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F.B.

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INDEX BOOK

IND



# KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO.

SAN FRANCISCO.

ST. LOUIS.

## TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

B 8.66  
 Rd + 0.90  
 —————  
 9.56  
 — 5.55  
 —————  
 4.01

RETURN TO CITY ENGINEER'S OFFICE  
 CITY HALL, SAN FRANCISCO, CAL.



Sewer Construction  
 & Alley bet Witherby &  
 Hortensia N. of Hickory

	1.02	252.05	251.03	
M.H. & Hickory +	940	25062	10.83	24122
Alley = 0+00				235.0
0+50	695	243.67	238.33	+ 5.34
1	362	247.0	241.67	+ 5.33
+ 35 DE	163	248.99	244.0	+ 4.99

15.36  
 38.26

A

1.22	12.04	
0.81	12.25	
1.53	12.87	
0.24	12.77	
0.99	12.73	
0.26	12.87	
0.34	13.00	
0.63	12.61	
1.18	12.75	
0.37	12.60	26706
1.28	12.19	118.34
<u>8.83</u>		<u>148.72</u>

0.25	12.63	
0.16	12.84	
1.80	12.40	
0.46	13.09	
1.45	12.86	
1.81	12.75	26706
<u>5.48</u>	203.76	189.48
14.28		<u>77.58</u>

0.17	12.99	
0.15	12.87	
0.37	13.06	
1.44	12.95	
1.23	13.01	
<u>3.36</u>	2.11	63.43
	66.99	<u>14.16</u>

135	9.00	66.66
	8.10	1.11
		<u>55.50</u>
		1.998
		<u>2.331</u>



1/21/28 Gregory Sewer Construction  
 Wetherby St & Hickory St

118.3  
 46.7

275 2170.00 789 0  
 19 250  
 2200  
 275

BM. GRADE

324	254.27	251.03		
Wetherby St + 50' N of = 0+00	0.58	253.69	249.0	+ 4.69
0+25	0.21	254.06	248.81	+ 5.25
0+75	0.35	253.92	248.42	+ 5.50
1+25	0.01	254.26	248.02	+ 6.24
1+75	0.90	253.37	247.62	+ 5.75
2+25	1.83	252.44	247.22	+ 5.22
2+75 M.H. & Hickory Δ 90° L.	2.58	251.69	246.93	+ 4.86
3+00	3.76	250.51	245.0	+ 5.51
3+50	7.96	246.31	241.33	+ 4.98
4+00	12.75	241.49	237.27	+ 3.82
4+50 M.H. Sta 31+282 page 46 Δ x Alley to North 446.47	6.56	240.11	235.9	To West + 5.11
5+05	5.10	241.57	237.75	+ 3.82
5 Δ + 60 (?) 2RN	1.27	245.40	240.5	+ 4.90

135 ft = width

EXTENSION OF SEWER from above  
 to 100' S of E of Chestnut.

Wetherby St 50' N of N.L. = 0+00	Ches. 7.53	258.56	251.03	
	8.95	249.61		
+25	4.83	253.73	249.87	+ 3.86
+75 M.H. & Chestnut break	5.32	253.24	250.37	+ 2.85
1+25	5.32	253.24	250.74	+ 2.50
+35	4.85	253.71	251.09	+ 2.62

= Flowline present End. This pipe not put to grade.

275 } 2461  
 24673  
 288  
 275  
 13.66  
 11.00  
 2.66

01.48  
 5.24  
 26



1/22/25 Gregory

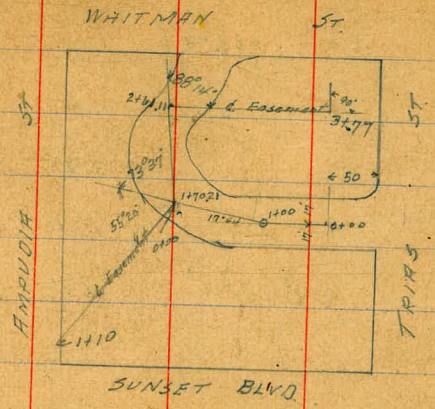
Sewer Construction  
CRESCENT DRIVE

	012	249.13		249.01	NE Whitman + Trias
2 Crescent Dr 50W of Trias 20x20	049	236.79	12.83	236.30	GRADE
+50			9.47	227.32	223.5 + 3.82
1+00 M.H. 5.78			10.85	225.94	222.33 + 3.61
+35			5.86	224.26	220.32 + 3.94
+70.21 = M.H.			6.63	223.49	219.5 + 3.99
2+15.41			5.90	224.22	220.75 + 3.47
+61.11 = M.H.			4.02	226.10	222.0 + 4.10
3	1248	242.54	006	230.06	
+10			9.24	232.70	225.5 + 7.20
+60			8.55	233.99	231.0 + 2.99
+77 Δ 90°			2.70	239.84	233.56 + 6.28
4+27			7.62	239.92	235.27 + 4.65

1250  
230  
1425  
22770

4300 7 908  
22770

12857  
5470  
7387



Sewer Construction from Crescent to

Ampudia

230.12				
6.63	223.49	219.5	+3.99	
11.03	219.09	217.0	+2.09	
+3.70 + 55' break				
+3.15 T.P.	0.53	217.33	13.32	216.80
T.P.	3.00	208.89	11.44	205.89
1+10			9.69	199.20
				196.0 + 3.20

0512  
221  
2126  
1109  
1534  
171

117 16.00 6.513  
581  
113  
500 256

277  
1704

2011  
1721  
1704



1/28/25

Sewer Construction  
 & TRIAS ST  
 from & Hickory to & Whitman

17,500 U14  
 1.5  
 20

	300	270.06	-7.60	267.06	GRADES SP. ESTIMATION	
M&E Factory + 0+00	127	263.73		262.46		
		FOR LINE FROM HICKORY TO STOCKTON SEE PAGE 3				
		2.14		261.59	256.0	+ 5.59
+ 50		3.34		260.39	254.85	+ 5.54
1		4.56		259.17	253.71	+ 5.46
+ 50		5.88		257.85	252.57	+ 5.28
2		7.23		256.50	251.43	+ 5.07
+ 50		8.49		255.26	250.28	+ 4.96
3		9.64		254.09	249.14	+ 4.95
+ 50 & Chesnut 6.06	255.97	10.32		253.41	248.10	+ 5.41
4		12.00		252.17	247.28	+ 4.89
+ 50		13.54		251.53	246.56	+ 4.97
5		14.90		250.77	245.85	+ 4.92
+ 50		16.86		250.21	245.13	+ 5.08
6		18.55		249.52	244.42	+ 5.10
+ 50		20.31		248.76	243.71	+ 5.05
7 + 00 & Whitman		22.58		248.49	243.0	+ 5.49



2 1/2 hrs Gravel SEWER CONSTRUCTION  
 FROM 50' S. of 5L of FT STOCKTON  
 To & Hickory on 2. of  
 TRIAS ST.

50' S. of 5L 599	FT Stockton on West 268.45	262.26			
0000		307	205.38	261.0	+ 4.38
+50		361	264.84	260.09	+ 4.75
-		439	264.06	259.18	+ 4.88
+50		509	263.36	258.27	+ 5.09
Y		592	262.53	257.36	+ 5.17
+50		674	261.71	256.48	+ 5.26
+75' to Hickory				256.0	

1877  
 1901  
 277.3

2075.00  
 1827.00  
 248.00



NAPA

2 3 1 4 357	2 3 1 4 366	2 3 1 4 388	2 3 1 4 417	2 3 1 4 418	2 3 1 4 442	43	2 3 1 4 471	2 3 1 4 472	2 3 1 4 499
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CHERRY

2 3 1 4 358	2 3 1 4 385	2 3 1 4 389	2 3 1 4 416	2 3 1 4 419	2 3 1 4 441	2 3 1 4 443
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PINE

2 3 1 4 352	2 3 1 4 359	2 3 1 4 384	2 3 1 4 390	2 3 1 4 415	2 3 1 4 420	2 3 1 4 440
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

FORT STOCKTON

2 3 1 4 351	2 3 1 4 360	2 3 1 4 383	2 3 1 4 391	2 3 1 4 414	2 3 1 4 421	2 3 1 4 439
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

HICKORY

2 3 1 4 350	2 3 1 4 361	2 3 1 4 382	2 3 1 4 392	2 3 1 4 413	2 3 1 4 422	2 3 1 4 438
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

CHESTNUT

2 3 1 4 349	2 3 1 4 362	2 3 1 4 381	2 3 1 4 393	2 3 1 4 412	2 3 1 4 437
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

WHITMAN

2 3 1 4 348	2 3 1 4 363	2 3 1 4 380	2 3 1 4 394	2 3 1 4 411	2 3 1 4 436
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUNSET BLVD.

2 3 1 4 347	2 3 1 4 364	2 3 1 4 379	2 3 1 4 395	2 3 1 4 410	2 3 1 4 425
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

WALLACE

SHERMAN ST  
 BAY ST  
 CUMMINGS ST  
 ALBANY ST  
 VERNON PARK

ST

ST

ST

ST

ST

ST

WALLACE

MASON

SUNSET BLVD

WALLACE

MASON

12

3556  
 1045  
 140.50  
 7.19  
 150.07

110

15 22  
 27 22  
 199

FT 5  
 X

24+80  
 500

29+699

33+35

36+692

34+80

34+50

10+50

9+42

WALLACE

WALLACE

SUNSET

SUNSET

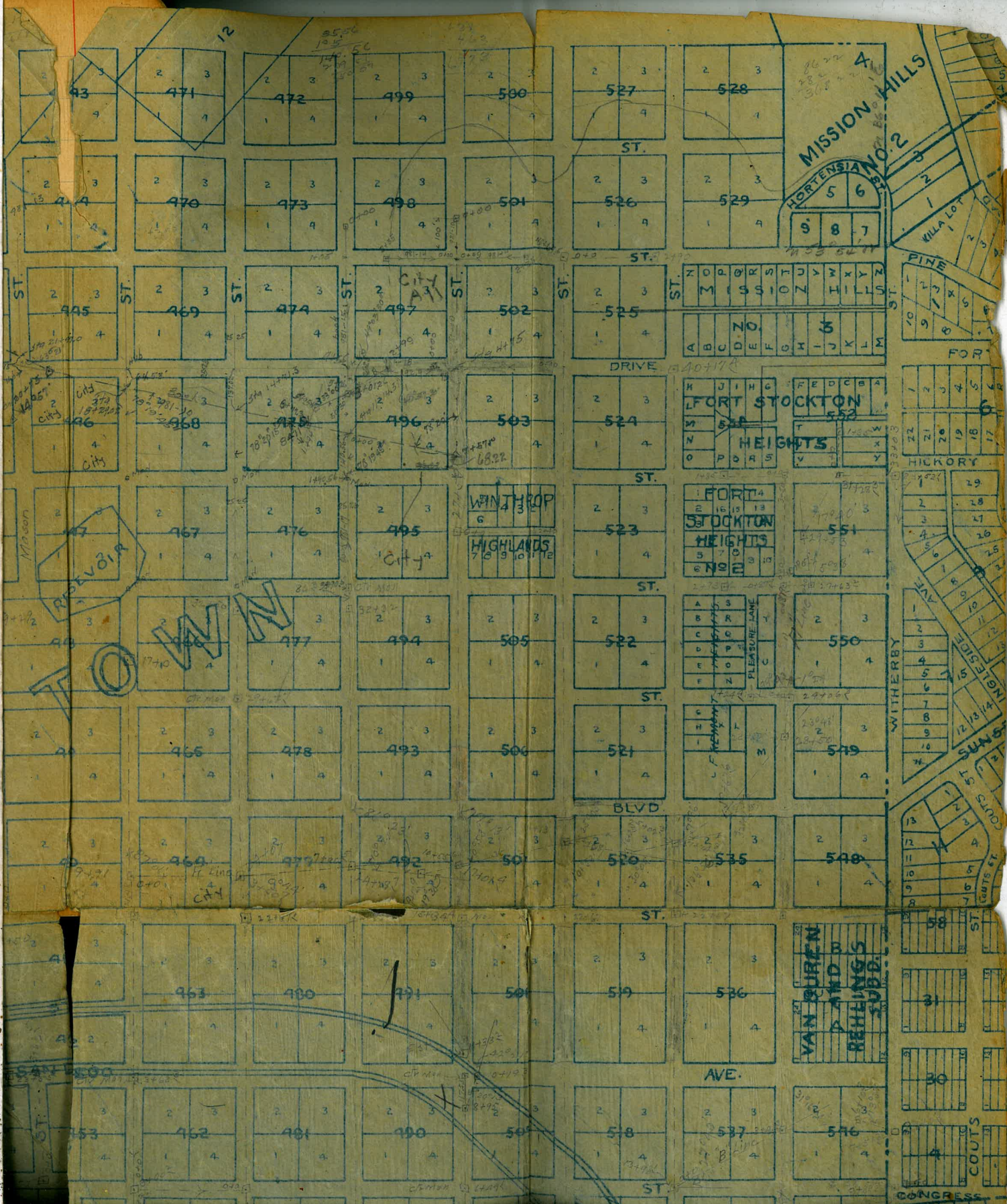
WALLACE

MASON









MISSION HILLS

HORTENSIA NO. 2

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

A B C D E F G H I J K L M

H J I G F E D C B A

ST. N O P Q R S T U V W X Y Z

TOWN

RESERVOIR

VAN BUREN AND BEHLINGS SUPP.

CONGRESS

COURTS

COURTS

COURTS

COURTS

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COURTS





for change in line  
see 1003-1003-31 5:44



2/2/25 Cooper Sower Construction & WHITMAN ST  
 X from & TRIPS TO & AMPUDIA ST  
 NEW Whitman St

2 TRIPS 20100	6.06 0.42	25507 245.96	953	24901 245.54	243.0	+5.49
+50			0.16	24581	239.21	+6.60
1			4.32	24164	235.49	+6.21
+50			8.41	23755	231.64	+5.91
2	0.75	233.91	12.80	223.16	227.85	+5.31
+50			4.50	22941	224.07	+5.34
3			8.55	225.38	220.29	+5.09
+50 & Ampudia			11.30	222.61	216.5	+6.11

SEWER CONSTRUCTION  
 & CHESNUT from & Ampudia to 185 East

2 Ampudia 20400					241.5	
		25297				
0 + 46.25	6.06	25507	5.44	247.53	242.9	+4.63
0 + 92.50			6.83	243.44	244.2	+4.14
1 + 38.75			5.72	249.35	245.7	+3.65
1 + 85			4.83	250.24	247.1	+3.14
2 + 31.25			4.02	251.05	243.5	+3.65

SEWER CONSTRUCTION  
 & HICKORY from & Ampudia to 185 E

2 Ampudia 20400		261.50			245.0	
+46.25			10.98	250.32	246.7	+3.65
0 + 92.5			9.07	252.73	248.75	+3.69
1 + 38.75			7.08	254.42	250.00	+3.80
1 + 85			5.12	256.33	252.50	+3.88
2 + 31.25			3.11	258.94	254.37	+4.02
2 + 77.50			2.49	260.01	256.00	+3.76

944

2557

350  
2557



Levels for "A" Line

B.M. Mon N.E. San Diego & Harney		33.26			3+0			12.0	59.2
M	12.70	45.96			+50	L <sup>o</sup> 44'		9.27	61.89
T.P.	12.02	53.90	4.08	41.88	4			3.9	67.3
O+O	R 87° 06'	12.30	60.01	6.19	47.71	750		1.3	69.9
+50			9.9	50.1	T.P.	11.97	82.06	1.07	70.09
1			8.5	51.5	5			9.5	72.6
+0.3			9.1	50.9	+50			6.9	75.2
+0.4			10.8	49.2	6			4.8	77.3
+1.5			11.9	48.1	+70			4.8	77.3
+2.0			11.8	48.2	+23			8.1	74.5
+3.0			6.9	53.1	T.P.	11.06	90.67	2.25	79.61
+5.0			5.4	54.6	+50			15.3	75.4
+5.7			9.6	50.4	+60			15.1	75.6
+7.6			8.2	51.8	+65			12.6	78.1
+8.3			1.6	58.4	+75			13.3	77.4
2			1.5	58.5	+82			10.2	80.5
T.P.	12.11	71.16	0.96	59.05	+100	R 10° 21'		9.13	81.54
+50			9.5	61.7	+70			8.3	82.4
+82			8.4	62.8	+75			9.9	80.8
+9.5			13.3	57.9	+50			8.2	82.5

Sheet 1

Sum of  
1/2  
1/2  
Bunker

71.16



		90.67		
8+0			6.5	84.2
+10			4.1	86.6
T.P.	12.06	100.32	2.41	88.26
+50			11.2	89.1
+55			13.2	87.1
+60			11.0	89.3
+85			10.7	89.6
+90			9.2	91.1
.9			8.6	91.7
9+12 <sup>9</sup>	L19030		7.4	92.9
+17			7.4	92.9
+20			8.7	91.6
+23			7.1	93.2
+50			5.1	95.2
+66			6.0	94.3
+69			4.4	95.9
+93			2.9	97.4
10+0			4.2	96.1
+08			2.5	97.8
T.P.	9.83	109.70	0.95	99.87

		109.70		
+50			7.4	102.3
+55 <sup>b</sup>	P0°53'	113.36	9.09	100.61
	12.75			
+60			14.0	99.4
11			12.2	101.2
+50			10.4	103.0
+89			8.6	104.8
+96			2.8	110.6
12			2.2	111.2
+27			0.3	113.1
+30			6.1	107.3
+40			5.7	107.7
+50			4.4	109.0
+63			5.0	108.4
+73			4.5	108.9
T.P.	10.67	123.68	0.35	113.01
13			8.0	115.7
+25			12.4	111.3
+35			12.2	111.5
+50			7.2	116.5
+69			3.9	119.8



13+80		123.68	7.2	116.5
14			7.1	116.6
+13 A	R25°05'		3.41	120.3
+35			2.1	121.6
T.P.	11.50	134.29	0.89	122.79
+50			16.7	117.6
+65			16.0	118.3
+88			7.0	127.3
15			5.6	128.7
+45			2.6	131.7
+50			6.5	127.8 ✓
+55			8.7	125.6
+87			5.3	129.0
16			3.6	130.7
+95			5.6	128.7
+25	∠ 30°04'	11.93	2.05	132.24
+30		144.17	12.2	132.0
+35			13.8	130.4
+40			11.0	133.2
+50			8.2	136.0

16+58		144.17	6.6	137.6
+73			8.2	136.0
+75			10.2	134.0
17			6.1	138.1
+07			5.7	138.5
+15			8.0	136.2
+29			4.3	139.9
+34			6.6	137.6
+50			6.0	138.2
+74 <sup>8</sup> ∠	7°36'	12.42	0.65	143.52
18		155.94	8.2	147.7
+08			8.9	147.0
+20			7.4	148.5
+25			5.4	150.5
+50			3.5	152.4
+75			5.2	150.7
19			2.7	153.2
T.P.	12.97	167.58	1.33	154.61
+20			11.6	156.0
+40			13.4	154.2



167.58				
194.50		16.0	151.6	
+67.6	$\Delta$ $L 32^{\circ} 06'$	6.1	161.5	
+98		4.3	162.3	
20		10.1	157.5	
+50		6.3	161.3	
+70		6.3	161.3	
+80		2.7	164.9	
21		1.2	166.4	
T.P.	12.33	178.84	16.7	166.51
+25		12.4	166.4	
+42		11.0	167.8	
+50		13.9	164.9	
+55		11.9	166.9	
22		10.2	168.6	
+05		11.0	167.8	
+25		4.1	174.7	
+50		1.2	177.6	
T.P.	11.24	188.96	11.2	177.72
+82	$\Delta$ $L 23^{\circ} 48'$		10.47	178.5
+94			15.2	173.8

188.96				
23+0			13.4	175.6
+25			9.3	179.7
+50			3.6	185.4
T.P.	5.40	194.21	0.15	188.81
+75			6.1	188.1
24			10.3	183.9
+06 <sup>3</sup>	$L R 1^{\circ} 24'$		10.44	183.77
+10			12.0	182.2
+15			10.0	184.2
+50			7.3	186.4
+60			10.2	184.0
+20			3.6	190.6
25+0			0.6	193.6
T.P.	10.52	209.17	0.56	193.65
+25			8.3	195.7
+50			9.0	195.2
+65			9.8	194.4
26			6.7	197.5
+20			6.4	197.8
+35			9.2	195.0



		204.17		
26+40			7.4	196.8
+50			6.6	197.6
+80			2.6	201.6
+92			5.1	199.1
27			4.9	199.3
+10			2.3	201.7
+25			3.5	200.7
T.P.	12.28	214.84	1.61	202.56
+50			10.3	204.5
+63 <sup>2</sup> Δ	L 5° 38'		8.28	206.56
28+0			4.0	210.8
+25			4.3	210.5
+50			2.6	212.2
T.P.	12.52	225.83	1.53	213.31
29+0			13.2	212.6
+30			12.2	213.6
+50			8.2	217.6
+53 A	R 17° 40'		7.9	217.9
+70			6.1	219.7
30+0			6.1	219.7

		225.83			9
30+23			5.1	220.7	
T.P.	12.43	238.12	0.14	225.69	
+50			11.8	226.3	
+80			7.4	230.7	
31+0			1.2	236.9	
T.P.	11.14	249.27	10.91	238.10	
+04			9.3	240.0	
+28 <sup>2</sup>	10-47 Highway	250.70	9.04	240.23	X
+50			10.4	240.3	
32			6.6	244.1	
+50			2.0	248.7	
T.P.	7.11	255.81	2.00	248.70	
33+0			3.4	252.4	
+03	Highway & Witterby		3.27	252.54	



Levels for Canyon Line "B"

Bush near S.W. Amphitheatre Congress	49.46		
12.58	57.04		
T.P.	12.44	69.21	0.27
			56.77
0+0 = Q Triassic Congress	1.95	67.3	
+10	1.2	68.0	
+35	1.2	68.0	
+50	2.8	66.4	
+60	3.4	65.8	
+95	2.0	67.2	
T.P.	12.13	80.69	0.65
1		9.8	70.9
+50		5.9	74.8
2		3.4	77.3
+27		2.2	78.5
+35		5.7	75.0
+50		5.4	75.3
T.P.	11.76	91.46	0.99
+70		13.9	77.6
+75		10.2	81.3
3		9.4	82.1

Sheet 1

21 Bunker  
153 Shaver  
15 Bunker

	91.46		
3+10		8.6	82.9
+30		3.9	87.6
+50		4.1	87.4
+94.3	4 Concordia 5 1/2 15+85 R 31° 16'	3.06	88.4
4		3.1	88.4
+20		3.0	88.5
+30		5.1	86.4
+22		2.3	89.2
+50		1.5	90.0
T.P.	12.78	102.91	1.33
			90.13
+60		12.2	90.7
+73		14.3	88.6
+90		11.0	91.9
5		11.7	91.2
+10		11.8	91.1
+35		7.5	95.4
+50		8.5	94.4
+64		9.5	93.4
+75		7.4	95.5
+84		8.0	94.9



	102.91		6.6	96.3
64.0				
+10 <sup>8</sup> R 13° 37'			3.8	99.1
+30			2.9	100.0
+35			4.9	98.0
+50			3.1	99.8
T.P.	12.23	112.10	3.04	99.87
+81			11.1	101.0
+85			9.0	103.1
7			7.6	104.5
+25			6.2	105.9
+29			8.6	103.5
+51 <sup>3</sup> E Weatherby 0512 21102			6.15	106.0



Levels of Witherby from Q Kurtz to Q Hickory <sup>Simple</sup> <sub>Plan</sub>

Level	From	To	12.54	12.61	12.61	12.61	12.61	12
B. M. No. 1	S. M. Hancock	W. W. Witherby			3+10		11.8	10.8
	2.07	12.61			T.P.	12.26	24.26	0.61
+00 = Q Kurtz			8.58	4.03	+50		11.6	12.7
+30			8.1	4.5	4		9.6	14.7
+31			7.3	5.3	+50		6.9	17.4
+50			6.4	6.2	5		4.3	20.0
+54			5.7	6.9	T.P.	12.47	36.58	0.15
+90			9.0	3.6	+50		12.5	24.1
1			9.9	2.7	+75		11.1	25.5
+20			10.2	2.4	+85		6.2	30.4
+32			3.4	9.2	+90 = 5 rail to J. L. P. R.		5.2	31.4
+35 = 7 rail str. Fe. Track			2.3	10.3	6		6.9	29.7
+45			4.0	8.6	+04		8.3	28.3
+50			6.4	6.2	+08		7.0	29.6
+60			11.4	1.2	+25		6.3	30.3
2			11.7	0.9	+50		2.8	33.8
+50			7.8	4.8	T.P.	12.33	48.85	0.06
+80			4.1	8.5	7		8.7	40.2
+86 = 4 rail pt. home str. Ry			2.5	10.1	T.P.	12.66	61.31	0.20
+98			2.6	10.0				
3			3.3	9.3	+50		12.3	49.0
					+70		2.5	58.8
					T.P.	12.36	73.67	0.00

Sheet 3



		73.67		
8+15			5.7	68.0
+50			5.1	68.6
+97			2.7	71.0
T.P.	12.46	86.06	0.07	73.60
9			9.3	76.8
+03			7.8	78.3
+25			3.8	82.3
+28			2.1	84.0
T.P.	12.47	98.37	0.16	85.9.0
+50			9.0	89.4
+75			1.6	96.8
T.P.	12.62	110.83	0.14	98.23
10			8.2	102.6
+25			1.4	109.4
T.P.	12.69	123.50	0.02	110.81
+50			6.8	116.7
T.P.	12.76	135.83	0.43	123.07
+75			12.3	123.5
11			5.8	130.0
+25			0.5	135.3
T.P.	12.36	147.92	0.27	135.56

		147.92		
11+50			5.4	142.5
+75			0.9	147.0
T.P.	12.56	160.12	0.36	147.56
12			8.8	151.3
+25			4.2	155.9
+50			2.4	159.7
	bet. Middletown & Middletown Add.			
+75	-20' south of Division Line,		0.46	159.66
	0+0=10' N of Division Line		2.30	157.8
+50			5.0	155.1
+75			10.5	149.6
T.P.	16.0	148.96	12.76	147.36
1			6.8	142.2
T.P.	0.24	136.23	12.97	135.99
+25			1.5	134.7
+50			9.5	126.7
T.P.	0.01	123.31	13.93	123.30
+75			4.6	118.7
2			13.1	110.2
T.P.	5.54	115.89	12.96	110.35

Sheet 2



		115.89			
2+107			9.94	106.0	
+16			10.7	105.2	
+25			6.4	109.5	
T.P.	11.79	127.12	0.56	115.33	
+50			9.2	117.9	
+75			1.6	125.6	
T.P.	12.83	139.43	0.52	126.60	
3			2.5	130.9	
+25			3.7	135.7	
T.P.	12.96	152.26	0.13	139.30	
+50			11.9	140.4	
+75			5.9	146.4	
4			1.2	151.1	
T.P.	12.54	164.63	0.17	157.09	
+25			7.3	157.3	
T.P.	12.49	176.85	0.27	164.36	
+50			11.3	165.6	
+75			4.3	172.6	
T.P.	12.34	188.95	0.24	176.61	
5			10.6	178.4	

		138.95			
5+25					3.3
					185.7
T.P.	12.31	200.62	0.64	188.31	
+50					3.8
					191.8
+75					2.6
					198.0
T.P.	12.71	213.29	0.04	200.58	
6					9.0
					204.3
T.P.	12.54	225.82	0.01	213.28	
+25					11.5
					214.3
+50					3.6
					222.2
T.P.	12.39	238.07	0.14	225.68	
+75					9.9
					228.2
7					5.3
					232.8
+25					2.5
					235.6
T.P.	11.45	249.33	0.19	237.88	
+50					10.8
					238.5
+75					9.3
					240.0
8					3.4
					240.9
+50					6.4
					242.9
9					3.1
					246.2
T.P.	11.90	260.51	0.72	248.61	



	260.51		
9.50		9.6	250.9
10		4.7	255.8
+50		1.5	259.0
T.P.	7.47	0.46	260.05
11		5.0	262.5
+50		3.4	264.1
12		2.3	265.2
+25		1.2	266.3
+50		5.4	262.1
13		6.8	260.7
+50		7.6	259.9
14		8.3	259.2
+50		8.4	259.1
15		8.8	258.7
+50		9.7	257.8
16		10.3	257.2
+50		10.9	256.6
T.P.	2.13	10.73	256.79
17		3.1	255.8
+50		3.6	255.3

	258.92		
18		3.9	255.0
+50		4.6	254.3
19		4.9	254.0
+50		5.4	253.5
20		5.4	253.5
+50		5.6	253.3
21		5.4	253.5
+50		5.1	253.8
22		4.6	254.3
+50		5.9	253.0
23		6.2	252.7
+50 - Hickory		6.38	252.54

15



Levels on ~~Concrete~~ <sup>Hartford</sup> St. from Q Kurtz north  
for 2850 to sta "H" line

B.M.	9.83	13.86	4.03
+0 to Q Kurtz		11.30	2.56
+50		11.9	2.0
1		9.8	4.1
+40		6.6	7.3
+46		4.0	9.9
+50		4.0	9.9
+55 - E. rail pt. lower st. RR		3.4	10.5
+63 - " " " " " "		3.6	10.3
+65 <sup>5</sup> - S. rail 3/4 E. RR		3.7	10.2
+70 <sup>8</sup> - N " " " " " "		3.9	10.0
+81		4.6	9.3
+87		2.0	11.9
2		0.7	13.2
T.P.	11.16	24.87	0.15
+72		10.3	14.6
+15		8.3	16.6
+50		8.3	16.6
3		9.3	15.6
+50		9.6	15.3

Sheet 4

	3+54 <sup>6</sup> = E. H. 2nd 18	24.87	9.8	15.1	16
4			9.3	15.6	
+50			9.1	15.8	
+60			10.4	14.5	
5			10.1	14.8	
+50			7.2	17.7	
6			4.4	20.5	
+50			1.1	23.5	
T.P.	12.88	37.63	0.12	24.75	
+96			11.9	25.7	
7			9.7	27.9	
+105			7.8	29.8	
+108 <sup>9</sup> - S. rail La Jolla R.R.			7.0	30.6	
+15			8.5	29.1	
+20			9.4	28.2	
+50			7.3	30.3	
9			3.1	34.5	
+25			1.1	36.5	
T.P.	12.60	50.12	0.12	37.52	
+50			9.5	40.6	



		50.12		
970			1.6	48.5
T.P.	12.48	62.58	0.02	50.10
+50			8.9	53.7
10			1.4	61.2
T.P.	11.60	74.08	0.10	62.48
+08			10.3	63.8
+50			9.0	65.1
11			6.7	67.4
+10			4.1	70.0
+17			0.0	74.1
T.P.	12.30	86.33	0.05	74.03
T.P.	12.40	98.71	0.02	86.31
+23			12.2	86.5
+50			6.5	92.2
+84			0.2	98.5
T.P.	12.39	110.86	0.24	98.47
12			10.7	100.2
+25			8.7	102.2
+50			4.5	106.4
+78			0.9	110.0
T.P.	6.24	116.56	0.54	110.32

		116.56		
1370			5.6	111.0
+10			4.5	112.1
+50			1.2	115.4
14+02 <sup>0</sup> - \$ Congress St.			2.2	114.4
+50			6.0	110.6
+50			12.5	104.1
T.P.	0.62	104.71	12.47	104.09
+25			7.4	97.3
T.P.	0.86	92.72	12.85	91.86
+50			1.9	90.8
+67			5.2	87.0
+72			9.0	83.7
+79			5.2	87.5
15+85 <sup>7</sup> - \$ 23+94 <sup>3</sup> B' Line			4.32	88.4
T.P.	12.49	105.68	0.03	92.69
16			12.5	93.2
+25			4.9	100.8
T.P.	12.26	117.82	0.12	105.56
+50			10.6	107.2
+75			4.2	113.6
T.P.	12.08	129.84	0.06	117.76



		12984		
1740			9.9	119.9
+25			5.9	123.9
+50			3.8	126.0
T.P.	11.92	141.28	0.48	129.36
+75			12.1	129.2
+75			14.9	126.4
+80			15.6	125.7
18			10.4	130.9
+13			3.2	138.1
T.P.	12.42	153.53	0.17	141.11
+25			11.6	141.9
+50			1.5	152.0
T.P.	11.89	164.90	0.52	153.01
+75			0.2	164.7
T.P.	12.07	176.91	0.06	164.84
19			0.1	176.8
T.P.	12.28	189.03	0.16	176.75
+25			0.6	188.4
T.P.	12.56	201.41	0.18	188.85
+50			7.4	194.0

		201.41		
2050			6.4	195.0
+50			5.7	195.7
21			1.0	200.4
T.P.	12.39	213.61	0.19	201.22
+50			6.9	206.7
22			0.3	213.3
T.P.	12.29	225.66	0.24	213.37
+50			6.6	219.1
T.P.	12.17	237.60	0.23	225.43
23			11.8	225.8
+50			6.9	230.7
24	cut 8'		2.2	235.4
T.P.	10.76	246.60	1.76	235.84
+50	cut 10'		4.2	242.4
25	cut 10'		3.2	243.4
+50			5.2	241.4
+75			9.2	237.4
T.P.	11.05	224.56	13.09	233.51
26			5.6	229.0
+25			8.2	226.4



		234.56		
76+50			12.2	222.4
T.P.	1.15	223.14	12.57	221.99
+75			11.7	211.4
T.P.	0.46	210.54	13.06	210.08
27			5.6	204.9
+25			12.1	198.4
T.P.	1.62	199.79	12.37	198.17
+50			4.2	195.6
+75			6.3	193.5
28			11.0	188.8
T.P.	0.65	187.73	12.71	187.08
+25			3.3	184.4
+50 = 50'22+82 "A" Line			9.24	178.47



Levels of Trias st from Kurtz North

21 Dunkle  
29 Shaw  
15 Bunde

B.M.	7.11	9.67	2.56
0+0 = Kurtz st.		12.01	- 2.34
+50	↓	11.1	- 1.4
1		11.9	- 2.2
+50		11.4	- 1.7
2		8.2	1.5
+12		4.4	7.3
+16 <sup>8</sup> - 5 rail 5/8 Fe. P.P.		1.4	8.3
+27		3.6	6.1
+34		1.1	8.6
T.P.	12.55	21.93	0.29 9.38
+50		10.8	11.1
3		3.0	18.9
T.P.	11.83	33.52	0.24 21.69
+50		9.4	24.1
4		5.5	28.0
+50		4.6	28.9
5		4.5	29.0
+50		4.7	28.8
6		5.7	27.8

Sheet 5

64.50		33.52	8.5	25.0	20
7			8.2	25.3	
+50			5.0	28.5	
8			2.1	31.4	
T.P.	12.23	45.15	0.65	32.87	
+50			10.7	34.5	
+58			11.1	34.1	
+56			9.3	35.9	
+86 <sup>7</sup> - 5 rail 1/2 Fe. P.P.			8.7	36.5	
+98			9.9	35.3	
9			8.5	36.7	
+50			5.5	39.7	
10			2.8	42.4	
T.P.	12.35	57.42	0.08	45.07	
+50			12.3	45.1	
+60			11.5	45.9	
+85			5.5	51.9	
11			5.2	52.2	
+50			3.4	54.0	
+80			4.1	53.3	



57.42

12.10			3.9	53.5
+35			3.8	53.6
+40			2.5	54.9
+50			2.2	55.2
+53			0.1	57.3
T.P.	12.01	69.33	0.10	57.32
13			4.6	58.7
+22			8.8	60.5
+24			11.6	57.7
+30			10.0	59.3
+50			7.8	61.5
+98! = \$ Compressor to "B" Line			2.07	67.3
14			2.0	67.3
T.P.	12.55	81.70	0.18	69.15
+50			10.0	71.7
T.P.	12.45	93.82	0.33	81.37
15			12.0	81.8
+25			6.4	87.4
+50			0.5	93.3
T.P.	12.52	106.07	0.27	93.55

106.07

15.75				6.7	99.4	21
16				1.0	105.1	
T.P.	12.37	118.33		0.11	105.96	
+25				6.7	111.6	
T.P.	12.49	130.82		0.00	118.33	
+50				12.4	118.4	
+75				6.7	124.1	
17				1.9	128.9	
T.P.	12.05	142.74		0.13	130.69	
+25				8.8	133.9	
+50				3.4	139.3	
T.P.	12.40	155.14		0.00	142.74	
+75				8.5	146.6	
18				1.4	153.7	
T.P.	12.42	167.34		0.22	154.92	
+25				5.7	161.6	
T.P.	12.37	179.50		0.11	167.23	
+50				11.0	168.5	
+75				1.8	177.7	
T.P.	12.41	191.68		0.43	179.07	



1940		191.68	2.3	189.4
T.P.	12.50	203.99	0.19	191.49
+25			5.9	198.1
+50			0.6	203.4
T.P.	7.36	211.11	0.24	203.75
+75			3.1	208.0
2040			1.7	209.4
+50			4.3	206.8
21			10.8	200.3
+30			13.2	197.9
T.P.	0.58	198.66	13.03	198.08
+50			4.9	193.8
+60			7.2	191.5
22			9.2	189.5
+50			11.6	187.1
+67 $\phi$ Jan 57			12.1	186.6
T.P.	1.20	188.16	12.40	186.26
23			3.0	185.2
+50			6.9	181.3
T.P.	0.22	175.47	12.91	175.25

2440		175.97	2.2	173.3
+10			2.5	173.0
+25			6.7	168.8
T.P.	0.22	162.88	12.81	162.66
+50			3.4	159.5
+75			9.6	153.3
+85			11.5	151.4
T.P.	1.36	151.45	12.77	150.09
+87			3.4	148.1
+94			11.5	140.0
2540			8.2	143.3
+0.2 <sup>3</sup> = 17474 <sup>3</sup> "A" Line			7.93	143.5
T.P.	11.97	162.96	0.46	150.99
+25			11.1	151.9
+50			2.3	160.7
T.P.	12.10	174.83	0.23	162.73
+75			4.1	170.7
T.P.	12.63	187.14	0.32	174.51
26			2.8	184.3
T.P.	12.36	199.06	0.44	186.70
+25			0.1	199.0
T.P.	12.31	211.08	0.29	198.77
T.P.	11.77	222.43	0.42	210.66



		222.43		
26750			6.1	216.3
T.P.	8.90	230.47	0.86	221.57
+61			6.2	224.3
+63	Hub 12.44	236.96	5.95	224.52
2740			9.3	227.7
+50			5.1	231.9
2840			0.9	236.1
T.P.	12.34	248.36	0.44	236.52
+50			8.5	240.4
2940			4.2	244.7
T.P.	9.80	258.10	0.56	248.30
+50			9.3	248.8
3040			9.3	248.8
+50			8.5	249.6
3140			7.7	250.4
+50			7.0	251.1
3240			6.5	251.6
+50			5.7	252.4
3340			5.0	253.1
+50			3.8	254.3

		258.10		
3440			2.6	255.5
+50			1.2	256.9
T.P.	12.50	270.49	0.11	257.99
3540			12.3	258.2
+50			11.0	259.5
36			9.8	260.7
+50			8.7	261.8
37			8.0	262.5
+50			7.3	263.2
38			6.3	264.2
+50			5.7	264.8
39			5.0	265.5
+50			4.3	266.2
40			3.8	266.7
40+17.2	FT Stockton		4.0	266.5



Levels on Lot Line BIK 488 from sta 8+73<sup>5</sup> Conde.

st no. sta 1+25 Arista st

B.M. 11.29 15.68 4.39

24

0+0 = sta 8+73<sup>5</sup> Conde st 11.3 4.4

+07 ↓ 12.6 3.1

+50 12.7 3.0

1 12.2 3.5

+50 11.6 4.1

2 9.4 6.3

+50 6.7 9.0

3 4.6 11.1

+49<sup>7</sup> = Arista 2.0 13.7

Sheet 8

1+70  
5

2+74  
10



Levels of Congress from Harney to Triggs

Point	San Diego	11.34	22.50
B.M. Harney	33.84		
T.P. Harney	27.00	4.5	22.5
+50		4.7	22.3
1		4.9	22.1
+50		4.9	22.1
2		5.1	21.9
+50		5.3	21.7
3+0		5.4	21.6
+50 <sup>2</sup> = Triggs		5.5	21.5

Sheet 9

Levels of Triggs from Congress south for 285'

Point	27.00	21.5
B.M. Congress	5.5	21.5
+25	5.1	21.9
+50	4.2	22.8
1	3.6	23.4
+50	3.6	23.4
2	3.7	23.3
+50	3.6	23.4
+85	3.7	23.3

Sheet 9



Levels of Ampudia from Kurtz North

Station	12.20	9.86	-2.34	3775	21.71	9.0	12.7	26
0+0 = Kurtz			8.83	1.03	470		3.9	17.8
+05	✓		8.8	1.1	T.P.	11.93	33.38	0.26 21.45
+12			11.1	-1.2	+50		8.5	24.9
+50			11.0	-1.1	5		5.1	28.3
1			10.6	-0.7	+50		4.7	28.7
+50			10.5	-0.6	6		5.2	28.2
2			9.8	0.1	+50		5.4	28.0
+14			10.3	-0.4	7		5.4	28.0
+20			11.5	-1.6	+50		3.7	29.7
+50			11.6	-1.7	8		1.7	31.7
+95			11.5	-1.6	+50		0.4	33.0
3			10.1	-0.2	T.P.	11.97	45.08	0.27 33.11
+10			4.2	5.7	9		11.7	33.4
+15 = s. 1/2 mile Fe R.R.			3.2	6.7	+50		11.3	33.8
+26			4.5	5.4	10		9.8	35.3
+32			7.0	2.9	+30		10.8	34.3
+44			6.5	3.4	+33		13.3	31.8
+50			3.8	6.1	+43		16.6	28.5
T.P.	12.76	21.71	0.91	8.95	+50		13.4	31.7

Sheet 6

9+90  
35  
10+10  
35  
10+11  
30  
10+44  
30



	45.08			
1140		11.4	33.7	
+30		10.0	35.1	11430
+50		6.6	38.5	
1240		4.1	41.0	11480 20
+05		4.1	41.0	
+10		7.7	37.4	12207 20
+18 <sup>8</sup> - 5 tail 1/2 Jolla R.R		7.0	38.1	
+44		7.0	38.1	12447 20
+50		3.7	41.4	
+75		3.9	41.2	
+76		9.2	35.9	
+85		10.3	34.8	12483 20
+94		7.8	40.3	12485 20 12494 20
1340		4.3	40.8	
+50		2.4	42.7	
1440		1.1	44.0	
+18		1.4	43.7	
+20		0.4	44.7	
T.P.	11.63	56.47	0.24	44.84
+50		12.5	44.0	

		56.47		
1540		11.8	44.7	27
+50		11.1	45.4	15222
16		9.4	47.1	
+50		2.6	53.9	16421 20
T.P.	12.32	67.91	0.88	55.59
+75		10.0	57.9	16437
1740		3.0	64.9	
T.P.	12.52	80.15	0.28	67.63
+75		9.5	70.7	
+50		1.3	78.9	
T.P.	12.70	92.68	0.17	79.98
+75		5.3	87.4	
T.P.	12.56	104.62	0.62	92.06
1840		7.4	99.2	
T.P.	11.81	116.31	0.12	104.50
+75		9.8	106.5	
+50	12.04	126.92	1.93	114.38
+75		0.7	125.7	
T.P.	12.57	138.77	0.22	126.20
19		0.8	138.0	
T.P.	12.66	150.93	0.50	138.27



		150.93		
19+25			3.2	147.7
T.P.	12.49	163.44	0.28	150.65
+50			6.7	156.4
T.P.	12.37	175.37	0.09	163.05
+75			12.2	163.2
20+0			5.8	169.6
+25			2.5	172.9
T.P.	11.87	185.99	1.25	174.12
+50			10.2	175.8
21+0			6.5	179.5
+50			5.3	180.7
22			3.0	183.0
T.P.	4.25	189.80	0.44	185.55
+50			3.9	186.9
+67 <sup>5</sup> $\phi$ Janu st			3.5	186.3
23			1.2	188.6
+50			4.7	185.1
+75			9.3	180.5
T.P.	0.11	177.23	12.68	177.12
24			5.4	171.8
+12			9.4	167.8
T.P.	0.71	165.07	12.87	164.36

		165.07		
24+23			5.6	159.5
+25			7.9	157.2
T.P.	0.50	152.70	12.37	152.20
+50			8.6	144.1
T.P.	0.26	140.20	12.76	139.94
+75			7.8	132.4
T.P.	1.58	128.97	12.81	127.39
+77			2.9	126.1
25+0			13.0	116.0
+04			11.9	117.1
+08 = 5 <sup>1</sup> / <sub>2</sub> 14+10 "H" line			8.67	120.3
T.P.	11.49	139.63	0.83	128.14
+25			10.1	129.5
T.P.	12.24	151.77	0.10	139.53
+50			11.7	140.1
T.P.	12.44	163.89	0.32	151.45
+75			11.5	152.4
26+0			0.7	163.2
T.P.	12.53	176.28	0.14	163.75
+25			2.7	173.6
T.P.	12.45	188.62	0.11	176.17



		188.62		
26450			8.2	180.4
+75			1.0	187.6
T.P.	12.31	200.92	0.01	188.61
2740			7.2	193.7
+25			7.1	198.8
T.P.	4.37	205.02	0.27	200.65
+50			2.9	202.1
+75			2.6	202.4
+85			3.9	201.1
2840			9.6	195.4
+06			12.0	193.0
T.P.	0.66	193.41	12.27	192.75
+10			4.1	189.3
+25			11.6	181.8
+34			14.7	178.7
+37			13.0	180.4
+50			3.8	189.6
T.P.	11.77	204.18	0.40	193.01
T.P.	11.80	215.90	0.08	204.10
+75			11.0	204.9
T.P.	11.73	223.86	3.77	212.13
8495Hul	12.87	232.04	4.69	219.17

		232.04		
2940			12.6	219.4
+50			9.9	222.1
3040			8.9	223.1
+50			4.2	227.8
31			0.3	231.7
T.P.	12.59	244.44	0.19	231.85
+50			9.0	235.4
32			5.1	239.3
+50			1.3	243.1
T.P.	9.97	254.23	0.18	244.26
33			7.7	246.5
+50			6.8	247.4
34			6.3	247.9
+50			6.0	248.2
35			5.8	248.4
+50			5.5	248.7
36			5.1	249.1
+50			4.4	249.8
37			4.2	250.0
+50			2.9	251.3
38			1.5	252.7
+50			0.6	253.6
T.P.	11.41	265.46	0.18	254.05

29



265.46

37+0			10.7	254.8
+50			9.7	255.8
40+0			8.8	256.7
+17			8.6	256.9
+30			5.8	259.7
+50			6.3	259.2
+88			7.5	258.0
41			7.3	258.2
+50			6.3	259.2
42			3.6	261.9
+50			0.8	264.7
T.P.	6.88	272.04	0.30	265.16
43			6.2	265.8
+50			5.5	266.5
+67 <sup>5</sup>	= Pine St		5.5	266.5

Levels of Pine St from Ampodia East for  
290 or 30 West of Trias St  
B.M. Brass Plg Ft Stanton 2 Trias 267.06

30

B.M. 8.05 275.14

0+0 = Ampodia St 8.6 266.5  
450 ↓ 7.7 267.4  
1 7.0 268.1  
+50 6.2 268.9  
2 5.5 269.6  
+50 4.9 270.2  
+90 4.7 270.4

Sheet 6



Levels of Aristo St from Kurtz North  
for

B.M.	8.27	9.30	1.03
0+0 = Kurtz		8.13	1.07
+07	✓	8.2	1.1
+12		10.8	-1.5
+50		10.3	-1.0
1		10.0	-0.7
+50		9.7	-0.4
2		8.8	0.5
+50		9.2	0.1
3		8.9	0.4
+50		9.7	-0.4
4		10.2	-0.9
+10		10.8	-1.5
+21		4.6	4.7
+26 = S. rail STE Fe R.R.		3.4	5.9
+37		4.7	4.6
+46		9.6	-0.3
+50		9.6	-0.3
+60		8.7	0.6
+68		9.8	-0.5
+70		10	-0.7

Sheet 7

	9.30			
5+20		8.7	0.6	5710=00 31
+56		1.2	8.1	5+38 5
T.P.	12.71	21.63	0.38	8.92
+65		9.2	12.4	5+56 10
+75		5.6	16.0	572 13
6+0		1.5	20.1	6+00 20
T.P.	8.40	29.61	0.42	21.21
+25		2.1	22.5	6+84
+30		3.8	25.8	25
+39 = Moore St		1.9	27.7	
Aristo St				
0+0 = 50 N. of Moore		3.9	25.7	
50		7.9	21.7	0+9 13 0+63 20
1+0		14.7	14.9	1+00 10
+25 = lot line		15.9	13.7	
+50		16.4	13.2	
2		16.4	13.2	
+40		15.0	14.6	
+50		14.0	15.6	2+64 10
3		8.2	21.4	2+88 20



		29.61		
3+25			5.2	24.4
+50			4.6	25.0
4			3.8	25.8
+50			3.5	26.1
5			3.6	26.0
+50			3.3	26.3
6+0			3.4	26.2
T.P.	12.25	39.35	2.51	27.10
+50			12.9	26.5
+72			13.0	26.4
+75			16.5	22.9
+90			16.0	23.4
+94			13.2	26.2
7+0			12.7	26.7
7+25			11.4	28.0
+50			11.9	27.5
+95			12.0	27.4
8			9.7	29.7
+05			7.2	32.2
4+2 S. rail La Jolla R.R.			5.9	33.5

				39.35				
8+30						6.9	33.0	32
+44						8.9	30.5	
+50						8.3	31.1	
+95	R	20° 13'				5.7	33.7	
9						4.8	34.6	
+50						1.6	37.8	
T.P.		11.95		50.25		1.05	38.30	
10						9.4	40.9	
+19	L	42° 21'				8.9	41.4	
+41						6.7	43.6	
+50						8.6	41.7	
+56	S. rail	S. D. E. R.R.				7.6	42.7	
+73						7.9	42.4	
+85						4.1	46.2	
11+0						2.9	47.4	
+33						1.1	49.2	
T.P.		12.66		62.23		0.68	49.57	
+50						11.7	50.5	
12+0						8.0	54.2	
T.P.		12.55		74.32		0.46	61.77	
7+25						11.9	62.4	



		74.32			
12+45			4.0	70.3	
+50			4.3	70.0	
+55			1.4	72.9	
T.P.	12.53	86.55	0.30	74.02	
+75			5.6	81.0	
T.P.	12.28	98.74	0.09	86.46	
13			5.8	92.9	
T.P.	12.48	111.23	+0.01	98.75	
+25			7.0	104.2	
T.P.	12.56	123.59	0.20	111.03	
+50			9.3	114.3	
T.P.	12.64	135.78	0.45	123.14	
+75			10.0	125.8	
T.P.	12.20	147.60	0.48	135.30	
14			11.7	135.9	
+25			5.6	142.0	
+50	cut 8'		2.3	145.3	
+75	cut 8'		1.7	145.9	
+79			3.6	144.0	
+83			1.3	146.3	

		147.60			
15+0			0.2	147.4	33
T.P.	3.54	150.99	0.15	147.45	
+07			3.2	147.8	
+10			4.2	146.8	
+15			2.6	148.4	
+34	Φ	Juan st	2.1	148.9	
+50			2.0	149.0	
+75			3.8	147.2	
16+0			11.7	139.3	
T.P.	0.76	139.02	12.73	132.26	
+25			10.7	128.3	
T.P.	0.56	126.82	12.76	126.26	
+50			7.7	119.1	
T.P.	0.82	114.97	12.67	114.15	
+75			8.0	107.0	
T.P.	7.26	710.13	12.10	102.87	
+85			10.0	100.1	
+93			10.0	100.1	
+95			11.3	98.8	
17+019 = sta 10+55	6" A' Line		9.52	100.61	
T.P.	12.01	122.06	0.08	110.05	



		122.06		
17+25			7.2	114.9
T.P.	12.02	134.83	0.05	122.01
+50			6.2	127.8
T.P.	12.55	146.44	0.14	133.89
+75			8.5	137.9
18+0			1.3	145.1
T.P.	12.68	158.76	0.36	146.05
+25			6.8	152.0
+50			1.7	157.1
T.P.	12.49	171.18	0.07	158.69
+75			7.1	164.1
T.P.	12.37	183.28	0.27	170.71
19+0			11.5	171.8
+25			7.7	175.6
+50			6.6	176.7
+75			1.1	182.2
T.P.	12.17	194.70	0.75	182.53
20+0			5.7	189.0
T.P.	12.20	206.58	0.32	194.38
+25			10.1	196.5
T.P.	10.62	216.32	0.88	205.70

		216.32		
20+50			8.5	207.8
+65	12.11	225.64	2.79	213.53
21			10.5	215.1
+50			8.9	216.7
22			7.4	218.2
+50			5.9	219.7
23			4.1	221.5
+50			2.4	223.2
24			0.4	225.2
T.P.	11.49	237.03	0.10	225.54
+50			9.9	227.1
25			8.0	229.0
+50			5.9	231.1
26			4.6	232.4
+50			3.6	233.4
27			2.8	234.2
+50			2.5	234.5
+59	Alley bet Chestnut & Hickory		2.6	234.4



Levels  $\Phi$  Alle-6<sup>t</sup> Chestnut 2410<sup>ry</sup> from  $\Phi$   
 Arista East for 240' or 85' west of Ampudia  
 237.03

35

040- $\Phi$ Arista of			2.6	234.4
+14	4		2.7	234.3
+15			1.8	235.2
+23			1.7	235.3
T.P.	11.75	247.10	1.68	235.35
+25			6.2	240.9
+50			5.3	241.8
1			3.6	243.5
+50			2.1	245.0
2			0.8	246.3
T.P.	8.24	254.84	0.50	246.60
+40			7.4	247.4

Sheet 7

✓



SEWER CONSTRUCTION

from ~~LA~~ F. Stockton to 113' 5" of Whitman

6 F. Stockton 172.25

261.50

249.25

10

233.91

884

225.07 220.07

36 + 5.00

486 256.64 252.5 + 4.14 + 50' of Whitman

1130

222.61 216.5

+ 6.11

+ 50 601 255.49 251.28 + 4.21 + 80.5 064 222.17 1238 221.53 215.75 + 5.78

1238

221.53 215.75

+ 5.78

1 708 254.42 250.09 + 4.35 11+ 23' break

232

219.85 215.0

+ 4.85

+ 50 832 253.18 248.85 + 4.33 11+ 68 ✓

272

101

210.65 197.91

1222

11.75

862

209.93

198.90

191.29 189.0

+ 2.29

2 932 252.18 247.64 + 4.54

+ 50 1052 250.98 246.43 + 4.55

3 1159 249.97 245.21 + 4.70

3.72 252.97

1225

249.25

1163

1050

11

+ 50 - @ Hickory Drop Mt. 3.78 249.19 246.0 + 5.19

4 4.12 248.85 243.64 + 5.21

+ 50 4.55 248.42 243.28 + 5.14

5 4.83 248.14 242.93 + 5.21

+ 50 5.03 247.94 242.59 + 5.37

6 5.30 247.67 242.21 + 5.46

+ 50 5.70 247.29 241.86 + 5.41

7 - @ Chesnut 6.24 246.73 241.5 + 5.23

+ 50 9.10 243.57 237.82 + 5.75

13.14 241.87

0.38

241.49

8 1.70 240.19 234.35 + 5.82

+ 50 5.65 236.22 230.78 + 5.44

9 9.44 232.43 227.21 + 5.22

233.91

13.14

5.18

228.73

223.64

+ 5.09

+ 50



Levels of Conde st from Kurtz north.

Level	8.06	9.23	1	1.17		7.23			
B.M.					-5448		4.5	4.7	
040- $\phi$ Kurtz, st.			7.42	1.81	+50		5.2	4.0	
+07	↓		7.4	1.8	+59		8.6	0.6	
+25			9.6	-0.4	+62		7.7	1.5	
+35			8.0	1.2	+60		9.1	0.1	
+50			8.0	1.2	+05		9.5	-0.3	
1			8.8	0.4	+20		8.8	0.4	
+50			9.3	-0.1	+50		7.6	1.6	
2			8.9	0.3	+70		7.6	1.6	
+50			8.7	0.5	+50		7.5	1.7	
3+0			8.8	0.4	8+0		7.4	1.8	
+50			8.8	0.4	+50		6.6	2.6	
4+0	Sheet 8		8.4	0.8	+73 <sup>5</sup> Lot Line		4.84	4.39	
+50			8.1	1.1	9		2.2	7.0	
+80			8.0	1.2	T.P.	11.71	20.80	0.14	9.09
5+0			9.6	-0.4	+50		9.7	11.1	
+17			9.3	-0.1	10		6.0	14.8	
+23			10.5	-1.3	+50		4.2	16.6	
+30			4.5	4.7	11+0		4.0	16.8	
+36 <sup>8</sup> - 5 rail ste. Fe. R.R.			3.5	5.9	+13		4.5	16.3	

5+50  
8.2

6+01  
0.0  
6+12  
0.0

0+22  
0.0  
0+28  
0.0

1+40  
0.0  
1+62  
0.0

8+50  
1.0

9+37  
1.0

10+06  
1.5



	20.80			
11+16		5.8	15.0	11+16 10
+15		6.6	14.2	
+50		9.3	11.5	
+76		13.2	7.6	11+60 10
12+0		13.4	7.4	
+50		11.7	9.1	
13+0		6.9	13.9	12+59 10
+43		4.1	16.7	12+17 10
+50		6.0	14.8	13+49 10
+62		3.2	17.6	13+57 10
+98 <sup>2</sup> - Congress st		2.1	18.7	
14+20		1.8	19.0	
+27		0.3	20.5	14+55 20
T.P.	11.51	31.53	0.78	20.02
+50		11.2	20.3	
15+0		9.4	22.1	
+50		7.4	24.1	
+91		6.4	25.1	15+87 20
16+0		5.3	26.2	
+50		5.0	26.5	

	31.53			
17		3.9	27.6	38
+03		3.0	28.5	
+26		2.1	29.4	
+30		0.8	30.7	17+28 30
T.P.	12.56	44.00	0.09	31.44
+35 <sup>9</sup> S. rail La Jolla R.R.		12.1	31.7	
+46		12.5	31.5	17+50 30
+50		14.0	30.0	
+60		11.5	32.5	
+65		11.8	32.2	
+75		13.9	30.1	
+80		12.9	31.1	
18+0		12.5	31.5	
+50		10.4	33.6	18+19 35
19		7.8	36.2	
+17		6.7	37.3	19+19 40
222		2.9	41.1	
+48 <sup>5</sup> S. rail S.D.E. Ry		1.8	42.2	
+30		11.9	42.1	
+58		2.4	41.6	
T.P.	12.87	56.84	0.03	43.97



		56.84			
19469			10.8	46.0	
+75			9.7	47.1	
2040			4.0	52.8	
T.P.	12.76	69.49	0.11	56.73	
+25			9.9	59.6	
+50			0.8	68.7	
T.P.	12.68	81.89	0.22	69.21	
+75			3.7	78.2	
T.P.	12.70	94.53	0.06	81.83	
2140			7.2	87.3	
T.P.	12.56	107.00	0.09	94.44	
+25			10.6	96.4	
+50			1.2	105.8	
T.P.	12.56	119.31	0.25	106.75	
+75			4.7	114.6	
+90			1.4	117.9	
2240			2.0	117.3	
+06			2.6	116.7	
+50			2.7	116.6	
46.7 @ J200 ST			2.2	117.1	
T.P. N	2.99	122.19	0.11	119.20	

		122.19			
2340			2.6	119.6	39
+25			3.7	118.5	
+50			10.7	111.5	
T.P.	0.22	109.75	12.66	109.53	
+75			9.1	100.7	
T.P.	0.48	97.48	12.75	97.00	
2440			12.1	85.4	
T.P.	6.46	91.25	12.69	84.79	
+04			8.3	83.0	
+06			10.6	80.7	
+20			11.7	79.6	
+25			9.4	81.9	
+28 = 7+00 5" H line			9.71	81.5	
+32			9.2	82.1	
+50			3.3	88.0	
T.P.	12.73	103.64	0.34	90.91	
+75			8.8	94.8	
2540			0.6	103.0	
T.P.	12.56	116.13	0.07	103.57	
+25			6.6	109.5	



25450		116.13	2.8	113.3
T.P.	10.84	125.31	1.66	114.47
+75			10.2	115.1
+90			10.2	115.1
26+0			19.2	106.1
+09			7.7	117.6
+25			1.7	123.6
T.P.	12.44	137.70	0.05	125.26
+50			4.9	132.8
T.P.	12.05	149.67	0.08	137.62
+75			4.9	144.8
T.P.	12.66	162.17	0.16	149.51
27+0			5.1	157.1
T.P.	12.77	174.31	0.63	161.54
+25			6.9	167.4
+41			0.7	173.6
T.P.	12.19	186.45	0.05	174.26
+50			11.9	174.6
+69			12.0	174.5
+75			10.1	176.4

28+0		186.45	1.3	185.2	10
T.P.	12.20	198.25	0.40	186.05	
+25			5.5	192.8	
+39			0.4	197.9	
T.P.	11.73	209.63	0.35	197.90	
+50			9.6	200.0	
29+0			4.4	205.2	
+15			4.3	205.3	
+22			2.9	206.7	
+25	4.6	12.01	2.32	207.31	
+50	cut 8'		10.2	209.1	
30+0	cut 8'		6.2	213.1	
+50			3.0	216.3	
31+0			0.8	218.5	
T.P.	10.06	228.86	0.52	218.30	
+50			2.3	220.6	
32'			7.4	221.5	
+32	cut 10'		6.0	222.9	



Sewer Construction in Chestnut St  
from 60' N.W. of N.W. Line of Witherby to E Trias

1/19/22  
miller  
Shaw  
C.W.  
2222

2+70  
1  
93  
77

41

B.M.	2.17	253.70		251.03	N.W. Hickory	
T.P.	0.14	241.45	12.39	241.31	Witherby	
00=60' N.W. of N.W. Line of Witherby						
T.P.	0.17	228.90	9.53	231.92	229.00	+ 2.92
			12.72	228.73		
0+50			2.75	226.5	219.85	+ 6.30
1+00						
T.P.	1.41	217.66	10.92	217.98	210.70	+ 7.28
			12.65	216.25		
B.K. 1+47.6			8.54	209.12	202.00	+ 7.12
M.H. 1+72.6						
T.P.	13.02	230.56	11.83	205.83	201.00	+ 4.83
			0.12	217.54		
0+51.5						
T.P.	12.68	243.09	8.14	222.42	218.00	+ 4.42
			0.15	230.41		
B.K. 1+03						
T.P.	11.63	254.29	3.55	239.54	235.00	+ 4.54
			0.43	242.66		
1+58.67						
CHK 1+93 = d Pleasure			8.28	246.01	238.00	+ 8.01
			8.81	245.48		
2+14.34					239.86	S.W. Cor Chestnut & Pleasure Lane
T.P.	10.32	261.16	2.93	251.36	241.00	+ 10.36
			3.45	250.84		
DE 2+70			6.68	254.48	244.0	+ 10.48
ChK on Eb			8.14	253.02		S.E. Cor Chestnut & Trias

Chestnut St. Construction.

103 N. of M.H. Trunk line on Chestnut	11.24	239.50	235.0	+ 4.50
148 W	7.41	243.38	237.43	+ 5.95
193 = M.H.	5.15	245.64	239.86	+ 5.78
231.5 W	3.54	242.27	241.93	+ 5.34
270 W = DE	2.44	244.0	244.0	+ 4.36
193 M.H. = 0+00 E. Chestnut & Pleasure Lane			239.86	+ 5.78

M.H. Hickory  
N.W. of Pleasure  
251.00  
3.88  
254.94  
4.30  
245.64  
5.15  
250.79



## PLEASURE LAKE SEWER

(HORTENSIA STN.)

42

52.5 W	753	247.41	241.72	+ 5.69
102.5 ✓	6.0	248.94	243.50	+ 5.44
152.5 ✓	439	250.55	245.28	+ 5.27
202.5 ✓	323	251.71	247.06	+ 4.65
252.5 ✓	178	253.16	248.84	+ 4.32
255 W = DE.	115	253.79	250.00	+ 3.79



Levels Harney St from Kurtz North

9.31

43  
6+59  
5

B.M.	7.50	9.31	1.81
0+0 = Kurtz St	6.88	2.43	
+07	6.9	2.4	
+20	8.8	0.5	
+25	7.8	1.5	
+50	7.6	1.7	
1	7.9	1.4	
+50	8.1	1.2	
2	8.3	1.0	
+50	9.1	0.2	
3	9.2	0.1	
+50	9.3	0.0	
4	8.9	0.4	
+50	8.6	0.7	
5	8.1	1.2	
+50	8.2	1.1	
6+0	8.2	1.1	
+32	9.5	-0.2	
+40	5.0	4.3	
+97.4 - Small Sta. Co. R.R.	3.6	5.7	

Sheet 9

3+20  
00

4+27  
00  
6+32  
00

6+44  
00

6+50			3.9	5.4	
+62			5.2	4.1	
+70			8.6	0.7	
+70			8.4	0.9	
+25	00		8.9	0.4	
+50	0+21		6.4	2.9	
T.P.	12.67	21.98	0.00	9.31	7+58 5
+75	0+50		12.3	9.7	7+70 10 8=15
8+0	0+75		7.0	15.0	
+25	1+00		3.1	18.9	8+36 20
+50	1+25		0.7	21.3	
T.P.	8.64	29.95	0.67	21.31	
9+0	1+50		7.2	22.8	
+50	2+00		6.3	23.7	
10+0	2+25		5.5	24.5	
+50	2+50		4.8	25.2	10+37 25
11+0	3+00		4.8	25.2	
+50	3+25		4.8	25.2	
12	4+00		4.8	25.2	
+50	4+25		5.3	24.7	12+20 25



2995

75+0			5.8	24.2
+50			7.3	22.7
14+0			7.6	22.4
+50			6.5	23.5
15+0			5.3	24.7
+50			4.2	25.8
16+0			3.0	27.0
+50			1.4	27.6
T.P.	12.36	41.78	0.33	29.62
17			11.9	30.1
+50			10.0	32.0
+60 <sup>3</sup>	= 5 tail 1/2 J & 1/2 P.R.		9.7	32.3
18+0			8.7	33.3
+50			6.2	35.8
19+0			4.0	38.0
+50			1.2	40.8
+80 <sup>6</sup>	= 5 tail 1/5 D.E. Ry.		0.0	42.0
T.P.	12.40	54.37	0.01	41.97
20+0			11.5	42.9
+50			8.3	46.1

15+14  
2616+98  
3017+34  
3519+36  
40

54.37

21+0			4.4	50.0
+50			0.5	53.9
T.P.	10.71	64.67	0.41	53.96
22+0			6.3	58.4
+50			2.9	61.8
+67 <sup>5</sup>	= Juan St		2.15	62.52
+78			5.4	69.6
23+0			2.0	73.0
T.P.	6.33	80.54	0.30	74.21
+25			3.4	77.1
+50			2.3	78.2
475			9.1	71.4
T.P.	8.01	76.58	11.97	68.57
+90			11.9	64.7
24+0			15.3	61.3
+07	= 3+507 H Line		14.69	61.9
+12			11.9	64.7
+25			10.0	66.6
+59			5.7	70.9
24+75			1.9	74.7
T.P.	12.45	88.84	0.19	76.39

44



		88.84			
7540			8.1	80.7	
+25			2.8	86.0	
T.P.	12.25	100.82	0.27	88.57	
+50			7.6	93.2	
T.P.	12.44	113.18	0.08	100.74	
+75			12.3	100.9	
2640			5.5	107.7	
T.P.	12.37	125.51	0.04	113.44	
+25			9.9	115.6	
+50			2.0	123.5	
T.P.	12.11	137.50	0.12	125.39	
+75			6.2	131.3	
T.P.	12.26	149.48	0.28	137.22	
2740			10.9	138.6	
+25			2.0	147.5	
T.P.	12.44	161.49	0.43	149.05	
+50			5.1	156.4	
T.P.	12.46	173.65	0.30	161.19	
+75			6.9	166.8	
T.P.	10.07	182.92	0.80	172.85	

		182.92			
2840			5.7	177.2	45
+12 <sup>3</sup>	12.00	192.12	2.80	180.12	
+50			10.4	181.7	
2940			6.5	185.6	
+50			0.9	191.2	
T.P.	12.45	203.98	0.59	191.53	
3040			5.2	198.8	
T.P.	12.36	215.84	0.50	203.48	
+50			11.2	204.6	
3140	cut 8'		10.1	205.7	
+50			9.3	206.5	
3240	cut 9'		7.4	208.4	
+07			7.4	208.4	
+20			2.0	213.8	
+50	cut 12'		2.1	213.7	



1/17/24 Grappt. from Sta 27+63.2 To 31+28.2  
page 9

GRADE  
B.P. Hack  
+ With

	0.46	251.49		251.03			
31+28.2 = d Hickory			11.30	240.19	234.0	+ 6.19	
31+03.2	1.36	241.55	10.61	240.88	230.87	+ 10.01	
30+53.2	0.11	229.10	11.30	240.19	228.99		
			12.56	225.94	224.58	+ 1.36	
30+03.2			3.16	220.39	218.29	+ 2.10	
29+53 M.H. Δ 17° 10'			8.71	218.88	212.0	+ 6.88	
	0.73	217.45	10.22	216.72	210.25	+ 2.75	
29+05.55			4.45	212.25	206.50	+ 5.75	
28+58.10			5.20	210.41	203.75	+ 6.66	
28+10.05			7.04	205.83	201.0	+ 4.83	
27+63.2 M.H. & Chestnut			11.62				

7 1/2 3 4 5  
2.43 2.7  
6.29



Levels of Whitman from sta 24+06<sup>3</sup>" H' Line west for  
124.8' to ♀ Pleasure Lane thence north on pleasure to  
sta 4+10

B.M.	12.35	196.12		183.77
0+0 = sta 24+06 <sup>3</sup> " H' Line			12.4	183.7
+25	✓		0.5	195.6
T.P.	11.64	207.36	0.40	195.72
T.P.	12.33	219.28	0.41	206.75
+50			10.2	209.1
T.P.	11.83	230.49	0.62	218.66
+75			6.9	223.6
T.P.	12.41	242.57	0.03	230.46
+98			7.6	235.3
1+0			7.7	235.2
+24 <sup>4</sup> ♀ Pleasure Lane			6.9	236.0
+50			6.4	236.5
2			5.1	237.8
+50			3.7	239.2
3			2.0	240.9
+50			0.2	242.7
T.P.	5.23	247.92	0.18	242.69
4			3.8	244.1
4+10			3.5	244.4

Sheet 1

Levels of Chestnut from sta 27+63<sup>2</sup>" H' Line west for  
273

B.M.	12.93	219.49		206.56
0+0 = sta 27+63 <sup>2</sup> " H' Line			12.9	206.6
+25	✓		7.4	212.1
T.P.	11.93	231.01	0.41	219.08
+50			8.8	222.2
T.P.	11.99	242.92	0.08	230.73
+75			10.5	232.4
+127 <sup>2</sup> ♀ Hartenoid	12.14	248.75	6.31	236.61
+138			6.4	242.4
+150			2.8	246.0
+173			0.9	247.9
+173			0.0	248.8

Sheet 2



Levels  $\Phi$  Hortensia from  $\Phi$  Chestnut to  $\Phi$  Hickory

B.M.	6.31	242.72		236.61
0+0 $\Phi$ Chestnut			6.3	236.6
+50			2.3	240.6
T.P.	11.68	254.07	0.53	242.39
1	✓		9.7	244.4
+50.			8.2	245.9
2			6.7	247.4
+50			5.3	248.8
3			3.2	250.9
+25			2.3	251.8
+26			5.4	248.7
+50 $\Phi$ Hickory			4.84	249.23

Sheet 2

Levels  $\Phi$  Hickory from  $\Phi$  Hortensia west for

135'				249.23	48
B.M.	11.81	261.04		249.23	
0+0 $\Phi$ Hortensia St			11.8	249.2	
+25		✓	11.5	249.5	
+50			10.2	250.8	
1			7.0	254.0	
+50			3.8	257.2	
+85			2.0	259.0	

Sheet 2

Levels  $\Phi$  Alley between Witherby & Hortensia from  $\Phi$  Hickory North for 135'

B.M.	10.78	251.01		240.23
0+0 $\Phi$ Hickory		✓	10.8	240.2
+14			11.5	239.5
+15			10.7	240.3
+40			9.6	241.4
+50			7.9	243.1
+63			6.0	245.0
+70			3.9	247.1
+35			2.4	248.6

Sheet 2



Levels of Triggs from Congress north

3/4  
1/2  
Beant  
Shaw

53.13

49

	27.00				64.50		11.3	41.8	
0+0 = Congress		5.5	21.5		74.0		8.2	44.9	
+50		5.0	22.0		75.0		4.8	48.3	
1		4.3	22.7		84.0		1.7	51.4	
+50		3.4	23.6		T.P.	7.28	59.41	1.00	52.13
2		1.9	25.1	1497 25	+50		7.6	51.8	
+50		0.1	26.9		+54		11.5	47.9	
T.P.	7.30	34.17	26.87		+85		10.7	48.7	
3		5.7	28.5		+90		8.0	51.4	
+50		4.2	30.0	3470 30	+90		8.4	51.0	
+62 = San Diego	11.56	41.17	29.61	CP. Mon 4.56	+10		7.4	52.0	
+85		9.6	31.6	2467 30	+10		8.9	50.5	
4+0		8.5	32.6		+50		13.4	46.0	
+50		7.2	34.0		+65		17.2	42.2	
5+0		5.8	35.4	1486 30	+75		17.7	41.7	
+50		3.8	37.4		+70		15.5	43.9	
+73		3.9	37.3		+75		12.9	46.5	
+84		5.3	35.9		+91 = 0.4 H. 4103		11.70	47.7	
489		4.9	36.3		10+0		11.1	48.3	
6+0		1.9	39.3		+150		5.9	53.5	
T.P.	12.61	53.13	40.52	6414 40	T.P.	12.75	71.74	0.42	58.99

Sheet 9



		71.74		
10+65			13.8	57.9
+75			8.7	63.0
+90			3.5	68.2
+94			5.8	65.9
11+0			4.3	67.4
+13			0.5	71.2
T.P.	12.41	83.92	0.23	71.51
+25			6.4	77.5
+50			1.7	82.2
+63			2.0	81.9
T.P.	12.27	95.64	0.55	83.37
+75			11.3	84.3
12+0			6.6	89.0
+07			6.5	89.1
+21			11.7	83.9
+25			6.3	89.3
+28			4.4	91.2
T.P.	12.59	107.96	0.27	95.37
+50			11.6	96.4
+75			5.8	102.2

		107.96		50
12+92			5.9	102.1
13+0			1.6	106.4
T.P.	12.38	120.09	0.25	107.71
+25			8.0	112.1
+50			2.1	118.0
T.P.	12.76	132.09	0.26	119.83
+75			8.8	123.3
14+0			3.9	128.2
T.P.	12.10	143.90	0.29	131.80
+25			10.6	133.3
+50			4.5	139.4
T.P.	12.15	155.66	0.39	143.51
+75			11.4	144.3
15+0			6.7	149.0
+25			5.5	150.2
+50			2.6	153.1
T.P.	11.30	166.59	0.42	155.24
+69 <sup>2</sup> $\phi$ Whitman			11.3	155.2
16+0			7.9	158.6
+50			4.0	162.5
17+0			3.0	163.5



Levels & Mason st from \$ Joun st north 929'

B.M.	2.13	49.84		49.71
T.P.	0.05	36.93	12.96	36.88
0+0 = \$ Joun	✓		10.6	26.3
+50			12.4	24.5
1			14.2	22.7
+50			15.4	21.5
2			15.9	21.0
+50 cut 6'			15.2	21.7
3+0 cut 10'			11.8	25.1
+50			9.8	27.1
4 cut 9'			4.3	32.6
T.P.	12.35	48.69	0.59	36.34
+50 cut 10'			10.7	38.0
5 cut 10'			4.7	44.0
+50			0.1	48.6
T.P.	11.93	60.55	0.07	48.62
6+0			9.9	50.7
+20			9.3	51.3
+38			10.2	50.4
+50			9.5	51.1
+75			1.6	59.0
T.P.	12.81	73.03 ✓	0.33	60.23

Sheet 11

73.03

6+99 \$ Whitman St	2.4	90.6		
T.P.	12.42	85.22	0.23	72.80
+25			0.5	84.7
T.P.	12.52	97.42	0.32	84.90
T.P.	12.19	109.62	+0.01	97.43
+50			11.7	97.9
T.P.	12.48	121.93	0.17	109.45
+75			9.3	112.6
T.P.	12.65	134.37	0.21	121.72
8+0			8.0	126.4
T.P.	12.28	146.04	0.61	133.76
+25			7.8	138.2
T.P.	12.64	158.07	0.61	145.43
+50			9.7	148.4
T.P.	12.35	169.93	0.49	157.58
+75			10.8	159.1
9+0			7.0	162.9
+29			0.6	169.3



Levels of Kurtz from  $\Phi$  Greenwood to  $\Phi$  Witherby

B.M. Mon Cor Juan & Wallace 14.41  $\frac{3}{15}$  <sup>sum</sup> <sub>Blank</sub>

	5.44	19.85		
T.P.	3.88	17.11	6.62	13.23
T.P.	3.46	8.58	11.99	5.12
T.P.	4.64	7.89	5.33	3.25
T.P.	3.92	6.50	4.81	3.08
0+0 = $\Phi$ Greenwood at		4.71	1.79	
+50		4.5	2.0	
1		4.8	1.7	
+50		5.3	1.7	
2		5.0	1.5	
+50		4.8	1.7	
3		5.1	1.4	
+49 <sup>8</sup> $\Phi$ Riley		4.82	1.68	
4		5.0	1.4	
+50		5.1	1.4	
5		4.6	1.9	
+50		4.5	2.0	
6		4.7	1.8	
+50		4.9	1.6	

Sheet 10

6.50  
6+99<sup>8</sup> =  $\Phi$  Gaines 5.79 0.71 52  
5.76 6.67

7+50	5.9	0.8
8	6.3	0.4
+50	5.6	1.1
9	4.6	2.1
+50	3.4	3.3
10	4.1	2.6
+49 <sup>8</sup> $\Phi$ Scott	4.30	2.37
11+0	3.4	3.3
+50	3.6	3.1
12	3.6	3.1
+50	3.6	3.1
13	3.5	3.2
+50	3.4	3.3
14	3.6	3.1
+49 <sup>8</sup> $\Phi$ Taylor	3.68	2.99
5.42 8.41		
+50	5.5	2.9
15	5.4	3.0
+50	5.5	2.9
16	5.7	2.9



16+50	8.41	5.8	2.6
17		6.0	2.4
+50		6.1	2.3
+99.7 $\Phi$ Wallace		6.23	2.18
18+50		6.6	1.8
19		6.6	1.8
+50		6.5	1.9
20		6.4	2.0
+50		6.4	2.0
21		6.0	2.4
+99.7 $\Phi$ Smith		5.96	2.45
	4.06		
22	6.51	4.1	2.4
+50		4.1	2.4
23		4.5	2.0
+50		4.4	2.1
24		4.7	1.8
+50		4.7	1.6
25+00 <sup>3</sup> $\Phi$ Mason		4.94	1.57
+50		5.0	1.5
26		5.5	1.0

+50	6.51	5.6	0.9	53
27		5.5	1.0	
+50		4.8	1.7	
28		5.0	1.5	
49 <sup>8</sup> $\Phi$ Triggs		4.77	1.72	
	5.25			
29+0	6.97	5.4	1.6	
+50		4.9	2.1	
30		4.8	2.2	
+50		4.9	2.1	
31		4.8	2.2	
+50		4.7	2.3	
32+0 $\Phi$ Harney		4.54	2.4	
+50		4.9	2.1	
33		5.0	2.0	
+50		5.0	2.0	
34		4.9	2.1	
+50		5.2	1.8	
35		5.2	1.8	
+49 <sup>5</sup> $\Phi$ Conde		5.1	1.9	
T.P.	3.87	5.76	5.08	1.89



5.76

86+0		4.2	1.6
+50		4.0	1.8
37		3.9	1.9
+50		4.2	1.6
38		4.0	1.8
+50		4.2	1.6
+99 <sup>2</sup> - $\phi$ <i>Arista</i>		4.5	1.3
39+50		4.7	1.1
40		4.5	1.3
+50		4.6	1.2
41		4.8	1.0
+50		4.8	1.0
42		4.7	1.1
+49 <sup>4</sup> - $\phi$ <i>Ampudia</i>		4.7	1.1
T.P.	2.20	3.36	4.70
43		2.4	1.0
+40		2.6	0.8
+50		3.4	0.0
+72		4.7	-1.3
44+0		4.9	-1.5

3.36

44+50		6.0	-2.6
45		5.7	-2.3
+50		4.9	-1.5
+99 <sup>2</sup> - $\phi$ <i>Thias</i>		5.70	-2.3
46+50		5.4	-2.0
47		5.7	-2.3
+50		5.5	-2.1
+50		5.1	-1.7
+50		2.9	0.5
48		2.3	1.1
+50		1.2	2.2
T.P.	6.57	8.55	1.38
49		5.2	3.4
+49 <sup>3</sup> - $\phi$ <i>Concordia</i>		6.0	2.6
50+0		5.8	2.8
+50		5.5	3.1
51+0		5.1	3.5
+50		4.9	3.7
52+0		4.6	4.0
+50		4.3	4.3
53+0		4.5	4.1
+49 <sup>4</sup> - $\phi$ <i>Wittherby</i>		4.5	4.1

54



## Levels &amp; Triggs from &amp; Kurtz North for 700'

B.M.	3.43	5.15	1.72
0+02 & Kurtz		3.4	1.8
+50		3.3	1.9
1		3.4	1.8
+50		3.8	1.9
2		4.2	1.0
+50		4.4	0.8
3		4.5	0.7
+50		4.8	0.4
4		4.9	0.3
+50		4.5	0.7
5		3.9	1.3
+50		3.6	1.6
6		3.2	2.0
+50		2.8	2.4
7+0		3.70	1.45

Sheet 3

## Levels &amp; Mason St from &amp; Kurtz North for 600'

B.M.	5.19	6.76	1.57
0+0 & Kurtz St		5.2	1.6
+10		5.1	1.7
+17		7.7	-0.9
+35		8.8	-2.0
+50		8.1	-1.3
1		7.3	-0.5
+50		6.5	0.3
2		6.1	0.7
+50		5.5	1.3
3		4.3	2.5
+50		7.8	2.0
4		4.7	2.1
+50		4.5	2.3
5		4.4	2.4
+50		6.0	0.8
+73		8.5	-1.7
6		8.2	-1.4

Sheet 3

55



Levels of Smith from Kurtz to Congress

B.M. 3.88 6.33 2.45

0+0 = Kurtz 3.9 2.4

+07 3.9 2.4

+20 6.9 -0.6

+30 5.7 0.6

+50 5.9 0.4

1 5.6 0.7

+50 4.6 1.7

2 4.5 1.8

+50 4.4 1.9

3 4.5 1.8

+50 5.2 1.1

4 4.9 1.4

+50 5.0 1.3

5 5.0 1.3

+50 5.0 1.3

6 4.9 1.4

+50 4.5 1.8

7+0 2.46 9.22 4.57 1.76

+50 7.2 2.0

Sheet 12

+18  
00  
+25  
00

9.22

2+0	7.2	2.0	8+2 00
+50	9.6	-0.4	8+90 00
.9	9.1	0.1	7+10 00
+50	9.6	-0.4	
10	10.0	-0.8	
+50	10.5	-1.3	
+85	10.7	-1.5	10+88 00
+98	4.2	5.0	10+98 5
11	4.1	5.1	
+04 side rail ste Fe RR	3.1	6.1	
+15	4.4	4.8	11+13 5
+30	9.1	0.1	11+30 00
+50	9.7	-0.5	
12	9.2	0.0	12+00 00
+50	8.4	0.8	
+55	7.2	2.0	
13	5.7	3.7	13+28 5
+30	4.1	5.1	
+50	0.9	8.3	
T.P. 11:30	19.80	8.50	12+69 10
+68		9.5	
+83		14.2	
+99 = Congress		14.3	



Levels of Congress St from  $\Phi$  Smith to  $\Phi$  Mason

1980

0+0 = $\Phi$ Smith	5.5	14.3
+50	4.6	15.2
1	4.0	15.8
+50	3.3	16.5
2	2.7	17.1
+50	2.3	17.5
3	1.7	18.1
+50 = $\Phi$ Mason	1.44	18.36

Sheet 12

Levels of Moore St from  $\Phi$  Smith East for 575'

B.M. 5.27 7.03 1.76

57

0+0 = $\Phi$ Smith	5.3	1.7
+47	5.9	1.1
+50	7.2	-0.2
+55	7.9	-0.9
+67	5.6	1.4
1	6.0	1.0
+30	8.0	-1.0
+50	7.6	-0.6
2	6.6	0.4
+50	6.8	0.2
3'	8.2	-1.2
+50	8.1	-1.1
4	9.3	-2.3
+20	4.4	2.6
+50	3.9	3.1
471	4.8	2.7
+75	3.8	3.2
5	4.6	2.4
+50	4.4	2.6
+75	4.8	2.2

Sheet 12

0+50  
00  
0+59  
00  
1+10  
00  
1+80  
00  
2+57  
00  
4+10  
00



Levels of Jefferson St from  $\Phi$  Smith E. for 550'

B.M. 3.51 9.60 6 6.09

0+0 =  $\Phi$  Smith 10.9 -1.3

+50 11.3 -1.7

+75 4.4 5.2

+83<sup>8</sup> - S. Rail St Fc R.R. 3.5 6.1

1 4.8 4.8

+05 5.3 4.3

+37 10.8 -1.2

+50 11.0 -1.4

+60 10.8 -1.2

+70 3.6 6.0

+95 11.3 8.3

T.P. 12.50 20.85 12.5 8.35

+76 9.4 11.5

+91 4.5 16.4

2+0 4.2 16.7

T.P. 7.89 27.58 11.6 19.69

+50 8.1 19.5

3 6.9 20.7

+50 6.2 21.4

4+0 5.4 22.2

+50 5.8 21.8

5 5.8 21.8

+50 6.2 21.4

Sheet 12

0+56  
00  
0+72  
5

0+97  
5

1+30  
00

1+62  
00  
1+69  
00

1+76  
10

1+87  
15

2+71  
20

Levels of Mason from  $\Phi$  Congress To  $\Phi$  San Diego Ave

B.M. 7.96 26.32 12.36

0+0 =  $\Phi$  Congress 8.0 18.3

+12 8.2 18.1

+50 7.1 19.2

1 7.3 19.0

+50 7.9 18.4

2 9.3 17.0

+50 8.5 17.8

3 5.8 20.5

+50 4.6 21.7

+62<sup>5</sup> =  $\Phi$  S.D. Ave 4.4 21.9

Sheet 12

2+91  
20



Levels for "C" Line - Line in  $\Phi$  of streets except  
 San Diego Ave which is 7' south of  $\Phi$   
 B.M. 6.23 8.41 2.18 <sup>(Wallace St)</sup> <sub>15' above</sub> <sup>Point</sup>

5.89

59

0+0 =  $\Phi$  Kurtz

+50  $\nabla$

1

+50

2

+50

3

+50

4

+50

5

+50

6

+50

7

T.P. 3.31

+50

8

+50

Sheet 12

6.2

5.7

5.5

5.9

5.5

4.9

5.2

5.2

5.2

5.1

5.1

5.0

5.0

5.0

5.5

5.89

3.0

3.3

3.3

2.2

2.7

2.9

2.5

2.9

3.5

3.2

3.2

3.2

3.3

3.3

3.4

3.4

3.4

2.9

2.58

2.9

2.6

2.6

9+0

+50

10

+17

+30

+50

11

+50

12

+20

+50

+85

+92

13

+35

+50

+50

T.P.

+53

+59<sup>5</sup>

5.69

9.31

Sixth St. E

3.7

3.8

3.6

4.0

5.8

5.6

5.3

5.1

5.0

5.4

6.6

6.5

7.6

7.5

8.6

6.6

2.5

2.27

4.4

3.5

2.2

2.1

2.3

1.9

0.1

0.3

0.6

0.8

0.9

0.5

-0.7

-0.6

-1.7

-1.6

-2.7

-0.7

3.4

3.62

4.9

5.8

11+50  
00

13+42  
00

13+50  
5



	9.31			
13470		4.2	5.1	13470 5
+85		9.5	-0.2	13485 60
1440 = $\Phi$ Congress		10.4	-1.1	
+50		10.0	-0.7	14470 60
15		8.5	0.8	
+37 <sup>5</sup> = $\Phi$ Wallace		8.4	0.9	
150		8.2	1.1	
16		7.7	1.6	
+50		6.9	2.4	
17		5.7	3.6	
+50		4.9	4.4	
18		2.8	6.5	17464 5
T.P.	10.93	18.63	1.61	7.70
+45			9.5	9.1
+50			8.0	10.6
				18488 10
+59		2.1	10.5	
+77 <sup>3</sup> = $\Phi$ Garden Place		6.2	12.4	
19		6.0	12.6	
+50		6.4	12.2	
+73 <sup>4</sup> = $\Phi$ Garden Place 16' E of W.L. Platz		4.7	13.7	
+88		3.4	15.2	19480 10
+88 <sup>7</sup> = 16' E of W.L. Platz 7' S of $\Phi$ S.D. Ave		4.8	13.8	19488 10

	12.63			
2040		3.4	15.2	19498 10 60
+15		4.3	14.3	
+50		3.8	14.8	
21		3.6	15.0	21400 10
+50		3.0	15.6	
T.P.	10.51	26.31	2.83	15.80
22		9.6	16.7	
+50		9.0	17.3	
23		7.5	18.8	
+55		5.8	20.5	23429 10



Levels of Fitch St from F Taylor to F Payne  
 Colours Mason

B.M. Men	Juan & Wallace	14.41	21.50	8.3	19.2
	5.31	19.72			
T.P.	7.97	14.62	13.97	6.65	9
0 to F Taylor		11.65	2.87		+50
+50		11.0	3.6		+62.7 = F Payne
1		10.5	4.1		
+50		9.9	4.7		
2		9.1	5.5		
+50		8.0	6.6		
3		7.0	7.6		
+50		6.1	8.5		
4		5.1	9.5		
+50		4.0	10.6		
5		2.9	11.7		
+50		2.1	12.5		
6		1.0	13.6		
+50		0.6	14.0		
T.P.	12.91	27.45	0.08	14.54	
7			12.3	15.2	
+50			11.2	16.3	
8			10.1	17.4	

Sheet 12

27.45

21.50	8.3	19.2
9	6.6	20.9
+50	4.8	22.7
+62.7 = F Payne	4.5	23.0

Mason Colours  
 Levels of Payne from F Fitch north for 250'

0 to F Fitch	27.45	4.5	23.0
+50		3.5	24.0
1		2.7	24.8
+50		1.5	26.0
2		1.3	26.2
+50		0.9	26.6

Sheet 12

61



Levels of Taylor St from Kurtz St north

B.M.	412	7.11	2.99
0+0 = Kurtz		4.1	3.0
+08	✓	4.4	2.7
+15		6.3	0.8
+20		5.3	1.8
+50		5.1	2.0
1		5.0	2.1
+50		4.8	2.3
2		4.7	2.4
+50		4.5	2.6
3		4.6	2.5
+50		5.7	1.4
4		4.6	2.5
+50		5.1	2.0
5		4.8	2.3
+50		4.5	2.6
6		4.6	2.5
+50		4.6	2.5
7		4.6	2.5
+50		4.3	2.8

Sheet 11

7.11

8+0		4.2	2.9
+50		4.1	3.0
9		3.9	3.2
+50		3.9	3.2
T.P.	4.93	8.29	3.75
10		5.0	3.3
+50		5.1	3.2
11		5.4	2.9
+50		4.3	4.0
12		5.4	2.9
+50		4.7	3.6
13		4.2	4.1
+50		4.6	3.7
14		4.7	3.6
+50		3.7	4.6
15		4.4	3.9
+09		5.0	3.3
+25		7.7	0.6
+50		6.6	1.7
16		8.0	0.3
+10		8.4	-0.1
T.P.	5.24	10.23	4.99

62

16+09  
00  
16+10  
00



10.23

16+30		5.2	5.0	16+30
+35 <sup>5</sup>	5. rail ste Fe RR	4.6	5.6	
+47		5.2	5.0	16+47
+50		6.0	4.2	
+65		9.6	0.6	
17		9.0	1.2	
+20		7.6	2.6	
+30		5.2	5.0	17+30
+35 <sup>3</sup>	5. rail La Jolla B.R.	4.1	6.1	
+45		4.2	6.0	
+50		6.2	4.0	17+48
+58		9.5	0.7	
18		9.5	0.7	
+50		9.5	0.7	
19		9.1	1.1	
+50		9.3	0.9	
+57		9.0	1.2	
+65		7.0	3.2	
+69 <sup>3</sup>	Calhoun 4 <sup>1</sup> / <sub>2</sub> st Mon 6.84 9.81	7.26	2.97	
+75		6.6	3.2	

9.31

+83		8.7	1.1	63
20		8.3	1.5	
+50		7.9	1.9	
21		7.1	2.7	
+50		7.5	2.3	
22		7.5	2.3	
+50		5.8	4.0	
+63		4.4	5.4	
23		4.7	5.1	
+50		4.9	4.9	
24		4.5	5.3	
+50		4.2	5.6	
25		4.1	5.7	
+50		4.0	5.8	
26		4.0	5.8	
+50		3.8	6.0	
27		3.8	6.0	
+50		3.7	6.1	
28		3.6	6.2	
T.P.	5.24 11.60 3.55	6.26		



	11.60			
28 <sup>150</sup>		5.1	6.5	
29		5.0	6.6	
+50		5.1	6.5	
30		4.9	6.7	
+50		4.9	6.7	
31		4.9	6.7	
+50		4.7	6.9	
32		4.5	7.1	
+50		4.2	7.4	
33		3.8	7.8	
+50		3.3	8.3	
34		2.5	9.1	
+50		1.9	9.7	
35		1.2	10.4	
+50		0.4	11.2	
T.P.	4.66	16.14	0.12	11.98
36		3.6	12.5	
+50		2.0	14.1	
+69 <sup>2</sup>	Mon & Hickory St.	1.9	14.2	



Levels of Juan St from  $\Phi$  Taylor to  $\Phi$  Mason

B.M.	7.77	10.74	2.97	
0+0 = $\Phi$ Taylor			5.2	5.5
+50			5.4	5.3
1			5.3	5.4
+50			4.9	5.8
2			4.3	6.4
+50			3.5	7.2
3			2.6	8.1
+50			1.5	9.2
4			0.7	10.0
T.P.	12.03	22.52	0.25	10.49
+50			11.6	10.9
5			10.6	11.9
+50			10.2	12.3
6			8.6	13.9
+50			7.4	15.1
7			5.7	16.8
+50			4.1	18.4
8+0			2.3	20.7
+50			0.5	22.0
T.P.	20.4	29.93	0.63	21.89
9			6.0	23.9
+50 = $\Phi$ Mason			3.6	26.3
+				

Sheet 11

Levels of Hancock from  $\Phi$  Witherby to  $\Phi$  Concordia

B.M.	21.39	17.49	15.10	Hortensia 65
0+0 = $\Phi$ Witherby			5.8	11.9
+50			7.0	10.5
1			7.5	10.0
+50			2.6	8.9
+78			9.3	8.2
2			2.6	8.9
+29			7.9	9.6
+27			2.4	9.1
+50			5.5	12.0
3			3.6	13.9
+50			3.1	14.4
+65 = $\Phi$ Hortensia <del>Concordia</del>			2.4	15.1



Levels & Wallace st from  $\Phi$  Juan to  $\Phi$  Chestnut

	Ben. man	Juan	2 Wallace		
	9.60	24.01	14.41		
010 = $\Phi$ Juan			10.4	13.6	
+50			11.7	12.3	
1			12.7	11.3	
+50			13.0	11.0	
2			14.1	9.9	
+50			15.1	8.9	
3			15.6	8.4	
+50			16.0	8.0	
4			15.9	8.1	
+50			16.2	7.8	
5			15.5	8.5	
+50			14.4	9.6	
6			12.7	11.6	
+50			9.0	15.0	
7			5.7	18.3	
+12			5.3	18.7	
+25			2.2	21.8	
T.P.	12.30	35.79	0.52	23.49	
+50			8.5	27.3	

Sheet 11

35.79

65

7-75			1.0	34.8
T.P.	12.39	47.70	0.48	35.31
8			6.3	41.4
T.P.	12.29	59.68	0.31	47.39
+25			11.1	48.6
+50 cut 10'			7.4	52.3
+75			1.8	57.9
T.P.	12.39	71.79	0.28	59.40
9 cut 10'			2.2	63.6
+25			3.6	68.2
T.P.	9.80	81.95	0.14	71.65
+50 cut 10'			9.4	72.1
10			6.5	75.0
+50 = $\Phi$ Chestnut			5.14	76.3



Levels of Rose Crans <sup>or Scott</sup> St from Kurtz north <sup>Sample</sup> <sub>Share</sub> <sub>Bump</sub>

B.M.	5.07	7.44	2.37	8+50
0+0 = Kurtz		5.1	2.3	9
+15	✓	5.7	1.7	+50
+50		5.6	1.8	10
1		5.2	2.2	+50
+50		5.0	2.4	11
2		5.5	1.9	+50
+50		5.0	2.4	12
3		4.7	2.7	+50
+50		4.7	2.7	13
4		4.5	2.9	+50
+50		4.6	2.8	14
5		4.5	2.9	+50
+50		4.3	3.1	15
6		4.2	3.2	+50
+50		4.0	3.4	T.P.
7		4.2	3.2	16
+50		4.5	2.9	+50
8		4.5	2.9	17
T.P.	5.27	8.38	4.33	3.11

Sheet 13

8.38

67

8+50	5.9	2.5
9	5.3	3.1
+50	4.4	4.0
10	5.2	3.2
+50	4.8	3.6
11	4.6	3.8
+50	4.7	3.7
12	4.9	3.5
+50	4.8	3.6
13	4.3	4.1
+50	4.5	3.9
14	4.9	3.5
+50	6.1	2.3
15	5.9	2.5
+50	7.0	1.4
T.P.	6.87	8.40
16	6.85	1.53
+50	6.6	1.8
17	6.4	2.0
+50	6.8	1.6
18	8.1	0.3



8.40

17+75	7.6	0.8
+85	3.8	4.6
+89 <sup>8</sup> = Srail La Jolla R.R.	2.8	5.6
18+0	3.9	4.5
+05	4.3	4.1
+08	7.2	1.2
+50	7.5	0.9
+92	7.9	0.5
19+0	5.0	3.4
+05	3.2	5.2
+11 <sup>4</sup> = Srail Ste Fe R.R.	2.3	6.1
+25	2.7	5.7
+34	5.7	2.7
+50	6.2	2.2
20+0	5.7	2.7
+50	5.4	3.0
21	5.7	2.7
+50	5.0	3.4
22	3.6	4.8
+50	3.3	5.1
T.P.	4.63	9.94
	3.09	5.31

9.94

23+0	6.6	3.3	68	
+50	5.1	4.8		
24+0	4.8	5.1		
+50	5.3	4.6		
25	4.6	5.3		
+50	4.7	5.2		
26	5.0	4.9		
+50	5.0	4.9		
27	4.6	5.3		
+50	4.4	5.5		
28	4.2	5.7		
+50	3.6	6.3		
29	3.7	6.2		
+50	3.8	6.1		
T.P.	5.60	11.92	3.62	6.32
30+0	5.1	6.8		
+50	5.1	6.8		
31	4.7	7.2		
+50	5.0	6.9		
32	4.9	7.0		



11.92.

32+50	4.6	7.3
+75 = S.L. Chest approx,		
33	5.1	6.8
+25	5.6	6.3
+35	4.9	7.0
+50	4.1	7.8
34	4.3	7.6
+50	4.4	7.5
35	4.3	7.6
+50	4.8	7.1
+85 S. line Dyke	4.3	7.6
	6.64	5.23

Levels of Gaines st from E Kurtz north

B.M.	6.24	7.35	0.71
0+0 = E Kurtz			0.8
+45		✓	6.6
			5.7
+50			4.2
+65			5.2
+88			6.7
1			5.4
+50			5.4
2			5.1
+50			5.0
3			5.0
+50			5.0
4			4.9
+50			4.7
5			4.3
+50			3.9
6			4.5
+50			4.9
7			4.5
T.P.	5.57	8.83	4.09
			3.26

Sheet 13

Dunkle  
Shaw  
B. 69



8.83

7+50		5.8	3.0
8		5.8	3.0
+50		5.6	3.2
9		6.1	2.7
+50		6.1	2.7
10		5.8	3.0
+50		5.8	3.0
11		5.4	3.4
+50		5.5	3.3
12		5.1	3.7
+50		4.9	3.9
13		4.9	3.9
+50		6.1	2.7
T.P.	3.09	6.02	5.90
14		3.0	3.0
+50		2.7	3.3
15		4.3	1.7
+50		4.7	1.3
16		5.3	0.7
+50		4.7	1.3

6.02

17+0			4.6	1.4
+50			3.4	2.6
18			3.9	2.1
+50			3.7	2.3
+65			4.5	1.5
+75			6.1	-0.1
19			2.3	3.7
+50			2.0	4.0
T.P.	7.34	11.48	1.88	4.14
20+0			7.1	4.4
+25			6.9	4.6
+32			4.4	7.1
+43 <sup>6</sup>	Strail La Jolla R.R.		4.7	6.8
+50			5.4	6.1
+60			4.5	7.0
+90			7.1	4.4
21+0			7.2	4.3
+10			7.3	4.2
+35			10.7	0.8
+46			10.7	0.8

70



	11.48		
21+50		9.3	2.2
+64		4.8	6.7
+68 <sup>7</sup> = 5.12 1/2 SE Fe. R.R.		3.8	7.7
+82		4.6	6.9
22+0		10.1	1.4
+23		9.3	2.2
+32		5.6	5.9
+50		4.9	6.6
+08 <del>15</del> 15+58		7.7	3.8
23+0		6.0	5.5
+50		5.9	5.6
24		5.8	5.7
+50		5.7	5.8
25		5.4	6.1
+50		5.4	6.1
26		5.6	5.9
750		5.6	5.9
T.P. 548	11.61	5.35	6.13
27		6.0	5.6
150		5.7	5.9

	11.61		71
28+0		5.8	6.1
+50		5.3	6.3
29		5.2	6.4
+50		4.7	6.9
30		4.9	6.7
+50		4.8	6.8
31		4.9	6.7
+50		5.1	6.5
32		5.6	6.0
+50		5.8	5.8
33+0		6.6	5.0
+35 S.L. Dyke		6.8	4.8



## Levels of Riley St from Kurtz north

B.M.	6.33	8.01	1.68
0+0 = Kurtz		6.3	1.7
+50	✓	6.2	1.8
1		5.9	2.1
+50		5.6	2.4
2		5.8	2.2
+25		5.5	2.5
+50		5.5	2.5
3		5.3	2.7
+50		4.9	3.1
4		4.9	3.1
+50		4.7	3.1
5		5.3	2.7
+50		4.8	3.2
6		4.7	3.3
+50		4.4	3.6
7		4.9	3.1
+50		4.5	3.5
T.P.	5.57	9.13	4.45
8+0		5.1	4.0

Sheet 14

3/19  
1/19  
1/15

	8+50	9.13	5.1	4.0	72
	9		4.7	4.1	
	+50		4.6	4.5	
	10		4.4	4.7	
	+50		4.4	4.7	
	11		4.9	4.2	
	+50		4.8	4.3	
	12		5.0	4.1	
	+50		4.4	4.7	
	13		4.6	4.5	
	+50		4.3	4.8	
	T.P.	1.90	7.28	3.75	5.38
	14		2.5	4.8	
	+50		3.4	3.9	
	+50		5.4	1.9	
	15+0		5.7	1.6	
	+50		6.2	1.1	
	16		5.9	1.4	
	+50		4.3	3.0	
	17		4.3	3.0	



		7.28		
17+50			4.8	2.5
18			4.3	3.0
+50			4.0	3.3
19			4.4	2.9
+50			5.4	1.9
20+0			3.4	3.9
T.P.	9.46	13.53	3.21	4.07
+50			9.2	4.3
21			8.7	4.8
+50			7.7	5.8
22			8.8	4.7
+50			8.2	5.3
+80			7.7	5.8
+88			4.8	8.7
23			5.3	8.2
+01 = s. rail La Jolla RR			4.6	8.9
+11			5.5	8.0
+15			4.3	9.2
+31			4.9	8.6
+44			9.0	4.5

		13.53		
23+50			9.1	4.4
+82			10.7	2.8
24			9.1	4.4
+06			9.4	4.1
+20			4.9	8.6
+26 <sup>0</sup> = s. rail sta P.R.R.			4.0	9.5
+38			4.6	8.9
+50			9.1	4.4
+85			6.0	7.5
25			6.9	6.6
+50			9.7	3.8
26			8.9	4.6
+50			8.4	5.1
27			8.1	5.4
+50			7.9	5.6
28			7.7	5.8
+50			7.5	6.0
29			7.9	5.6
+40			8.8	4.7
+50			10.0	3.5
+69 <sup>0</sup> = Whitman st.			9.5	4.0



Levels @ Greenwood at from @ Kurtz north

B.M.	5.79	7.58	1.79
0+0 = @ Kurtz		5.8	1.8
+15		6.0	1.6
+25		4.4	3.2
+50		4.7	2.9
+60		6.0	1.6
1		5.1	2.5
+50		5.1	2.5
2		5.2	2.4
+50		5.4	2.2
3		5.0	2.6
+50		4.7	2.9
4		4.7	2.9
+50		4.1	3.5
5		4.6	3.0
+50		4.3	3.3
6		4.0	3.6
+50		3.7	3.9
7		3.8	3.8
+50		3.8	3.8
T.P.			

Sheet 14

7.58

8+0			3.7	3.9	74
+50			3.5	4.1	
T.P.	4.88	8.93	3.53	4.05	
9			4.9	4.0	
+50			4.9	4.0	
10			4.9	4.0	
+50			4.8	4.1	
11			4.8	4.1	
+50			4.3	4.6	
12			4.0	4.9	
+50			4.1	4.8	
13			3.9	5.0	
+50			3.9	5.0	
14			4.0	4.9	
T.P.	5.46	10.54	3.85	5.08	
+36			5.9	4.6	
+50			7.9	2.6	
+70			9.6	0.9	
15			9.6	0.9	
+50			8.5	2.0	
16			8.4	2.1	







Levels of Chestnut st from  $\Phi$  Taylor to  $\Phi$  Jackson

B.M.	Mon	S.M.	Chestnut & Taylor	6.04	
	9.32	15.36			
0+0	= $\Phi$ Taylor		7.3	8.1	
+25		↓	8.7	6.7	
+50			8.5	6.9	
1			7.3	8.1	
+50			7.1	8.3	
2			6.3	9.1	
+50			5.2	10.2	
3			4.0	11.4	
+41			3.0	12.4	
+43			1.6	13.8	
+50	= $\Phi$ Jackson		0.7	14.7	

Sheet 11

Is this the N.L. or the  $\Phi$ ?

See Book 981, page 28 for continuation of this line

Levels of Whitman from  $\Phi$  Taylor East for 515'

B.M.			6.04	v76
	4.41	10.45		
0+0	= $\Phi$ Taylor		4.0	6.5
+50		↓	5.1	5.4
1			5.1	5.4
+50			5.5	5.0
2			5.7	4.8
+50			4.7	5.8
3			4.7	5.8
+50			4.2	6.3
4			5.1	5.4
+50			4.1	6.4
5			7.2	9.3
+15			+ 0.3	10.8

Sheet 11



Levels on production of  $\Phi$  Kurtz from  $\Phi$  Greenwood  
to San Diego river

13.M.	6.55	8.34	1.79	
0+0 $\Phi$ Greenwood			6.6	1.7
1+0			5.5	2.8
2+0			5.4	2.9
3+0			5.4	2.9
4+0			4.9	3.4
5+0			4.7	3.6
6+0			4.0	4.3
7+0			4.7	3.6
8+0			4.2	4.1
T.P.	3.47	7.94	3.87	4.47
9+0			4.2	3.7
10			4.8	3.1
11			5.0	2.9
12			5.3	2.6
13			5.4	2.5
14			6.0	1.9
15			6.3	1.6
T.P.	4.16	6.18	5.92	2.02
16+0			4.3	1.9

Sheet 10

	6.18			
17+0			4.8	1.4
18			4.9	1.3
19			5.0	1.2
20			5.2	1.0
21			5.3	0.9
22			5.3	0.9
T.P.	9.79	10.96	5.01	1.17
23+0			10.4	0.6
+47			9.6	1.4
+62			4.9	6.1
+85 = R 35° 00'			4.7	6.3
+94			9.4	1.6
24+0			9.8	1.2
25+0			7.4	3.6
+15			7.2	3.8
+20			7.4	1.6
26+0			9.7	1.3
+39: Top river bank			9.7	1.3
+44: River bed			17.7	-6.7

077



Levels Lot bet Guy & Juan from <sup>Hortensio</sup> Concordia  
 South for 300' or 25' N of Wetherby

B.M.				206.70
	12.36	219.06		
0+0 = Concordia			12.7	206.0
+50			8.4	210.7
1			4.4	214.7
+13			1.9	217.2
T.P.	12.48	231.22	0.32	218.74
+25			13.0	218.2
+50			8.7	222.5
2			4.2	227.0
T.P.	11.92	242.96	0.18	231.04
+25			14.4	228.6
+44			12.9	230.1
+50			11.5	231.5
+75			8.8	234.2
3+0 = 25' N of Wetherby			5.7	237.3

Levels of Guy St from <sup>Hortensio</sup> Concordia South for 300'

B.M.	2.66	209.36		206.70
0+0 = Concordia			14.3	195.1
+50			14.9	194.5
+77			14.9	194.5
1			11.9	197.6
+25			3.1	201.3
+50			4.6	204.8
+75			1.4	208.0
T.P.	12.12	220.86	0.62	208.74
2			11.2	209.7
+25			9.7	211.2
+50			7.2	213.7
+60			5.2	215.7
+75			3.7	217.2
T.P.	11.96	231.84	0.92	219.88
3			10.3	221.5

11.66 241.88 1.62 230.78  
 2.52 239.36

078



B.M. Brass Pkg. Rosecrans & Lytton

41.75

2.66 44.41

T.P. 0.05 32.52 11.94 32.47

T.P. 1.59 21.58 12.53 19.79

T.P. 1.09 10.24 12.43 9.15

end curbs in

T.P. 2.89 4.79 8.34 1.9

at Lytton & Tide

T.P. 1.10 4.91 4.08 0.81

at Post Mt.

5.15 -0.24

at F.L. Gulf Links

170/400 (0.235)

340 117  
600 72  
510 72  
900 16450

12715  
493

38.10

66

38100/263

8/66/80

76

64

240

20

128

120

114

38.10

80.66

73.69

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