

889

F.B.

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LEVEL BOOK.

No. 410 T

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Please Return  
to  
City Engrs Office  
City Hall.  
San Diego, Calif.

MICROFILMED

DEC 15 1964

EUGENE DIETZGEN CO.,

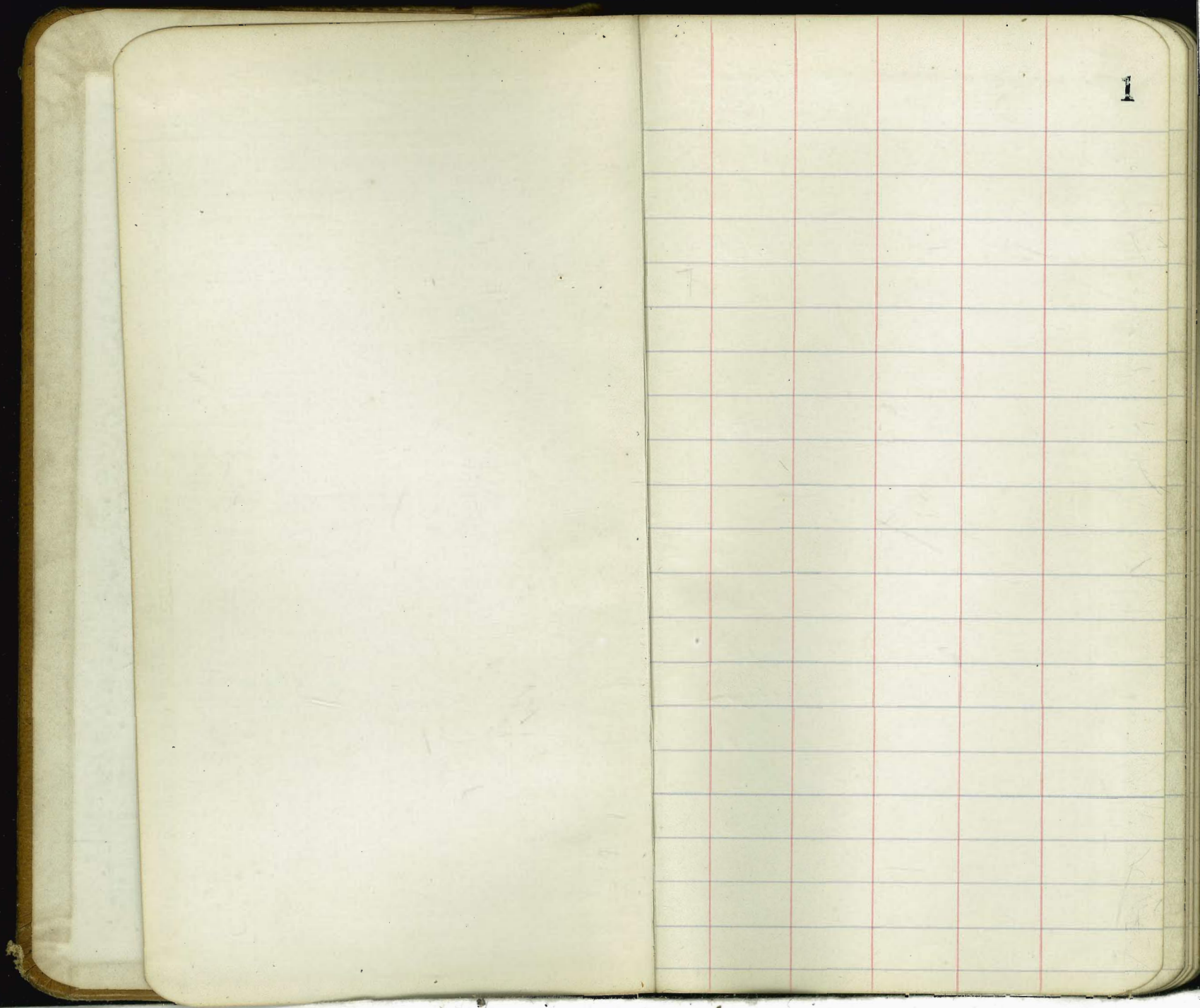
Drawing Materials and Surveying Instruments.  
NEW YORK. CHICAGO. SAN FRANCISCO.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.  
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 20 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

Copyright, 1902. No. 39340.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	0
1	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	1
2	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	2
3	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	3
4	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	4
5	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	5
6	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	6
7	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	7
8	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	8
9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	9
10	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	10
11	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	11
12	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	12
13	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	13
14	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	14
15	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	15
16	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	16
17	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	17
18	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	18
19	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	19
20	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	20
21	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	21
22	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	22
23	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	23
24	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	24
25	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	25
26	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	26
27	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	27
28	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	28
29	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	29
30	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	30
31	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	31
32	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	32
33	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	33
34	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	34
35	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	35
36	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	36
37	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	37
38	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	38
39	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	39
40	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	40

Calculated by F. E. Paradis, C. E.



1

CROSS-SECTIONS  
STATE STREET

3L Prospect. to E.L. Girard.  
80' Wide, 14' Walks, 13 1/2' Sid.

B.M. NW Cor. State + Ictinus. 133.26

11.62 144.88

T.P. 0.85 144.03

11.65 155.68

T.P. 0.18 165.50

14.91 167.48

T.P. 5.99 161.49

2.06 163.55

5L Prospect.

E.L. 11.3 152.3

C 11.6 152.3

H 12.1 151.5

S 12.3 151.5

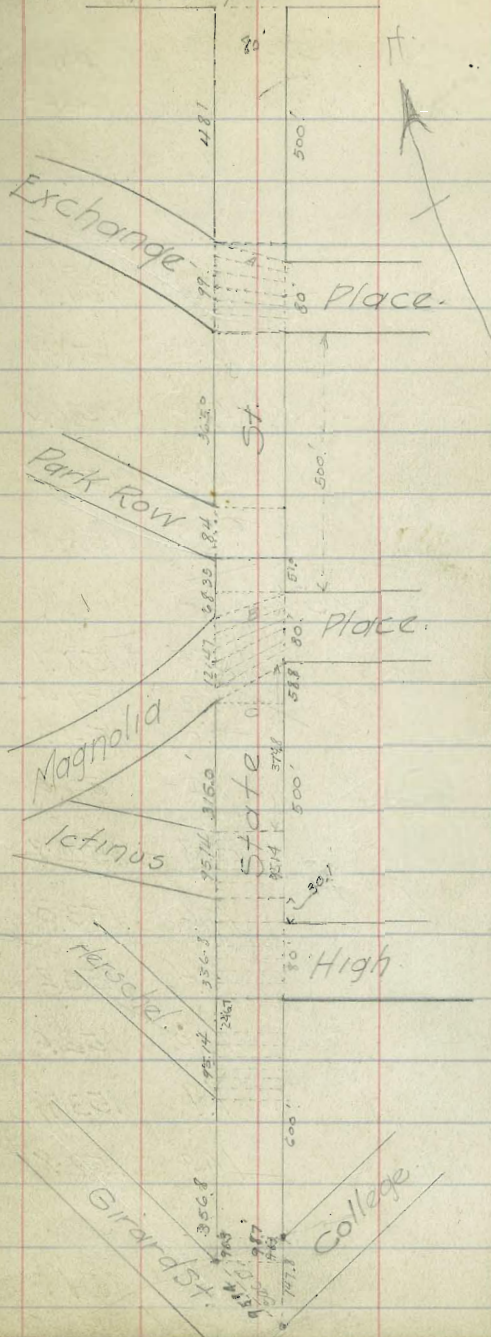
H 13.0 150.6

C 13.5 150.1

W.C. 13.3 150.5

April-18-1913. Prospect.

West  
Evans  
Moore.



287

16355

2'5 SL Prospect

WL	11.4	1522
C	10.8	1528
1/4	11.8	1518
E	12.2	1514
1/4	12.0	1516
C	11.0	1526
EL	9.5	1541

25'5

EL	5.5	158.1
+11	6.2	157.4
+12	9.0	154.6
C	9.6	154.0
1/4	10.8	152.8
E	10.6	153.0
1/4	10.4	153.2
C	11.0	152.6
+2	9.9	153.7
WL	10.8	152.8

16355

50'5

3

WL	9.9	153.6
+12	9.3	154.3
C	10.2	153.4
1/4	9.5	154.1
E	9.3	154.3
1/4	9.2	154.4
C	8.5	155.1
+2	5.5	158.1
EL	4.7	158.9

75'5

EL	3.9	159.7
C	6.9	156.7
1/4	7.8	155.8
E	8.1	155.5
1/4	9.1	154.5
C	9.9	153.7
+2	9.6	154.0
+3	9.0	154.6
WL	9.8	153.8

163.55

100' S.

WL.	9.8	153.8
C	9.3	154.0
1/4	8.8	154.8
⊕	7.5	156.4
1/4	7.3	156.3
+12	6.4	157.2
C	4.7	158.9
EL.	3.2	160.4

125' S.

EL.	2.6	161.0
C	5.6	158.0
1/4	6.5	157.1
⊕	6.7	156.9
1/4	7.6	156.0
C	8.5	155.1
WL	9.6	154.0

150' S.

WL	10.1	153.5
C	8.9	154.7

163.55

4

1/4	7.7	155.9
⊕	6.9	156.7
1/4	6.0	157.6
C	5.3	158.3
EL.	4.2	159.4

175' S.

EL.	3.8	159.8
C	5.1	158.5
1/4	5.6	158.0
⊕	6.7	156.9
1/4	7.8	155.8
C	8.9	154.7
WL.	9.6	154.0

225' S.

WL	8.0	155.6
C	7.3	156.3
1/4	5.9	157.7
⊕	5.1	158.5
1/4	4.8	158.8
C	4.3	159.3
EL.	3.0	160.6

16355

275'S

EL	0.4	163.2
C	1.7	161.9
1/4	3.1	160.5
1/2	3.8	159.8
3/4	5.0	158.6
C	5.8	157.8
WL	6.6	157.0
T.P.	4.13	159.42

9.80 169.22

325'S

WL	11.3	157.9
C	10.3	158.9
1/4	9.2	160.0
1/2	8.0	161.2
3/4	7.6	161.6
C	6.6	162.6
EL	5.5	163.7

16922

375'S

EL	4.8	164.4
C	5.8	163.4
1/4	6.3	162.9
1/2	7.0	162.2
3/4	8.4	160.8
C	9.3	159.9
WL	10.0	159.2

425'S

WL	7.9	151.3
C	7.3	151.9
1/4	6.7	152.5
1/2	6.4	152.8
3/4	5.8	153.4
C	5.9	153.3
EL	3.6	155.6

450'S

EL	2.8	156.4
C	3.8	155.4
1/4	4.7	154.5

5

16922

Φ	5.6	163.6
1/4	6.0	163.2
C	6.8	162.4
WL	7.3	161.9

481's - of Prospect.

WL	5.6	163.6
C	5.1	164.1
1/4	4.4	164.8
Φ	4.3	164.9
1/4	2.6	166.6
C	2.5	166.7
EL	1.9	167.3

500A = NL Exchange  
 being 281's on WL + 500's on EL  
 50' wide  
 14' high  
 13' 1/2

EL	1.6	167.6
C	2.3	166.9
1/4	2.6	166.6
Φ	3.6	165.6
1/4	4.1	165.1
C	4.6	164.6
WL	5.6	163.6

16922

N Curb.

6

WL	5.6	163.6
C	4.6	164.6
1/4	3.8	165.4
Φ	3.5	165.7
1/4	2.8	166.4
C	2.1	167.1
EL	1.9	167.3

N 1/4

EL	1.6	167.6
C	2.0	167.2
1/4	2.9	166.3
Φ	3.2	166.0
1/4	3.7	165.5
C	4.4	164.8
WL	5.2	164.0

Φ Exchange

WL	5.2	164.0
C	4.2	165.0
1/4	3.6	165.6



16922

Φ	3.1	166.1
1/4	2.8	166.4
C	2.5	166.7
EL	2.3	166.9
5/4		
EL	2.7	166.5
C	2.9	166.3
1/4	3.0	166.2
Φ	3.3	165.7
1/4	4.0	165.2
C	4.6	164.6
WL	5.6	163.6
S. Corb.		
WL	6.3	162.9
C	5.2	164.0
1/4	4.8	164.4
Φ	4.1	165.1
1/4	3.6	165.6
C	3.3	165.9
EL	2.7	166.5

16922

Exchange?  
3.L Prospect.?

7

EL	3.4	165.8
C	3.9	165.3
1/4	4.1	165.1
Φ	4.8	164.4
1/4	5.7	163.5
C	6.1	163.1
WL	6.7	162.5
50'S		
WL	8.2	161.0
C	8.4	160.8
1/4	8.1	161.1
Φ	7.2	162.0
1/4	6.4	162.8
C	5.8	163.4
EL	5.3	163.9
100'S		
EL	6.7	162.5
C	7.2	162.0
1/4	7.9	161.3

16922

Φ	8.5	160.7
1/4	9.1	160.1
C	9.3	159.9
WL	10.0	159.2
150'S.		
WL	10.5	158.7
C	10.0	159.2
1/4	9.3	159.9
Φ	9.3	159.9
1/4	8.8	160.4
C	8.7	160.5
EL	8.5	160.7
200'S.		
EL	9.3	159.9
C	9.6	159.6
1/4	9.8	159.4
Φ	10.8	158.4
1/4	11.0	158.2
C	11.1	158.1
WL	11.2	158.0

16922

8

250'S.

WL	12.6	156.6
C	12.2	157.0
1/4	11.5	157.7
Φ	11.6	157.6
1/4	11.4	157.8
C	10.7	158.5
EL	10.4	158.8
T.P.	10.85	158.37

0.97 159.34

300'S.

EL	1.4	157.9
C	1.9	157.4
1/4	2.5	156.8
Φ	2.7	156.6
1/4	2.9	156.4
C	3.5	155.8
WL	4.0	155.3

159.34  
350' S.

WL	4.9	154.4
C	4.2	155.1
1/4	3.4	155.9
Φ	3.3	156.0
1/4	3.1	156.2
C	3.0	156.3
EL	2.5	156.8

N.L. Park Row = 365' S.   
 { 80' Wide  
 14' Walk 13' 1/4  
 84' on st angle

EL	2.6	156.7
C	3.4	155.9
1/4	3.7	155.6
Φ	3.7	155.6
1/4	3.8	155.5
C	4.7	154.6
WL	5.4	153.9

N.Curb.

WL	5.4	153.9
C	5.0	154.3
1/4	4.6	154.7

159.34

9

Φ	4.2	155.0
1/4	4.1	155.1
C	3.9	155.4
EL	3.4	155.9

N/A

EL	3.7	155.6
C	4.2	155.4
1/4	4.3	155.0
Φ	4.5	154.8
1/4	4.8	154.5
C	5.2	154.1
WL	5.4	153.9

Φ

WL	5.4	153.9
C	5.1	153.2
1/4	4.9	154.4
Φ	4.9	154.4
1/4	4.6	154.7
C	4.2	155.1
EL	3.5	155.8

15934

D/A

EL.	4.0	155.3
C	4.6	154.7
1/4	4.9	154.4
£	5.3	154.0
1/4	5.5	153.8
C	5.5	153.8
WL.	5.5	153.8

S. Curb

WL.	5.7	153.6
C	5.8	153.5
1/4	5.8	153.5
£	5.7	153.6
1/4	5.3	154.0
C	5.0	154.3
EL.	4.3	155.0

84' S. of WL = 5 L. Park Row. + 449' S. of Exchange

EL.	4.3	155.0
C	5.3	154.0
1/4	5.6	153.7

15934

10

£	5.8	153.5
1/4	6.4	152.9
C	6.4	152.9
WL.	6.7	152.6

51' S. of Park Row  
or 500' S. of Exchange

WL.	8.0	151.3
C	7.4	151.9
1/4	7.0	152.3
£	6.5	152.8

1/4	6.0	153.3
C	5.6	153.7
EL.	5.6	153.7

Sec B. N.L. Magnolia Place. 17.35' S. of last point on WL.

EL.	5.6	153.7
C	5.9	153.4
1/4	6.1	153.2
£	7.0	152.3
1/4	7.3	152.0
C	8.0	151.3
WL.	8.7	150.6

15934

N Curb.

WL	8.4	150.9
C	7.9	151.4
1/4	7.5	151.8
Φ	7.3	152.0
1/4	7.0	152.3
C	6.3	153.0
EL	6.0	153.3

N 1/4

EL	6.9	153.2
C	6.4	152.9
1/4	7.1	152.2
Φ	7.6	151.7
1/4	7.9	151.4
C	8.4	150.9
WL	9.4	149.9

Φ

WL	9.9	149.4
C	9.3	150.0
1/4	8.3	151.0

15934

11

Φ

8.0	151.3	
1/4	7.4	151.9
C	7.0	152.3
EL	6.1	153.2

S 1/4

EL	6.7	152.6
C	7.1	152.2
1/4	7.4	151.9
Φ	8.3	151.0
1/4	8.4	150.9
C	9.7	149.6
WL	10.3	149.0

S Curb.

WL	10.6	148.7
C	9.5	149.8
1/4	9.0	150.3
Φ	8.6	150.7
1/4	7.5	151.8
C	6.8	152.5
EL	7.0	152.3

15934

## S.L. Magnolia St.

EL.	7.2	152.1
C	7.7	151.6
1/4	8.4	150.9
⊕	9.1	150.2
1/4	9.3	150.0
C	10.0	149.3
WL.	11.0	148.3

Sec C. Opposite S.W. Cor. Mag + State  
+ being 58.0' S. on EL of last point

WL.	11.0	148.3
C	10.1	149.2
1/4	9.6	149.7
⊕	9.1	150.2
1/4	8.8	150.5
C	8.7	150.6
EL.	8.5	150.8

100'S. of S.E. Cor. State + Magnolia

EL.	9.1	150.2
C.	10.0	149.3

15934

12

1/4	9.8	149.5
⊕	10.2	149.1
1/4	10.4	148.9
C	11.4	147.9
WL.	11.8	147.5
T.P.	11.73	147.61
	140	149.01
		150'S

WL.	3.3	145.6
C	2.8	146.2
1/4	2.2	146.8
⊕	1.9	147.1
1/4	1.9	147.1
C	1.4	147.6
EL.	1.0	148.0

200'S

EL.	3.8	145.2
C	4.2	144.8
1/4	4.6	144.4
⊕	4.7	144.3

14901

1/4	50	144.0
C	5.5	143.5
WL	5.9	143.1

250'S.

WL	7.3	141.7
C	7.3	141.7
1/4	7.6	141.4
⊖	7.6	141.4
1/4	7.6	141.4
C	7.9	141.1
EL	8.1	140.9

300'S.

EL	11.3	137.7
C	11.1	137.9
1/4	10.7	138.3
⊖	11.0	138.0
1/4	11.0	138.0
C	11.0	138.0
WL	11.1	137.9

13

14901

T.P.	11.04	137.97
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0.73 138.70

B.M.

5.46 133.24

133.26

133.24

0.02

350'S.

WL	4.3	134.4
C	4.4	134.3
1/4	4.4	134.3
⊖	4.3	134.4
1/4	4.3	134.4
C	3.8	134.9
EL	3.8	134.9

374'S. - N.L. T. finus

60' Wide  
20' Walks.  
10' 1/2"

EL	6.8	131.9
C	6.5	132.2
1/4	6.9	131.8
⊖	6.6	132.1
C	6.2	132.5
1/4	6.4	132.3
WL	6.1	132.6

B.M. State + Ictinus		133.26	
1.93	135.19		
	<sup>N</sup>		
	398.6'S - Curb. Ictinus		
	produced rt. angles across state		
WL		6.0	129.2
C		5.0	130.2
$\frac{1}{4}$		4.5	130.7
$\phi$		4.6	130.6
$\frac{1}{4}$		4.6	130.6
C		4.7	130.5
EL		5.0	130.2
	410.5'S = $\frac{1}{4}$ Ictinus Produced		
EL		5.6	129.6
C		5.4	129.8
$\frac{1}{4}$		5.5	129.7
$\phi$		5.6	129.6
$\frac{1}{4}$		5.6	129.6
C		6.2	129.0
WL		6.4	128.8

April - 21 - 1913

West  
Evans  
Moore

135.19

14

422.4'S =  $\phi$  Produced

WL		7.3	127.9
C		7.1	128.1
$\frac{1}{4}$		6.6	128.6
$\phi$		6.2	129.0
$\frac{1}{4}$		6.2	129.0
C		6.2	129.0
EL		6.0	129.2

434.3'S =  $\frac{1}{4}$  Produced

EL		6.8	128.4
C		6.9	128.3
$\frac{1}{4}$		6.9	128.3
$\phi$		7.3	127.9

$\frac{1}{4}$		7.9	127.3
C		8.1	127.1
WL		8.8	126.4

446.2'S =  $\frac{1}{4}$  Curb. produced

WL		8.8	126.4
C		9.4	125.8
C		9.2	126.0
$\frac{1}{4}$		9.0	126.2



13519

ϕ	8.5	126.7
1/4	8.0	127.2
C	8.3	126.9
EL	8.4	126.8
469.94' S = SL. Ic. produced		
EL	10.5	124.7
C	10.3	124.9
1/4	10.2	125.6
ϕ	10.5	124.7
1/4	10.6	124.6
C	10.5	124.7
WL	8.9	126.3
80' wide 12' walks 13' 1/2 S.		
500'S = N1. High St.		
WL	12.1	123.1
C	12.2	123.0
1/4	12.5	122.7
ϕ	12.7	122.5
1/4	13.0	122.2
C	13.1	122.1
EL	13.1	122.1

15

13519		
TP.	12.87	122.32
116	123.48	
N. Curb. High St.		
EL	2.1	121.4
C	2.3	121.2
1/4	2.2	121.3
ϕ	1.8	121.7
1/4	1.4	122.1
C	1.2	122.3
WL	1.2	122.3
N 1/4		
WL	1.8	121.7
C	1.8	121.7
1/4	1.9	121.6
ϕ	2.5	121.0
1/4	2.6	120.9
C	3.0	120.5
EL	3.0	120.5

12348

Φ

EL	3.7	119.8
C	3.6	119.9
1/4	3.2	120.3
Φ	2.8	120.7
1/4	2.5	121.0
C	2.5	121.0
WL	2.5	121.0

S/A

WL	3.1	120.4
C	3.1	120.4
1/4	3.2	120.3
Φ	3.3	120.2
1/4	3.8	119.7
C	4.1	119.4
EL	4.5	119.0

S. Curb

EL	4.9	118.6
C	4.7	118.8
1/4	4.2	119.3

12348

16

Φ

1/4

C

WL

WL

C

1/4

Φ

1/4

C

EL

EL

C

1/4

Φ

1/4

C

WL

4.0 119.5

3.6 119.9

3.9 119.6

3.7 119.8

S.L. High St.

4.4 119.1

4.5 119.0

4.6 118.9

4.5 119.0

4.8 118.7

5.2 118.3

5.6 117.9

50' S.

7.7 115.8

7.1 116.4

6.6 116.9

6.5 117.0

6.6 116.9

6.7 116.8

6.4 117.1

12348

100' S.

WL	8.9	114.6
C	9.0	114.5
1/4	8.9	114.6
☉	9.0	114.5
1/4	9.3	114.2
C	9.4	114.1
EL	9.7	113.8

150' S.

FL	11.9	111.6
C	11.5	112.0
1/4	11.2	112.3
☉	11.1	112.4
1/4	11.2	112.3
C	11.3	112.2
WL	11.0	112.5

200' S.

WL	12.4	111.1
C	12.6	110.9
1/4	12.6	110.9

12348

17

☉

12.7 110.8

1/4

12.8 110.7

C

13.0 110.5

EL

13.2 110.3

T.P.

12.53 110.95

155

112.50

80' Wide  
14' Walks  
13' 1/2 S.

246.74 S - NL. Herschell.

EL

3.9 108.6

C

3.3 109.2

1/4

3.0 109.5

☉

2.4 110.1

1/4

2.2 110.3

C

2.2 110.3

WL

1.9 110.6

263.4 S - N. Curb. Produced.

WL

2.6 109.9

C

2.4 110.1

1/4

2.5 110.0

☉

2.6 109.9

1/4

3.0 109.5

C

3.4 109.1

EL

3.5 109.0

112.50

278.87'S = 1 1/4 produced

EL 3.7 108.8

C 3.7 108.8

1/4 3.4 109.1

E 3.0 109.5

1/4 2.6 109.9

C 2.3 110.2

WL 3.0 109.5

294.34'S = E Produced

WL 3.6 108.9

C 2.7 109.8

1/4 2.9 109.6

E 3.4 109.1

1/4 3.6 108.9

C 3.9 108.6

EL 4.4 108.1

309.81'S = 5/4 produced.

EL 4.7 107.8

C 4.1 108.4

1/4 4.0 108.5

112.50

18

E 3.9 108.6

1/4 4.0 108.5

C 3.7 108.8

WL 3.8 108.7

325.28'S = 5 Curb. produced

WL 4.0 108.5

C 4.1 108.4

1/4 4.2 108.3

E 4.3 108.2

1/4 4.4 108.1

C 4.2 108.3

EL 4.7 107.8

341.88'S = 5 L Herschel produced

EL 5.3 107.2

C 4.9 107.6

1/4 4.6 107.7

E 4.8 107.7

1/4 4.9 107.6

C 4.7 107.8

WL 4.1 108.4

11250

350'S. = 8.1'S of Herschel

WL	4.5	108.0
C	4.8	107.7
1/4	5.0	107.5
ϕ	5.0	107.5
1/4	4.8	107.7
C	5.0	107.5
EL	5.2	107.3

400'S. = 58.1'S

EL	6.5	106.0
C	6.5	106.0
1/4	6.5	106.0
ϕ	6.5	106.0
1/4	6.6	105.9
C	6.9	105.6
WL	6.9	105.6

425'S. = 53.1'S

WL	8.3	104.2
C	7.8	104.7
1/4	8.1	104.4

11250

19

ϕ	7.9	104.6
1/4	7.6	104.9
C	7.4	105.1
EL	7.3	105.2

450'S. = 108.1'S

EL	8.4	104.1
C	8.8	103.7
1/4	9.1	103.4
ϕ	9.3	103.2
1/4	9.3	103.2
C	9.5	103.0
WL	9.7	102.8

475'S. = 103.1'S

WL	10.8	101.7
C	11.6	100.9
1/4	11.4	101.1
ϕ	11.6	100.9
1/4	11.9	101.5
C	10.6	101.9
EL	10.0	102.5

	112.50		
T.P.	11.78	100.72	
	7.47	103.19	
	500'S = 158.1'S		
EL.	3.4	99.8	
C	2.5	100.7	
1/4	3.0	100.2	
+	4.5	98.7	
⊖	4.4	98.8	
1/4	4.9	98.3	
C	4.2	99.0	
WL.	2.3	100.9	
	525'S = 183.1'S		
WL.	2.1	101.1	
C	4.2	99.0	
1/4	6.0	97.2	
⊖	6.4	96.8	
1/4	6.0	97.2	
C	6.0	97.2	
EL.	6.9	96.3	

	103.19		
	550'S = 208.1'S		
EL.	9.0	94.2	
C	8.8	94.4	
1/4	8.6	94.6	
+	7.4	95.8	
⊖	7.7	95.5	
1/4	7.1	96.1	
C	5.3	97.9	
WL.	3.3	99.9	
	575'S = 233.1'S		
WL.	5.0	98.2	
C	7.7	95.5	
1/4	10.0	93.2	
+	8.3	94.9	
⊖	8.2	95.0	
1/4	8.3	94.9	
C	8.8	94.4	
EL.	8.2	95.0	
	258.1'S		
	600'S = NL College on Edst.		
EL.	8.6	94.6	
C	8.4	94.8	
1/4	8.6	94.6	

10319

Φ	88	94.4
1/4	10.8	92.4
1/4	10.9	92.3
C	10.6	92.6
WL	7.8	95.4

625'S

WL	10.6	92.6
C	10.9	92.3
1/4	10.1	93.1
Φ	9.1	94.1
1/4	8.9	94.3
C	9.1	94.1
EL	8.2	95.0

650'S

EL	7.5	95.7
C	8.4	94.8
1/4	8.8	94.4
Φ	9.2	94.0
1/4	9.4	93.8
C	10.9	92.3
WL	11.1	92.1

10319

21

675'S

WL	11.6	91.6
C	9.4	93.8
1/4	9.1	94.1
Φ	9.1	94.1
1/4	7.9	95.3
C	7.6	95.6
EL	6.9	96.3

698.70'S - Inters. With Grand St. on WL.

EL	7.1	96.1
C	7.4	95.8
1/4	8.2	95.0
Φ	8.8	94.4
1/4	9.2	94.0
C	9.5	93.7
WL	8.4	94.8

10219

Sec 17 = 698.66' S. 07 WL  
= 747.8' S. 07 EL - Int. with  
Girdich

WL 84 948

C 9.2 940

1/4 8.7 945

1/4 8.2 950

1/4 8.4 948

C 8.6 946

EL 7.8 954

T.P. x Gds Pipe  
SE Cor State + College 7.60 95.69

T.P. 0.30 102.89

12.11 115.00

T.P. 0.34 114.66

12.70 127.36

T.P. 0.55 126.81

11.49 138.30

B.M. .508 133.22 133.26

133.22  
04

Interpolated

Grand St. on W. to College St. on E.

W.L. 94.8

C 94.6

1/4 94.3

E 94.0

1/4 94.2

C 94.4

E.L. 94.6

SMS  
Dec. 22-13



CROSS SECTIONS  
COLLEGE ST

S.L. Prospect to E.L. State St.  
80' Wide, 20' Walks - 10' / 4's

Concrete Mon.

B.M. Cor State & Ictinus. 133.26

12.87 146.13

T.P. 0.24 145.89

11.34 157.23

T.P. 0.25 156.98

11.30 168.28

T.P. 8.92 159.36

6.20 165.56

T.P. 0.12 165.44

12.09 177.53

T.P. 0.26 177.27

12.30 189.57

T.P. 0.99 188.58

7.64 196.22

T.P. Top 2"x2" sub. SW Cor. Pros. + College. 566 190.56

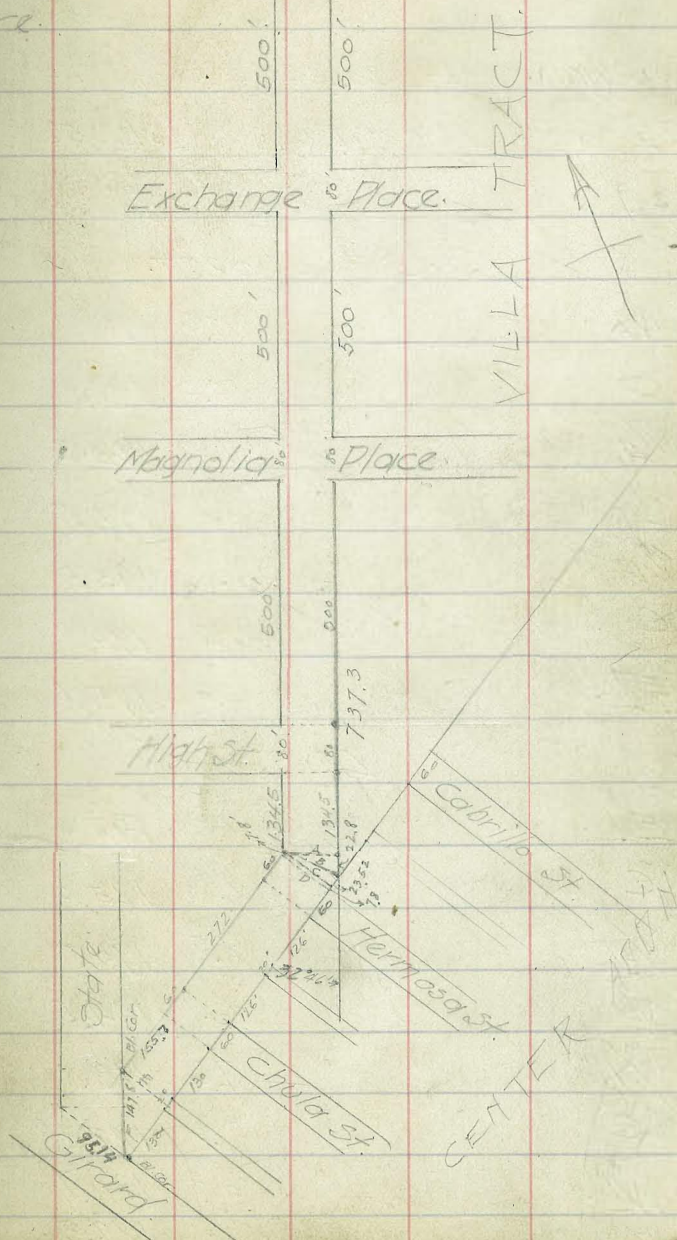
Cor Walk. 6.10 190.52

April 22-1913

West  
Evans.  
Moore.

Prospect.

23



Cor Walk 11.24 201.36 } 190.12  
 Top 2"x2" 10.80 201.36 } 190.56

## J.L. Prospect.

WL 11.6 189.8  
 C 10.0 191.4  
 1/4 9.2 192.2  
 Φ 8.7 192.7  
 1/4 7.9 193.5  
 C 6.5 194.9  
 EL 5.6 195.8

25' S

EL 4.0 197.4  
 C 6.4 195.0  
 1/4 6.5 194.9  
 Φ 6.9 194.5  
 1/4 7.6 193.8  
 C 9.3 192.1  
 WL 10.7 190.7  
 +15 12.1 189.3

201.36

50' S

-15 12.6 188.8  
 WL 10.5 190.9  
 C 9.1 192.3  
 1/4 7.3 194.1  
 Φ 5.4 196.0  
 1/4 5.3 196.1  
 C 5.6 195.8  
 EL 3.9 197.5

75' S.

EL 3.8 197.6  
 C 4.4 197.0  
 1/4 4.6 196.8  
 Φ 5.1 196.3  
 1/4 7.6 193.8  
 C 9.3 192.1  
 WL 11.0 190.4  
 -15 12.8 188.6  
 +15 12.9 188.5  
 WL 11.7 189.7  
 C 9.2 192.2  
 1/4 7.6 193.8

100' S.

20136

£	7.0	194.4
1/4	5.9	195.5
C	5.7	195.7
FL	4.0	197.4

125'S.

FL	4.5	196.9
C	6.9	195.4
1/4	6.7	194.7
£	7.3	194.1

1/4	7.7	193.7
C	9.5	191.9

WL	11.4	190.0
+15	13.0	188.4

150'S.

-15	14.0	187.4
WL	11.6	189.8

C	10.5	190.9
---	------	-------

1/4	9.0	192.4
-----	-----	-------

£	6.9	194.5
---	-----	-------

1/4	5.3	196.1
-----	-----	-------

C	5.1	196.8
---	-----	-------

FL	4.4	197.0
----	-----	-------

20136

25

175'S.

FL	3.4	198.0
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C	5.4	196.0
---	-----	-------

1/4	5.6	195.8
-----	-----	-------

£	7.3	194.1
---	-----	-------

1/4	9.7	191.7
-----	-----	-------

C	10.5	190.9
---	------	-------

WL	12.0	189.4
----	------	-------

+15	14.4	187.0
-----	------	-------

200'S.

-15	14.2	187.2
-----	------	-------

WL	11.5	189.9
----	------	-------

C	9.5	191.9
---	-----	-------

1/4	9.2	192.2
-----	-----	-------

£	8.3	193.1
---	-----	-------

1/4	6.7	194.7
-----	-----	-------

C	6.2	195.2
---	-----	-------

FL	4.7	196.7
----	-----	-------

20136

225'S.

EL	4.1	1973
C	6.1	1953
1/4	7.0	1944
Φ	8.6	1928
1/4	9.5	1919
C	10.3	1911
WL	12.3	1891
+15	13.0	1884

250'S.

-15	13.8	1876
WL	12.4	1890
C	8.8	1926
1/4	8.1	1933
Φ	8.4	1930
1/4	5.9	1955
C	4.4	1970
EL	4.1	1973

20136

275'S.

EL	4.1	1973
C	6.0	1954
1/4	6.9	1945
Φ	7.8	1936
1/4	8.2	1932
C	9.0	1924
WL	11.8	1896
+15	12.5	1889

300'S.

-15	13.1	1883
WL	11.4	1900
C	9.9	1915
1/4	9.0	1924
Φ	8.6	1928
1/4	7.6	1938
C	6.1	1953
EL	4.2	1972

26

20136

375'5

FL	3.6	197.8
C	6.5	194.9
1/4	7.7	193.7
Φ	8.6	192.8
1/4	9.1	192.3
C	9.1	192.3
WL	9.6	191.8
+15	12.0	189.4
	350'5	
-15	12.1	189.3
WL	10.9	190.5
C	10.1	191.3
1/4	9.6	191.8
Φ	8.0	193.4
1/4	6.9	194.5
C	6.2	195.2
FL	3.9	197.5

27

20136

T.P.	3.34	198.02
406	202.08	
	375'5	
EL	5.5	196.6
C	6.7	195.4
1/4	7.0	195.1
Φ	8.5	193.6
1/4	9.6	192.5
C	10.7	191.4
WL	11.7	190.4
+15	12.6	189.5
	400'5	
-15	13.4	188.7
WL	12.2	189.9
C	10.7	191.4
1/4	10.7	191.4
Φ	10.0	192.1
1/4	9.4	192.7
C	8.6	193.5
FL	6.7	195.4

20208  
425'S

EL	6.0	196.1
+3	7.9	194.2
C	9.7	192.4
1/4	10.8	191.3
⊕	11.3	190.8
1/4	12.5	189.6
C	12.3	189.8
WL	13.9	188.2
+15	15.2	186.9
	450'S	
-15	16.2	185.9
WL	15.0	187.1
C	13.2	188.7
1/4	12.8	189.3
⊕	11.4	190.7
1/4	10.3	191.8
C	10.0	192.1
+11	7.1	192.4
EL	6.7	195.4

20208

T.P.	11.56	190.52
3.81	194.33	

475'S

EL	1.4	192.9
C	3.2	191.1
1/4	4.5	189.8
⊕	5.6	188.7
1/4	6.8	187.5
C	7.7	186.6
WL	9.0	185.3
+15	10.5	183.8

80' Wide  
Graded for 20' 16" S.

500'S = NE Exchange Place.

WL	9.3	185.0
C	8.9	185.4
1/4	8.0	186.3
⊕	7.0	187.3
1/4	5.7	188.6
C	{ 4.0	195.3 } = Top.
	{ 5.5	188.8 } = at bottom
EL	{ 1.7	192.6 } = Top.
	{ 5.3	189.0 }

19433

N. Curb.

EL.	5.8	188.5
C	5.9	188.4
1/4	6.1	188.2
Φ	6.8	187.5
1/4	7.6	186.7
C	8.9	185.4
WL.	11.5	182.8

N 1/4

WL.	11.7	182.6
C	8.6	185.7
1/4	7.4	186.9
Φ	7.1	187.2
1/4	6.8	187.5
C	6.5	187.8
EL.	5.9	188.4

Φ

EL.	5.9	188.4
C	7.2	187.1
1/4	7.5	186.8

19433

29

Φ	7.6	186.7
1/4	8.3	186.0
C	9.9	184.4
WL	12.1	182.2
3/4		
WL.	12.2	182.1
C	11.0	183.3
1/4	9.8	184.5
Φ	9.2	185.1

1/4	8.7	185.6
C	8.2	186.1
EL	6.7	187.6

S. Curb.

EL.	6.6	187.7
C	8.7	185.6
1/4	9.3	185.0
Φ	10.1	184.2
1/4	10.8	183.5
C	11.4	182.9
WL	12.2	182.1

19433

## S. L. Exchange

WL	12.6	181.7
C	11.9	182.4
1/4	11.3	183.0
ϕ	10.6	183.7
1/4	9.9	184.4
C	9.0	185.3
EL	6.5	187.8

25'S

EL	6.3	188.0
+8	8.2	186.1
C	9.4	184.7
1/4	9.9	184.4
ϕ	11.0	183.3
1/4	11.4	182.9
C	12.0	182.3
WL	13.6	180.7

50'S

WL	13.4	180.9
C	11.8	182.5
1/4	10.8	183.5

19433

30

ϕ	9.6	184.7
1/4	8.2	186.1
C	7.3	187.0
+17	6.0	188.3
EL	4.6	189.7

75'S

FL	5.8	188.5
C	7.6	186.7
1/4	8.5	185.8
ϕ	9.5	184.8
1/4	10.2	184.1
C	10.4	183.9
WL	11.3	183.0
H0	13.3	181.0

100'S

-10	13.6	180.7
WL	12.6	181.7
C	11.5	182.8
1/4	10.7	183.6
ϕ	10.2	184.1
1/4	9.3	185.0
C	7.7	186.6
EL	5.5	188.8



19433

150'5.

EL	7.2	187.1
C	9.7	184.6
1/4	10.2	184.1
Φ	10.3	184.0
1/4	11.6	182.7
C	12.5	181.8
WL	13.1	181.2
+10	13.6	180.7

200'5.

-10	16.1	178.2
WL	15.6	178.7
C	16.4	178.9
1/4	15.1	179.2
Φ	13.5	180.8
1/4	12.6	181.7
C	12.0	182.3
EL	10.1	184.2

19433

31

T.P.

	12.79	181.54
165	183.19	

250'5.

EL	2.3	180.9
C	4.0	179.2
1/4	4.4	178.8
Φ	4.4	178.8
1/4	5.1	178.1
C	6.9	176.3
WL	7.2	176.0
+10	8.7	174.5

300'5.

-10	11.4	171.8
WL	10.8	172.4
C	9.2	174.0
1/4	9.0	174.2
Φ	8.7	174.5
1/4	7.5	175.7
C	7.0	176.2
EL	5.5	177.7

18319

350's.

EL	8.2	175.0
C	10.8	172.4
1/4	11.3	171.9
£	11.4	171.8
1/4	11.8	171.4
C	11.8	171.4
WL	14.4	168.8
+10	14.7	168.5
400's.		
-10	16.6	166.6
WL	16.0	167.2
C	15.6	167.6
1/4	15.4	167.8
£	14.6	168.6
1/4	13.6	169.6
C	13.2	170.0
+15	12.3	171.0
EL	10.7	172.5

32

18319<sup>4</sup>

T.P.	12.80	170.39
0.96	171.35 <sup>4</sup>	
450's.		
EL	1.7	169.7
C	3.4	168.0
1/4	4.0	167.4
£	4.9	166.5
1/4	5.1	166.3
C	6.6	164.8
WL	7.7	163.7
+10	8.0	163.4
475's.		
-10	9.7	161.7
WL	9.2	162.2
C	8.3	163.1
1/4	7.2	164.2
£	6.6	164.8
1/4	5.1	166.3
C	3.1	168.3
EL	1.2	170.2

80' Wide  
1/4 Walks

17135

13 1/4

500's - NL Magnolia

EL	2.3	169.1
C	5.5	165.9
1/4	6.6	164.8
Φ	7.7	163.7
1/4	7.8	163.6
C	8.0	163.4
NL	9.2	162.2
+10	10.6	160.8

N Carb.

-10	11.5	159.9
NL	10.0	161.4
C	8.5	162.9
1/4	8.6	162.8
Φ	8.3	163.1
1/4	7.8	163.6
C	5.6	165.8
+10 EL	3.3	168.1
	2.2	169.2

17135

N 1/4

EL	3.2	168.2
C <sup>10</sup>	4.7	166.7
	7.2	164.2
1/4	8.2	163.2
Φ	8.6	162.8
1/4	9.7	161.7
C	10.1	161.3
NL	11.5	159.9
+10	12.1	159.3

Φ Magnolia

-10	12.7	158.7
NL	12.3	159.1
C	11.3	160.1
1/4	10.5	160.9
Φ	9.3	162.1
1/4	8.6	162.8
C	7.7	163.7
EL	4.6	166.8

17/35

3/4

EL	4.8	166.6
C <sup>+12</sup>	6.3	165.1
	8.0	163.4
1/4	9.3	162.1
⊖	10.1	161.3
1/4	11.0	160.4
C	11.9	159.5
WL	12.6	158.8
+10	13.1	158.3

J. Carb.

-10	13.2	158.2
WL	12.7	158.7
C	12.2	159.2
1/4	11.1	160.3
⊖	10.5	160.9
1/4	10.0	161.4
C	9.3	162.1
C <sup>+10</sup>	6.5	164.9
EL	5.7	165.7

17/35

5L Magnolia

34

EL	7.5	163.9
C	10.1	161.3
1/4	10.6	160.8
⊖	10.9	160.5
1/4	11.5	159.9
C	12.6	158.8
WL	13.2	158.2
+10	14.3	157.1

25'S.

-10	15.0	156.4
WL	15.0	156.4
C	13.8	157.6
1/4	13.3	158.1
⊖	13.0	158.4
1/4	12.4	159.0
C	11.4	160.0
EL	8.0	163.4

		17135 <sup>1</sup>	
T.P.		12.95	158.40 <sup>1</sup>
	208	160.48 <sup>1</sup>	
	50'S		
EL		(40.4)	160.9
C		0.8	159.7
1/4		2.4	158.1
⊖		3.1	157.4
1/4		3.8	156.7
C		4.8	155.7
WL		5.0	155.5
+10		5.1	155.4
	100'S		
-10		7.7	152.8
WL		6.9	153.6
C		5.4	155.1
1/4		5.4	155.1
⊖		5.2	155.3
1/4		3.9	156.6
C		3.4	157.1
EL		2.5	158.0

		16048 <sup>1</sup>	
	150'S		
EL		5.6	154.9
C		6.2	154.3
1/4		6.4	154.1
⊖		6.5	154.0
1/4		7.8	152.7
C		8.2	152.3
WL		8.5	152.0
	200'S		
WL		10.0	150.5
C		9.6	150.9
1/4		9.6	150.9
⊖		9.5	151.0
1/4		9.3	151.2
C		8.9	151.6
EL		8.4	152.1
	250'S		
EL		10.7	149.8
C		11.7	148.8
1/4		11.7	148.8

16048

ϕ		11.8	148.7
1/4		12.1	148.4
C		12.2	148.3
WL		12.5	148.0
T.P.		12.83	147.65
	240	150.05	
		300'S	
WL		5.9	144.2
C		5.2	144.9
1/4		4.6	145.5
ϕ		3.1	147.0
1/4		1.9	148.2
C		1.5	148.6
EL		1.6	148.5
		350'S	
EL		3.8	146.3
C		4.9	145.2
1/4		5.8	144.3
ϕ		6.3	143.8
1/4		6.7	143.4

15005

36

C		7.4	142.7
WL <sup>+8</sup>		8.6	141.5
		9.3	140.8
		400'S	
WL		12.2	137.9
C		11.2	138.9
1/4		10.5	139.6
ϕ		9.4	140.7
1/4		8.8	141.3
C		8.6	141.5
EL		7.1	143.0
		450'S	
EL		12.5	137.6
C		13.1	137.0
1/4		13.8	136.3
ϕ		14.1	136.0
1/4		15.1	135.0
C		15.2	134.9
WL		15.1	135.0

15005

T.P.

80' Wide  
14' Walk

W/L

C

1/4

Φ

1/4

C

EL

EL

C

1/4

Φ

1/4

C

W/L

12.97 137.08

0.64 137.72

500' S - N.L. High St. on W. side.

6.7 131.0

6.2 131.5

5.6 132.1

5.2 132.5

4.9 132.8

4.8 132.9

4.1 133.5

N. Corb.

5.5 132.2

5.6 132.1

5.7 132.0

6.4 131.3

7.1 130.6

7.4 130.3

7.7 130.0

13772

N 1/4

W/L

C

1/4

Φ

1/4

C

EL

EL

C

1/4

Φ

1/4

C

W/L

W/L

C

1/4

8.9 128.8

8.4 129.3

8.1 129.6

7.7 130.0

7.2 130.5

6.8 130.9

6.9 130.8

Φ High

8.2 129.5

8.1 129.6

8.3 129.4

8.3 129.4

9.0 128.7

9.4 128.3

9.8 127.9

S 1/4

11.0 126.7

10.4 127.3

9.7 128.0

37

137.72

Φ	9.2	128.5
1/4	8.9	128.8
C	9.0	128.7
EL	9.3	128.4
S Curb		
EL	9.9	127.8
C	9.9	127.8
1/4	9.9	127.8
Φ	10.0	127.7
1/4	10.8	126.9
C	11.6	126.1
WL	12.2	125.5
SL High		
WL	13.0	124.7
C	12.7	125.0
1/4	12.3	125.4
Φ	11.7	126.0
1/4	11.5	126.2
C	11.2	126.5
EL	10.9	126.8

38

137.72<sup>✓</sup>

T.P.	11.60	126.12 <sup>✓</sup>
0.30	126.42 <sup>✓</sup>	
50' S High		
EL	2.0	124.4
C	2.7	123.7
1/4	3.0	123.4
Φ	3.1	123.3
1/4	3.6	122.8
C	3.6	122.8
WL	3.5	122.9
100' S		
WL	5.9	120.5
C	5.4	121.0
1/4	5.4	121.0
Φ	5.3	121.1
1/4	5.5	120.9
C	5.3	121.1
EL	4.7	121.7



12642

Sec A = 134.5' S - Angle pt on WL.

FL.	6.8	119.6
C	7.3	119.1
1/4	7.2	119.2
ϕ	6.8	119.6
1/4	6.2	120.2
C	5.7	120.7
WL.	5.8	120.6

22.8' S on EL = Angle pt Sec B - See Sketch Page 23.

WL.	5.8	120.6
C	6.2	120.2
1/4	6.7	119.7
ϕ	7.2	119.2
1/4	7.7	118.7
C	8.2	118.2
EL.	8.8	117.6

See page 23 = Sec C = 23.53' S of Sec B.

EL	9.5	116.9	on EL
C	8.5	117.9	
1/4	8.0	118.4	

12642

39

ϕ	7.5	118.9
1/4	6.9	119.5
C	6.4	120.0
WL.	5.8	120.6

60' Wide  
10' W + 1/4's.Sec D = 7.8' S of C. = N.L. Hermosa  
on E side st.

WL.	6.0	120.4
C	6.4	120.0
1/4	7.0	119.4

ϕ	7.3	119.1
1/4	8.1	118.3
C	8.5	117.9
EL	9.0	117.4

N. Curb. of Hermosa

EL.	8.5	117.9
C	8.5	117.9
1/4	8.0	118.4

ϕ	7.2	119.2
1/4	6.7	119.7
C	6.1	120.3
WL.	5.4	121.5

126.42

W 1/4

WL	4.7	121.7
C	5.9	120.5
1/4	6.6	119.8
ϕ	7.1	119.3
1/4	8.1	118.3
C	8.5	117.9
EL	9.0	117.4

ϕ Hermosa

EL	9.5	116.9
C	8.7	117.7
1/4	8.1	118.3
ϕ	7.1	119.3
1/4	6.7	119.7
C	6.1	120.3
WL	5.0	121.4

S 1/4

WL	5.5	120.9
C	6.4	120.0
1/4	6.9	119.5

126.42

40

ϕ	7.2	119.2
1/4	8.2	118.2
C	8.7	117.7
EL	9.5	116.9

S. Corb.

EL	9.6	116.8
C	8.7	117.7
1/4	8.1	118.3
ϕ	7.3	119.1
1/4	7.3	119.1
C	7.0	119.4
WL	6.7	119.7

S.L. Hermosa

WL	8.1	118.3
C	7.9	118.5
1/4	7.9	118.5
ϕ	7.8	118.0
1/4	8.4	118.0
C	8.8	117.6
EL	9.4	117.0

12642

50'S.

EL.		112	115.2
C		11.1	115.3
1/4		11.2	115.2
⊖		11.1	115.3
1/4		11.7	114.7
C		12.0	114.4
WL.		13.0	113.4
T.P.		12.89	113.53

0.87 114.40

100'S.

WL.		1.44	110.0
C		4.1	110.3
1/4		3.6	110.8
⊖		3.0	111.4
1/4		2.5	111.9
C		2.2	112.2
EL.		1.9	112.5

11440

150'S.

EL.		5.2	109.2
C		5.6	108.8
1/4		6.1	108.3
⊖		6.3	108.1
1/4		6.8	107.6
C		6.8	107.6
WL.		6.9	107.5

200'S.

WL.		8.8	105.6
C		9.0	105.4
1/4		9.0	105.4
⊖		8.8	105.6
1/4		8.7	105.7
C		8.7	105.7
EL.		8.2	106.2

250'S.

EL.		11.1	103.3
C		10.2	104.2
1/4		10.4	104.0

41

11440

Φ		10.5	103.9
1/4		11.0	103.4
C		11.6	102.8
WL		12.0	102.4
60' Wide 10' Walks. 1/4	272' S = NL Chula St.		
WL		12.5	101.9
WC		12.1	102.3
1/4		11.6	102.8
Φ		10.8	103.6
1/4		11.1	103.3
C		11.4	103.0
EL		12.2	102.2
T.P. Hub. N.E. Cor. College & Chula	12-23	102.17	
	194	104.11	
	N Corb.		
EL		2.3	101.8
C		2.1	102.0
1/4		1.7	102.4
Φ		1.5	102.6
1/4		1.8	102.3

104.11

42

C		2.1	102.0
WL		3.3	100.8
	N 1/4		
WL		3.9	100.2
C		2.3	101.8
1/4		2.3	101.8
Φ		2.4	101.7
1/4		2.7	101.4
C		3.0	101.1
EL		3.0	101.1
	Φ Chula St.		
EL		3.9	100.2
C		3.3	100.8
1/4		3.1	101.0
Φ		2.8	101.3
1/4		2.4	101.7
C		2.4	101.7
WL		4.4	99.7

104.11

5 1/4

WL	4.9	99.2
C	2.9	101.2
1/4	3.1	101.0
⊕	3.2	100.9
1/4	3.8	100.3
C	4.0	100.1
EL	4.3	99.8

S. Curb.

EL	5.0	99.1
C	4.7	99.4
1/4	4.7	99.4
⊕	4.2	99.9
1/4	3.7	100.4
C	3.5	100.6
WL	5.2	98.9

S.L. Chulq sf

WL +10	5.6	98.5
C	5.5	98.6
C	4.3	99.8
1/4	4.5	99.6

104.11

43

⊕	5.3	98.8
1/4	5.7	98.4
C	5.8	98.3
EL	5.6	98.5

25' S

EL	4.8	99.3
<sup>78</sup>	4.5	99.6
C	5.4	98.7
1/4	6.7	97.4
⊕	7.0	97.1
1/4	7.2	96.9
C	6.9	97.2
WL	6.5	97.6

50' S

WL	7.6	96.5
C	7.9	96.2
1/4	7.5	96.6
⊕	6.3	97.8
1/4	5.8	98.3
C	5.5	98.6
EL	5.2	98.9

104.11

75'S

EL.	55	98.6
C	60	98.1
1/4	6.3	97.8
1/4	6.8	97.3
1/4	7.0	97.1
C	7.3	96.8
WL.	9.4	94.7
+10	9.0	95.1

100'S

WL.	8.4	95.7
C	7.9	96.2
1/4	7.6	96.5
1/4	7.1	97.0
1/4	6.6	97.5
C	6.4	97.7
EL.	5.7	98.4

104.11

44

Sec E. 155'6'S = Int on WL with State

EL.	6.3	97.8
C	7.0	97.1
1/4	7.5	96.6
1/4	7.8	96.3
1/4	8.4	95.7
C	8.8	95.3
WL.	9.5	94.6

Int with  
State on EL.Sec F. = 280'S on EL. 155.7 on  
WL.

WL.	9.5	94.6
C	8.8	95.3
1/4	8.7	95.4
1/4	7.8	96.3
1/4	8.0	96.1
C	8.0	96.1
EL.	8.7	95.4

T.P. Gas Pipe.

8.52 95.59 95.59

Check's OK.



349.5

349.2

1138 E = Angl. of Insein in S

S	60	43.2
	60	43.2
	55	43.7
b	47	44.5
	48	44.4
	48	44.4
n	46	44.6

150 E of Louisiana

n	47	44.5
	47	44.5
	49	44.3
b	48	44.4
	54	43.8
	38	45.4
S	44	44.8

349.5

349.2

208 E of Louisiana

S	50	44.2
	57	43.5
	52	44.0
	49	44.3
l	50	44.2
	46	44.6
	42	45.0

n 208 E = E of Insein n

n 2

250 E of Louisiana

n	29	46.3
	38	45.4
	46	44.6
b	43	44.9
	45	44.7
	45	44.7
S	48	44.3

46



34915

349.2

(Graded)

340' E = rd Texasst (50)

S 2

(32)  
(38) 44.0  
45.4

bl

(23)  
(41) 44.9  
45.1

y

44 44.8

b

38 44.4

y

42 45.0

h

40 45.2

na

38 45.4

TP

1062 355.96

381 345.34

m

E line of Texas

356.0

97 46.3

99 44.1

102 45.8

b

100 46.0

102 45.8

99 44.1

S

96 46.4

+

356.0

47

50

E of Texas

S

94 46.6

93 46.7

90 47.0

L

89 47.1

92 46.8

77 48.3

n

70 49.0

100

E of Texas

n

70 49.0

70 49.0

72 48.8

b

70 49.0

72 48.8

77 48.3

S

79 48.1

34915  
361  
345.34  
1062  
355.96

353.96

356.0

150 E of Texas

S	46	51.4
	47	51.3
	40	52.0
b	33	52.7
	42	51.8
	41	51.9
n	34	52.4

TP 1239 367.1 063 355.23

200 E of Texas

347.7

n	106	57.1
	160	57.7
	105	57.2
y	127	55.5
	108	54.9
	111	54.6
	115	55.2
S	120	55.7

367.71

367.7

250 E of Texas

S	69	40.8
	67	41.0
	61	41.4
b	58	41.9
	70	40.7
	60	41.7
	61	41.4
n	58	41.9

275 E of Texas

n 25 45.2

300 E of = West of Arizona (80)

n	18	45.9
	16	44.1
	22	45.5
b	13	44.4
	16	44.1
	25	44.3
S	25	45.2

TP 1195 378.74 097 366.79

X Sec of Arizona Insects is in B 876 P 42

Madison

48

353.96  
 63  
 355.33  
 1.38  
 367.71  
 .92  
 366.79  
 11.95  
 378.74

37874

3787

E side of Arizona

S

86 70.1

83 70.4

78 70.9

b

77 71.0

84 70.3

81 70.6

n

74 71.3

50 E of Arizona

n

57 73.5

58 72.9

64 72.3

b

58 72.9

61 72.6

54 73.3

S

60 72.7

37874

3787

Mason

49

100 E of Arizona

S

46 74.1

45 74.2

44 74.3

b

40 74.7

45 74.2

44 74.3

n

40 74.7

150 E of Arizona

n

37 75.5

31 75.6

34 75.3

b

29 75.8

31 75.6

32 75.5

S

38 74.9

378.74

378.7

175'

2 f

Arizona

S

37 75.0

16 77.1

10 77.7

b

23 76.4

34 75.3

33 75.4

n

20 76.7

200'

3 f

Arizona

n

19 76.8

27 76.0

28 75.9

b

21 76.4

23 76.4

28 75.9

S

27 76.0

378.74

378.7

200'

2 f

Arizona

S

23 76.4

18 76.9

16 77.1

b

12 77.5

20 76.7

70'

0.0 78.7

1.3 77.4

n

00 78.7

834

38610

099

277.76

300'

2 = 482 of

Hamilton (50)

Graded

n

84.1 74 78.7

75 78.6

84 77.7

b

80 78.1

82 77.9

S

82 77.9

79 78.2

Measure

50

378.74  
98  
377.76  
378.11

38610

84.1

E 100' of Hamilton

S	69	79.2
	71	79.0
	74	78.7
b	68	79.3
	73	78.7
	66	79.5
n	63	79.8

50' E of Hamilton

n	63	79.8
	69	79.2
	71	79.0
b	64	79.7
	69	79.2
	68	79.3
S	68	79.3

38610

84.1

100' E of Hamilton

S	65	79.6
	67	79.4
	64	79.7
b	61	80.0
	66	79.5
	50	81.1
	66	79.5
n	68	79.3

150' E of Hamilton

n	62	79.9
	52	80.9
	48	81.3
	60	80.1
b	58	80.3
	63	79.8
	61	80.0
S	60	80.1

Madison

51

38610

81.1

200 E of Hamilton

s	58	80.3
	57	80.4
	58	80.3
b	54	80.7
	60	80.1
	58	80.3
n	53	80.8

250 E of Hamilton

n	55	80.6
	59	80.2
+10	47	81.4
	58	80.3
b	51	81.0
	55	80.6
	57	80.4
s	53	80.8

38610

81.1

300 E = W of Oregon st (80) 52

s	57	80.4
	50	81.1
	51	81.0
b	49	81.2
	55	80.6
	55	80.6
n	55	80.6

TP 412 38460 560 38050

84.5 E side of Oregon st

n	43	80.5
	40	80.6
	40	80.6
b	36	81.0
	37	80.9
	27	81.9
s	37	80.9

38610  
560  
38050  
412  
38462

38462

84.4

50 EJ Oregon

S 46 80.0

76

33 81.3

24 82.2

40 80.6

b 38 80.8

43 80.3

45 80.1

n 42 80.4

100 EJ Oregon

n 49 79.7

50 79.4

46 80.0

b 43 80.3

44 80.3

45 80.1

S 49 79.7

38462

84.4

150 EJ Oregon

S 44 80.2

52 79.4

48 79.8

b 46 80.0

48 79.8

50 79.6

n 36 81.0

200 EJ Oregon

n 61 78.5

55 79.1

59 78.7

b 53 79.3

56 79.0

63 78.3

S 49 79.7

Madison

53

384.60

84.6

250 E 8. Oregon

S 62 78.4

60 78.6

60 78.6

b 56 79.0

63 78.3

63 78.3

n 61 78.5

300 E = W line of Idaho at (80)

a 52 79.4

52 79.4

56 79.0

b 53 79.3

56 79.0

on curb (6.0) 78.6

on grade (4.8) 79.8

(6.8) 77.8

S

TP 350 382.97 515 379.47

382.97

83.0

E line of Idaho at

Madison

54

S 39 79.1

40 79.0

45 78.5

b 40 79.0

44 78.6

5.0 better 42 78.4

to curb 40 79.0

curb side walk on in on North

side of street Idaho at Alley

50' E of Idaho

n curb curb 43 78.7

5.3 77.7

5.0 78.0

b 48 78.2

5.2 77.8

5.5 77.5

S 58 77.2

384.60  
5.15  
379.45  
350  
382.97



38297

83.0

	100	EJ	Idaho	
S			59	77.1
			61	74.9
			53	77.7
b			47	78.3
			51	77.9
nbl			52	77.8
			45	78.5
	150	EJ	Idaho	
n			56	77.4
bb			50	78.0
			56	77.4
b			50	78.0
			51	77.9
			55	77.5
S			56	77.4

28297

83.0

Madison

55

	200	EJ	Idaho	
S			59	77.1
			55	77.5
			55	77.5
b			50	78.0
			56	77.4
			53	77.7
n			50	78.0
	250	EJ	Idaho	
n			48	78.2
			50	78.0
			55	77.5
b			50	78.0
			54	77.6
			56	77.4
S			47	78.3

38297

83.0

300 E = N of Octah 1st (80')

S 50 78.0

60 77.0

57 77.3

b 51 77.9

55 77.5

50 78.0

n 49 78.1

W 6th of Octah

n 49 78.1

50 78.0

53 77.7

b 50 78.0

55 77.5

60 77.0

S 59 77.1

38297

83.0

W 1/4 of Octah 1st

S 60 77.0

61 76.9

55 77.5

b 48 78.2

52 77.8

54 77.6

n 51 77.9

center of Octah

n 53 77.7

52 77.8

51 77.9

b 48 78.2

53 77.7

59 77.1

S 60 77.0

Madison

56

38297

83.0

E 1/4 of Aitah

S 6.2 76.8

6.0 77.0

5.5 77.5

b 4.9 78.1

5.5 77.5

5.6 77.4

n 5.6 77.4

E 1/4 of Aitah

n 5.3 77.7

5.3 77.7

5.5 77.5

b 5.0 78.0

5.5 77.5

6.0 77.0

S 6.1 76.9

38297

83.0

E 1/4 of Aitah

S 6.4 76.5

5.7 77.2

5.2 77.8

T 5.0 78.0

5.8 77.2

5.5 77.4

n 5.4 77.6

TP 5.35 381.89 643 376.94

4.0 81.9 E 1/4 of Aitah

S 3.4 78.5

5.0 E 1/4 of Aitah

S 4.0 77.7

4.8 77.1

4.5 77.4

b 3.9 78.0

4.7 77.2

4.2 77.7

n 4.1 77.8

Median

57

382.97  
643  
376.94  
535  
381.89

4.5 E 1/4 of Aitah

381.89

81.9

100

E of

Water

n

41 77.8

43 77.6

44 77.7

b

41 77.8

43 77.6

48 77.1

s

50 76.9

125

E of

Water

s

33 78.6

150

E of

Water

s

50 76.9

50 76.9

46 77.3

b

44 77.5

47 77.2

44 77.5

n

43 77.6

175

E of

Water

s

35 78.4

381.89

81.9

200

E of

Water

n

46 77.3

45 77.4

49 77.0

b

43 77.6

49 77.0

52 76.7

s

50 76.9

225

E of

Water

s

35 78.4

250

E of

Water

s

54 76.5

51 76.8

48 77.1

b

42 77.7

46 77.3

44 77.5

n

40 77.9

280

E of

Water

8

51 76.8

42

38 78.1

710

28 79.1

4

47 77.3

Madison

58

38189

81.9

300 E = W of Kansas 1/4 (80')

n 40 77.9

43 77.4

43 77.6

b 38 78.1

46 77.3

75 40 77.9

47 77.2

S 52 74.7

TP 698 38392 495 37694

83.9 E of Kansas 1/4

S 50 78.9

60 77.9

57 78.2

b 57 78.8

57 78.2

58 78.1

n 56 78.3

38392

83.9

20 E of Kansas

n 32 80.7

48 79.1

52 78.3

b 51 78.8

60 77.9

45 79.4

S 56 78.3

50 E of Kansas

S 30 80.9

41 79.8

51 78.8

b 44 79.5

49 79.0

30 80.9

n 44 79.5

Madison

59

38189  
291  
376.94  
698  
380.92

38392

83.9

75' E of Kansas

n	44	79.5
	42	79.7
	43	79.6
b	40	79.9
	49	79.0
	50	78.9
S	48	79.1

100' E of Kansas

S	38	80.1
	46	78.3
	40	79.9
b	33	80.6
	40	79.9
	38	80.1
n	20	81.9

38392

83.9

125' E of Kansas

n	30	80.9
	37	80.2
	33	80.6
b	28	81.1
	36	80.3
	26	81.3
S	32	80.7

150' E of Kansas

S	20	81.9
	28	81.1
	28	81.1
b	20	81.9
	26	81.3
	28	81.1
n	15	82.4

Madison

60

38392

83.9

175' E of Kansas

n		16	82.3
		0.2	82.7
	76'	0.1	82.7
		2.0	81.9
		2.0	81.9

b		17	82.3
		25	81.4
		26	81.3

S		20	81.9
---	--	----	------

TP	570	38825	137	38205
----	-----	-------	-----	-------

	200	88.3	28	Kansas
--	-----	------	----	--------

S		45	82.8
		60	82.3
		59	
		62	82.1

b		55	82.8
		60	82.3
		66	81.7

n		57	82.5
---	--	----	------

38825

88.3

225' E of Kansas

a		47	83.4
		47	83.6
		54	82.9

b		50	83.3
		56	82.7

		54	82.9
--	--	----	------

S		60	82.3
---	--	----	------

	250	88	Kansas
--	-----	----	--------

S		50	83.3
---	--	----	------

		44	83.9
		52	83.1

b		44	83.9
---	--	----	------

		51	83.2
--	--	----	------

		53	83.0
--	--	----	------

n		52	83.1
---	--	----	------

		46	
--	--	----	--

Medison

61

38392  
137  
38205  
570  
38825

38825  
88.3

275

E of

Kansas

n

46 83.7

33 85.0

46 83.7

s

40 84.3

48 83.5

50 83.3

s

49 83.4

Nebraska

300

E = W of

300 ft (80)

s

36 84.7

46 83.7

46 83.7

s

37 84.4

42 84.1

37 84.4

n

41 84.2

38825  
88.3

Nebraska

Nebraska

62

E of

300 ft

n

22 86.1

25 85.8

33 85.0

s

25 85.8

31 85.2

31 85.2

s

33 85.0

50

E of

Nebraska

s

24 85.9

23 86.0

23 86.0

s

18 86.5

25 85.8

13 87.0

n

10 87.3

75 E

n

20 86.3



38825

88.3

100

E 7

Nebraska

n

01 88.3

+10

09 87.4

00 88.3

15 86.8

b

10 87.3

14 86.9

15 86.8

s

18 86.5

TP

586

39297

106

38711

150

E 7

300

v

s

60 87.0

64 86.6

56 87.4

b

48 88.2

54 87.6

55 87.5

n

55 87.5

39297

93.0

200

E 7

30

n

57 87.9

59

35 89.5

36 89.4

48 88.2

51 87.9

b

49 88.1

56 87.4

+10

40 89.0

40 89.0

s

50 88.0

200

E 8

30

s

50 88.0

54 87.5

50 88.0

b

45 88.5

49 88.1

49 88.1

n

50 88.0

Madison

63

38825

100

38711

586

39297

392.17

93.0

250 E of NEBIORSKO

n 30 90.0

34 89.5

48 88.2

42 88.8

46 88.4

41 88.9

S 52 87.8

300 E of WA Ohio (80) (Gunder)

S 38 89.2

on emb 41 88.9

45 88.5

b 43 88.7

43 88.7

on emb 41 88.9

n 38 89.2

392.97

93.0

Modison

64

E of Ohio (80) (Gunder)

n 39 89.1

41 88.9

44 88.6

b 41 88.9

42 88.8

41 88.9

S 38 89.2

TP 410 388.57 TP on emb

TP 511 392.46 392 88.95

486 392.73 390 390.26

50 93.7 486 392.73 388.57

E of Ohio (80) 486 392.73 388.57

S 54 88.3

on emb 52 88.5

n 50 88.7

l 44 89.3

53 88.4

53 88.4

n 47 89.0

392.97

486

388.57

392.97

392

388.57

486

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

390.26

29373

93.7

100

E of

Ohio st

n

46 89.1

47 89.0

50 88.7

b

44 89.3

51 88.6

52 88.5

s

54 88.3

150

E of

Ohio

s

53 88.4

53 88.4

51 88.6

b

43 89.4

48 88.9

48 88.9

n

48 88.9

29373

93.7

200

E of

Ohio st

n

50 88.7

48 88.9

53 88.4

b

47 89.0

50 88.7

52 88.7

s

43 89.4

250

E of

Ohio

s

51 88.6

40 89.7

50 88.7

b

44 89.3

51 88.6

48 88.9

n

48 88.9

Madison

65



393.70  
93.7

Acute of Jura + Boundary

S	41	89.6
	45	89.2
	53	88.4
b	46	89.1
	50	88.7
	49	88.8
n	50	88.7

E 1/4 of Jura + Boundary

n	46	89.1
	48	88.9
	51	89.6
b	45	89.2
	52	88.5
	52	88.5
S	51	88.6

393.70

93.7

Proctor

67

E 1/4 of Jura + Boundary

S	42	89.5
	52	88.5
	50	88.7
b	45	89.2
	52	88.5
	48	88.9
n	48	88.9

(83.2) E 1/4 Boundary

n	50	88.7
	49	88.7
	51	88.7
b	46	89.1
	50	88.7
	51	88.6
S	51	88.6



34966

(349.7)

150 nE of Park Blm

S	42	345.5
	45	345.2
	48	344.9
b	47	345.0
	48	344.9
	44	345.3
n	47	345.0

200 nE P-B

n	40	345.7
	45	345.2
	43	345.4
b	42	345.5
	43	345.4
	40	345.7
S	40	345.7

34966

(349.7)

250 nE of Park Blm

S	37	346.0
	36	346.1
	37	346.0
b	42	345.5
	38	345.9
	42	345.5
n	37	346.0

n. 281' nE of  
S. 272' nE of

Seymour St or School

n	35	346.2
	35	346.2
	40	345.7
b	40	345.7
	38	345.9
	34	346.3
S	48	345.2

Mission

69





349.95

100' n e y Surge

S		71	342.8
		60	343.9
	+8	55	344.4
	+10	9.6	339.9
b		9.6	340.3
		9.7	340.2
	+3	6.2	343.7
		5.7	344.2
n		4.7	345.2

150' n e y Surge

n		4.8	345.1
n		6.2	343.7
	+8	12.0	337.9
y		12.3	337.6
b		12.3	337.6
y		12.3	337.6
	+2	8.2	341.7
n		8.8	341.1
S		11.3	338.6

349.95

(349.9)

160' s e y Surge

S		12.0	337.9
		10.6	339.3
	+22	14.8	335.1
	+24	14.0	335.9
n		13.6	336.3
b		13.0	336.9
		13.0	336.9
		13.4	336.5
		13.4	336.5
		6.5	343.4
n	+8	6.4	343.5
	+20		

7P 110 342.4 860 341.35

200' s e y Surge

n		0.4	341.0
		1.0	341.4
	+8	8.0	334.4
	+12	8.4	334.0
		8.5	333.9
b		7.9	334.5
		8.5	333.9
		8.5	333.9
	+12	6.7	335.7
n		9.8	334.6
S			

Missouri

71

349.95  
~~860~~  
 241.35  
 110  
 342.45

34245

342.4

250' n E of George

S	161	326.3
	130	329.4
	120	330.4
b	114	331.0
	118	330.6
	98	332.6
n	76	334.8

298

281

n E = w of Florida Sta S

n	118	330.6
---	-----	-------

TP	0.68	330.63	1310	329.35
----	------	--------	------	--------

5.15

330.02

~~330.02~~ 224.54

b	21	328.0
---	----	-------

	15	328.6
--	----	-------

b	18	328.3
---	----	-------

	25	327.6
--	----	-------

	37	326.4
--	----	-------

S	62	323.9
---	----	-------

This section should have been taken 120 feet further east or at 298.0' from station point

34245  
13.20  
329.35  
65  
330.05  
41.75  
0

33111

330.1

293

281

n E of S } = w of Florida

298

271.8

(80) \* 72

(1435)

S

(40.6)

(11.0)

b

(40.6)

n

0.27

325.11

324.84

near n w summit Florida

(1435)

End of Florida

(325.1)

n

(40.6)

b

(40.6)

S

\* Two Florida 60' wide sea

The End of this Book

See Page

See Page

✓

325.11

(120) E of Florida n n  
78.8 n E of Florida n S) - 0.0

S  
b  
This section should  
have been taken  
with the West  
96 315.5  
77 317.4  
70 318.1  
60 319.1  
66 318.5  
65 318.6  
54 319.7

6 <sup>112.0</sup> n E of Florida = S of Monroe n n  
act. 60' n. instead of 80'

92 53 319.8  
25' n of Florida  
72 50 320.1  
710' 48 320.3

325.11

325.1

620,  
50 n E of Florida

n  
80 317.1  
82 316.9  
82 316.9  
b  
74 317.7  
82 316.9  
88 316.3  
S  
97 315.4

112.0  
45.0 n E of Florida

S  
789 314.2  
100 315.1  
94 315.7  
b  
83 316.8  
90 316.1  
96 315.5  
n  
87 316.4

73

32571

162.0  
~~158~~

NE of Florida

n	76	317.5
	87	316.4
	81	317.0
b	81	317.0
	89	316.2
	90	316.1
s	88	316.3

164.2  
~~158.2~~

NE = NE of Monroe St in n

n	75	317.6
---	----	-------

200.8

~~188.8~~

NE = S of Monroe St in S

s	69	318.2
	77	317.4
	80	317.1
b	72	317.9
	78	317.3
	67	318.4
n	62	318.9

32571

212.0  
~~200~~

NE of Florida

n	48	320.3
	60	319.1
	65	318.6
b	60	319.1
	66	318.5
	62	318.9
s	55	319.6

262.0

~~250~~

NE of Florida

s	30	322.1
	36	321.5
	41	321.0
b	33	321.8
	38	321.3
	37	321.4
n	33	321.8
	70	319.7
	71	319.7
	345	321.66

Missouri

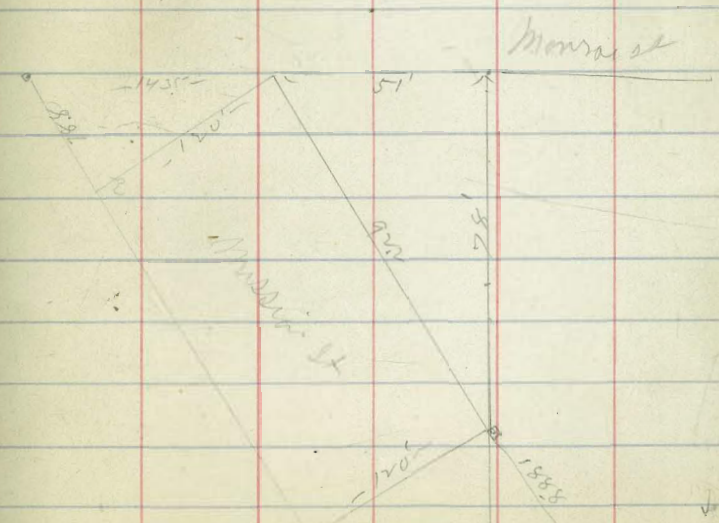
74

315.1  
- 0.38  
315.6  
- 2.21  
313.39

	293.0	329.57		
	281	329.4		
		NE = W2 Alabama St (80)		
n		71	322.3	
		73	322.1	
		71	322.3	329.37
b		65	322.9	324.49
		73	322.1	
		67	322.7	
s		66	322.8	
	293.0			
1435	281	NE = W2 Alabama St		
	359.8	NE =		
s	311.8	66	322.8	
		62	323.2	329.37
		62	323.2	326.83
b		58	323.6	
		57	323.7	
		53	324.1	
n		45	324.9	
Bm		484	324.99	Bm SW Monroe
TP		250	326.87	5' E of Belton rd

The Triangle of Monroe & Alabama St  
Bm 75

	288	327.7		324.49
				288
				327.31
			327.4	
SE Ch of Monroe		91	318.3	
25 E of Monroe		69	320.5	
50 "		67	320.7	
75' "		51	322.3	
78' = W2 Alabama St		42	323.2	
51' = S2 "		46	322.8	
51' W		53	322.1	
86' "		78	319.6	
92' W = Sd Monroe		71	318.3	



(1425)

8/3

335.00

326.87

TP Pay, 75

E. side of Alabama

326.57

n

67

328.3

n

on study 8  
(8.2)

327.2

326.8

510  
335.00

70

328.0

405

88

326.2

64

328.6

89

326.1

b

57

329.3

b

90

326.0

66

328.4

88

326.2

50

330.0

on study 96  
(8.6)

325.4 #

327.0

s

40

331.0

405

on study 93  
(8.7)

325.7

327.0

100

on E of

Alabama

s

00 on  
78.8 in

n

s

= 00

s

34

331.6

s

57

329.3

33

331.7

67

328.3

46

330.4

76

327.4

b

43

330.7

b

76

327.4

50

330.0

76

327.4

52

329.8

n

78

327.2

n

54

329.6

n

82

326.8

335.00

Missile

76

335.00

150' n.e. of Alabama

n	36	331.4
	23	332.7
	26	332.4
b	22	332.8
	27	332.3
	17	333.3
s	05	334.5

200' n.e. of Alabama

s	405	335.5
	02	334.8
	12	333.8
b	05	334.5
	08	334.2
	13	333.7
n	18	333.2

TP 697 341.65 032 334.68

341.65

341.6

Missouri

77

250' n.e. of Alabama

n	72	334.4
	62	335.4
	63	335.3
b	59	335.7
	68	334.8
	55	336.1
s	45	337.1

280' n.e. of Alabama = W of Missouri

s	42	337.4
	48	336.8
	58	335.8
b	52	336.4
	58	335.8
	59	335.7
n	63	335.3

335.00  
 334.68  
 697  
 341.65

341.6

341.6

281?  
141  
3598on S } = W 2 y Mississippi 80  
m n }

(1435)

n

405

53 336.3

47 336.9

54 336.2

b

45 337.1

49 336.7

44 337.2

405

S

41 337.5

(1435)

E Long of Mississippi W

S

405

43 337.3

41 337.5

40 337.6

b

34 338.2

38 337.8

36 338.0

405

n

37 338.2

341.6

341.6

00 on n } = 40  
788 r S }

Missouri

78

n

34

338.2

33

338.3

33

338.3

b

29

338.7

35

338.1

34

338.2

38

337.8

(1435)

S 2 2 S Mississippi

S

32

338.4

24

339.2

32

338.4

b

21

339.5

26

339.0

25

339.1

n

27

338.9



34165

341.6

100' n E of Mississippi

n 19 339.7

18 339.8

20 339.6

b 14 340.2

21 339.5

15 340.1

s 0.5 341.1

TP 6.70 340.8 1.57 340.8

150' n E of Mississippi

346.8

s 50 341.8

54 341.4

58 341.0

b 54 341.4

58 341.0

58 341.0

n 57 340.9

34678

346.8

200' n E of Mississippi

n 56 341.2

53 341.5

53 341.5

b 48 342.0

55 341.3

48 342.0

s 45 342.3

250' n E of Mississippi

44 342.4

44 342.4

50 341.8

b 43 342.5

48 342.0

46 342.2

n 42 342.6

Mississippi

79

341.65
1.57
340.08
6.70
346.78

346.78

(346.8)

281 n E = W2 Louisiana or S

2	43	342.5
40.5		
	41	342.7
	48	342.0
6	41	342.7
	50	341.8
	47	342.1
46.5		
8	51	341.7

330.8 n E or n S = Madison 15

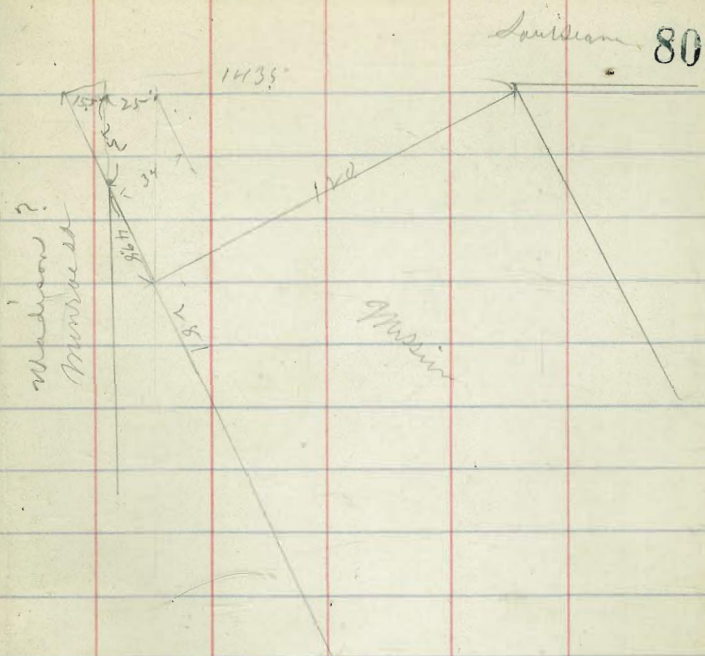
n	45	342.3
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(128') W2 of Louisiana or

3	51	341.7
46.5		
	56	341.2
	53	341.5
6	53	341.5
	53	341.5
66	55	341.3
725' S2 Madison	47	342.1
Br	258	344.2

T 12 on p

45



The Intersection of Mission  
 & Florida St for 60' width.  
 From Page 72  
 0.30 323.14 324.87 mm

(1435) The West side of Florida St  
 Parallel to 10.28 the same as P 72

n 405	16	323.5
	19	323.7
	16	323.5
b	09	324.1
	09	324.2
	18	323.3
405 S	25	322.6
The E Side of Florida		
Parallel to 10.28 the same as P 72		
S 405	78	317.3
	58	319.3
	48	320.3
b	46	320.5
	53	319.8
	53	319.8
405 n	52	319.9

See page 4, Book 900 for  
 extra notes

STANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
7.00	7.15	7.30	7.45	7.60	7.75	7.90	8.05	8.20	8.35	0
8.50	8.65	8.80	8.95	9.10	9.25	9.40	9.55	9.70	9.85	1
10.00	10.15	10.30	10.45	10.60	10.75	10.90	11.05	11.20	11.35	2
11.50	11.65	11.80	11.95	12.10	12.25	12.40	12.55	12.70	12.85	3
13.00	13.15	13.30	13.45	13.60	13.75	13.90	14.05	14.20	14.35	4
14.50	14.65	14.80	14.95	15.10	15.25	15.40	15.55	15.70	15.85	5
16.00	16.15	16.30	16.45	16.60	16.75	16.90	17.05	17.20	17.35	6
17.50	17.65	17.80	17.95	18.10	18.25	18.40	18.55	18.70	18.85	7
19.00	19.15	19.30	19.45	19.60	19.75	19.90	20.05	20.20	20.35	8
20.50	20.65	20.80	20.95	21.10	21.25	21.40	21.55	21.70	21.85	9
22.00	22.15	22.30	22.45	22.60	22.75	22.90	23.05	23.20	23.35	10
23.50	23.65	23.80	23.95	24.10	24.25	24.40	24.55	24.70	24.85	11
25.00	25.15	25.30	25.45	25.60	25.75	25.90	26.05	26.20	26.35	12
26.50	26.65	26.80	26.95	27.10	27.25	27.40	27.55	27.70	27.85	13
28.00	28.15	28.30	28.45	28.60	28.75	28.90	29.05	29.20	29.35	14
29.50	29.65	29.80	29.95	30.10	30.25	30.40	30.55	30.70	30.85	15
31.00	31.15	31.30	31.45	31.60	31.75	31.90	32.05	32.20	32.35	16
32.50	32.65	32.80	32.95	33.10	33.25	33.40	33.55	33.70	33.85	17
34.00	34.15	34.30	34.45	34.60	34.75	34.90	35.05	35.20	35.35	18
35.50	35.65	35.80	35.95	36.10	36.25	36.40	36.55	36.70	36.85	19
37.00	37.15	37.30	37.45	37.60	37.75	37.90	38.05	38.20	38.35	20
38.50	38.65	38.80	38.95	39.10	39.25	39.40	39.55	39.70	39.85	21
40.00	40.15	40.30	40.45	40.60	40.75	40.90	41.05	41.20	41.35	22
41.50	41.65	41.80	41.95	42.10	42.25	42.40	42.55	42.70	42.85	23
43.00	43.15	43.30	43.45	43.60	43.75	43.90	44.05	44.20	44.35	24
44.50	44.65	44.80	44.95	45.10	45.25	45.40	45.55	45.70	45.85	25
46.00	46.15	46.30	46.45	46.60	46.75	46.90	47.05	47.20	47.35	26
47.50	47.65	47.80	47.95	48.10	48.25	48.40	48.55	48.70	48.85	27
49.00	49.15	49.30	49.45	49.60	49.75	49.90	50.05	50.20	50.35	28
50.50	50.65	50.80	50.95	51.10	51.25	51.40	51.55	51.70	51.85	29
52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	30
53.50	53.65	53.80	53.95	54.10	54.25	54.40	54.55	54.70	54.85	31
55.00	55.15	55.30	55.45	55.60	55.75	55.90	56.05	56.20	56.35	32
56.50	56.65	56.80	56.95	57.10	57.25	57.40	57.55	57.70	57.85	33
58.00	58.15	58.30	58.45	58.60	58.75	58.90	59.05	59.20	59.35	34
59.50	59.65	59.80	59.95	60.10	60.25	60.40	60.55	60.70	60.85	35
61.00	61.15	61.30	61.45	61.60	61.75	61.90	62.05	62.20	62.35	36
62.50	62.65	62.80	62.95	63.10	63.25	63.40	63.55	63.70	63.85	37
64.00	64.15	64.30	64.45	64.60	64.75	64.90	65.05	65.20	65.35	38
65.50	65.65	65.80	65.95	66.10	66.25	66.40	66.55	66.70	66.85	39
67.00	67.15	67.30	67.45	67.60	67.75	67.90	68.05	68.20	68.35	40

Calculated by F. E. Paradis, C. E.

**DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING**

ROADWAY 16 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4

Calculated by F. E. Paradis, C. E.

