

895

F.B. 895

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LEVEL BOOK

373

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# KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO.

SAN FRANCISCO.

ST. LOUIS.

**MICROFILMED**

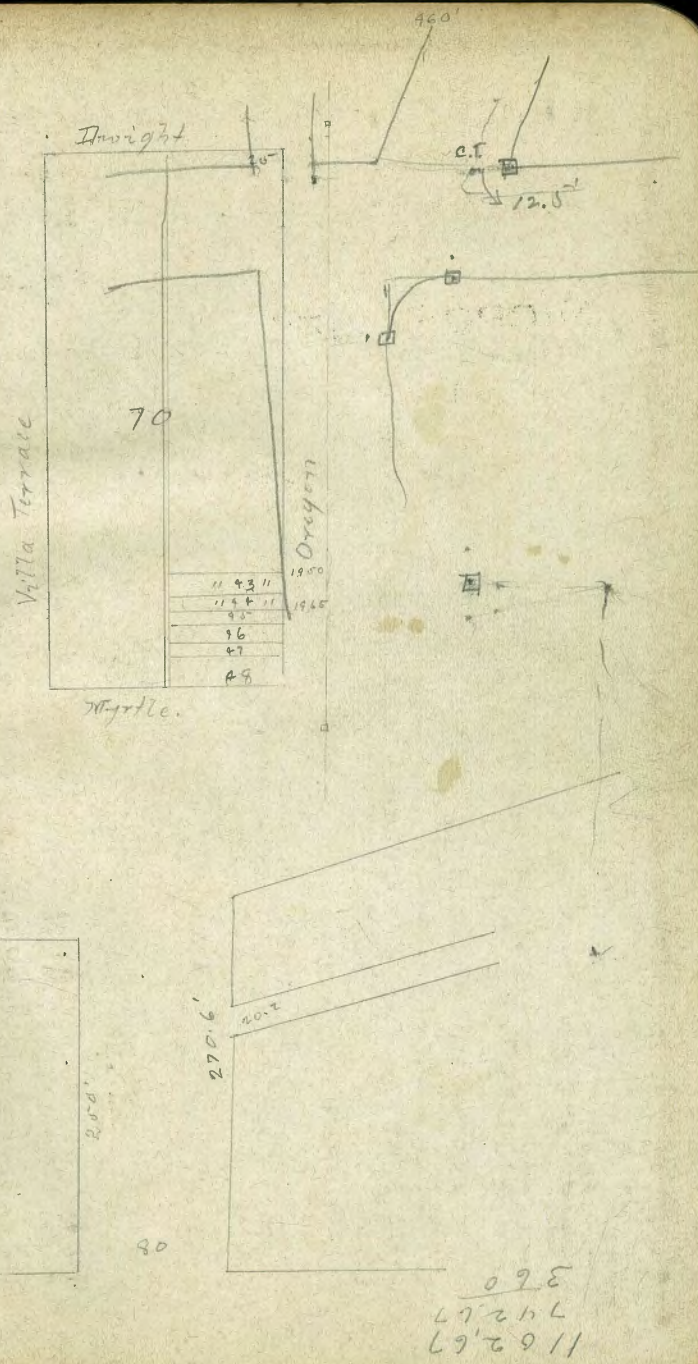
TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 10 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1885, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.



Section of Nebraska St. 30 wide, 14 walks, 12 quarters,  
from the North line of Adams Ave. to the South line of  
Worley St.

1

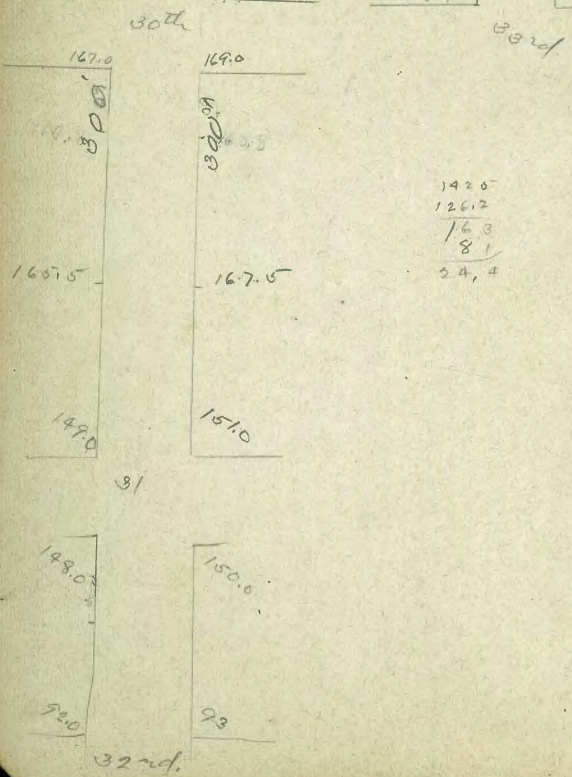
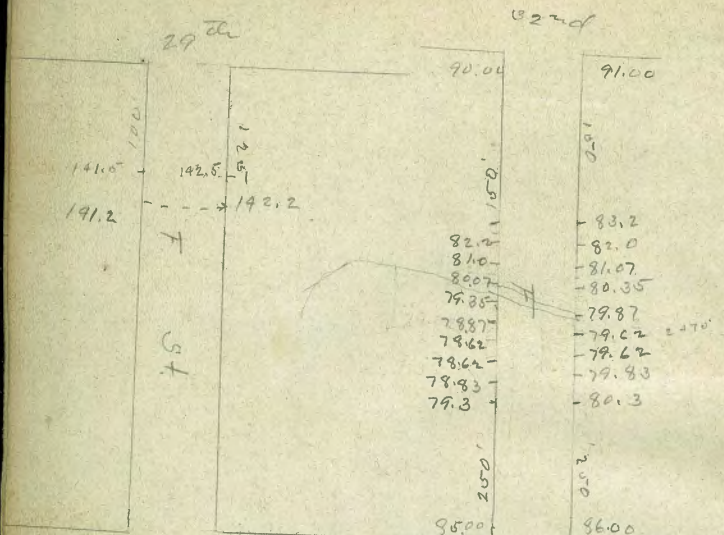
B.N. 388.85 Spk Pole SW Cor Nebraska & Adams Ave.

July 24, 1913  
Hennrich,  
Bedford,  
Buchanan.

+	H.I.	-
4.81	393.66	388.85

North line of Adams Ave.

1/2	4.7	389.0
1/4	4.9	388.8
1/4	5.2	388.5
1/4	5.0	388.7
1/4	5.3	388.4
1/4	4.8	388.9
1/4	4.6	389.1
1/4	3.9	389.8
1/4	3.7	390.0
1/4	4.2	389.7
1/4	4.0	389.4
1/4	4.4	389.3
1/4	4.5	389.2
1/4	4.4	389.3



142.0  
126.2  
16.8  
8.1  
24.4

	H.I. 393.66	Meridian W. (80° wide)
1400 W.L.		4.7 389.0
cl		4.7 389.0
1/2		4.6 389.1
c		4.1 389.6
1/2		4.2 389.5
cl		4.5 389.2
E.L. 1450		4.4 389.3
E.L.		4.6 389.1
cl		4.6 389.1
1/2		4.7 389.0
c		4.9 388.9
1/2		4.7 389.0
cl		4.9 388.9
W.L. 2400		4.7 389.0
W.L.		5.1 388.6
cl		5.1 389.6
1/2		5.2 389.5
c		5.1 389.6
1/2		5.0 389.7
cl		5.0 388.7
E.L.		5.0 388.7

	H.I. 393.66	
2450 = North line of Harbor on the West		
W.L.		5.4 388.3
cl		5.5 388.2
1/2		5.2 388.6
c		5.4 389.3
1/2		5.4 388.3
cl		5.6 388.1
W.L.		5.3 388.4
2465 = North line of Harbor on the East.		
2465 = 2455 along North line of Harbor		
W.L.		5.3 388.4
cl		5.6 388.1
1/2		5.2 389.5
c		5.4 389.3
1/2		5.6 388.1
cl		5.5 388.2
E.L.		5.7 388.0
c		4.91 388.35 Initial B.M.

Sections of 7 St. from the East line of 28th St to the West  
line of 3rd St. 50' wide 14' curbs 13' quarters.

July 1913

Donnan,  
Bedford  
Buchanan.

5

136.55 I.F. in Section of 28th St. Book 850, Page 24.

+	H.I.	-
11.22	148.23	136.55

00 = East line of 29th St.

00

M.L.

1.9 146.5

cl

5.5 142.9

1/4

9.8 138.6

c

13.7 134.5

1/2

16.3 132.1

cl

13.0 130.4

+ 11

19.5 129.9

cl

17.2 131.2

+ 25

M.L.

11.3 137.1

cl

14.4 134.0

1/2

13.9 135.1

c

11.6 136.8

1/2

9.2 139.2

cl

5.6 142.8

M.L.

0.6 147.8

	HI 148.93		Test (80' wide)
1.4			147.0
cl			6.4 142.0
1/4			9.6 138.8
c			11.6 137.9
1/4			10.7 147.7
cl			8.1 140.3
cl			4.0 144.4
1/4			+1.4 147.0
cl			1.8 146.6
1/4			5.1 143.3
c			7.6 140.8
1/4			7.1 141.3
cl			5.5 142.9
1/4			3.0 144.8
1/4			3.2 145.2
cl			4.4 144.0
1/4			2.8 145.6
#	12.63	160.95	0.11 148.32
c			12.3 148.7
1/4			10.3 149.7

	HI 160.95		
9.0			152.0
9.1			152.9
6.8			154.2
3.1			156.9
4.8			155.2
5.3			155.7
6.5			154.5
7.7			152.3
9.8			151.2
12.4			148.8
5.9			155.1
3.6			157.4
3.2			157.8
2.7			158.3
1.3			159.7
0.6			160.4
0.00	12.81	173.76	160.95
12.5			161.3

	H.I. 173.76	Fst (80' wide)
1275 V.L.		9.2 164.6
cl		9.9 163.9
1/2		11.0 162.8
c		12.0 161.8
1/2		12.9 160.9
cl		12.7 161.1
1/2 2400		13.3 160.5
1/2		9.5 164.3
cl		9.5 164.3
1/2		8.9 165.0
c		8.0 165.3
1/2		7.4 166.4
cl		6.4 167.4
V.L. 2425		5.3 168.5
V.L.		2.0 171.8
cl		2.4 171.4
1/2		2.9 170.9
c		3.9 170.0
1/2		4.9 169.0
cl		5.5 168.3
1/2		6.1 167.7

	H.I. 173.76	
1250 M.L.		3.0 170.8
cl		0.7 173.1
1/2		0.6 173.2
c		0.3 173.5
1/2		0.2 173.6
#	3.33 177.14	0.08 173.76
cl		3.3 173.8
V.L. 2470		2.9 174.2
V.L.		2.4 174.7
cl		2.2 174.9
1/2		2.4 174.7
c		2.6 174.5
1/2		2.8 174.3
cl		3.2 173.9
1/2		3.9 173.2

	+	71.1 177.19	- F 94 (80 wide)	
3+00 1/2			2.0 176.1	
cl			2.5 174.6	
1/2			2.3 174.8	
c			2.2 174.9	
1/2			2.3 174.8	
cl			2.5 174.6	
1/2			2.6 174.5	
3+25 1/2			3.2 173.9	
cl			3.1 174.0	
1/2			2.8 174.3	
c			2.7 174.4	
1/2			2.3 174.8	
cl			2.0 175.1	
1/2			1.7 175.4	
3+50 1/2			1.3 175.8	
cl			1.6 175.5	
1/2			2.3 174.8	
c			2.6 174.5	
1/2			2.7 174.4	
cl			3.3 173.8	
1/2			4.0 172.3	

	+	71.5 177.19	-	
3+75 1/2			6.5 171.6	
cl			4.0 173.1	
1/2			3.4 173.7	
c			2.6 174.5	
1/2			2.4 174.7	
cl			2.0 175.1	
1/2			1.7 175.4	
4+00 1/2			3.2 173.9	
cl			3.1 173.9	
1/2			3.6 173.5	
c			4.3 172.8	
1/2			5.0 172.1	
cl			5.9 171.2	
1/2			7.0 170.1	
4+25 1/2			9.6 167.5	
cl			9.5 168.6	
1/2			7.4 169.7	
c			6.9 170.3	
1/2			6.5 170.6	
cl			5.9 171.2	
1/2			5.0 171.1	



		HI 177.14	F St (60' wide)		HI 165.82			7	
4+50 1/2			9.2	167.9	1/2		3.3	161.9	
cb			9.0	169.1	5+25 1/2		6.1	159.1	
1/2			9.5	168.16	cb		5.6	159.6	
c			9.6	167.5	1/2		5.2	160.0	
1/2			9.7	167.4	c		5.0	160.2	
cb			10.4	166.7	1/2		4.7	160.5	
1/2			10.5	166.6	cb		4.6	160.6	
4+75 1/2			13.1	164.0	1/2		4.2	161.0	
cb			13.1	164.0	5+60 - West line of 29 <sup>th</sup> St (60' wide)				
1/2			12.5	164.6	5+60 1/2		3.3	156.9	
c			12.2	164.9	cb		3.0	156.2	
1/2			12.3	164.8	1/2		10.3	154.9	
cb			12.0	165.1	c		11.2	154.0	
1 1/2			11.3	165.8	1/2		11.4	153.8	
H	0.42	165.22	12.34	164.80	cb		11.3	153.9	
5+00 1/2			11.9	163.4	South side of F St, 3rd fence Post Center of Lot 4, Between 28 <sup>th</sup> & 29 <sup>th</sup> .				
cb			2.1	163.1	1/2		11.5	153.7	
1/2			2.7	162.5	H	0.00	152.64	12.58	152.64
c			2.5	162.7					
1/2			2.9	162.3					
cb			3.5	161.7					

H.I.  
152.64

F St. (80' wide)

West end of 29th St.

S.L.	1.2	151.4
cb	0.6	152.0
1/4	1.1	151.5
c	0.5	152.1
1/4	+0.2	152.4
cb	+1.6	151.0
1/4	+2.6	150.0

West 1/2 of 29th St.

1/4	0.2	152.4
cb	0.9	151.7
1/4	2.4	150.2
c	3.2	149.4
1/4	3.5	149.1
cb	3.8	149.8
1/4	4.1	148.5

Center of 29th St.

S.L.	7.2	145.4
cb	6.8	145.9
1/4	6.9	146.2

H.I.  
152.64

8

c	5.9	146.8
1/4	5.1	146.5
cb	3.9	148.7
1/4	2.3	150.3
0	3.13	149.51 15' from 29th St.

East 1/2 of 29th St.

1/4	5.3	147.3
cb	6.6	146.0
1/4	7.4	145.2
c	8.6	144.0
1/2	9.1	143.5
cb	10.3	142.3
1/4	10.7	141.9

East end of 29th St.

1/4	12.5	140.1
cb	12.2	140.4
1/4	11.9	140.7
c	11.3	141.3
1/4	10.0	142.6
cb	9.2	143.4
1/4	8.0	144.6

	+	H.I. 152.60	F St. (80 wide)	
00. End line of 29 <sup>th</sup> St.				
Slope 12' North of 00			9.6	143.0
00				
1/2			10.4	142.2
cb			11.0	141.6
1/4			11.7	140.9
c			13.3	139.3
#	0.22	139.89	13.02	139.62
1/2			1.2	138.6
cb			1.6	138.2
1/4			2.9	136.9
Slope 12' North of 00			3.5	136.3
" 20' " " 0+20			13.1	126.7
" 10' " " 0+25			11.9	127.9
0+20				
1/2			11.3	128.5
cb			9.2	130.6
1/4			7.3	132.5
c			6.1	133.8
1/2			5.0	134.8
cb			4.0	135.8
1/2			3.4	136.4

	+	H.I. 139.80		
Slope 12' North of station 0+25			2.0	137.4
" 15' " " 0+50			6.4	133.4
0+50				
1/2			7.0	132.8
cb			8.6	131.2
1/4			9.9	129.9
c			10.5	129.3
1/4			12.5	127.3
#	6.37	133.63	12.58	127.26
cb			9.0	124.9
1/2			11.2	122.4
Slope 15' North of station 0+50			12.4	121.2
" 30' " " " "			12.1	121.0
" 30' " " " 0+75			11.8	121.8
" 15' " " " "			11.5	122.1
0+75				
1/2			11.4	122.2
cb			12.1	121.5
1/4			11.8	121.8
c			9.5	125.1
1/4			7.4	126.2
cb			6.1	127.5
1/2			4.0	129.6

		H.I. 193.63	F St. (80' wide)	
Slope 20' north of Station	1+75	2.1	131.5	
" 30' "	" "	7.5	126.1	
" 15' "	" "	8.0	125.0	
1+00 M.L.		8.9	124.7	
cb		8.9	124.7	
1/2		10.3	123.3	
c		10.6	123.0	
1/2		10.4	123.2	
cl		10.1	123.5	
U.L.		10.0	123.6	
Slope 15' north of Station	1+00	10.2	123.4	
" 30' "	" "	10.7	122.9	
" 30' "	1+25	6.1	127.5	
" 15' "	" "	7.0	126.6	
1+20 U.L.		7.4	126.2	
cl		7.7	125.9	
1/2		8.4	125.2	
c		10.5	123.1	
1/2		9.6	124.0	
cl		9.0	124.6	
M.L.		8.9	124.7	

		H.I. 193.63	
Slope 15' north of Station	1+25	9.0	124.6
" 30' "	" "	8.3	125.3
" 30' "	1+50	8.2	125.4
" 15' "	" "	8.0	125.6
1+50 M.L.		7.8	125.8
cl		6.9	126.7
1/2		5.5	128.1
c		5.1	128.5
1/2		4.5	129.1
cl		4.6	129.0
U.L.		4.2	129.4
Slope 10' north of Station	1+50	3.9	129.7
" 20' "	" "	2.8	130.7
#	12.68 139.94	6.37	127.14
Slope 20' north of Station	1+75	5.8	134.1
" 10' "	" "	6.6	133.3
1+75 U.L.		6.9	133.0
cl		4.2	135.7
1/2		2.2	137.7
c		2.9	137.2
1/2		2.2	137.7

		715 152.69	F St. (80' wide)			
cl			3.9	136.1		
1/2			4.7	135.2		
Slope 10' North of Station	1+75		5.8	134.1		
" 20' "	" "		5.5	134.4		
#	13.03	152.69	0.00	139.61		
Slope 20' North of Station	2+00		9.9	142.8		
" 10' "	" "		9.9	142.8		
2+00 1/2			9.7	143.0		
cl			9.8	142.9		
1/4			9.5	143.2		
c			9.5	143.2		
1/2			9.7	143.6		
cl			12.1	140.6		
1/2			15.4	137.3		
Slope 10' North of Station	2+00		16.0	136.7		
" 20' "	" "		14.5	138.2		
" 20' "	" "	2+25	10.1	142.6		
" 10' "	" "	" "	11.2	141.5		
2+25 1/2			10.5	142.2		
cl			6.5	146.2		
1/2			3.9	148.8		

		715 152.69				
c			3.0	149.7		
1/2			2.9	149.8		
cl			2.4	120.3		
1/2			3.3	149.4		
Slope 10' North of Station	2+25		3.8	148.9		
#	13.03	152.69	0.00	152.69		
2+00 1/2			12.0	153.7		
cl			11.3	154.4		
1/4			12.1	153.6		
c			12.5	153.2		
1/2			13.3	152.4		
cl			15.5	150.2		
1/2			18.5	147.2		
Slope 10' North of Station	2+50		19.1	146.6		
2+50 1/2			13.5	152.2		
cl			11.5	154.2		
1/2			11.4	154.3		
c			10.9	154.9		
1/2			10.1	155.6		
cl			8.4	157.3		
1/2			8.3	157.4		

H.L.  
16572

F St (80' wide)

2+78  
with line only

3+00  
M.L.

cl

1/2

c

1/2

cl

M.L.

3+25

M.L.

cl

1/2

c

1/2

cl

1/2

3+50

M.L.

cl

1/2

c

1/2

cl

9.5 156.2

5.2 160.5

6.1 159.6

7.5 158.2

9.0 156.7

9.1 156.6

9.1 156.6

9.4 157.3

6.1 159.6

6.5 159.2

5.9 159.8

5.5 160.2

4.2 161.5

2.6 163.1

2.0 163.7

10.2 165.5

1.0 164.7

1.8 163.9

4.9 162.8

3.6 162.1

4.2 161.5

H.L.  
16572

M.L.

3+75

M.L.

cl

1/2

c

1/2

#

cl

M.L.

3+00

M.L.

cl

1/2

c

1/2

cl

M.L.

9.32

17 15.04

9.1 161.6

1.4 164.3

2.1 163.6

1.8 163.9

0.9 164.8

0.3 165.4

0.00 165.72

9.6 166.4

7.5 167.5

6.6 168.4

7.5 167.5

9.1 166.9

8.9 166.2

9.1 165.9

8.8 166.2

8.0 167.0

HI  
175.04

F. 37 (80' wide)

37.5 2.2		6.5	168.5
ob		6.7	168.3
1/2		7.1	167.9
c		7.1	167.9
1/2		6.6	168.4
ob		6.2	168.8
1/2		5.7	169.3
44.50 11.2		5.0	170.0
ob		5.2	169.8
1/2		5.5	169.5
c		5.8	169.2
1/2		5.7	169.3
ob		5.7	169.3
1/2		5.4	169.6
44.75 2.2		5.6	169.4
ob		4.9	170.1
1/2		4.5	170.5
c		4.4	170.6
1/2		3.9	171.1
ob		3.9	171.1
11.2		3.6	171.4

HI  
175.04

13

5.00 11.2		3.1	171.9
ob		3.6	171.4
1/2		3.9	171.1
c		4.3	170.7
1/2		4.6	170.4
ob		5.3	169.7
1/2		6.0	169.0
5.00 2.2		6.6	168.4
ob		6.1	168.9
1/2		5.3	169.7
c		4.4	170.6
1/2		4.1	170.9
ob		3.7	171.3
11.2		3.3	171.7
5.00 11.2		2.6	172.4
ob		3.6	171.4
1/2		4.1	170.9
c		4.9	170.1
1/2		5.9	169.1
ob		5.1	169.9
2.2		6.7	168.3

	+	71.1 1767.24	F St. (80 wide)
5+25 0.5			5.7 169.3
cl			6.2 168.8
1/2			6.0 169.0
c			4.7 160.3
1/2			4.2 160.8
cl			3.4 161.6
7/8			2.7 162.3
5+96 1/2			3.4 161.6
cl			4.4 160.6
1/2			5.0 160.0
c			5.6 169.4
1/2			6.5 168.5
cl			6.4 168.6
1/2			7.5 167.5
6+00 = West line of 30 <sup>th</sup> St. (graded)			
6+00 1/2			7.9 167.1
cl			8.0 167.0
1/2			7.3 167.7
c			6.8 168.2
1/2			6.3 168.7
cl			6.0 169.0

	+	42.1 1760.4		14
11.5			5.7	169.3
#	509	171 90	9.33	166.71
= East line of 30 <sup>th</sup> St				
11.5			2.4	169.4
cl			2.5	169.3
1/2			3.5	168.3
c			3.8	167.0
1/2			4.4	167.4
cl			4.8	167.0
1/2			4.6	167.2
11.5			5.6	166.2
cl			5.2	166.6
1/2			5.9	167.9
c			3.9	167.9
1/2			5.1	168.7
cl			1.7	170.1
+10			0.9	170.8
11.5			2.0	169.7

14  
 2000.00  
 169.33  
 166.71  
 166.71



	HI 171.80	F 37 (80' wide)
+25 1/2		3.1 167.7
cb		4.0 167.5
1/4		4.5 167.3
c		5.2 166.6
1/2		5.1 166.7
cb		5.3 166.5
1/2		7.0 164.3
Slope 9' North of Station	+25	8.5 163.3
" 20 "	+50	15.8 156.0
" 10 "	"	12.1 157.7
+50 1/2		12.2 159.6
cb		9.7 161.9
1/4		7.5 164.3
c		6.5 165.3
1/2		6.6 165.2
cb		6.5 164.3
1/2		5.5 166.3
Slope 10' North of Station	+100	4.2 167.8
+100 East property only.		14.8 157.0
Slope 10' North of Station	+75	4.2 167.8

	HI 171.80		15
+75 1/2		5.7 166.1	
cb		7.2 164.6	
1/4		8.5 163.3	
c		10.1 161.7	
1/2		11.2 160.6	
cb		12.2 159.8	
1/2		10.9 160.9	
Slope 10' North of Station	+75	11.0 160.8	
" 20 "	"	11.2 160.6	
" 10 "	"	8.4 163.4	
+100 1/2		8.1 163.7	
cb		7.3 164.5	
1/4		6.7 165.1	
c		6.0 165.8	
1/2		4.9 167.0	
cb		4.8 167.0	
1/2		3.6 168.2	
Slope 5' North of Station	+100	2.9 168.9	
+100		0.3 171.5	
cb		1.3 170.5	
1/4		2.3 169.5	

		H.I. 171.80	0-	F 37 (80' wide)
1/8			3.0	168.8
c				
1/4			3.6	168.2
cl			4.0	167.7
1/2			4.6	167.2
1/2			1.9	169.9
1/2			1.5	170.3
1/4			1.5	170.3
c			1.1	170.7
#	9.43	176.14	5.29	166.71
1/4			4.7	171.4
cl			4.2	171.9
1/2			3.0	173.1
1/2			2.5	173.6
cl			3.4	172.7
1/4			3.4	172.7
c			4.2	171.9
1/2			4.9	171.2
cl			5.4	170.7
1/2			5.6	170.5
1/2			5.4	170.7
cl			5.0	171.1

		H.I. 176.14	-		16
1/4			4.5	171.6	
c			3.4	172.7	
1/4			2.9	173.3	
cl			2.8	173.3	
1/2			2.2	172.9	
1/2			2.2	173.9	
cl			2.2	173.9	
1/4			2.9	173.2	
c			3.5	172.6	
1/4			4.0	172.1	
cl			4.6	171.5	
1/2			5.0	171.0	
1/2			4.8	171.3	
cl			4.9	171.2	
1/4			4.3	171.8	
c			3.5	172.6	
1/4			3.0	173.1	
cl			2.1	174.0	
1/2			1.4	174.7	

	7.I 176.14	Fst. (80 wide)
2+75 1/2	2.0	174.1
cl	2.7	173.4
1/4	3.9	172.2
c	4.2	171.9
1/4	4.8	171.3
cl	5.5	170.6
1/2 3+00	6.0	170.1
1/2	5.8	170.3
cl	5.7	170.4
1/4	5.0	171.1
c	4.4	171.7
1/4	3.9	172.2
cl	3.0	173.1
1/2 3+25	2.2	173.9
1/2	2.5	173.6
cl	3.2	172.9
1/4	3.7	172.4
c	4.2	171.9
1/4	4.6	171.5
cl	5.6	170.5
1/2	6.2	169.9

	7.I 176.14	
2+50 1/2	6.3	169.8
cl	5.8	170.3
1/4	5.1	171.0
c	4.6	171.5
1/4	4.3	171.8
cl	3.5	172.6
1/2	2.9	173.2
3+75 1/2	2.8	173.3
cl	3.4	172.7
1/4	4.3	171.8
c	5.0	171.1
1/4	5.6	170.5
cl	6.4	169.7
1/2	6.5	169.6
4+00 1/2	9.0	167.1
cl	8.0	166.1
1/4	6.9	169.2
c	6.1	169.9
1/4	5.5	170.6
cl	4.5	171.6
1/2	3.4	172.7

	+	HI 176.14	F St (80' wide)		-	HI 176.14		
4+25 M.L.			4.5	171.6	-		2.10	163.26
cl			5.6	170.5				12.98
1/2			6.4	169.7	1/2			163.16
c			7.4	168.7	1/2			2.0
1/2			8.5	167.6	5+00 1/2			4.1
cl			9.6	166.5	cl			3.5
1/2			11.0	165.1	1/2			2.5
4+50 1/2			12.3	163.8	c			0.0
cl			10.9	165.2	1/2			+2.0
1/2			9.6	166.5	cl			+3.2
c			8.3	167.8	M.L.			+4.8
1/2			7.0	169.1	5+25 M.L.			+1.0
cl			6.0	170.1	cl			1.1
M.L.			4.3	171.8	1/2			2.3
4+75 M.L.			4.9	171.3	c			4.1
cl			7.1	169.1	1/2			5.0
1/2			8.2	167.9	cl			5.5
c			9.6	166.5	1/2			6.4
1/2			11.0	165.1	5+50 1/2			3.5
cl			13.4	162.7	cl			7.9
					1/2			7.2
					c			6.0
					1/2			5.3

	71.1 163.26	F St (80' wide)
cl	4.0	159.3
7/2 5475	2.3	161.0
7/2	5.1	158.2
cl	5.9	157.5
1/4	7.2	156.1
c	8.3	155.0
1/4	9.3	154.0
cl	9.9	153.4
1/2	10.0	153.3
6+00 = West line of 31 <sup>st</sup> St 10' center 10' quarter		
6+00 1/2	12.3	151.0
cl	12.1	151.2
1/4	11.5	151.8
c	10.6	152.7
1/4	10.0	153.3
cl	8.9	154.4
7/2	7.5	155.8
West end of 31 <sup>st</sup> St.		
7/2	9.1	154.2
cl	10.3	153.0
1/4	11.4	151.9

	71.1 163.26		19
c	12.4	150.9	
1/4	12.8	150.5	
cl	13.3	150.0	
1/2	13.9	149.4	
#	0.11	150.28	13.09
West 1/4 of 31 <sup>st</sup> St.			
1/2	2.4	147.9	
cl	1.9	148.4	
1/4	1.0	149.3	
c	0.6	149.7	
1/4	0.3	150.0	
cl	10.8	149.5	
7/2	7.5	148.8	
Center of 31 <sup>st</sup> St.			
7/2	1.7	148.6	
cl	1.3	149.0	
1/4	2.0	148.3	
c	2.1	148.2	
1/4	2.3	148.0	
cl	3.6	146.7	
1/2	4.1	146.2	

	H.I. 150.29	F St (80' wide)
Slope 6' North of Center of 31 <sup>st</sup> St	9.2	146.1
East 1/2 of 31 <sup>st</sup> St		
0	0.65	149.65 <small>31<sup>st</sup> E.F.</small>
1/2	5.5	144.8
cb	9.8	145.5
1/2	3.8	146.5
c	3.4	146.9
1/2	3.5	146.8
cb	3.7	146.6
M.S.	6.3	144.0
Slope 12' North of East 1/2 of 31 <sup>st</sup> St	5.4	144.9
" 6' " " " " " "	3.3	147.0
East curb of 31 <sup>st</sup> St		
M.S.	6.0	144.3
+10	8.4	141.9
cb	7.7	142.6
1/2	5.7	144.6
c	5.5	144.8
1/2	5.7	144.6
cb	6.1	144.2
M.S.	6.6	143.7

	H.I. 150.28	
Slope 10' North of Station 0+00	9.7	141.6
0+00 East line of 31 <sup>st</sup> St		
M.S.	8.0	142.3
cb	7.5	142.8
1/2	8.4	141.9
c	8.8	141.5
1/2	9.5	140.8
cb	8.9	141.4
M.S.	4.0	146.3
Slope 6' North of Station 0+00	1.8	148.5
+25 M.S.	6.3	150.0
cb	3.8	146.5
1/2	7.0	143.3
c	11.5	138.8
1/2	13.8	136.5
cb	14.0	136.3
M.S.	12.4	137.9
Slope 12' North of Station 0+25	12.3	138.0
" 12' " " " " " 0+00	17.0	133.3

		H.I. 150.29	F St (80' wide)	
0.59 1/2			18.0	132.3
cl			15.6	134.7
1/2			11.2	138.1
c			6.3	144.0
1/2			3.3	147.0
cl			1.0	149.3
#	494	155.11	0.11	150.17
1/2 0.75			2.8	151.3
1/2			1.3	153.8
cl			4.9	150.7
1/2			7.2	147.9
c			9.6	145.5
1/2			12.5	142.6
cl			16.7	138.4
H.I.			21.5	133.6
1/2 1.00	1/2 North of Station 0+75		24.4	130.7
1/2			17.5	137.6
cl			13.3	141.8
1/2			10.2	144.9
c			7.3	147.8
1/2			4.7	150.7

		H.I. 155.11		
cl			2.2	152.9
1/2 14.26			40.2	154.9
1/2			0.0	155.1
cl			2.0	153.9
1/2			4.4	150.7
c			6.8	148.3
1/2			9.5	145.6
cl			12.4	142.7
1/2 14.50			15.8	139.3
1/2			17.3	137.8
cl			19.3	140.8
1/2			11.0	144.1
c			8.3	146.8
1/2			5.6	149.5
cl			2.9	152.2
1/2			1.1	154.0

		7.I 155.11	F 94 (80 wide)		
1270 M.L.			3.6	151.5	cl
cl			6.2	148.9	1/2
1/2			8.9	146.3	2+50 1/2
c			11.5	143.6	cl
#	00.2	142.14	12.99	142.12	1/4
1/2			1.3	140.8	c
cl			3.3	138.8	1/2
1/2			5.9	136.2	cl
2+00 1/2			8.3	133.8	1/2
cl			5.8	136.3	2+75 1/2
1/2			3.4	138.7	cl
c			1.9	140.2	1/2
1/2			+2.1	142.0 = 142.2	#
cl			+1.5	140.6 = 143.6	c
1/2			+4.2	137.9 = 146.3	1/2
2+25 1/2			0.8	141.3	cl
cl			2.0	140.1	1/2
1/2			3.9	138.2	
c			5.3	136.8	
1/2			6.7	135.4	

		7.II 142.14			142.1 22
			8.6	132.5	
			11.0	131.1	
			14.4	127.7	
			12.7	129.4	
			11.3	130.8	
			9.8	132.3	
			8.5	133.6	
			7.0	135.1	
			5.7	136.4	
			10.8	131.3	
			12.0	130.1	
			12.8	129.3	
	0.07	142.30	12.91	129.23	
			1.3	128.0	
			2.4	126.9	
			4.4	124.9	
			6.2	123.1	



		42. 129.30	F St (80 wide)	
3+00 2.2			10.2	119.1
cb			9.2	120.1
1/2			8.2	121.1
c			7.1	122.2
1/2			6.1	123.2
cb			4.9	124.4
M.L.			4.5	124.8
3+25 M.L.			10.9	118.4
cb			11.3	118.6
1/2			12.2	117.1
#	0.18	116.61	12.97	116.90
c			0.6	116.0
1/2			0.6	116.0
cb			0.5	116.1
M.L.			0.9	115.8
Slope 10' North of Station 3+50			7.5	109.1
3+50 M.L.			7.0	109.6
cb			6.3	110.3
1/2			5.6	111.0
c			3.9	112.7
1/2			2.5	114.1

		71 116.61		
cb			2.1	114.3
M.L.			1.5	115.1
Slope 10' North of Station 3+50			0.7	115.9
" " " " " 3+75			4.4	112.2
3+75 M.L.			5.2	111.4
cb			6.0	110.6
1/2			7.3	109.3
c			8.5	108.1
1/2			9.7	106.9
cb			10.7	105.9
1/2			11.7	104.9
Slope 15' North of Station 3+75			13.4	103.2
" 20' " " " 4+00			17.9	98.8
" 10' " " " "			17.6	99.0
4+00 M.L.			17.2	99.4
cb			15.9	100.8
1/2			13.4	103.2
c			12.0	104.6
1/2			11.0	106.6
cb			9.9	106.8
M.L.			8.2	108.4

		71.2 116.61	F 37 (80' wide)	
Slope 10' North of Station	4+100	7.5	109.1	
" 12' "	" "	4.25	119	104.7
4+25 M.L.			12.7	103.9
#	0.33	104.15	12.79	103.82
cl			1.3	103.8
1/2			2.3	101.8
c			3.3	100.8
1/2			5.1	111.5
cl			6.5	97.6
M.L.			7.0	97.1
Slope 13' North of Station	4+25	7.8	96.2	
" " " "	" "	4+50	9.6	94.5
4+50 M.L.			9.5	94.6
cl			8.3	95.8
1/2			7.2	96.9
c			5.9	98.2
1/2			4.6	99.5
cl			3.6	100.5
M.L.			2.1	102.0
Slope 12' North of Station	4+50	1.0	103.1	

		71.2 104.15	
Slope 12' North of Station	4+75	1.3	102.8
4+75 M.L.			2.3
cl			3.6
1/2			5.4
c			6.7
1/2			7.8
cl			9.1
M.L.			10.3
Slope 14' North of Station	4+75	10.9	93.3
" " " "	" "	5+00	11.5
5+00 M.L.			10.3
cl			9.9
1/2			7.6
c			6.3
1/2			4.7
cl			3.7
M.L.			2.6
Slope 15' North of Station	5+00	1.5	102.6

	H.I. 104.15	F 57 (30' wide)
54.25 11.2		2.4 101.8
cb		3.5 100.7
1/2		4.6 99.6
c		5.5 98.7
1/2		6.6 97.6
cb		8.1 96.1
1/2		9.5 94.7
Slope 12' South of Station 5425	10.7	93.5
" 10 " " " " 5450	10.2	94.0
5450 1/2	9.3	93.9
cb	7.6	96.6
1/2	6.3	97.9
c	5.3	98.9
1/2	4.6	99.6
cb	3.8	100.4
11.25 5475	3.2	101.0
11.25	4.5	99.7
cb	5.4	98.8
1/2	5.7	98.5
c	7.0	97.2
1/2	7.6	96.6

	H.I. 104.15		25
cb		8.0	96.2
1/2		9.0	95.2
6+00 = West line of 32 <sup>nd</sup> St 60' wide. 10' curb 10' gutter			
6+00 1/2		10.2	94.0
cb		9.8	94.4
1/2		9.4	94.8
c		8.3	95.9
1/2		8.1	96.1
cb		7.6	96.6
1/2		6.2	98.0
West curb of 32 <sup>nd</sup> St.			
1/2		6.7	97.5
cb		7.7	96.5
1/2		8.5	95.7
c		9.0	95.2
1/2		9.8	94.4
cb		10.5	93.7
1/2		10.6	93.6

H.I.  
102.15

F St (80 wide)

West 1/2 of 32nd St.

W.L.	11.5	92.7
cb	11.1	93.1
1/2	10.6	93.6
c	9.6	94.6
1/2	8.7	95.5
cb	8.3	95.9
M.L.	7.3	96.9

West quarter + 7

M.L.	7.5	96.1
cb	8.6	95.6
1/2	8.9	95.3
c	9.8	94.4
1/2	10.9	93.3
cb	12.1	92.1
W.L.	12.9	91.3
#	3.37	96.95

302 710 715  
Cor. 32nd & H St  
83.23  
85.29  
87.35  
89.41  
91.47  
93.53  
95.59  
97.65  
99.71  
101.77  
103.83  
105.89  
107.95  
109.95

Center of 32nd St.

W.L.	6.4	93.5
cb	5.4	91.5
1/2	4.3	92.6

H.I.  
96.95

c		2.7	94.2
1/2		1.8	95.1
cb		1.5	95.4
+6		1.0	95.9
M.L.		7.7	98.2
#	0.99	94.52	3.37

East 1/2 of 32nd St.

M.L.		5.0	89.3
cb		5.0	89.5
1/2		5.1	89.4
c		5.4	89.1
1/2		5.5	89.0
cb		5.3	89.2
W.L.		5.6	88.9

East curb of 32nd St.

W.L.		5.9	88.6
cb		5.5	89.0
1/2		5.5	89.0
c		5.3	89.2
1/2		5.0	89.5
cb		5.0	89.5

	H.I. 94.52	F.A. (80' wide)
1/2	4.7	89.8
cc = East line of road St.		
1/2	5.1	89.4
cl	5.2	89.3
1/4	5.6	88.9
c	5.8	88.7
1/4	6.0	88.5
cl	6.3	88.2
1/2	6.6	87.9
+3 on North line only	6.4	88.1
+4 " " " "	3.9	90.6
+7 on North line only	5.4	89.1
1/2	5.8	88.7
cl	4.6	89.9
+3	7.3	86.7
1/4	8.0	86.5
c	7.9	86.6
1/4	7.0	87.5
cl	6.3	88.2
1/2	12.1	82.4

	H.I. 94.52		
Slope 15' North of Station 0200	12.5	82.0	27
" " " " 0225	12.5	92.0	
1/2	14.4	80.1	
cl	13.4	81.1	
1/4	9.0	85.5	
c	9.8	84.7	
1/4	10.0	84.5	
+3	7.6	84.9	
+5	5.8	88.7	
1/2	7.3	87.2	
+75	7.7	86.8	
cl	6.8	87.7	
+6	7.0	87.5	
+8	11.6	82.9	
1/2	11.9	82.6	
c	11.8	82.7	
1/2	11.8	82.7	
#	6.77	87.59	12.70
cl	7.8	79.8	91.82
1/2	8.2	79.4	

	F.I. 87.59	F.S. (30" wide)
Wagon's North of Station	0+75	7.9 79.8
" " " " "	1+00	8.2 78.4
" " " " "	1+25	8.9 78.7
cb		9.4 77.2
+9		6.8 80.8
1/4		6.6 81.0
c		6.3 81.3
1/4		6.9 80.7
+5		2.6 85.0
cb		0.5 81.1
W.L.		0.8 76.8
1+25		1.3 76.3
W.L.		1.7 85.9
cb		3.0 84.6
+6		7.6 80.0
1/4		8.0 79.6
c		7.6 80.0
1/4		8.0 79.6
+4		8.4 79.2
cb		10.7 76.9
W.L.		10.2 77.4

	F.I. 87.59		28
Wagon's North of Station	1+25	10.4 77.2	
" " " " "	1+50	11.1 76.5	
" " " " "	1+75	11.9 75.7	
cb		12.1 75.5	
+8		9.8 78.2	
1/4		9.0 78.6	
c		8.7 78.9	
1/4		8.9 78.7	
+4		5.0 82.6	
cb		4.0 83.6	
W.L.		2.9 84.8	
1+65 South line only		3.9 83.7	
1+75		6.3 81.3	
W.L.		6.5 81.1	
cb		6.6 81.0	
+10		9.8 77.8	
c		9.5 78.1	
1/4		9.9 77.7	
+4		10.7 76.9	
+10		14.9 72.7	
cb		14.9 72.7	

+				-					
		H.I.	F.H. (80' wide)				H.I.		
		87.59					80.32		
1/2			13.2	74.4	+3		4.5	73.8	
Slope 15' north of Station 2175			13.4	74.2	cb		9.7	70.6	
"	15'	2100	14.2	73.7	+2		10.7	69.6	
#	2.81	80.32	10.25	77.51	1/2		9.3	71.0	
2100	1/2		7.6	72.7	Slope 15' north of Station 2125		6.7	73.6	
cb			9.7	70.6	"	15'	2150	9.6	71.7
1/4			3.4	76.9	2150	1/2		10.4	69.9
0			3.1	77.2	cb		10.8	69.5	
1/4			3.6	76.7	+5		9.7	70.6 60.6	
+5			5.7	74.6	1/2		4.3	76.0	
cb			7.3	73.0	c		3.9	76.4	
1/2			9.0	71.3	+10		4.1	76.2	
10' north of Station 2100			10.3	70.0	1/2		5.0	75.3	
15'	"	2125	11.9	68.4	+9		11.1	69.2	
2125	1/2		11.5	68.8	cb		11.8	68.5	
cb			11.0	69.3	1/2		11.8	68.5	
+5			10.0	70.3	Slope 15' north of Station 2150		12.3	68.0	
1/4			4.3	76.0	"	"	2175	11.7	69.6
0			3.6	76.7	2175	1/2		11.7	69.6
1/4			4.1	76.2	cb		11.1	69.2	

	+	H.I. 80.32	-	F 57 (80' wide)
+0.5			10.1	70.2
1/2			4.9	75.4
+4			4.1	76.2
c			3.9	76.4
1/2			4.6	75.7
+9			10.0	70.3
cb			10.5	69.8
M.L.			11.0	69.3
Slope 15' North of Station	3+70		10.3	70.0
" " " " "	3+80		9.9	71.4
3+00 M.L.			9.1	71.2
cb			9.1	71.2
+5			8.9	71.4
1/2			4.8	75.3
c			3.9	76.4
1/2			4.0	75.8
+9			9.1	71.2
cb			9.7	70.6
M.L.			10.2	70.1
Slope 15' South of Station	3+00		11.0	69.3
" " " " "	3+25		5.5	74.8

	+	H.I. 80.32	-		
3+20 M.L.			6.7	73.6	50
+6			5.6	71.7	
cb			8.2	72.1	
1/2			4.6	75.7	
c			3.8	76.5	
1/2			4.4	75.9	
+7			5.7	74.6	
cb			5.1	75.2	
M.L.			2.6	77.7	
H	8.01	86.69	1.69	79.69	
3+50 M.L.			4.7	82.0	
cb			6.7	80.0	
+9			9.7	77.0	
1/2			10.1	76.6	
c			9.9	76.8	
1/2			10.5	76.2	
+5			10.9	75.8	
cb			8.9	77.8	
M.L.			7.7	79.0	



	+	HI 86.69	F. 97. (80 wide)
0+75 1/2			5.5 81.2
cl			5.8 80.9
+2			6.5 80.2
+9			10.0 76.7
1/2			9.9 76.9
c			9.0 77.7
1/4			9.2 77.5
+6			9.2 77.5
cl			6.4 80.3
1/2			4.8 81.9
4+00 1/2			5.4 81.3
cl			5.8 80.9
+6			8.9 77.8
1/2			8.6 78.5
c			8.3 78.4
1/2			9.3 77.4
+5			9.5 77.2
+10			6.7 80.0
cl			6.5 80.2
1/2			5.7 81.0

	+	HI 86.69	
4+05 1/2			6.7 80.0
cl			6.9 79.8
+5			7.0 79.7
+7			9.1 77.6
1/2			8.7 78.0
c			7.9 78.8
1/2			7.9 78.8
+9			8.8 77.9
cl			5.6 81.1
1/2			5.8 80.9
4+50 1/2			5.1 81.6
cl			6.1 80.6
+4			9.2 78.5
1/2			7.1 79.6
c			7.1 79.6
1/2			8.0 78.7
+6			9.3 78.4
+9			7.1 79.6
cl			6.9 79.8
1/2			6.6 80.1

	H.I. 86.69	F. St (80 mids)
4175 S.L.		7.1 79.6
cl		7.4 79.3
1/2		7.3 79.4
c		6.4 80.3
1/2		6.5 80.2
+ 10		7.0 79.7
cl		6.0 80.7
M.L.		5.4 81.3
5+00 M.L.		5.8 80.9
cl		6.5 80.2
1/2		5.8 80.9
c		6.0 80.7
1/2		6.2 80.5
cl		7.2 79.5
V.L.		7.2 79.5

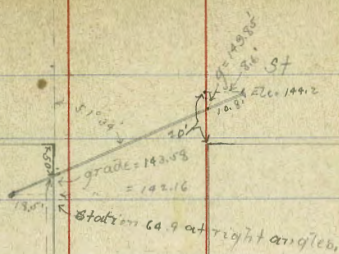
	H.I. 86.69		32
5+25 S.L.		7.0	79.7
cl		6.8	79.9
1/2		6.0	80.7
c		5.3	81.4
1/2		5.2	81.5
cl		5.6	81.1
S.L.		4.7	82.0
5+50 M.L.		3.0	83.7
cl		4.5	82.2
1/2		4.2	82.5
c		4.2	82.5
+ 9		4.5	82.2
1/2		5.8	80.9
cl		6.6	80.1
V.L.		6.9	79.8
5+75 S.L.		6.8	79.9
cl		6.3	80.4
1/2		5.2	81.5
+ 6		3.0	83.7
c		2.9	83.8



1/2 + 50	3.7	
1/2 + 51	3.9	
1/2 + 63	9.9	
N 2 + 90 = North line	10.6	69.3
North of Station 2 + 70 = End Culvert	9.7	70.2

H.I.  
79.87

31<sup>st</sup>



34

32<sup>nd</sup>

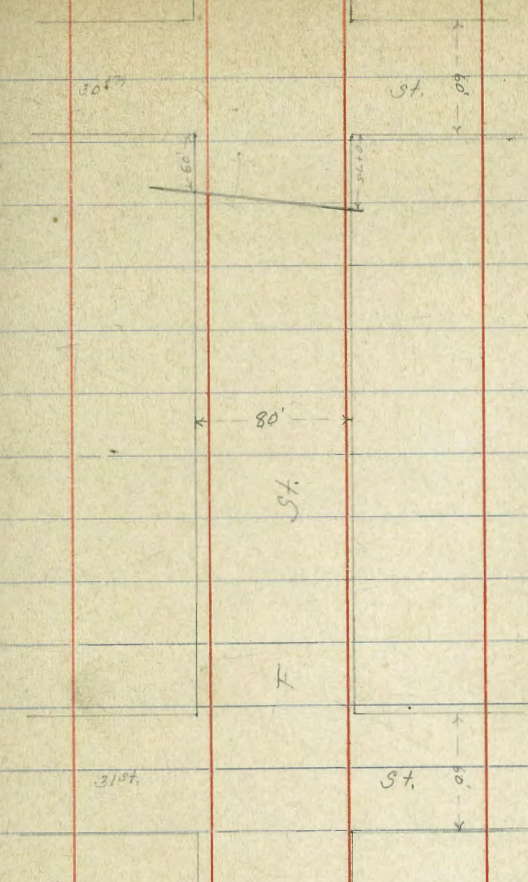
B.T. 142.63 18' High F.B. 31<sup>st</sup> St. See page 30 this book.

H.I.		
0.27	149.90	149.63

3.6 at right angles North of North line on East 1/4 of 31<sup>st</sup> St.

North end of Culvert	5.7	149.2
North line of F St & Culvert line	6.0	

	H.I.		
	149.90		
42. + 25		9.6	
+ 50		12.4	
#	0.97	127.94	136.57
+ 75		2.9	
+ 101.5 =	South line of F St. = Sta + 50		5.3
24	South of South line of Hubert		8.0



I would that a subject was not necessary here.

But 166.71 is 30' from St. See page 14 this book.  
 H.I.  
 1.19      167.95      166.71



9/20/44  
 13/1/44

X sec of Point Loma on (60')  
 Ocean to Santa Barbara

2427

P. Loma  
 36

036 2427 2431  
 180' W of Pt. Loma on S 2 = Ocean Bank  
 175' " " " " " " " " " " " "

Bm 74 Post  
 at Pt. Loma  
 2427

						100	W of	Pt. Loma
								30 21.3
S			0.0	24.3				35 20.8
			0.6	23.7				40 20.3
			1.4	23.1				43 20.0
b			2.0	22.3				44 19.9
			1.9	22.4				46 19.7
			2.5	21.8				46 19.7
N			3.2	21.2		50	W of	Pt. Loma
	150'	W of						48 19.5
n			4.2	20.1				48 19.5
			3.4	20.9				48 19.5
			3.3	21.0				48 19.5
b			2.8	21.5				45 19.8
			1.7	22.6				44 19.9
			1.4	22.9				43 20.0
S			1.2	23.1				

PLOTTED

W line of De Foe W (60)

S	46	19.7
	46	19.7
	48	19.5
	47	19.6
	48	19.5
	48	19.5
N	50	19.3

W line of De Foe

N	53	19.0
	49	19.4
	49	19.4
b	48	19.5
	48	19.5
	47	19.6
S	47	19.6

PLOTTED

W line of De Foe

S	47	19.6
	47	19.6
	48	19.5
	47	19.6
	48	19.5
	50	19.3
2	52	19.1

center of De Foe

9	48	19.5
	49	19.4
	48	19.5
b	48	19.5
	49	19.4
	48	19.5
S	47	19.6



	E	1/4 of	De Jul	
S			47	196
			47	196
			49	194
b			47	196
			49	194
			49	194
M			49	194

	E	1/4 of	De Jul	
A			52	191
			48	195
			49	194
b			47	196
			49	194
			47	196
S			47	196

PLOTTED

	E	1/4 of	De Jul	
S			47	196
			48	195
			49	194
b			47	196
			49	194
			49	194
A			48	195

	50	E of	De Jul	
M			48	195
			49	194
			48	195
b			47	196
			49	194
			47	196
S			47	196

24.27

100

E of

De Zee

W

S

47 196

46 197

47 196

b

46 197

47 196

49 194

n

47 196

150

E of

De Zee

n

45 198

45 198

45 198

b

44 199

45 198

45 198

S

45 198

PLOTTED

24.27

H. Lina

39

200

E of

De Zee

W

S

38 205

37 206

35 208

b

34 209

34 209

35 208

n

34 207

250

E of

De Zee

n

25 218

26 217

24 219

b

24 219

24 219

25 218

S

26 217

TP

1013

3187

253

2174

24.27  
155  
21.74  
20.23  
51.87

3187

	300	E of	Q. Zn	
S			91	22.8
			88	23.1
			86	23.3
b			85	23.4
			85	23.4
			85	23.4
n			83	23.6

	350	E of	Q. Zn	
n			65	25.4
			66	25.3
			67	25.2
b			66	25.3
			68	25.1
			70	24.9
S			70	24.9

PLOTTED

3187

P. to 40

	400	E of	Q. Zn	
S			51	26.8
			50	26.9
			46	27.3
b			44	27.5
			44	27.5
			44	27.5
n			40	27.9

	450	E of	Q. Zn	
n			13	30.6
			19	30.0
			17	30.0
b			21	29.8
			26	29.3
			30	28.9
S			37	28.7

TP	1029	4030	196	29.91
----	------	------	-----	-------

3187  
196  
29.91  
1029  
4030

4020

	500	E 1	Q 7m	
S			98	30.4
			94	30.8
			89	31.3
b			82	32.0
			80	32.2
			80	32.2
n			76	32.6
	550	E 1	Q 7m	
n			67	33.5
			70	33.2
			71	33.1
b			76	32.6
			83	31.9
			85	31.8
S			87	31.5

PLOTTED

4020

R. L. Linn

41

	600	E = W 2	Eber 17 (60)	
S			67	33.5
			64	33.8
			64	33.8
b			58	34.4
			56	34.6
			54	34.8
n			51	35.1
	W	66 f	Eber 17	
n			46	35.6
			47	35.5
			52	35.0
b			55	34.7
			60	34.2
			62	34.0
S			63	33.9

	W	1/4 of	Eber St	
S			60	34.2
			57	34.5
			56	34.6
b			53	34.9
			53	34.9
			44	35.8
n			40	36.2

	Center	Eber	
n		37	36.5
		38	36.4
		43	35.9
b		47	35.5
		51	35.1
		50	35.2
S		53	34.9

	E	1/4 of	Eber	
S			46	35.6
			43	35.7
			45	35.7
b			40	36.2
			38	36.4
			35	36.7
n			32	37.0

	E	66 ft	Eber	
n			26	37.6
			29	37.3
			35	36.7
b			36	36.6
			41	36.1
			38	36.4
S			42	36.0

PLOTTED

4020

E 2 f

Elev

S 34 36.8

32 37.0

34 36.8

b 28 37.4

29 37.3

26 37.6

n 23 37.9

TP

1280

5075

225

3795

2.04 Elev

50

E f

Elev

n 99 40.9

106 40.2

105 40.3

b 105 40.3

110 39.8

112 39.6

S 114 39.4

5075

100

E f

Elev

S 95 41.3

92 41.6

92 41.6

b 82 42.6

80 42.8

82 42.6

n 72 43.6

150

E f

Elev

n 55 45.3

64 44.4

67 44.1

b 67 44.1

71 43.7

73 43.5

S 74 43.4

P. Stone

43

4020  
225  
3795  
1280  
5075

PLOTTED

5075

6142

R Jones

44

200

E

of Eben

300

E

of Eben

S 50 45.8

S 101 51.3

50 45.8

102 51.2

46 46.2

102 51.2

b 41 46.7

b 102 51.2

37 47.1

102 51.2

36 47.2

101 51.3

2 32 47.6

2 97 51.7

250

E

of Eben

350

E

of Eben

2 12 49.6

2 66 54.8

16 49.2

72 54.2

22 48.6

68 54.6

b 19 48.9

b 67 54.7

24 48.4

71 54.3

20 48.8

71 54.3

S 27 48.1

S 71 54.3

7P

1285

6142

218

4857

PLOTTED

PLOTTED

5075  
1285  
4857  
6142

61.42

400

E 7

Eben

5

55 55.9

50 56.1

48 56.6

6

42 57.2

40 57.4

42 57.2

2

35 57.9

450

E 7

Eben

2

20 59.4

27 58.7

31 58.3

6

34 58.0

41 58.3

41 58.3

5

45 58.9

PLOTTED

61.42

500

E 7

Eben

5

32 58.2

25 58.9

20 59.4

14 60.0

11 60.3

04 60.8

2

02 61.2

BMP

528

6281

100

60.42

Bm Stanley  
Jr

550

E 7

Eben

2

57 44.1

64 43.4

6

69 42.9

76 42.2

78 42.0

5

86 41.2

94 40.4

D Jones

45

6043

6120

62.81



6981

600

E

W2 Founds (60)

S 76 42.2

70 42.8

63 43.5

6 58 44.0

52 44.4

48 45.0

N 37 44.1

W 606 Founds

N 32 46.3

42 45.4

48 45.0

6 56 44.2

61 43.7

67 43.1

S 73 42.5

6981

D Jones

46

9W

1/4

Founds

B 66 43.2

58 44.0

57 44.1

49 44.9

44 45.4

36 46.2

N 25 47.3

Center of Founds

20 47.8

32 44.4

38 44.0

6 43 45.5

50 44.8

55 44.3

S 62 43.6

PLOTTED

6981

	E	1/4 of	Front	
S			5.8	64.0
			4.8	65.0
			4.8	65.0
b			3.8	66.0
			3.3	66.5
			2.7	67.1
n			2.0	67.8
	E. 1/4 of Front			
n			1.6	68.2
			2.6	67.2
			3.0	66.8
b			3.5	66.3
			4.5	65.3
			5.2	64.6
S			5.7	64.1

PLOTTED

6981

P. Front

47

	E	Line	Front	
S			5.0	64.8
			4.5	65.3
			3.8	66.0
			3.2	66.6
			2.6	67.2
			2.1	67.7
n			1.3	68.5
	TP	968	78.21	1.28
				68.50
		50	E of	Front
n			7.5	70.7
			8.2	70.0
			8.3	69.9
b			9.3	68.9
			9.4	68.8
			10.0	68.2
S			10.7	67.5

n E of  
Front6981  
1.28  
68.50  
7.68  
78.21

7821

100 E of Founds

S	87	69.5
	85	69.7
	80	70.2
b	73	70.9
	65	71.7
	60	72.2
n	51	73.1

150 E of Founds

n	30	75.2
	40	74.2
	44	73.8
b	51	73.1
	58	72.4
	64	71.8
S	71	71.1

PLOTTED

7821

200 E of Founds

S	59	72.3
	52	73.0
	44	73.8
b	38	74.4
	31	75.1
	27	75.5
n	19	74.3

250 E of Founds

n	11	77.1
	16	76.6
	19	76.3
b	26	75.4
	32	75.0
	38	74.4
S	38	74.4
TP	1314	71.08
		027
		77.24

P Founds

48

7821  
27  
77.1  
1314  
91.08

91.08

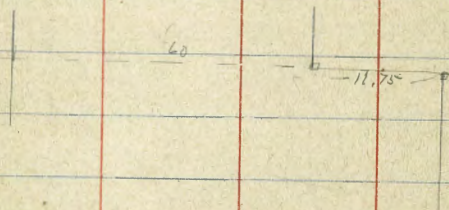
91.1

311 E = PL 22 Q.B.

S	114	79.3
	115	79.9
	111	80.0
	108	80.3
	103	80.8
	100	81.1
N	103	80.9
1175 m of = 70' in R down P. 15	107	80.9

This St is 71.75' wide at its base +

70' at Santa Barbara



-708-

PLOTTED

91.04

91.1

P. 4. 0. 0. 0.

49

(71.75) 50' E of it. P. 4. 0. 0. 0.

N	34	87.7		
	40	87.1		
	48	86.3		
b	49	86.2		
	52	85.9		
	55	85.6		
S	59	85.2		
TP	1295	10266	142	89.6
	100	E 8	P. 2	
S			94	93.2
			104	92.2
			101	92.5
b			97	92.9
			90	93.4
			81	94.5
N			78	94.8

91.08  
- 1.04  
89.66  
12.95  
102.61

102.01

114.62

R. Jones

50

114.6

150 E 8 P 2

250 E 8 P 2

n  
10 101.6  
15 101.1  
28 99.8  
b 35 99.1  
36 99.0  
35 99.1  
S 34 99.2

n  
18 112.8  
21 112.5  
24 112.4  
b 24 112.4  
23 112.3  
25 112.1  
S 32 111.4

102.01  
101.50  
101.00  
114.62  
22  
114.40  
130  
127.5

TP 1232 114.62 031 102.30

TP 1302 117.92 022 114.40

200 E 8 P 2

289 E 2 W 2 S 2 (60)

S  
94 105.2  
90 105.6  
86 104.0  
b 94 105.2  
94 105.2  
85 104.1  
2 78 104.8

S  
93 18.1  
104 17.0  
93 18.1  
b 88 18.6  
89 18.5  
85 18.9  
2 84 19.0

PLOTTED

12742

	W	66 f	Suzot
n			67 120.7
			70 20.4
			75 19.9
s			70 20.4
			72 20.2
			73 20.1
S			67 20.7

	W	14 f	Suzot
S			47 22.7
			48 22.6
			46 22.8
s			60 21.4
			57 21.7
			54 22.0
n			48 22.6

PLOTTED

12742

Alma

	Center of	Suzot
n		30 124.4
		43 23.1
		44 23.0
s		40 23.4
		38 23.6
		30 24.4
S		27 24.7

	E	10 f	Suzot
S			08 26.6
			14 26.0
			20 25.4
s			25 24.9
			27 24.7
			23 25.1
n			25 24.9

7P	1170	12884	028	12714
BM Chik	51117		7.68	12118 ✓

12742  
 12719  
 1129  
 10884  
 267  
 13177

13884

138.8

13884

138.8

P. 50

52

	E	bl of	Sumpt
1			118 127.0
			120 25.8
			120 26.8
6			121 26.7
			121 26.7
			114 27.4
S			113 27.5

	E	bl of	Sumpt
S			108 28.0
			106 28.2
			110 27.8
6			109 27.9
			98 29.0
			107 28.1
n			99 28.9

	50	E f	Sumpt
9			48 134.0
			57 33.1
			63 32.5
6			65 32.3
			72 31.6
			80 30.8
S			87 30.6

	100	E f	Sumpt
S			64 32.4
			60 32.8
			50 33.8
6			44 34.4
			36 35.2
			30 35.8
n			24 36.4

PLOTTED

13884

138.8

150

E of

Gauget

n	0.2	138.6
	1.4	37.4
	1.6	37.2
b	2.5	34.3
	2.8	34.0
	3.5	35.3
S	4.0	34.8

TP

1308

150.7

150.68

12.4

132.60

200

E of

Gauget

S	11.6	139.1
	11.2	39.5
	10.8	39.9
b	10.3	40.4
	9.4	41.3
	9.3	41.4
n	9.0	41.7

PLOTTED

150.68

150.7

250

E of

Gauget

n	4.3	146.4
	4.8	45.9
	5.6	45.1
b	5.9	44.8
	6.4	44.3
	6.8	43.9
S	7.0	43.7

300

E of

Gauget

S	2.0	48.7
	1.7	49.0
	1.3	49.4
TP	1.60	149.08
b	12.2	149.5
	11.7	50.1
	11.0	50.8
n	10.2	51.5

58

138.84  
 1.26  
 137.58  
 1.308  
 150.68  
 1.60  
 149.08  
 12.23  
 161.81

PLOTTED



11181

141.8

350

E 8

Guzot

n

52 156.6

55 156.3

65 155.3

b

67 155.1

76 154.2

86 153.2

S

86 153.2

400

E 8

Guzot

S

33 158.5

29 158.9

20 159.8

b

21 159.7

15 160.2

n

08 161.0

TP

1281

17396

06 161.5

n

120 162.0

17396

174.0

P. J. J. J.

54

450

E 8

Guzot

n

61 147.9

68 147.2

78 146.2

b

83 145.7

88 145.2

92 144.8

S

97 144.3

500

E 8

Guzot

S

29 171.1

27 171.3

20 172.0

b

20 172.0

03 173.7

TP

1263

18630

020 173.67

119 174.4

n

119 174.4

11181  
141.8  
1281  
17396  
1263  
18630  
173.67  
174.0  
174.0

PLOTTED

18630  
184.3

550' E of Survey

N 44 181.9

47 81.4

52 81.1

6 75 78.8

75 79.8

82 78.0

S 84 77.9

595' E of Survey

TP 736 1932 044 185.86

S 101 183.1

94 83.8

86 84.4

6 81 85.1

66 86.4

63 86.9

N 53 87.9

PLOTTED

1932  
1932

Ploma

55

(70.8) 600' E = WS Santa Barbara (blind)

N 55 187.7

57 87.5

64 84.8

1 56 87.6

59 87.3

64 84.8

S 69 84.3

TP 1239 20560 00 1932

1036 21500 052 20504

Bm 303 212.37

Bm Shady

PLOTTED

18630  
184.3  
185.86  
1932  
1239  
20560  
20504  
1036  
21500  
303  
212.37



16845

70676 W = P b

n	35	145.0
	39	144.4
	44	144.1
	45	144.0
	49	143.5
	51	143.4
S	47	143.9

13176 W = E of Chatsworth  
(on top of Bank)

25' S of SA	60	142.5
SA	54	143.1
	52	143.3
	48	143.5
	44	144.1
	39	144.6
	35	145.0
n	36	144.9
25' N of SA	31	145.4

PLOTTED

PLOTTED

1485

E of Chatsworth  
on graded street

25' N of rd	78	140.7
n	69	141.4
b	71	141.4
SA	69	141.4
25' S of SA	68	141.7

PLOTTED

9  
23  
13

X Sec Browning St (70')  
Wd Roseville to Chatsund  
166.31 P 50

Probably in Wd Roseville 221' W of Glen

S	8.0	158.3
	9.6	
	10.5	
b	11.1	55.2
	13.0	
	13.7	
2	14.8	51.5
	50' W of P 2	
2	12.1	50.2
	12.6	
	12.1	
b	11.5	55.8
	10.4	
	9.4	
S	8.5	57.8

166.31

57

105.76 W = B b

S	7.5	158.8
	7.8	
	8.5	
b	9.0	57.3
	9.8	
	9.8	
2	10.2	56.1
	131.76 W = E 2 Chatsund Graded	
25' in pond	10.4	
11.2	9.1	57.2
	8.6	
	8.5	
b	8.0	58.3
	7.8	
	7.6	
	7.2	
9.2		
25' sq sec	6.8	59.5

PLOTTED

9  
22  
13.8

X 2c  
Bluff  
Rossville

Centers St(70)  
to Chasworth Blm  
15099 7 5%

PA

W.L. Rossville - no willow

S  
76 143.4  
78  
82

6  
86 42.4  
92  
93

7  
82 41.8

n 50' W J PA  
70 44.0  
78  
70

6  
67 44.3  
66  
55

S  
51 45.9

This stat has been graded  
roughly

PLOTTED

1510

58

10676 W = PA

S  
28 148.2  
30  
45  
47  
Sutta

6  
47 46.3  
47  
53  
44  
Sutta

7  
44 46.5

13176 W = S of Chasworth  
5' W J PA  
41 46.9  
44  
45 46.5  
50

6  
45  
42 46.8  
40

S  
37

52  
25 57.32  
44  
12 49.8

PLOTTED

X sect. line of a.	4th street	street H.I.	from	South line Cedar	to North	110.98	110.76	150' 20.	Aug 27/13	Chert. ds letter Bunker
13' quarter	0.22	110.98								
			South line Cedar	W gutter						
E gutter			3.1	107.9				9.8	101.2	
			2.6	84	C			8.9	2.1	
C			2.4	84				8.4	2.4	
			2.9	81	E gutter			8.7	2.3	
W gutter			3.6	74				8.7	2.3	
								200' 20.		
	50' 20.				E gutter					
W. gutter			5.6	54				10.7	100.3	
			4.8	62	C			10.5	0.5	
C			4.3	47				10.4	0.4	
			4.6	44	W gutter			10.9	0.1	
E. gutter			4.9	41	S.P.			11.8	99.2	
								H.E.		
						0.90	99.23	1265	98.33	
	100' 20.							250' 20.		
E gutter			6.9	41	W gutter					
			6.5	45				2.1	97.1	
C			6.4	44	C			1.1	98.1	
			6.7	43				0.6	98.4	
W gutter			7.7	33	E gutter			0.8	98.4	
								0.9	98.3	

99.23

300' so. (North line of Beech)

E guttes	2.5	96.7
	2.7	96.5
C	2.6	96.6
	3.2	96.0
W guttes	4.3	94.9

Center Beech

<del>W guttes</del>	4.4	94.8
W guttes	4.2	95.0
	4.2	95.0
C	3.7	95.5
	3.7	95.5
E guttes	3.7	95.5
E prop.	2.9	96.3

99.23

60

20' line Beech

E guttes	5.0	94.2
	4.8	94.4
C	4.7	94.5
	5.4	93.8
W guttes	6.6	92.4

50' so.

W guttes	8.6	90.4
	7.6	91.4
C	7.0	92.2
	7.0	92.2
E guttes	7.2	92.0

100' so.

E guttes	9.7	89.5
	9.4	89.8
C	9.4	89.8
	9.9	89.3
W guttes	10.8	88.4



99,23

61

150' 20.

W gutter		12.9	84.3
		12.2	87.0
C		11.7	87.5
		11.7	87.5
E gutter		12.1	87.1
J.P.	0.04	H.I. 86.29	12.98 86.25

200' 20.

E gutter		1.7	84.5
		1.2	85.1
C		1.2	85.1
		1.4	84.9
W gutter		2.3	84.0

250' 20.

W gutter		4.3	82.0
		3.9	82.4
C		3.4	82.9
		3.5	82.8
E gutter		4.0	82.3

84.79

300' 20. (north line ash)

E gutter	6.2	80.1
	5.8	80.5
C	5.6	80.7
	6.0	80.3
w gutter	6.6	79.7
	Center	
w. fine	6.9	79.4
w. gutter	7.5	78.8
	6.9	79.4
C	6.6	79.7
	6.7	79.4
E gutter	7.3	79.0
E line	6.4	79.9

86.29

62

50' line ash

E gutter	8.4	77.9
	8.0	78.3
C	7.9	78.4
	8.3	78.0
w gutter	8.9	77.4
	50' 20.	
w gutter	11.9	74.4
	11.1	75.2
C	10.8	75.5
	11.0	75.3
E gutter	11.6	74.7
J.P.	0.47	74.26
	H.I. 12.50	
	73.79	
	100' 20.	
E gutter	2.6	71.7
	2.0	72.3
C	1.8	72.5
	2.2	72.1
w gutter	2.9	71.4

74,26

150' 20.

W gutter

5.9 48.4

C

5.2 49.1

4.9 49.4

5.0 49.3

E gutter

5.6 48.7

200' 20.

E gutter

8.8 45.5

8.1 46.2

C

8.0 46.3

8.3 46.0

W gutter

8.9 45.4

250' 20.

W gutter

11.9 42.4

11.6 42.7

C

11.1 43.2

11.4 42.9

E gutter

11.9 42.4

N.E.

63

S.P.

3.09 65.33 12.02 62 24

370' 20. north line A.

E gutter

5.7 59.4

5.4 59.9

C

5.1 40.2

5.4 59.9

W gutter

5.4 59.9



LEVELS OVER CURB  
ON ROBINSON AVE.  
ALBATROSS WEST.

B.M. 2.95 270.01 267.06

W. L. ALBATROSS

N 3.73 266.38

S 4.40 265.61

25' WEST

S 4.77 265.24

N 4.18 265.83

50' WEST

N 4.49 265.52

S 5.07 264.94

75' WEST

S 5.30 264.71

N 4.86 265.15

100' WEST

N 5.18 264.83

S 5.43 264.58

125' WEST

S 5.40 264.61

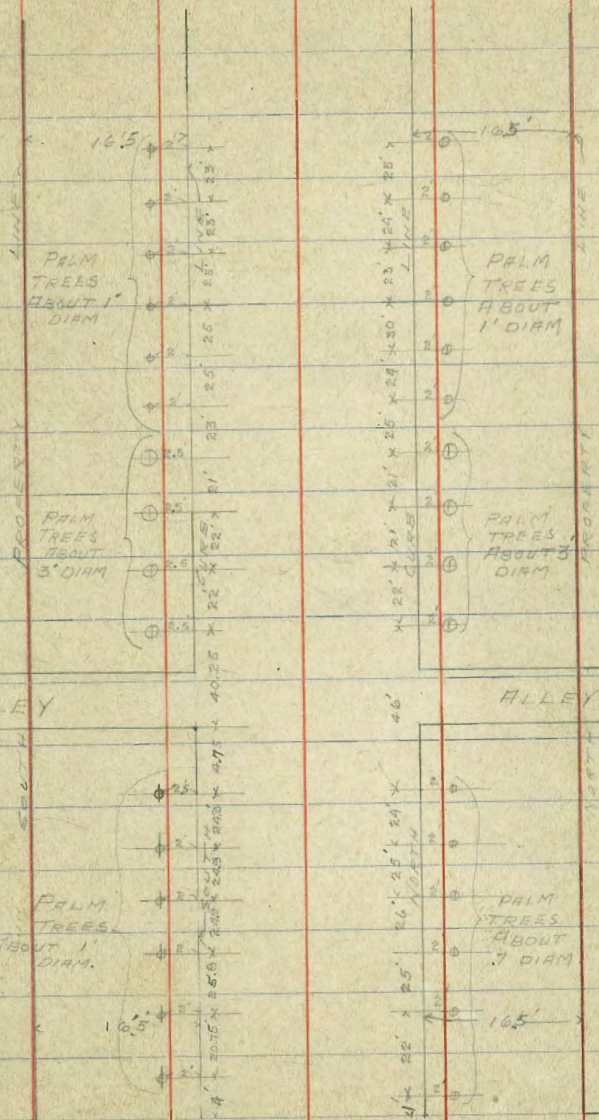
N 5.47 264.54

130' WEST = END ON SOUTH

S 5.41 264.60

NEALB.  
+ ROBN.

LOCATION OF TREES ON ROBINSON AVE. WEST OF ALBATROSS ST. 65



ALBATROSS

ST.

270.01

150' WEST

N 5.83 264.18

S No. CURB

175' WEST

S No. CURB

N 6.08 263.93

200' WEST

N 6.43 263.58

225' WEST

N 6.73 263.28

245' WEST = END ON NO.

N 6.94 263.07

9  
30  
10  
blows

Levels for Culvert on  
Plum St bet Zouch & Albert

	1275	106.50		9375
	1240	118.58	0.32	106.18
TP	451	<u>121.54</u>	1.55	117.03

114.5  
122.5  
4' 6" = E } Culvert dia  
about a W }

34' 3" gnd		120		109.5
32		112		110.3
Cent		82		113.3
W2		63		115.2
23' 2" gnd		46		116.9

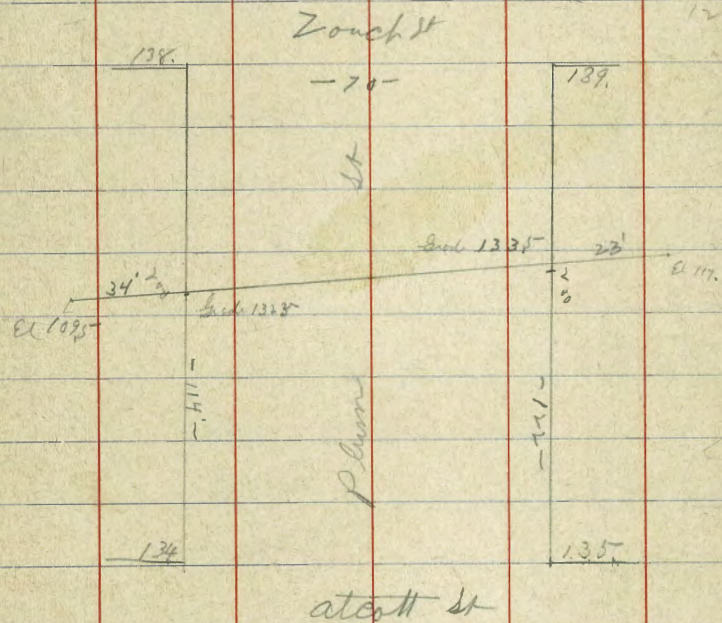
3m. 1 inch  
at Millers  
& Albert

18" 20" Culvert

67

No Slopes required

9.175  
12.25  
102.50  
10.75  
106.75  
12.40  
118.58  
1.55  
121.03  
1.54  
122.57



9/30 Along Slopes at Plum + Newell st

080	10048		9968	Bm NE R
20	<u>8280</u>	1288	8260	Macaulay & Plum

S line of Newell at Plum st

82		66	9968
73' 0" 01		82	10048
			1288
			8260
			8280

Center of Newell

82		110	
73' 3" 91		142	
TP	080	<u>75.90</u>	1270 7540

W line of Newell

82		60	
74' 3" 42		110	



9  
10

Levels for culvert on Plum St  
at Gothe St

250 9475 9225

055 8280 1250 8225

50' n of S of Gath } culvert line  
60' n of S of Gath }

18' n of rd 84

rd 96

cent 124

EL 128

25.5' E of line 144

Br SW H  
Goth St  
Plum

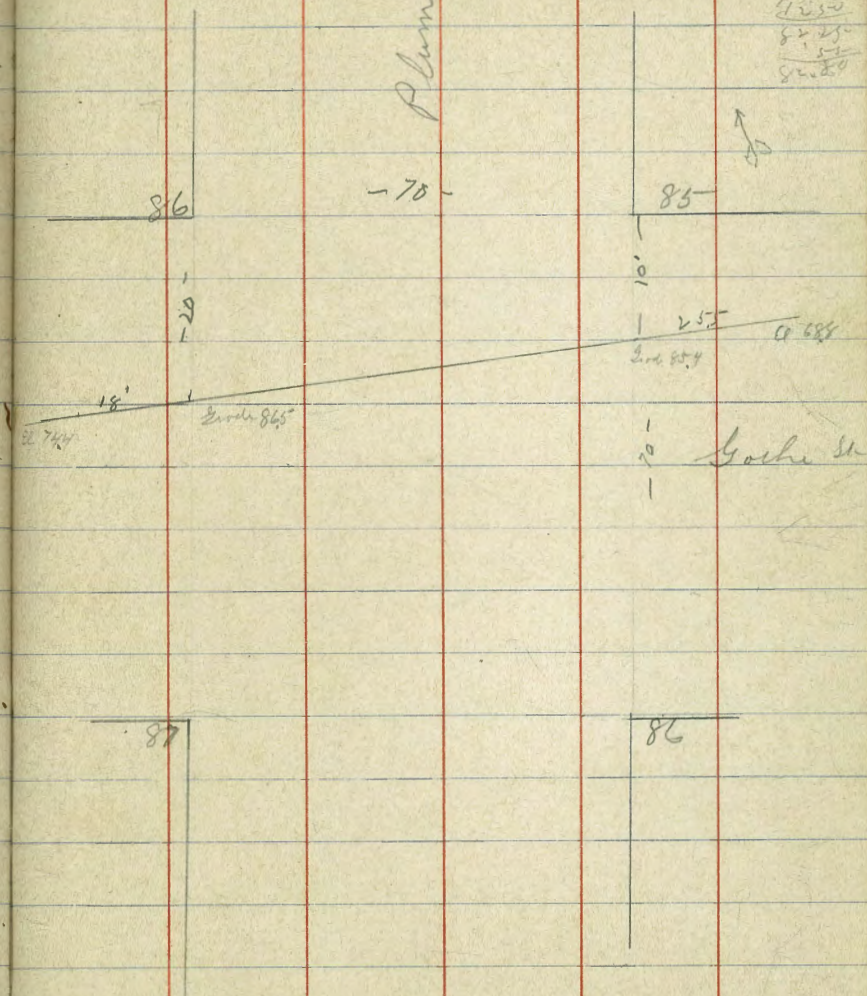
30" or 36" culvert

no slopes required

69

Plum St

9225  
9475  
9225  
8225  
8280



2  
30  
73

Level notes for Culvert on Plum St  
Bet Emerson & Fenelon

015      95.55      95.40      TD 13.364  
1920

47' E 88 E	19.2
E line	130
South	80
W 2	38
2 1/2' depth	18

18" Culvert

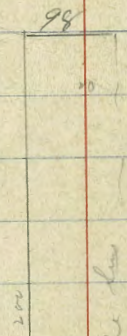
Slopes on next page

70

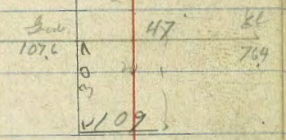
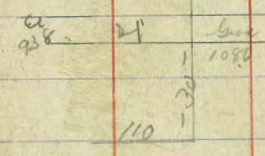
Fenelon



Plum St



Emerson



Emerson

10 1/3 along		Dikes on Plum St dit		
Emerson & Fenelon				TP on P's
1.70	96.10		95.40	
on line		20' E of E of Plum		
N. of Emerson	1.0	95.1	$\begin{array}{r} 100.0 \\ - 4.9 \\ \hline 95.1 \end{array}$	
30' N of Emerson	1.3	80.8	$\begin{array}{r} 100.0 \\ - 19.2 \\ \hline 80.8 \end{array}$	
30' N of Emerson 47' E of Plum	2.0	76.1	$\begin{array}{r} 100.0 \\ - 23.9 \\ \hline 76.1 \end{array}$	
50' N of "	9.0	87.1	$\begin{array}{r} 100.0 \\ - 12.9 \\ \hline 87.1 \end{array}$	
75' N of "	4.6	91.5	$\begin{array}{r} 100.0 \\ - 8.5 \\ \hline 91.5 \end{array}$	
100' N of "	1.0	95.5	$\begin{array}{r} 100.0 \\ - 4.5 \\ \hline 95.5 \end{array}$	
TP	11.00	103.45	92.45	
150' N of "	7.6	96.3	$\begin{array}{r} 100.0 \\ - 3.7 \\ \hline 96.3 \end{array}$	
200' N = S of Fenelon (2)	11.0	97.9	$\begin{array}{r} 100.0 \\ - 2.1 \\ \hline 97.9 \end{array}$	
South "	13.5	90.4	$\begin{array}{r} 100.0 \\ - 9.6 \\ \hline 90.4 \end{array}$	
N. of Fenelon	14.1	89.8	$\begin{array}{r} 100.0 \\ - 10.2 \\ \hline 89.8 \end{array}$	
25' N of "	15.0	88.9	$\begin{array}{r} 100.0 \\ - 11.1 \\ \hline 88.9 \end{array}$	

10  
13

Sends for Culvert or Plum  
at Dickens

040

12845

12805

on top  
of  
Dickens  
Plum

8" culvert

72

7' 70' w.d.

76

N.E. corner Dickens & Plum

86

Leant

131

TP 076

11637

1294

11591

Edin

58

23' edge

80

Slope

TP

293

11890

030

11607

Slope 70' E of E.L. Plum

S.L. Dickens

71.0

Leant

11.0

N.L.

73

no Slopes required at Byron  
Level E+W

Dickens

1235  
7'  
1208

1238  
End

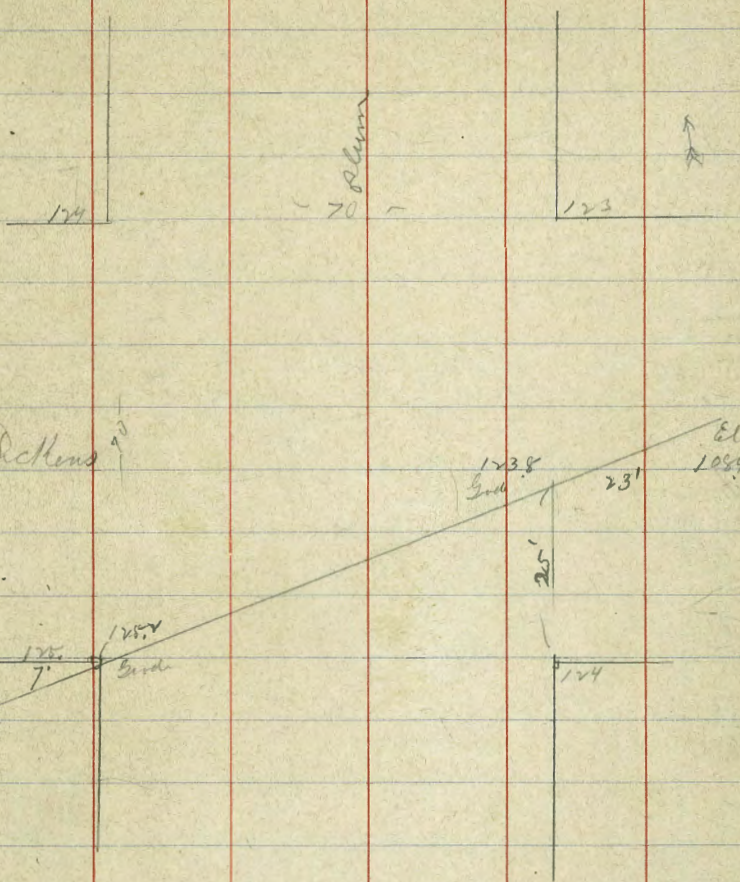
23'

EL  
1084

25'

124

Plum

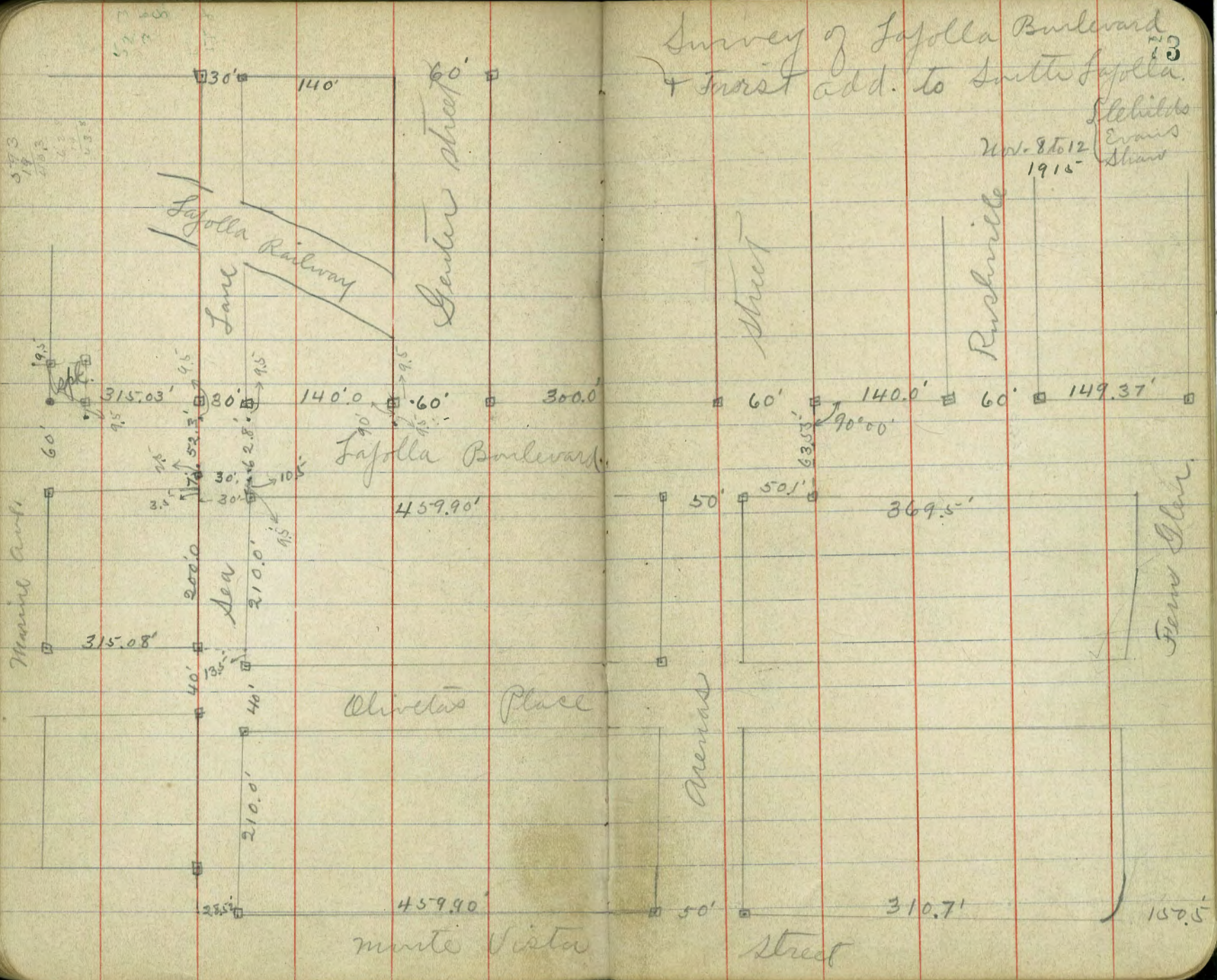


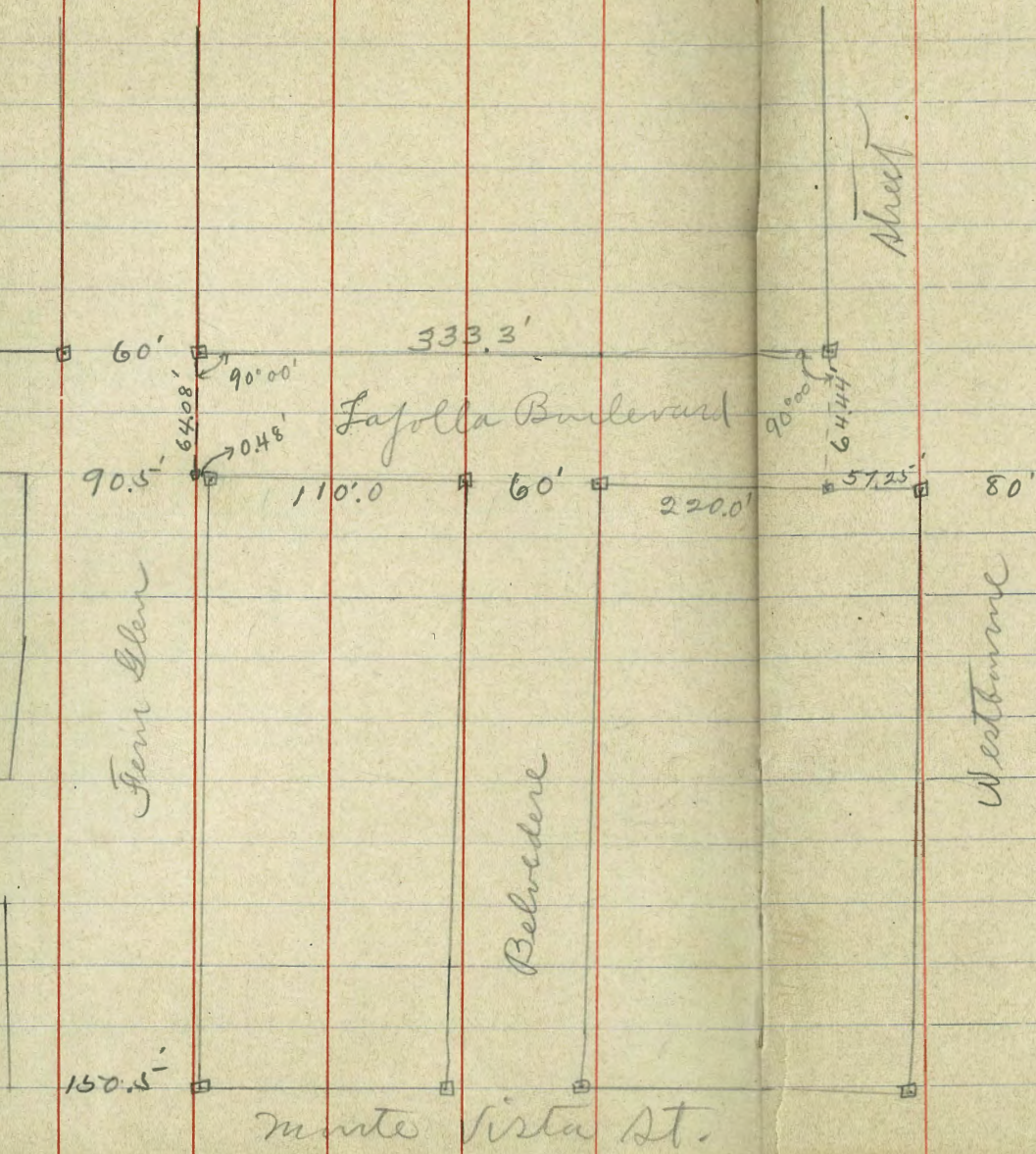
Survey of Lafayette Boulevard  
 & first add. to South Lafayette.

Stebbins  
 Evans  
 Shaw

Vol. 8 to 12  
 1915

13















Hansley St

833	769.0	68.7	3m brams m
H. N. E. Int. Errors	83	68.6	
E. Prop. Errors 50' n m	95	67.4	
100' E. g. Errors 25' n m	89	68.0	
End of Subint at Hansley	75	69.4	

106.76 4<sup>th</sup> ash nry of first hd.  
 110.76 " " Cedar SW bot Elect's

204.80  
 80  
 624.80  
 37  
 587.80  
 281  
 68  
 693  
 1386  
 14553

363 } 856  
 726  
 1300  
 1089  
 2110

251  
 65  
 693  
 1386  
 144

112.19  
 110.23  
 .01.96  
 .04 88

115.1  
 157  
 301 1593

02131  
 80  
 170480

01967  
 37  
 13769  
 5901  
 72779

11  
 14.5  
 39  
 19.5

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.