

943

943

F. B. 943

380

FIELD



MICROFILMED  
DEC 16 1964

780  
3260



#47  
 $\Delta = 165^\circ$  L  
 $R = 50'$   
 $L = 144'$   
 $BC = 358 + 162$   
 $EC = 359 + 602$

#48  
 $\Delta = 28^\circ 50'$  R  
 $R = 300$   
 $St = 77.12$   
 $L = 150.97$   
 $BC = 361 + 3312$   
 $EC = 362 + 8420$

#49  
 $\Delta = 22^\circ 50'$  R  
 $R = 300$   
 $St = 60.58$   
 $L = 119.56$   
 $BC = 366 + 2878$   
 $EC = 367 + 6830$

#50  
 $\Delta = 82^\circ 17'$  L  
 $R = 300$   
 $St = 86.83$   
 $L = 169.13$   
 $BC = 369 + 3627$   
 $EC = 371 + 5450$

#51  
 $\Delta = 83^\circ 08'$  L  
 $R = 300$   
 $St = 70.94$   
 $L = 116.08$   
 $BC = 376 + 3050$   
 $EC = 377 + 4658$

#52  
 $\Delta = 87^\circ 11'$  L  
 $R = 300$   
 $St = 70.94$   
 $L = 116.08$   
 $BC = 376 + 3050$   
 $EC = 377 + 4658$

# Tarry Pipes Change of Line

0.75 225.89  
 TP. top of West Fence post 225.44  
 North of Road Sta about 357+85 ✓  
 TP. 072 214.01 12.60 213.29

359+60<sup>2</sup> EC 50' R left

W	3.4	210.6
cr	3.5	210.5
3 E	2.9	211.1
6 E	1.9	212.1
13 E	6.0	208.0
20 E	10.5	203.5

360+00

20 E	13.5	200.5
13 E	8.6	205.4
9 E	6.5	207.5
cr	6.5	207.5
W	7.1	206.9

360+50

W	10.2	203.8
cr	10.3	203.7
8 E	10.4	203.6
13 E	13.1	200.9
20 E	16.0	198.0

TP. 059 201.64 12.96 201.05

361+00

W	1.6	200.0
cr	1.1	200.5
13 E	6.6	195.0
20 E	8.9	192.7



20164

361+33<sup>13</sup> BC 300' R. Right

20'E	13.2	188.4
13'E	10.7	190.9
CV	5.2	196.4
3'W	9.4	198.2
13'W	3.6	198.0

361+50

13'W	4.5	197.1
4'W	4.4	197.2
CV	7.3	194.3
13'E	12.6	189.0
20'E	15.8	185.8

361+75

20'E	16.0	185.6
13'E	13.8	187.8
CV	9.8	191.8
7'W	5.8	195.8
13'W	6.0	195.6

362+00

13'W	7.1	194.5
11'W	7.3	194.3
CV	12.0	189.6
13'E	15.9	185.7
20'E	18.5	183.1

20164

362+25

13'W	10.2	191.4
CV	12.9	188.7
TR 195	190.77	1282
13'E	5.7	185.1
20'E	8.2	182.6

362+50

20'E	9.2	181.6
13'E	6.4	184.4
CV	3.7	187.1
13'W	2.3	188.5

362+75

13'W	6.8	184.0
CV	9.8	181.0
13'E	12.8	178.0
20'E	14.3	176.5

362+84<sup>10</sup> EC 300' R. Right

20'E	14.6	176.2
13'E	13.5	177.3
CV	10.7	180.1
13'W	7.9	182.9

363+00

13'W	9.8	181.0
CV	11.5	179.3
13'E	13.8	177.0
20'E	15.2	175.6

TR 184

190.10 1261

178.16



150.00

363+50

13W	3.5	176.5
CV	5.7	174.3
13E	8.0	172.0
20E	8.8	171.2

364+00

20'E	14.1	165.9
13E	13.1	166.9
CV	10.7	169.3
13W	7.8	172.2

364+50

13W	9.9	170.1
10W	10.1	169.9
TP 041	168.03	1238
CV	2.9	165.1
13E	4.3	163.7
20E	5.5	162.5

365+00

20E	9.1	158.9
13E	9.7	158.1
CV	6.3	161.7
13W	3.6	164.4

365+50

13W	9.9	158.1
CV	11.9	156.1
13E	17.0	154.0
20E	15.4	152.6

Note Pine Tree Sta 365+94  
13' W of R Eley ground. 142.11 3

168.03

TP 004

155.39 1268

155.35

366+00

13W	4.5	150.9
CV	5.2	150.2
13E	7.0	148.4
20E	8.1	147.3

366+38<sup>23</sup> BC 300' R Right

20'E	12.9	142.5
13E	11.6	143.8
CV	9.0	146.4
13W	6.4	149.0

366+50

13W	7.3	148.1
CV	9.1	146.3
13E	11.9	143.5
20E	13.7	141.7

366+75

20E	15.1	140.3
13E	13.0	142.4
CV	9.5	145.9
13W	8.2	147.2

367+00

13W	10.5	144.9
CV	12.0	143.4
13E	15.8	139.6
20E	17.2	138.2

TP 017

143.50 1206

143.33



143.50

367+25

13 W	1.4	142.1
CV	2.5	141.0
13 E	5.5	138.0
20 E	6.5	137.0

367+58<sup>90</sup> EC 300' R Right

20 E	10.5	133.0
10 E	9.7	133.8
CV	6.6	136.9
13 W	4.5	139.0

368+00

13 W	8.2	135.3
CV	10.7	132.8
13 E	13.5	130.0
20 E	14.7	128.8
TP	0.46	131.16
	1280	131.70

368+50

13 W	0.2	131.0
CV	2.8	128.4
13 E	5.3	125.9
20 E	6.4	124.8

369+00

20 E	11.2	120.0
13 E	9.5	121.7
CV	7.0	124.2
8 W	3.6	127.6
13 W	3.6	127.6

131.16

369+35<sup>90</sup> EC 300' R Left

13 W	7.3	123.9
CV	11.3	119.9
13 E	13.4	117.8
20 E	15.5	115.7

369+50

20 E	17.3	113.9
13 E	15.0	116.2
CV	13.2	118.0
13 W	9.6	121.6

TP 0.63

118.90 1229

118.27

369+75

13 W	1.4	117.5
CV	3.3	115.6
13 E	6.9	112.0
20 E	7.6	111.3

370+00

20 E	10.1	108.8
13 E	9.5	109.4
CV	6.8	112.1
13 W	4.0	114.9

370+25

13 W	6.2	112.7
CV	8.8	110.1
13 E	11.2	107.7
20 E	12.3	106.6



	11890		
	370+50		
20'E		146	104.3
13'E		13.3	105.6
CV		11.1	107.8
13'W		8.2	110.7
	370+75		
13'W		9.1	109.8
CV		12.9	106.0
13'E		15.5	103.4
20'E		17.0	101.9
TP	028	106.44 <u>97.44</u>	127.4 <u>97.16</u> 106.16
		371+04 <sup>50</sup>	EC 300 R Left
20'E		6.0	100.5
13'E		4.1	102.3
CV		2.3	104.1
13'W		+0.5	107.0 <u>97.0</u>
	371+50		
13'W		2.5	103.9
CV		6.6	99.8
13'E		8.7	97.7
20'E		9.5	96.9
	372+00		
20'E		14.7	91.7
13'E		14.0	92.4
CV		10.5	95.9
13'W		7.4	99.0

	106.44		
	<u>97.44</u>		
	372+50		
13'W	Present in Road	9.0	97.4
10'W		9.8	96.6
CV		13.8	92.6
TP	145	95.59 <u>86.69</u>	123.0 <u>94.14</u> <u>85.13</u>
13'E		6.3	89.3
20'E		7.8	87.8
	373+00		
20'E		10.1	85.5
13'E		8.1	87.5
CV		4.5	91.1
6'W	in present road	2.1	93.5
13'W		2.2	93.4
	373+50		
13'W		6.4	89.2
CV	edge of present road	7.1	88.5
13'E		8.7	86.9
20'E		10.2	85.4
	374+00		
20'E		18.1	77.5
13'E		16.4	79.2
CV		13.3	82.3
6'W	in road	10.7	84.9
13'W		11.2	84.4
TP	206	82.55 <u>73.65</u>	131.0 <u>82.49</u> <u>73.59</u>



82.55

73.66

374+50

12W edge of road	3.9	78.7
CV	9.8	72.8
13E	11.9	70.7
20E	13.7	68.9

375+00

12W edge of Road	9.9	72.7
T.P. 0.02	<u>69.87</u>	<u>60.95</u> 69.85
CV	4.1	65.8
13E	7.5	62.4
20E	8.7	61.2

375+50

20E	14.2	55.7
13E	12.4	57.5
CV	8.1	61.8
9W in road	3.1	66.8
18W " "	3.0	66.9

376+00

13W	9.6	60.3
3W	8.6	61.3
CV	10.3	59.6
T.P. 1.75	<u>58.69</u>	<u>57.24</u> 56.94
13E	5.2	53.5
20E	7.0	51.7

58.69

57.79376+30<sup>50</sup>

BC 50' R Left

20E	9.5	49.2
13E	6.6	52.1
CV in road	0.5	58.2
18W " "	1.4	57.3

376+50

12W	3.3	55.4
CV	2.7	56.0
7E	2.4	56.3
18E	6.5	52.2
20E	9.1	49.6

376+75

E	4.7	54.0
CV	5.4	53.3
W	6.0	52.7

377+00

W	9.0	49.7
CV	8.1	50.6
E	7.6	51.1

377+25

E	10.9	47.8
CV	11.3	47.4
W	12.2	46.5

377+41<sup>52</sup> 377+63<sup>57</sup>

W	14.7	44.0
CV	13.9	44.8
E	13.8	44.9



5269  
 5879  
 48.43

TP, 1.15 12.11 46.58  
 check. See B931P62 4.14 44.39 44.36

6/11/4 Hajah floors Hall Levels on side from Garnet to Touringuard

Comp. Grand	11.80	29.60	17.80
TP	13.24	41.22	27.95
N <sub>h</sub> Garnet			
E		13.5	27.7
cr		13.5	27.7
W		13.2	28.0
20 N			
W		13.1	28.1
cr		13.3	27.9
E		13.2	28.0
70 N			
E		12.7	28.5
cr		12.5	28.7
W		12.5	28.7
120 N			
W		11.8	29.4
cr		11.5	29.7
E		12.2	29.0
170 N			
E		11.5	29.7
cr		10.4	30.8
W		11.2	30.0
220 N			
W		10.2	31.0
cr		9.4	31.8
E		10.0	31.7



4122

270 N = 31.2 Fullport

E	9.1	32.1
cr	8.5	32.7
W	9.3	31.9

cr

W	8.4	32.8
cr	7.7	33.5
E	8.0	33.2

1 Nh

F	7.8	33.4
cr	7.2	34.0
W	7.9	33.3

50' N

W	7.2	34.0
cr	6.5	34.7
E	6.8	34.4

100' N

F	6.0	35.2
cr	5.7	35.5
W	6.4	34.8

150' N

W	5.6	35.6
cr	4.9	36.3
E	5.4	35.8

200' N

E	4.7	36.5
cr	4.1	37.1
W	4.9	36.3

4122

270' N = 31.2 Emerald

W	4.1	37.1
cr	3.2	38.0
E	3.7	37.5

cr

E	3.1	38.1
cr	2.9	38.3
W	3.6	37.6

Nh.

W	2.8	38.4
cr	2.4	38.8
E	2.7	38.5

50' N

E	2.2	39.0
cr	1.6	39.6
W	2.0	39.2

100' N

W	1.3	39.9
cr	0.7	40.5
E	1.0	40.2

TD

12.44

53.06 0.60

40.62

150' N.

E	12.0	41.1
cr	11.5	41.6
W	12.3	40.8



5306

200 N

W	11.1	42.0
cr	10.5	42.6
E	11.0	42.1
* Angle - w	370 N = SL	Diamond
E	9.6	43.5
cr	9.8	43.8
W	10.1	43.0
	cr	
W	9.4	43.7
cr	8.4	44.7
E	8.9	44.2
	NA	
E	8.1	45.0
cr	7.7	45.4
W	8.6	44.5
	50 N	
W	7.0	45.6
cr	6.6	46.5
E	7.2	45.9
	100 N	
E	6.2	46.9
cr	5.7	47.4
W	6.7	46.4
	150 N	
W	5.2	47.9
cr	4.4	48.7

5306

200 N

E	4.9	48.2
	200 N	
E	3.8	49.3
cr	3.2	49.9
W	4.2	48.9
	270 N = SL	Missouri Ave
W	2.3	50.8
cr	1.5	51.6
E	2.0	51.1
	cr	
E	1.0	52.1
cr	0.7	52.4
W	1.5	51.6
TP	12.97	65.76 0.27
	NA	52.79
W	13.2	52.6
cr	12.4	53.4
E	13.0	52.8
	50 N	
E	11.7	54.1
cr	11.1	54.7
W	12.0	53.8
	100 N	
W	10.8	55.0
cr	9.8	56.0
E	10.4	55.4



65.76

150' N

E	9.4	56.4
cr	8.7	57.1
W	9.7	56.1

200' N

W	8.4	57.4
cr	7.7	58.1
E	8.5	57.3

270' N = SL Chalcedony

E	6.7	59.1
cr	6.0	59.8
W	6.8	59.0

cr

W	5.9	59.9
cr	5.0	60.8
E	5.7	60.1

Nh.

E	4.7	61.1
cr	4.1	61.7
W	4.9	60.9

50' N

W	3.8	62.0
cr	3.1	62.7
E	4.0	61.8

100' N

E	3.1	62.7
cr	2.2	63.6

65.76

2.9

62.9

150' N

W	1.8	64.0
cr	1.2	64.6
E	1.7	64.1

200' N

E	0.7	65.1
cr	0.2	65.6
W	0.9	64.9

TP 13.30

78.57 055 65.21

270' N = SL Law

W	12.4	66.1
cr	11.7	66.8
E	12.3	66.2

cr

E	11.6	66.9
cr	11.2	67.3
W	11.8	66.7

Nh.

W	11.0	67.5
cr	10.4	68.1
E	11.1	67.4

50' N

E	10.5	68.0
cr	9.6	68.9
W	10.1	68.4



78.51  
100' N

W	9.6	68.9
cr	9.0	69.5
E	9.8	68.7

150' N

F	8.9	69.6
cr	8.3	70.2
W	8.8	69.7

200' N

W	7.9	70.6
cr	7.4	71.1
E	8.0	70.5

270' N = SL Buryl

F	7.0	71.5
cr	6.2	72.3
W	6.9	71.6

cr

W	6.0	72.5
cr	5.4	73.1
E	5.9	72.6

NH

F	5.0	73.5
cr	4.6	73.9
W	5.3	73.2

50' N

W	4.1	74.4
cr	3.4	75.1

78.51

E	4.1	74.4
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100' N

E	2.5	76.0
cr	2.1	76.4
W	2.6	75.9

150' N

W	1.1	77.4
cr	0.7	77.8
E	1.5	77.0

TP 1300 9124 032 78.19  
200' N

E	12.5	78.7
cr	12.0	79.2
W	12.4	78.8

270' N = SL Millbur

W	10.6	80.6
cr	10.3	80.9
E	10.9	80.3

cr

E	10.0	81.2
cr	9.4	81.8
W	9.5	81.7

NH

W	8.6	82.6
cr	8.5	82.7
E	8.9	82.3



		91.24	
	50' N		
E		7.7	83.5
cr		7.3	83.9
W		7.6	83.6
	100' N		
W		6.3	84.9
cr		5.9	85.3
E		6.5	84.7
	150' N		
E		5.1	86.1
cr		4.7	86.5
W		5.0	86.2
	200' N		
W		3.3	87.9
cr		3.2	88.0
E		3.6	87.6
	270' N = Sh Loring Pt.		
E	128' wide instead of 20	1.7	89.4
cr		1.8	89.4
W		1.6	89.6
	cr		
W		0.0	91.2
TP	1305	104.19	91.12
cr		12.7	91.5
E		12.9	91.3
* 3.5 Jog E	Nh		
E		11.5	92.7
cr		11.0	93.2

		104.19	
W		11.1	93.1
	50' N		
W		10.0	94.2
cr		9.7	94.5
E		10.4	93.8
	100' N		
E		9.2	95.0
cr		8.6	95.6
W		8.9	95.3
	150' N		
N		7.6	96.6
cr		7.2	97.0
E		7.9	96.3
	200' N		
E		6.5	97.7
cr		5.8	98.4
W		4.2	98.0
	260' N = Sh Hyacinth		
W		4.2	100.0
cr		4.0	100.2
E		4.5	99.7
	cr		
E		3.0	101.2
cr		2.7	101.5
W		2.9	101.3



104.19  
NA.

W		16	102.6
cr		1.4	102.8
E		1.9	102.3
TIP	1310	117.15	0.14
		50' N	104.05
E		13.2	104.0
cr		12.7	104.5
W		13.0	104.2
		100' N	
W		11.3	105.9
cr		11.1	106.1
E		11.5	105.7
		150' N	
E		10.3	106.9
cr		9.4	107.8
W		9.8	107.4
		200' N	
W		8.5	108.7
cr		8.1	109.1
E		8.8	108.4
		250' N = Sh	Journal line
E		7.4	109.8
cr		6.9	110.3
W		7.1	110.1

117.15  
cr

W		6.0	111.2
cr		5.7	111.5
E		5.9	111.3
		NA.	
E		5.0	112.2
cr		4.6	112.6
W		5.0	112.2
		50' N	
W		3.9	113.3
cr		3.5	113.7
E		3.8	113.4
		100' N	
E		2.8	114.4
cr		2.0	115.2
W		2.3	114.9
		150' N	
W		0.7	116.5
cr		0.4	116.8
E		1.0	116.2
TIP	1193	128.81	0.37
		200' N	116.88
E		10.7	118.1
cr		10.3	118.5
W		10.5	118.3



125.51

255 N = SL Daphnia

W	8.3	120.5
cr	8.2	120.6
E	8.8	120.0

CV

E	7.0	121.8
cr	6.6	122.2
W	6.7	122.1

NV

W	4.8	124.0
cr	4.8	124.0
E	5.2	123.6

50' N

E	3.0	125.8
cr	2.7	126.1
W	2.9	125.9

100' N

W	0.8	128.0
cr	0.6	128.2
E	1.1	127.7

TP 1198 140.44 0.38 128.46

150' N

E	10.6	129.8
cr	10.1	130.3
W	10.4	130.0

140.44

200' N

W	8.3	132.1
cr	7.9	132.5
E	8.3	132.1

~~255 N = SL Tourguois~~

E	6.9	
cr	6.3	
W	6.6	

CV Tourguois

cr 4.5  
TP NW Sub. 11.6 137.55 4.05 136.39

255 S = SL Tourguois

W	2.7	134.9
cr	2.3	135.3
E	3.1	134.5

CV

CV	1.4	136.2
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W/L Tourguois (Pass?)

N	2.1	135.5
cr	2.9	135.2
O	3.2	134.4

100' W

S	5.7	131.9
cr	4.9	132.7
N	4.7	132.9



137.58  
200 W

N	7.0	130.6
cr	6.9	130.7
S	7.5	130.1

300 W

S	9.7	127.9
cr	9.2	128.4
N	9.3	128.3

400 W

N	11.3	126.3
cr	11.0	126.6
S	11.6	126.0
T.P	0.12	124.67
		13.00
		124.58

500 W

S	1.0	123.7
cr	0.7	124.0
N	1.2	123.5

600 W

N	3.9	120.8
cr	3.6	121.1
S	4.2	120.5

700 W

S	7.2	117.5
cr	6.8	117.9
N	7.1	117.6

800 W

N	10.1	114.6
cr	10.1	114.6
S	10.5	114.2

T.P 0.70

124.67  
112.84  
900 W

12.73  
111.94

S	2.0	110.6
cr	1.8	110.8
N	1.6	111.0

1000 W

N	5.6	107.0
cr	5.3	107.3
S	5.7	106.9

1100 W

S	8.3	104.3
cr	8.1	104.5
N	7.7	104.9

1200 W

N	10.7	101.9
cr	10.5	102.1
S	10.8	101.8

1300 W

S	12.9	99.7
cr	12.9	99.7
N	12.9	99.7

T.P 0.51

100.35  
12.80  
1400 W

99.84

N	1.6	98.8
cr	1.9	98.5
S	2.0	98.4



100.35

1500 W

S	4.0	96.4
cr	3.9	96.5
N	3.8	96.6

1600 W

N	6.8	93.6
cr	6.8	93.6
S	7.2	93.2

1700 W

S	9.9	90.5
cr	9.6	90.8
N	9.5	90.9

TP 0.10 81.00 ~~82.95~~ 81.30

1800 W

N	1.5	86.9
cr	1.7	87.6
S	1.3	87.1

15+98 ON Proj.

Top of Rail 5.36 83.04

TP 2.60 82.55 8.45 77.95

Check. Mon - 9.58 72.97 73.25

8/7/14  
8/8/14  
8/13/14

Levels on Bayard St from - 16  
Grand Ave to Tourquois -

B77 <sup>522</sup> Bas. Gravel. 18.73 17,804  
525 17.88 589 12,83  
TP. 50 36 7.52 23.55 187 16.01

Nh Gravel

E	11.3	17.3
13	11.8	11.8
cr	12.2	11.4
13	12.6	11.0
W	11.5	17.1

30' N

W	11.2	17.4
13	11.6	17.0
cr	11.2	17.4
13	10.9	17.7
E	10.7	17.9

70' N

E	10.1	13.5
13	10.2	13.4
cr	10.5	13.1
13	10.5	13.1
W	10.5	13.1

120' N

W	9.9	13.7
13	9.5	14.1
cr	9.5	14.1
13	9.2	14.0
E	8.6	15.0

PLOTTED



23.55

170' N

E	8.3	15.3
13	8.1	15.5
cr	8.4	15.7
13	8.7	14.9
W	9.0	14.6

220' N

W	7.6	16.0
13	7.5	16.1
cr	7.8	15.8
13	7.5	16.1
E	7.2	16.4

270' N - 5th Humbleud

E	6.6	17.0
13	6.8	16.8
cr	7.2	16.4
13	7.2	16.4
W	7.3	16.5

cr

W	6.4	17.7
13	6.4	17.7
cr	6.6	17.0
13	6.6	17.0
E	5.9	17.7

23.55

NL

E	5.6	18.0
13	5.9	17.7
cr	6.2	17.4
13	6.2	17.4
W	6.5	17.1

50' N

W	6.0	17.6
13	5.5	18.1
cr	5.8	17.8
13	5.4	18.2
E	4.9	18.7

100' N

PLOTTED

E	4.4	19.2
13	4.7	18.9
cr	5.3	18.3
13	5.2	18.4
W	5.5	18.1

150' N

W	5.0	18.6
13	4.9	18.7
cr	4.8	18.8
13	4.6	19.0
E	3.7	19.9



2355

300' N

E	3.2	20.6
13	3.9	19.7
cr	4.4	19.7
13	4.3	19.3
W	4.5	19.1

2665 N = Sh. Garnet

W	3.9	19.7
13	3.5	20.1
cr	3.4	20.7
13	3.0	20.6
E	2.7	20.9

cr

E	2.1	21.5
13	2.3	21.3
cr	2.8	20.8
13	2.6	21.0
W	2.9	20.7

NW Garnet

W	2.1	21.5
13	2.6	21.0
cr	2.3	21.3
13	1.7	21.9
E	1.6	22.0

Inside edge of Cementwalk

NW Cor. 2.04 21.51

TR 265 31.16 204 21.51

3116

50' N of Garnet

E	8.4	22.8
13	8.9	22.3
cr	9.1	22.1
13	9.6	21.6
W	9.2	22.0

100' N

W	8.9	22.3
13	8.9	22.3
cr	8.6	22.6
13	8.3	22.9
E	7.9	23.2

PLOTTED

180' N

E	7.3	23.9
13	7.7	23.5
cr	8.0	23.2
13	8.0	23.2
W	8.6	22.6

200' N

W	7.6	23.6
13	7.6	23.6
cr	7.3	23.9
13	7.0	24.2
E	6.4	24.8



3/16  
270' N = Sh. Feldspar

E	5.6	25.6
13, E	7.4	23.8
10 E	5.2	24.0
CV	6.2	24.0
13	6.4	24.8
W	6.9	24.2

CV Feldspar

W	6.0	25.2
13	5.9	25.7
CV	5.8	25.4
13	5.8	25.4
E	4.8	26.4

Nh.

E	4.7	26.5
13	5.4	25.8
CV	5.3	25.9
13	5.4	25.8
W	5.9	25.7

50' N

W	5.1	26.1
13	4.8	26.4
CV	4.6	26.6
13	4.7	26.5
E	4.0	27.2

3/16  
100' N

E	3.3	27.9
13	3.9	27.3
CV	3.9	27.3
13	4.2	27.0
W	4.3	26.9

150' N

W	4.0	27.2
13	3.3	27.9
CV	3.2	28.0
13	3.5	27.7
E	2.7	28.3

PLOTTED

200' N

E	2.2	29.0
13	2.8	28.4
CV	2.9	28.7
13	2.7	28.5
W	3.1	28.1

270' N = Sh. Emerald

W	2.3	28.9
13	1.9	29.3
CV	2.0	29.2
13	2.2	29.0
E	1.5	29.7

TP <sup>on slab</sup> 12.60

42.26 150

29.66



4226

CV

E	11.7	70.6
13	12.2	70.1
CV	12.0	70.7
13	12.0	70.7
W	12.2	70.1

N. L. Emerald

W	11.3	71.0
13	11.4	70.9
CV	11.0	71.3
7	11.2	70.9
13	12.5	79.8
E	11.9	70.4

50' N

E	9.7	74.6
13	12.2	70.1
10 from CV	10.6	71.7
CV	10.4	71.9
8	10.6	71.7
13	9.3	77.0
W	10.3	74.0

100' N

W	9.2	77.1
13	9.0	77.3
CV	9.3	77.0
9'	{ 9.2 10.1	{ 77.1 77.7
13	10.8	71.5
E	8.6	77.7

4226

150' N

E	7.5	76.8
13	8.8	73.5
	8.8	73.7
10	8.8	74.5
CV	8.1	76.7
13	8.2	74.1
W	8.3	74.0

500' N

W	7.4	76.9
13	7.4	76.9
CV	7.0	75.3
11	7.1	75.7
13	8.0	76.3
E	6.6	75.7

PLOTTED

570' N = St. Diamond

E	5.1	77.7
13	6.5	75.8
9	6.8	76.5
CV	6.0	76.3
13	4.1	76.7
W	6.3	76.0

CV

W	5.7	76.6
13	5.4	76.9
CV	5.4	76.9
13	4.9	77.4
E	4.3	78.0



4226

NL Diamond

E	3.7	38.6
13	4.4	37.9
CV	4.3	38.0
13	4.4	37.9
W	4.6	37.7

50' N

W	3.9	38.4
13	3.5	38.8
CV	3.1	39.2
8	2.9	39.4
13	3.7	38.6
E	2.5	39.8

100' N

E	1.7	40.6
13	2.7	39.6
10	2.2	40.1
CV	2.1	40.2
13	2.6	39.7
W	2.8	39.5

150' N

W	1.7	40.6
13	1.4	40.9
CV	1.1	41.2
10	1.2	41.1
13	1.9	40.4
E	0.6	41.7

4226

TPP 11.27

53.51 0.02

4224

200' N

E	10.7	42.8
13	11.1	42.0
10	11.8	41.7
CV	11.0	42.6
13	11.6	41.9
W	11.6	41.9

270' N = Sh Missouri Arc

W	9.8	43.7
137m. May 8' N of SW Cor.	9.68	43.88 43.95

13	9.9	43.6
CV	9.3	44.2
10	9.3	44.2
13	10.1	43.4
E	9.1	44.4

PLOTTED

CV

E	8.3	45.2
13	8.4	45.1
CV	8.6	44.9
13	8.8	44.7
W	8.9	44.6

NH Missouri Arc

W	8.1	45.4
13	7.9	45.6
CV	7.8	45.7
13	7.8	45.7



5351

E	7.4	46.1
50' N		
E	6.2	47.3
13	6.5	47.0
10	7.6	45.9
8	6.8	46.7
W	6.3	47.2
13	7.0	46.5
W	6.7	46.8
100' N		
W	5.8	47.7
13	5.7	47.8
W	5.5	48.0
11	6.3	47.2
13	5.4	48.1
E	5.0	48.5
150' N		
E	3.8	49.7
13	4.4	49.1
W	4.8	48.7
13	4.8	48.7
W	5.1	48.4
200' N		
W	4.0	49.5
13	3.7	49.8
W	3.7	49.8
13	3.5	50.0

5351

E	2.8	50.7		
270' N = Sh. Chalcedony				
E	1.4	52.1		
13	1.7	51.8		
W	2.3	51.2		
13	2.2	51.3		
W	2.6	50.9		
W				
W	1.6	51.9		
13	1.3	52.2		
W	1.4	52.1		
13	0.8	52.7		
E	0.5	52.0		
11.9	11.20	64.53	0.18	53.33
Nk. Chalcedony				
E	10.8	53.7		
13	11.2	53.3		
W	11.7	52.8		
13	11.5	53.0		
W	11.8	52.7		
50' N				
W	10.8	53.7		
13	10.2	54.3		
W	10.7	53.8		
13	10.4	54.1		
E	9.8	54.7		

PLOTTED



6453

100' N

E	89	55.6
13	9.2	55.3
cr	9.7	54.8
13	9.3	55.4
W	9.8	54.7

150' N

W	8.6	55.9
13	8.5	56.0
cr	8.7	55.8
13	7.8	56.7
E	8.0	56.5

200' N

E	6.9	57.6
13	7.2	57.3
cr	7.7	56.8
13	7.2	57.3
W	7.7	56.8

270' N = 3L Low

W	6.4	58.1
13	6.0	58.5
cr	6.1	58.6
13	6.0	58.5
E	5.5	59.0

6453

cr

E	4.8	59.7
13	5.3	59.7
cr	5.5	59.0
13	5.3	59.7
W	5.6	58.9

1L Low

W	5.0	59.0
13	4.7	59.8
cr	4.2	60.3
13	4.3	60.7
E	4.1	60.6

PLOTTED

50' N

E	3.5	61.0
13	3.7	60.8
cr	3.9	60.6
13	3.8	60.7
W	3.5	61.0

100' N

W	3.3	61.7
13	3.2	61.3
cr	3.3	61.7
13	2.9	61.6
E	2.7	61.8



6453

150' N

E	1.7	62.8
13	2.0	62.4
cr	2.3	62.2
13	2.1	62.6
W	2.2	62.3

200' N

W	0.7	63.8
13	1.9	63.6
cr	1.0	63.6
13	0.7	63.8
E	0.6	63.9

T.P. 1099 75.51 0.01 6452

270' N = Sh. Beryl

E	9.4	66.1
13	9.6	65.9
cr	10.0	65.5
13	9.6	65.9
W	9.7	65.8

cr

W	8.4	67.1
13	8.6	66.9
cr	8.8	66.7
13	8.5	67.0
E	8.3	67.2

75.51

Nh. Beryl

E	6.9	68.6
13	7.5	68.0
cr	7.8	67.7
13	7.6	67.9
W	7.5	68.0

50' N

W	6.5	69.0
13	6.4	69.1
cr	6.5	69.0
13	6.2	69.3

PLOTTED

E	6.0	69.5
---	-----	------

100' N

E	4.9	70.6
13	5.1	70.4
cr	5.4	70.1
13	5.1	70.4
W	5.1	70.4

150' N

W	4.1	71.4
13	4.1	71.4
cr	3.9	71.6
13	3.4	72.1
E	3.4	72.1



75.51  
500' N

F	2.0	73.5
13	2.3	73.2
C2	2.8	72.7
13	2.6	72.9
W	3.0	72.5

270' N = 5L Wilbur

W	1.1	74.4
13	0.7	74.8
C2	0.6	74.9
13	0.3	75.2
E	0.3	75.2

TP	9.89	85.34	0.06	75.45
----	------	-------	------	-------

CW

F	9.1	76.2
13	9.3	76.0
C2	9.4	75.9
13	9.8	75.5
W	10.2	75.1

NH Wilbur

W	9.1	76.2
13	8.6	76.7
C2	8.5	76.8
13	8.4	76.9
E	7.9	77.4

85.34  
50' N

F	6.9	78.5
13	7.1	78.2
C2	7.2	78.1
13	7.5	77.8
W	7.2	78.1

100' N

W	5.9	79.4
13	5.6	79.7
C2	5.9	79.4
13	6.0	79.2
E	5.0	80.2

TP	9.238	2.63	52.71
----	-------	------	-------

PLOTTED

125' N = 5 end of Curve

W	11.8	80.6
13	12.0	80.4
C2	12.1	80.3
13	12.0	80.4
E	11.3	81.1

50' N of end of Curve (on 2)

F	10.6	81.8
13	10.5	81.9
C2	10.7	81.7
13	10.3	82.1
W	10.9	81.5



9238  
100' N

W	8.9	87.5
13	9.2	87.7
CV	9.0	87.6
13	9.2	87.7
E	9.3	87.1

Sh Loring (on line)

F	6.9	85.6
13	6.9	85.5
CV	7.1	85.3
13	7.7	84.7
W	7.7	84.7

End of North Curve (Normal to Curve)

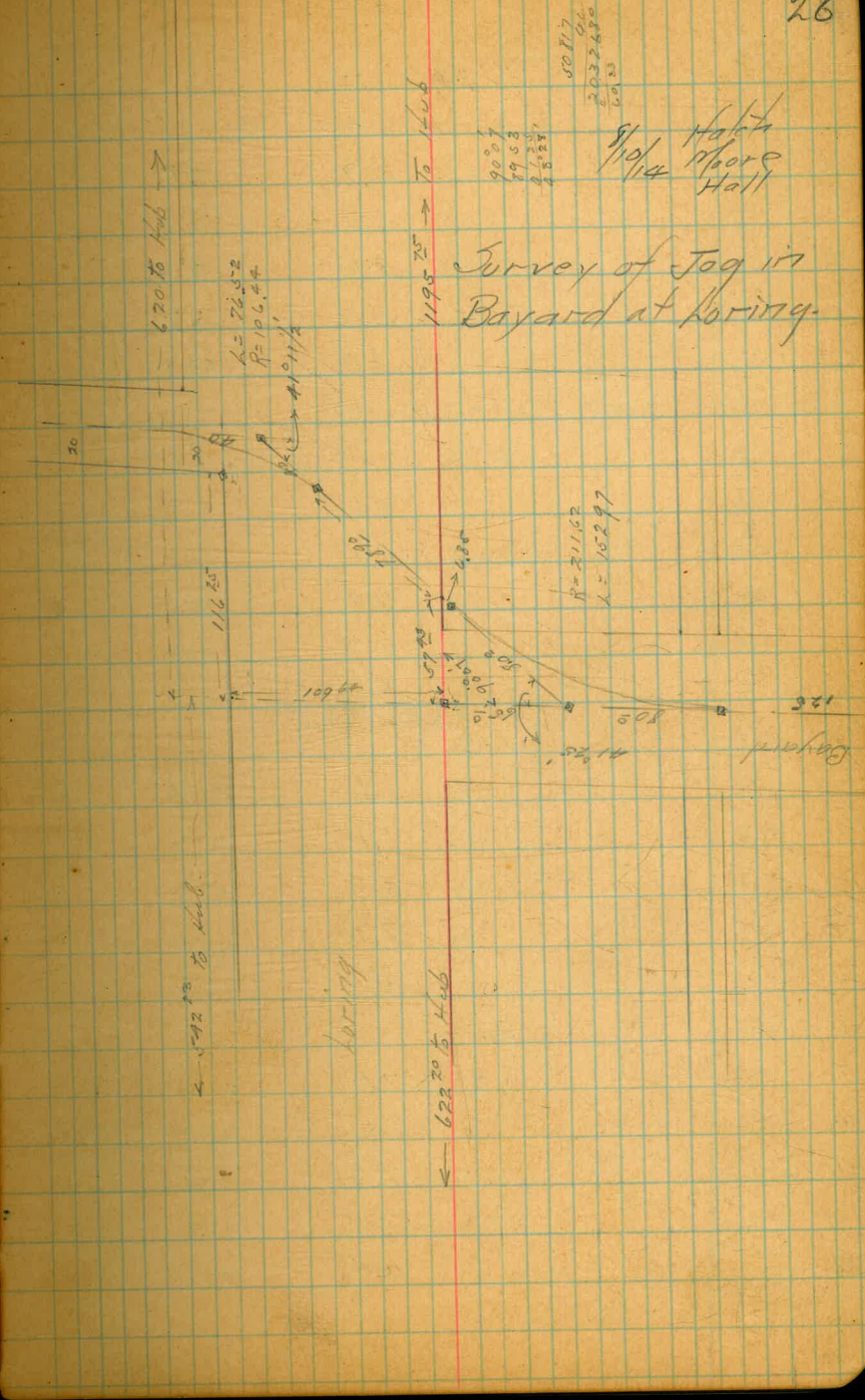
FV=20	4.7	87.7
10	5.2	87.7
CV	5.4	87.0
10	5.8	86.6
E=20	5.9	86.5

Cr. of Curve.

E	4.8	87.6
10	5.0	87.6
CV	5.0	87.6
10	4.5	87.9
W	4.0	88.4

Nh. Loring on West

W	3.7	88.7
---	-----	------





92.38

Nh. Loring on E = end of Curve.

W	3.7	88.7
10	3.7	88.7
cr	3.6	88.8
10	3.7	88.7
E	3.6	88.8

B.M. mark. 1147 100.29 3.56 88.82 8902

65' N of Loring on East

E	9.6	90.7
10	9.8	90.5
cr	9.9	90.6
10	9.7	90.6
W	10.2	90.1

115' N

W	8.8	91.5
10	8.7	91.6
cr	8.3	91.0
10	7.7	91.6
E	8.1	91.1

165' N

E	7.0	92.3
10	7.1	92.1
cr	7.2	92.1
10	7.5	92.8
W	7.5	92.8

100.29

215' N

W	7.0	92.7
10	7.3	92.0
cr	6.9	92.4
10	6.7	92.6
E	6.2	92.1

265' N = 3h. Hyacinth

E	5.7	94.6
10	5.9	94.4
cr	6.3	94.0
10	6.5	93.8
W	6.4	92.9

**PLOTTED**

W	5.6	94.7
10	5.2	95.1
cr	5.5	94.8
10	4.9	95.4
E	4.8	95.5

Nh. Hyacinth

E	4.4	95.9
10	4.4	95.9
cr	5.1	95.2
10	5.2	95.1
W	5.1	95.1



100.29  
65' N

W	3.7	96.6
10	3.5	96.8
cr	3.2	97.1
10	3.1	97.2
E	2.4	97.9

115' N

E	1.5	98.8
10	2.0	98.3
cr	2.2	98.1
10	2.5	97.8
W	2.7	97.6

165' N

W	2.5	97.8
10	2.4	97.9
cr	1.7	98.6
10	1.7	98.6
E	1.0	99.3
7.0	1.0	98.99

1275

111.74  
215' N

E	12.4	99.3
10	13.0	98.7
cr	12.8	98.9
10	13.2	98.4
W	13.3	98.4

111.74

265' NE Sh. Tourmaline

W	12.7	99.0
10	12.3	99.0
cr	12.2	99.1
10	12.3	99.0
E	11.8	99.9

cr

E	11.4	100.3
10	11.7	100.0
cr	11.9	99.8
10	12.2	99.4
W	12.2	99.4

PLOTTED

265' NE Tourmaline

W	11.9	99.8
10	11.5	100.2
cr	11.3	100.0
10	11.2	100.5
E	11.2	100.5

30' N

E	10.1	101.6
10	9.8	101.9
cr	10.1	101.6
10	10.4	101.3
W	10.3	101.4



111.74  
65' N

W	7.2	106.5
10	7.3	106.6
C1	7.5	106.7
10	7.7	106.0
E	6.7	106.0

115' N

E	4.3	107.6
10	5.0	106.7
C2	4.8	106.9
10	5.3	106.6
W	5.0	106.7

165' N

W	4.2	107.6
10	4.0	107.7
C2	3.9	107.8
10	3.8	107.9
E	3.5	108.7

215' N

E	1.9	109.8
10	2.1	109.6
C2	2.2	109.5
10	2.4	109.7
W	2.6	109.1

TP 12.59 122.81 1.52 110.22

122.81

265' N = Sh Sapphire

W	11.2	111.6
10	11.4	111.6
C2	11.1	111.7
10	11.1	111.7
E	10.5	112.7

CV

E	9.7	112.1
10	9.1	113.7
C2	9.4	112.4
10	9.7	113.1
W	9.6	113.7

PLOTTED Sapphire

W	7.9	114.9
10	7.9	114.9
C2	7.7	115.1
10	7.5	115.3
E	7.0	115.8

50' N

E	5.1	117.7
10	5.3	117.5
C2	5.2	117.6
10	5.4	117.4
W	5.6	117.7







9/29 Hatch  
Missouri  
Hall

Levels on Streets crossing Bayard St - from  
Missouri St to Tourgouis St.

B.M. Mon. Sw. Missouri - Bayard 7.71 51.66 43.95

Direction	Distance	Level	Height
Missouri St			
E. Line Allison (80' wide)			
N		11.1	40.6
Cr		11.5	40.2
S		12.4	39.3
50' E			
S		11.2	40.5
Cr		10.5	41.2
N		9.7	42.0
110' E			
N		9.0	42.7
Cr		10.1	41.6
S		10.9	40.8
150' E			
S		10.7	41.0
Cr		9.9	41.8
N		9.0	42.7
200' E			
N		8.8	42.9
Cr		9.4	42.3
S		10.5	41.2
250' E			
S		10.0	41.7
Cr		9.1	42.6
N		8.3	43.4

51.66  
500 E

Direction	Distance	Level	Height
N		8.0	43.7
Cr		8.8	42.9
S		9.7	44.0
350 E			
S		9.1	42.6
Cr		8.2	43.7
N		7.4	44.3
400 E			
N		7.1	44.6
Cr		7.7	44.0
S		8.5	43.2
450 E			
S		8.2	43.5
Cr		7.2	44.5
N		6.3	45.4
500 E Wk Bayard St			
N		6.2	45.5
Cr		7.0	44.7
S		7.9	43.8
E. Bayard St			
S		7.1	44.6
Cr		6.3	45.4
N		5.4	46.3



57.66

50'E

N	4.8	46.9
cr	5.5	46.2
S	6.7	45.0
100'E		
S	6.2	45.5
cr	5.0	46.7
N	4.2	47.5
150'E		
N	3.7	48.0
cr	4.9	46.8
S	5.6	46.1
200'E		
S	5.1	46.6
cr	4.1	47.6
N	3.0	48.7
250'E		
N	2.5	49.2
cr	3.4	48.3
S	4.4	47.3
300'E		
S	3.7	48.0
cr	2.5	49.2
N	2.0	49.7

57.66

350'E

N	1.5	50.2
cr	1.7	50.0
S	2.8	48.9
400'E		
S	2.0	49.7
cr	1.5	50.2
N	0.9	50.8
TP	866	59.49
450'E		
N	7.6	51.9
cr	8.3	51.2
S	9.2	50.3
500'E = W. Cass St.		
S	8.7	50.8
cr	7.4	52.1
N	6.8	52.7
TP	132	57.47
Chalchony St.		
W. Cass St.		
S	3.0	58.9
cr	1.8	60.1
N	1.8	61.1
50'W		
N	1.7	60.2
cr	2.6	59.3
S	3.7	58.2



6189

100 W

S	4.5	57.4
cr	3.5	57.4
N	2.7	59.2

150 W

N	3.4	58.5
cr	4.4	57.5
S	5.2	56.7

200 W

S	5.8	56.1
cr	4.8	57.1
N	4.0	57.9

250 W

N	4.7	57.2
cr	5.6	56.3
S	6.2	55.7

300 W

S	6.8	55.1
cr	6.0	55.9
N	5.2	56.9

350 W

N	6.1	55.8
cr	6.8	55.1
S	7.5	54.4

6189

400 W

S	8.3	53.6
cr	7.6	54.3
N	7.0	54.9

450 W

N	7.3	54.3
W	8.1	53.8
S	9.0	52.9

500 W = EL Bayard St

S	9.7	52.2
cr	8.8	53.1
N	8.1	53.8

W = Bayard St

N	9.1	52.8
cr	9.8	52.1
S	10.9	51.0

50 W

S	11.2	50.7
cr	10.3	51.6
N	9.5	52.4

100 W

N	9.5	52.4
cr	10.6	51.3
S	11.2	50.7



61.89

150' W

S	12.0	49.9
W	11.3	50.6
N	10.4	51.5

200' W

N	11.0	50.9
W	11.9	50.0
S	12.6	49.3

250' W

S	12.8	49.1
W	11.8	50.1
N	11.3	50.6

300' W

N	11.6	50.3
W	12.5	49.4
S	13.3	48.6

350' W

S	13.7	48.2
W	13.0	48.9
N	12.1	49.8

400' W

N	12.5	49.4
W	13.3	48.6
S	14.0	47.9

61.89

450' W

S	14.5	47.4
W	13.8	48.1
N	12.9	49.0

500' W = E.L. Allison

N	13.6	48.3
W	14.6	47.3
S	15.4	46.5

Low St

E.L. Allison

S	8.7	53.2
W	8.1	53.8
N	7.5	54.4

50' E

N	6.5	55.4
W	7.2	54.7
S	7.7	54.2

100' E

S	6.4	55.5
W	6.2	55.7
N	5.4	56.5

150' E

N	4.7	57.2
W	5.1	56.8
S	5.7	56.2



61.89

500' E

S	57.5	56.4
cr	4.4	57.5
N	3.7	58.2

250' E

N	2.6	59.3
cr	4.1	57.8
S	5.1	56.8

300' E

S	4.8	57.2
cr	3.6	58.3
N	1.8	60.1

350' E

N	2.1	59.8
cr	2.7	59.2
S	4.6	57.3

400' E

S	4.4	57.5
cr	3.3	58.6
N	2.6	59.3

450' E

N	2.5	59.4
cr	3.2	58.7
S	4.0	57.9

61.89

500' E = W. Bayard St.

S	3.5	58.4
cr	2.5	59.1
N	2.2	59.7

E. Bayard

N	1.3	60.6
cr	2.0	59.9
S	2.6	59.3

50' E

S	1.9	60.0
cr	1.3	60.6
7.70 12.81	7.3.65 1.25	60.84
N	12.5	61.2

100' E

N	11.8	61.9
cr	12.2	61.5
S	12.9	60.8

150' E

S	12.5	60.9
cr	11.8	61.9
N	11.2	62.5

200' E

N	10.8	62.9
cr	11.5	62.2
S	12.2	61.5



73.65  
250' E

S	11.7	62.0
Cr	10.9	62.8
N	10.1	63.6

300' E

N	9.3	64.4
Cr	10.2	63.5
S	10.7	63.0

350' E

S	10.0	63.7
Cr	9.4	64.3
N	8.8	64.9

400' E

N	7.9	66.3
Cr	8.7	65.0
S	9.2	64.5

450' E

S	8.5	65.2
Cr	7.7	66.0
N	7.2	66.5

500' E = Wk Cass St

N	6.2	67.5
Cr	6.8	66.9
S	7.5	66.2

73.65  
Beryl St  
Wk Cass St

S	2.1	71.6
Cr	1.5	72.2
N	0.8	72.9

50' W

N	1.1	72.6
Cr	1.5	71.9
S	2.8	70.9

100' W

S	3.4	70.3
Cr	2.4	71.3
N	1.9	71.8

150' W

N	2.3	71.4
Cr	2.7	71.0
S	4.3	69.4

200' W

S	4.7	69.0
Cr	3.4	70.3
W	2.6	71.1

250' W

N	3.2	70.5
Cr	4.1	69.6
S	5.2	68.5



73.65  
300' W

S	5.5	68.2
cr	4.4	69.3
N	3.6	70.1

350' W

N	3.9	69.8
cr	5.0	68.7
S	5.9	67.8

400' W

S	6.5	67.2
cr	5.4	68.3
N	4.3	69.4

450' W

N	4.8	68.9
cr	5.7	68.0
S	7.1	66.6

500' W = E of Bayard St

S	7.5	66.2
cr	6.3	67.4
N	4.8	68.9

W of Bayard St

N	5.6	68.1
cr	6.5	67.2
S	7.4	66.3

73.65  
50' W

S	7.9	65.8
cr	6.7	67.0
N	5.9	67.8

100' W

N	6.4	67.3
cr	7.2	66.5
S	8.0	65.7

150' W

S	8.0	65.7
cr	7.4	66.3
N	6.5	67.2

200' W

N	7.6	66.1
cr	8.3	65.4
S	9.4	64.3

250' W

S	10.3	63.4
cr	9.5	64.7
N	8.9	64.8

300' W

N	9.7	64.0
cr	10.4	63.3
S	11.1	62.6



73.65  
350 W

S	12.1	61.6
cr	11.4	62.3
N	10.3	63.4

400 W

N	12.0	61.7
cr	12.6	61.1
S	13.3	60.4

450 W

S	14.4	59.3
cr	13.5	60.2
N	12.9	60.8

500 W = E of Allison St

N	13.6	60.1
cr	14.0	59.7
S	14.9	58.8

Wilbur St

E of Allison St.

S	7.3	66.4
cr	6.3	67.4
N	5.8	67.9

50' E

N	5.5	68.2
cr	6.2	67.5
S	7.0	66.7

73.65  
100' E

S	7.3	66.4
cr	6.0	67.7
N	5.3	68.4

150' E

N	4.1	69.6
cr	4.8	68.9
S	5.8	67.9

200' E

S	5.2	68.5
cr	4.2	69.5
N	3.4	70.3

250' E

N	2.4	71.3
cr	3.2	70.4
S	3.6	70.1

300' E

S	2.5	71.2
cr	1.8	71.9
N	1.2	72.5

T.D	11.65	89.99	0.31	73.34
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350' E

N	11.2	73.8
cr	12.0	73.0
S	12.7	72.3



5499

400 E

S	12.0	73.0
cr	11.0	74.0
N	10.2	74.8

450 E

N	9.3	75.7
cr	10.3	74.7
S	11.1	73.9

500 E = Wk Bayard

S	10.5	74.5
cr	9.7	75.3
N	8.6	76.4

TP nail in the 8.51 91.33 2.17 72.82

Eh Bayard

N	13.8	77.5
cr	15.1	76.2
S	15.7	75.4

50 E

S	15.6	75.7
cr	14.6	76.7
N	13.8	77.5

100 E

N	13.1	78.2
cr	14.2	77.1
S	15.1	76.2

91.33

150 E

S	15.1	76.2
cr	13.6	77.7
N	12.6	78.7

200 E

N	11.8	79.5
cr	13.0	78.3
S	14.1	77.2

250 E

S	13.6	77.7
cr	12.4	78.9
N	11.4	79.9

300 E

N	11.2	80.1
cr	12.2	79.1
S	13.3	78.0

350 E

S	13.1	78.2
cr	11.8	79.5
N	10.5	80.8

400 E

N	10.3	81.0
cr	11.4	79.9
S	12.5	78.8



9133  
250 E

S	11.5	79.8
cr	10.5	80.8
N	9.5	81.8

500 E = W. Cass St.

N	8.9	82.4
cr	9.7	81.6
S	10.6	80.7

Loring St

W. Cass St.

S	2.1	89.2		
cr	0.5	90.8		
TP	8.53	93.90	0.96	90.37
N	1.5	92.4		

50 W

N	2.5	91.4
cr	4.0	89.9
S	5.6	88.3

100 W

S	6.2	87.5
cr	4.6	89.3
N	3.0	90.9

150 W

N	2.4	91.5
cr	5.5	88.4
S	7.0	86.9

9390

250 W

S	7.4	86.5
cr	5.7	88.2
N	3.5	90.4

250 W

N	3.8	90.1
cr	5.6	88.3
S	7.3	86.6

300 W

S	7.3	86.6
cr	5.4	88.5
N	3.7	90.2

350 W

N	5.1	88.8
cr	5.8	88.1
S	6.5	87.4

381<sup>5</sup> W = E. Bayard St on North

S	7.7	86.2
cr	6.5	87.4
N	5.00	88.90

137 M. Men.

121<sup>5</sup> W = W. Bayard St on North

N	5.1	88.8
cr	7.2	86.7
S	8.3	85.6



9390

450 W

S	8.3	85.6
cr	7.8	86.6
N	5.3	88.6

500 W = EL Bayard on South

N	6.8	87.1
cr	7.5	86.4
S	9.3	84.6

1 cr Bayard on South

S	9.1	84.8
cr	8.8	85.1
N	8.1	85.8

Wh Bayard on South

N	9.1	84.8
cr	10.1	83.8
S	10.1	83.8

50 W

S	11.6	82.3
cr	11.3	84.6
N	10.4	83.5

100 W

N	11.0	82.9
cr	12.4	81.5
S	13.0	80.9

TR	302	8424	12.68	81.22
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8424

150 W

S	4.5	79.7
cr	3.7	80.5
N	2.5	81.7

200 W

N	3.2	81.0
cr	4.8	79.4
S	5.6	78.6

250 W

S	6.6	77.6
cr	5.5	78.7
N	4.0	80.2

300 W

N	4.8	79.4
cr	6.5	77.7
S	6.9	77.3

350 W

S	8.9	75.3
cr	7.7	76.5
N	5.5	78.7

400 W

N	6.8	77.4
cr	8.8	75.4
S	10.1	74.1

41



8424  
450 W

S	11.1	73.1
W	9.8	74.4
N	8.1	76.1

500 W = EH Allison St

N	9.1	75.1
W	10.8	73.2
S	11.5	72.7

9.26 9345 0.05 8419

Hyacinth St (70' wide)

EH Allison St.

S	12.6	80.9
W	11.6	81.9
N	11.4	82.1

58° E = 600 W of Bayard.

N	10.4	83.1
W	10.4	83.1
S	11.6	81.9

500 W

S	10.3	83.2
W	9.4	84.1
N	9.2	84.3

500 W

N	7.8	85.7
W	8.1	85.4
S	9.2	84.3

9345  
450 W

S	8.9	84.6
W	7.7	85.8
N	7.7	85.8

400 W

N	6.7	86.8
W	6.9	86.6
S	8.2	85.3

350 W

S	7.2	86.3
W	5.8	87.7
N	5.8	87.7

300 W

N	4.9	88.6
W	5.1	88.4
S	6.4	87.1

250 W

S	5.0	88.5
W	3.8	89.7
N	3.6	89.9

200 W

N	2.6	90.9
W	2.8	90.7
S	2.8	90.7



9345

150' W

S		2.8	90.7
cr		1.1	92.4
N		1.1	92.0
T.P	11.61	104.73	0.33
		93.12	

100' W

N		11.4	93.3
cr		11.6	93.1
S		12.8	91.9

50' W

S		11.9	92.8
cr		10.5	94.2
N		10.5	94.2

W W Bayard St

N		9.5	95.2
cr		9.9	94.8
S		10.6	94.1

E L Bayard St

S		10.5	94.6
cr		9.1	95.6
N		8.7	96.0

(about) 33' E = 350' W of Cass St.

N		7.9	96.8
cr		8.2	96.5
S		9.2	95.5

10473

300' W

S		7.9	96.8
cr		6.6	98.1
N		6.4	98.3

250' W

N		5.4	99.3
cr		5.3	99.4
S		7.2	97.5

500' W

S		6.9	97.8
cr		5.0	99.7
N		4.2	100.5

150' W

N		3.6	101.1
cr		4.4	100.3
S		5.6	99.1

100' W

S		5.3	99.4
cr		3.7	101.0
N		2.2	102.5

50' W

N		2.5	102.2
cr		3.1	101.6
S		4.7	100.0



10273

W. Cass St.

S		4.2	100.5
cr		2.6	102.1
N		2.1	102.6
TP	10.10	113.94	0.89
			103.84

Tourmaline St

W. Cass St

S		3.8	110.1
cr		2.6	111.3
N		1.9	112.0

50' W

N		3.0	110.9
cr		3.6	110.3
S		4.6	109.3

100' W

S		5.5	108.4
cr		4.9	109.0
N		4.5	109.4

150' W

N		7.6	106.3
cr		6.8	107.1
S		7.0	106.9

200' W

S		1.7	105.2
cr		2.9	105.0
N		9.7	104.2

11394

250' W

N		10.8	103.1
cr		10.0	103.9
S		10.3	103.6

300' W

S		10.7	103.2
cr		11.1	102.8
N		11.6	102.3

350' W

N		12.8	101.1
cr		12.9	101.0
S		13.2	100.7

TP 337

104.41

12.90

101.14

(about) 382' W = E. Bayard St

S		4.4	100.0
cr		4.0	100.4
N		3.9	100.5

W. Bayard St.

N		4.5	99.9
cr		4.9	99.5
S		5.3	99.1

50' W

S		6.8	97.6
cr		6.6	97.8
N		5.1	99.3



10441

100 W

N	7.0	97.4
or	8.1	96.3
S	8.5	95.9

150 W

S	9.9	94.5
or	8.7	95.7
N	7.4	97.0

200 W

N	7.6	96.8
or	9.2	95.2
S	10.5	93.9

250 W

S	10.9	93.5
or	10.1	94.3
N	9.4	95.0

300 W

N	9.8	94.6
or	10.5	93.9
S	11.1	93.3

350 W

S	11.7	92.7
or	10.8	93.6
N	10.0	94.4

10441

400 W

N	10.2	94.2
or	11.3	93.1
S	12.4	92.0

450 W

S	12.7	91.7
or	11.8	92.6
N	11.1	93.3

500 W

N	11.3	93.1
or	12.3	92.1
S	13.2	91.2

T.P. 0.55

93.07 11.89

92.52

550 W

S	2.3	90.8
or	1.5	91.6
N	0.3	92.8

600 W

N	1.3	91.8
or	2.2	90.9
S	3.0	90.1

625 W

S	3.6	89.5
or	3.3	89.8
N	3.2	89.9



93.17  
658<sup>5</sup>W

N		7.4	85.7
cr		8.3	84.8
S		4.1	89.0

675 W1

S		5.2	87.9
cr		8.9	84.2
N		7.4	85.7

700<sup>2</sup>W = Elk Allison St

N	Sub.		6.20	86.87
cr			9.2	83.9
S			8.2	84.9
TPO	1291	99.78	620	86.87
TPO	1208	111.50	036	99.12

Sapphire St

Elk Allison = 700<sup>2</sup>W of Bayard

S		12.4	99.1
cr		11.1	100.4
N		9.9	101.6

650W

N		9.7	101.8
cr		10.9	100.6
S		12.1	99.4

600 W1

S		11.1	100.4
cr		10.2	101.3
N		9.2	102.3

111.50

550W

N		7.3	103.2
cr		8.8	102.7
S		10.0	101.5

500 W

S		9.5	102.0
cr		7.8	103.7
N		6.5	104.0

450 W

N		6.1	105.4
cr		7.7	103.8
S		8.8	102.7

400 W

S		8.1	103.4
cr		6.8	104.7
N		5.3	106.2

350 W

N		4.7	106.8
cr		6.1	105.4
S		7.5	104.0

300 W

S		7.6	103.9
cr		6.7	104.8
N		4.6	106.9



111.50

250' W

N	3.8	107.7
Cr	5.7	105.8
S	7.6	103.9

200' W

S	5.7	105.8
Cr	3.2	108.3
N	2.2	109.3

150' W

N	0.1	111.4
Cr	1.6	109.9
S	3.7	107.8

100' W

S	2.3	109.2
TP	11.46	121.44
Cr	1.52	109.98
Cr	10.4	111.0
N	8.2	113.2

50' W

N	6.9	114.3
Cr	8.9	112.5
S	10.5	110.9

W/L Bayard

S	9.8	111.6
Cr	8.3	113.1
N	6.4	115.0

121.44

Fk Bayard

N	5.8	115.6
Cr	7.3	114.1
S	7.0	112.4

(about) 30'E - 350' W of Cass

S	7.9	113.5
Cr	6.4	115.0
N	4.9	116.5

300' W

N	4.1	117.3
Cr	5.4	116.0
S	7.0	114.4

250' W

S	6.4	115.0
Cr	5.0	116.4
N	4.0	117.4

200' W

N	2.7	118.7
Cr	3.6	117.8
S	5.0	116.4

150' W

S	3.6	117.8
Cr	2.3	119.1
N	1.7	119.7

TP	10.91	130.82	15.3	119.91
----	-------	--------	------	--------



130.82

100 W

N	9.6	121.2
cr	10.9	119.8
S	12.3	117.5

50 W

S	11.6	119.2
cr	9.6	121.2
N	8.1	122.7

Wh Pass

N	6.9	123.9
cr	8.3	121.5
S	10.4	120.4

TP	11.12	140.65	1.29	129.53
----	-------	--------	------	--------

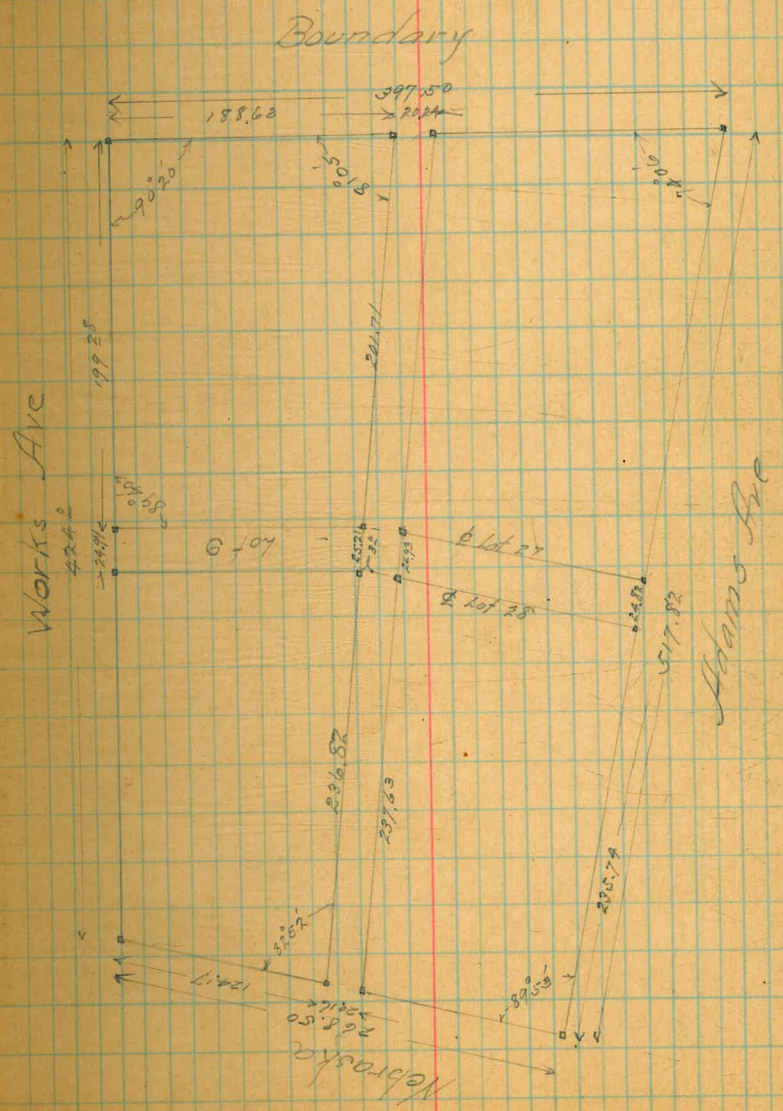
Herb Pass - Tanguais	4.19	136.46	136.39
----------------------	------	--------	--------



10/13/12  
12/10/12  
Hatch  
Moore  
Hall

Survey for opening Alley  
Through South 1/2 of Blk J  
University Heights Subd. Ph 1113

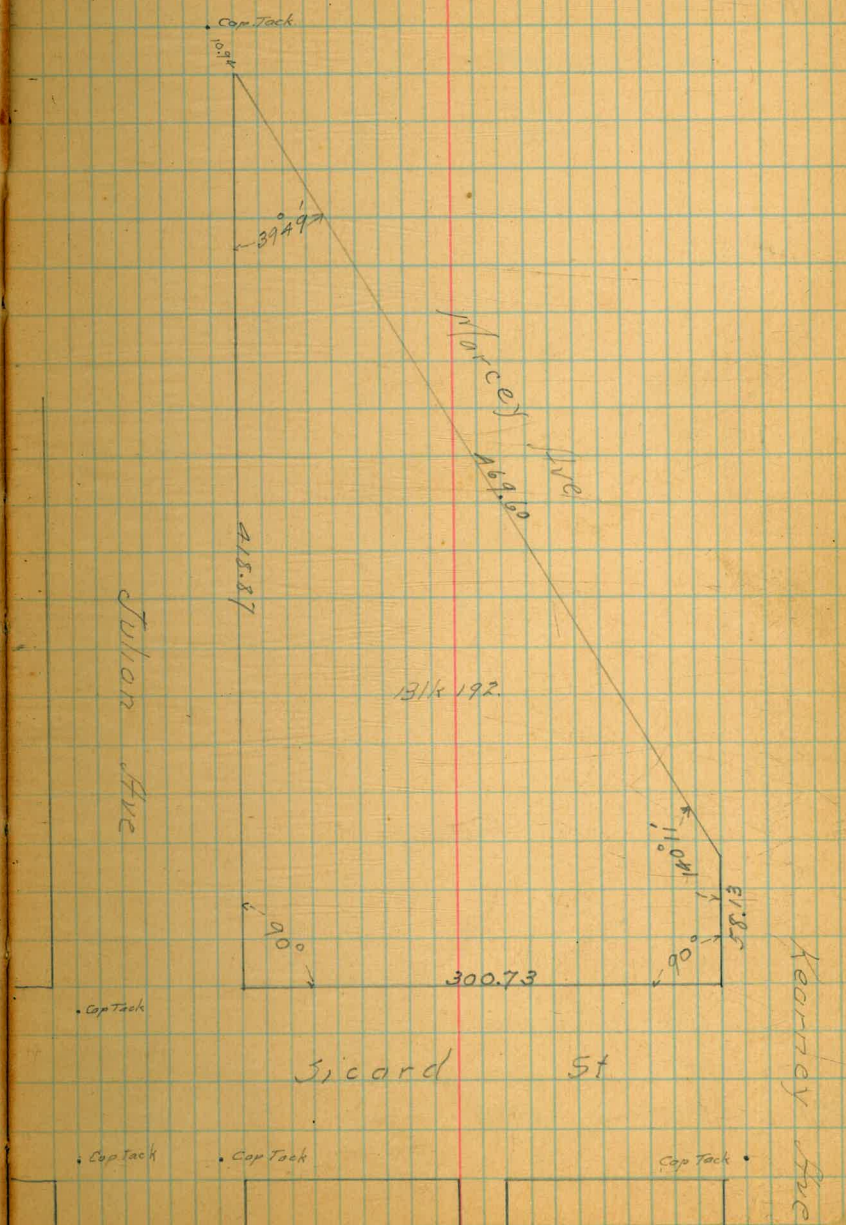
49





10/25/10 Hatch  
Map  
Hatch

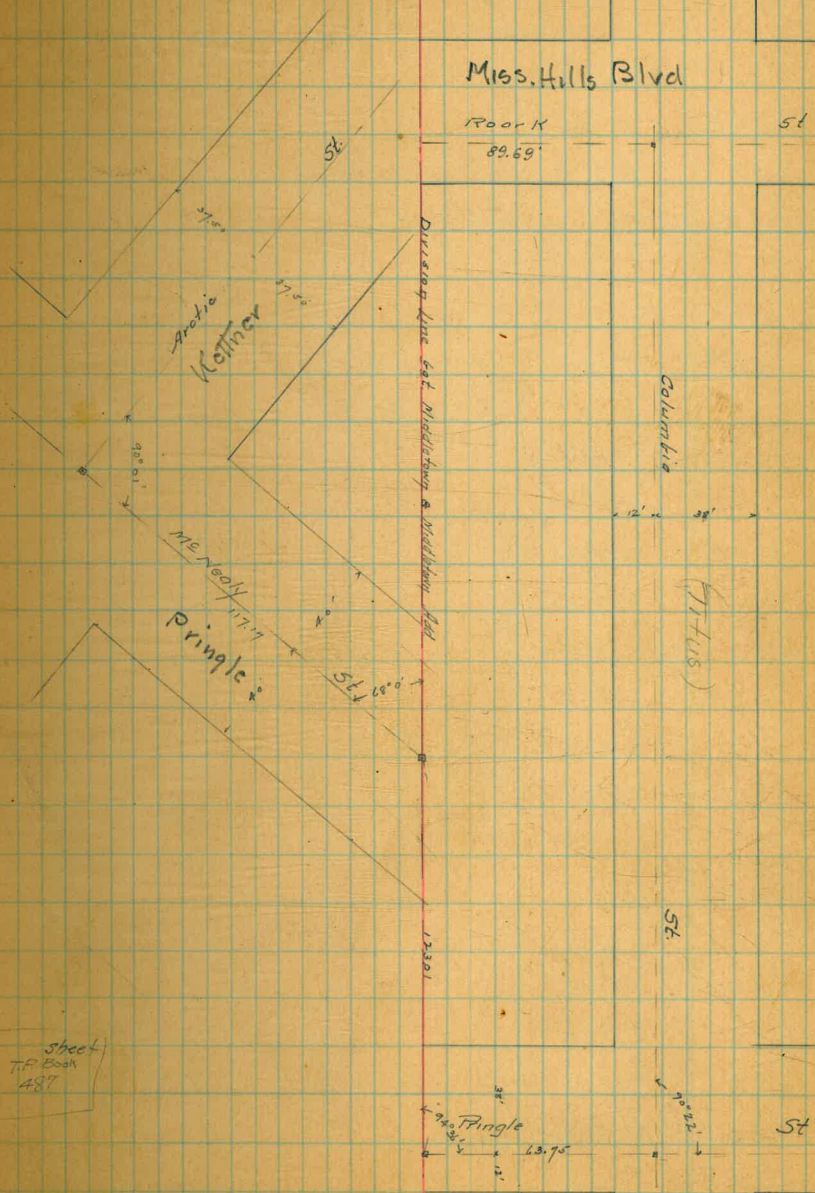
Survey of Blk 192 for Board of Education  
2" x 2" Redwood hubs set at Block Corners.





Survey to show connection of McNeely St in Middletown  
with Pringle St in Middletown Add.

17 Davis  
17 Johnson  
100 Johnson  
100 Johnson



Sheet  
T.R. Book  
487

Pringle  
13.95'

13.90'



Location of Railroad Connection with  
Municipal Pier, from Proposed Municipal track  
on Atlantic St.

Spur "A"

+17 54' = End Track on Pier

+81 EC	6° 30'	} T = 38.44 Δ = 13° 00' R. L = 76.47
+50	3° 52'	
9 + 04 53 B.C. 17° L		

9

+50

8 +38 24 EC.	7° 30'	} T = 44.41 Δ = 15° 00' L L = 88.24
8	4° 15'	
7 + 50 P.R.C. 17° L	55° 15'	

7

+50 46° 45'

6 + 00 42° 30'

5 + 55 = "B" 0 + 00 38° 40' 30"

+50 38° 15'

5	34° 00'	} T = 486.28 Δ = 110° 30' R. L = 650.00
+50	29° 45'	
4	25° 30'	

4

+50 21° 15'

3 17° 00'

+50 12° 45'

2 8° 30'

+50 4° 15'

1 + 00 P.C.C. 17° R 24'		} T = 50.08 Δ = 7° 30'
+50	1° 22' 30"	

40 + 00 B.C. 7° 30' R } L = 100.00



Spurs to Municipal Pier  
(cont. from p 52)

53

SPUR "D"

+51.71 - End Track on Pier

1+48.07 EC 4°24' } T=30.64  
1+00 0°56' } Δ=8°48' R  
0+86.96 BC 14°34' R } L=61.11

+61.11 PF, EC, 4°24' } T=30.64  
#6 1/2 } Δ=8°48' L  
+50 3°36' } L=61.11  
="D" 0+00 BC 14°24' L  
B2+66.77

+17.74 - End Track on Pier

SPUR "B"

4  
+50  
3  
+50  
2+ 01.30 EC, 2°35' }  
2 2°34' } Δ=5°10' R  
+50 1°55'30" }  
1 1°17' }  
+50 0°38'30" }  
="B" 0+00 BC 2°34' R  
A5+55



Spurs to Municipal Pier  
(cont.)

54

SPUR "C"

1+47.25 End Track on Pier

+90.28 E.C. 6°30'

+50 3°36'

"C" 0+00 B.C. 14°24' L

"A" 8+38.24

T = 45.30,

Δ = 13°00' L

L = 90.28



# Abandoned

Levels over proposed R.R. line from Q of Atlantic St to Municipal Pier

Sta	+	41	-	Elev
	2.03	12.53		
T.P.	6.41	9.75	9.19	3.24
A <sup>o</sup> 0+00 - P.C.			6.4	3.4
+50			6.4	3.4
1+00 - P.C.			6.2	3.6
+50			6.0	3.8
2			5.7	4.1
+50			5.6	4.2
3			5.5	4.3
+50			5.5	4.3
4			4.5	5.2
+50			4.2	5.5
5			4.2	5.6
+50			2.8	6.0
+55 - 0+00 'B' Spur			3.7	6.1
T.P.	5.88	11.86	4.27	5.48
6+00			5.1	6.3
+50			4.9	6.5
7			4.4	7.0
+50			4.6	6.8
8			5.1	6.3
+38 <sup>24</sup> E.C. - 0+00 'C' Spur			6.1	5.3
+50			6.3	5.1
9+04 <sup>53</sup> P.C.			6.3	5.1
+50			6.5	4.9
+91 - E.C.			7.0	4.4
+87 <sup>54</sup> End Track Top rail			6.95	4.41

B.M.S.E. Point  
& Bench Pk. 11  
510.50

M  
11.36  
Spur 'B'

0+00	5.3	6.1
+50	5.0	6.4
1	5.0	6.4
+50	5.2	6.2
2+01 <sup>30</sup> - E.C.	5.5	5.9
+50	6.2	5.2
3	6.8	4.6
+50	7.4	4.0
4	6.3	5.1
+17 <sup>24</sup> End Track Top rail	6.93	4.43
Spur 'C'		
0+00 - P.C.	6.1	5.3
+50	6.4	5.0
+96 <sup>24</sup> E.C.	6.6	4.8
+147 <sup>25</sup>	6.95	4.41
Spur 'D'		
0+00 - P.C.	6.4	5.0
+50	7.1	4.3
+61.11 E.C.	7.2	4.2
+86 <sup>21</sup> P.C.	7.6	3.8
1+00	7.6	3.8
+51.21 - End Track Top rail	6.95	4.41



Location of Railroad Connection with Municipal  
Pier from St. Fe Spur on Atlantic St

56

Spur 'A'

5  
13  
15 } Davis  
Hansell  
Herrick

11 14° 57' 30" } 17° Curve  
+50 10° 42' 30" } Δ 52° 35' 30"  
10 6° 27' 30" } T 166.69  
+50 2° 12' 30" } L 309.36  
+24° 22' P.C. P 52° 35' 30"

9

+50

8

+50

12814 = B + 00

7

+50

6

+50

5

+50

4

+50

3

+50

+3385 PT 0° 43'

2 0° 32' 50" } 1° Curve  
+50 0° 17' 50" } T 71.68  
1+00 0° 2' 50" } Δ 1° 26'  
L 143.33

+90.55 P.C. 1° 26' R

+50

"A" 0+00 = P.C. 12° 26' C. Δ 36° 02'



Spur "B"

+41<sup>25</sup> = End Present Track on Pier  
 +37<sup>25</sup> EC 5° 58' 1/2' } 17° Curve  
 4            2° 45' 45" } Δ 110.57'  
                                   } T 35.21  
 +67<sup>25</sup> = PC R 11° 57' } L 70.30  
 +50

3  
 +82 = EC 20° 18' 15" }  
 +50    18° 0' }  
 2            14° 24' } 14° 24' Curve  
                                   } T = 147.31  
 +50    10° 48' } Δ 40° 36' 1/2'  
 1            7° 12' } L 282.0  
 +50    3° 36' }

A7+28<sup>25</sup> = BOT 40° 36' 30" R

+36<sup>25</sup> = End Present Track on Pier

+33<sup>25</sup> PT. 26° 17' 45"  
 17            23° 27' 30"  
 11 + 50    19° 12' 30"

Levels over Spur "B"

	6.60	11.02	Prod	1+23 Top Rail 5 <sup>th</sup> Track
4+41 <sup>25</sup> Top rail			6.60	4.46
+37 <sup>25</sup> EC			6.6	4.4
4			6.3	4.7
3+67 <sup>25</sup> PC			6.3	4.7
+50			6.2	4.8
3			6.2	4.8
+82			5.8	5.2
+50			6.6	4.4
2			4.9	6.1
+50			5.0	6.0
1			4.9	6.1
+50			4.8	6.2
0+00 = A7+28 <sup>25</sup>			4.8	6.2

Spur A

12+36 <sup>25</sup> = End Track on Pier Top rail	6.60	4.43
+33 <sup>25</sup> EC	6.8	4.2
12	6.7	4.3
+50	6.8	4.2
11	6.0	5.0
+50	4.9	6.1
10	7.5	5.0 6.5
+50	7.9	6.1
+24 <sup>25</sup> PC	4.7	6.3
9	4.8	6.2
+50	4.9	6.1

7.3  
 3.2  
 3.3  
 0.1  
 6.33  
 1.68



## Levels over Spur A"

	11.03			Elev
8+00			4.9	6.1
+50			4.6	6.4
+28 <sup>14</sup> P.C. B' 0+00			4.8	6.2
T.P	4.12	M1 P. 45	4.70	6.33
7			5.8	4.7
+100			7.0	4.5
6			4.6	3.9
+50			4.9	3.6
5			5.1	3.4
+50			5.1	3.4
4			5.1	3.4
+50			5.5	3.0
3			5.7	2.8
T.P	3.13	M1 6.64	5.64	2.81
+50			4.3	2.3
+33 <sup>14</sup> E.C.			4.4	2.2
2			4.5	2.1
+50			4.3	2.3
+50			2.8	3.8
1			3.1	3.5
+90 <sup>55</sup> P.C.			3.4	3.2
+50			4.2	2.4
0+00 - P.C. 12" x 6" Curve on St Fe Spur			3.7	3.1
Top rail			3.65	2.99



Levels over pouring in Park Blvd & Univ Area on New  
Curb lines for 25' Closing on Univ Blvd.

Davis  
Hancock  
Hewitt

59

	+	M.	-
	3.39	31924	315.85 dm
New Ct line W.L. Park Blvd		4.69	314.55
High pt. in paving on return.		3.99	315.25
New Ct line P. Blvd S.L. Univ.		4.23	315.01



Grades for cut off.

	335.59	345.96	357.51	366.47	373.77	370.92
10.37	10.37	10.37	10.37	10.37	10.37	10.37
352.08	345.96	357.51	366.47	373.77	370.92	
175	175	175	175	175	175	
353.83	345.29	357.51	366.47	373.77	370.92	
127.61	127.61	127.61	127.61	127.61	127.61	
341.06	345.29	357.51	366.47	373.77	370.92	
175	175	175	175	175	175	
345.91	345.29	357.51	366.47	373.77	370.92	
10.37	10.37	10.37	10.37	10.37	10.37	
335.54	345.29	357.51	366.47	373.77	370.92	
175	175	175	175	175	175	
357.51	345.29	357.51	366.47	373.77	370.92	
148	148	148	148	148	148	
356.03	345.29	357.51	366.47	373.77	370.92	
115	115	115	115	115	115	
367.18	345.29	357.51	366.47	373.77	370.92	
0.71	0.71	0.71	0.71	0.71	0.71	
366.47	345.29	357.51	366.47	373.77	370.92	
7.31	7.31	7.31	7.31	7.31	7.31	
373.77	345.29	357.51	366.47	373.77	370.92	
2.95	2.95	2.95	2.95	2.95	2.95	
370.92	345.29	357.51	366.47	373.77	370.92	
61.22	61.22	61.22	61.22	61.22	61.22	
5.85	5.85	5.85	5.85	5.85	5.85	
4.25	4.25	4.25	4.25	4.25	4.25	
64.86	64.86	64.86	64.86	64.86	64.86	
5.34	5.34	5.34	5.34	5.34	5.34	
40.2	40.2	40.2	40.2	40.2	40.2	
66.10	66.10	66.10	66.10	66.10	66.10	
7.67	7.67	7.67	7.67	7.67	7.67	
42.67	42.67	42.67	42.67	42.67	42.67	

Sta	L	C	R
0+00	335.30	35.8	36.3
+25	36.90		37.81 37.90
+50	38.51		39.23 39.51
+75	40.11		40.64 41.11
+100	41.72		42.06 42.71
+125	43.34		43.30 44.21
+150	44.93		44.38 45.63
+175	46.50		46.49 47.05
+200	48.05	49.00	48.50
+225	49.59	50.25	50.65
+250	51.20		52.16
+275	52.78		53.67
+300	54.41		55.18
+325	56.02		56.69
+350	57.60		58.20
+375	59.16		59.71
+400	60.70	61.50	61.23
+425	62.23		62.74
+450	63.78		64.25
+475	65.34		65.76
+500	66.84		67.27
+525	68.37		68.78
+550	69.91		70.29
+575	71.46		71.80
+600	73.02		73.31
+625	74.57		74.82
+650	76.13		76.33
+675	77.68		77.84
+700	79.24		79.35
+725	80.79		80.86
+750	82.34		82.37
+775	83.89		83.88
+800	85.44		85.39
+825	86.99		86.90
+850	88.54		88.41
+875	90.09		90.00
+900	91.64		91.51
+925	93.19		93.02
+950	94.74		94.53
+975	96.29		96.04
+1000	97.84		97.55







L      £      R

84 +08.72 EC	<u>70.10</u> ✓	<u>70.60</u>	<u>71.10</u> ✓
+25			
+50			
+78.93 PC	<u>71.80</u> x	<u>72.30</u>	<u>72.80</u> ✓
85	<u>72.52</u> ✓		<u>73.52</u> ✓
+25			
+50	<u>73.38</u> x		<u>74.38</u> ✓
+75	<u>74.24</u> x		<u>75.24</u> ✓
86	<u>75.09</u> x		<u>76.09</u> ✓
+25	<u>75.95</u> x		<u>76.95</u> ✓
	<u>76.81</u> x		<u>77.81</u> ✓
+44.85 EC	<u>77.50</u> x	<u>78.00</u>	<u>78.50</u> ✓
+50			
+75			
+82.25 End Curt W. Side PC E Side	<u>80.01</u> ✓		<u>79.67</u> ✓
+94.85			
87	<u>81.87</u> ✓	<u>81.87</u>	<u>81.87</u> ✓
+25			
+50			
+75			
88	<u>84.96</u> x	<u>84.96</u>	<u>84.96</u> ✓
+25			
+33.97			
+50			
+75			
+83.97 PC	<u>86.97</u> ✓	<u>86.80</u>	<u>86.63</u> ✓
89	<u>88.18</u> ✓		<u>87.84</u> ✓
+25	<u>90.07</u> ✓		<u>89.73</u> ✓
+50	<u>91.96</u> ✓		<u>91.62</u> x

77.31 x

62

72.80 TP	71.80	73.52	74.38	75.24	76.09	76.95	77.81	78.50
9.25	5.51	8.34	7.48	6.62	5.77	4.91	4.05	3.20
77.86 M1	80.01	78.67	81.87	84.96	86.97	86.63		
77.00	9.52	9.86	7.66	4.57	2.56	2.96		
89.53 M1	81.87	87.84	89.73	90.07	91.96	91.62	79.63	
89.81	10.87	11.20	9.20	9.00	7.11	7.41	8.47	
88.62 TP	72.63	73.12	72.81	74.71	75.57	76.42	75.92	
91.45	4.68	4.18	3.46	2.60	1.74	0.89	1.39	
99.07 M1	77.31 M1	75.07	74.21	73.35	74.78	76.64	78.33	77.28
	5.51	2.40	3.10	3.96	0.53	8.99	8.00	9.36
								8.49
76.73 TP	78.82	80.34	80.50	82.00	82.70	85.79	85.29	
99.0	7.80	6.29	6.13	4.43	3.93	0.84	1.34	
86.63 M1	87.00	88.51	90.40	92.29	94.16	88.67	90.56	92.45
0.24	11.07	9.87	7.92	6.08	10.86	9.65	7.76	5.87
85.69 TP	72.63	72.25	74.21	75.07	75.91	76.78	77.64	
12.63	5.07	4.35	3.49	2.63	1.79	0.92	0.26	
72.82 M1	77.70 M1	78.32	85.79	82.70	85.29	87.20	87.46	
	0.66	9.67	2.16	5.27	2.66	0.65	0.29	
72.64 TP	10.31	88.51	90.56	92.45				
		11.35	9.20	7.01				
87.95 M1	57.30 TP							
	12.56							
92.86 M1								



L      £      R

89+50			
+75	93.84		93.50
90			
+03.35 EC	95.97	95.80	95.63 TP
+75			
+50			
+75			
91			
+75			
+50			
+68.68 <sup>beginning of</sup> 8" Ch <sub>a</sub> outside	107.41	107.24	107.07
+75			
92			
+18.68 PC	111.20	110.70	110.20
+75	112.72 ✓		111.55 ✓
+50			
+75	114.24 ✓		112.90 ✓
+84.13 center	115.25 ✓	115.15	114.25
93			
+75	117.20 ✓		115.87 ✓
+49.58 EC	118.65 ✓		117.49 ✓
+75	120.10	119.60	119.10 ✓
+99.58 end of 8" Ch <sub>a</sub> outside			
94			
+22.67 PC	125.67 ✓	125.50	125.33 ✓
+50	127.51 ✓		127.17 ✓
+75	129.17 ✓	129.00	128.83 ✓
95			

115.86 PT Hut. Ketch's

63

11.07.81	93.50	93.84	95.97	95.63
115.86 cur	120.10	19.10	17.29	19.65
122.75 HT	2.65	3.65	5.26	4.18
1138	14.25	14.72	14.90	11.05
115.86	8.50	8.57	9.85	11.20
12.96	107.41	107.07	105.33	107.72
122.82 HT	9.83	10.17	3.49	3.75
128.52 TIP	38.83	29.17	24.17	24.23
128.52 HT	9.41	9.07	4.15	3.97
128.52 HT	96.46	96.30	108.41	107.90
128.52 TIP	6.82	6.98	8.08	8.59
128.52 HT	15.86	12.72	14.26	16.75
128.52 HT	5.25	5.39	1.87	4.26
128.52 HT	21.11	18.32	16.70	15.08
128.52 HT	19.93	18.32	16.70	15.08
128.52 HT	2.18	2.79	4.41	6.03
128.52 HT	2.11	2.60	2.66	2.16
128.52 HT	7.60	2.60	2.94	2.40
128.52 HT	29.50	29.65	29.33	29.46
128.52 HT	7.67	7.51	5.53	3.40
128.52 HT	12.38	12.20	10.53	11.03
128.52 HT	2.80	2.82	3.94	3.73
128.52 HT	3.26	8.41	1.20	13.72
128.52 HT	15.86	10.81	7.02	5.58
128.52 HT	18.22	18.22	18.22	18.22
128.52 HT	1.02			
137.17 HT				
99.16 HT				







L      ±      R

84	100+25			
	+50			
	+56.72	153.34	153.17	153.00
	+75			
8	101			
	+25			
	+50			
	+75			
8	102			
	+25			
	+50			
	+75			
	+99.95	168.30	168.13	167.96
	103+25			
8	+49.95 PC	171.70✓	171.20	170.70✓
	+75	PC centerline 172.34✓		171.37✓
		174.05✓		172.89✓
	104			
	X+27.18 center	177.45✓	176.70	175.95✓
	+50	179.00✓		177.62✓
	+75	180.56✓		179.30✓
	105.	E.C. centerline 182.12✓		180.97✓
	+04.41 EC	182.70✓	182.20	181.70✓
	+25			
	+50			
8	+54.41	185.87✓	185.70	185.53✓
	+75			
	106.	189.07✓	188.90	188.73✓

X 174.05 BM PI Curve Hal.

65

151.41 TP	53.04	153.00	68.30	67.96
33	1.45	1.79	8.77	9.08
154.79 M				
174.05	174.70	170.70	122.34	71.77
299	11.31	2.81	10.67	11.64
177.0	75.71	72.20	75.95	74.45
174.05	72.6	8.69	7.06	4.84
179.6	79.30	80.50	82.2	80.97
182.0	3.71	2.43	0.89	2.04
171.70	85.87	85.87	85.83	88.73
1286	8.69	9.69	10.03	6.83
1845.6 M	53.83	53.67		5.49
8270	2.2	2.36		
12 PC				
174.05	174.05	68.63	68.79	171.53
97.33 M	77.95 M	9.32	9.16	9.19
77.33	75.21	76.78	78.45	80.13
104.89 M	5.07	3.94	2.27	5.9
174.05	79.33	80.89	82.45	82.03
667	1.39	9.65	8.09	7.51
180.7 M	86.31	86.20	89.52	89.40
137	4.18	4.34	0.98	1.14
79.33 TP	174.05	172.67	74.03	72.03
11.21	2.55	3.93	5.57	4.57
90.54 M	176.60 M			



	L	±	R
106	189.07	188.90	188.73
+25			
+34.85	190.81	190.64	190.47
+47.25 E chom E PC on W			
+50	191.36	191.40	191.44
+75			
+84.85 PC	192.16 ✓	192.66	193.16
107	192.63 W		93.42 W
+25	93.10 W		94.00 ✓
+29.33 center	193.56 X	194.26	195.16 ✓
+50	94.16 W		95.51 ✓
+73.81 EC	94.76 W		95.86 ✓
	95.36 X	195.86	196.36 ✓
108	198.30 X	197.80	197.30
+27.48 PC			
+50	199.80 ✓		198.65 ✓
+75	201.30 ✓		200.05 ✓
+95.55 center	202.95 ✓	202.05	201.45 ✓
109	204.25 ✓		202.92 ✓
+55			204.39 ✓
+50	205.55 ✓		
+63.62 EC	206.80 ✓	206.30	205.80 ✓
+75			
110	209.87 ✓	209.70	209.53 ✓
+25			
+50			
+75			

	99.07	90.81	90.47	91.04	91.36
95.56 M	6.49	4.75	5.09	4.12	4.20
202.03	92.16	93.14	92.16	92.72	92.28
202.04	2.40	2.40	10.68	10.12	9.56
202.05	92.4	94.4	95.36	96.34	96.22
202.06	8.92	8.20	7.48	6.48	6.64
202.07	95.01	95.16	94.75	95.93	93.42
202.08	7.43	7.68	8.09	8.91	9.42
202.09	98.30	99.0	10.30	2.95	4.25
202.10	10.60	9.10	7.20	5.95	4.65
202.11	4.39	2.95	4.45	9.05	3.33
202.12	4.51	5.99	7.45	8.25	10.25
202.13	9.87	4.52	9.11	8.25	10.25
202.14	11.35	11.69	11.23	11.07	10.60
202.15	92.99	93.49	92.46	93.92	94.39
202.16	9.38	8.88	8.91	8.42	7.98
202.17	6.59	96.19	93.75	94.33	95.49
202.18	6.18	8.62	8.52	7.42	6.88
202.19	96.69	98.63	200.13	1.63	3.28
202.20	5.68	9.99	8.49	6.99	5.34
202.21	6.62	3.22	3.75	2.28	0.88
202.22	1.99	3.90	4.87	6.34	7.74
202.23	10.20	10.20	9.49	9.29	9.43
202.24	7.97	7.81	10.33	9.86	9.39
202.25	95.09	95.69	98.63		
202.26	7.73	7.10	4.19		

111



L      €      R

111

+05.32      216.12 ✓      215.78  
 +75  
 +50  
 +55.32 PC      219.85 ✓      218.85 ✓

+75      1708 } 210.2 ✓      20.02 } 16.47

112

+75      2231 } 225.1 ✓      21.37 } 19.04  
 +75      2231 } 240.6 ✓      22.7 ✓      19.04

Δ

+33.55 center      225.58 ✓      224.08 ✓

+50      2231 } 26.89 ✓      25.48 ✓      19.04

+75      2231 } 28.20 ✓      26.88 ✓      19.04

113

+11.78 EC      1708 } 230.50 ✓      229.00 ✓      16.47

+75

+50

+50.13 E on R. P. on L.

+75

+88.48 PC      234.73 ✓      235.73

114

+27.94 center      1107 } 36.02 ✓      1.37 ✓      24.1

+50      1107 } 237.31 ✓      238.81 ✓      7.75 RPO

+67.40 EC      1107 } 39.70 ✓      39.32 ✓      9.75

+75      1107 } 240.10 ✓      240.60 ✓      241.10 ✓      24.11

115

+15.21 PC      244.66 ✓      244.32 ✓

+75      45.46 ✓      45.12 ✓

+50      47.50 ✓      47.16 ✓

+75      49.53 ✓      49.19 ✓

Δ 222.79 Bm. Hdr PI

10014  
9  
2077  
1976  
9  
67

RP on 2205

11457

221.22 NI	15.78	16.12	19.85		
221.59 TP	3.44	3.10	7.55		
222.16 NI	21.02	22.54	24.06	19.85	
222.31 NI	11.14	9.62	9.10	12.21	
223.18 TP	30.50	29.50	28.20	26.89	25.58
223.18 TP	1.66	2.66	3.96	5.27	6.58
224.21 NI	12.85	20.02	21.37	22.72	24.08
224.51 TP	13.31	12.14	10.79	9.44	8.08
224.51 TP	21.88	22.28	29.60	9.37	34.73
224.51 TP	0.20	0.20	0.20	0.20	0.20
224.51 TP	5.28	3.89	2.66	222.79	10.08
224.51 TP	37.31	35.70	42.10	4.10	39.83
224.51 TP	7.50	6.11	4.71	3.71	4.98
224.51 TP	3.81	3.12	3.43	3.73	2.23
224.51 TP	1.00	6.69	7.38	9.08	10.58
224.51 TP	4.46	4.46	4.75	4.75	4.75
224.51 TP	8.46	7.66	5.62	2.59	
224.51 TP	4.22	4.51	4.71	4.98	16.41
224.51 TP	8.90	8.00	5.96	3.93	1.72
224.51 TP	20.18	19.68	20.85	22.22	22.55
224.51 TP	12.49	11.89	10.72	9.37	8.06
224.51 TP	22.71	20.21	30.22	30.82	28.53
224.51 TP	3.86	2.46	1.24	2.74	1.74
224.51 TP	4.29	2.97	1.25	3.55	36.25
224.51 TP	7.18	28.70	10.22	8.62	7.50
224.51 TP	36.06	41.42	40.11	39.65	39.65
224.51 TP	8.32	2.95	4.22	4.70	5.24
224.51 TP	44.99	45.79	47.83	48.86	5.15
224.51 TP	10.17	9.30	7.33	5.00	10.01
224.51 TP	42.53	36.35	37.64	39.03	40.43
224.51 TP	46.41	11.05	9.76	8.47	7.08
224.51 TP	42.89	45.79	47.86	49.91	47.83
224.51 TP	55.47	9.68	7.61	5.61	7.64
224.51 TP					5.61







	L	C	R
84 121 +50			
+55.89 PRC ✓	279.00 ✓		279.00 ✓
+75	280.42 ✓		280.04 ✓
122			
+05.9	282.169 ✓		281.169 ✓
+25	83.92 ✓		82.92 ✓
+50	85.52 ✓		84.52 ✓
+75	87.12 ✓		86.12 ✓
+86.50 E.C.	287.86 ✓		286.86 ✓
84 123			
+072 E.C. on R.			
+27.84 PC	289.50 ✓		290.50 ✓
+50	90.75 ✓		91.75 ✓
+75	92.15 ✓		93.15 ✓
124			
+25	93.56 ✓		94.56 ✓
+75	94.99 ✓		95.97 ✓
+50	96.38 ✓		97.38 ✓
+75	97.78 ✓		98.78 ✓
+117.48 E.C.	298.50 ✓		299.50 ✓
125 +99.0	99.60 ✓		100.47 ✓
+25	301.78 ✓		302.47 ✓
+32.21 E.C. on L	303.96 ✓		303.44 ✓
+50			
+77.95 PC	306.40 ✓		305.40 ✓
126			
+25	7.83 ✓		6.80 ✓
+75	9.45 ✓		8.45 ✓
+50	11.08 ✓		10.08 ✓
+75	12.71 ✓		11.71 ✓
127			
+24.12 EC	315.90 ✓		314.90 ✓

284.97 x cut E. End Col. Sta 122+40

310.76 Hub P.I - 12+50

69

284.97	82.92	83.92	84.92	85.92	86.92	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92
285.97	83.92	84.92	85.92	86.92	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92
286.97	84.92	85.92	86.92	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92
287.97	85.92	86.92	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92
288.97	86.92	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92
289.97	87.92	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92
290.97	88.92	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92
291.97	89.92	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92
292.97	90.92	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92
293.97	91.92	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92
294.97	92.92	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92
295.97	93.92	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92
296.97	94.92	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92
297.97	95.92	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92
298.97	96.92	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92
299.97	97.92	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92
300.97	98.92	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92
301.97	99.92	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92
302.97	100.92	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92
303.97	101.92	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92
304.97	102.92	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92
305.97	103.92	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92
306.97	104.92	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92
307.97	105.92	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92
308.97	106.92	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92
309.97	107.92	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92
310.97	108.92	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92
311.97	109.92	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92
312.97	110.92	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92
313.97	111.92	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92
314.97	112.92	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92
315.97	113.92	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92
316.97	114.92	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92
317.97	115.92	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92
318.97	116.92	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92
319.97	117.92	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92
320.97	118.92	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92
321.97	119.92	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92
322.97	120.92	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92
323.97	121.92	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92	139.92
324.97	122.92	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92	139.92	140.92
325.97	123.92	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92	139.92	140.92	141.92
326.97	124.92	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92	139.92	140.92	141.92	142.92
327.97	125.92	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	135.92	136.92	137.92	138.92	139.92	140.92	141.92	142.92	143.92
328.97	126.92	127.92	128.92	129.92	130.92	131.92	132.92	133.92	134.92	13									



	L	C	R
84	315.90		316.31V
127+50 <sup>48</sup> PC	317.21V		
+75	318.51V		317.51V
128	319.80V		318.80V
+75	321.07V		320.07V
85	322.35V		321.35V
+150			
+80	323.90V		322.90V
129	25.65V		24.65V
+20 <sup>34</sup> EC. Ecton R	327.42V		326.42V
+53.30 PC.	329.30V		330.30V
+75	30.55V		31.55V
130	332.00V		333.00V
+75	34.56V		33.56V
+75	33.12V		34.12V
+75	33.68V		34.68V
87	34.24V		35.24V
131	34.80V		35.80V
+75			
+75	335.30		336.30
88			
+75			
+33.9			
+50			
+75			
+83.9			
89			
+75			
+50			

	16.31	17.57	18.80	20.07	21.35	22.90
323.70 NT	16.31	17.57	18.80	20.07	21.35	22.90
35	7.39V	6.19V	4.90V	3.63V	2.35	0.90
333.35 TP	22.35	23.90	25.65	27.42	29.30	30.55
122	13.22	11.67	9.92	8.15	6.27	5.02
334.57 NT	32.00	32.50	32.65	32.42	30.30	31.55
1-32	3.57	3.01	2.92	2.15	1.27	1.02
34.27 TP	33.56	34.12	34.68	35.24	35.80	36.30
5-21	2.07	5.53	4.97	4.07	3.85	3.35
39.65 NT	35.30	34.12	34.24	33.62	33.12	32.14
321.83 NT	4.35	4.83	5.41	5.97	6.53	7.14
43					4.69	3.49
321.80 TP	19.62	20.90	21.40	20.12	18.84	17.18
12-62	2.20	0.93	0.43	1.70	2.89	4.19
334.02 NT	5.48	7.12	7.63	31.88	33.33	34.83
6-3	8.54	4.77	3.89	2.10	0.67	1.19
33.39 TP	30.12	32.75	35.98	4.23	2.68	33.39
6-25	3.89	6.27	8.04	9.79	11.52	13.25
39.40 NT	4.57	5.07	5.63	33.89	34.45	35.01
35.61	5.73	4.57	5.07	5.95	5.19	4.63
	36.13	26.62				35.57
	4.51	3.01				4.07
						3.51



Cutr-68

3794 BM. 446 26'E 7+91.6

53.24/dub - SE of EC 20572

44 25 71

	L	C	R
8 0+00	35.30	35.80	36.30
	36.23 ✓		36.70 ✓ 493
	37.16 ✓		37.65 ✓
	38.08 ✓		38.60 ✓
	39.01 ✓		39.54 ✓
	39.94 ✓		40.48 ✓
8 1+0283 CC	40.87 ✓		41.42 ✓
	41.80 ✓		42.36 ✓
	42.76 ✓		43.30 ✓
	43.71 ✓		44.12 ✓
	44.67 ✓		44.94 ✓
	45.63 ✓		45.81 ✓
	46.58 ✓		46.64 ✓
	47.54 ✓		47.48 ✓
8 2+0565 EC	48.50 ✓		49.31 ✓ 493
+ 5565	50.99 ✓		50.65 ✓

checked with 11/11/12

7992	67.24	67.26	68.04	67.01	67.84	68.64
7950 H	9.24	8.34	9.44	8.44	7.64	6.64
8561	37.06	37.99	38.91	39.84	40.77	41.70
11.75	10.30	9.37	8.45	7.52	6.59	5.66
47.36 M	47.50	46.41	37.02	37.92	38.82	39.77
0.9	1.86	0.90	10.30	9.38	8.43	7.49
46.97 TP	47.63	44.47	45.30	46.14	46.97	47.81
7.28	3.73	2.87	2.00	1.22	0.39	0.40
50.25 M	49.53	48.37	47.47	46.48	45.42	44.30
11.01	4.92	5.88	6.84	7.80	8.72	9.61
53.24 12mm	10.57	61.04	60.20	59.37	58.57	57.74
	63.81 M	3.44	3.78	4.11	4.45	4.79
	1.61	67.42	67.50	67.89	68.39	68.79
	62.15 TP	7.08	6.93	6.83	6.73	6.63
	69.48 M	6.64	6.27	6.89	6.49	6.09
	60.04	5.83	6.23	6.63	7.03	7.43
	8.44	25.63	30.63	32.03	33.43	34.83
	24.52 M	9.11	8.11	7.11	6.11	5.11
	35.61	4.95	26.80	37.49	38.41	39.34
	9.13	53.24	11.80	10.93	10.01	9.08
	4.27 M	62.18	41.20	42.13	43.09	44.04
	35.61	7.22	6.28	5.33	4.38	3.43
	12.81	47.97	37.99	38.93	39.87	40.81
	48.42 M	0.58	10.44	9.49	8.55	7.61
		23.63	24.47	25.30	26.14	26.98
		4.79	3.70	2.72	1.78	0.84

3			
8	+50		
4			
	+50		
5			
8	+50	61.67	61.33
6			62.16
	+50		
7			
	+4166	65.71 ✓	65.37
	+9116 PC	67.10 ✓	66.10 ✓
8		67.26 ✓	66.26 ✓
	+25	67.66 ✓	66.66 ✓
	+50	68.06 ✓	67.06 ✓
	+75	68.46 ✓	67.46 ✓
9		68.86 ✓	67.86 ✓

5.87  
12  
5.54







Sta 78+43<sup>59</sup> to 83+58 16.5 wide

From 83+58 on roadway is 17.25 wide or 1.25 wider than plans show

Widened curves are 21.25 wide at widest point.

2 1/4' fl of curb 6" x 10"







75



Biological Grade- Torrey Road- Widened Curve

92+18 <sup>68</sup> P.C. of $\phi$ .	R 100'
92+06 <sup>90</sup> P.C. of inner curve	R= 107.355 $\Delta 75^{\circ}00'$
95+76 <sup>82</sup> P.C. of $\phi$	R 57.70 $\Delta 171^{\circ}50'$
95+81 <sup>12</sup> P.C. of outer Curve	R 65.39 $\Delta 171^{\circ}50'$
98+06 <sup>50</sup> P.C. of $\phi$	R 120 $\Delta 95^{\circ}36'$
98+15.53 P.C. of outer Curve	R 119.81 $\Delta 95^{\circ}36'$
103+49.95 P.C. of $\phi$	R=180' $\Delta 49^{\circ}00'$
103+40 <sup>77</sup> P.C. of inner curve	R 192.07 $\Delta 49^{\circ}00'$
103+59.13 P.C. of outer curve	R=167.93 $\Delta 49^{\circ}00'$
106+84 <sup>85</sup> P.C. of $\phi$ .	R=45' $\Delta 113^{\circ}16'$
106+92.27 P.C. of outer Curve	R=48.11 $\Delta 113.16$
108+27 <sup>48</sup> P.C. of $\phi$	R=200' $\Delta 39^{\circ}00'$
108+50 <sup>76</sup> P.C. of outer Curve	R 142.27 $\Delta 39^{\circ}00'$
111+55 <sup>37</sup> P.C. of $\phi$ .	R 170' $\Delta 52^{\circ}44'$
111+72 <sup>40</sup> P.C. of outer Curve	R 143.55 $\Delta 52^{\circ}44'$
113+88 <sup>48</sup> P.C. of $\phi$	R 120 $\Delta 37^{\circ}41'$
114+12 <sup>59</sup> P.C. of outer Curve	R 57.35 $\Delta 37^{\circ}41'$
117+92 <sup>55</sup> P.C. of $\phi$ Curve	R=29.71 $\Delta 149.50$
117+87.07 P.C. of inner curve	R=2343 $\Delta 150^{\circ}52'48''$
117+100 P.C. of $\phi$	R=98.22 $\Delta 119^{\circ}58'$
117+06 <sup>93</sup> P.C. of outer curve	R=102.21 $\Delta 119.58$



Bl

92+185

92+06

95+76

95+81

98+065

98+15.5

103+49.95

103+40.77

103+59.13

106+84.85

106+92.27

108+27.48

108+50.76

111+55.32

111+72.40

113+88.45

114+12.59

117+92.55

117+87.07

117+00 = PC of 4

106.33 PC of out

		N1	2.63	10.50	BW
	2.975	13.475		4.845	
T.P.	301	7.855		4020	SpK Polo
		Over N.W. Atlantic	3.835		
			3.19	4.115	
T.P.	628	10.945		6.290	SpK Polo half way to Pitt
	363	10.52	4.055		
			6.06	4.46	N. Rail to Track out
			3.62	6.89	
T.P.	403	10.92		7.75	
		7.75	6.17		
T.P.	300		1.53	6.22	
	7.47	13.69			
			3.19		

27.52  
 22.92  
 403 ) 2.52 1.273  
 22.92  
 29.60  
 27.21  
 1.290

11.56  
 29  
 11.27

87.2  
 1.7 48  
 22.90  
 20.65

26.52  
 22.90  
 4.62  
 4.66



