

952

F.B. 952

LEVEL BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO.

SAN FRANCISCO.

ST. LOUIS.

MICROFILMED

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION

"Copyright, 1885, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

10
11
12
13

Sec 8 Stephens St (50)
N of Lewis to S of Stecker

1
Bm sur
Lewis
Harker S

620 27991 27371

486 28187 290 27701

Curb
27371
620
27991
290
27701
486
28187

N of Lewis St

W 46 27773

47 27772

48 27771

E 49 27770

48 27771

49 27770

E 48 27771

PLOTTED

50 N of Lewis St

W 35 27884

36 27883

35 27884

E 36 27883

36 27883

36 27883

W 31 27888

28187

100

n of Lewis st

w	42	2777
	45	2774
	45	2774
b	43	2776
	43	2776
	46	2773
E	44	2775

150

n of Lewis st

E	56	2763
	57	2762
	57	2768
b	52	2767
	56	2763
	56	2763
w	57	2762

28187

Stephano st

2

200

n of Lewis st

w	76	2753
	75	2752
	72	2757
b	68	2751
	64	2753
	67	2752
E	67	2752

250 PLOTTED

Lewis st

E	78	2751
	85	2752
	85	2752
b	85	2752
	88	2751
	80	2759
w	85	2752

28187

300

n = S. 2 of Montecito

W		88	2771	28187
		85	2776	28187
		82	2777	28187
b		79	2740	
		80	2779	
		80	2779	
E		77	2747	
TP	682	657	27530	28187
	S		level of	Montecito
E		77	2744	
		78	2747	
		78	2747	
b		79	2747	
		81	2740	
		84	2777	
W		86	2745	

28222

Stephens

3

S. 1/4 of Montecito

W		82	2739
		81	2740
		79	2747
b		78	2747
		76	2745
		78	2747
E		77	2744
		74	2747
		76	2745
		74	2747
b		76	2745
		77	2744
		80	2741
W		82	2743

PLOTTED

Center of Montecito

28212

N 1/4 of Montecido

W	76	2755
	77	2764
	75	2766
L	73	2768
	73	2768
	75	2766
E	73	2768

N Cont of Montecido

E	72	2769
	72	2769
	70	2761
L	70	2761
	71	2750
	74	2767
W	73	2768

28214

Stephens

4

N line of Montecido St

W	69	2752
	69	2752
	67	2754
L	66	2755
	65	2756
	68	2766
E	65	2756

PLOTTED

50 N of Montecido

E	45	2776
	44	2777
	50	2771
L	50	2771
	52	2769
	53	2766
W	53	2766

28212

100 n of Montecido

W 64 2757

60 2761

57 2764

b 52 2769

51 2770

51 2770

E 44 2777

150 n of Montecido

E 45 2776

52 2769

52 2769

b 55 2766

59 2762

62 2759

W 63 2758

28212

200 n of Montecido

W 58 2767

64 2757

60 2761

b 59 2762

52 2765

54 2767

E 49 2772

Tp 573 28285 540 2772

PLOTTED

250 n of Montecido

E 58 2771

60 2769

63 2766

64 2765

64 2765

65 2760

W 63 2766

28212
100
2772
573
28285

5

28285

300

n =

S 2 of Stocker 11 (51)

W

54 2775

52 2777

52 2777

b

52 2777

52 2777

52 2777

53 2776

E

47 2777

S bank of

Stocker

E

50 2779

52 2777

51 2778

b

53 2774

56 2777

55 2776

W

56 2777

28285

Stocker

6

S

1/4 of

Stocker

W

57 2777

57 2778

52 2777

b

49 2780

58 2777

58 2777

E

52 2777

Center of

PLOTTED

Stocker

E

50 2779

46 2787

48 2781

b

48 2781

50 2779

52 2777

W

56 2777

28285

N 1/4 of Stock

W 56 2777

52 2777

50 2779

b 47 2782

48 2781

49 2780

E 51 2778

N cont of Stock

E 51 2778

51 2778

51 2778

b 51 2778

51 2778

52 2777

W 55 2774

28285

Stephens

N 1/2 of Stock

W 55 2774

54 2775

55 2774

b 53 2776

49 2780

PLOTTED

50 2779

E 505 27780

new line
of Stock

X sec of Montecito St 50
WS of Stevens to E of Highway

100 276.30

275.30

Montecito

WS of Montecito St

n

10 275.3

15 276.8

17 276.6

b

20 276.3

24 277.9

27 277.6

S

32 277.1

30

w

of Stevens

S

55 270.8

54 270.9

51 271.2

B

50 271.3

47 271.6

43 272.0

n

43 272.0

276.30

Montecito

8

100

w

of

Stevens

n

70 269.3

71 269.2

71 269.2

b

71 269.2

71 269.2

73 269.0

PLOTTED

73 269.0

150

w =

E of Street 50

S

89 267.4

87 267.6

87 267.6

b

86 267.7

89 267.4

90 267.3

n

92 267.1

27630

E 1/4 of Station

n	95	7668
	92	7671
	92	7671
b	92	7671
	88	7675
	89	7670
S	90	7673

PLOTTED

E 1/4 of Station

S	92	7671
	92	7671
	92	7671
b	92	7671
	94	7669
	97	7666
n	88	7665

27630

Muntzite

9

Center of Station

n	99	7662
	97	7666
	95	7668
b	94	7669
	94	7669
	96	7667
S	95	7668

W 1/4 of Station

S	100	7667
	100	7667
	98	7665
b	98	7665
	99	7662
	99	7664
n	101	7662

276.30

W lb of Stock

n 104 2659

101 2667

100 2663

b 100 2663

100 2663

104 2659

2660
270.00
PLOTTED
2660

S 2660

W Side of Stock

S 108 2655

109 2654

109 2654

b 116 2657

105 2658

105 2658

n 107 2656

JP 410 270.30 1010 26620

270.30

Mistake

10

35' W of Stock

n 63 2640

63 2640

65 2638

b 63 2640

64 2639

80 2627

S 78 2625

50 W of Stock

S 56 2647

PLOTTED

50 2653

52 2651

b 58 2655

60 2647

66 2627

n 76 2627

no slope, heavy level

270.30

20' m	100	w	g	Stackin
15' m			40.0	270.30
n			27.8	268.3
			12.6	267.7
			6.0	266.3
			4.1	266.2
b			4.0	266.3
			5.0	265.3
			4.8	266.5
s			4.8	266.5
	150	w	g	Stackin
s			4.4	265.9
			4.0	266.3
			4.0	266.3
l			3.8	266.5
			3.8	266.5
			4.3	266.0
n			12.0	268.3

Level 20' north



270.30

Monteato
11

200	w	g	Stackin
		2.3	268.0
		1.6	268.7
		1.8	268.5
		1.9	268.4
		2.0	268.3
		1.9	268.4
		2.6	267.7
TP	820	277.65	085
	250	w	g
		5.8	271.9
		6.2	271.4
		6.5	271.7
		7.0	270.7
		7.0	270.7
		7.0	270.7
		6.9	270.8

PLOTTED

270.30
 269.55
 8.20
 277.65

27765

12

300

w

= 2

Guided
Hermosa way to

n

49

4778

48

4779

2778

50

4780

2775

l

45

4777

45

4777

44

4776

PLOTTED

s

38

4779

Spuk

470

27295

on w
Hermosa

10/15
5/19
14/19
Blount
Forsyth
July

X Sec of Stockton St 50
N L of Montecito to wd Stephens

560 271.80 266.20

TP P10

N L of Montecito

266.20
500
271.80

E

47

50

52

b

53

56

58

W

61

50 n of Montecito

W

94

80

73

b

65

61

56

E

47

271.80

Stockton

13

75' n

100

n

of Montecito

E

51

55

60

b

66

72

75

W

92

20' W

280

X

75' n

n of

Montecito

E

46

55

62

b

71

80

95

W

125

20' n

220

27180

150 n of B6 to R

W

81

66

57

52

48

44

E

37

TP

818

27906

0.92

27088

Stations on base { 50 m W
37.5 m E

200 n m W

E

96

100

100

L

102

102

104

W

105

27180
92
27088
818
27906

27906

Stokto

14

250 n of Monheata on W

W

80

78

77

L

75

73

73

E

73

300 n of Monheata on W

E

55

68

80

L

88

90

91

W

97

27906

350 n on w

w 80

76

77

b 74

70

65

E 57

400 n on w

E 36

34

36

b 40

40

33

w 34

TP 684 28225 365 27541

28225

450 n = e on w = n

w = n 51

53

58

b 56

54

51

E = S 52

4690' n = E } = w dir of Stephens
38560' n = S }

E = S 50

50

50

50

49

48

w = n 49

48

Sheet ✓

Sheet No

15

28225

445

27780

xx 300

300

27780

10
5
14

X sec of Kalimia St (80)

E 2 32nd to

690

30452

29762

Plus SW
Kalimia BL

100

E

g

32nd

Kalimia

16

E 2 of 32nd St

29762

S

56

1989

S

62

1983

690
30452

55

1990

58

1987

51

1994

56

1989

b

50

1991

b

54

1991

50

1995

51

1994

47

1998

48

1997

n

46

1999

PLOTTED

45

3000

150

E

g

32nd

n

50

E of 32nd

n

50

1995

n

48

1997

53

1992

51

1994

53

1992

53

1992

1

55

1990

b

52

1993

57

1988

54

1991

60

1985

56

1989

S

66

1979

S

57

1988

30452

200

E = W of Bancroft (80)

S		77	2968
		77	2973
		77	2973
b		70	2975
		68	2977
		74	2971
n		78	2967

7P

096

PLOTTED

42

29510

1314
Bancroft

E line of Bancroft

S		41	2940
		44	2917
		48	2913
b		50	2911
		52	2909
		51	2910
n		53	2908

29606

50

E

of Bancroft

n		100	2861
		97	2860
		97	2860
b		100	2861
		99	2862
		101	2860
S		101	2860

7P

072

100'

28444

E %

1234

28372

Bancroft

S		52	2797
		50	2790
		45	2799
b		44	2800
		46	2798
		46	2798
n		42	2802

Kalmia

17

28444

150

E

of Bancroft

n

113 277.1

105 277.9

104 276.0

b

102 276.2

110 277.4

112 277.2

S

106 273.8

70

260

PLOTTED

1133 277.1

175

E

of Bancroft

S

62 269.5

176

E

S

9.5 266.2

200

E

= N of 33d st

S

12.5 267.2

6.4 269.3

6.4 269.3

b

7.2 268.5

7.8 267.9

9.2 266.5

n

10.5 265.2

18

Carrington 30 dup 60' E of 32d

28444

1133

277.1

277.9

276.0

276.2

277.4

277.2

273.8

277.1

269.5

266.2

267.2

269.3

269.3

268.5

267.9

266.5

265.2

10
 6
 54
 70 ft
 7 ft
 V sec of S St (80)
 E of 32nd rd
 200' East

8375

19

670 8375 7705 SW of 32
 E line of 32nd st

50 E of 32nd

S

6.3 77.5

77.05
6.28
83.75

48 79.0

5.2 78.6

5.1 78.7

6.3 77.5

6.0 77.8

b

4.3 79.5

b

5.8 78.0

4.5 79.2

5.6 78.2

4.9 78.9

5.8 78.0

n

4.7 79.1

n

5.4 78.4

160 E of ground

Same line on top

n

5.0 78.8

n

5.2 78.6

5.1 78.7

5.3 78.5

5.2 78.6

5.0 78.8

b

5.2 78.6

l

5.3 78.5

5.3 78.5

5.8 78.0

5.7 78.7

5.6 78.2

s

4.8 79.0

S

5.3 78.5

150 E of 32nd

S 47 791

48 790

50 788

b 53 785

51 787

51 787

n 50 788

200 E of 32nd

n 48 790

50 788

50 788

b 53 791

43 791

52 786

S 50 788

Level 25 E on 2nd center

Buffs of 5 E of S line

10/6/1904
6/10/1904
14/10/1904

Xmas Haytt St (80)
Entire Haytt

1140 90.87 99.47

0.5E 29
K

N line of K st

E 67 84.2

79.14
1140
91.14
6.02
85.12
11.98
95.78

67 84.2

61 84.8

b 51 85.8

58 85.1

59 85.0

W 57 85.2

Same line as top

W 41 86.8

+10

42 86.7

57 85.2

58 85.1

b 51 85.8

61 84.8

41 86.8

E 45 86.4

90.87

Haytt

21

50 n of K st

E 30 87.9

30 87.9

28 88.1

25 88.4

27 88.2

25 88.4

W 28 88.1

100 n of K st

W 08 80.1

06 90.3

05 90.4

b 03 90.6

07 90.2

12 89.7

E 10 89.9

TP 11.98 10232 0.53 90.34

10232

1

150

n

of

K st

E 84 93.9

82 94.1

83 94.0

L 83 94.0

87 93.6

92 93.1

W 95 92.8

200

n

of

K st

W 55 96.8

45 97.8

31 99.2

L 23 100.0

23 100.0

23 100.0

E 20 100.3

TP

1267

114.35

674 101.58

11425

14074

22

250

n of

K st

E 30 111.3

42 110.1

55 108.8

L 67 107.6

83 106.0

99 104.4

W 124 101.9

300

n =

S 2 of J st

W 87 105.6

44 109.9

07 113.6

TP 11.57 122.9 353 110.72

L 66 115.7

48 117.5

30 119.3

E 23 120.0

1229

S

center of jet

E 0.2 122.1

2.0 120.3

3.6 118.7

b 5.4 116.9

8.0 114.3

12.2 110.1

w 16.4 105.9

S

1/4 of jet

w 16.7 105.6

12.7 109.6

8.5 113.8

b 6.6 115.7

3.5 118.8

2.0 120.3

E 4.3 122.6

1229

Height

23

center of jet

E 4.5 122.8

2.0 120.3

4.0 118.3

b 7.0 115.3

9.4 112.9

11.8 108.5

w 17.7 104.6

N

1/4 of jet

w 17.8 104.5

14.0 108.3

10.5 111.8

b 8.0 114.3

4.5 117.8

2.8 119.5

E 1.4 120.9

12229

N bb of J⁵

E			20	120.3
			35	118.8
			50	117.3
			88	113.5
			120	110.3

N S of Jst

E			1.0	121.3
			4.3	118.0
			6.9	115.4
			10.8	111.5

W

TP

517 114.46

1300 109.29

7.0 107.5

9.8 104.7

W 12.4 102.1

N bank of Jst

W 9.7 104.8

bb 8.3 106.2

1.5

114.46

50 - n of Jst

E			1.0	113.5
			2.0	112.5
			6.5	108.0
			9.5	105.0
			12.5	102.0

TP 5.25 108.53

11.18 103.28

9.6 98.9

W 13.1 95.4

20' W 17.0 91.5

20' W 100 n of Jst 18.0 90.5

W 15.9 92.6

14.0 94.5

12.5 96.0

10.2 98.3

6.8 104.7

2.2 106.3

E 1.8 106.7

May 7

24

11705
 12
 10405
 1512
 10922
 11118

10853

125'

n

q

f w

E

4.6 103.9

5.2 103.3

10.6 97.9

b

13.0 95.5

TP

660

10257

1256

95.97

8.3 94.2

9.1 93.4

W

135'

n

125 90.0

140 101.885

150

n f

f w

W - level red top

W

13.0 89.5

13.0 89.5

9.6 92.9

b

9.0 93.5

7.3 95.2

1.7 100.8

E

1.2 101.3

10257

200

n

q

f w

E

4.5 98.1

5.0 97.6

9.0 93.6

b

12.4 90.2

10.8 92.1

10.2 92.4

W

10.2 92.4

250

n

q f w

W

4.8 92.7

5.7 96.9

8.8 93.8

b

9.7 92.9

8.6 94.0

7.2 95.4

E

6.6 96.0

Hay St

25

10257

300 n = S.d. of J₁ (80)

E 77 94.9

86 94.0

72 95.4

L 15 101.1

TP 1156 113.88 025 10202

106 103.3

93 104.6

W 76 106.3

Mom 780 106.08

(Interachi in Book 935)
N line of J₁ at

E 80 105.9

53 108.6

23 111.6

TP 1248 1262 014 11374

L 115 114.7

100 116.2

92 117.0

W 90 117.2

12622

May 26

50 n g J₁ at

W 03 125.9

15 124.7

45 121.7

L 34 122.8

43 121.9

57 120.5

E 79 118.3

TP 1303 13825 020 12532

100 n g J₁ at

E 116 126.8

101 128.3

86 129.8

76 130.8

63 132.1

50 133.6

W 47 137.7

TP 1260 14984 111 13724

14984

150 n of J

W

9.7 140.1

10.4 139.4

11.1 138.7

b

11.5 138.3

12.2 137.6

12.7 137.1

E

13.6 136.5

200

n

of J

E

7.3 147.5

8.0 141.8

7.0 144.8

1

6.3 143.5

6.4 143.4

6.7 143.1

W

6.6 143.2

14984

250 n of J

W

47 145.1

40 145.8

42 145.6

37 146.1

37 146.1

37 146.1

E

40 145.8

300

n

of

J

(100)

E

14 148.4

12 148.6

17 148.1

21 147.7

28 147.0

30 146.8

W

32 146.6

TP
mm

1320

161.64

140

148.44

34V
mm SE
A14984
148.44
148.44
148.44
148.44
148.44

27

~~114.64~~
161.64

N line of R st

W	115	150.1
	107	150.9
	102	151.4
b	102	151.4
	89	152.7
	86	153.0
E	83	153.3

50 n of R st

E	47	156.9
	50	156.6
	56	156.0
b	64	155.2
	72	154.4
	79	153.7
W	93	151.3

161.64

100 n of R st

W	72	154.4
	58	155.8
	44	157.5
b	32	158.4
	28	158.8
	16	160.0
E	12	160.4

140 n = Parallel line End of st

E	07	160.9
	10	160.6
	12	160.4
b	12	160.4
	16	160.0
	33	158.7
W	54	156.7

28

X sec of 20th St (80)
K to End

770

8717

7947

58029

N line of K St

W

60 81.2

63 80.9

62 81.0

W

67 80.5

69 80.7

75 79.7

E

72 80.0

50 n of K St

E

77 79.5

73 79.9

72 80.0

W

70 80.2

66 80.6

63 80.9

W

52 81.0

87.17

29

100

n

of

K St

W

44 82.8

44 82.8

46 82.6

W

52 82.0

54 81.8

57 81.5

E

58 81.2

150

n

of

K St

W

31 82.1

34 83.8

29 84.3

W

26 84.6

20 85.2

09 86.3

W

01 87.1

70

1286

9803

20 85.17

194

n

of

K

W

94 88.6

W

101 87.9

7947
770
87.17
200
85.17
1286
98.03

9803

200 n of K 21

W 64 91.6

82 90.8

100 88.0

S 108 87.2

110 87.0

114 86.6

E 120 86.0

250 n of K 21

E 70 91.0

64 91.6

64 91.6

S 56 92.0

50 92.0

42 92.8

W 26 93.2

TP 1257 11018 042 9761

11018

275 n of K 21

W 114 98.8

113 98.9

132 97.0

S 144 95.8

155 94.7

153 94.9

E 162 94.0

300 n = SD of (80)

E 122 98.0

117 98.5

118 98.0

S 92 101.0

81 102.1

70 103.2

W 54 104.8

2907

30

9803

642

97.61

1257

110.18

110.18

S 66 of 1st

W 27 107.5

42 106.0

57 105.1

b 59 104.3

72 103.0

84 101.8

E 96 100.6

S 1/4 of 1st

E 74 102.8

61 101.1

50 105.2

b 35 106.7

32 107.0

20 108.2

W 03 109.9

TP 12.30 121.76 0.72 109.46

121.76

center of 1st

W 91 112.7

110 110.8

120 109.8

b 127 109.1

142 107.6

153 106.5

E 166 105.2

N 1/4 of 1st

E 148 107.0

136 108.2

121 109.7

b 110 110.8

96 112.2

82 113.6

W 65 115.3

29.4

31

110.18
- 22
109.46
12.30
121.76

12176

N bank of Jst

W	33	1185
	50	116.8
	64	115.4
b	74	114.4
	91	112.7
	107	111.1
E	126	109.2

N line of Jst

E	92	112.6
	80	112.8
	62	115.6
b	44	117.0
	35	118.3
	19	119.9
W	0.9	120.9
TP	1245	13304
	117	12059

13304

29 st

32

50 n b Jst

W	25	120.5
	48	128.2
	64	126.6
b	69	126.1
	75	125.5
	82	126.8
E	86	126.6
me	705	12520

12176
117
1205
1245
122104
29
12265
1082
1239

n e 20

100 n b Jst

E	0.0	122.0
	0.3	122.7
	0.0	122.0
b	0.0	122.0
	0.1	122.9
	0.0	122.0
W	0.0	122.0

TP 1082 14097 029 13265

Subwell 13304 1070 12234

min n e
Kaya

14347

150

n

0.1

J 21

W

10.3 1377.4

9.3 1372.2

5.0 1388.5

b

2.0 1415

1.4 1421

0.9 1426

E

1.0 1425

175

n

0.1

J 21

E

0.1 1434

0.8 1427

2.0 1415

b

3.5 1400

7.0 1365

10.0 1375

W

11.0 1375

14347

292

33

200

n

0.1

J 21

W

13.2 1300.7

12.0 1315

11.3 1322

b

8.4 1351

5.8 1377

4.2 1393

E

2.8 1407

250

n

0.1

J 21

E

0.1 1346

11.5 1320

70

0.44

131.67

12.4 1314.3

b

1.7 1300

4.3 1296

6.7 1280

W

7.8 1272.9

10.1 1276

200

n

0.1

J 21

E

1.0 1307

14347
1228
13123
131.67

13167

300 n = S 2 II st

E 5.0 126.7

7.4 127.3

9.4 127.2

l 11.0 120.7

TP 0.62 119.82 124.7 119.20

1.3 118.5

2.7 117.1

W 4.6 115.2

Intersection of Sat in B 935

n S of II st

E 4.0

6.4

8.7

b 10.6

11.8

TP 1/13 109.15 11.8 108.02

3.2

7.0

10915

40 n of S

W 41 n o 9.0

W 45 n of S 12.0

W 50 n of S 13.0

W +8 12.0

13.0

8.0

6.5

l 3.4

1.1

0.0

E +1.2

7.5 n b S at

E +1.0

0.8

3.4

b 6.6

7.6

12.0

12.6

9.3

10.5

290

34

13167
12.07
179.20
62
119.82
11.82
108.02
1.13
109.15

109.15

100 n g SW

W 8.6

9.5

9.5

77

11.5

9.4

5.0

3.3

E 0.0

130 n g J

E 3.1

8.2

10.0

b 8.0

7.7

7.7

W 6.7

109.15

150 n g SW

W 4.8

5.9

7.0

b 7.2

7.4

8.6

e 9.4

200 n g SW

E 6.2

6.1

4.8

b 4.0

3.0

1.5

W 7.0

TP 10.49 117.83 1.80 109.35

109.15
1.80
107.35
1.248
117.83

11783

W	250	n	f	34
				14
				44
				68
b				94
				110
				122
E				133

E	275'	n a E	Bottom of Ditch	105
	295'	n n W		90
				73
b				51
				20

TP	1288	<u>13021</u>	050	11733
			112	
W			70	

300' n-s line of H St (100)
 Street is being graded
 (the S line will be on grade)

13021

290

36

E		N. line of	H St	60
				50
				15
TP	1192	<u>14213</u>	00	13021
b				103
				72
				47
W				30

E		3' n of H	n E l	12100
		50	n of H	W

E				132
				89
				48
				16
TP	783	<u>14855</u>	141	14072
				51
				35
W				25

11783
 50
 11733
 1288
 13021
 1192
 14213
 141
 14072
 783
 14855

14855-

37

100° N of H st

W

10,2

14855-
14855-

0,8

1,5

b

3,5

6,8

9,7

E

13,6

140° N = Approx Pueblo, Lim End of S

E

12,0

6,9

2,6

b

0,2

TP

1300

16155

0,0

14855-

12,3

11,6

W

10,2

chuck

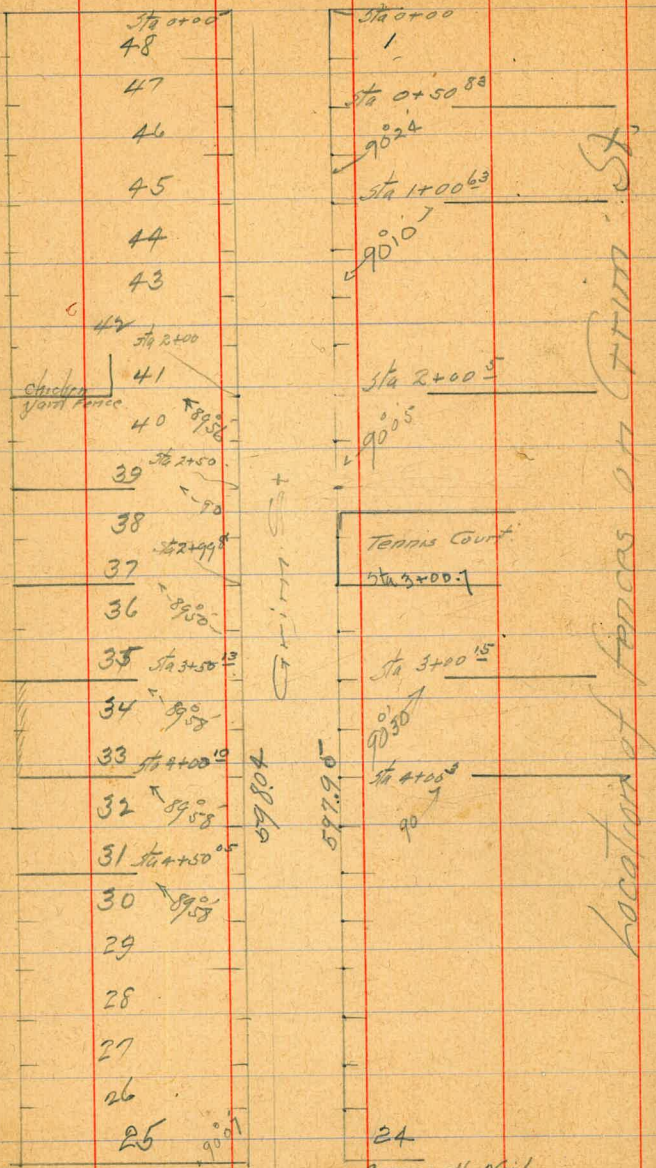
0,6

✓

Thorn St.
Hub

10/24/10
Hub
Hub

657-4 W
66795 E



Redwood

Hub

Cromwell's Nail

St.

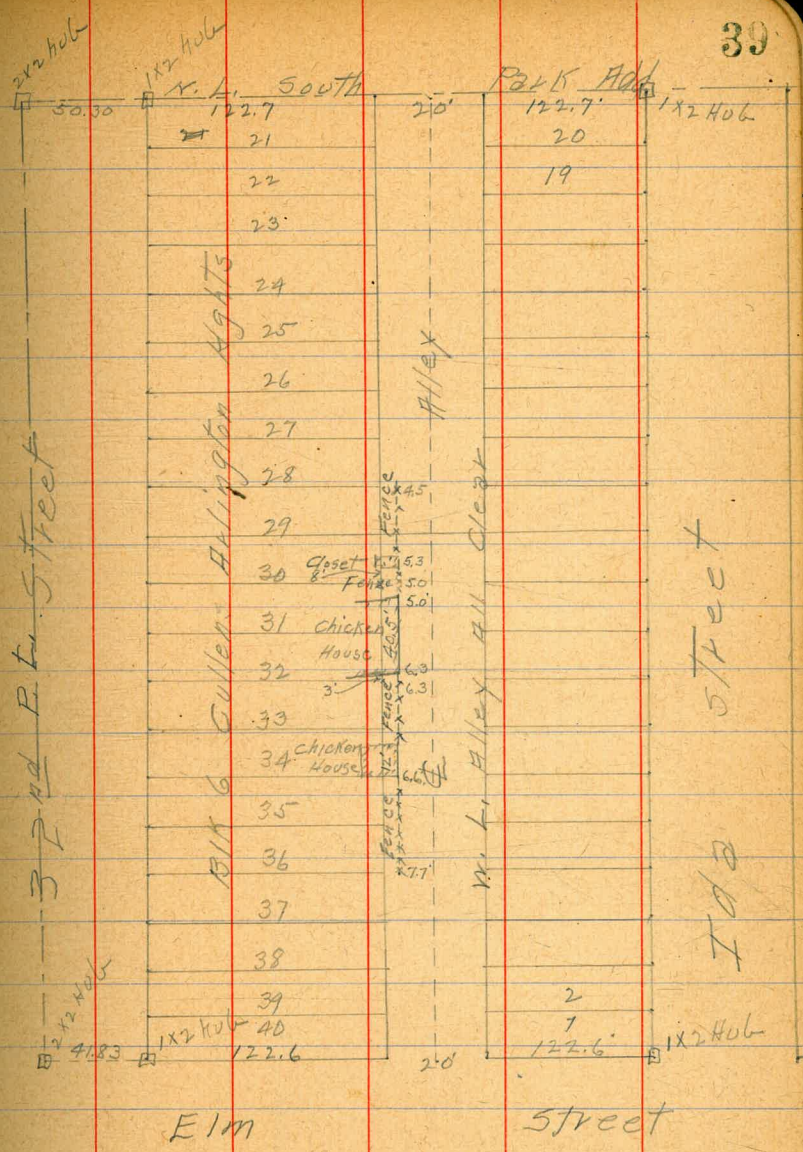
Location of fences on THORN ST.

Alley

Chicken Yard Fence

Culvert

4/30/11A Duple
Shaw
Kerr
Survey showing encroachments on
Alley BIK 6 Cullen's Arlington Heights Add.



This image shows an open notebook with two blank, lined pages. The pages are cream-colored and feature light blue horizontal ruling. Red vertical lines create margins on both pages. The right page has the number '40' printed in its top right corner. The notebook is placed on a white surface against a black background.

Gregory
Shoemaker
Moore

N ST
Showing Location of Franchise
Limes Etc.

19TH

ST

ST

19TH
Rail
27.4 24.9 28.7

Rail

Rail

Rail

26.3 23.9 29.3

18TH

ST

21ST

ST

North

South

North

South

VOID

27.5 23.85 28.4

26.6 24 29.2

17TH

ST

20TH

ST

North

South

North

South

28.4 24.1 27.5

27.65 23.35 29.0

16TH

ST

19TH

ST

N

N

2075

211

241

41

19

25.1

80

251

278

502

Opening of Hensley from K
Xsect.

7.09 ^{H.I.} 93.04

85.95

South line K

Elms

2.0

2.0

1.7

C

1.1

0.9

0.6

White

0.2

10' 20.

White

0.6

2.6

4.4

C

5.3

5.5

6.0

Elms

6.4

150' south
60' street 10' walks

Dec. 12/14 Heildelberg
Kerr

33' 20.

Elms

7.8

7.5

7.5

C

7.6

7.1

6.6

White

5.7

50' 20.

white

8.2

8.2

8.3

C

8.5

8.4

8.5

Elms

8.8

100' Ro.

Elms

11.3

11.8

11.9

c

11.9

11.6

11.6

White

11.3

150' Ro.

White

15.0

15.1

14.6

c

14.9

14.9

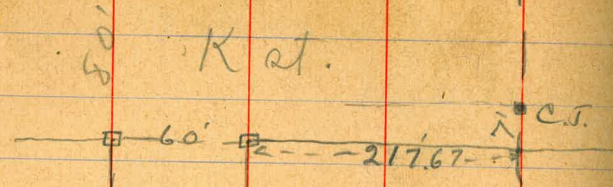
14.5

Elms

14.1

N St.

30' 30'



Hensley St.

Pueblo line

L St.

50'

- 14.70
- 40.19
- 156.38
- 13.73
- 36.08
- 13.67
- 274.80

15.70
36.08

136.7
3.58



Pueblo canal

Pueblo line

28th St.

webster

Everett

60'

0.8'

17' 43"
27' Pin

110'

110'

1
13
15

blaze
Taylor
Lib

X Sec of Dallas St (70')
E of Western add to Cholesterol Blvd
(10' width)

Play
w/

787	9342		8555	
1174	104.15	1.01	9241	8535
		763	965	787
		673	9241	9342
			1178	101
			104.15	
TP	131	93.96	1150	92.65 TP
				763
				965
513	86.17	12.9	81.84	10415
				673
				97.15
				10415
				1150
				92.65
				131

PL E of Western add

S		14.3	71.9	
		120	74.2	
		111	75.1	
b		105	76.0	
		94	76.8	
		93	76.9	
n		10.0	76.2	

8617

Dallas 45

25'

E of PL

n				46	81.6
				39	82.3
				32	83.0
b				38	82.4
				54	80.8
				61	80.1
S				66	79.6
TP	1178	9715	080		85.37
50					
S				109	86.3
				100	87.2
				100	87.2
b				108	86.4
				115	85.7
				105	86.7
n				104	86.8

9715

75

E of

P2

n

96 87.6

92 88.0

89 88.3

b

80 89.2

75 89.7

76 89.6

s

87 88.5

100

E of

P2

s

87 88.5

77 89.5

76 89.6

b

77 89.3

85 88.7

91 88.1

n

96 87.6

9715

46

125

E of

P2

n

97 87.5

87 88.5

84 88.8

b

80 89.2

73 89.9

66 90.6

s

68 90.4

160.2

E of

P2

169.72

E of

P2

S = B6

s

58 91.4

50 92.2

60 91.2

75 89.7

76 89.6

86 88.6

n

96 87.6

97.15
 18598 E m n } - P Isld of Villa Quin 70
 19548 E a S }

n	8.0	89.2
	75	89.7
	66	90.6
h	60	91.2
	55	91.7
	50	92.2
S	48	92.4
n	46	92.4
S	38	93.4
	38	93.4
	40	92.9
l	51	92.1
	55	91.7
	57	92.1
a	57	91.5

97.15
 Station 47

n	1/4 of	Villa	Quin
		27	94.5
		27	95.0
		33	93.9
h		36	93.6
		29	94.3
		23	94.9
S		23	94.9
	Center of	Villa	Quin
S		13	95.9
		07	96.5
		17	95.8
h		21	95.1
		23	94.9
		15	95.7
n		17	95.5
TP	109	109	220 96.95

97.15
 920
 96.95
 1227
 109.22

10922

	E	1/4 f	Villa	Dir
n			116	97.6
			127	96.5
			132	96.0
b			126	96.6
			124	96.8
			124	96.8
S			130	96.2
	E	1/4 f	Villa	Dir
S			116	97.6
			113	97.9
			110	98.2
b			107	98.5
			103	98.9
			95	99.7
n			90	100.2

10922

3

	E	1/4 f	Villa	Dir	⊕
n			75	101.7	↓
			80	101.2	
			85	100.7	
b			90	100.2	
			95	99.7	
			97	99.5	
S			97	99.5	
			97	99.5	
			97	99.5	
			97	99.5	
			98	99.7	
			90	100.2	
b			95	99.7	
			78	101.4	
			67	102.5	
n			59	103.3	16

This x sec is Valtan's produced
through Villa lots 34, 35, 7 & 8 to
Chateau and Blvd

109^m

25

E of

Villa Orin

n

40 105.2

40 105.2

45 104.7

b

53 103.9

59 103.3

61 103.1

S

64 102.8

50

E of

Villa Orin

S

40 105.2

36 105.6

38 105.4

b

31 106.1

25 106.7

26 106.6

n

25 106.7

109^m

75

E of

Villa Orin

n

03 108.9

06 108.6

10 108.2

b

17 107.5

22 107.0

20 107.2

S

22 107.0

TP

1280

12080

128 107.94

100

E of

Villa Orin

S

120 108.8

120 108.8

b

120 108.8

117 109.1

108 110.0

n

100 110.8

102 110.6

Village
49

109^m
128
107.94
1286
120.80

12080

	125'	E of	Villa	Dist
n				75 112.3
				80 112.8
				84 112.4
b				90 111.8
				99 110.9
				102 110.6
s				103 110.5

	150'	E of	Villa	Dist
s				85 112.3
				80 112.8
				75 113.3
b				71 113.7
				66 114.2
				66 114.2
n				62 114.6

12080Vollan
50

	175'	E of	Villa	Dist
n				45 116.3
				47 116.1
				53 115.5
b				60 114.8
				63 114.5
				67 114.1
s				74 113.4

	200'	E of	Villa	Dist
s				56 115.2
				50 115.8
				47 116.1
b				42 116.6
				37 117.1
				31 117.7
n				28 118.0

12080

225 E of Valla Drive

n 17 119.1

21 118.7

24 118.4

b 29 117.9

34 117.4

34 117.4

s 40 116.8

250 E of V-D

s 37 117.1

33 117.5

31 117.7

b 23 118.5

20 118.8

15 119.3

n 08 120.0

ip 330 123.29 081 119.99

123.29

275 E of Valla Drive

n 28 120.5

32 120.1

33 120.0

b 37 119.5

43 119.0

51 118.2

s 57 117.5

300 E of V-D

s 54 117.9

49 118.4

48 119.3

b 33 120.0

29 120.4

25 120.8

n 23 121.0

Valla
51

12080
81
119.99
5.30
123.29

325 E of Villa Rica

n 17 121.6

21 121.2

26 120.7

b 29 120.4

36 119.7

43 119.0

S 48 118.5

355 E or S } = W 2 Shotwell Bluff
362 E or N }

S 42 119.1

37 119.5

31 120.2

1 27 120.6

25 120.8

19 121.4

n 13 122.0

Sam Lee
W. side of Shotwell Bluff

257
1174

n 26 120.7

28 120.5

33 120.0

b 40 119.3

45 118.8

48 118.5

53 118.0

(S)

This Point is 317.10 n of Bluff for Tidal St

79 70 111.27 1200 111.29

270 104.35 765 101.62

bluff

700 97.35

cont. on
Page 45

12329
12
11828
965
10162
223
10435
700
9735

1/15
15/15

Blair
70 ft
4 ft

X Sec of Villa Drive (70)
Waltain St to Chelmsworth Blm

848

10/13

92.65

TR - 1/2

55.5 m W }
50.5 m E }

S of Waltain St

E = 361 m of Eb at Chelmsworth

b

W = (P.S.)

25' 5 m W } = End of Curve on W L
15' 5 m E }

W

b

E

> 61' E }
421' W }

14 99.7

34 97.7

47 96.4

53 95.8

63 94.8

76 93.5

87 92.4

111 90.0

92 91.9

76 93.5

64 94.7

52 95.9

36 97.5

16 99.5

92.65
848
10/13

E

b

W

W

b

E

10/13

53

28 98.3

44 96.7

60 95.1

72 93.9

82 92.9

92 91.9

110 90.1

55.5 m W }
50.5 m E }

123 88.8

113 89.8

100 91.1

86 92.5

70 94.1

58 95.3

46 96.5

10/13

55' S in w } = BC to 2nd st in w
 50' S " " }

E

65 94.6

7.2 93.9

8.1 93.0

9.5 91.6

10.2 90.9

11.3 89.8

12.4 88.7

W

20' S in E } = PA of 2nd st in w
 28' S " " }

EB rd toward

W

19.8 81.3

12.3 88.8

11.1 90.0

10.0 91.1

8.9 92.2

8.1 93.0

6.8 94.3

E

5.8 95.3

Sub 869

10/13

10' S - E } = n leg of 2nd st
 12' S - W }

E

5.3 95.8

6.8 94.3

7.9 93.2

8.7 93.4

9.7 91.4

11.1 90.0

12.4 88.7

W

12' S - E } = n leg of 2nd st
 14' S - W }

W

12.4 88.9

11.1 90.0

10.0 91.1

8.5 92.2

7.8 93.3

6.9 94.2

E

5.6 95.5

10113

$$\left. \begin{array}{l} 12'S \text{ or } E \\ 14'S \text{ or } W \end{array} \right\} = \text{center of tidal } W$$

E 53 95.8

66 94.5

75 93.6

b 86 92.5

101 91.0

111 90.0

W 120 89.1

$$\left. \begin{array}{l} 12'S \text{ or } E \\ 14'S \text{ or } W \end{array} \right\} = S \frac{1}{4} \text{ of tidal } W$$

W 120 89.1

110 90.1

100 91.1

b 84 92.7

73 93.8

64 94.7

E 57 95.4

10113

55

$$\left. \begin{array}{l} 12'S \text{ or } E \\ 14'S \text{ or } W \end{array} \right\} = S \frac{1}{4} \text{ of tidal } W$$

E 62 94.9

68 94.3

73 93.8

b 87 92.4

90 92.1

102 90.9

114

$$\left. \begin{array}{l} 10'S \text{ or } E \\ 12'S \text{ or } W \end{array} \right\} = S \frac{1}{4} \text{ of tidal } W$$

E 65 of tidal W

130 88.1

94 91.7

89 92.4

90 92.1

b 80 93.1

74 93.7

63 94.8

E 61 95.0

TP 620 102.38 4.95 96.18

10113

4.95

96.18

6.20

102.38

10238

26 S^o E
28 S^o W

End of bar on S side

E	67	95.7
	70	95.4
	75	94.9
b	80	94.4
	80	94.4
	80	94.4
W	77	94.7
	57	96.7
	58	96.6
	54	97.0
b	51	97.3
	50	97.4
	48	97.6
E	43	98.1

44 S^o E
48 S^o W

10238

56

44 S^o E } = Blk to end of blattmarch
47.5 S^o W } Blm

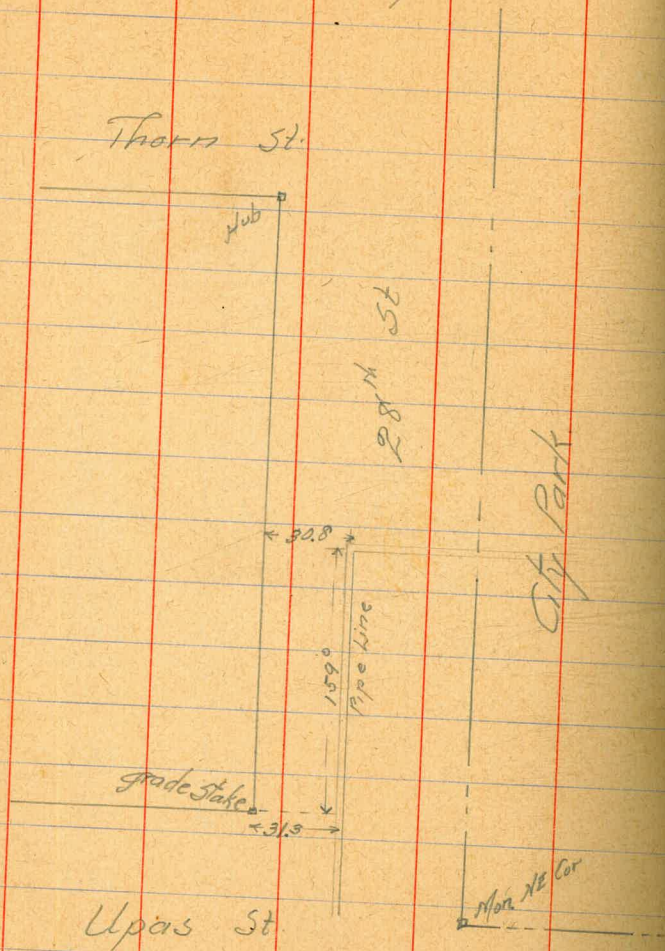
E	29	99.5	
	32	99.2	
	33	99.1	
b	32	99.2	10238
	35	98.9	4.95
	38	98.6	97.43
W	40	98.4	
	(43)	98.1	
E. B. W. d. n.	(32)	99.2	
	(40)	98.4	
W. A.	(27)	99.7	
	(36)	98.8	
	(26)	99.8	
	(34)	99.0	
	(28)	99.6	
b	33	99.1	
	32	99.2	
	30	99.4	
	28	99.6	
E. L.	18	100.6	
E. B. E. d. n.	4.95	97.43	✓

W. d. n. of blattmarch Blm Graded

✓ and 1 bl
Page 43

2/6/15
Hatch
Moore
Hall

Sketch showing location
of Water Main on 28th
St near Upas -



EM SW. Mason & S.D. Ave R.R. spr pole	22.60
EM NE. Cor. Raleigh Home R.R. spr pole.	23.33

2/15/15
Gregory
Shoemaker
Moore

CROSS-SECTION OF
27TH ST 60' WIDE 10' WALKS
From N.L. Logan to S.L. Marcey

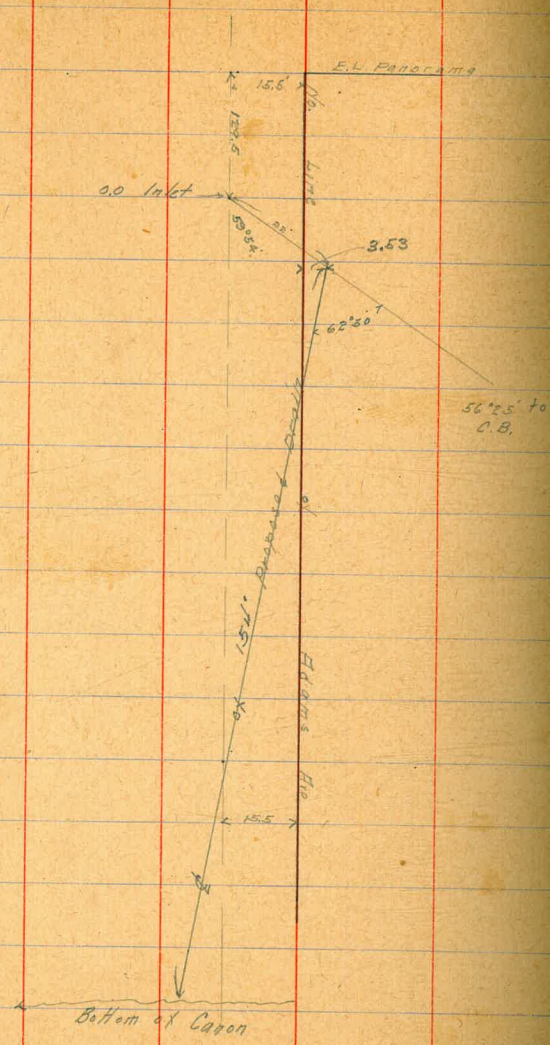
BM	6.01	6.02	6.03	N.L. 27th & Logan	100' No.	
		N.L. LOGAN				Top Curb 3.21 64.58
						W Cb 4.0 64.0
On Top Curb		6.02	64.00			1/4 4.3 63.7
W Cb		6.3	61.7			c 4.1 63.9
1/4		6.4	61.6			1/4 4.8 63.2
c		6.2	61.8			1/4 4.7 63.3
1/4		6.4	61.6			Top Curb 3.52 64.50
E Cb		6.0	64.0			140' No. = S.L. MARCEY AVE
Top Curb		6.01	64.01			Top Curb 2.52 65.50
		50' No				E. Cb 3.3 64.7
Top Curb		4.9	63.23			1/4 3.2 64.8
E Cb		5.2	64.8			c 2.8 65.2
1/4		5.4	64.6			1/4 3.0 65.0
c		6.0	64.0			1/4 3.0 65.0
1/4		5.7	64.3			Top Curb 2.48 65.52
cb		5.6	64.4			
Top Curb		4.77	63.25			

CEMENT CURB & WALK IN ON
 BOTH SIDES OF 27TH ST
 FROM MARCEY TO LOGAN

50

11/23/15
Gregory
Shoemaker
Moore

LOCATION OF PROPOSED
DRAIN ON ADAMS AVE AT
GEORGIA.



11/23/15
Gregory
Shoemaker
Moore
LEVELS OVER LINE
FOR DRAIN FROM WEST END
OF BRIDGE ON ADAMS AVE
AT GEORGIA.

BM	3.36	354.43	351.07	
0.0			4.50	= Top of Curb
0.0			6.06	= Bottom of Inlet
+17			4.30	
+22 = L.P.T.			9.50	
T.P.	0.13	342.45	12.41	342.02
+39			4.20	
T.P.	1.68	331.14	12.99	329.46
T.P.	0.32	318.65	12.82	318.32
10 +102			11.0	
T.P.	0.07	305.96	12.76	305.89
T.P.	0.73	293.63	13.06	292.90
+121			1.3	= Wedge Road
+142			0.0	= E.V. ✓
+155			7.5	
+166			13.9	
+176			23.5	= Bottom of Canon

11/29/15
 Gregory
 Shoemaker
 Moore

LOCATION OF DRAIN
 ADAMS AVE BRIDGE

LEVELS OVER \angle OF
 DRAIN.

335 354.42 351.07

BM 335 354.42 351.07

No. 66

5.09

0.0 4.50 349.92 = Top of Curb

0.0 6.06 348.36 = Bottom Inlet

E.L.

PEROGAMG

+22 4.6 349.8 = Top Abut.

+22 14.6 339.8 = Bottom

+22 13.6 340.8 = Top Ground at E side Abutment.

121.5
 121.5

22.1

31.30

ADAMS AVE

T.P. 0.0 340.14 14.28 340.14

+32 2.6 337.5

T.P. 1.28 328.72 12.70 327.44

T.P. 0.65 316.22 13.15 315.57

+90 4.1 307.1

T.P. 13.30 302.92

+112 292.3 = Wedge Rd

+133 293.6 = E

+146 286.1

← Bottom of Canon

+157 279.7

+167 270.1 = bottom Canon

31°36'

11 L

2/15
Gregory
Shoemaker
Moore

LEVELS ON THORN ST
from 110' E. of Brant to 1' East to
Determine if Temporary Grading is
acceptable

63

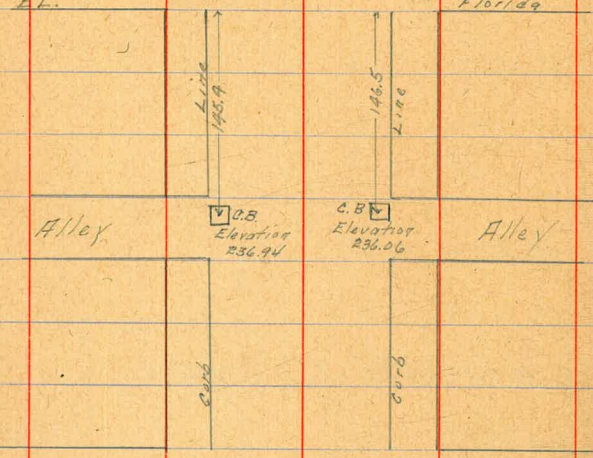
B.M.					Drake
	3.50	245.50		242.0	
			110' E		
N. on Curb		3.65		241.85	
S. ✓ ✓		5.25		240.25	
			120' E		
N. on Curb		4.60		240.90	241.0 ✓ OK
S. ✓ ✓		5.90		239.60	239.5 ✓ OK
			136' E		
N. on Curb		6.00		239.50	239.40 ✓ OK
S. ✓ ✓		7.70		237.80	238.06 ✓ OK
			144' E = Beginning of Curve		Street may be accepted to this point.
N. on Curb		6.90		238.60	238.60 ✓ OK
S. on Curb		8.55		236.95	237.34 ✓ OK low
			170' E		
N. in line with Curb ^{2nd} east edge of Driveway		9.60		235.90	236.00 ✓ OK
			160' E		
S. in line with Curb ^{2nd} at end of fill		9.80		235.70	235.90
			164' E on Center of St = Hard pan Curb of Driveway		
Top Curb		10.20		235.30	

Locations + Elevation
CATCH BASINS ON
ADAMS between Florida &
Alabama

146
145
145

B.M.	336	342.20	338.24	St. Adams Alabama
South basin		5.26	336.94	
North	✓	6.14	336.06	

Florida
Fl. St.
Florida



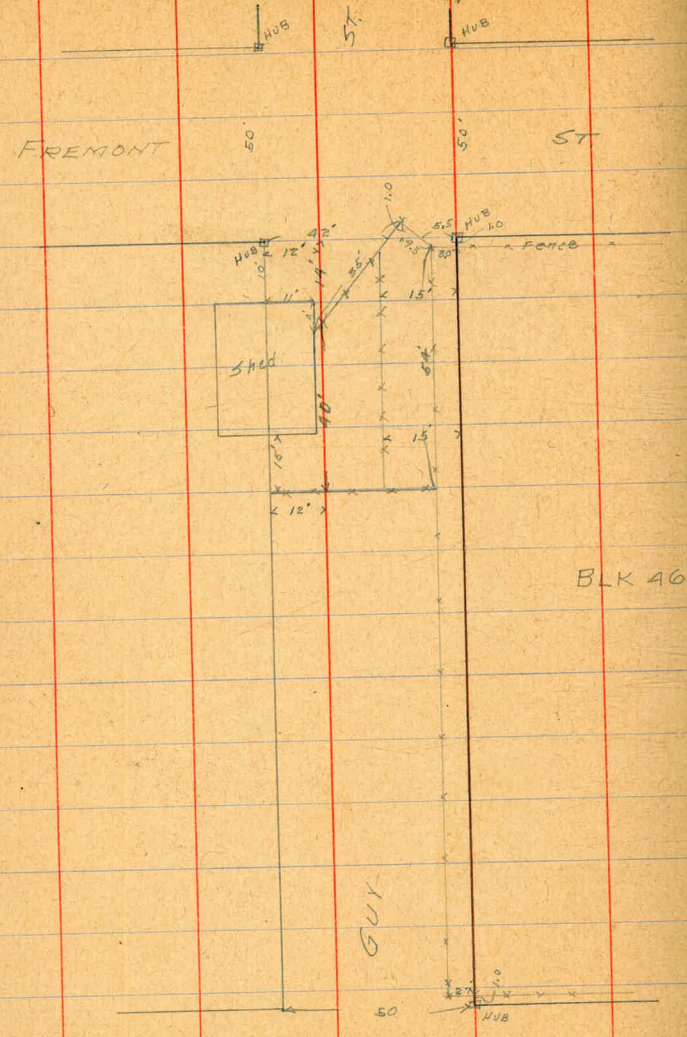
Alabama St.

	337.50	337.50	
	336.94	336.06	
S. basin to be raised	0.56	1.44	n. basin to be raised
	6 3/4"	17 1/4"	

3/10/15

Gregory
shoemaker
Moore.

SURVEY OF BLOCK 46
Middletown Addition
Showing fences etc. in GUY
and FREMONT STS.



Woodman Ave. X Secs - 40 St to City Lts

60' Wide except 40 St Int.
10' Wks 10' / 45.

3/16 W. West
Evans
Jennie

67

Bill SW 40 Woodman top fire hyd

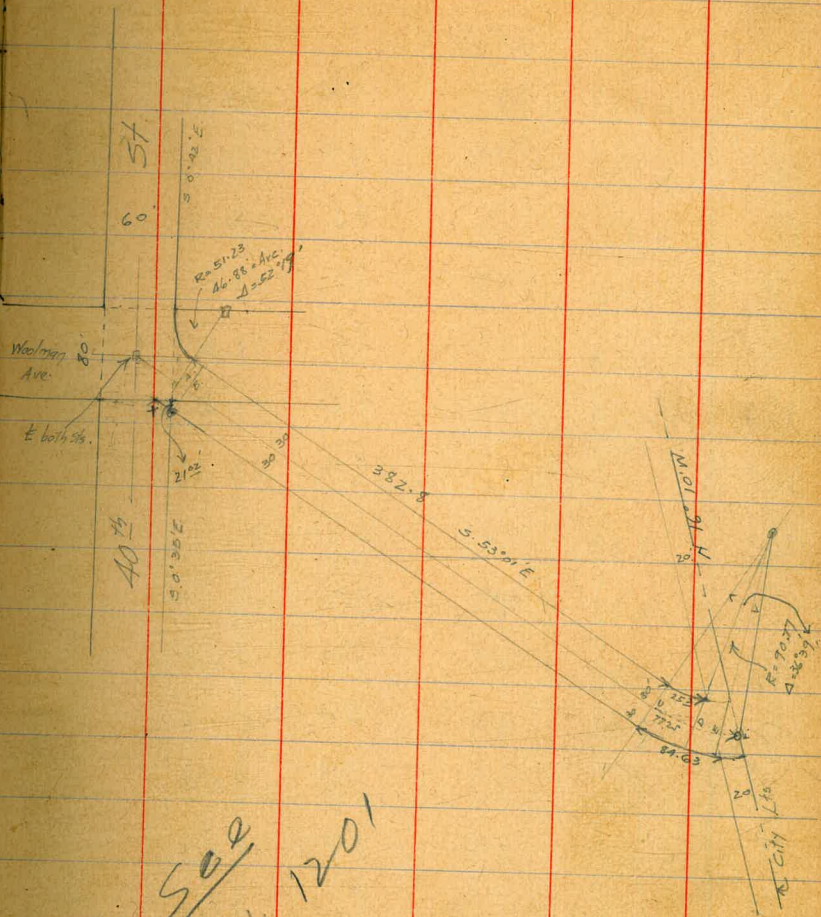
87.47

1.35

88.82

WL 40 St.

SL	3.6	85.2
C	4.2	84.6
1/4	3.9	84.9
±	4.0	82.8
1/4	4.4	84.4
H/L	5.0	83.8
C	4.0	84.8
NL	3.3	83.5
W. Curb		
NL	4.5	84.8
C	5.0	83.8
1/4	5.3	83.8
±	5.4	83.4
1/4	5.9	82.9
C	6.6	82.7
SL	7.3	81.5
+ 15	11.6	77.2



See
Field Book 1201
pp. 140-3

Woolman

88.82

W. 1/4

- 15	126	76.7
SL	11.0	77.8
C	9.6	79.7
1/4	8.0	80.8
E	7.8	81.0
1/4	6.8	82.0
C	6.2	82.6
NL	6.1	82.7
	E 405t	
NL	7.0	81.8
C	6.4	82.4
1/4	7.9	80.9
E	8.7	80.1
1/4	9.2	79.6
C	10.5	78.3
SL	11.3	77.5
+		

88.82

E. 1/4

68

SL	11.8	77.0
C	11.6	77.7
1/4	10.2	78.6
E	9.7	79.1
1/4	9.0	79.8
C	8.1	80.7
NL	8.4	80.4

E Curb.

NL	10.0	78.8
C	9.9	78.9
1/4	10.0	78.5
E	10.4	78.4
1/4	10.7	78.1
C	12.2	76.6
SL	12.3	76.5

Woolman.

88.82

EL. 40 st.

SL	12.9	75.9
C	13.0	75.8
1/4	11.7	77.1
±	11.1	77.7
1/4	11.2	77.6
C	11.1	77.7
NL	11.1	77.7

Sec X.

Int with SLines Woolman produced	11.4	77.4
Int SL Woolman & EL 40st.	14.6	74.7

Sec A.

NL Woolman	12.4	76.4
C	12.3	76.5
1/4	12.3	76.5
±	13.0	75.8
Int with EL 40st.	13.1	75.7
TR	12.10	76.72

0.94 77.66

77.66

77.7

Sec B - 21° E of Sec A.

69

SL

C

1/4

±

1/4

C

NL

NL

C

1/4

±

1/4

C

SL

3.6

3.0

2.5

2.8

3.0

3.1

2.5

50 E of A.

4.5

4.8

5.0

5.1

5.1

5.2

5.6

74.1

74.7

75.2

74.9

74.7

74.6

75.2

73.2

72.9

72.7

72.6

72.6

72.5

72.1

Woolmap.

77.66

77.7

75' E of A

SL	7.0	70.7
C	6.6	71.1
1/4	6.3	71.4
±	6.2	71.5
1/4	5.8	71.9
C	5.6	72.1
NL	5.1	72.6

100' E

NL	5.8	71.9
C	6.5	71.7
1/4	6.9	70.8
±	7.1	70.6
1/4	7.1	70.6
C	7.2	70.5
SL	7.6	70.1

77.66

77.7

70

125' E

SL	8.6	69.1
C	8.6	69.1
1/4	8.3	69.4
±	8.2	69.5
1/4	8.0	69.7
C	7.2	70.5
NL	6.6	71.1

150' E

NL	7.4	70.2
C	8.0	69.7
1/4	8.5	69.7
±	9.2	68.5
1/4	9.5	68.2
C	9.6	68.1
SL	9.8	67.9

Woolman

77.66

77.7

175' E

SL	10.8	66.9
C	10.7	67.0
1/4	10.1	67.6
±	9.3	68.4
1/4	8.8	68.9
C	8.4	69.3
NL	7.9	69.8

200' E

NL	8.7	69.0
C	9.0	68.7
1/4	9.4	68.3
±	9.5	68.2
1/4	10.5	67.2
C	11.4	66.3
SL	11.8	65.9

77.66

77.7

77.1

225' E

SL	11.8	65.9
C	11.3	66.4
1/4	10.8	66.9
±	10.2	67.5
1/4	9.6	68.1
C	9.2	68.5
NL	8.6	69.1

250' E

NL	7.6	70.1
C	8.2	69.5
1/4	8.5	69.2
±	8.8	68.9
1/4	9.4	68.3
C	10.3	67.4
SL	11.2	66.5

Woolman

77.66

77.7

275'E.

SL	10.6	67.1
C	9.6	68.1
1/4	9.0	68.7
E	8.3	69.4
1/4	7.7	70.0
C	7.0	70.7
NL	6.2	71.5

300'E

NL	5.2	72.5
C	5.7	72.0
1/4	6.4	71.3
E	7.2	70.5
1/4	8.1	69.6
C	8.8	68.9
SL	9.6	68.1

77.66

77.7

325'E.

SL	9.2	68.5
C	8.4	69.3
1/4	7.6	70.1
E	6.7	71.0
1/4	6.1	71.6
C	5.0	72.7
NL	4.5	73.2

350'E.

NL	4.6	73.1
C	5.0	72.7
1/4	5.8	71.9
E	6.8	70.9
1/4	7.8	69.9
C	8.5	69.7
SL	8.9	68.8

Woolman

77.66

77.7

382⁸ E = P.C. = Sec E.

SL	9.7	68.0
C	9.0	68.7
1/4	7.8	69.9
±	7.0	70.7
1/4	6.3	71.4
C	5.3	72.4
NL	4.6	73.1

Sec D = 25² E on Arc. on NL
 = Int NL with WL. Bound. St.
 = 41.9 E. on Arc. on SL

NL	4.6	73.1
C	5.3	72.4
1/4	6.2	71.5
±	7.3	70.4
1/4	8.2	69.5
C	9.0	68.7
SL	9.7	68.0

Woolman Ave

77.66

77.7

77.7

Sec E = Int NL & PL.
 with SL & WL Boundary St

SL	8.8	68.9
C	7.7	70.0
1/4	7.0	70.7
±	6.3	71.4
1/4	5.7	72.0
C	5.6	72.1
NL	4.2	73.5

Sec F = P.L. = City Lts.

NL	4.2	73.5
C	6.0	71.7
1/4	5.9	71.8
±	6.1	71.6
1/4	6.5	71.2
C	7.2	70.5
SL	8.0	69.7
T.P.	8.95	76.71

12.67 89.38

B.M. SW 40 of Woolman top fire hyd.

1.92

87.46

87.47 OK

40 St X Secs.

St Woolman to SL T-st. 60' W. ^{10' W. 10' W.}

BM SW 40 & Woolman top fire plug 87.47 88.00

0.50 87.97

Sec A.

WL.	27	85.3
C	8.0	80.0
1/4	10.6	77.4
1/4	11.2	76.8
1/4	12.2	75.8
C	13.0	75.0
BL.	13.9	74.1

Sec B

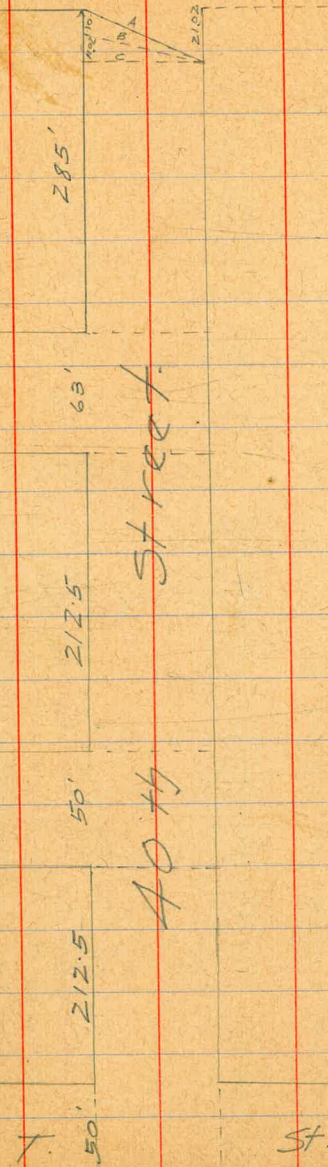
BL.	13.9	74.1
C	13.2	74.8
1/4	12.6	75.4
1/4	11.7	76.3
1/4	11.4	76.6
C	10.2	77.8
W.L.	9.3	78.7

1/2 mile West
Course
Devoted

Woolman Ave

Teak.

S. St



40 St

87.97

88.0

Sec C = 21.02 3.7 5L Woolmatt

WL	10.4	77.6
C	11.1	76.9
1/4	12.1	75.9
£	12.5	75.5
1/4	13.1	74.9
C	13.5	74.5
EL	13.9	74.1
TP	12.50	75.47

4.25 79.72

50's of 5L Woolmatt

EL	7.8	71.9
C	7.3	72.4
1/4	7.0	72.7
£	6.3	73.4
1/4	6.2	73.5
C	5.3	74.4
WL	5.1	74.6

40 St

79.72

79.7

75's

WL	7.0	72.7
C	7.5	72.2
1/4	8.0	71.7
£	7.8	71.9
1/4	8.5	71.2
C	8.9	70.8
EL	9.0	70.7

100's

EL	10.4	69.3
C	10.3	69.4
1/4	10.1	69.6
£	9.6	70.1
1/4	9.3	70.4
C	9.2	70.5
WL	8.8	70.9

125's

WL	8.2	71.5
C	9.2	70.5
1/4	9.8	69.9

	79.72	40 ST	79.7
£		10.2	69.5
1/4		10.6	69.1
C		11.0	68.7
EL		11.6	68.1
+15		12.1	67.6
	150's		
-10		12.6	67.1
EL		12.2	67.5
C		11.3	68.4
1/4		10.0	69.7
£		9.2	70.5
1/4		9.0	70.7
C		7.7	72.0
WL		6.9	72.8
	175's	27	
WL		3.7	76.0
+1		6.3	73.4
C		6.8	72.9
1/4		8.3	71.4
£		8.9	70.8
1/4		9.8	69.9

	79.72	40 ST	79.7
C		10.8	68.9
EL		11.4	68.3
+10		12.3	67.4
	200's		
-10		11.8	67.9
EL		10.7	69.0
C		9.7	70.0
1/4		8.5	71.2
£		7.4	72.3
1/4		7.2	72.5
C		5.9	73.8
WL		4.8	74.9
	225's		
WL		1.6	78.1
C		3.3	76.4
1/4		5.1	74.6
£		5.4	74.3
1/4		7.0	72.7
C		8.3	71.4
EL		7.9	69.8
+		11.0	68.7

	79.72	40 St. 79.7	84.5
	250'S.		
-10		10.4	69.3
EL		9.5	70.2
C		7.9	71.8
1/4		6.0	73.7
±		2.5	77.2
1/4		1.6	68.1
T.P.		0.89	78.83
	5.68	84.51	
C		4.7	79.8
WL		3.5	
	285'S = NL. TeqK. 63' Wide - 10' Wks.		
WL Man. BM.		3.43	81.1
C		4.7	79.8
1/4		6.0	78.5
±		6.5	78.0
1/4		8.1	76.4
C		9.7	75.8
EL		10.9	73.6
+10		12.5	72.0

	84.51	40 St. 84.5	77
	N Curb. TeqK.		
-10		12.5	72.0
EL		10.7	73.8
C		9.1	75.4
1/4		7.9	76.6
±		6.5	78.0
1/4		6.1	78.4
C		4.7	79.8
WL		3.5	81.0
	N 1/4		
WL		3.7	80.8
C		4.6	79.9
1/4		6.0	78.5
±		6.3	78.2
1/4		8.0	76.5
C		9.1	75.4
EL		10.7	73.8
+10		12.6	71.9

8451

40 St

84.5

£ Teak.

-10	12.1	74.4
EL	10.5	74.0
C	8.7	75.8
1/4	7.6	76.9
£	6.3	78.2
1/4	5.5	79.0
C	4.3	79.2
WL	3.6	80.9

5 1/4

WL	3.4	81.1
C	4.0	80.5
1/4	5.0	79.5
£	6.1	78.4
1/4	7.5	77.0
C	8.7	75.8
EL	10.0	74.5
+10	11.6	72.9

40 St

8451

84.5 78

S. curb.

-10	11.2	73.3
EL	9.9	74.6
C	8.6	75.9
1/4	7.4	77.1
£	5.8	78.7
1/4	4.9	79.6
C	4.2	80.3
WL	3.5	81.0

S.L. Teak St

WL	3.4	81.1
C	5.0	79.5
1/4	5.4	79.1
£	5.6	78.9
1/4	7.3	77.2
C	8.7	75.8
EL	9.9	74.6
+10	11.3	73.2

T.P. NW. Cor Teak + 40 Mon.

133

82.41

3.43

81.08

82.41

25'S.

WL

+1

C

1/4

£

1/4

C

EL

+10

34 79.0

40

44 78.4

47 77.7

46 77.8

46 77.8

5.9 76.5

7.7 74.7

9.3 73.1

50'S.

-10

EL

C

1/4

£

1/4

C

+8

WL.

9.5 72.9

8.5 73.9

7.7 74.7

7.1 75.3

6.4 76.0

6.3 76.1

5.6 76.8

5.2 77.2

4.4 78.0

40 ST

~~82.4~~

82.41

75'S

WL

+3

C

1/4

£

1/4

C

EL

+10

-10

EL

C

1/4

£

1/4

C

+6

WL.

40 ST

~~82.4~~

73

58 76.6

70 75.4

7.6 75.8

8.2 74.2

8.3 74.1

9.0 73.4

9.6 72.8

10.0 72.4

10.1 72.3

100'S.

12.0 70.4

11.8 70.6

10.9 71.5

10.3 72.1

9.7 72.7

9.9 72.5

9.0 73.4

8.7 73.7

7.9 74.5

82.41

125's

40 st.

82.472.0

WL

10.4 72.0

C

11.1 71.3

1/4

11.6 70.8

E

11.7 70.7

1/4

12.4 70.0

C

13.1 69.3

EL

13.6 68.8

+10

14.8 67.6

T.P.

11.02 71.39

0.64 72.03

150's

-10

5.5 66.5

EL

5.0 67.0

C

4.3 67.7

1/4

3.5 68.5

E

2.9 69.1

1/4

2.1 69.9

C

1.4 70.6

WL

0.5 71.5

72.03

175's

40 st.

72.0

87

WL

1.5 70.5

C

2.2 69.8

1/4

3.3 68.7

E

3.7 68.3

1/4

4.4 67.6

C

5.3 66.7

EL

6.4 65.6

200's

EL

6.8 65.2

C

6.2 65.8

1/4

5.4 66.6

E

4.5 67.5

1/4

4.0 68.0

C

3.1 68.9

WL

2.4 69.6

212's = NL 5. st 50' W 10' W Ks. 7 1/2 1/4.

WL

2.4 69.6

C

3.4 68.6

1/2

4.7 67.3

72.03

40 St.

72.0

£	5.1	66.9
1/4	5.9	66.1
C	6.6	65.4
EL	6.8	65.2

N Curb S. St.

EL	6.8	65.2
C	6.7	65.3
1/4	6.0	66.0
£	5.6	66.4
1/4	4.8	67.2
C	3.8	68.2
WL	3.1	68.9

N 1/4

WL	3.0	69.0
C	3.9	68.1
1/4	4.9	67.1
£	5.6	66.4
1/4	6.6	65.4
C	6.5	65.5
EL	7.0	65.0

72.0

	WL	C	1/4	£	1/4	C	EL	
£	3.0	4.0	5.1	6.0	6.8	7.2	7.5	↑ 72.03 H.I.
5/4	3.4	4.4	5.5	6.4	7.0	7.6	7.8	
C	4.0	4.8	6.1	6.7	7.4	7.8	7.8	
SLs	4.8	5.8	6.7	7.3	7.9	8.0	8.6	
25's	7.5	8.0	8.1	8.6	8.8	9.5	10.0	
50'	9.2	9.7	9.4	9.8	10.3	10.9	11.4	
75	10.1	11.6	11.3	11.8	12.0	12.5	13.0	
100	1.5	2.2	2.8	2.6	3.0	3.3	3.6	
125	4.0	4.1	4.1	4.1	4.2	4.4	4.3	
150	5.3	5.5	5.5	5.6	5.6	5.3	5.5	
175	6.7	6.6	7.0	7.0	6.8	6.6	6.4	
200	7.8	8.2	8.4	8.1	8.1	7.7	7.6	
225	8.6	9.1	7.0	8.7	8.5	8.2	8.2	
NL.T.	11.1	10.7	10.0	9.2	8.8	8.5	8.4	
N.C.		50.6		52.1		52.8	52.9	
1/4	11.0	10.7	10.2	9.7	9.2	9.0	8.8	
£	11.2	10.7	10.0	10.1	9.6	9.2	9.0	
2 1/4	11.7	11.5	11.3	11.0	10.4	9.8	9.7	
50	11.8	12.0	11.9	11.6	11.1	10.5	10.2	
SL	11.8	12.1	12.2	12.7	12.4	11.7	11.0	
TST		49.2		48.6		49.6	50.3	

84.60

84.60

72.03 H.I.

11.87

60.96 TP

8.34

61.30 H.I.

8.34

60.96 TP

12.12

73.08 H.I.

0.95

72.13 TP

12.47

84.60 H.I.

81.06 TP

10.32

91.38 H.I.

5.95

87.43 BM. SW. 40 & Woolman.

87.47 = OK.

61.30 H.I.

10
33
50

20,861.93
30
21.129

186
43
3
129

10526
19 2.00
1.00
95
38
120

846
355
81.05

21.29
20.86
52.15

52.15
51.75
0.40

2687.5
1112.0
1575.5

2664
1115
1549

1059
21
1110

16.09 180.00 73.34
8.40 105.49
105.49 740.11

89.40 180.00 73.34
16.09 73.31
73.31 106.29

797425
1234
106.05

36.08
32
32.9

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.