	5.0	302.4

## E Robinson

W.L.	5.3	302.1
crk	4.9	302.5
"4	4.1	303.3
M	3.9	303.5
"4	4.0	303.4
+95 from M.L. = 2' w of rail	4.2	303.2
crk	4.4	303.0
E.L.	4.1	303.3
+12 = 2' E of rail	4.1	303.3
+32	4.0	303.4
+52 = E.L. Indiana	3.8	303.6

S "4

E.L. Indiana	4.0	303.4
+20	4.3	303.1
+37 <sup>5</sup> = 2' E of rail	4.3	303.1
+60 <sup>30</sup> = E.L. Park	4.5	302.9
+2' = 2' w of rail	4.2	303.2
crk	4.2	303.2
"4	4.3	303.1
AV	4.4	303.0
"4	4.6	302.8
crk	5.0	302.4
W.L.	5.8	301.6



## Sou. Curve

W.L.	6.5	300.9
erb	5.8	301.6
"A	5.0	302.4
M	4.8	302.6
"A	4.6	302.8
erb	4.5	302.9
E.L. Park	4.4	303.0
+ 85 <sup>8</sup> = 2' E of rail	4.4	303.0
+ 32 <sup>8</sup> = 2' E of rail	4.5	302.9
+ 40	4.3	303.1
+ 69 <sup>50</sup> = E.L. Indiana	4.2	303.2

## S.L. Robinson

E.L. Indiana	4.2	303.2
erb	4.4	303.0
gutter	5.2	302.2
+ 34 = 2' E of rail	4.6	302.8
+ 58 = 2' W. "	4.6	302.8
+ 76 <sup>74</sup> = E.L. Park	4.8	302.6
erb	4.6	302.8
"A	4.7	302.7
M	5.2	302.2
"A	5.9	301.5
erb	6.4	301.0
W.L.	6.9	300.5

## x-section "B"

W.L. Indiana	5.1	302.3
erb	5.0	302.4
+ 31 <sup>7</sup> from W.L. = 2' W of rail	4.9	302.5
"A	4.9	302.5
M	4.8	302.6
+ 56 <sup>5</sup> from W.L. = 2' E of rail	4.8	302.6
"A	4.7	302.7
gutter	4.7	302.7
erb	4.4	303.0
E.L. Indiana	4.2	303.2

## x-section "C"

E.L. Park	5.1	302.3
erb	5.2	302.4
"A	5.2	302.2
M	5.6	301.8
"A	6.1	301.3
erb	6.4	301.0
W.L. Park	6.9	300.5



x-section "D"

W.L.	7.3	300.1
crk	7.2	300.2
"A	6.9	300.5
M	5.8	301.6
"A	5.3	302.1
crk	5.5	301.9
E.L.	4.9	302.5

+25 500 on W.L. from "D" see sketch page 42

E.L.	5.0	302.4
+2	5.0	302.4
+8	6.0	301.4
crk	6.2	301.2
"A	6.0	301.4
M	6.3	301.1
"A	7.5	299.9
crk	7.7	299.7
W.L.	7.5	299.6

+50

W.L.	8.7	298.7
crk	8.6	298.8
"A	7.8	299.6
M	6.8	300.6
"A	6.6	300.8
crk	6.8	300.4
+14	6.4	301.0
E.L.	5.8	301.6

+75

E.L.	6.4	301.0
crk	7.3	300.1
"A	7.2	300.2
M	7.3	300.1
"A	8.0	299.4
crk	8.9	298.5
W.L.	9.3	298.1



307.38

140

w.L.	10.2	297.2
crb	9.2	298.2
'4	8.5	298.9
+9'	7.8	299.6
M	7.7	299.7
'4	7.5	299.9
crb	7.6	299.8
+12	7.6	299.8
E.L.	6.9	300.5

1425

E.L.	8.0	299.4
+4	8.3	299.1
crb	7.7	299.7
'4	7.8	299.6
M	8.0	299.4
'4	9.1	298.3
crb	10.7	296.7
w.L.	11.2	296.2

54

$$\left. \begin{array}{l} +49^{\circ} 24' \text{ on West} \\ +71^{\circ} 32' \text{ on East} \end{array} \right\} = P.R.C.$$

w.L.	15.6	291.8
+1	14.5	292.9
crb	12.4	295.0
'4	11.3	296.1
+5	10.7	296.7
8	9.3	298.1
M	8.5	298.9
'4	8.0	299.4
crb	8.0	299.4
E.L.	8.4	299.0

$$\left. \begin{array}{l} A 42^{\circ} 40' \\ R 680' \\ L 506.33 \\ Defl' = 0.0921299 \end{array} \right\} \text{ East}$$

$$\left. \begin{array}{l} A 42^{\circ} 40' \\ R 780' \\ L 580.84 \\ Defl' = 0.036728^{\circ} \end{array} \right\} \text{ West}$$

Chords 25' on East & 28.675' West Radial Lines for all x-sections  
0+25 on East

E.L.	8.3	299.1
crb	8.1	299.3
'4	8.0	299.4
M	8.7	298.7
'4	9.9	297.5
crb	11.2	296.2
w.L.	13.9	293.5
T.P.	9.99	306.93
	10.44	296.94



306.93

0450

W.L.	11.9	295.0
crk	10.9	296.0
1/4	9.6	297.3
+ 13	7.2	299.7
M	7.8	299.1
1/4	7.3	299.6
crk	7.4	299.5
E.L.	7.9	299.0

0475

E.L.	7.6	299.3
crk	7.2	299.7
1/4	7.2	299.7
M	7.4	299.5
1/4	9.2	299.7
crk	9.5	297.4
W.L.	9.7	297.2

55

140

W.L.	6.4	300.5
crk	6.7	300.2
1/4	7.2	299.7
M	7.1	299.8
1/4	6.7	300.2
crk	6.7	300.2
E.L.	7.4	299.5

1425

E.L.	6.6	300.3
crk	6.2	300.7
1/4	6.0	300.9
M	6.5	300.4
1/4	6.5	300.4
crk	6.1	300.8
W.L.	5.8	301.1



1+60<sup>20</sup> = 0.5 E.L. 1+84<sup>20</sup> = M.L. = M.L. Penn<sup>20</sup>

W.L.	5.8	301.1
erb	5.6	301.3
"4	4.9	302.0
M	4.8	302.1
"4	4.9	302.0
erb	5.5	301.4
E.L.	6.0	300.9

North curb

E.L.	5.7	301.2
erb	5.2	301.7
"4	4.6	302.3
M	4.7	302.2
"4	5.3	301.6
erb	5.8	301.1
W.L.	6.1	300.8

56

N "4

W.L.	6.3	300.6
erb	5.8	301.1
"4	5.6	301.3
M	4.9	302.0
"4	4.4	302.5
erb	5.0	301.9
E.L.	5.4	301.5

Center

E.L.	4.4	302.5
"7	5.2	301.7
erb	4.9	302.0
"4	4.3	302.6
M	5.0	301.9
"4	5.5	301.4
erb	6.0	300.9
W.L.	6.6	300.3



Sec. 14

W.L.	6.3	300.6
crk	5.8	301.1
1/4	5.6	301.3
M	4.9	302.0
1/4	4.3	302.6
crk	4.8	302.1
+7	4.7	302.2
E.L.	3.7	303.2

Sec curl

E.L.	3.8	303.1
+11	4.7	302.2
crk	4.8	302.1
1/4	4.5	302.4
M	5.0	301.9
1/4	5.5	301.4
crk	5.8	301.1
W.L.	6.3	300.6

S. L. Penna

57

W.L.	6.9	300.0
crk	6.2	300.7
1/4	5.5	301.4
M	5.0	301.9
1/4	4.6	302.3
crk	4.9	302.0
+5	4.8	302.1
E.L.	4.0	302.9

x-sec "E" = crk of curve & going south

E.L.	4.1	302.8
+12	4.9	302.0
crk	5.0	301.9
1/4	4.7	302.2
M	5.1	301.8
1/4	6.0	300.9
crk	6.0	300.9
W.L.	6.2	300.7



306.93

0+25 on E.L. Sec. of X-sec "E"

W.L.	6.7	300.2
erb	6.2	300.7
1/4	6.2	300.7
M	5.7	301.2
1/4	5.0	301.9
erb	5.2	301.7
+9	5.0	301.9
E.L.	4.3	302.6

0+50

E.L.	5.1	301.8
erb	5.4	301.5
1/4	5.3	301.6
M	6.1	300.8
+10	5.7	301.2
1/4	6.0	300.9
erb	6.4	300.5
W.L.	7.2	299.7

58

0+75

W.L.	7.6	299.3
erb	6.4	300.5
1/4	6.3	300.6
M	6.2	300.7
1/4	5.6	301.3
erb	5.5	301.4
E.L.	5.2	301.7

1+0

E.L.	5.5	301.4
erb	5.7	301.2
1/4	5.8	301.1
M	6.7	300.2
1/4	7.1	299.8
erb	7.1	299.8
+8	7.4	299.5
W.L.	8.5	298.4



306.93

1+25

W.L.	8.9	298.0
erb	8.2	298.7
1/4	7.5	299.4
M	6.7	300.2
1/4	6.1	300.8
erb	5.8	301.1
E.L.	5.1	301.8

1+50

E.L.	5.7	301.2
erb	6.2	300.7
1/4	6.4	300.5
M	7.2	299.7
1/4	8.2	298.7
erb	8.3	298.6
W.L.	9.0	297.9

T.P.	7.05	305.01	8.77	297.96
------	------	--------	------	--------

1+75

W.L.	7.2	297.8
erb	6.6	298.4
1/4	6.5	298.5
M	5.7	299.3
1/4	4.7	300.3
erb	4.7	300.3
E.L.	3.9	301.1

305.01  
305.01

59

2+0

E.L.	3.6	301.4
+10	4.9	300.1
erb	4.8	300.2
1/4	4.7	300.3
M	5.5	299.5
1/4	6.7	298.3
erb	6.7	298.3

W.L.	7.4	297.6
------	-----	-------

2+25

W.L.	7.4	297.6
erb	7.1	297.9
1/4	6.8	298.2
M	5.6	299.4
1/4	4.7	300.3
erb	4.9	300.1
+6	4.6	301.4

E.L.	3.7	301.3
------	-----	-------

2+53<sup>19</sup> on E 2+90<sup>47</sup> on W = P.C. 10' N of N.L. Cypress st

E.L.	3.7	301.3
erb	4.7	300.3
1/4	4.8	300.2
M	5.3	299.7
1/4	6.4	298.6
erb	7.2	297.8
W.L.	7.4	297.6



N.L. Cypress St 60' wide 10' walks 10' 1/4's

W.L.	7.7	297.3
crk	7.1	297.9
1/4	6.4	298.6
M	5.3	299.7
1/4	4.9	300.1
crk	5.1	299.9
E.L.	4.7	300.9

N. curb

E.L.	6.1	298.9
crk	5.6	299.4
1/4	4.9	300.1
M	5.4	299.6
1/4	6.1	298.9
crk	7.2	297.8
W.L.	8.1	296.9

N 1/4

W.L.	8.4	296.6
crk	7.3	297.7
1/4	6.0	299.0
M	5.4	299.6
1/4	5.0	300.0
crk	5.6	299.4
E.L.	6.3	298.7

Center

E.L.	6.4	298.6
crk	5.7	299.3
1/4	5.1	299.9
M	5.4	299.6
1/4	6.0	299.0
crk	7.2	297.8
W.L.	8.3	296.7

S 1/4

W.L.	8.6	296.4
crk	6.8	298.2
1/4	5.9	299.1
M	5.3	299.7
1/4	5.0	300.0
crk	5.9	299.1
E.L.	6.6	298.4

S curb

E.L.	6.6	298.4
crk	5.4	299.6
1/4	5.0	300.0
M	5.1	299.9
1/4	5.5	299.5
crk	6.4	298.6
W.L.	8.1	296.9



305.01

## S.L. Cypress

W.L.	7.2	297.8
ck	6.0	299.0
1/4	5.5	299.5
M	5.1	299.9
1/4	5.0	300.6
ck	5.3	299.7
E.L.	4.8	300.2

## 0+50 Sof S.L. Cypress

E.L.	4.3	300.7
ck	4.9	300.1
1/4	5.1	299.9
M	5.1	299.9
1/4	5.9	299.1
ck	6.1	298.9
W.L.	7.2	297.8

1+0

W.L.	6.9	298.1
ck	6.8	298.2
1/4	5.7	299.3
M	5.1	299.9
1/4	5.2	299.8
ck	4.4	300.6
E.L.	4.2	300.8

305.01

1+50

L

E.L.	5.1	299.9
ck	5.0	300.0
1/4	5.2	299.8
M	5.4	299.6
1/4	6.2	298.8
ck	7.1	297.9
W.L.	7.4	297.6

2+0

W.L.	8.2	296.8
ck	7.7	297.3
1/4	6.6	298.4
M	5.7	299.3
1/4	5.6	299.4
ck	5.7	299.3
E.L.	4.7	300.3

T.P. 2.45 303.09 4.37 300.64

+50

E.L.	3.0	300.1
ck	3.3	299.8
1/4	3.8	299.3
M	4.0	299.1
1/4	4.7	298.4
ck	5.5	297.6
W.L.	6.4	296.7

61



303.09

3+0

w.L.	6.3	296.8
crk	5.8	297.3
"4	5.0	298.1
M	4.2	298.9
"4	4.1	299.0
crk	3.5	299.6

E.L.	2.5	300.6
------	-----	-------

3+19<sup>44</sup> = N.L. Brooks 60 wide 10' 1/2  
10' walk

E.L.	3.1	300.0
crk	4.2	298.9
"4	4.3	298.8
M	4.4	298.7
"4	5.2	297.9
crk	5.7	297.4
w.L.	6.6	296.5

N. curb

w.L.	8.2	294.9
crk	6.2	296.9
"4	5.3	297.8
M	4.5	298.6
"4	4.3	298.8
crk	4.3	298.8
E.L.	3.4	299.7

62

N "4

F.L.	3.7	299.4
crk	4.3	298.8
"4	4.4	298.7
M	4.6	298.5
"4	5.5	297.6
crk	6.1	297.0
w.L.	8.3	294.8

CENTER

w.L.	8.2	294.9
crk	6.3	296.8
"4	5.6	297.5
M	4.7	298.4
"4	4.4	298.7
crk	4.4	298.7
E.L.	3.7	299.4

S. "4

E.L.	3.8	299.3
crk	4.5	298.6
"4	4.5	298.6
M	4.7	298.4
"4	5.7	297.4
crk	6.5	296.6
w.L.	8.4	294.7



## S. curl

W.L.	8.0	295.1
curl	6.8	296.3
"A	5.7	297.4
M	4.7	298.4
"A	4.6	298.5
curl	4.7	298.4
E.L.	3.9	299.2

## S.L. Brooks

E.L.	4.1	299.0
curl	4.9	298.2
"A	4.6	298.5
M	4.7	298.4
"A	5.8	297.3
curl	6.7	296.4
W.L.	6.7	296.4

## 0.50 Sev. of Brooks

W.L.	7.5	295.6
curl	7.1	296.0
"A	6.2	296.9
M	5.1	298.0
"A	5.2	297.9
curl	5.1	298.0
E.L.	4.7	298.4

140

E.L.	4.6	298.5
curl	4.8	298.3
"A	5.5	297.6
M	5.2	297.9
"A	6.3	296.8
curl	6.8	296.3
W.L.	7.5	295.6

1450

W.L.	7.1	296.0
curl	7.3	295.8
"A	6.3	296.8
M	5.3	297.8
"A	5.5	297.6
curl	5.8	297.3
E.L.	5.3	297.8

240

E.L.	6.5	296.6
curl	6.4	296.7
"A	5.6	297.5
M	5.3	297.8
"A	6.2	296.9
curl	7.7	295.4
W.L.	8.0	295.1



303.09

2+50

W.L.	7.1	296.0
erb	7.0	296.1
1/4	6.4	296.7
M	5.6	297.5
1/4	5.9	297.2
erb	6.8	296.3
E.L.	5.8	297.3

T.P.	4.28	302.22	5.15	297.94
------	------	--------	------	--------

3+0

E.L.	4.9	297.3
erb	5.3	296.9
1/4	4.9	297.3
M	4.6	297.6
1/4	5.5	296.7
erb	6.2	296.6
W.L.	6.3	295.9

3+19.7<sup>2</sup> = W.L. Myrtle 60 wide 10 walks 10 1/4 5

W.L.	6.3	295.9
erb	6.2	296.0
1/4	5.4	296.8
M	4.6	297.6
1/4	4.8	297.4
erb	5.4	296.8
E.L.	5.2	297.0

302.22

64

North Curve

E.L.	5.3	296.9
erb	5.4	296.8
1/4	4.9	297.3
M	4.6	297.6
1/4	5.3	296.9
erb	6.1	296.1
W.L.	6.0	296.2

N 1/4

W.L.	6.1	296.1
erb	5.8	296.4
1/4	5.3	296.9
M	4.6	297.6
1/4	4.8	297.4
erb	5.3	296.9
E.L.	5.3	296.9

Center

E.L.	5.2	297.0
erb	5.3	296.9
1/4	4.8	297.4
M	4.6	297.6
1/4	5.2	297.0
erb	5.7	296.5
W.L.	6.4	295.8



30222

Sou. 14

W.L.	6.4	295.8
crk	5.7	296.5
14	5.2	297.0
M	4.6	297.6
14	4.7	297.5
crk	5.1	297.1
E.L.	5.0	297.2

Sou Crk

E.L.	5.0	297.2
crk	4.9	297.3
14	4.7	297.5
M	4.6	297.6
14	5.3	296.9
crk	5.8	296.4
W.L.	6.7	295.5

S.L. Myrtle

W.L.	6.7	295.5
crk	6.2	296.0
14	5.3	296.9
M	4.6	297.6
14	4.7	297.5
crk	4.8	297.4
E.L.	5.0	297.2

65

0+50 S. of S.L. Myrtle

E.L.	4.8	297.4
crk	5.0	297.2
14	4.8	297.4
M	4.6	297.6
14	5.3	296.9
crk	6.7	295.5
W.L.	7.0	295.2

1+0

W.L.	7.3	294.9
crk	7.1	295.1
14	5.7	296.5
M	4.9	297.3
14	5.0	297.2
crk	5.3	296.9
E.L.	5.2	297.0

1+50

E.L.	5.3	296.9
crk	5.2	297.0
14	5.1	297.1
M	5.1	297.1
14	5.8	296.4
crk	6.6	295.6
W.L.	6.9	295.3



302.22

270

W.L.	6.6	295.6
Crk	6.6	295.6
1/4	5.9	296.3
M	4.9	297.3
1/4	5.1	297.1
Crk	5.3	296.9
E.L.	5.2	297.0

T.P.	4.59	301.63	5.18	297.04
------	------	--------	------	--------

2750

E.L.	4.4	297.2
Crk	4.5	297.1
1/4	4.5	297.1
M	4.4	297.2
1/4	5.2	296.4
Crk	5.6	296.0
W.L.	5.9	295.7

370

W.L.	5.6	296.0
Crk	5.6	296.0
1/4	5.2	296.4
M	4.6	297.0
1/4	4.7	296.9
Crk	5.0	296.6
E.L.	5.5	296.1

301.63

66

3+35<sup>15</sup> on E.L. 2. 3+35<sup>21</sup> W.L. = N.L. Upas 50' wide 10' walk 137<sup>1/2</sup> 1/4<sup>5</sup>

E.L.	6.2	295.4
------	-----	-------

Crk	5.3	296.3
-----	-----	-------

1/4	4.9	296.7
-----	-----	-------

M	4.8	296.8
---	-----	-------

1/4	5.3	296.3
-----	-----	-------

Crk	5.8	295.8
-----	-----	-------

W.L.	5.8	295.8
------	-----	-------

N Crk

W.L.	5.8	295.8
------	-----	-------

Crk	5.6	296.0
-----	-----	-------

1/4	5.3	296.3
-----	-----	-------

M	4.9	296.7
---	-----	-------

1/4	4.9	296.7
-----	-----	-------

Crk	5.2	296.4
-----	-----	-------

E.L.	6.2	295.4
------	-----	-------



30163

N 14

E.L.	6.4	295.2
erb	5.4	296.2
14	5.0	296.6
M	4.9	296.7
14	5.3	296.3
erb	5.7	295.9
W.L.	5.9	295.7

Center

W.L.	6.0	295.6
erb	5.9	295.7
14	5.4	296.2
M	5.0	296.6
14	5.1	296.5
erb	5.6	296.0
E.L.	6.6	295.0

67

S 14

E.L.	6.7	294.9
erb	5.9	295.7
14	5.2	296.4
M	5.2	296.4
14	5.5	295.1
erb	6.0	295.6
W.L.	6.0	295.6

S. curb

W.L.	5.9	295.7
erb	6.0	295.6
14	5.6	296.0
M	5.3	296.3
14	5.3	296.3
erb	6.1	295.5
E.L.	7.1	294.5



S.L. UP23 = N.L. Balboa Park

E.L.	7.1	294.5
erb	4.3	295.3
"4	5.6	296.0
M	5.5	296.1
"4	5.6	296.0
erb	5.9	295.7
N.L.	6.0	295.6

295.73 m E Apt pole.

68

294.00

12.62

306.62 H.I.

10.91

295.71 D.P.

5.17

300.88

line of parking  
Aseline upus

58.9'  
20.7'



300.88 K-I

So. line 2 pas.

W. line Park  
Blvd.

5.2

5.1

4.7

C

4.6

4.7

5.2

E line

6.3

5' 20.

E. cb.

4.80

E. gutter

5.35

4.95

C

4.78

4.97

W gutter

5.32 295.56

W. cb.

4.76

about 30' walk  
+ 15' gutters

69

25' 20.

W. cb.

5.26

W. gutter

5.80 295.08

5.43

C

5.24

5.40

E gutter

5.85

E. cb.

5.20



29<sup>th</sup> St X Sec Kalmia South

5-29-26  
Miller

BM 0.69 286.77 286.08 S.E. cor 29<sup>th</sup> + Kalmia

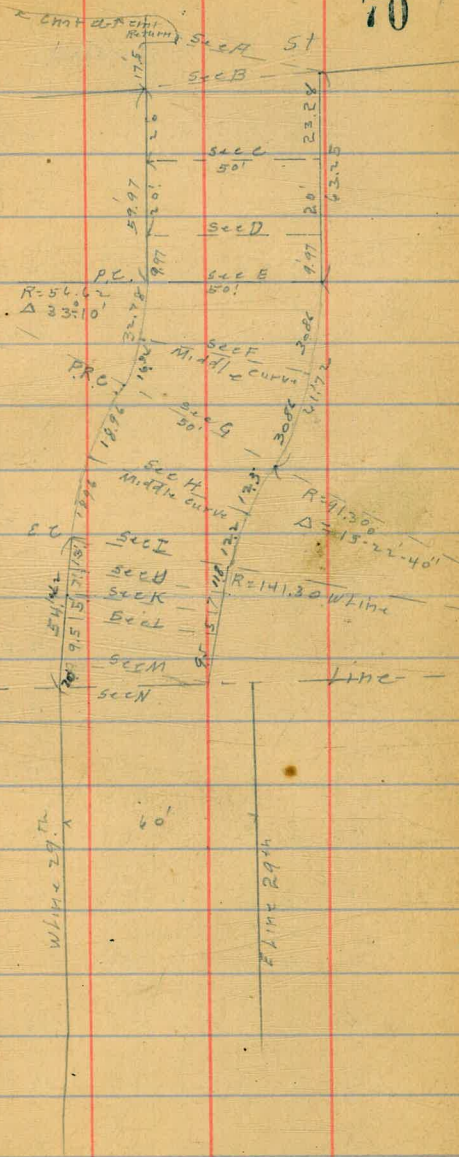
	Sec A		
whim	1.5	285.3	
w d	1.61	285.16	cmt el
1/4	1.6	285.2	
c	1.3	285.5	
1/4	1.4	285.4	
cl	0.95	285.82	cmt el

Sec B = S. Line Kalmia

E	1.8	285.0	
E cl	0.95	285.82	
1/4	1.7	285.1	
c	1.9	284.9	
1/4	1.9	284.9	
2/5	1.9	284.9	
cl	1.2	285.6	
w	1.4	285.4	
	Sons Robson W. = Sec C		
w	3.0	283.8	
cl	3.0	283.8	
1/4	3.1	283.7	

Kalmia St

70





286.77

Sec C (cont)

e	3.1	283.7	
1/4	3.0	283.8	
el	2.6	284.2	
+8	2.5	284.3	
e	1.4	285.4	on lawn
5" e 40' son W = Sec D			
E	2.2	284.6	on lawn
+2	3.3	283.5	
el	4.2	282.6	
1/4	4.6	282.2	
c	4.4	282.2	
1/4	4.8	282.0	
el	4.8	282.0	
W	4.5	282.3	

59.97 son W

63.25 S. E.

Sec E = P.C.

W	5.9	280.9	
el	4.5	280.3	
1/4	6.6	280.2	
c	4.4	280.4	
1/4	6.2	280.6	

286.77

71

el	5.1	281.7	
+8	4.2	282.6	
E	2.8	284.0	on lawn

ctr Curve Δ P6-35 = Sec F

E	5.4	281.2	
el	6.8	280.0	
+2	7.8	279.0	
1/4	8.0	278.8	
c	8.3	278.5	
1/4	8.4	278.4	
el	7.8	279.0	
+6	7.0	279.8	
W	9.5	277.3	
+10	18.0	268.8	
+25	20.3	266.5	

P.R.C. = Sec G

-25	23.2	263.6	
-7	21.0	265.8	
W	16.3	270.5	
el	9.3	277.5	



286.77

P.R.e. (con)

14		9.7	277.1	
e		10.3	276.5	
14		10.2	276.6	
cl		10.0	276.8	
+6		9.4	277.4	
E		8.5	278.3	
A Triangulation Curve = Sec H				
E		9.2	277.6	
+4		10.4	276.4	
cl		10.9	275.9	
14		11.4	275.4	
c		10.8	276.0	
14		10.3	276.5	
+3.5		10.1	276.7	
cl		12.6	274.2	
T.P.	0.86	277.07	10.56	276.21
N		10.5	266.6	
+13		19.2	257.9	
+30		23.0	254.1	

277.07

E.C. = Sec I.

72

-25		17.0	258.1	
-13		15.0	262.1	
N		10.2	267.9	
cl		3.1	274.0	
+2		2.3	274.8	
14		2.1	275.0	
e		2.4	274.7	
14		2.7	274.4	
cl		2.2	274.9	
E		2.20	274.87	on all-paving
13.5 of Sec I. = Sec J.				
e		3.1	274.0	
cl		3.5	273.6	
14		3.5	273.6	
c		3.6	273.5	
14		3.1	274.0	
cl		3.4	273.5	
N		6.2	270.9	
+15		11.5	265.6	



277.07

20' s of Sec I = Sec K = S. line Alley on E

- 10	8.9	268.2
w	6.4	270.7
cl	4.3	272.8
"4	3.8	273.3
c	4.2	272.9
"4	3.9	273.2
cl	3.4	273.7
E	3.1	274.0

E end Alley not paving same 2.80 274.3

25' S. of Sec I = Sec L.

E+7 = E cl of 29 <sup>th</sup> to S.	3.10	273.97	cont'd
+10 = cl	3.6	273.5	
"4	4.0	273.1	
c	4.5	272.6	
"4	4.4	272.7	
cl	4.3	272.8	
w	5.2	270.9	

277.07

34.5 S of Sec I = Sec M = P.L. on E

73

w	5.5	271.6
cl	5.1	272.0
"4	5.5	271.6
c	5.1	272.0
"4	4.6	272.5
cl	4.0	273.1
gutter	3.8	273.3
+6 = E cl of 29 <sup>th</sup> to South	3.40	273.5
sec N = P.L. 29 <sup>th</sup> St	10' wide 10' ELS 10' 44	

E cl	3.45	273.62	
gutter	4.1	273.0	
"4	4.2	272.9	
c	5.1	272.0	
"4	5.7	271.4	
gutter	6.0	271.1	
cl	5.50	271.6	cont'd
w	5.7	271.4	



80' wide  
14' elev  
13' 1/4"

JUNIPER ST  
X Sec. Granada West

6-22-24  
miller

237.61

74

B.M.	0.89	288.90		288.01	SE. Dak. Juniper	cb	9.1	228.5
T.P.	0.10	276.12	12.88	276.02		+1	8.0	229.6
T.P.	0.05	263.55	12.62	263.50		N	7.6	230.0
T.P.	0.12	250.55	13.12	250.43				
							90' W	
		W. Line Granada				N	9.9	227.7
s dirt el			10.6	240.0	chk	+12	10.2	227.4
N. end el			8.6	242.0	chk	cb	11.6	226.0
T.P.	0.10	237.61	13.04	237.51		+6	10.7	226.9
		45.0 W = W. end. end walk + el at N.				14	10.7	226.9
N. end el			2.70	234.9		c	11.4	226.2
s dirt el			4.7	232.9		14	12.1	225.5
		77' W of W. Line Granada				+4	12.4	225.2
S.			7.9	229.7	end walk to house	+5	14.2	223.4
+5			9.8	227.8		cb	14.4	223.2
cb			10.3	227.3		+1	12.3	225.3
+1			11.9	225.7		S	11.8	225.8
+5			10.4	227.2				
114			9.8	227.8		S	13.3	224.3
c			9.0	228.6		+6	14.2	223.4
114			8.6	229.0		cb	16.4	221.0

100' W



237.61

100' W (cont)

+5	16.0	221.6
+6	14.1	223.5
1/4	13.4	224.2
0	12.4	225.2
1/4	12.1	225.5
+7	12.4	225.2
+10	13.8	223.8
cl	11.8	225.8
N	11.6	226.0
+5	11.6	226.0
T.P.	2.64 228.11	12.18 225.43

114' W

-5	5.6	222.5
N	5.7	222.4
+10	5.5	222.6
cl	7.3	220.8
+5	4.7	223.4
1/4	3.5	224.6
0	3.2	224.9
1/4	4.3	223.8

228.11

75

cl	6.0	222.1
+1	7.9	220.2
5	9.5	218.6
+10	9.1	219.0

119' W

-15	9.6	218.5
-2	11.3	216.8
5	7.6	220.5
cl	5.9	222.2
1/4	4.2	223.9
0	3.2	224.9
1/4	4.6	223.5
+11	6.2	221.9
cl	8.9	219.2
+5	6.8	221.3
N	7.0	221.1
+5	6.8	221.3

125' W

-5	8.8	219.3
N	8.7	219.4



228.11

125'W (CON)

+8	8.8	219.3
+12	10.5	217.6
cl	10.3	217.8
+2	8.8	219.3
114	8.2	219.9
c	4.8	223.3
+4	4.0	224.1
114	4.2	223.9
cl	5.9	222.7
S	8.1	220.0

145'W

S	8.9	219.2		
d	11.0	217.1		
TP	3.60	218.71	13.00	215.11
114	4.7	214.0		
c	5.2	213.5		
114	5.5	213.2		
cl	5.5	213.2		
+2	5.6	213.1		
+3	7.9	210.8		

218.71

76

+9	7.8	210.9
+11	6.1	212.6
N	5.9	212.8
+5	6.2	212.5

170'W

-10	11.6	207.1
N	11.7	207.0
+5	15.2	203.5
+4	12.5	206.2
cl	11.9	206.8
114	12.4	206.3
c	12.6	206.1
114	12.4	206.3
cl	12.3	206.4
S	11.7	207.0
+5	11.6	207.1



77



Gregory  
Miller  
Foulston

Grades in Alley Bk 3 Galder Hill

EL 25th

No.	So.
184.38	184.14
192.01	184.78 ✓
195.5	185.42 ✓
196.2	186.06 ✓
196.23	186.69 ✓
197.43	187.33 ✓
197.80	187.97 ✓
198.77	188.73 ✓
* 199.6	189.5 ✓
199.15	189.15 ✓
198.87	189.57 ✓
198.58	189.58 ✓
198.29	189.29 ✓
* 198	189 ✓
197.16	189.16 ✓
196.38	186.38 ✓
195.31	185.31 ✓
* 184.3	184.3 ✓
183.5	183.5 ✓
182.5	182.5
* 181.6	181.5 changed to 181.1
180.90	180.89 ✓
180.27	180.27
181.0	180.96

EL 24th

120.26	184.14	184.28	185.01	184.78	185.42	185.5	186.2	186.23	186.29	186.38	186.39	186.69	187.33	187.80	188.77	189.6	189.15	189.87	189.58	189.29	189	189.16	186.38	185.31	184.3	183.5	182.5	181.6	180.90	180.27	181.0																																																																										
16.7	5.61	5.24	4.62	4.55	4.21	4.07	3.91	3.87	3.84	3.80	3.76	3.72	3.68	3.64	3.60	3.56	3.52	3.48	3.44	3.40	3.36	3.32	3.28	3.24	3.20	3.16	3.12	3.08	3.04	3.00	2.96	2.92	2.88	2.84	2.80	2.76	2.72	2.68	2.64	2.60	2.56	2.52	2.48	2.44	2.40	2.36	2.32	2.28	2.24	2.20	2.16	2.12	2.08	2.04	2.00	1.96	1.92	1.88	1.84	1.80	1.76	1.72	1.68	1.64	1.60	1.56	1.52	1.48	1.44	1.40	1.36	1.32	1.28	1.24	1.20	1.16	1.12	1.08	1.04	1.00	0.96	0.92	0.88	0.84	0.80	0.76	0.72	0.68	0.64	0.60	0.56	0.52	0.48	0.44	0.40	0.36	0.32	0.28	0.24	0.20	0.16	0.12	0.08	0.04	0.00



Curb Levels on Grove St - A St North 6-22-26  
mille.

B.M. 3.98 231.00 227.02 S.P. A + 30"  
I.P. on B.M. 5.69 230.22 6.47 224.53 = 224.16 Curb Settled

S. of Line of A St

W. Line Grove 5.16 w 506 cmt. cl  
E " " 5.90 w 432 cmt. cl  
Settled, below grade

N. of Line of A St

E. Line Grove 4.74 w 548 cmt. cl  
W " " 4.15 w 607 " "

N. Line of A St

W. of Line Grove 4.17 w 605 " "  
E. of Line " 4.69 w 553 " "

50' N of N Line of A Break

E. of Grove 4.82 w 540 cmt. cl  
W " " 4.57 w 665 " "

65' N = Break

W. of Grove 4.67 w 555 cmt. cl  
E " " 4.78 w 544 " "

S. Line of A St

E. of Grove 1.15 " "  
W " " 0.14 " "

Handwritten calculations and notes on the right page, including various numbers and small diagrams. Includes a large number '79' in the top right corner.

45.00	46.15	46.30	46.45	46.60	46.75	46.90	47.05	47.20	47.35	47.50	47.65	47.80	47.95	48.10	48.25	48.40	48.55	48.70	48.85	49.00	49.15	49.30	49.45	49.60	49.75	49.90	50.05	50.20	50.35	50.50	50.65	50.80	50.95	51.10	51.25	51.40	51.55	51.70	51.85	52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	53.50	53.65	53.80	53.95	54.10	54.25	54.40	54.55	54.70	54.85	55.00	55.15	55.30	55.45	55.60	55.75	55.90	56.05	56.20	56.35	56.50	56.65	56.80	56.95	57.10	57.25	57.40	57.55	57.70	57.85	58.00	58.15	58.30	58.45	58.60	58.75	58.90	59.05	59.20	59.35	59.50	59.65	59.80	59.95	60.10	60.25	60.40	60.55	60.70	60.85	61.00	61.15	61.30	61.45	61.60	61.75	61.90	62.05	62.20	62.35	62.50	62.65	62.80	62.95	63.10	63.25	63.40	63.55	63.70	63.85	64.00	64.15	64.30	64.45	64.60	64.75	64.90	65.05	65.20	65.35	65.50	65.65	65.80	65.95	66.10	66.25	66.40	66.55	66.70	66.85	67.00	67.15	67.30	67.45	67.60	67.75	67.90	68.05	68.20	68.35	68.50	68.65	68.80	68.95	69.10	69.25	69.40	69.55	69.70	69.85	69.95	70.00
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------



69  
100  
6900

354.43 B.M. Kansas & Main

Cypress to Brooks	319.44	299.05	
Brooks to Myrtle	319.72	291.10	
Myrtle to UP25 (50') on west	<del>338.41</del>	307.10	
" " " " " East	<del>338.15</del>	307.10	
	306.93	95	300.21
	6.75		
	300.18		26
	3.19		286.75
			17.47
	319	307.84	274.22
	127	17.47	308
	25		
	77	223.3	
	100	1276	290.47
	110	3.19	278.07
			0.89
			288.90
			11.82
			276.12
Brooks to Myrtle	319.72	276.12	295.67
	302.42		295.73
	6.65		
	305.68		
		4.51	2565
15' N - Break			
W. of Grove	4.47	2555	cmt
E. " "	4.78	2544	"
S. line Fish St			
E. of Grove	1.15		"
W. " "	0.14		"

336.05  
29.36  
365.41

260 10000 3.64 270.12  
780 9.07  
2200 267.05  
2080 1.92

336.05 36  
29.10 184 250.55 1200 38  
35.15 8.71 1040 2  
291.84 1600 76

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.00	7.15	7.30	7.45	7.60	7.75	7.90	8.05	8.20	8.35	0
1	8.50	8.65	8.80	8.95	9.10	9.25	9.40	9.55	9.70	9.85	1
2	10.00	10.15	10.30	10.45	10.60	10.75	10.90	11.05	11.20	11.35	2
3	11.50	11.65	11.80	11.95	12.10	12.25	12.40	12.55	12.70	12.85	3
4	13.00	13.15	13.30	13.45	13.60	13.75	13.90	14.05	14.20	14.35	4
5	14.50	14.65	14.80	14.95	15.10	15.25	15.40	15.55	15.70	15.85	5
6	16.00	16.15	16.30	16.45	16.60	16.75	16.90	17.05	17.20	17.35	6
7	17.50	17.65	17.80	17.95	18.10	18.25	18.40	18.55	18.70	18.85	7
8	19.00	19.15	19.30	19.45	19.60	19.75	19.90	20.05	20.20	20.35	8
9	20.50	20.65	20.80	20.95	21.10	21.25	21.40	21.55	21.70	21.85	9
10	22.00	22.15	22.30	22.45	22.60	22.75	22.90	23.05	23.20	23.35	10
11	23.50	23.65	23.80	23.95	24.10	24.25	24.40	24.55	24.70	24.85	11
12	25.00	25.15	25.30	25.45	25.60	25.75	25.90	26.05	26.20	26.35	12
13	26.50	26.65	26.80	26.95	27.10	27.25	27.40	27.55	27.70	27.85	13
14	28.00	28.15	28.30	28.45	28.60	28.75	28.90	29.05	29.20	29.35	14
15	29.50	29.65	29.80	29.95	30.10	30.25	30.40	30.55	30.70	30.85	15
16	31.00	31.15	31.30	31.45	31.60	31.75	31.90	32.05	32.20	32.35	16
17	32.50	32.65	32.80	32.95	33.10	33.25	33.40	33.55	33.70	33.85	17
18	34.00	34.15	34.30	34.45	34.60	34.75	34.90	35.05	35.20	35.35	18
19	35.50	35.65	35.80	35.95	36.10	36.25	36.40	36.55	36.70	36.85	19
20	37.00	37.15	37.30	37.45	37.60	37.75	37.90	38.05	38.20	38.35	20
21	38.50	38.65	38.80	38.95	39.10	39.25	39.40	39.55	39.70	39.85	21
22	40.00	40.15	40.30	40.45	40.60	40.75	40.90	41.05	41.20	41.35	22
23	41.50	41.65	41.80	41.95	42.10	42.25	42.40	42.55	42.70	42.85	23
24	43.00	43.15	43.30	43.45	43.60	43.75	43.90	44.05	44.20	44.35	24
25	44.50	44.65	44.80	44.95	45.10	45.25	45.40	45.55	45.70	45.85	25
26	46.00	46.15	46.30	46.45	46.60	46.75	46.90	47.05	47.20	47.35	26
27	47.50	47.65	47.80	47.95	48.10	48.25	48.40	48.55	48.70	48.85	27
28	49.00	49.15	49.30	49.45	49.60	49.75	49.90	50.05	50.20	50.35	28
29	50.50	50.65	50.80	50.95	51.10	51.25	51.40	51.55	51.70	51.85	29
30	52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	30
31	53.50	53.65	53.80	53.95	54.10	54.25	54.40	54.55	54.70	54.85	31
32	55.00	55.15	55.30	55.45	55.60	55.75	55.90	56.05	56.20	56.35	32
33	56.50	56.65	56.80	56.95	57.10	57.25	57.40	57.55	57.70	57.85	33
34	58.00	58.15	58.30	58.45	58.60	58.75	58.90	59.05	59.20	59.35	34
35	59.50	59.65	59.80	59.95	60.10	60.25	60.40	60.55	60.70	60.85	35
36	61.00	61.15	61.30	61.45	61.60	61.75	61.90	62.05	62.20	62.35	36
37	62.50	62.65	62.80	62.95	63.10	63.25	63.40	63.55	63.70	63.85	37
38	64.00	64.15	64.30	64.45	64.60	64.75	64.90	65.05	65.20	65.35	38
39	65.50	65.65	65.80	65.95	66.10	66.25	66.40	66.55	66.70	66.85	39
40	67.00	67.15	67.30	67.45	67.60	67.75	67.90	68.05	68.20	68.35	40

Calculated by F. E. Paradis, C. F.



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
 ROADWAY 16 FEET WIDE. SIDE SLOPES 1½ TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4

Calculated by F. E. Paradis. C. E.

Handwritten calculations and notes on the right page of the notebook. Includes various numbers, fractions, and a circular stamp for Eugene Dietzgen Co. The stamp text reads: "EUGENE DIETZGEN CO. MANUFACTURERS & IMPORTERS OF DRAWING MATERIALS AND SURVEYING INSTRUMENTS NEW YORK, CHICAGO, NEW ORLEANS & SAN FRANCISCO".

Handwritten notes include:

- 90.4, 214.68, 290, 228, 272, 690, 2395
- 37.5, 207.21, 41.5, 380, 43, 310, 690, 510
- 1.86, 1488, 548, 327, 360
- 90.5208, 1100, 3, 75, 360
- 225, 1800, 3.5, 359.3
- 330, 675, 330, 1925, 58, 315, 330, 315
- 300, 1200, 10.3, 218.2, 5.45
- 250, 1750, 38, 555.8, 360, 915.8
- 19, 1900, 265.7, 110, 127.2, 300, 318
- 633, 180, 1940, 127.2, 220, 318
- 176, 12, 268.7, 800, 6.36, 97, 37
- 16, 576, 750, 1000, 173, 300
- 180, 422.5, 76, 75, 134.5
- 100, 24, 865, 173, 259.5
- 24, 2424, 104, 6000, 3.15, 280, 2712, 2704, 1345, 2766, 4628, 1179.83
- 4032, 208, 2550, 2420, 2442, 26048
- 1200, 21893, 9860, 615, 2550, 2420, 1592, 8270, 7960, 23, 8, 184
- 100, 55, 308, 2420, 1592, 8270, 7960, 23, 8, 184
- 170, 49, 100, 6.4, 8270, 7960, 23, 8, 184
- 667, 1757, 4669, 333, 667, 104719
- 80, 63, 4.64, 15, 487