

888  
F.B.

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LEVEL BOOK.

No. 410 T

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Magnolia Pg 52

MICROFILMED

DEC 15 1964

EUGENE DIETZGEN CO.,

Drawing Materials and Surveying Instruments.

NEW YORK.

CHICAGO.

SAN FRANCISCO.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.  
 DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
 ROADWAY 20 FEET WIDE. SIDE SLOPES 1 TO 1.  
 FOR SINGLE TRACK EXCAVATION.

Copyright, 1902. No. 39370.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	0
1	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	1
2	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	2
3	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	3
4	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	4
5	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	5
6	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	6
7	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	7
8	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	8
9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	9
10	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	10
11	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	11
12	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	12
13	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	13
14	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	14
15	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	15
16	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	16
17	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	17
18	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	18
19	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	19
20	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	20
21	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	21
22	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	22
23	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	23
24	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	24
25	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	25
26	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	26
27	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	27
28	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	28
29	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	29
30	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	30
31	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	31
32	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	32
33	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	33
34	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	34
35	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	35
36	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	36
37	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	37
38	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	38
39	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	39
40	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	40

Calculated by F. E. Paradis, C. E.



CROSS-SECTIONS  
 EPSILON STREET  
 ETA: 80' wide, 14' Walks, 13' 1/4's.

T.P. Tie Pt. 40 & Epsilon. 53.03

1.28 54.31

T.P. 12.85 41.46

1.80 43.26

W.L. Porters Add.

N.L. 66 36.7

C 7.0 36.3

1/4 7.0 36.3

£ 6.4 36.9

1/4 6.2 37.1

C 6.1 37.2

SL 6.1 37.2

21.92 E. Porters W.L. 40 Produced.

SL 84 34.9

C 88 34.5

1/4 88 34.5

£ 87 34.6

1/4 95 33.8

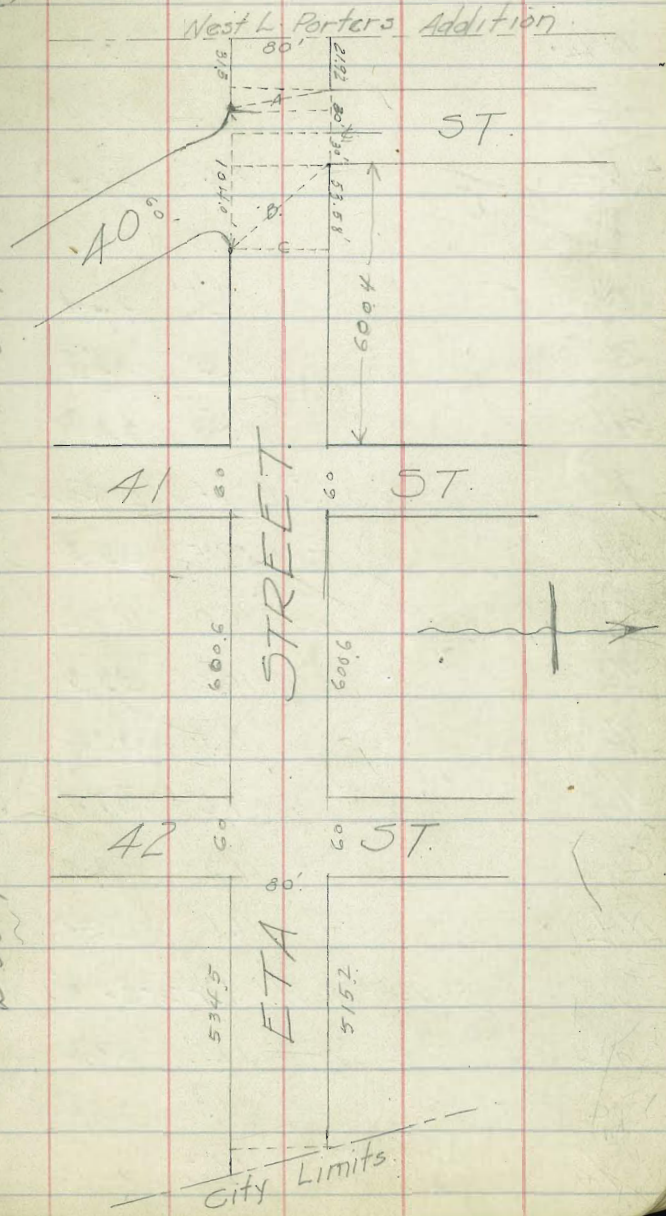
£ 98 33.5

N.L. 99 33.4

Add One foot to all elevations, as error of 1 ft.

is carried forward from book 880, all through.

April-15-1913.  
 West.  
 Evans  
 Moore.



4326

31.5 E on S - 24.92 E on N.

Sec A.

N.L.	9.9	33.4
C	10.3	33.0
1/4	10.0	33.3
Φ	9.3	34.0
1/4	9.5	33.8
C	9.6	33.7
S.L.	9.5	33.8

31.5 E. of W.L. Porters Add

S.L.	9.5	33.8
C	10.0	33.3
1/4	10.0	33.3
Φ	10.7	32.6
1/4	11.6	31.7
C	11.3	32.0
N.L.	11.1	32.2

51.92 E of W.L. Porters - Φ - 40 Prod.

N.L.	11.0	32.3
C	11.9	31.4
1/4	12.3	31.0

4326

3

Φ	12.0	31.3
1/4	11.9	31.4
C	12.1	31.2
S.L.	11.6	31.7
Φ	15.3	28.0
C	15.3	28.0
1/4	14.8	28.5
Φ	14.0	29.3

81.92 E of W.L. Porters Add - 40 Prod.

1/4	12.7	30.6
C	11.1	32.2
N.L.	9.2	34.1

NE Hub. Car-40+ctd.

T.P. tube used for 40 St Xlines 9.22 34.04

Sec. B. = 81.92 E of Porters. on N.L.  
135.5 " " " " S.L.

N.L.	9.2	34.1
C	10.7	32.6
1/4	12.8	30.5
Φ	13.5	29.8
1/4	13.7	29.6
C	13.6	29.7
S.L.	12.7	30.6

43.26

Sec. C 53.58' E of E.L. 40 St.

S.L.	12.7	30.6
C	12.1	31.2
1/4	11.8	31.5
Φ	11.2	32.1
1/4	10.5	32.8
C	10.1	33.2
N.L.	18.9	34.4

100' E. 40 St.

N.L.	4.0	39.3
C	4.2	39.1
1/4	4.0	39.3
Φ	4.2	39.1
1/4	5.0	38.3
C	6.3	37.0
S.L.	7.5	35.8

125' E

S.L.	3.7	39.6
C	2.2	41.1
1/4	0.9	42.4

43.26

4

Φ	0.8	42.5
1/4	0.4	42.9
C	0.5	42.8
N.L.	0.4	42.9
T.P.	0.69	42.57

652 49.09'

150' E

N.L.	3.8	45.3
C	4.0	45.1
1/4	4.4	44.7
Φ	4.3	44.8
1/4	5.2	43.9
C	5.8	43.3
S.L.	6.7	42.4

175' E

S.L.	4.6	44.5
C	4.5	44.6
1/4	3.7	45.4
Φ	3.7	45.4
1/4	3.4	45.7

49.09

N.C.	29	46.2
N.L.	26	46.5
200'E.		
N.L.	1.7	47.4
C	1.5	47.6
1/4	2.2	46.9
⊕	3.2	45.9
1/4	3.0	46.1
C	3.5	45.6
S.L.	3.8	45.3
250'E.		
S.L.	4.7	44.4
C	3.8	45.3
1/4	3.0	46.1
⊕	2.8	46.3
1/4	2.6	46.5
C	3.1	46.0
N.L.	3.2	45.9

49.09  
300'E.

N.L.	3.7	45.4
C	4.0	45.1
1/4	4.4	44.7
⊕	5.0	44.1
1/4	5.3	43.8
C	6.3	42.8
S.L.	7.2	41.9
350'E.		
S.L.	8.2	40.9
C	7.3	41.8
1/4	6.4	42.7
⊕	6.1	43.0
1/4	4.9	44.2
C	4.2	44.9
N.L.	3.7	45.4
400'E.		
N.L.	4.5	44.6
C	5.4	43.7
1/4	6.4	42.7

4909

£		7.0	42.1
1/4		7.1	42.0
C		8.0	41.1
S.L.		9.4	39.7

450'E.

S.L.		16.0	39.1
C		15.6	33.5
1/4		14.3	34.8
£		13.7	35.4
1/4		13.0	36.1
C		12.4	36.7
NL.		11.5	37.6

T.P.	391	41.25	11.75	37.34
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475'E.

NL		6.5	34.8
C		8.2	33.1
1/4		8.8	32.5
£		9.8	31.5
1/4		10.6	30.7
C		12.0	29.3
SL		12.6	28.7
420		13.3	28.0

4125

500'E.

-20		17.3	24.0
SL		16.6	24.7
C		15.1	26.2
1/4		14.6	26.7
£		14.4	26.9
1/4		12.1	29.2
1/4		10.9	30.4
NL		9.4	31.9
+20		8.8	32.5

525'E.

-20		6.5	34.8
NL		7.5	33.8
C		8.5	32.8
1/4		9.1	32.2
£		8.9	32.4
1/4	~	9.3	32.0
C		11.4	29.9
SL		14.2	27.1
+20		16.7	24.6

6



4125

550'E.

-20	15.8	25.5
5L	12.8	28.5
C	8.7	32.6
1/4	5.4	35.9
⊕	4.3	37.0
1/4	4.7	36.6
C	5.6	35.7
NL	5.2	36.1
+20	4.0	37.3

575'E.

NL	2.8	38.5
C	2.3	39.0
1/4	2.2	39.1
⊕	2.6	38.7
1/4	4.3	37.0
C	7.7	33.6
5L	11.1	30.3
+20	14.5	26.8

4125

W.L. 41ST. 60' Wide  
10' Walks + 1/4 5.

-20	15.1	26.2	
5L	11.4	29.9	309
C	8.0	33.3	343
1/4	5.4	35.9	369
⊕	3.9	37.4	384
1/4	2.9	38.4	394
C	1.7	39.6	406
NL	2.0	39.3	403

W. Curb.

NL	1.9	39.4	
C	1.3	40.0	
1/4	3.0	38.3	
⊕	4.5	36.8	
1/4	5.5	35.8	
C	7.9	33.4	
5L	11.2	30.1	
+20	14.9	26.4	

4125

W/4

-20	14.9	26.4	
SL	11.0	30.3	
C	7.5	33.8	
1/4	4.7	36.6	
ϕ	4.6	36.7	
1/4	3.1	38.2	
C	1.7	39.6	
NL	2.2	39.1	
Tie Pt. 41+ Etd.			
T.P. to be used for X Secs 41st.			
	1.88	39.37	
	ϕ 425+ 41		
N.L	2.8	38.5	395
C	3.5	37.8	388
1/4	4.3	37.0	380
ϕ	4.8	36.5	375
1/4	5.2	36.1	371
C	7.7	33.6	346
SL	11.0	30.3	313
+20	15.4	25.9	

4125

E/4

8

-20	15.4	25.9	
SL	11.7	29.6	
C	8.6	32.7	
1/4	6.3	35.0	
ϕ	5.9	35.4	
1/4	4.9	36.4	
C	4.1	37.2	
NL	3.4	37.9	
	E. Curb.		
NL	4.8	36.5	
C	5.1	36.2	
1/4	6.2	35.1	
ϕ	7.3	34.0	
1/4	8.5	32.8	
C	10.0	31.3	
SL	12.1	29.2	
+20	14.9	26.4	

41.25

E.L. 41st.

-20	14.8	26.5	
SL	12.0	29.3	303
C	10.4	30.9	31.9
1/4	9.6	31.7	32.2
1/4	8.4	32.9	33.9
1/4	7.3	34.0	35.0
C	5.9	35.4	36.4
NL	5.6	35.7	36.7

25'E 41st.

N.L	10.0	31.3	
C	10.6	30.7	
1/4	11.0	30.3	
1/4	11.7	29.6	
1/4	12.1	29.2	
C	12.4	28.9	
SL	13.0	28.3	
+20	14.1	27.2	

41.25

50'E.

9

-20	15.9	25.4	
SL	15.1	26.2	
C	14.5	26.8	
1/4	13.7	27.6	
1/4	12.8	28.5	
1/4	12.7	28.6	
C	12.5	28.8	
NL	11.8	29.5	
-20	11.2	30.1	

T.P.	7.79	36.89	12.15	29.10
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75'E.

-10	7.9	29.0	
NL	9.0	27.9	
C	9.8	27.1	
1/4	10.4	26.5	
1/4	10.9	26.0	
1/4	11.3	25.6	
C	12.0	24.9	
SL	12.7	24.2	
+10	13.2	23.7	

36.89

100'E

-10	13.8	23.1
SL	13.2	23.7
C	13.0	23.9
1/4	13.0	23.9
⊕	12.4	24.5
1/4	11.6	25.3
C	10.7	26.2
NL	10.6	26.3
+10	9.8	27.1

125'E

-10	10.4	26.5
NL	11.0	25.9
C	11.5	25.4
1/4	12.5	24.4
⊕	13.0	23.9
1/4	13.7	23.2
C	14.9	22.0
SL	18.9	18.0
+10	22.0	14.9

36.89

150'E

-10	18.1	18.8
SL	18.4	18.5
+5	22.4	14.5
+10	20.2	16.7
C	20.2	16.7
1/4	17.6	19.3
⊕	15.7	21.2
+10	13.0	23.9
1/4	12.8	24.1
C	12.0	24.9
NL	11.1	25.8
+10	10.7	26.2

175'E

-10	11.7	25.2
NL	11.8	25.1
C	12.3	24.6
1/4	13.4	23.5
⊕	13.9	23.0
+3	14.3	22.6
1/4	17.6	19.3
+8	20.0	16.9
C - bottom hole	24.5	12.4
SL	17.2	19.7
+10	18.3	18.6

10

3689

200'E.

-10	19.0	17.9
-4	19.2	17.7
SL	22.0	14.9
+4 = ditch bot.	23.5	13.4
C	18.7	18.2
1/4	15.2	21.7
1/4	14.8	22.1
1/4	14.0	22.9
C	13.4	23.5
NL	12.7	24.2
+10	12.6	24.3

225'E.

-10	13.2	23.7
NL	13.6	23.3
C	14.1	22.8
1/4	14.5	22.4
1/4	15.2	21.7
1/4	15.5	21.4
C	15.9	21.0
SL	17.5	19.4
+15 = bot. ditch.	22.0	14.9

3689

250'E.

-10	18.0	18.9
SL	16.8	20.1
C	16.5	20.4
1/4	16.0	20.9
1/4	15.6	21.3
1/4	15.0	21.9
C	14.7	22.2
NL	14.1	22.8
+10	13.6	23.3

275'E.

-10	13.3	23.6
NL	13.8	23.1
C	14.7	22.2
1/4	15.2	21.7
1/4	15.5	21.4
1/4	16.2	20.7
C	16.6	20.3
SL	17.3	19.6
+10	17.8	19.1

11

3689

300'E

-10	17.2	19.7
SL	17.0	19.9
C	16.4	20.5
1/4	15.7	21.2
ϕ	15.0	21.9
1/4	14.9	22.0
C	14.1	22.8
NL	13.2	23.7
+10	12.4	24.5

325'E

-10	10.5	26.4
NL	12.0	24.9
C	13.0	23.9
1/4	13.6	23.3
ϕ	14.0	22.9
1/4	14.9	22.0
C	15.6	21.3
SL	16.3	20.6
+10	16.9	20.0

3689

350'E

-10	15.8	21.1
SL	15.1	21.8
C	14.2	22.7
1/4	13.3	23.6
ϕ	13.0	23.9
1/4	12.3	24.6
C	11.5	25.4
NL	10.3	26.6
+10	9.2	27.7

375'E

-10	7.3	29.6
NL	7.7	29.2
C	8.3	28.6
1/4	8.9	28.0
ϕ	10.0	26.9
1/4	11.3	25.6
C	12.7	24.2
SL	14.1	22.8
+10	14.7	22.2

12

36.89

400'E

-10	12.9	24.0
SL	12.2	24.7
C	10.6	26.3
1/4	9.4	27.5
ϕ	8.1	28.8
1/4	6.7	30.2
C	5.0	31.9
NL	4.3	32.6
+10	4.8	32.1

425'E

-10	2.9	34.0
NL	2.6	34.3
C	2.8	34.1
1/4	3.3	33.6
ϕ	3.5	33.4
1/4	4.4	32.5
C	6.1	30.8
SL	7.9	29.0
+10	9.0	27.9

36.89

450'E

-10	5.6	31.3
SL	4.1	32.8
C	3.0	33.9
1/4	2.1	34.8
ϕ	1.9	35.0
1/4	1.5	35.4
C	0.9	36.0
NL	0.5	36.4

475'E

NL	0.4	36.5
C	1.0	35.9
1/4	1.1	35.8
ϕ	1.5	35.4
1/4	1.9	35.0
C	2.1	34.8
SL	2.8	34.1

13

36.89

500'E

SL	2.2	34.7
C	1.8	35.1
1/4	1.7	35.2
ϕ	1.8	35.1
1/4	1.1	35.8
C	0.6	36.3
NL	0.1	36.8
T.P	1.70	35.19

45.9 39.78

525'E

NL	3.7	36.1
C	4.9	34.9
1/4	6.4	33.4
ϕ	7.3	32.5
1/4	7.1	32.7
C	6.8	33.0
S.L	7.2	32.6
H0	8.0	31.8

39.78

550'E

-10	11.3	28.5
SL	10.7	29.1
C	10.2	29.6
1/4	10.7	29.1
ϕ	10.1	29.7
1/4	8.5	31.3
C	7.1	32.7
N.L	6.0	33.8
+10	4.6	35.2

575'E

-10	7.5	32.3
NL	8.5	31.3
C	10.5	29.3
1/4	11.6	28.2
ϕ	12.8	27.0
1/4	14.0	25.8
C	14.2	25.6
SL	15.0	24.8
+10	15.3	24.5

14



39.78  
 W.L. 42nd St.

60' Wide  
 10' Walks + 43'

-10	16.1	23.7
SL	16.0	23.8
C	15.2	24.6
1/4	14.6	25.2
Φ	14.2	25.6
1/4	13.8	26.0
C	13.0	26.8
NL	11.5	28.3
+	10.0	

W. Curb.

NL	12.4	27.4
C	13.7	26.1
1/4	13.8	26.0
Φ	14.2	25.6
1/4	14.7	25.1
C	15.0	24.8
SL	15.3	24.5
+	15.8	24.0

39.78

W 1/4

15

-10	15.8	24.0
SL	15.3	24.5
C	14.7	25.1
1/4	14.4	25.4
Φ	14.2	25.6
1/4	14.0	25.8
C	13.9	25.9
NL	13.2	26.6

Φ 42 St

NL	13.1	26.7
C	13.5	26.3
1/4	12.7	27.1
Φ	13.6	26.2
1/4	14.4	25.4
C	14.5	25.3
SL	15.0	24.8
+	15.4	24.4

39.78

E 1/4

-10.	14.9	24.9
SL	14.5	25.3
C	13.4	26.4
1/4	13.1	26.7
1/4	12.8	27.0
1/4	12.4	27.4
C	12.8	27.0
NL	13.0	26.8

E. Curb.

NL	12.7	27.1
C	12.3	27.5
1/4	11.9	27.9
1/4	11.9	27.9
1/4	12.0	27.8
C	12.4	27.4
SL	13.2	26.6
H0	13.8	26.0

39.78

E. L. 42 St.

16

-10	13.3	26.5
SL	12.5	27.3
C	11.1	28.7
1/4	10.6	29.2
1/4	10.3	29.5
1/4	10.3	29.5
C	11.1	28.7
NL	12.1	27.7

Tie Point for 42 X Sess. 12.99 26.79

25' E

NL	9.7	30.1
C	7.6	32.2
1/4	6.5	33.3
1/4	7.1	32.7
1/4	7.6	32.2
C	9.3	30.5
SL	10.6	29.2
+10	11.8	28.0

39.78

50'E

-10	10.7	29.1
SL	9.1	30.7
C	7.3	32.5
1/4	5.4	34.4
E	4.3	35.5
1/4	4.4	35.4
C	4.9	34.9
NL	6.3	33.5

75'E

NL	3.4	36.4
C	1.5	38.3
1/4	1.5	38.3
E	2.3	37.5
1/4	3.9	35.9
C	6.0	33.8
SL	7.8	32.0
+10	9.7	30.1

39.78

100'E

-10	8.4	31.4
SL	6.4	33.4
C	4.0	35.8
1/4	1.9	37.9
E	0.1	39.7
T.P.	0.39	39.39

11.01 50 H0

N/4	9.7	40.7
C	10.0	40.4
NL	11.3	39.1
+10	12.5	37.9

125'E

NL	9.1	41.3
C	7.4	43.0
1/4	8.0	42.4
E	9.5	40.9
1/4	11.5	38.9
C	13.5	36.9
SL	15.2	35.2
+10	17.1	33.3

17

5040

150'E

-10	16.1	34.3
SL	13.8	36.6
C	12.1	38.3
<del>1/4</del>	9.6	40.8
1/4	7.9	42.5
1/4	6.8	43.6
C	6.6	43.8
NL	7.8	42.6

175'E

NL	7.3	43.1
C	6.5	43.9
1/4	6.0	44.4
1/4	7.0	43.4
1/4	9.1	41.3
C	11.7	38.7
SL	13.9	36.5
f	15.1	35.3

5040

200'E

-10	13.9	36.5
SL	13.0	37.4
C	10.8	39.6
1/4	9.2	41.2
1/4	7.8	42.6
1/4	6.8	43.6
C	6.8	43.6
NL	7.3	43.1

225'E

NL	6.9	43.5
C	7.1	43.3
1/4	7.4	43.0
1/4	9.2	41.2
1/4	10.6	39.8
C	11.2	39.2
SL	12.0	38.4
f	12.9	37.5

18

5040

250'E

SL	10.5	39.9
C	10.5	39.9
1/4	10.1	40.3
ϕ	8.9	41.5
1/4	7.5	42.9
C	6.8	43.6
NL	5.4	45.0

275'E

NL	4.9	45.6
C	6.4	44.0
1/4	6.7	43.7
ϕ	7.5	42.9
1/4	8.2	42.2
C	9.5	40.9
SL	9.8	40.6
H0	9.9	40.5

5040

300'E

-10	9.2	41.2
SL	9.2	41.2
C	8.6	41.8
1/4	7.5	42.9
ϕ	7.0	43.4
1/4	6.2	44.2
C	5.3	45.1
NL	4.5	45.9

325'E

NL	3.4	47.0
C	4.2	46.2
1/4	5.1	45.3
ϕ	5.4	45.0
1/4	6.2	44.2
C	6.7	43.7
SL	7.4	43.0
H0	8.4	42.0

19

5040

350'E.

-10	7.2	43.2
SL	6.6	43.8
C	6.1	44.3
1/4	4.8	45.6
ϕ	4.3	46.1
1/4	4.6	45.8
C	3.5	46.9
NL	3.0	47.4

375'E.

NL	2.5	47.9
C	2.9	47.5
1/4	4.3	46.1
ϕ	4.3	46.1
1/4	5.0	45.4
C	5.7	44.7
SL	6.2	44.2
+10	6.8	43.6

5040

400'E.

SL	5.9	44.5
C	5.4	45.0
1/4	5.1	45.3
ϕ	4.7	45.7
1/4	4.2	46.2
C	3.4	47.0
NL	2.2	48.2

425'E.

NL	3.2	47.2
C	3.8	46.6
1/4	3.7	46.7
ϕ	3.7	46.7
1/4	4.6	45.8
C	5.4	45.0
SL	5.7	44.7

20

5040

450'E.

SL	56	44.8
C	5.1	45.3
1/4	4.5	45.9
1/4	4.3	46.1
1/4	4.5	45.9
C	4.4	46.0
NL	4.4	46.0

475'E.

NL	4.2	46.2
C	5.1	45.3
1/4	6.0	44.4
1/4	6.8	43.6
1/4	7.7	42.7
C	8.3	42.1
SL	9.6	40.8
T.P. Mon. City/Lim.	5.91	44.49

0.10 44.59

44.59

on SL

21

510'E. - Edge fill Co Road.

SL	4.4	40.2
C	3.4	41.2
1/4	2.5	42.1
1/4	1.4	43.2
1/4	0.6	44.0
C	0.0	44.6
NL	7.0	45.6

515.2'E = City Lim. on N.L.

SL	6.9	37.7
C	6.7	37.9
1/4	6.3	38.3
1/4	6.0	38.6
1/4	4.3	40.3
C	2.3	42.3
NL	0.1	44.5

44.59  
 Sec. on City Lim. being  
 515.2' E. on N.L. + 534.5' E. on S.L.

N.L.	0.1	44.5
C	3.5	41.1
1/4	6.6	38.0
1/4	9.0	35.6
1/4	10.8	33.8
C	13.0	31.6
S.L.	14.2	30.4

Non. City Lim

44.49

12.80 57.29

N.L. Epsilon + City Lim	5.8	51.5	51.5
Gr.			
S.L. " " " "	3.0	54.3	54.4

checks O.K.



CROSS-SECTIONS  
 42nd St.  
 60' Wide, 10' Walks + 1/4's.

April 15 - 1913.  
 West  
 Moore  
 Evans.

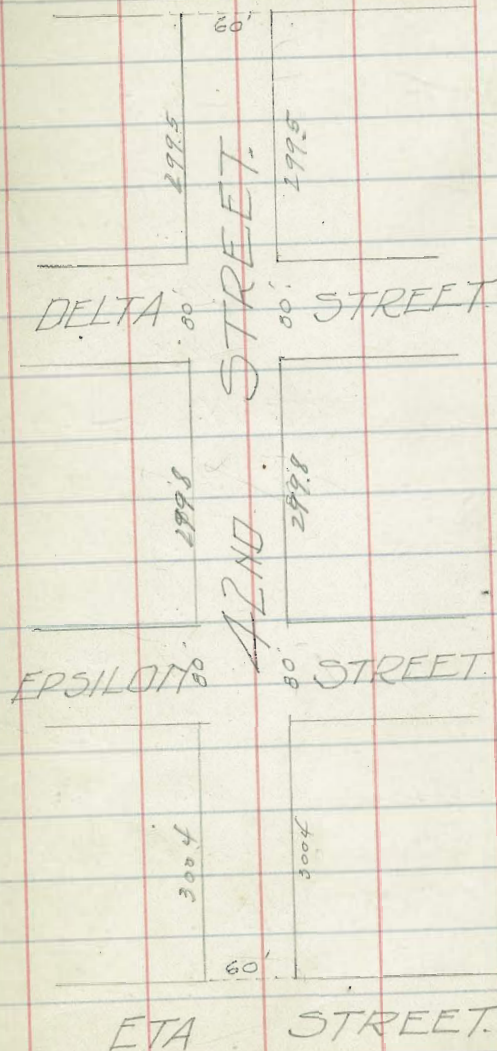
See note p. 2

Tie pt. 42+Epsilon 26.79  
 12.94 39.73

N.L. Eta St.

WL	11.4	28.3
C	12.3	27.4
1/4	13.1	26.6
1/4	13.1	26.6
1/4	13.0	26.7
C	12.7	27.0
E.L.	12.1	27.6
25' E		
EL	12.0	27.7
C	12.1	27.6
1/4	12.2	27.5
1/4	11.4	28.3
1/4	10.8	28.9
C	9.7	30.0
WL	7.9	31.8

GAMMA ST.



39.73

50' N of N.L. Etg.

W.L.	6.0	33.7
C	7.4	32.3
1/4	8.5	31.2
2	9.6	30.1
1/4	9.9	29.8
C	10.7	29.0
E.L.	10.6	29.1

76' N.

E.L.	10.0	29.7
C	9.6	30.1
1/4	9.1	30.6
2	8.1	31.6
1/4	6.9	32.8
C	5.8	33.9
W.L.	4.6	35.1

100' N.

W.L.	2.9	36.8
C	3.7	36.0
1/4	4.7	35.0

39.73

24

2	5.7	34.0
1/4	6.7	33.0
C	7.4	32.5
E.L.	8.2	31.5
+5	7.5	30.2
+10	8.4	31.3
+12	8.3	31.4

125' N.

-10	6.1	33.6
-5	8.8	30.9
E.L.	8.8	30.9
+2	6.5	33.2
C	5.6	34.1
1/4	4.4	35.3
2	3.5	36.2
1/4	2.3	37.4
C	1.2	38.5
W.L.	0.1	39.8

39.73

150' N.

-10	4.1	35.6
EL.	7.7	32.0
+4	4.4	35.3
C	3.6	36.1
1/4	2.3	37.4
⊖	1.3	38.6
1/4	0.1	39.6
T.P.	2.26	37.47

12.74 50.21

C	9.4	40.8
W.L.	8.2	42.0

175' N.

W.L.	5.3	44.9
C	6.5	43.7
1/4	8.4	41.8
⊖	9.8	40.4
1/4	11.7	38.5
C	13.0	37.2
+9	13.9	36.3
EL.	17.0	33.2

50.21

25

-10

13.4 36.8

200' N.

-10	12.0	38.2
-5	15.4	34.8
EL.	12.3	37.9
C	11.4	38.8
1/4	10.3	39.9
⊖	8.3	41.9
1/4	6.3	43.9
C	4.8	45.4
W.L.	3.6	46.6

225' N.

W.L.	0.8	48.4
C	3.2	47.0
1/4	5.1	45.1
⊖	7.3	42.9
1/4	9.8	40.4
C	10.7	39.5
+9	11.4	38.8
EL.	13.8	36.4
+10	10.3	39.9

5021

250' N.

-10	10.3	39.9
E.L.	10.7	39.5
C	10.8	39.4
1/4	9.9	40.3
⊕	8.1	42.1
1/4	6.0	44.2
C	3.6	46.6
W.L.	0.7	49.5

275' N.

W.L.	2.7	47.5
C	5.3	44.9
1/4	6.9	43.3
⊕	8.8	41.4
1/4	9.7	40.5
C	10.3	39.9
E.L.	9.6	40.6
+10	8.7	41.5

5021

26

S.L. Epsilon.

E.L.	8.8	41.4
C	9.8	40.4
1/4	8.8	41.4
⊕	7.3	42.9
1/4	6.4	43.8
C	5.2	45.0
W.L.	4.4	45.8

N.L. Epsilon.

W.L.	5.8	44.4
C	7.0	43.2
1/4	7.8	42.4
⊕	8.2	42.0
1/4	8.1	42.1
C	6.6	43.6
E.L.	6.1	44.1

50.21

25' N. Epsilon

EL.	4.5	45.7
C	5.2	45.0
1/4	6.1	44.1
ϕ	7.0	43.2
1/4	7.3	42.9
C	7.3	42.9
W.L.	6.8	43.4

50' N.

W.L.	6.0	44.2
C	6.0	44.2
1/4	4.5	45.7
ϕ	4.4	45.8
1/4	4.0	46.2
C	3.2	47.0
EL.	2.7	47.5

75' N.

EL.	0.2	50.0
C	1.2	49.0
1/4	1.7	48.5

50.21

27

ϕ	2.7	47.5
1/4	3.0	47.2
C	4.0	46.2
W.L.	4.8	45.4
T.P.	1.13	49.08

12.16 61.24

-10

100' E.

W.L.	13.9	47.3
	14.2	47.0
C	13.1	48.1
1/4	12.2	49.1
ϕ	12.0	49.2
1/4	11.3	49.9
C	10.1	51.7
EL.	8.7	52.5

125' E.

-10

W.L.

C

1/4

ϕ

1/4

	13.2	48.0
	12.5	48.7
	11.4	49.8
	10.9	50.3
	11.1	50.1
	10.2	51.0

61.24

C.	8.6	52.6
E.L.	6.2	55.0

150' N.

E.L.	5.9	55.3
C	7.2	54.0

1/4	8.0	51.2
±	9.1	52.1

1/4	9.8	51.4
C	10.3	50.9

W.L.	11.0	50.2
------	------	------

+10	11.9	49.3
-----	------	------

200' N.

-10	8.0	53.2
-----	-----	------

W.L.	7.7	53.5
------	-----	------

C	7.4	53.8
---	-----	------

1/4	7.2	54.0
-----	-----	------

±	6.7	54.5
---	-----	------

1/4	5.8	55.4
-----	-----	------

C	4.7	56.5
---	-----	------

E.L.	4.4	56.8
------	-----	------

61.24

28

250' N.

E/A	0.0	61.2
-----	-----	------

±	0.9	60.3
---	-----	------

1/4	1.5	59.7
-----	-----	------

C	1.5	59.7
---	-----	------

W.L.	2.0	59.2
------	-----	------

+10	2.5	58.7
-----	-----	------

T.P.	0.59	60.65
------	------	-------

12.48 73.13

E. Curb	1.12	61.9
---------	------	------

E.L.	7.7	63.4
------	-----	------

S.L. Delta St.

E.L.	2.7	70.4
------	-----	------

C	3.3	69.8
---	-----	------

1/4	3.6	69.5
-----	-----	------

±	4.0	69.1
---	-----	------

1/4	4.5	68.6
-----	-----	------

C	4.4	68.7
---	-----	------

W.L.	4.5	68.6
------	-----	------

73.13

N.L. Delta St.

WL.	7.9	65.2
C	7.9	65.2
1/4	8.5	64.6
1/2	8.2	64.9
3/4	9.3	63.8
C	10.3	62.8
F.L.	11.2	61.9

25'N.

-15	14.1	59.0
EL.	13.2	59.9
C	12.7	60.4
1/4	12.2	60.9
1/2	11.7	61.4
3/4	11.2	61.9
C	10.7	62.4
WL.	10.4	62.7
+15	9.7	63.4

73.13

50'N.

-15	12.2	60.9
WL.	12.6	60.5
C	13.0	60.1
1/4	13.4	59.7
1/2	13.4	59.7
3/4	13.8	59.3
C	14.2	58.9

EL.	14.9	58.2
+15	15.9	57.2
T.P.	11.62	61.51

12.85 74.36

75'N.

-15	19.5	54.9
EL.	19.1	55.3
C	18.0	56.4
1/4	17.6	56.8
1/2	17.2	57.2
3/4	16.6	57.8
C	15.7	58.7
WL.	15.4	59.0
+15	14.4	60.0

29

74.36

100' N.

-15	14.0	60.4
W.L.	15.0	59.4
C	16.3	58.1
1/4	16.8	57.6
E	17.1	57.3
1/4	18.0	56.4
C	18.2	56.2
E.L.	18.3	56.1
+15	19.1	55.3

150' N.

-15	14.7	59.7
E.L.	14.3	60.1
C	14.1	60.3
1/4	14.2	60.2
E	14.2	60.2
1/4	13.9	60.5
C	13.9	60.5
W.L.	13.1	61.3
+15	12.5	61.9

74.36

200' N.

-15	9.9	64.5
W.L.	10.1	64.3
C	10.0	64.4
1/4	10.1	64.3
E	10.0	64.4
1/4	9.9	64.5
C	9.8	64.6
E.L.	10.1	64.3
+15	10.2	64.2

250' N.

-15	3.4	71.0
E.L.	3.3	71.1
C	3.3	71.1
1/4	4.0	70.4
E	4.6	69.8
1/4	4.8	69.6
C	4.7	69.7
W.L.	4.6	69.8
+15	5.1	69.3

30



7436

T.P.

1.39

72.97

11.40 84.37

5L. Gamma St.

WL.

8.3

76.1

76.1

C

7.9

76.5

1/4

7.9

76.5

C

7.9

76.5

1/4

8.3

76.1

C

8.4

76.0

EL.

8.3

76.1

76.0

Checks, OK

CROSS-SECTIONS  
 A1 STREET  
 60' Wide, 10' Walks + 1/4's.

Mon. Cor A1st  
 & Eta St.

39.37

12.70 52.07

N.L. Eta St.

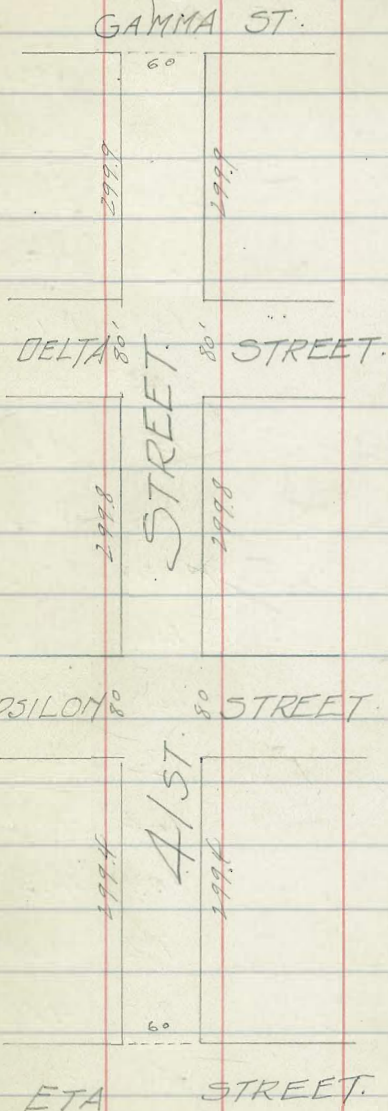
W.L.	12.9	39.2	402
C	12.8	39.3	
1/4	13.0	39.1	
1/4	13.7	38.4	394
C	14.4	37.7	
EL	15.4	36.7	
	16.1	36.0	320
	25' N.		
-15	18.0	34.1	
EL	16.0	36.1	321
C	14.8	37.3	
1/4	14.0	38.1	
1/4	13.2	38.9	399
C	13.0	39.1	
1/4	12.8	39.3	
WL	12.5	39.6	406

April 16-1913.  
 West.  
 Evans.  
 Moore.



See note  
 p. 2

32



5207

50' N.

WL.	11.4	40.7	41.7
C	11.7	40.4	
1/4	11.6	40.5	
Φ	12.0	40.1	41.1
1/4	12.9	39.2	
C	14.0	38.1	
EL	15.0	37.1	38.1
+15	16.0	36.1	3

75' N.

-15	14.4	37.7	
EL	12.9	39.2	40.2
C	12.0	40.1	
1/4	11.2	40.9	
Φ	10.1	42.0	43.0
1/4	9.2	42.9	
C	9.0	43.1	
WL	9.1	43.0	44.0

52.07

33

100' N.

WL	7.5	44.6	45.6
C	8.2	43.9	
1/4	9.3	42.8	
Φ	9.9	42.2	43.2
1/4	10.3	41.8	
C	11.0	41.1	
EL	11.8	40.3	41.3
+15	13.8	38.3	

125' N.

-15	12.8	39.3	
EL	9.8	42.3	43.3
C	9.0	43.1	
1/4	8.9	43.2	
Φ	8.2	43.9	44.9
1/4	7.1	45.0	
C	6.5	45.6	
WL	6.3	45.8	46.8

52.07

150'N.

WL.	4.9	47.2	45.2
C	5.2	47.0	
1/4	6.0	46.1	
⊕	6.8	45.3	46.3
1/4	7.7	44.4	
C	8.8	43.3	
EL.	10.2	41.9	42.9
+15	13.2	38.9	

175'N.

-15	12.3	39.8	
EL	9.9	42.2	43.2
C	7.2	44.9	
1/4	5.9	46.2	
⊕	5.5	46.6	47.6
1/4	5.1	47.0	
C	4.5	47.6	
WL.	3.7	48.4	49.4

52.07

200'N.

WL.	3.9	48.2	49.2
C	4.2	47.9	
1/4	4.4	47.7	
⊕	5.5	46.6	47.6
1/4	6.6	45.5	
C	8.3	43.8	
EL	10.0	42.1	43.1
+15	12.5	39.6	

225'N.

-15	bottom draw.	12.3	39.8
EL.		10.0	42.1
C		7.6	44.5
1/4		5.5	46.6
⊕		3.6	48.5
1/4		2.9	47.2
C		2.7	49.4
WL.		2.8	49.3

50.3

5207

250' N.

W.L.	0.2	51.9	52.9
C	0.9	51.2	
1/4	2.5	49.6	
1/4	4.0	48.1	49.1
1/4	5.5	46.6	
C	6.7	45.4	
E.L.	8.1	44.0	45.0
+15	10.6	41.5	
+20	11.4	40.7	
+30	10.0	42.1	

275' N.

+30 bottom draw.	11.0	41.1	
-15	9.3	42.8	
E.L.	6.1	46.0	47.0
C	4.1	48.0	
1/4	3.7	48.4	
1/4	2.8	49.3	50.3
1/4	2.1	50.0	
C	1.2	50.9	
W.L.	0.4	51.7	52.0

5207

S.L. Epsilon

W.L.	+0.4	52.5	53.8
C	+0.4	52.5	
1/4	+0.1	52.2	
1/4	0.6	51.5	52.8
1/4	1.5	50.6	
C	2.6	49.5	
E.L.	3.9	48.2	49.2
T.P.	0.42	51.65	
	11.64	63.29	
S.W. Cor. 1/4 Epsilon	10.81	52.48	52.53 51.42

N.L. Epsilon

E.L.	9.0	54.3	55.3
C	8.3	55.0	
1/4	7.3	56.0	
1/4	6.2	57.1	58.1
1/4	6.4	56.9	
C	6.2	57.1	
W.L.	6.2	57.1	58.1

35

6329

25'N.

WL.	4.8	58.5	575.
C	5.0	58.3	
1/4	5.4	57.9	
ϕ	5.5	57.8	577
1/4	6.5	56.8	
C	7.7	55.6	
EL.	9.6	53.7	547
+ 40 bottom draw.	14.4	48.9	

50'N.

- 30 bottom.	13.1	50.2	
EL.	9.8	53.5	545
C	8.0	55.3	
1/4	6.7	56.6	
ϕ	5.4	57.9	589
1/4	5.2	58.1	
C	4.8	58.5	
WL.	4.8	58.5	591.5

6329

75'N.

WL.	5.9	57.4	584
C	6.1	57.2	
1/4	6.4	56.9	
ϕ	6.5	56.8	578
1/4	7.7	55.6	
C	8.2	55.1	
EL.	9.3	54.0	550
+ 30 bottom.	12.0	51.3	

100'N.

- bottom.	10.3	53.0	
EL.	8.3	55.0	560
C	7.8	55.5	
1/4	7.2	56.1	
ϕ	6.2	57.1	581
1/4	6.3	57.0	
C	6.0	57.3	
WL.	5.6	57.7	587

86

63.29

125'N.

WL.	3.2	60.1	61.1
C	3.2	60.1	
1/4	4.7	58.6	
ϕ	4.8	58.5	59.5
1/4	5.5	57.8	
C	5.1	58.2	
EL.	5.3	58.0	59.0
+15	6.4	56.9	

150'N.

- N	5.0	58.3	
EL.	3.1	60.2	61.2
C	3.7	59.6	
1/4	3.8	59.5	
ϕ	3.2	60.1	61.1
1/4	3.6	59.7	
C	3.1	60.2	
WL.	3.0	60.3	61.3

63.29

200'N.

WL.	4.2	63.5	64.8
C	0.0	63.3	
1/4	0.3	63.0	
ϕ	0.0	63.3	64.3
1/4	0.5	62.8	
C	0.6	62.7	
EL.	1.0	62.3	63.3
T.P.	0.39	62.90	

12.57 75.47

250'N.

EL.	9.9	65.6	66.4
C	10.1	65.4	
1/4	10.0	65.5	
ϕ	9.2	66.3	67.3
1/4	9.5	66.0	
C	9.5	66.0	
WL.	9.2	66.3	67.3

37

7547

S.L. Delta St.

WL	5.6	69.9	70.9
C	5.7	69.8	
1/4	6.0	69.5	
Φ	5.5	70.0	71.0
1/4	5.9	69.6	
C	5.9	69.6	
EL	5.9	69.6	70.6
T.P.	1.73	73.74	

12.28 86.02

N.L. Delta St.

EL	4.5	81.5	82.5
C <sup>+2</sup>	4.1	81.9	
4.3		81.7	
5.3		80.7	
1/4	5.0	81.0	
Φ	4.5	81.5	82.5
1/4	5.0	81.0	
4.9		81.1	
4.2		81.8	
C	4.5	81.5	
WL	5.0	81.0	82.0

58

86.02

T.P. 1.39 84.63

6.68 91.31

50' N.

WL	4.6	86.7	87.0
C	4.5	86.8	
4.4		86.9	
5.1		86.2	
1/4	4.8	86.5	
Φ	4.0	87.3	88.3
1/4	3.9	87.4	
4.4		86.9	
3.8		87.5	
C	3.7	87.6	
EL	3.5	87.8	88.8

75' N.

EL	1.5	89.8	90.8
C	1.9	89.4	
+2	2.0	89.3	
+3	2.5	88.8	
1/4	2.0	89.3	
Φ	2.0	89.3	90.3
1/4	3.1	88.2	
3.2		88.1	
+2	2.4	88.9	
+3	2.7	88.6	
C	3.0	88.3	89.3
WL			



91.31

100' N.

WL.	3.2	88.1	89.1
C	2.8	88.5	
+7	2.5	88.8	
+8	3.0	88.3	
1/4	2.5	88.8	
∅	1.7	89.6	90.6
1/4	2.0	89.3	
+5	2.2	89.1	
+7	1.7	89.6	
C	1.6	89.7	
EL.	1.5	89.8	90.8

150' N.

EL.	5.9	85.4	86.4
C	6.0	85.3	
+5	6.0	85.3	
+6	6.8	84.5	
1/4	6.3	85.0	
∅	5.4	85.9	86.9
1/4	6.2	85.1	
+3	6.5	84.8	
+4	5.6	85.7	
C	5.7	85.6	
WL	5.5	85.8	86.8

91.31

200' N.

WL.	10.2	81.1	82.1
C	10.4	80.9	
+6	10.2	81.1	
+7	10.8	80.5	
1/4	10.2	81.1	
∅	9.5	81.5	82.5
1/4	10.5	80.8	
+3	11.0	80.3	
+4	10.5	80.8	
C	11.0	80.3	
EL.	11.3	80.0	81.0

250' N.

EL.	16.0	74.3	75.3
C	15.8	75.5	
+7	15.5	75.8	
+8	15.9	75.4	
1/4	15.4	75.9	
∅	14.7	76.6	77.6
1/4	14.5	76.8	
C	14.3	77.0	
WL.	13.8	77.5	78.5

91.31

T.P.

12.23 79.08

3.11 82.19

S.L. Gamma St.

WL.

8.3 73.9 ~~74.1~~  
74.9

C

8.4 73.8

1/4

8.6 73.6

E

8.0 74.2

1/4

8.3 73.9 74.9

C

8.2 74.0

EL.

8.0 74.2 74.3

OK for check.  
28

CROSS SECTIONS  
 40TH ST.  
 60' Wide, 10' Walks + 1/4's.

April - 16, 1913  
 West  
 Evans.  
 Moore.

See note  
 p. 2

41

Hub. NE Cor.  
 40 + Eta.

34.04

12.48 46.52

N.L. Eta Street

EL 12.5 34.0

C 13.0 33.5

1/4 14.0 32.5

ϕ 14.0 32.5

1/4 14.2 32.3

C 13.9 32.6

WL 12.9 33.6

25' N.

WL 13.0 33.5

C 11.9 34.6

1/4 11.4 35.1

ϕ 11.1 35.4

1/4 10.7 35.8

C 10.1 36.4

E.L 10.3 36.2

GAMMA STREET

60'

300.2

300.2

DELTA STREET

80'

80'

300

300

40 ST.

EPSILON STREET

80'

80'

299.3

299.3

60'

ETA STREET

46.52

50'N.

EL. 9.5 37.0

C 9.5 37.0

1/4 10.0 36.5

E 9.8 36.7

1/4 10.2 36.3

C 11.1 35.4

WL 11.6 34.9

75'N.

WL 10.5 36.0

C 10.0 36.5

1/4 9.1 37.4

E 8.9 37.6

1/4 8.6 37.9

C 7.9 38.6

EL 7.6 38.9

100'N.

EL 5.7 40.8

C 5.6 40.9

1/4 6.3 40.2

46.52

42

E 6.9 39.6

1/4 7.8 38.7

C 9.1 37.4

WL 9.4 37.1

125'N.

WL 7.3 39.2

C 7.0 39.5

1/4 6.2 40.3

E 5.0 41.5

1/4 3.8 42.7

C 3.0 44.5

EL 3.3 43.2

150'N.

EL 3.4 43.1

C 3.1 43.4

1/4 3.3 43.2

E 3.8 42.7

1/4 4.4 42.1

C 4.8 41.7

WL 4.6 41.8

46.52

175' N.

WL.	3.9	42.6
C	3.0	43.5
1/4	2.4	44.1
1/2	2.1	44.4
3/4	2.0	44.5
C	1.5	45.0
EL.	1.1	45.4
T.P.	2.45	44.07

13.01 57.08

200' N.

EL.	9.0	48.1
C	9.3	47.8
1/4	10.1	47.0
1/2	10.2	46.9
3/4	10.6	46.5
C	11.6	45.5
WL.	12.2	44.9

57.08

250' N.

WL	7.3	49.8
C	7.3	49.8
1/4	7.1	50.0
1/2	6.8	50.3
3/4	6.4	50.7
C	6.2	50.9
EL.	6.5	50.6

S.L. Epsilon St.

EL.	4.4	52.7
C	5.0	52.1
1/4	5.3	51.8
1/2	5.2	51.9
3/4	5.0	52.1
C	5.3	51.8
WL.	5.5	51.6

Mon 40' Epsilon

4.12 52.96

53.03
52.96
0.07

43

5708

N.L. Epsilon

WL	3.4	53.7
C	3.6	53.5
<del>1/4</del>	3.5	53.6
<del>ϕ</del>	3.2	53.9
<del>1/4</del>	2.8	54.3
C	1.9	55.2
E.L.	0.9	56.2

50' N.

E.L.	0.2	56.9
C	0.3	56.8
<del>1/4</del>	1.2	55.9
<del>ϕ</del>	1.2	55.9
<del>1/4</del>	1.7	55.4
C	2.0	55.1

WL	1.9	55.2
----	-----	------

100' N.

WL	2.0	55.1
C	2.0	55.1
<del>1/4</del>	1.7	55.4

5708

44

<del>ϕ</del>	1.4	55.7
<del>1/4</del>	1.4	55.7
C	0.8	56.3
E.L.	0.1	57.0
T.P.	0.44	56.64

10.89 67.53

150' N.

E.L.	9.2	58.3
C	9.4	58.1
<del>1/4</del>	10.3	57.2
<del>ϕ</del>	10.6	56.9
<del>1/4</del>	11.0	56.5
C	11.3	56.2
WL	11.6	55.9

200' N.

WL	9.4	58.1
C	9.7	57.8
<del>1/4</del>	9.6	57.9
<del>ϕ</del>	9.1	58.4
<del>1/4</del>	9.3	58.2
C	8.8	58.7
E.L.	8.7	58.8

67.53

250' N.

EL.	7.0	60.5
C	7.3	60.2
1/4	7.2	60.3
Φ	7.5	60.0
1/4	7.9	59.6
C	7.9	59.6
WL.	7.7	59.8

S.L. Delta St.

WL.	6.1	61.4
C	6.5	61.0
1/4	6.4	61.1
Φ	6.3	61.2
1/4	6.1	61.4
C	5.7	61.8
E.L.	5.7	61.8

N.L. Delta.

EL.	10	66.5
C	12	66.3
1/4	26	64.9

67.53

45

Φ	3.0	64.5
1/4	3.5	64.0
C	3.8	63.7
WL.	3.7	63.8
T.P.	0.88	66.65

12.57 79.22

50' N.

WL.	12.9	66.3
C	12.3	66.9
1/4	11.7	67.5
Φ	10.9	68.3
1/4	10.9	68.3
C	10.6	68.6
EL.	10.4	68.8

100' N.

EL.	4.8	74.4
C	5.5	73.7
1/4	6.0	73.2
Φ	6.2	73.0
1/4	6.6	72.6
C	7.4	71.8
WL.	8.1	71.1

	79.22		
T.P.		1.59	77.63
	12.85	90.48	
		150'N.	
WL.		11.7	78.8
C		11.2	79.3
1/4		10.4	80.1
⊕		9.7	80.8
1/4		9.2	81.3
C		8.5	82.0
EL.		7.6	82.9
T.P.		0.19	90.29
	9.35	99.64	
		200'N.	
EL.		7.0	92.6
C		7.0	92.6
1/4		7.4	92.2
⊕		7.8	91.8
1/4		8.3	91.3
C		9.1	90.5
WL.		9.6	90.0

	99.64		
		225'N.	
WL.		5.9	93.7
C		5.7	93.9
1/4		5.4	94.2
⊕		5.1	94.5
1/4		5.0	94.6
C		4.8	94.8
EL.		4.6	95.0
		250'N.	
EL.		4.0	95.6
C		4.3	95.3
1/4		4.5	95.1
⊕		4.7	94.9
1/4		4.9	94.7
C		5.0	94.6
WL.		5.1	94.5



9964

275' N.

WL.	5.5	94.1
C	5.3	94.3
1/4	5.2	94.4
1/2	5.1	94.5
3/4	5.0	94.6
C	4.9	94.7
EL.	5.1	94.5

S.L. Gamma St.

EL.	7.1	92.5	92.7
C	7.0	92.6	
1/4	7.1	92.5	
1/2	7.2	92.4	
3/4	7.4	92.2	
C	7.8	91.8	
WL.	8.2	91.4	

$$\frac{715}{270}$$

checks OK.

CROSS-SECTIONS

39TH STREET

N.L. Epsilon to S.L. Gamma.

60' Wide. 10' Walks + 1/4's.

S.W. Cor. 39 + Delta.

44.52

5.71 50.23

N.L. Epsilon.

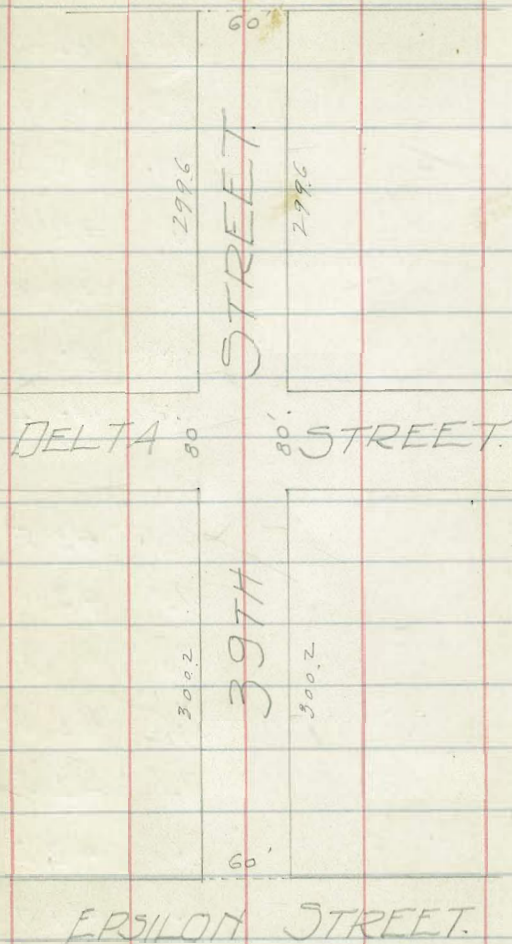
WL	8.5	41.7
C	8.2	42.0
1/4	8.0	42.2
1/2	7.9	42.3
3/4	7.6	42.6
C	7.4	42.8
EL	7.0	43.2
50' N.		
EL	6.4	43.8
C	6.6	43.6
1/4	6.8	43.4
1/2	7.0	43.2
3/4	7.2	43.0
C	7.5	42.7
WL	7.8	42.4

April 16-1913.

West.  
Evans.  
Moore.

48

GAMMA STREET.



5023

100' N.

WL	7.4	42.8
C	7.3	42.9
1/4	7.1	43.1
Φ	6.6	43.6
1/4	6.4	43.8
C	6.3	43.9
EL	6.0	44.2

150' N.

EL	6.7	43.5
C	7.1	43.1
1/4	7.3	42.9
Φ	7.6	42.6
1/4	7.7	42.5
C	8.0	42.2
WL	8.3	41.9

175' N.

WL	7.4	42.8
C	6.7	43.5
1/4	5.8	44.4

5023

49

Φ	5.3	44.9
1/4	5.5	44.7
C	6.0	44.2
EL	6.4	43.8

200' E.

EL	5.6	44.6
C	5.6	44.6
1/4	5.6	44.6
Φ	5.8	44.4
1/4	6.2	44.0
C	6.8	43.4
WL	7.4	42.8

250' E.

WL	7.3	42.9
C	7.1	43.1
1/4	6.8	43.4
Φ	6.1	44.1
1/4	5.4	44.8
C	4.9	45.3
EL	4.8	45.4

5023

## S.L. Delta St.

EL.	4.3	45.9
C	4.6	45.6
1/4	5.0	45.2
Φ	5.4	44.8
1/4	6.0	44.2
C	6.4	43.8
W.L.	6.5	43.7

## N.L. Delta.

WL	4.5	45.7
C	4.8	45.4
1/4	4.2	46.0
Φ	3.8	46.4
1/4	3.7	46.3
C	4.0	46.2
EL.	3.9	46.3

50'N.

EL.	3.4	46.8
C	3.4	46.8
1/4	3.4	46.8

5023

Φ	3.3	46.9
1/4	3.8	46.4
C	3.7	46.5
WL	3.6	46.6

100'N.

WL	2.8	47.4
C	3.0	47.2
1/4	3.0	47.2
Φ	2.6	47.6

1/4	2.6	47.6
C	2.7	47.5
EL.	2.8	47.4

150'N.

EL.	1.7	48.5
C	2.0	48.2
1/4	2.1	48.1
Φ	2.3	47.9
1/4	2.4	47.8
C	2.4	47.8
WL.	2.5	47.7

5023

200' N.

WL.	1.8	48.4
C	1.6	48.6
1/4	1.7	48.5
⊕	1.6	48.6
1/4	1.2	49.0
C	1.2	49.0
EL	1.1	49.1
T.P.	1.58	48.65

4.55 53.20

250' N.

EL.	3.8	49.4
C	3.8	49.4
1/4	4.1	49.1
⊕	4.5	48.7
1/4	4.4	48.8
C	3.9	49.3
WL	4.2	49.0

51

5320

J.L. Gamma St-

EL.	3.4	49.8	49.1
C	3.6	49.6	
1/4	3.7	49.5	
⊕	3.7	49.5	
1/4	3.2	50.0	
C	3.2	50.0	
WL	3.1	50.1	50.0

o.k.

Notch. tel post.

24.78

2.88 27.66

T.P.	9.60	18.06
	5.12	23.18
T.P.	3.59	19.59
	1.98	21.57

B.M. 7.98 13.59 14.60

Note. All elevations to this page are 1 foot low as bench carried forward from book.

880 is 1 ft low. P.S.W.

CROSS SECTIONS

MAGNOLIA STREET

W L State to E L Ictinus  
80' Wide, 14' Walks, 13' / 14'

B.M. NE-Cor State + Ictinus. 133.26

12.63 145.89

EP

145 144.44

8.39 152.83

Sec A

5L

46 148.2

C

3.9 148.9

1/4

3.7 149.1

Q

3.4 149.4

1/4

2.9 149.9

C

1.9 150.9

NL

2.1 150.7

Sec B

NL

5.9 146.9

C

5.6 147.2

1/4

5.2 147.6

Q

5.1 147.7

1/4

4.8 148.0

C

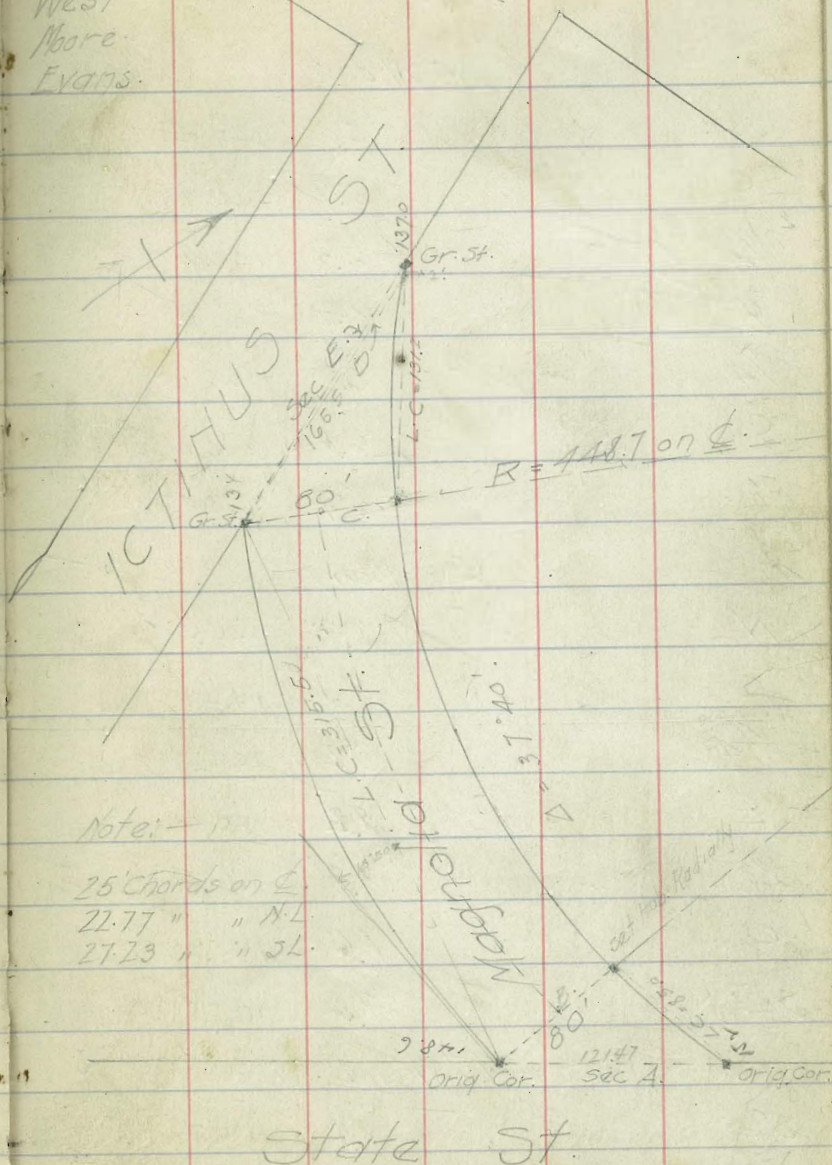
4.4 148.4

5L

4.6 148.2

April - 17 - 1913.

West  
Moore  
Evans.



Note: -  
25' Chords on Q  
22.77 " " NL  
27.23 " " 5L

15283

25' Won  $\phi$ 

SL	5.6	147.2
C	5.9	146.9
$\frac{1}{4}$	6.0	146.8
$\phi$	6.7	146.1
$\frac{1}{4}$	6.9	146.0
C	6.8	146.0
NL	6.7	146.1

50' Won  $\phi$ 

NL	8.4	144.4
C	8.7	144.1
$\frac{1}{4}$	8.2	144.6
$\phi$	8.2	144.6
$\frac{1}{4}$	8.5	144.3
C	7.6	145.2
SL	7.3	145.5

75' Won  $\phi$ 

SL	8.6	144.2
C	9.3	143.5
$\frac{1}{4}$	10.6	142.2

15283

58

 $\phi$ 

$\frac{1}{4}$	9.9	142.9
C	9.9	142.9
NL	13.2	142.6
	9.8	143.0

100' Won  $\phi$ 

NL	9.0	143.8
C	9.6	143.2
$\frac{1}{4}$	10.2	142.6

 $\phi$ 

$\frac{1}{4}$	10.9	141.9
C	11.6	141.2
SL	11.7	141.1
	11.3	142.5

125' Won  $\phi$ 

SL	11.4	141.4
C	13.2	139.6
$\frac{1}{4}$	11.7	141.1
$\phi$	10.0	142.8
$\frac{1}{4}$	9.5	143.3
C	8.7	144.1
NL	7.6	145.2

152.83

150' Work

NL	7.3	145.5
C	8.1	144.7
1/4	8.9	143.9
ϕ	9.7	143.1
1/4	10.7	142.1
C	11.6	141.2
SL	12.1	140.7

175' Work

SL	12.5	140.3
C	11.8	141.0
1/4	10.6	142.2
ϕ	9.6	143.2
1/4	8.7	144.1
C	8.2	144.6
NL	7.3	145.5

200' Work

NL	7.1	145.7
C	8.2	144.6
1/4	9.0	143.8

152.83

ϕ

ϕ	9.6	143.2
1/4	10.6	142.2
C	11.8	141.0
SL	13.2	139.6
T.P.	9.5	143.58

1.59 145.17

225' Work

SL	6.5	138.7
C	5.0	140.2
1/4	3.8	141.4
ϕ	2.9	142.3
1/4	1.7	143.5
C	1.2	144.0
NL	40.1	145.3

250' Work

NL	1.0	144.2
C	2.0	143.2
1/4	2.2	143.0
ϕ	3.5	141.7
1/4	4.7	140.5

54



14517

C	6.5	138.7
SL	7.5	137.7
275' Won &		
SL	8.0	137.2
C	7.2	138.0
1/4	5.8	139.4
ϕ	4.3	140.9
1/4	3.3	141.9
C	2.8	142.4
NL	1.9	143.3

Sec. C. 19.25' Won &amp;

NL	2.7	142.5
C	3.3	141.9
+2	3.6	141.6
+3	4.9	140.3
1/4	5.1	140.1
ϕ	5.4	139.8
1/4	5.5	139.7
C	7.6	137.6
+13	8.7	136.5
SL	10.9	134.3

14517

55

Sec. D. Top bank

SL	10.9	134.3
+2	8.7	136.5
C	8.2	137.0
<sup>7.1.0</sup> 1/4	7.6	137.6
1/4	9.2	136.0
ϕ	10.0	135.2
+7 1/4	8.5	136.7
1/4	8.9	136.3
C	9.1	136.1
+13 NL	9.4	135.8
	11.8	133.5

Sec. E. Graded for Ectinus.

NL	11.8	133.4
C	11.8	133.4
1/4	11.4	133.8
ϕ	10.0	135.2
1/4	10.0	135.2
C	11.2	134.0
SL	10.9	134.3
T.P.	11.23	133.94
<hr/>		
	5.60	139.54
B.M. 5416 + Ectinus	6.28	133.26 133.26 OK.

CROSS SECTION  
19 STREET.

80' Wide from N. St to Intersection  
with Kearney Street produced,  
60' wide at N.E. line of Sigsbee.  
14' Walks, 13' 1/4" on 80' St.  
10' " 10' " " 60' St.

B.M. N.E. Cor. 19+17. 32.99

.103 34.02

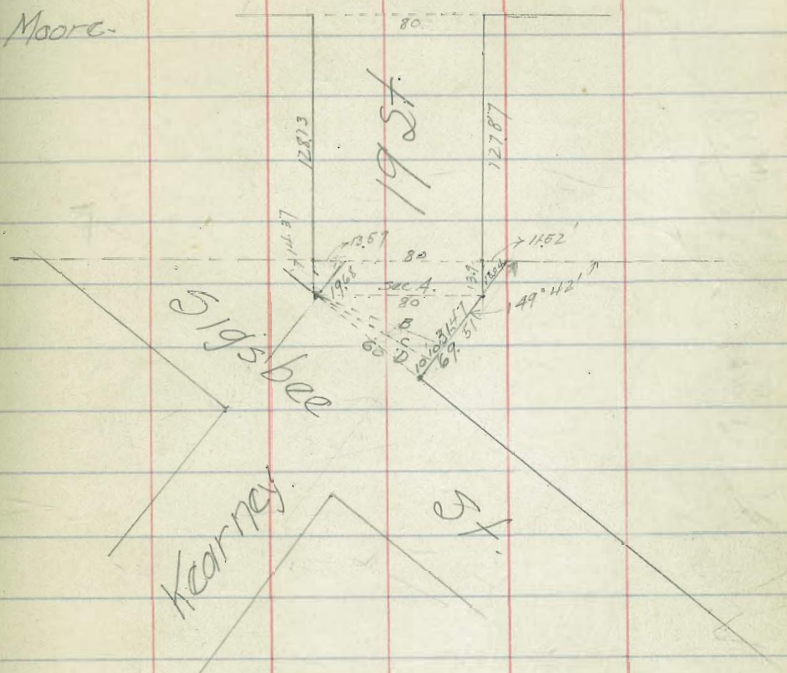
S.L. N. St.

EL.	3.7	30.3
C	3.8	30.2
1/4	4.1	29.9
1/2	4.3	29.7
3/4	4.7	29.3
C	5.2	28.8
+12	5.7	28.3
WL.	5.0	29.6

April 26-1913  
West  
Evans  
Moore.

N. St.

56



3402

25'S.

WL	4.8	29.2
Emb.	6.4	27.6
1/4	5.8	28.2
ϕ	5.7	28.3
1/4	5.3	28.7
C	4.8	29.2
EL	4.0	30.0

42'S.

-20	6.7	27.3
EL	5.6	28.4
C	6.4	27.6
1/4	6.9	27.1
ϕ <sup>+5</sup>	8.4	25.6
ϕ	7.8	26.2
1/4	8.0	26.0
C	8.8	25.2
+4	8.1	25.9
+5	6.9	27.1
WL	6.4	27.6
+20	6.8	27.2

3402

57

50'S.

-20	9.9	24.1
WL	8.9	25.1
C	7.8	24.2
1/4	9.3	24.7
ϕ	9.0	25.0
+8	9.1	24.9
<del>1/4</del>	7.9	26.1
C	7.1	26.9
EL	7.0	27.0
+20	9.1	24.9

65'S.

-20	13.7	20.3
EL	13.4	20.6
+5	12.2	21.8
C	13.0	21.0
+1	12.7	21.3
+2	11.6	22.4
1/4	12.3	21.7
ϕ	10.8	23.2
1/4	11.3	22.7
C	11.4	22.6

Upas - India to Columbia

3402

+12		11.2	22.8
WL		11.7	22.3
+20		11.7	22.3
	75'5"		
-20		12.3	21.7
T.P.		12.55	21.47
	6.86 28.33		
WL		6.9	21.4
C		6.8	21.5
1/4		7.4	20.9
+6		6.7	21.6
⊕		7.1	21.2
+2		7.8	20.5
1/4		7.9	20.4
C		7.3	21.0
EL		8.1	20.2
+10	Bottom	9.4	18.9
+20		8.1	20.2

28.33

58

83'5"

-20		8.3	20.0
EL	bottom ditch	9.4	18.9
+5		8.6	19.7
C		8.2	20.1
1/4		8.3	20.0
⊕		8.6	19.7
1/4		8.5	19.8
C		7.9	20.4
WL		7.7	20.6
+10		7.5	20.8
	100'5"		
+10		9.0	19.3
WL		8.7	19.6
C		9.4	18.9
1/4	bottom ditch	9.5	18.8
⊕	" "	9.5	18.8
1/4	" "	9.4	18.9
C	" "	9.3	19.0
EL		8.4	19.9
+20		8.2	20.1

2833

126.13 S. on WL, 127.87 S on EL.  
= Pueblo Lot 117c.

-20	66	21.7
EL	7.4	20.9
C	8.2	20.1
1/4	9.0	19.3
±	9.1	19.2
1/4	9.7	18.6
C	9.8	18.5
WL	10.3	18.0
+1	8.5	19.8
+10.	8.2	20.1

Sec A = 14.37 S of PL on W  
13.9 " " " " E.

WL	4.9	23.4
+3	5.5	22.8
+4	10.9	17.4
C	10.3	18.0
1/4	9.7	18.6
±	9.4	18.9

opening Culvert.

2833

59

+5	8.6	19.7
±	8.8	19.5
1/4	9.0	19.3
C	8.9	19.4
+13	7.7	20.6
EL	5.9	22.4

Sec B = 31.47 S on EL.

EL	6.2	22.1
+1	8.5	19.8
C	8.7	19.6
1/4	9.0	19.3
±	9.1	19.2
1/4	8.2	20.1
C	8.0	20.3
+5	6.6	21.7
WL	4.9	23.4

28.33

Sec C = 41.375 of A on EL

WL	4.9	23.4
+5	6.0	22.3
C	7.5	20.8
1/4	6.7	21.6
£	6.9	21.4
1/4	7.6	20.7
C	8.3	20.0
+13	8.1	20.3
EL	6.2	22.1

Sec D = 51.375 of A on EL =  
N.L. Sig 5600

EL	4.3	24.0
C	4.8	23.5
1/4	5.1	23.3
£	4.8	23.5
1/4	5.3	23.0
C	5.5	22.8
WL	4.9	23.4

60

2833

T.P.

3.98 24.35

11.13 35.48

B.M. spike

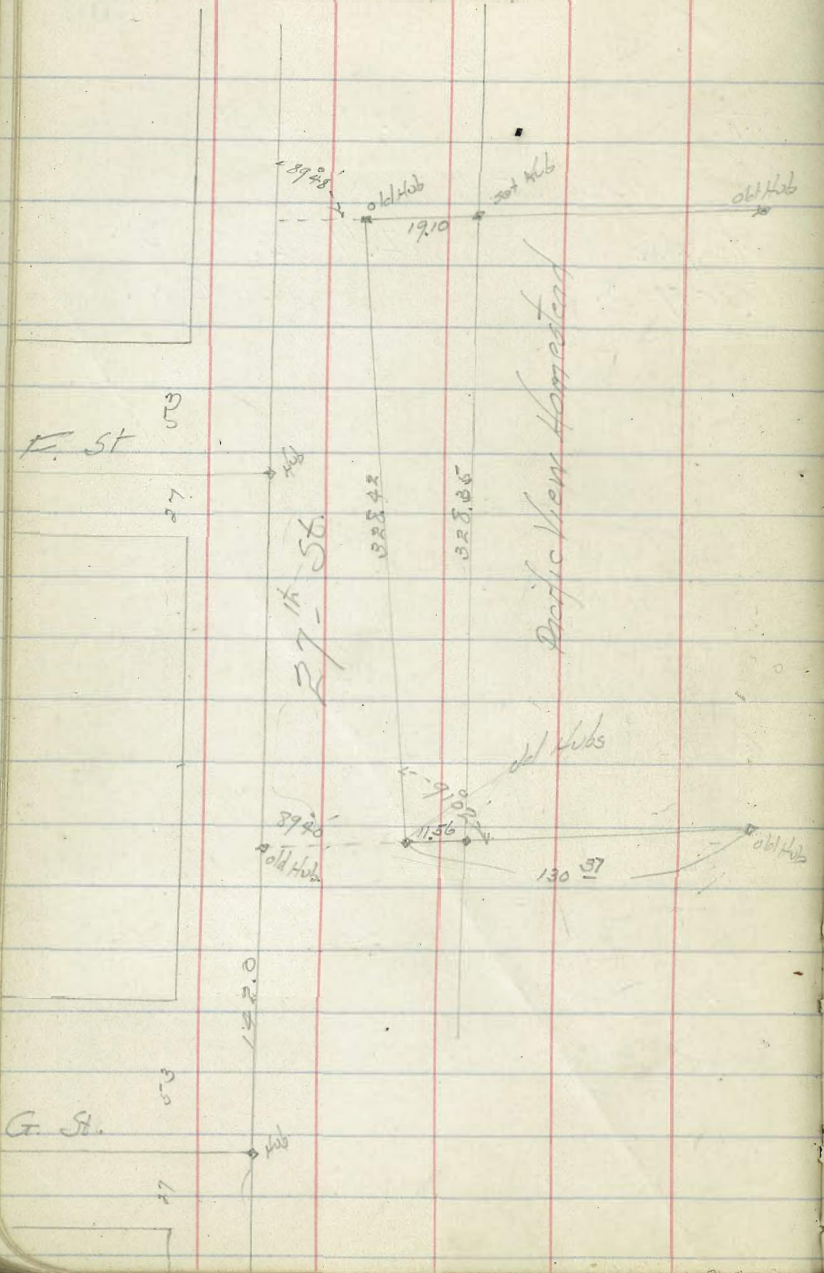
2.49 32.99 32.99

NE Cor 19+N.

O.K.

61  
1/4  
1/8  
Hall

Survey for opening 27<sup>th</sup> St  
between F. - G.





6 Change x sec of Dipas st (50') (Sd = S 2 of  
 19 India to E of Columbus st (80' st)  
 13 July

96.54

Dipas st

62

	5.61	86.66	81.95	man St India	25'	E of	India st		
	12.2	96.52	83.90	n			7.2	81.05 2.61 86.66 2.75 83.90 2.42 96.52 12.23 108.75	
	E of India st							8.0	
n		12.2					7.2		
		12.6					(7.2)		
		12.0					2.0		
b		11.4		H			0.0		
		12.4		S			-		
		12.6			50'	E of	India		
S		12.2		n			4.2		
	2 E of India							4.7	
S		3.0					4.3		
		3.7		b			(3.7)		
		5.0		TP	12.23	108.75	0.0	96.52	
b		8.0			25'	E of	India		
		11.0		S 2			10.1		
		12.2			50'	E of	India		
n		11.6		S			7.2		
				b			7.5		
				5/4			11.6		

10875

60

75' E of India

S 23  
70  
97

b (11.0)  
(132)  
132  
132  
132

100' E of India

n 92  
100  
100  
97  
(62)  
47  
30

S 11

10875

Chapas

63

125' E of India

2 52  
54  
48

b (44)  
(07)

TP 1285 12037 123 10752

4 108  
95

S 87

150' E of India

S 46  
55  
71  
(82)  
(125)

120  
127  
130

n

10875  
123  
10752  
1285  
12037

12037

1204

175 E of India

n	9.5	
	9.3	
	8.8	
b	(9.0)	(4.0)
	3.0	
	1.8	
S	1.0	
	200 E = 72 of Colombia	
n	6.4	114.0
n	5.8	14.5
y	6.7	14.2
b	5.3	15.1
	NW 66 of Colombia	
n	5.9	14.5
n	3.3	14.9
y	4.8	15.4
b	4.0	14.4

12037

1204

W 147 Colombia

n	5.8	114.4
n	5.0	15.4
y	3.3	17.1
b	2.0	18.4

center of Colombia

n	8.0	12.4
n	5.2	15.2
y	0.0	20.2

E 147 of Colombia

n	7.4	13.2
n	4.2	18.2

E 66 of Colombia

n	4.0	16.4
---	-----	------

E S of Colombia

n	2.0	18.4
---	-----	------

TP 1203 1204 608 1140  
 1140 1204 430 1204

Chas

64

12037  
 608  
 1140  
 1204  
 430  
 1204  
 1204  
 1204

max heat  
 Colombia

13362

1336

200 E - WR of Columbia

S	10.7	12.29
bl	12.2	21.4
y	13.8	19.8
+5	14.6	19.0

W bl of Columbia

S	8.5	25.1
bl	10.2	23.4
y	11.8	21.8
+5	13.2	20.4

W 1/4 of Columbia

S	6.7	24.9
bl	8.5	25.5
y	10.0	23.6
+5	11.4	22.2

Center of Columbia

S	4.6	29.0
bl	6.6	27.0
y	8.2	25.4
+5	9.6	24.0
6	12.0	21.6

13362

1336

E 1/4 of Columbia

S	2.3	31.3
	4.0	29.6
	6.3	27.3
+5	8.0	25.6
bl	10.4	23.2
	11.0	22.6

E 66 of Columbia

S	1.3	32.3
bl	2.6	31.0
y	4.6	29.0
	7.0	25.5
y	9.3	24.3
bl	12.3	21.3

65

13362

1336

E Sin of Columbia

S 00 33.4

ll 14 32.2

9 36 30.0

b 57 27.9

y 80 25.4

ll 11.3 22.3

TP 988 13460 00 13362

25' E of Columbia

n 136 121.0

ll 94 25.2

" 60 28.4

b 38 30.8

s/g 08 33.8

50' E of Columbia

n 127 21.9

ll 84 24.2

y 47 29.9

b 23 32.3

TP 1051 14393 98 13362

14393

1439

25' E of Columbia

S 66 137.3

ll 85 35.4

50' E of Columbia

S 43 39.4

ll 72 34.7

y 93 34.4

75' E of Columbia

S 10 42.9

28 41.1

54 38.5

b 72 35.7

94 34.5

120 31.9

n 153 28.6

Refas

66

13362

13485

13362

1001

14393

14393

1439

100 E of Columbus

n 87 135.7

52 38.7

32 40.7

b 10 42.9

TP 1246 15519 120 142.75

7 1552 103 44.9

b 81 47.1

S 62 49.0

125 E of Columbus

S 14 53.8

30 52.2

48 50.4

b 75 47.7

95 46.7

110 44.2

n 153 39.9

14393  
130  
14293  
1246  
15519  
170  
15349  
665  
16014

15519

1552

150 E of Columbus

n 121 143.1

84 44.8

62 49.0

b 53 49.9

35 51.7

18 53.4

S 703 155.5

TP 665 16014 170 15549

175 E of Columbus

S 21 158.0

35 54.4

51 55.0

b 78 52.3

99 50.2

116 48.5

n 133 44.8

Wfas

67

16014

140!

200  $\Sigma =$  W of State W

21 99 150.2

61 54.0

65 53.4

b 44 55.7

27 57.3

12 58.9

S 00 60!

113 159.01

one bent  
56642/100

6 Blough  
7/10  
Lutz  
X sec of McCall St (50)

1308 2758 1450

1284 40.08 0.34 2224

1201 4801 5.08 3500

Block Bet San Antonio

+ Rosecrans too

not changed Book 454 P 20

Σ of Rosecrans St (50)

S 101 37.9

105 37.5

96 38.4

b 93 38.7

97 38.3

Sutta 101 37.9

96 38.4

n 90 39.0

Elev. flow line of 6' culvert across Rosecrans  
on E. gutter line of McCall St. 35.0 at w. end  
and 31.9 at E. end.

4801

McCall

69

50 w of Rosecrans

n 53 49.7

Sutta 54 49.6

62 41.7

61 41.9

58 49.0

58 49.2

58 49.2

60 49.0

60 49.0

S 55 49.5

100 w of Rosecrans

S 26 45.4

26 45.4

23 45.7

b 23 45.7

25 45.5

Sutta 27 45.3

22 45.8

n 19 46.1

TP 1230 6024 0.0 4801



6030

	150	20 y	Rosicams	
n			95	508
			100	503
Gutter			10.8	49.5
			10.6	49.7
b			10.5	49.8
			10.4	49.9
			10.8	49.5
S			10.8	49.5

	20 y	W 7	Rosicams	
S			60	543
			65	538
			58	545
			63	540
b			63	540
			66	537
			59	544
n			57	546

6031

Mc-bell

70

	250	W 7	Rosicams	
n			10	59.3
			11	59.2
Gutter			20	58.3
			19	58.4
b			18	58.6
			16	58.7
			18	58.6
S			16	58.7
TP	1220	2226	0.5	61.06
	300	W 7	S 1 y	San Eliego
S			9.3	63.0
			9.0	63.3
			9.0	63.7
			8.9	63.4
			9.0	63.3
			9.2	63.1
			8.5	63.8
n			8.3	64.0

6030  
41  
6031  
420  
7.24

7226

	E	bt f	San Elijo	
n			73	65.0
			<del>74</del>	
			73	65.0
	South		83	64.0
			82	64.1
b			81	64.2
			81	64.2
			82	64.1
S			84	63.9

	E	1/4 f	San Elijo	
S			77	64.6
			74	64.9
			73	65.0
b			72	65.1
			75	64.8
	South		78	64.5
			67	65.6
n			64	65.9

7226

McCall

71

	n	South	San Elijo	
			60	66.3
			62	66.1
		South	70	65.3
			68	65.5
b			64	65.9
			66	65.7
			67	65.6
S			69	65.4

	n	1/4 f	Elijo	
S			64	65.9
			60	66.3
			59	66.4
b			58	66.5
			61	66.2
		South	62	66.1
			53	67.0
			55	
n			57	66.6

7226

	W	Bl of	Elyo	
n			44	67.9
			48	67.5
	Sutta		56	66.7
			54	66.9
b			50	67.3
			50	67.3
			51	67.2
s			53	67.0

7225  
7205  
1220  
8475

	W	Line of	Sp	Elyo
s			45	67.8
			45	67.8
			41	68.2
b			40	68.3
			44	67.9
	Sutta		46	67.7
			40	68.3
n			33	69.0

TP 1220 8476 020 7206

8476

The base

72

	50	W of	Sp	Elyo
n			105	74.3
			105	74.3
		Sutta	120	77.8
			117	73.1
b			113	73.5
			116	73.2
			116	73.2
s			115	73.3

	100	W of	Sp	Elyo
s			65	78.3
			64	78.4
			61	78.7
b			61	78.7
			65	78.3
			67	78.1
		Sutta	57	79.1
n			51	79.7

8476

	150	W of	Elizav	
n			0,0	808
			1,0	838
Sutler			2,2	826
			1,8	830
b			1,7	831
			1,8	830
			2,1	827
S			2,3	825
TP	1183	8579	130	8346
	200	W of	Elizav	
S			85	868
			84	869
			76	877
b			75	878
			75	878
Sutler			78	875
			70	883
n			60	893

9579

The ball

78

	250	W of	Elizav	
n			0,0	953
			0,8	946
Sutler			1,8	935
			1,8	935
b			1,7	936
			1,6	937
			2,2	931
S			2,0	933
TP	1288	10679	138	9398
	300	W of	San Fernando	(50)
S			76	99.2
			70	99.8
Sutler			80	98.8
			72	99.6
b			65	100.3
			63	100.5
			63	100.5
n			27	106.1
	200	W of	95670	
n			70	99.8

10679

E 668 San Fernando

n			
		(28)	104.0
		4.0	107.8
		4.8	107.0

		4.7	102.1
--	--	-----	-------

b		5.2	101.6
---	--	-----	-------

		5.6	101.2
--	--	-----	-------

		6.4	100.4
--	--	-----	-------

S		(6.2)	100.6
		6.7	99.9

E 1048 Fernando

S		5.6	101.2
---	--	-----	-------

		5.6	101.2
--	--	-----	-------

		4.6	102.2
--	--	-----	-------

b		4.3	102.5
---	--	-----	-------

		4.0	102.8
--	--	-----	-------

		3.8	103.0
--	--	-----	-------

n		3.0	103.8
---	--	-----	-------

10679

McBall

74

Banta 8 Fernando

n		2.3	104.5
---	--	-----	-------

		2.8	104.0
--	--	-----	-------

		3.0	103.8
--	--	-----	-------

b		3.6	103.2
---	--	-----	-------

		3.7	103.1
--	--	-----	-------

		4.4	102.4
--	--	-----	-------

S		4.6	102.2
---	--	-----	-------

W 1048 Fernando

S		3.5	103.3
---	--	-----	-------

		3.5	103.3
--	--	-----	-------

		2.6	104.2
--	--	-----	-------

b		2.5	104.3
---	--	-----	-------

		2.4	104.6
--	--	-----	-------

		2.5	104.3
--	--	-----	-------

n		2.5	104.3
---	--	-----	-------

10679

W side of Fernando

n	20	106.8
	19	106.9
	19	106.9
b	18	105.0
	20	106.8
	26	106.9
S	27	106.1

W side of San Fernando

S	1.0	105.8 ✓
	1.6	105.9 ✓
	1.0	105.8 ✓
b	0.6	106.9 ✓
	0.8	106.0 ✓
	0.8	106.0 ✓
n	1.0	105.8 ✓

1265

11923

0.12

106.58

13m SW  
Fernando

n

11953

50 W of Fernando

n	61	113.2 ✓
	72	112.1 ✓
	74	111.9 ✓
	74	111.9 ✓
b	74	111.9 ✓
	74	111.9 ✓
	80	111.3 ✓
	75	111.8 ✓
S	57	113.6 ✓

100 W of Fernando

S	14	117.9 ✓
	24	116.9 ✓
	20	117.3 ✓
	18	117.5 ✓
b	14	117.9 ✓
	12	118.1 ✓
	14	117.9 ✓
	0.8	118.5 ✓

TP

1207

12114

0.36

118.79

9.3

121.7 ✓

Mc base

75

119.32  
 118.96  
 12.07  
 131.03

131.0  $\times$

150' W of Fernando

n		4.0	127.0 ✓	131.03
	+4'	6.2	126.8 ✓	131.0
		6.2	126.8 ✓	131.13
		6.1	126.9 ✓	
b		6.0	126.0 ✓	
		6.4	126.6 ✓	
		7.0	126.0 ✓	
	+9'	7.0	127.9 ✓	
S		6.4	126.6 ✓	
	TP	8.0	131.0 ✓	

131.0 144.4

200' W of Fernando

S		13.3	130.8 ✓
	+1'	14.1	130.0 ✓
		13.9	130.9 ✓
		13.3	130.8 ✓
b		13.1	131.0 ✓
		12.5	131.6 ✓
		12.6	131.5 ✓
		12.1	132.0 ✓
n	+5'	10.0	132.1 ✓

144.3

250' W of Fernando

n		1.0	142.1 ✓
		7.2	136.9 ✓
		7.2	136.9 ✓
b		7.4	136.5 ✓
		7.8	136.7 ✓
		8.2	135.9 ✓
	+9'	9.4	134.7 ✓
S		10.2	133.9 ✓

300' W of Fernando = E of Suzanne

S		30.0	141.1 ✓
		1.6	142.5 ✓
		1.0	143.1 ✓
b		8.5	143.6 ✓
		0.0	144.1 ✓
		40.4	144.5 ✓
n		40.4	144.5 ✓

The Ball

76

X Sec's Vermont  
 S.L. Lincoln to N.L. Pascoe.  
 80' Wide, 14' W. 13 1/4's.

3W 40' W plug. rat 289.756

July 26-1913

West

Expts

Moore

77.

B.M. S.W. Vermont + Lincoln

292.06

296.61

25' S

4.55 296.61

S.L. Lincoln

WL	4.2	287.9	292.4
C	3.9	288.2	292.7
1/4	4.5	287.6	292.1
£	4.0	288.1	292.6
1/4	4.6	287.5	292.0
C	3.7	288.4	292.9
E.L.	3.6	288.5	293.0
-10	10' S 9.6		287.0
EL	8.3	288.8	288.3
C	6.6	285.5	290.0
1/4	5.0	287.1	291.6
£	3.9	288.2	292.7
1/4	4.2	287.9	292.4
C	3.8	288.3	292.8
WL	3.9	288.2	292.7

WL

4.0 292.2

C

3.9 292.7

1/4

3.9 292.7

£

3.9 292.7

1/4

4.8 291.8

C

5.9 290.7

EL

7.8 288.8

4.5

10.0 286.6

50' S

= 25  
 = 15

11.3 287.7

EL

7.0 289.6

C

5.6 291.0

1/4

5.0 291.6

£

4.0 292.6

1/4

3.6 293.0

C

3.9 292.7

WL

4.2 292.4



XSec Vermont St

296.61

75' S.

WL	4.8	291.8
c	4.2	292.4
1/4	3.9	292.7
ϕ	3.9	292.7
1/4	4.9	291.7
c	5.6	291.0
EL	6.6	290.8
+25	10.3	286.3
+40	14.6	282.0

100' S.

= 40	13.0	
- 20	8.6	
EL	6.2	290.4
c	5.3	291.3
1/4	4.6	292.0
ϕ	3.8	292.8
1/4	4.4	292.2
c	5.0	291.6
WL	5.3	291.3

78

296.61

125' S.

WL	5.8	290.8
c	5.0	291.6
1/4	4.2	292.4
ϕ	4.3	292.3
1/4	4.1	292.5
c	4.9	291.7
EL	5.7	290.9
+25	8.3	288.3

150' S.

-25	7.4	289.2
EL	4.8	291.8
c	4.2	292.4
1/4	3.9	292.7
ϕ	4.9	291.7
+8	3.7	292.9
1/4	5.0	
c	5.9	290.7
WL	6.0	290.6

X Sec. Vermont St

296.61

275's

WL	6.5	290.1
C	6.3	290.3
1/4	5.7	290.9
ϕ	4.9	291.7
1/4	4.9	291.7
C	4.7	291.9
EL	5.0	291.6

200's

EL	5.4	291.2
C	5.3	291.3
1/4	5.6	291.0
ϕ	5.9	290.7
1/4	6.6	290.0
C	7.1	289.5
WL	7.2	289.7

296.61

225's

-15	8.2	
-5	13.8	
WL	14.2	282.4
C	12.7	283.9
1/4	13.1	283.5
ϕ	8.3	288.3
1/4	6.8	289.8
C	6.7	289.9
EL	6.6	290.0
-15	6.6	290.0
T.P.	11.86	284.75

1.42 286.17

250's

-15	1.7	284.5
EL	1.2	285.0
C	3.1	283.1
1/4	4.5	281.7
ϕ	9.2	277.0
1/4	13.2	273.0
C	16.4	269.8
+10	19.0	267.2
WL	14.0	272.2
-10	8.8	277.4

same slope.

X Sec Vermont St.

	286.17		
T.P.	12.72	273.45	
	1.69	275.14	
	275'S.		
+15	3.9	282.3	271.2
WL	12.6	273.6	262.5
C	17.0	269.2	258.1
1/4	14.9	271.3	260.2
1/2	8.3	277.9	266.8
3/4	5.3	280.9	269.8
C	4.3	281.9	270.8
EL.	1.2	284.0	273.9
+30	0.2	286.0	274.9
T.P.	12.38	262.76	

3.91 266.67

300'S = N.L. Pascoe N.L. Pascoe.

-30	3.4	263.3	
EL.	6.1	260.6	
C	7.8	259.9	
1/4	9.3	257.4	
1/2	10.2	256.4	

July 26-1913  
West

~~286.17~~  
266.67

80

1/4	15.2	251.5	
+10	17.7	249.0	
C	15.6	251.1	
WL	7.1	259.6	
+10	1.5	265.2	
same slope up			
T.P.	0.82	265.85	
	12.45	278.30	
T.P.	11.6	277.14	
	11.98	289.12	
T.P.	0.95	288.17	
	9.14	297.31	
BM 3W Lincoln Vermont.	5.26	292.05	292.06 292.05
Checks OK			
West			

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.00	7.15	7.30	7.45	7.60	7.75	7.90	8.05	8.20	8.35	0
1	8.50	8.65	8.80	8.95	9.10	9.25	9.40	9.55	9.70	9.85	1
2	10.00	10.15	10.30	10.45	10.60	10.75	10.90	11.05	11.20	11.35	2
3	11.50	11.65	11.80	11.95	12.10	12.25	12.40	12.55	12.70	12.85	3
4	13.00	13.15	13.30	13.45	13.60	13.75	13.90	14.05	14.20	14.35	4
5	14.50	14.65	14.80	14.95	15.10	15.25	15.40	15.55	15.70	15.85	5
6	16.00	16.15	16.30	16.45	16.60	16.75	16.90	17.05	17.20	17.35	6
7	17.50	17.65	17.80	17.95	18.10	18.25	18.40	18.55	18.70	18.85	7
8	19.00	19.15	19.30	19.45	19.60	19.75	19.90	20.05	20.20	20.35	8
9	20.50	20.65	20.80	20.95	21.10	21.25	21.40	21.55	21.70	21.85	9
10	22.00	22.15	22.30	22.45	22.60	22.75	22.90	23.05	23.20	23.35	10
11	23.50	23.65	23.80	23.95	24.10	24.25	24.40	24.55	24.70	24.85	11
12	25.00	25.15	25.30	25.45	25.60	25.75	25.90	26.05	26.20	26.35	12
13	26.50	26.65	26.80	26.95	27.10	27.25	27.40	27.55	27.70	27.85	13
14	28.00	28.15	28.30	28.45	28.60	28.75	28.90	29.05	29.20	29.35	14
15	29.50	29.65	29.80	29.95	30.10	30.25	30.40	30.55	30.70	30.85	15
16	31.00	31.15	31.30	31.45	31.60	31.75	31.90	32.05	32.20	32.35	16
17	32.50	32.65	32.80	32.95	33.10	33.25	33.40	33.55	33.70	33.85	17
18	34.00	34.15	34.30	34.45	34.60	34.75	34.90	35.05	35.20	35.35	18
19	35.50	35.65	35.80	35.95	36.10	36.25	36.40	36.55	36.70	36.85	19
20	37.00	37.15	37.30	37.45	37.60	37.75	37.90	38.05	38.20	38.35	20
21	38.50	38.65	38.80	38.95	39.10	39.25	39.40	39.55	39.70	39.85	21
22	40.00	40.15	40.30	40.45	40.60	40.75	40.90	41.05	41.20	41.35	22
23	41.50	41.65	41.80	41.95	42.10	42.25	42.40	42.55	42.70	42.85	23
24	43.00	43.15	43.30	43.45	43.60	43.75	43.90	44.05	44.20	44.35	24
25	44.50	44.65	44.80	44.95	45.10	45.25	45.40	45.55	45.70	45.85	25
26	46.00	46.15	46.30	46.45	46.60	46.75	46.90	47.05	47.20	47.35	26
27	47.50	47.65	47.80	47.95	48.10	48.25	48.40	48.55	48.70	48.85	27
28	49.00	49.15	49.30	49.45	49.60	49.75	49.90	50.05	50.20	50.35	28
29	50.50	50.65	50.80	50.95	51.10	51.25	51.40	51.55	51.70	51.85	29
30	52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	30
31	53.50	53.65	53.80	53.95	54.10	54.25	54.40	54.55	54.70	54.85	31
32	55.00	55.15	55.30	55.45	55.60	55.75	55.90	56.05	56.20	56.35	32
33	56.50	56.65	56.80	56.95	57.10	57.25	57.40	57.55	57.70	57.85	33
34	58.00	58.15	58.30	58.45	58.60	58.75	58.90	59.05	59.20	59.35	34
35	59.50	59.65	59.80	59.95	60.10	60.25	60.40	60.55	60.70	60.85	35
36	61.00	61.15	61.30	61.45	61.60	61.75	61.90	62.05	62.20	62.35	36
37	62.50	62.65	62.80	62.95	63.10	63.25	63.40	63.55	63.70	63.85	37
38	64.00	64.15	64.30	64.45	64.60	64.75	64.90	65.05	65.20	65.35	38
39	65.50	65.65	65.80	65.95	66.10	66.25	66.40	66.55	66.70	66.85	39
40	67.00	67.15	67.30	67.45	67.60	67.75	67.90	68.05	68.20	68.35	40

Calculated by F. W. Paradis, C. F.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
 ROADWAY 16 FEET WIDE. SIDE SLOPES 1½ TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4

Calculated by F. E. Paradis. C. E.

48.3

57.3  
 2.9 = 5.2  
 54.4 = 52

57.3  
 5.8  
 51.5 = 7.2

57.3  
 5.1  
 51.5

57.3  
 3.0  
 54.3 = 52

12.22  
 12.14  
 134.68

58  
 3.0  
 2.8

53.7  
 5.1  
 48.6  
 57.3  
 52.2

57.3  
 5.8  
 51.5

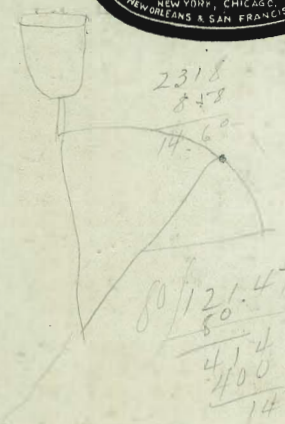
57.3  
 2.7  
 54.6

54.4  
 54.6

53.1  
 53.6



15.26  
 1.66  
 3.21



2318  
 848  
 14.60

2318  
 14.60  
 8.58

15.26  
 1.66  
 19.16

608  
 15.2  
 21.28

79.04  
 4.2