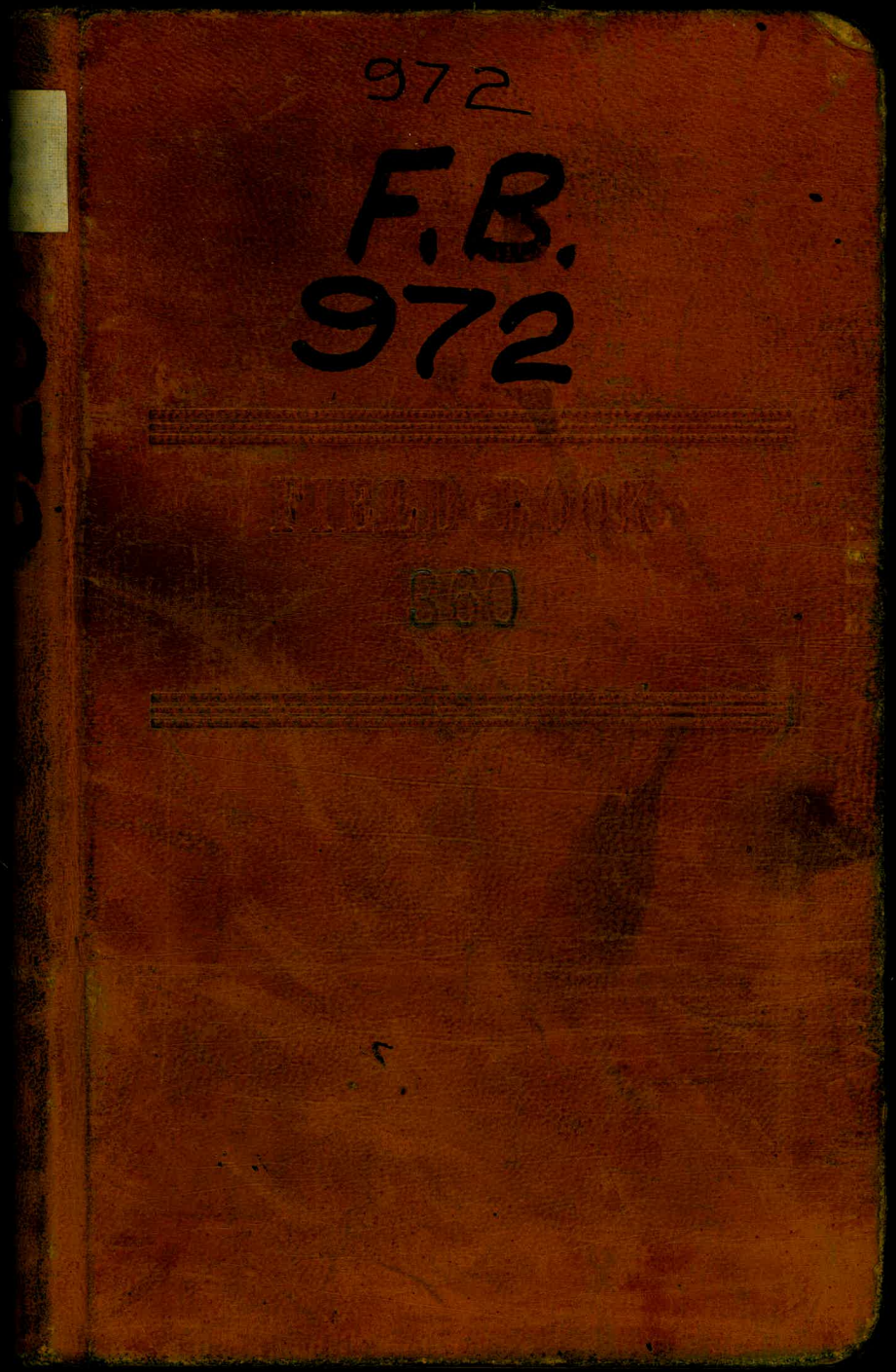
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F.B.
972
FIELD BOOK
360

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tabels see end of book.

All Notes in this book Copied into Book # 973

Bub HR Transit.
Nichols CL - Rod
Schoedsack LE - Rod.
Time June 17 to July 1
1915

Topog Survey Mission Valley

June 23

At Ridge Sight Sandy for zero Az Rt

NE Cor House 15x30	142	263°50'		✓
Fence Cor 1	95	302°40'		✓
" Cor 2	100	326°50'		✓
91 1	220	76°35'		✓
87 4	260	67°0'		✓
83 8	310	57°20'		✓
79 11	370	52°0'		✓
75 14	460	46°20'		✓
71 15	540	45°0'		✓
67 19	640	42°50'		✓
63 19	702	41°35'		✓
Ridge (B)	700	41°32'	3°6'	✓
County R	20'	00		✓

June 24 At Ridge-B- Sight Ridge for zero Az Rt

A in Fence 1	1300	67°26'	①	✓
63 ① RC	155	138°30'	①	✓
63 2 RC	207	226°15'	②	✓
63 3 RC	58	247°55'	②	✓
63 4 RC	283	194°20'	2	✓
Angle in F 3	750	78°10'	1	✓
59 23	295	179°55'	2	✓
L in Fence 4	537	91°35'	1	✓
L " " 5	460	98°0'	1	✓
55 25 Top Bank	487	96°30'	1	✓

At Ridge B

59 2R	425	97° 30'		✓	
Fence Cor 6	350	106° 5'		✓	
Casing 10" Well	282	115° 40'		✓	Ele 6234
Fence Cor 7	222	128° 30'		✓	
East end Water hole	280	124° 10'		✓	
West End Water Hole	370	107° 35'		✓	
55 26	320	180° 0'		✓	
Well 26 Private	175	105° 10'		✓	
59 24	564	244° 50'		✓	
55 27	565	244° 45'		✓	
Bott Bank North Side River 55 4R	885	107° 45'		✓	
59 1RC	780	108° 20'		✓	
T.B.N. 59 5RC	56R	138° 45'			West Side Murry Creek Junction San Diego "
B Bank N 55 41	570	139° 30'		✓	
Bott Bank N 55 37	535	144° 5'		✓	E side Murry Creek
Top Bank N 59 1RC	54R	144° 40'		✗	" " "
Bottom Bank 55 36	490	185° 30'		✓	
Top Bank 59 3RC	510	184° 0'		✓	
Ridge C	964	284° 49'	1° 3'	?	
Ridge D	48R	242° 18'	0 15'	✓	

At Ridge D Sight Ridge B Zero Az Pt

Ridge	48R	322° 36'	check	✓ ✗

At Ridge D Sight Ridge for Zero Az Pt

North Ridge 55 33	240	117° 40'	✓

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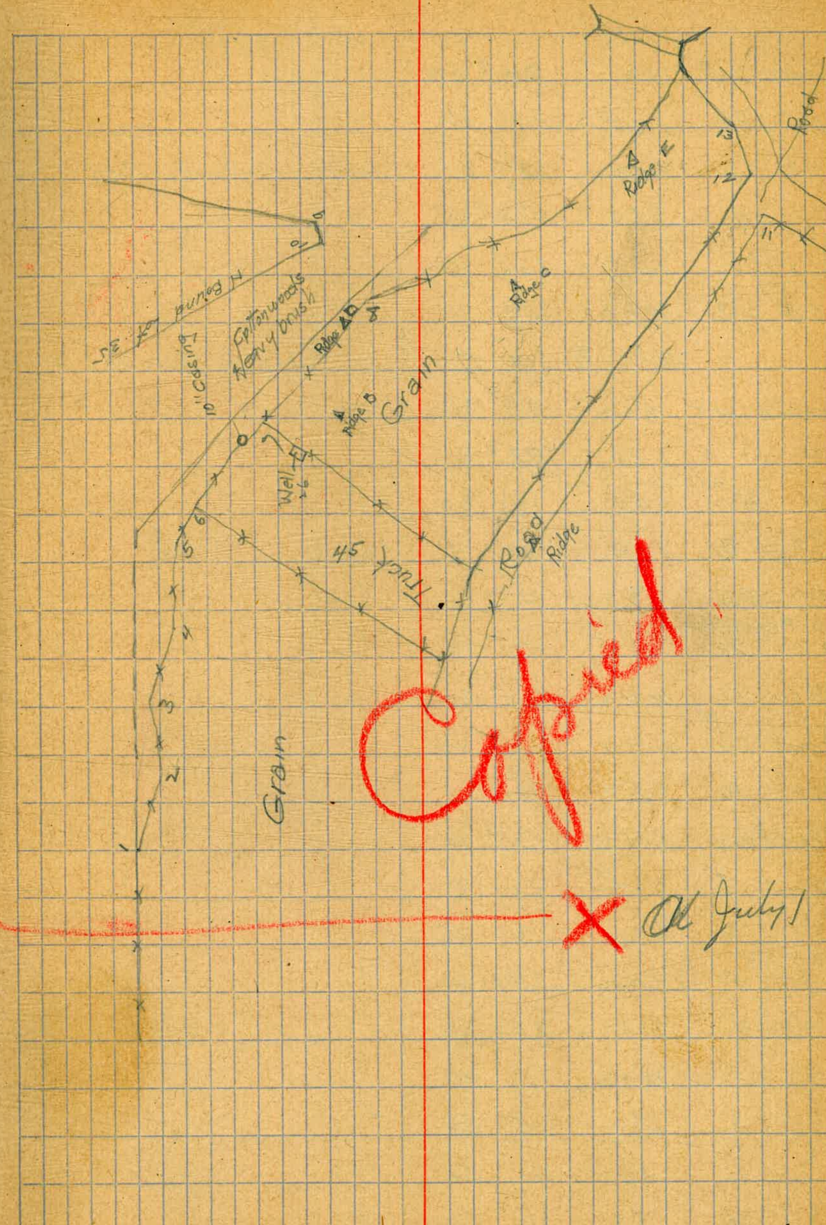

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X Ok July 1

		At Ridge D.			
Fence Cor 8	112	248°50		✓	
55 32	100	191° 50'		✓	
55 28	400	247° 0'	Center of River Bed		
55 30	385	234° 10'		✓	
55 31	167	225° 10'		✓	
55 29	550	249° 15'		✓	
	At Ridge C	Sight Ridge for Zero Az. Rd			
Fence Cor 9	610	93° 40'		✓	
" 10	620	92° 0'		✓	
59 5 North side	540	105 30	✓	✓	
Ridge B	964	40 25	Check	? OK	
59 25	390	93°30	✓		
on Fence Cor Bank 63 20	385	92° 25'	✓		
91 Y	425	185° 30'	✓		
Fence Cor 1	550	240 40	✓		
91 4	550	240 20	✓		
Fence Cor 11	550	235° 5'	✓		
91 3	487	239° 0'	✓		
87 6	430	230 40	✓		
on F. Line 87 5	330	284 20	✓		
83 9	265	284 10	✓		
79 17	167	283 40	✓		
75 13	68	275 50	✓		
71 16	40	141 50	✓		
67 20	120	171 50	✓		
63 21	247	116 10	✓		
on F Line					

Checked

480
180
96°

175

		AT Ridge C			
63 27	320	184 25			19
67 21	320	185 40			20
71 17	310	186 50			21
75 14	300	188 45			22
79 13	310	203 25			23
83 10	355	220 0			24
Ridge E	385	196°53	0 30'		25
		AT Ridge E Sight Ridge for Zero Az Rd			
Ridge C	385	12°20'	Check		
Bridge		129°22'	Check		
87 7	318	256 35			1
Fence Cr 13	315	255 30			2
83 11	300	244 30			3
79 14	295	214 35			4
South End Bridge & Road County	328	211 10			5
75	300	217 10			6
71	300	215 5			7
67	295	213 50			8
63	295	211 50			9
59	290	208 0			10
& Road County North End Bridge	478	147 70			11
59 1	455	152 20	Starting back on N Bank		12
59 1 RC	340	173 20	South Bank Top		13
59 2	280	163 10	N B.		14
59 2 RC	215	181 30	South Bank		15

Sta		Dist	Az At Ridge	V. Angle E		
59	3 RC	370	198 0	✓	S. Side	Island 16
59	3	185	161 40	✓	N Side	17
59	4	360	75 55	✓	" "	18
59	5	670	66 0	✓	" "	19
Fenceline		80	65 0	8° 30'	✓	20
59		100	65 0	7° 30'	✓ Bank	21
		At Bridge Sight Knot for Zero Az Rt				
Bridge	A	9	138°34		✓	
Bridge		9	318 40		✓	9K
Fence	Cr 1	37	315 30		✓	
63	1	35	343 30		✓	
F.	Cr 2	590	714 15		✓	
F.	Cr 3	230	22 10		✓	
59	8	475	250 40		✓	1
67	~~1~~	~~1130~~	29 30		✓	(2)
59	7	776	284 20		✓	1
Fence	Cr	~~1170~~	~~30 15~~		✓	2
59	9	760	293 20		✓	1
		1210	25 15			2
Fence	Cr 5	880	298 50		✓	1
59	10	1200	25 30			2
F.	Cr 6	880	305 30		✓	1
		~~1230~~	~~345 30~~			2
F.	Cr 7	900	316 10		✓	1
		~~1250~~	~~25° 45'~~			2

Checked

	1265	25 40			✓
Fence 8	960	326 30		✓	✓
63 ✓	1040	335 20		✓	✓
Angle in Fence	60 ✓	336 40		✓	✓
SE Cor P. House	660	342 30		✓	✓
House NE Cor Pump	680	245 50		?	✓
F. Cor 9	304	212 45		✓	✓
Bridge B	1250	314° 45'		✓	✓

At Bridge B Sight Bridge for zero Az R

Bridge A	1250'	0° 2'		✓	
Pump House	305'	279° 5'	SE Cor Pump House		✓
F. Cor 10	195'	215 20		✓	
59 11	65'	239 40	On Fence Line		✓
F. Cor 11	240	212 40		✓	
F Cor 12	380	231 30		✓	
F Cor 13	360	235 10		✓	
SW Cor Barn	425	245 50		✓	
SW Cor "	410	259 10		✓	
F. Cor 14	300	261 15'		✓	
Bridge C	700	217° 58'		✓	

at Bridge C Sight Gibson for zero Az to Pt

Bridge B	700	289° 32'	Check	OK	
59 12	150	260 15'		✓	
N W Cor House	225	220 54			

Point in old R channel

Corner

At Bridge C

East End Bridge	128	248 0'	Bridge over Murrey Creek
W End Bridge	100	245 35'	
59 13	260	180 50	
F Cor 15	50	226 10	
F Cor 16	50	330 0	
T Cor 17	145	338 30	
55 40	125	326 20	W side M. Creek
55 39	105	258 20	
55 38	322	334 30	E side M Creek
59 6	325	333 10	" " " "
59 15	250	177 35	
59 16	25	332° 10'	
59 17	442	112° 30'	
Stand pipe	490	104° 20'	
Well	485	101° 10'	See Huston for Number
59 18	690	94 10	
55 54	715	91 55	
F Cor 18	750	93 10	
Test Well 6	530	309 10	
F Cor 19	740	39 50	
Test Well 7	680	32° 0'	On Fence Line
F Cor 20	590	343 0	
Bridge D	668	346 22	

Corrected

At Bridge D Sight Gibson for Zero Az To Right

Bridge C	66	162° 55'	Check		✓ ok	
Knob		170° 27'	"		✓ ?	172° 35'
59 2 RC	145	299° 40'	E side NT Creek			✓
59 3 RC	380	270° 20'	E " " "			✓
59 4 RC	65	337° 0'	W " " "			
59 RC 1	280	228 10'	Check			?
Test Well 8	650	75° 30'				✓
59-2-R-C	580	45° 50'				✓
59-3 RC	700	73 45'				✓
Bridge E	300	270° 58'				✓

At Bridge E Sight Bridge D for Zero Az R

Bridge D	300	00			✓
55 34	195	168° 30'			✓
Water Hole	90	149 30'			✓
55 35	70	105 20'			✓

At Knob Sight Bridge for 0 Az R

Fence Cor 4	1216	332° 2'			✓
" " 71	1200	330 5'			✓
63 9	505	78 50'	10° 30'	496	✓
67 1	1240	332° 10'	4° 0'	1238	✓
71 1	1100	331 10'	4° 0'	1097	✓
75 1	1095	330 45'	4° 2'	1091	✓
79 1	1084	330 30'			✓
83 1	1080	330 10'			✓

Cupied

		At Knob				
87	1	1090	329 30			✓
91	1	1050	328 45			✓
63	3	570	71 25	-10° 0′	512	✓
67	2	655	337 40	-7° 45′	650	✓
71	2	660	336 50	-7° 15′	656	✓
75	2	670	335 40	-6° 45′	665	✓
79	2	675	334 40	-6° 25′	671	✓
83	2	680	334 5	-6° 0′	677	✓
87	2	690	333 20	-5° 35′	688	✓
91	2	700	332 35	-5° 10′	697	✓
Knob a		130	87° 14′	-15 0	125.5	
June 26		At Knob a		Sight Knob for Zero		At Rt.
F. Cor	23	363	69° 40′	-8° 0′	360	✓
Fence Cor	24	380	70° 0	-8° 40′	375	✓
"	" 24	350	64° 0	-6° 15′	348	✓
67	3	98	156° 0	-28° 15′	Edge Road North 86.3	✓
L in Fence	25	135	141 50	-26° 0′	121	✓
on Fence 71	3	95	158 50	-29° 30′	82.5	✓
F. Cor	26	180	204 45	-18° 45′	170.5	✓
63	4	190	204 40	-17° 10′	181.5	✓
75	3	88	159 10	-30° 30′	75.8	✓
79	3	80	160 30	-30 30′	69	✓
83	3	70	161 45	-30 25′	60.25	✓
87	3	63	162 0	-30 25′	54.4	✓
91	3	58	162 50	-30 25′	50.0	✓

Corrected

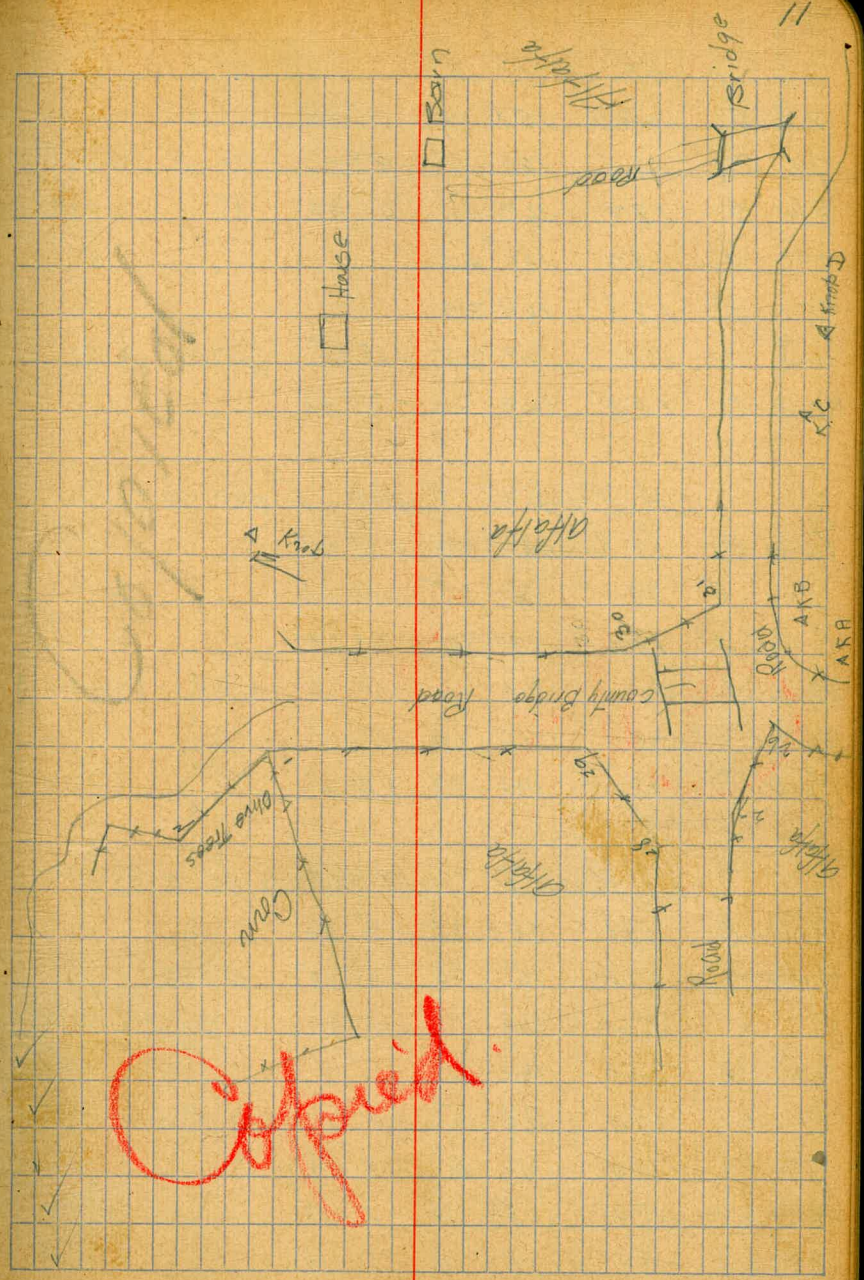
At Knob A

63 8	245	204 50	-13° 35'	238	✓
F Cov 27	260	195 0	-13 30	253	✓
59 14	210	195 10	-14° 15'	204	✓
F Cov 28	280	197 50	-10° 45'	275	✓
F Cov 29	300	213° 45'	-10° 45'	295	✓
County W End Bridge	250	215° 25'	-12° 15'	244.5	✓
F. Cov 30	300	221° 45'	-10° 45'	295	✓
Test Hole 5	250	212° 35'	-12° 50'	244.3	✓
County E END Bridge	210	214 50'	-15° 10'	203	✓
Bridge		89° 45'	Check		ok ✓
Knob B	108	248° 30'	-9° 30'	107.5	✓
Knob	132	00	+15° 30'	6' Rod	127.2 ✓

Checked

At Knob B Sight Ridge for Az Rt

Knob A	110	299° 7'	+9 35'	108.2	✓
63 7	228	141 30	-9 45'	224	✓
63 5	210	148 10	-10 40.	206	✓
91 4	25	75 40	-11° 0'	24.6	✓
87 4	35	71 0	-15 30	33.8	✓
83 4	50	68° 40'	-17° 45'	On Fence Line 47.7	
79 4	55	66° 45'	-20° 0'	Top Vert Bank 51.5	
67 5	205	150° 0'	-10° 0'	Edge Road 202	
67 4	70	68° 45'	-23 45'	Bott. Bank 64	
71 5	190	156° 0'	-8° 15'	Edge Road 188	



	At Knob B				
75 5	190	158 15	-7°45'	188.5	
79 5	185	160 15	-8°0'	On F Line	183
83 5	182	163 45	-5 30	181	
87 5	180	166 40			
91 5	178	169 40			
Private Well	170	6° 35'	-12°45'	Cement Pipe	165.6
Knob C	178	169 25	-3°45'		177.6
	At Knob C Sight Ridge for 0 Az Pt				
Knob B	178	349 59	+3°45'		177.6
67 5	282	167 25	-4°45'		281.
F. Cor. 31	180	27°20	-9°30'		177.5
P. House Allens	405	169°40	-2°30'	S.E. Cor Pump House	
Allen Well	382	168 40	-3°15'		381
Knob D	180	195.39	+4°0'		179.3
	At Knob D Sight Gibson for 0 Az. Pt.				
Knob C	178	354 35	-3°50'		177.5
W End Bridge	370	157 30	-5°15'	Allens	368
E. " "	360	162 50	-4°30'	" On F Line	358.5
63 6	350	162 0	-5°0'		348.5
91 6	170	164 15	-4°0'	on F Line	169.5
87 6	175	160 4	-4°45'		174.2
83 6	182	158 10	-5°15'		181.2
79 6	180	156 0	-7 15		178.5

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		Mt Knob D				
75	6	190	154 35	-7 15	9 R.	188.5
71	6	200	147 15	-7 30	On F Line 10' R.	
67	6	205	145 40	-9 30		202.0
SE Cor		770	113 10		Barn	
71	1	770	81 40			
75	1	780	81 40			
79	1	790	81 40			
83	1	800	81 50			
87	1	810	82 0			
67	3	880	55 10			
71	4	890	55 50			
75	4	910	56 0			✓
79	4	920	56 25			✓
83	4	940	56 55			✓
87	4	960	57°40'			✓
67	✓	750	73 10	Toe of Slope		✓
71	✓	775	74 20			✓
75	✓	800	75 15			✓
79	✓	815	75 30			✓
83	✓	830	75 55			✓
87	✓	855	76°10'			✓
87	3	820	69°50'			✓
83	3	805	69 45			✓
79	3	790	69 40			✓
75	3	780	69 30			✓
71	3	770	69 30			✓

148+6

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	At	Knob D			
Allens House	900	85° 9'		S.E Cor	✓
Knob E	1063	58° 28	00		✓
	At Knob	E Sight	Knob for Zero	Rz Rt	
Knob D	1065	343° 55			✓
Ridge		67° 0'	Check		✓
Gibson		92° 43	"		✓
F. Cor 1	118	76 30	-22 15	109.7	✓
63 10	355	76 30	-6° 50'	352.5	✓
Angle in F. 2	340	136° 5	-6° 15'	335.3	✓
59 19	970	114° 25		Red Edge of Com	✓
Knob F	785	141° 44	-3° 45'	781	✓
	At Knob F Sight				

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June 30 At Mary Sight Back for 0 Az Pt

Mary B	705	244 15		✓	
Mary A	840	42° 3'		✓	
~~St 51~~	Same as F Cor #1 ~~next page~~			✓	

At Mary B Sight Mary for zero Az Pt

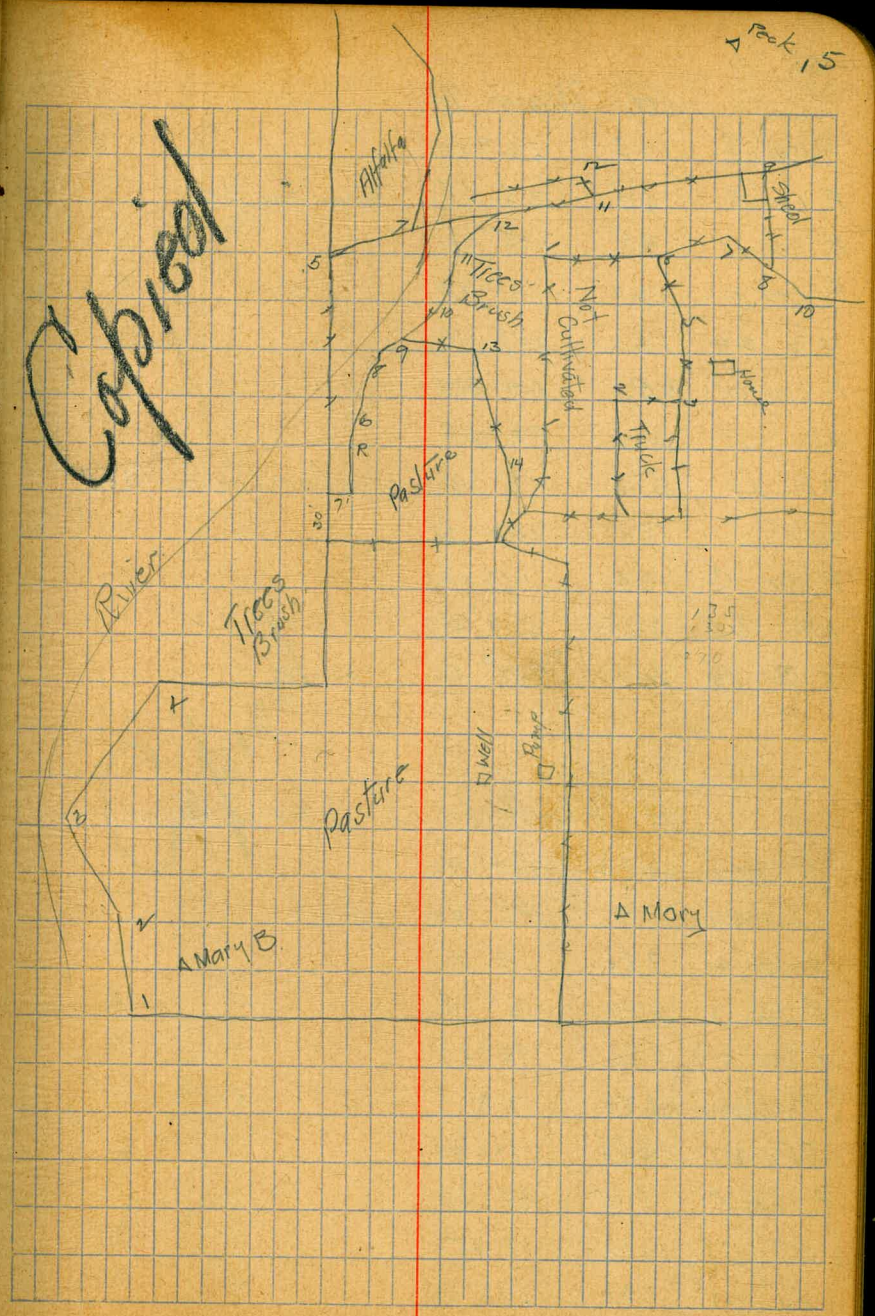
Mary B	705	00		✓	
F Cor 1	52'	88° 20'		✓	1
F Cor 2	105	264 0'		✓	2
F Cor 3	170	264 0'		✓	3
47 28	220	115 20	Top S Bank	✓	4
F Cor 4	250	277 20		✓	5
Mary C	622	271 36		✓	6

At Mary C Sight Boundry S for 0 Az To Pt

Mary B	625	209°27		✓	
47 29	440	214° 0'		✓	1
47 30	165	192 5		✓	2
47 31	290	100° 2'		✓	3
Mary D	568	97° 59'		✓	4

At Mary D Sight Boundry S for 0 Az Pt

Mary C	570	293 52		✓	1
Highway		282 20	Check		
F Cor 5	270	239 5		✓	2
F Cor 6	270	267 20		✓	3
F Cor 7	120	35 10		✓	4
47 RC	210	280 50		✓	5

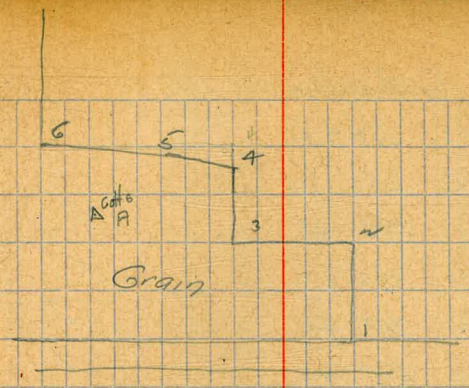


At Mary D

F Cor 8	145	259 10		6 ✓
F Cor 9	60	216 25	Taken from Mary	7 ✓
F Cor 10	98	138 40		8 ✓
F Cor 11	140	108 20		9 ✓
43 24	160	108 20		10 ✓
F Cor 12	260	107 30		11 ✓
A3 25	410	90° 50		12 ✓
43 23	385	85 20	Center Creek Bed	13 ✓
Well	180	164 25		14 ✓
F Cor. 13	130	188 10		15 ✓
47 36	375	208° 50		16 ✓
F Cor 14	315	200° 5		17 ✓

At Gottesburen A Sight Gottesburen for 0

F Cor 1	1084	134° 40	✓	1
Highway		93 24	Check ✓	
F Cor 2	780	112° 0'	✓	3
F Cor 3	670	116° 15	✓	4
F Cor 4	558	94° 35	✓	5
Gottesburen	1450	0 0	✓ (AP)	
55 67	385	77 40	✓	6
F Cor 5	330	68 30	✓	7
59 28	135	17 25	✓	8
63 21	170	273 20	✓	9
67 14	240	254° 5	✓	10



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At Gettesburen A

71	17	320	253 10	✓	11
75	17	355	251 35	✓	12
F. Cor	6	300	336 40	✓	13
79	17	390	250 30	✓	14
83	17	425	249 40	✓	15
79	18	620	209 40	✓	16
67	15	432	166 30	✓	17
75	18	540	200 30	✓	18
63	22	460	145° 18	✓	19
71	18	465	186° 30	✓	20
59	19	545	178 50	✓	21
55	68	640	119 10	✓	22

At Mary A Sight Mary for 0 Az Rf

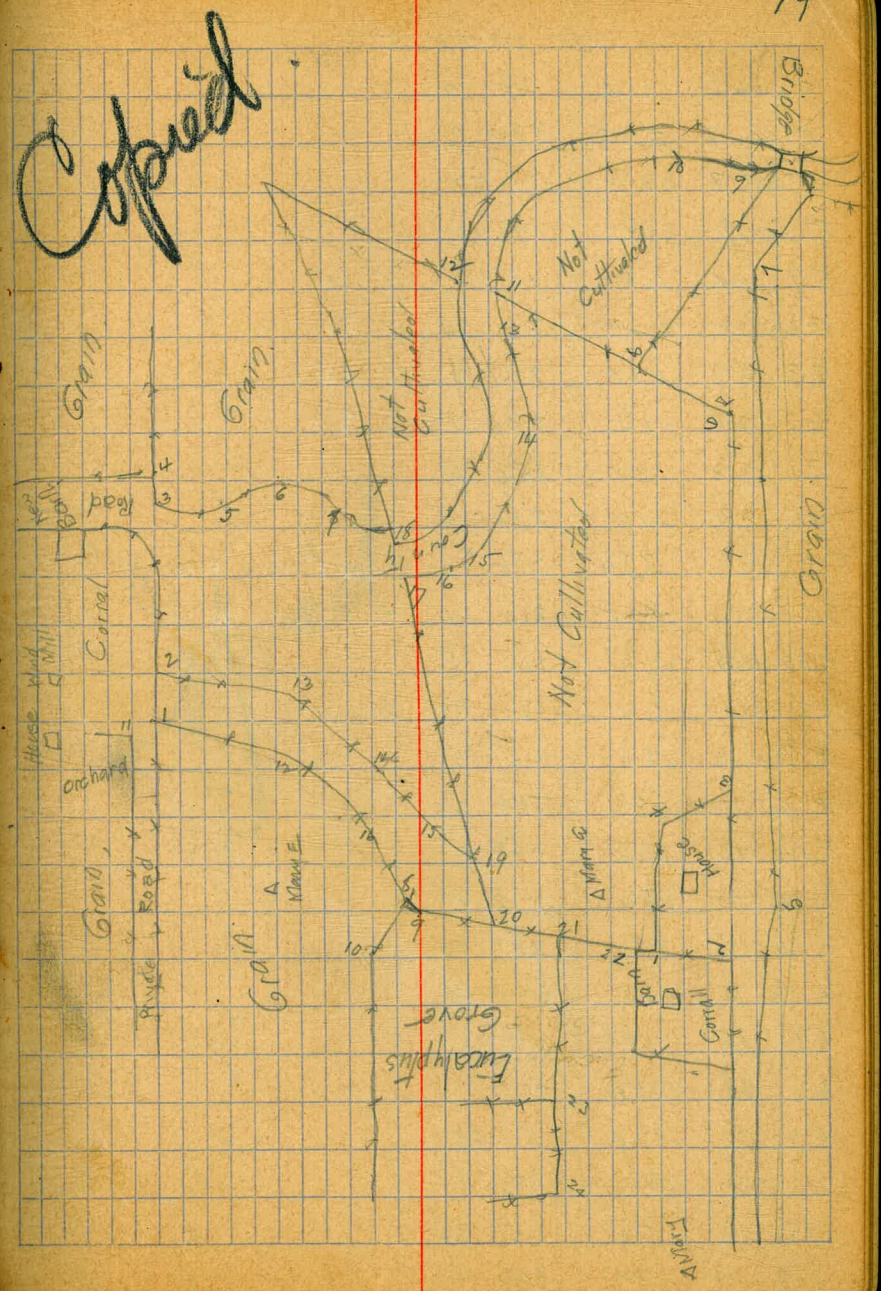
Well		322	333 30	Concrete 4x4	1 ✓
Fence Cor	22	235	331 0		✓ ✓
F. Cor	1	265	329 30		3 ✓
Mary	Δ	840	00		
F. Cor	2	440	325 30		4 ✓
F. Cor	3	390	271 20		5 ✓
F. Cor	4	275	276 15		6 ✓
F. Cor	5	420	270 15		7 ✓
71	19	470	270 10		9 ✓
F Cor	6	700	233 10		9 ✓
75	19	580	258 20		10 ✓

Copied

		At Mary A			
79 19	670	253° 10'		✓	11
F Cov 7	900	227 5		✓	12
79 20	895	243 45		✓	13
F Cov 8	760	220 50		✓	14
75 20	705	248 15		✓	15
71 20	590	254 30		✓	16
Center	1060	229 5	Bridge C. Road	✓	17
67 17	490	262 5		✓	18
F Cov 9	1025	227 0		✓	19
63 24	310	268 55		✓	20
79 21	920	227 55		✓	21
F Cov 10	960	223 0		✓	22
63 25	445	321 30	check	✓	23
F Cov 11	810	213 30		✓	24
F Cov 12	820	211 10		✓	25
67 16	405	298 35		✓	26
F Cov 13	765	211 20		✓	27
F Cov 14	655	209 5		✓	28
59 31	185	225 40		✓	29
F Cov 15	342	188 0		✓	30
F Cov 16	335	167° 50'		✓	31
F Cov 17	370	161 5		✓	32
F Cov 18	390	163 40		✓	33
59 33	275	142 5		✓	34
F Cov 19	262	135 30		✓	35

Offset

		At Mary A			
63 26	298	147 15		✓	36
F Cor 20	250	128 50		✓	37
67 19	308	151 10		✓	38
71 22	325	154 15		✓	39
75 22	342	157 10		✓	40
79 22	365	160 5		✓	41
63 25	265	180 0		✓	42
67 18	448	167 10		✓	43
F Cor 21	123	117 50		✓	44
71 21	590	219 10		✓	45
F Cor 23	520	36 35		✓	46
75 21	730	226 5		✓	47
F Cor 24	630	33 35		✓	48
59 32	230	150 0		✓	49
55	315	5° 0		✓	50
55	240	48 40		✓	51
Mary E	555	134 57		✓	52
		At Mary E Sight Gotesburen for 0 to A			
Mary A	555	14° 30'		✓	1
F Cor 1	215	232 55		✓	2
F Cor 2	268	238 40		✓	3
F Cor 3	362	244 40		✓	4
F Cor 4	390	246 0		✓	5
55 71	730	25 15		✓	6
F Cor 5	298	156 45		✓	7



		At Mary E			
F Cor 6	255	281 0		✓	8
F Cor 7	250	320 0		✓	9
F Cor 8	223	17 40		✓	10
F Cor 9	238	19 25		✓	11
59 34	168	1° 0'	6° 30'	✓	12
F Cor 10	220	30 50	6° 30	✓	13
63 27	120	325 20	6° 45	✓	14
67 20	115	296 10	6 30	✓	15
71 23	160	253 5		✓	16
75 23	210	239 35		✓	17
SE Cor	380	222 30	New Barn 40x30	✓	18
SE Cor	325	210 20	Old Barn 30x20	✓	19
Wind Mill	315	198 15		✓	20
NE Cor	315	191 30	House	✓	21
F. Cor 11	168	215 15		✓	22
F Cor 12	130	264 20		✓	23
F Cor 13	200	258 0		✓	24
F Cor 14	165	278 5		✓	25
F Cor 15	190	343 20		✓	26
F Cor 16	120	338 10		✓	27
59 35	165	11° 0'		✓	28
63 28	150	10 20		✓	29
67 21	120	8° 40		✓	30
71 24	90	7° 50		✓	31
75 24	70	359 20		✓	32
79 24	40	242 10		✓	33

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	At Mary E				
79 33	300	236 20		✓	34
79 25	360	98 45		✓	35
75 25	408	96 40		✓	36
71 25	435	95 40		✓	37
67 22	455	94 20		✓	38
63 29	476	92 50		✓	39
59 36	485	91 30		✓	40
55 22	520	90 55		✓	41
Knob		90 31	Check	✓	42
July 1	At Peck Sight Bound S for 0 Az Rt				
47 38	495	305 0		✓	1
F Cor. 1	522	304 30		✓	✓
47 37	682	287 55		✓	3
F Cor 2	580	286		✓	4
51 52	765	267 30	on F line	✓	5
Well	595	263 30		✓	6
Fence Cor 3	460	265 40		✓	7
SW Cor House	466	261 30		✓	8
F Angle 4	415	267 10		✓	9
F Angle 5	373	271 0		✓	10
F Cor 6	310	282 30		✓	11
F Angle 7	260	264 5		✓	12
F Cor 8	268	256 10		✓	13
F Cor 9	200	256 45	NW Cor Shed	✓	14

Continued

		At Rock			
F Cor 10	310	244 6"		✓	15
51 53	245	265 30		✓	16
Water hole	305	287 50	5' Dia.	✓	17
F Cor 11	320	293 50		✓	18
F Cor 12	330	297 30		✓	19
End of F 13	485	309 15		✓	20
F Cor 14	182	252 0		✓	21
~~F Cor 15~~	182	270 10	End of Fence 15	✓	22
79 26	50	206 5		✓	23
75 26	35	237 50	On F line	✓	24
F Cor. 16	62	84° 55"		✓	25
71 26	28	264 20		✓	26
67 23	42	285 0		✓	27
63 30	52	299 55		✓	28
59 37	70	309 40	5° 0'	✓	29
55 73	85	316 15	70 45 F Cor 17	✓	30
51 54	95	317 20	9° 40'		31
F Cor 18	90	38 40	9° 0	✓	32
F Angle 19	110	22 0	11° 30	✓	33
47 43	150	2 0	10° 15	✓	34
N. Side Water Hole	210	330 45	6° 15	✓	35
47 40	270	350 15	5° 15	✓	36
S. Side Water Hole	270	337 55	4° 45"	✓	37
43 20	1060	21 25		Top Bank D.	38
43 21	880	21 10		~~On F line~~	39

Offset

Off Peck

43 26	410	16° 5		✓	1
F Cor 20	260	2° 0		✓	2
F Angle 21	240	4° 25		✓	3
47 41 F. Cor 22	495	59 55		✓	4
43 32	520	56 40	1	✓	5
43 27	630	37° 35	Both B N S. River Bed	✓	6
43 28	840	42 30	Both B N S. "	✓	7
43 29	1150	39 20		✓	8
43 30	1100	56 30		✓	9
43 31	1140	73 50		✓	10
43 36	1520	75 20	+	✓	11
43 35	1240	76 20	+ Water Hole	✓	12
43 38	1370	80 35		✓	13
43 37	1300	78 50		✓	14
43 34	1300	80 45		✓	15
43 33	764	71 20		✓	16
F Cor 23	310	103 5		✓	17
79 27	285	101 15		✓	18
75 27	290	98 0		✓	19
71 27	290	94 40		✓	20
67 24	290	92 35		✓	21
63 31	298	90 35		✓	22
59 38	300	89 5		✓	23
47 39	300	317 0		✓	24
~~47 41~~	~~310~~	~~36 30~~			

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~~47 AV~~	~~450~~	~~80° 30'~~			
Peak A	653	74° 54'		✓	25

At Peak A Sight Texas N for 0 Az Pt.

Peck	655	190° 0	✓		
59 38	375	178 40	✓	1	
55 74	365	179 40	✓	2	
51 55	360	180 30	✓	3	
F. Angle 24	340	178 30	✓	4	
F Angle 25	290	163 0	✓	5	
51 56	293	157 45	✓	6	
55 75	300	157 0	✓	7	
59 39	310	156 25	✓	8	
63 37	318	155 50	✓	9	
67 25	328	155 25	✓	10	
71 28	340	155 20	✓	11	
75 28	350	155 20	✓	12	
79 28	360	154 55	✓	13	
F Cov 26	503	125 20	5° 30'	✓ 14	
F Cov 27	410	121 10		✓ 15	
F Cov 28	300	142 10		✓ 16	
47 44	272	145 10		✓ 17	
47 47	120	116 50		✓ 18	
Texas S		383 40		✓ 19	

Closed

	At Peck A				
43 4	270	102° 35'		✓	20
43 5	325	65° 35'		✓	21
43 3	285	51 20		✓	22
Peck B	698°	101° 5'		✓	23
	At Peck B Sight	Texas N for 0 Az Rt			
Texas S		341 17		✓	
Peck A	698	298 32		✓	
47 45	270	310 35	6°10	✓	1
51 57	210	286 40	6°40	✓	2
55 76	190	283 55	6°15	✓	3
59 40	150	282 40	6°40	✓	4
63 33	140	279 0	5°15	✓	5
67 26	135	274 10		✓	6
71 29	130	269 15		✓	7
75 29	130	262 0		✓	8
F Cov 29	215	192 0		✓	9
F Cov 30	250	181 10		✓	10
L. C Road	230	187 45		✓	11
75 30	142	197 55		✓	12
E Road	150	216 35		✓	13
71 30	100	220 15		✓	14
67 27	85	239 20		✓	15
63 38	75	268 40	5° 10'	✓	16
59 41	80	287 15	7°45'	✓	17

Closed.

	At Rock 13				
55 77	110	311 15	7 45	✓	18
E Road	100	306 40	7 45	✓	19
51 58	150	314 40	7° 10'	✓	20
F Cor 31	148	354 25	8° 15	✓	21
51 59	95	25 30	12° 30	✓	22
55 78	85	27° 45	11° 0	✓	23
59 42	70	31 0	9° 30	✓	24
63 35	60	30 45	7° 30	✓	25
17 28	50	32 55	4° 45	✓	26
71 31	35	37 30		✓	27
75 31	20	55° 0		✓	28
E Road	135	3° 50	9° 15	✓	29
" "	195	38° 0	7° 0	✓	30
F Angle 31	222	38° 0	6° 15	✓	31
F Angle 32	380	49° 30		✓	32
E Road	445	52 42		✓	33
" "	580	51 20		✓	34
F Angle 33	605	50 35		✓	35
	At Texas N-E	Sight Texas N for zero			
43 2	225	345 50		✓	1
Boundy N		298 47		✓	
47 16	300	276 0		✓	2
51 60	98	274 10		✓	3
55 79	85	264 55		✓	4
59 43	85	256 0		✓	5

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Capitol

At Texas N. E

63	36	90	251 35	✓	6
67	29	95	247 30	✓	7
71	32	100	243 55	✓	8
75	32	105	240 15	✓	9
75	33	80	166° 10	✓	10
71	33	60	168° 0	✓	11
67	30	30	164 20	✓	12
63	37	10	187 20	✓	13
59	44	15	339 0	✓	14
55	80	30	315 15	✓	15
51	61	53	350 30	✓	16
47	47	75	349 55	✓	17
43	6	125	349 0	✓	18
51	62	90	71 30	✓	18a
55	81	70	74 55	✓	19
59	45	60	86 50	✓	20
63	38	63	97 10	✓	21
67	31	65	105 0	✓	22
71	34	70	108 15	✓	23
75	34	75	111° 0	✓	24
F angle 32		325	58 35	✓	25
F " 35		450	63 30	✓	26
A3	7	1100	71 45	✓	27
47	48	1120	73 40	✓	28
51	64	1140	75° 55	✓	29
55	83	1150	75 45	✓	30

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At Texas N.E.?

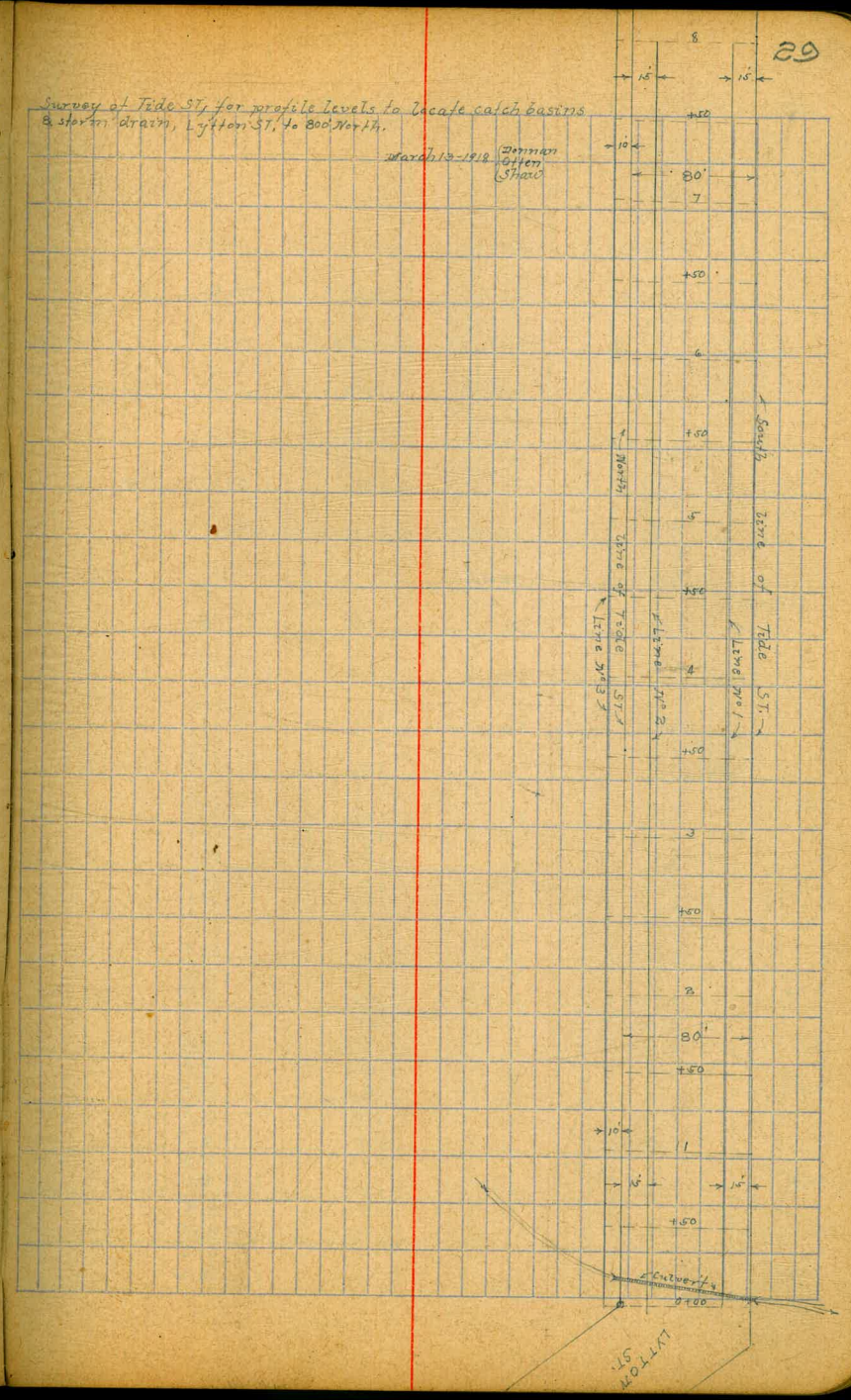
59 47	1140	76° 10	✓	31
63 40	1130	76° 40	✓	32 ✓
67 33	1130	77° 0	✓	33
71 36	1120	77 25	✓	34 ✓
75 36	1130	77 50	✓	35
43 6a	500	72 10	✓	36
51 63	500	78 50	✓	37
55 8x	510	80 40	✓	38
59 46	520	81 55	✓	39
63 39	52x	83 5	✓	40
67 3x	520	84° 30	✓	41
71 35	530	85° 50	✓	42
75 35	533	87° 10		43
				44
				45

43 1 On F line about 100 S of F Cor.
39 2 Closed at Test hole 10
39 1 At F Cor.
39 3 25' N of F Cor.

Copied

Survey of Tide ST, for profile levels to locate catch basins & storm drain, Lytton ST, to 800 North.

March 13-1918 Denman Otten Shaw

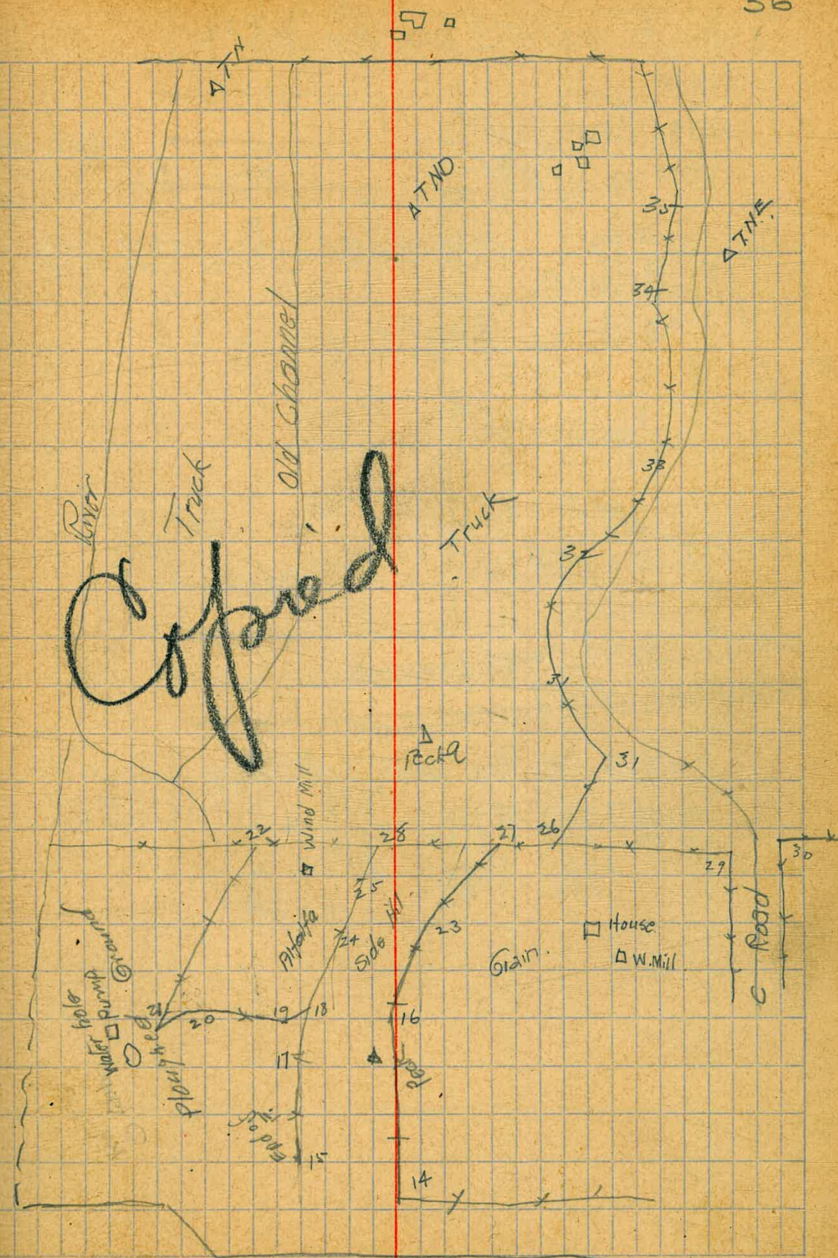


	+	π	−	
S.W. Cor Rosecrans & Lytton Cen of Curve. Brass Plug in Curb 41.75 Curb possibly settled				
	2.02	43.77		41.75
	0.24	31.06	12.95	30.82
	1.12	19.40	12.80	18.26
	1.83	8.39	12.84	6.56
	3.46	5.59	6.26	2.13
			4.91	0.68 = 0.60 B.M.
B.M. North side Tide St, Pole 28# R.R. Spk 0.60				
	4.93	5.53		0.60
Line N°1				
00			3.9	1.6
+94 = E.L. Curb			4.0	1.5
+50				
1 Curb.			4.1	1.4
Gutter.			4.3	1.2
			4.8	0.7
+50			4.3	1.2
			5.0	0.5
2			4.6	0.9
			5.2	0.3
+50			4.7	0.8
			5.2	0.3
			5.0	0.5
3			5.3	0.2
+50			4.7	0.8
			5.3	0.2
4			4.8	0.7
			5.5	0.0
+50			4.9	0.6
			5.5	0.0
5			4.7	0.8
			5.6	− 0.1
+50			5.1	0.4
			5.6	− 0.1
6			5.1	0.4
			5.7	− 0.2
+50			5.0	0.5
			5.7	− 0.2

	+	π	−	
		5.53		
7			5.1	0.4
			5.7	− 0.2
+50			4.9	0.6
			5.6	− 0.1
8			4.8	0.7
			5.5	0.0
Line N°2				
00			4.4	1.1
+167 = E.L. Curb			4.4	1.1
Curb			3.8	1.7
+50 Gutter			4.5	1.0
			4.1	1.4
1			4.8	0.7
			4.1	1.4
+50			4.9	0.6
			4.3	1.2
2			4.6	0.9
			5.0	0.5
+50				
			5.0	0.5
3				
			5.0	0.5
+50				
			5.2	0.3
4				
			5.2	0.3
+50			5.1	0.4
			5.5	0.0
5			5.3	0.2
			5.9	− 0.4
+50			5.5	0.0
			6.0	− 0.5
6			5.4	0.1
			5.8	− 0.3
+50			5.5	0.0
			5.8	− 0.3
7			5.3	0.2
			5.7	− 0.2
+50			5.2	0.3
			5.6	− 0.1
8				
8+00 On Ocean Beach Tract.			4.20	0.7
North end, at bottom of 4½" x 8" Curb, for Tide St			11.2	− 5.7
South " " " " " " " " " "			11.5	− 6.0

Line N ~3 = 10' N of P.L

	+	H.I. 5.53	−	
0.0			4.7	0.8
+8			7.9	-2.4
+12			11.2	-5.7
+18			11.2	-5.7
+30			7.6	-2.1
+50			6.3	-0.8
1			6.3	-0.8
+50			6.1	-0.6
2			5.5	0.0
+50			6.5	-1.0
3			7.0	-1.5
+50			6.8	-1.3
4			6.3	-0.8
+50			6.2	-0.7
5			6.0	-0.5
+50			5.9	-0.4
6			6.0	-0.5
+50			5.8	-0.3
7			5.6	-0.1
+50			5.2	0.3
8			4.7	0.8
			4.93	0.60 = Initial B.M.


Copied
River
Truck
Old Channel
Truck
Wind Mill
Alfalfa
Side Hl.
Grain
House
W. Mill
Road

LOT 6 BLK. 55 ADD. La Jolla

OWNER

CONTR. Edgell

PERMIT NO. 1144 Aug 21/17 { Childs Evans Moore

43.00 / 5.27 / 48.27 H.I. 4028 / 7.99 4062 / 7.65 3994 / 462 / 44.56 H.I. 4029 / 4.27 4063 / 3.93

37.94 / 8.33 3 stakes 1.36 / 9.520

39.95 / 3.42 / 43.37 ✓ 40.29 / 3.08 ✓ 40.63 / 2.74 ✓

chk o.k. Childs

LOT 8-9 BLK. 55 ADD. { Evans Moore La Jolla park Oct. 4/17

OWNER

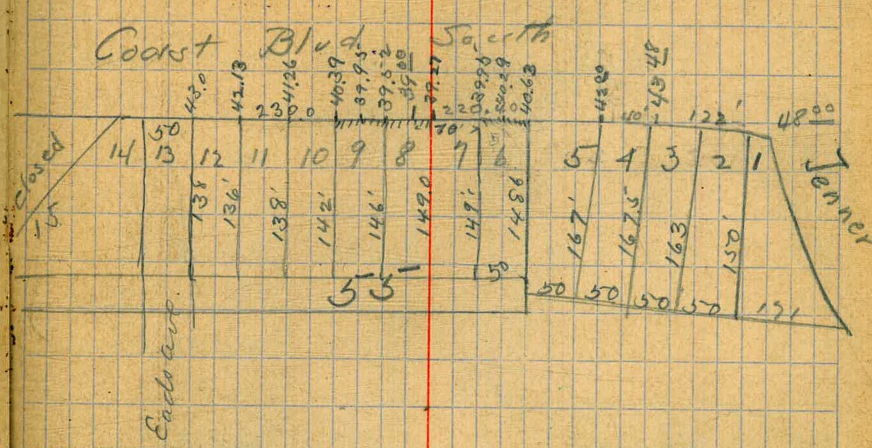
CONTR. Jas Molyneaux

PERMIT NO. 1207

45.75 B.M. top wall Eads ave. Apr. 9/18 { Childs Evans Moore

40.39 / 8.12 39.52 / 8.99 39.27 / 9.24 3995 / 8.56 / 48.51 H.I. / 5.52 / 43.00

3995 / 8.56 3900 / 9.57 5 stakes

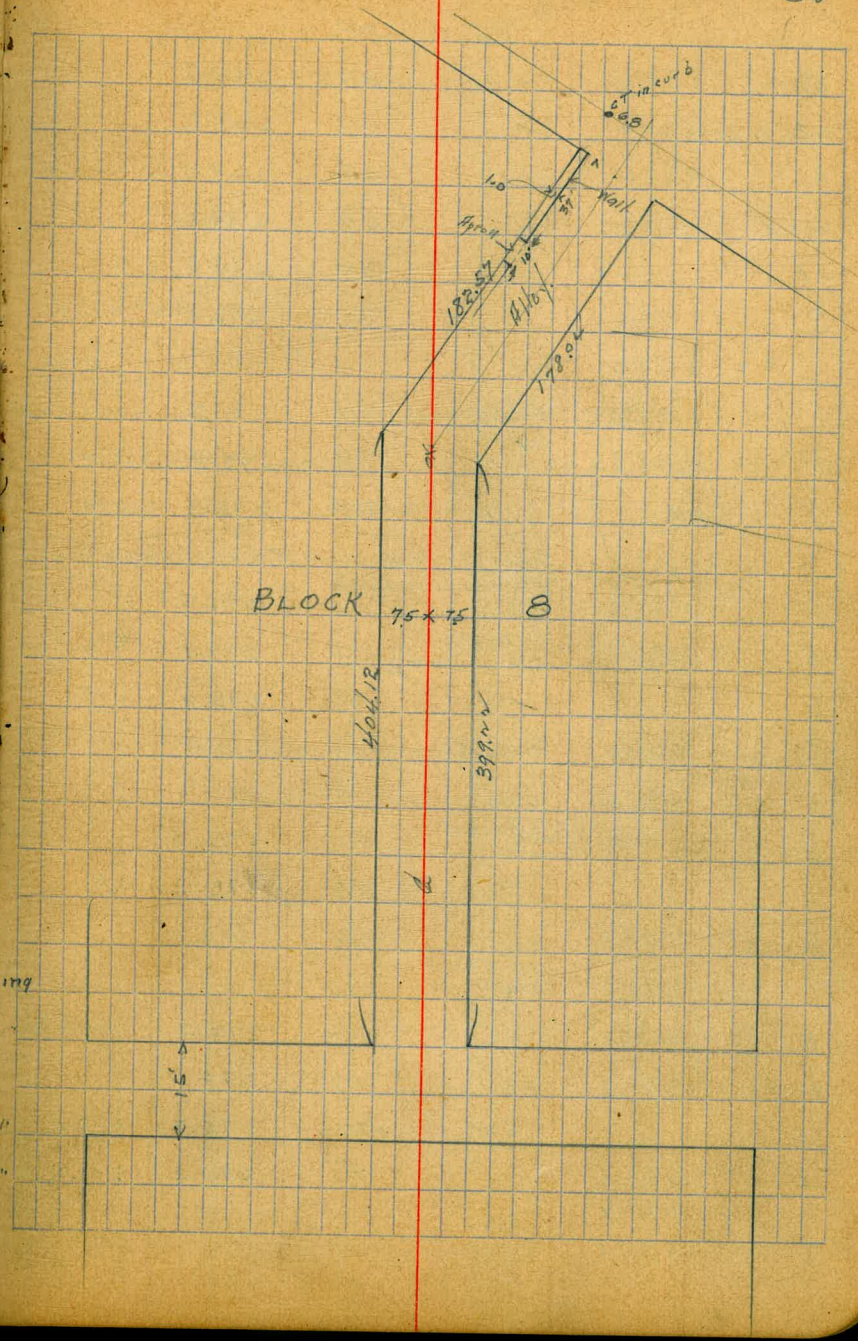


11/18/22 Gregory Moore Ellis Shaw

CROSS SECTION OF ALLEY BLK 8 MISSION HILLS

15 wide

	11.62	46x.68		251.06	BP NW Withers + Hickory
	3 Curb Line Hickory				
W.L.	12.75	273.48	1.45	261.23	on cement ab
	3 Line Hickory				
E			10.4	263.1	
+x			10.5	263.0	
+x			11.30	262.18	
C			11.6	261.9	
+6.4			11.90	261.58	on sidewalk
		8'5			
W + 1.0 = Edge of wall			9.50	263.98	= Top of wall + dirt
C			9.30	264.18	
+6			9.7	2638	
+6			8.1	265.4	
E			8.x	265.3	
		47'5			
6.5 W. of C			7.76	266.22	= Edge of cement apron
W			7.20	266.28	on apron
		48'5			
E			4.8	268.7	New 267.85 on Paving
+0.5			5.0	268.5	
+			6.7	266.8	
C			7.1	266.4	267.40 "
W			7.1	266.4	267.41 "



273.48

66 S

W		5.7	267.8	
+2 = fence		4.9	268.6	
C		5.0	268.5	
+6		4.9	268.6	
+6		3.0	270.5	
E		3.0	270.5	

100' S

New Section for Yardage

105' S
W 270.6
C 270.4
+4.5 270.6
271.8

					New Use for yardage Toward S.
E			2.2	271.3	269.97 on End Pav't
C			2.7	270.8	269.63 " " "
W			3.2	270.3	269.83 " " "

130' S O.K. = S End of Garage facing S.

New Sec. 155' S = Garage on W cm't 2.5 Back
E 273.2
C 272.9
W 272.6
+2.5 273.30 on floor

(175' S. Garage on W 12' Back)

W			2.0	271.5	O.K.
C			1.4	272.1	
E			0.7	272.8	
T.P.	10.84	282.92	1.40	272.08	

187.57 on W } = Angle point.
178 on E

32' S on E Garages E & W Facing N & S

E	9.4	273.5	O.K	
C	9.6	273.3		
W	9.6	273.3		

50' S on E
54.9 " " W

W	7.2	275.7	275.8
+1.5	7.9	275.0	
C	7.7	275.2	275.5
E	7.7	275.2	276.0

282.92.

100' S on E New Garage on W 9' Back

137' S on E. Garage on W 6' Back
New 278.7 on floor

			New
E	6.3	276.6	277.0
C	6.3	276.6	276.9
+6	6.5	276.4	
W	5.8	277.1	277.0

156' S on E

195' S on E Garages E & W
W - 8 278.80 on floor
E + 1 278.50 on cem't apron
New

W	5.2	277.7	o K
C	5.3	277.6	
E	4.8	278.1	
+2.5 = front of garage	4.1	278.8	

200' S on E

240' S on E = Garages E & W
E - 4 278.80 cem't apron
W + 6 279.30 " floor

E	4.7	278.2	O.K
C	4.8	278.1	
W	4.6	278.3	

250' S on E

290' S on E = Garage on E 8' Back

W	4.0	278.9	O.K
C	4.4	278.5	
E	4.5	278.4	

300' S on E

E	4.4	278.5	ok
C	4.3	278.6	
+6	4.1	278.8	
W	3.2	279.7	

350' S on E

W	4.4	278.5	O.K.
C	4.4	278.5	
E	4.4	278.5	

393. S. on E. Garage on W
W 289.00 on cem't apron
290.0 " " floor
28292

		399.22' S. on E = W.L. E+W Alley			
E			4.2	278.7	} ok
C			4.0	278.9	
W			3.5	279.4	
		℄ of E+W Alley			
W			3.7	279.2	
C			3.9	279.0	
E			4.2	278.7	
T.P.	4.62	283.46	4.08	278.84	

CROSS SECTION OF E+W Alley Blk 8 Mission Hills
Paved with concrete from W.L. Arguello to 46' West.

	25' W. of W.L. Arguello to establish grades			
N		10.30	273.16	on paving
C	ok	10.40	273.06	✓ ✓
S		10.30	273.16	✓ ✓
	46' W = End of paving			
S		9.2	274.3	on paving
C	ok	9.2	274.3	✓ ✓
N		9.2	274.3	✓ ✓
	100' W			
N		6.5	277.0	
C	o.K.	6.6	276.9	
S		6.3	277.2	
	140' W = E.L. N+S alley			
S		4.6	278.9	on cement
C	ok	4.8	278.7	

28346

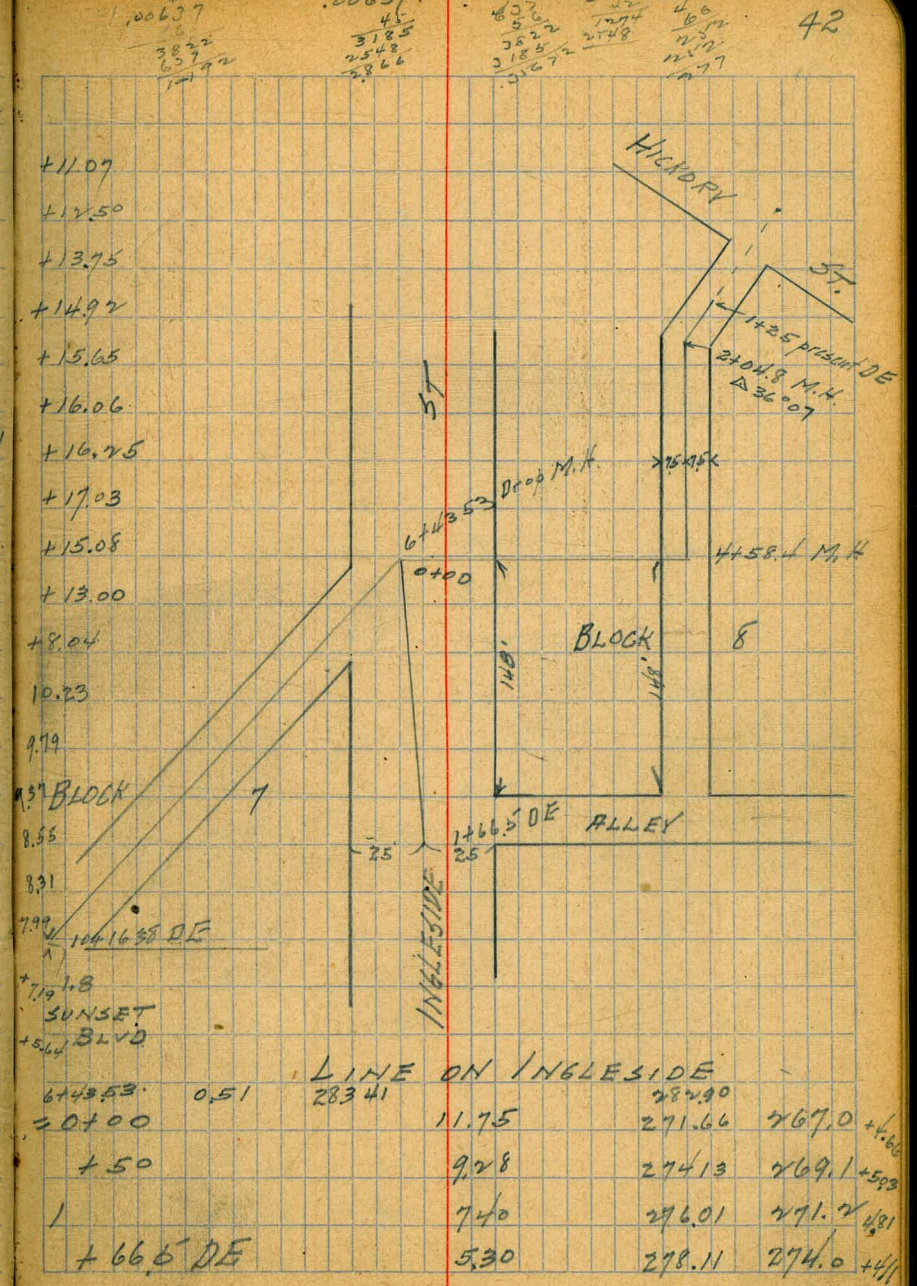
N		4.8	278.7	
	155' W = W.L. N+S alley			
N		4.1	279.4	
C	ok	4.3	279.2	
S		4.0	279.5	on cement drive
	200' W			
S		3.3	280.2	
C	ok	3.6	279.9	o.K.
N		3.7	279.8	
	250' W			
N		4.1	279.4	
C	ok	4.1	279.4	
S		3.6	279.9	
	295' W = W.L. Ingleside St			
S		5.0	278.5	
C	o.K.	4.7	278.8	o.K
N		5.1	278.4	
Chk BM		0.61	282.85 .90	Mon NE Ingleside + Sunset
	295 W = W Line Ingside HI. 283.83			
N		5.40	278.43	on cb
C		5.00	278.8	
S		5.09	278.74	on cb

3/8/23 Gregory Moore Miller Shaw. Elevs on Curb East Side Maryland 5.0 X Meade

0+ BM	1.16	325.23		324.07	BP NW Meade + Maryl
	0.56	323.97	11.82	323.41	
200 S. of Meade			3.73	20.3	
225			5.15	18.8	
250			6.90	17.1	
275			8.52	15.5	
287			9.23	14.8	
300			9.53	14.4	
313.5			9.78	14.2	
325			10.20	13.8	

4/18/23 Gregory Moore Miller — Sewer Construction 6 Alley 3 Blk 7 & 8 Mission Hills

1+25 DE	0.51	283.41		282.90	260.32
1+50			11.86	271.55	260.48
2+04.8 M.H			10.08	273.33	260.83
2+50			8.54	274.87	261.17
3			7.05	276.36	261.44
+50			6.00	277.41	261.76
4			5.27	278.14	262.08
+58.4 M.H			4.72	278.69	262.44
5			3.67	279.74	262.71
+50			5.30	278.11	263.03
6			7.06	276.35	263.35
+43.53 Drop M.H			11.75	271.66	263.62
7			9.20	274.21	263.98
+50	4.85	278.94	9.32	274.09	264.30
8			4.95	273.99	264.62
+50			5.45	273.49	264.94
9			5.37	273.57	265.26
+50			5.37	273.57	265.58
10			5.85	273.09	265.90
+16.38 DE			7.30	271.64	266.0



LINE ON INGLESIDE

6+43.53	0.51	283.41		282.90		
=0+00			11.75	271.66	267.0	+4.66
+50			9.28	274.13	269.1	+5.03
1			7.40	276.01	271.2	+4.81
+66.5 DE			5.30	278.11	274.0	+4.11

Moore
Earle
Kelley
10/29/24

Cross Section of Middle 60' of Bancroft

from NL Date to SL of Elm

60' wide
10' s/w

	0.20	231.72		231.52	Sw Mon Date of Bancroft
		NL Date			
W			3.0	228.7	
cb			3.5	228.2	
1/4			4.1	27.6	
Q			4.5	27.2	
+6			4.6	27.1	
+8			5.5	26.2	
1/4			5.3	26.4	
CB			5.4	26.3	
E			5.7	26.0	
		25' N			
E			6.0	25.7	
cb			5.8	25.9	
1/4			5.8	25.9	
+2			6.0	25.7	
+5			5.4	26.3	
C			5.3	26.4	
1/4			4.9	26.8	
CB			4.3	27.4	
W			3.9	27.8	
		50' N			
W			4.8	26.9	
cb			4.9	26.8	
1/4			5.5	26.2	

231.72 — Bancroft — #3

C	5.9	25.8
+B	6.0	25.7
+8	6.5	25.2
1/4	6.3	25.4
CB	6.3	25.4
E	6.5	25.2
	75' N	
E	7.1	24.6
cb	7.1	24.6
1/4	7.1	24.6
+2	7.2	24.5
+5	6.5	26.2
C	6.4	26.3
1/4	5.9	25.8
CB	5.7	26.3
W	6.8	25.3
	100' N	
W	6.7	25.0
cb	6.6	25.1
1/4	6.2	25.5
Q	7.0	24.7
+3	7.2	24.5
+8	7.8	23.9
1/4	7.7	24.0
CB	7.7	24.0
E	7.9	23.8

	231.72		
	125'N		
E		8.4	23.3
cb		8.5	23.2
1/4		8.5	23.2
+2		8.6	23.1
+6		8.1	23.6
C		8.0	23.7
1/4		7.7	24.0
cb		7.9	23.8
W		8.3	23.4
+10		8.6	23.1
	150'N		
-10		10.5	21.2
W		9.8	21.9
cb		9.2	22.5
1/4		9.4	22.3
C		9.6	22.1
+4		9.8	21.9
1/4		9.2	22.5
cb		8.8	22.9
E		8.4	23.3
	162'N		
E		8.3	23.4
cb		8.8	22.9
1/4		9.4	22.3
+5		9.8	21.9

	231.72		
+7		10.4	21.3
C		10.4	21.3
1/4		11.1	20.6
cb		11.8	19.9
W		11.7	20.0
+10		12.5	19.2
	175'N		
-10		12.3	19.4
-5		11.2	20.5
W		10.9	20.8
cb		10.4	21.3
1/4		9.8	21.9
C		9.5	22.2
+4		9.3	22.4
+6		9.6	22.1
1/4		9.1	22.6
cb		8.8	22.9
E		8.4	23.3
	200'N		
E		8.9	22.8
cb		8.8	22.9
1/4		9.2	22.5
C		9.5	22.2
1/4		9.7	22.0
+9		10.2	21.5
W		10.4	21.3
+13		11.0	20.7

23172

225'N

-10	10.8	20.9
W	10.5	21.2
cb	10.1	21.6
1/4	9.8	21.9
C	9.7	22.0
+5	9.5	22.2
1/4	9.0	22.7
cb	8.8	22.9
E	8.6	23.1

250'N

E	9.0	22.7
cb	8.9	22.8
1/4	9.0	22.7
C	8.9	22.8
1/4	9.0	22.7
cb	9.4	22.3
W	9.3	22.4
+10	9.5	22.2

275'N

-5	8.2	23.5
W	8.3	23.4
cb	8.3	23.4
1/4	8.3	23.4
C	8.7	23.0
1/4	8.8	22.9

23172 Bancroft #5

cb	8.9	22.8
E	9.4	22.3
+5	9.7	22.0

300'N = SL Elm

-10	11.3	20.4
E	10.2	21.5
+6	8.8	22.9
cb	8.7	23.0
1/4	8.5	23.2
+6	8.2	23.5
C	8.4	23.3
+7	7.8	23.9
1/4	7.8	23.9
cb	7.3	24.4
W	6.5	25.2
on Com curb w/ Bancroft	6.60	25.1 S cb line of Elm

Alley Blk 178 M+S X Sec 4/10/25 mills

Beardsley to Crosby bet Logan & Kearney

S.E. of Beardsley & Kearney

B.M.	2.22	48.26	46.04	
		00 = E Line Beardsley		
		(48.3)		
N		4.21	44.05 ✓	encmt. ck.
N		4.4	43.9 ✓	dirt
C		4.8	43.5 ✓	
S		4.53	43.73 ✓	encmt ck
		25' E		
S		4.5	43.8 ✓	
C		4.7	43.6 ✓	
N		4.5	43.8 ✓	
		59' E = Garage on N. dirt 1.30 Back		
N		4.2	44.1 ✓	
C		4.4	43.9 ✓	
S		4.1	44.2 ✓	
		90' E = Garage on N. dirt 0.6 Back		
S		4.2	44.1 ✓	
C		4.1	44.2 ✓	
N		4.2	44.1 ✓	
		112' E = Garage on No. 3. in Alley Dirt		
N		3.9	44.4 ✓	
C		4.3	44.0 ✓	
S		4.2	44.1 ✓	
		on N.		
		129' E = N. edg House 1.1 in Alley		
S		3.9	44.4 ✓	
C		4.0	44.3 ✓	
N		3.6	44.7 ✓	

48.26 (46.3)

168' E = Garage on N dirt 1.0 in Alley

46

N		3.2	45.1 ✓
C		3.3	45.0 ✓
S		3.0	45.3 ✓
	200' E		
S		1.8	46.5 ✓
C		1.7	46.6 ✓
N		1.9	46.4 ✓
	215 E = Garage on S. wood floor 0.1 in Alley		
S		1.8	46.5 ✓
	242' E = Garage on N. dirt 1.1 in Alley		
N		1.9	46.4 ✓
C		2.0	46.3 ✓
S		2.0	46.3 ✓
T.P.	2.94	49.16	46.22 ✓
	267' E = Gar. on N. wood floor 1.3 in Alley		
	(49.2)		
S		2.9	46.3 ✓
C		2.9	46.3 ✓
N		3.1	46.1 ✓
	294' E = Gar. on N. dirt 1.5 in Alley		
N		3.0	46.2 ✓
C		3.0	46.2 ✓
S		3.0	46.2 ✓
	300' E House on N. is 0.1 in Alley		

49.16 (49.2)

333'E = w.end 3 Garages on each side dirt {on N 1.0 in Alley
" S 0.5 Back

S		3.6	45.6 ✓
C		3.6	45.6 ✓
N		4.0	45.2 ✓

340'E = E. end 3 garages each side {on N. 1.0 in Alley
" S Line

N		4.3	44.9 ✓
C		4.1	45.1 ✓
S		4.0	45.2 ✓

393'E = Garage on N. dirt 0.9 in Alley

S		4.6	44.6 ✓
C		4.5	44.7 ✓
N		4.4	44.8 ✓

455'E = Gar. on N dirt on Line

N		4.8	44.4 ✓
C		4.8	44.4 ✓
S		4.8	44.4 ✓

475'E Gar. on S dirt on Line

S		4.7	44.5 ✓

493'E Gar on N. dirt 0.3 in alley

S		4.4	44.8 ✓
C		4.7	44.5 ✓
N		4.7	44.5 ✓

565'E = 3 Garages on S cmt floors 0.4 Back

N		4.1	45.1 ✓
C		4.1	45.1 ✓
W		4.2	45.0 ✓

49.16 (49.2) 47

590'E

S			4.1	45.1 ✓
C			4.0	45.2 ✓
N			3.8	45.4 ✓

600'E = W. line Crosby

N			3.07	46.09 ✓ on cb.
N			3.25	45.91 ✓ " paving
C			3.67	45.49 ✓ " "
S			3.60	45.56 ✓ " "
S			3.39	45.77 ✓ " cb
T.P.	5.20	52.24	2.12	47.04 ✓
T.P.			4.27	47.97 = 47.99 BM SE {Kearney Crosby

Alley Blk 187 N & S. ½ Sec 4/10/25 mille

Beardsley to Crosby Bet Kearney & Julian

B.M.	4.24	50.28		46.04	S.E. Beardsley & Kearney
	2'. W. of E line Beardsley = Inside edge walk		(50.3)		
S			4.45	45.83	on walk
N			4.58	45.70	
		00 = E Line Beardsley			
N			3.2	47.1	
C			4.6	45.7	
S			3.8	46.5	
		5'E			
S			2.1	48.2	
+6			4.1	46.2	
C			4.1	46.2	
+2			4.0	46.3	
N.			1.8	48.5	
T.P.	4.56	53.22	1.62	48.66	
		30'E	(53.2)		
N			5.1	48.1	
C			5.7	47.5	
+5			5.7	47.5	
+7			4.8	48.4	
S			4.8	48.4	
	67'E = Garage on N. dirt on line				
S			4.8	48.4	
C			5.2	48.0	
N			5.1	48.1	

53.22

109'E = Garages N & S. dirt {N is 0.5 Back; S .. on line} (53.2)

N	5.2	48.0
C	5.2	48.0
S	5.1	48.1

135'E = Garages N & S — N 0.5 Back; S 1.0 ..

S	5.0	48.2
C	5.1	48.1
N	5.1	48.1

160'E

N	5.3	47.9
C	5.2	48.0
S	5.0	48.2

185'E

S	4.8	48.4
C	4.8	48.4
N	5.0	48.2

215'E = Garage on N. dirt 0.5 Back

N	5.0	48.2
C	5.0	48.2
S	4.9	48.3

271'E = Garage dirt 3.0 back

S	4.5	48.7
C	4.7	48.5
N	4.7	48.5

53.22 (53.2)

308' E = Garages N & S dirt N is 4.0 Back S " 1.7 in alley

N	4.6	48.6
C	4.7	48.5
S	4.8	48.4

323' E Garage on N dirt 4.0 Back

N	4.9	48.3

350' E garage on S. dirt 2.1 in alley

S	4.6	48.6
C	4.8	48.4
N	4.8	48.4

377' E Garage on N dirt 5.0 Back

N	4.9	48.3

405' E = Garage on S. dirt 3.0 in alley

N	5.0	48.2
C	5.0	48.2
S	5.0	48.2

440' E Garage on S. dirt 2.5 Back

S	5.0	48.2
C	4.8	48.4
N	4.8	48.4

485. E garages N & S N 1.8 Back S 2.3 " dirt

N	4.9	48.3
C	4.9	48.3
S	4.6	48.6

53.22

510' E garages N & S dirt N 1.0 Back S " Line (53.2)

S	4.6	48.6
C	4.8	48.4
N	4.5	48.7

530' E garages N & S dirt N 10.0 Back S 0.2 in alley

N	4.5	48.7
C	4.6	48.6
S	4.6	48.6

562' E garages N & S. dirt N. Line S. 4.0 Back

S	4.1	49.1
C	4.1	49.1
N	4.2	49.0

590' E

N	3.5	49.7
C	3.5	49.7
S	3.4	49.8

601. E = W. Line Crosby

S	2.60	50.62	on ck.
S	2.75	50.47	" Paving
C	2.90	50.32	" "
N	2.53	50.69	" "
N	2.34	50.88	" ck
T.P.	4.10 54.26	3.06	50.16
		6.28	47.98 = 47.99 BM Crosby & Kearney

60' wide
10 lbs.
10 '4

32nd St X Sec.

from N. Line Woolman to S. Line Imperial

4/10/25

Top Hydt S. of Woolman + 32nd

B.M	10.45	70.85		60.40
	⊙⊙ = N. Line Woolman		70.9	
E			10.2	60.7 ✓
cb			10.0	60.9 ✓
1/4			11.2	59.7 ✓
C			11.7	59.2 ✓
1/4			11.3	59.6 ✓
cb			11.7	59.2 ✓
W			11.5	59.4 ✓
	3' N			
W			11.4	59.5 ✓
cb			11.7	59.2 ✓
1/4			11.3	59.6 ✓
C			11.6	59.3 ✓
1/4			10.7	60.2 ✓
+7			5.4	65.5 ✓
cb			5.4	65.5 ✓
E			4.5	66.4 ✓
	50' N			
E			3.0	67.9 ✓
cb			3.0	67.9 ✓
+7			4.9	66.0 ✓
+7.5			8.6	64.3 ✓
1/4			9.7	61.2 ✓
C			9.7	61.2 ✓
1/4			9.3	61.6 ✓

70.85 (70.9) 50

+6		9.5	61.1 ✓
cb		9.2	61.4 ✓
W		5.8	65.1 ✓
	67' N		
W		4.2	66.7 ✓
+6		7.2	63.7 ✓
cb		7.6	63.3 ✓
+5		8.3	62.6 ✓
1/4		7.9	63.0 ✓
C		8.3	62.6 ✓
+5		8.9	62.0 ✓
1/4		8.0	62.9 ✓
+3		3.1	67.8 ✓
cb		2.6	68.3 ✓
+4		1.48	69.1 ✓
E		2.0	68.9 ✓
	90' N		
E		1.0	69.9 ✓
+8		0.9	70.0 ✓
cb		1.7	69.2 ✓
1/4		4.0	66.9 ✓
+4		5.2	65.7 ✓
+5		7.3	63.6 ✓
C		6.8	64.1 ✓
1/4		6.4	64.5 ✓
+5		6.8	64.1 ✓

70.85

90'N (cont) 70.9

cb			6.0	69.4	✓
+4			5.8	69.1	✓
W			2.6	68.3	✓
	110'N				
W			1.6	69.3	✓
+6			4.5	66.4	✓
cb			4.8	66.1	✓
+5			5.4	65.5	✓
1/4			5.1	65.8	✓
C			5.2	65.7	✓
+4			5.7	65.2	✓
1/4			3.9	67.0	✓
cb			1.2	69.7	✓
+5			0.5	70.4	✓
E			0.7	70.2	✓
	130'N				
E			0.7	70.2	✓
cb			0.8	70.1	✓
+5			1.1	69.8	✓
1/4			2.9	68.0	✓
+2			4.4	66.5	✓
C			3.8	67.1	✓
1/4			3.9	67.0	✓
+4			4.1	66.8	✓
cb			3.5	67.4	✓
+4			2.9	68.0	✓

70.85 70.9 32 mg St

+8			1.1	69.8	✓
W			1.1	69.8	✓
	155'N				
W			0.8	70.1	✓
cb			1.6	69.3	✓
+6			2.2	68.7	✓
1/4			1.9	69.0	✓
C			1.7	69.2	✓
1/4			2.3	68.6	✓
+6			0.3	70.6	✓
cb			0.3	70.6	✓
E			0.0	70.9	✓
T.P.	9.53	80.08	0.30	70.55	
	170'N		80.1		
E			9.0	71.1	✓
cb			9.3	70.8	✓
+4			9.4	70.7	✓
1/4			10.7	69.4	✓
C			10.0	70.1	✓
1/4			10.2	69.9	✓
+5			10.6	69.5	✓
+7			9.0	71.1	✓
cb			9.3	70.8	✓
+7			9.4	70.7	✓
W			9.0	71.1	✓

80.08

200

80.1

W		8.4	71 1 ✓
+2		8.8	71 3 ✓
eb		8.7	71 1 ✓
+2		8.6	71 5 ✓
+6		9.5	70 6 ✓
1/4		9.1	71.0 ✓
C		8.7	71 1 ✓
1/4		9.3	70 8 ✓
+3		9.7	70 1 ✓
+4		8.8	71 3 ✓
eb		8.8	71 3 ✓
E		8.9	71 2 ✓
	250' E		
E		8.3	71 8 ✓
eb		8.3	71 8 ✓
+5		8.5	71 6 ✓
1/4		8.1	71 0 ✓
C		7.6	71 5 ✓
1/4		7.8	71 3 ✓
+4		8.1	71 0 ✓
+8		7.3	71 8 ✓
eb		7.5	71 6 ✓
W		7.3	71 8 ✓
	300' N. = S. Line Franklin		80' wide 20' C.P.S. 10' 1/4's
W		6.7	73 4 ✓
eb		6.8	73 3 ✓

80.08

80.1

32nd St

52

+3		6.7	73 4 ✓
+7		7.6	71 5 ✓
1/4		7.5	71 6 ✓
C		7.1	73 0 ✓
1/4		7.2	71 9 ✓
+6		7.4	71 7 ✓
eb		7.0	73.1 ✓
E		7.1	73 0 ✓
	S. eb.		
E		6.5	73 6 ✓
eb		6.7	73 4 ✓
1/4		6.9	73 2 ✓
C		6.9	73 2 ✓
1/4		7.2	71 9 ✓
eb		6.6	73 5 ✓
W		6.6	73 5 ✓
	2' N. of S. eb.		
W		7.2	71 9 ✓
eb		7.0	73 1 ✓
1/4		7.1	73 0 ✓
C		6.9	73 2 ✓
1/4		6.8	73 3 ✓
eb		6.7	73 4 ✓
E		6.6	73 5 ✓

80.08

80.1

S 1/4		6.6	735	✓
E		6.7	734	✓
CP		6.8	733	✓
1/4		6.8	733	✓
E		6.9	732	✓
1/4		6.7	734	✓
CP		6.9	732	✓
W				
	℄			
W		6.5	736	✓
CP		6.4	737	✓
1/4		6.6	735	✓
E		6.6	735	✓
1/4		6.6	735	✓
CP		6.6	735	✓
E		6.8	733	✓
	N. 1/4			
E		6.7	734	✓
CP		6.5	736	✓
1/4		6.4	737	✓
E		6.4	737	✓
1/4		6.5	736	✓
CP		6.3	738	✓
W		6.5	736	✓
	N. CP			
W		6.4	737	✓
CP		6.0	741	✓

80.08

80.1

32nd St

5-3

1/4		6.3	738	✓
E		6.2	739	✓
1/4		6.3	738	✓
CP		6.3	738	✓
E		6.4	737	✓
	00 = N. Line Franklin			
E		5.1	750	✓
CP		6.0	741	✓
1/4		5.9	742	✓
E		5.7	744	✓
1/4		6.0	741	✓
CP		5.6	745	✓
W		5.3	748	✓
	30' N			
W		4.7	754	✓
CP		5.1	750	✓
1/4		5.4	747	✓
E		5.1	750	✓
1/4		5.0	751	✓
+6		5.1	750	✓
+7		3.9	762	✓
CP		3.5	766	✓
E		3.7	764	✓
	55' N			
E		3.9	762	✓
CP		4.0	761	✓

80.08

55' N cont. 80.1

+2	4.2	75	✓
+3	4.9	75	✓
1/4	4.8	75	✓
e	4.8	75	✓
1/4	5.3	74	✓
cb	4.9	75	✓
+2	4.2	75	✓
w	3.9	76	✓

80' N

w	6.0	74	✓
cb	5.6	74	✓
1/4	5.0	75	✓
c	4.6	75	✓
1/4	4.5	75	✓
+4	4.5	75	✓
+8	3.7	76	✓
cb	3.6	76	✓
e	3.3	76	✓

115' N

e	3.7	76	✓
cb	3.8	76	✓
+2	3.8	76	✓
+4	4.7	75	✓
1/4	4.6	75	✓
e	4.7	75	✓
1/4	5.5	74	✓

80.08

32nd St

54

80.1

cb	6.3	73	✓
w	7.1	73	✓
+5	7.5	72	✓

140' N

-5	7.1	73	✓
w	6.7	74	✓
cb	6.2	73	✓
1/4	5.6	74	✓
c	5.0	75	✓
1/4	4.9	75	✓
cb	4.9	75	✓
e	4.4	75	✓

157' N

e	4.0	76	✓
cb	4.7	75	✓
+3	5.1	75	✓
1/4	4.7	75	✓
c	4.9	75	✓
1/4	5.4	74	✓
cb	5.7	74	✓
w	6.5	73	✓
+5	6.8	73	✓

175' N

w	4.6	75	✓
cb	4.8	75	✓
+5	4.8	75	✓

80.08

175.' N (con)

	80.1		
+6	5.2	749	/
1/4	5.0	75.1	/
c	4.5	75.6	/
1/4	4.5	756	/
+6	4.6	755	/
+9	4.0	761	/
cb	4.0	761	/
E	3.5	761	/

200' N.

E	2.7	771	/
cb	3.1	77.0	/
+2	3.1	77.0	/
+4	3.7	764	/
1/4	3.5	766	/
c	3.5	766	/
1/4	3.9	762	/
+2	4.2	759	/
+4	3.6	765	/
cb	3.4	767	/
W	3.3	768	/

2.50' N

W	2.5	776	/
cb	2.6	775	/
+5	2.7	774	/
+7	3.0	771	/
1/4	2.8	773	

	80.1		
c	2.4	777	/
1/4	2.3	778	/
+7	2.7	774	/
+8	1.7	784	/
cb	1.7	784	/
E	1.9	782	/

299' N

E	1.3	788	/
cb	1.5	786	/
+1	2.4	772	/
1/4	2.1	780	/
c	2.3	778	/
1/4	2.8	773	/
+4	2.9	772	/
+8	1.8	783	/
cb	1.8	783	/
W	2.0	781	/

300' N. Ξ S. Line Clay

W	2.7	774	/
cb	2.8	773	/
+6	3.1	770	/
1/4	2.8	773	/
c	2.4	777	/
1/4	2.1	780	/
+8	2.4	777	/
cb	1.7	784	/
E	1.7	784	/

80.08

S. cb

80.1

E		2.03	78 07	on cmt. cb.
W		2.97	77 13	" " "

N. cb

W		2.01	78 09	" " "
E		1.02	79 08	

00 = N Lime Clay

E		0.8	79 3
cb		0.7	79 7
+5		1.5	78 7
1/4		1.3	78 8
C		1.2	78 9
1/4		1.6	78 5
+3		2.0	78 1
+6		1.5	78 6
cb		1.5	78 6
W		1.4	78 7

4' N

W		1.2	78.9
cb		1.2	78 9
+4		1.2	78 9
+6		1.7	78 4
1/4		1.3	78 8
C		1.0	79 1
1/4		1.5	78 6
+5		1.3	78 8
+6		0.2	79 9

80.08

32nd St

56

80.1

cb		0.2	79 5	
E		0.3	79 8	
T.P.	8.89	1.02	79.06	Back of cb N.E. Cor Clay & 32nd

35' N 88°

E		7.6	80 1
cb		7.5	80 5
+3		7.6	80 4
+5		8.5	79 5
1/4		8.2	79 8
C		7.9	80 1
1/4		8.3	79.7
+3		8.7	79 3
cb		8.1	79 9
W		8.2	79 8

80' N

W		7.6	80 1
cb		7.5	80 5
+6		7.7	80 3
1/4		7.4	80 6
C		7.0	81 0
1/4		7.4	80 6
+2		7.6	80 4
+7		6.4	81 4
cb		6.8	81 4
E		7.2	80 8

	87.95			
	140'N	88.0		
E		5.6	8√1	/
cb		5.2	8√8	/
+2		5.3	8√7	/
+5		5.8	8√√	/
1/4		5.5	8√5	/
c		5.3	8√7	/
1/4		5.5	8√5	/
+3		5.7	8√3	/
cb		5.1	8√9	/
W		5.5	8√5	/
	170'N			
W		5.1	8√9	/
cb		4.8	83√	/
+7		5.3	8√7	/
1/4		5.2	8√6	/
c		5.0	830	/
1/4		5.4	8√6	/
+4		5.5	8√5	/
+6		5.1	8√9	/
cb		5.3	8√7	/
E		5.3	8√7	/
	185'N			
E		5.1	8√9	/
cb		5.0	830	/
+6		5.4	8√6	/
1/4		5.2	8√8	/

	87.95	88.0	32nd St	
c		4.9	831	/
1/4		5.3	8√7	/
cb		5.4	8√6	/
W		5.4	8√6	/
	230'N			
W		4.5	835	/
cb		4.3	837	/
+7		4.6	831	/
1/4		4.4	836	/
c		4.2	838	/
1/4	/	4.2	838	/
+4		4.4	836	/
cb		3.9	841	/
E		4.1	839	/
	270'N			
E		3.8	84√	/
cb		3.6	841	/
+6		3.9	841	/
1/4		3.6	841	/
c		3.5	845	/
1/4		3.9	841	/
+3		3.9	841	/
+5		3.2	848	/
cb		3.1	849	/
W		3.1	849	/

87.95

300' N = S. Line Webster

			88.0		
W			2.6	85.4	✓
cb			2.6	85.4	✓
+7			3.5	84.5	✓
1/4			3.3	84.7	✓
c			3.0	85.0	✓
1/4			3.0	85.0	✓
+4			3.1	84.9	✓
cb			2.6	85.4	✓
E			2.6	85.4	✓
		S. cb			
E			2.81	85.19	on cement cb
W			2.76	85.19	" " "
		N. cb			
W			0.81	87.19	" " "
E			0.82	87.13	" " "
T.P.	4.56	92.33	0.18	87.77	
		00 = N. Line Webster	92.3		
E			4.9	87.4	✓
cb			5.2	87.1	✓
1/4			5.1	87.2	✓
c			5.1	87.2	✓
1/4			5.2	87.1	✓
cb			4.7	87.6	✓
W			5.0	87.3	✓

92.33 32 ng St.

	5' N	92.3		
W		4.8	87.5	✓
cb		3.8	88.5	✓
+7		4.8	87.5	✓
1/4		4.9	87.4	✓
c		4.8	87.5	✓
1/4		4.7	87.6	✓
cb		4.2	88.1	✓
E		4.0	88.3	✓
	40' N			
E		2.5	89.8	✓
cb		3.0	89.3	✓
1/4		3.2	89.1	✓
c		3.2	89.1	✓
1/4		3.2	89.1	✓
cb		3.0	89.3	✓
W		3.1	89.2	✓
	75' N			
W		2.8	89.5	✓
cb		2.8	89.5	✓
1/4		2.5	89.8	✓
c		2.3	90.0	✓
1/4		2.2	90.1	✓
+6		1.1	91.2	✓
cb		1.2	91.1	✓
E		1.0	91.3	✓

92.33

135' N Gr. 3

E	1.9	901	✓
cb	2.7	896	✓
1/4	3.5	888	✓
C	3.5	868	✓
1/4	3.4	889	✓
cb	3.3	890	✓
W	3.9	881	✓
165' N.			
W	5.6	867	✓
cb	5.5	868	✓
1/4	5.1	87 ✓	✓
C	5.1	87 ✓	✓
1/4	4.7	876	✓
cb	4.0	863	✓
E	3.7	886	✓
205' N			
E	5.2	871	✓
cb	5.6	867	✓
1/4	6.0	863	✓
C	7.0	853	✓
1/4	7.2	851	✓
cb	7.5	848	✓
W	7.8	845	✓
225' N			
W	9.3	830	✓
cb	9.1	83 ✓	✓

92.33

32nd St

Gr 3

59

1/4	8.7	836	✓
C	8.6	837	✓
1/4	7.5	848	✓
cb	6.3	860	✓
E	6.0	863	✓
260' N			
E	9.5	818	✓
cb	9.9	81 ✓	✓
1/4	10.4	814	✓
1/4	12.0	80.3	✓
E	13.2	79.1	✓
T.P.	1.21 80.59	12.95	79.38
1/4	(80.6) 1.3	793	✓
cb	1.5	791	✓
W	1.5	791	✓
285' N = S. 4th & N. St			100' wide 16' cbs 17' 1/4 s
W	3.4	77 ✓	✓
cb	3.7	769	✓
1/4	3.6	770	✓
C	3.4	77 ✓	✓
1/4	3.2	774	✓
cb	2.1	785	✓
+ 7	1.4	791	✓
E	0.8	798	✓

80.59 5'N 80.6

E		2.2	781
eb		2.9	777
1/4		3.5	771
e		3.6	770
1/4		3.8	768
eb		4.0	766
w		4.1	765
	S. eb		
w		4.8	758
eb		4.8	758
1/4		4.3	763
e		3.9	767
1/4		3.9	767
eb		3.7	769
E		3.3	773
	S. 1/4		
E		3.6	770
eb		4.2	762
1/4		4.5	761
e		4.6	760
1/4		4.9	757
eb		5.3	753
st		5.6	750
w		5.3	753

80.59 E 80.6

w		6.6	740
st		7.2	734
eb		6.5	741
1/4		5.7	749
e		4.6	760
1/4		4.0	766
eb		4.3	763
E		4.8	758
	12'N. of E		
E		4.2	764
eb		3.9	767
1/4		3.7	769
e		4.7	759
st		5.9	747
1/4		6.3	743
eb		7.6	730
st		8.8	718
w		7.8	728
	N 1/4		
-5		10.1	705
w		9.4	714
st		9.4	714
eb		7.2	734
st		6.7	739
1/4		5.4	752
e		6.1	745

32.21 St

80.59 80.6

N. ¼ (COH)

℄ +6		6.0	746
¼		5.3	753
+6		3.9	767
cb		3.9	767
℄		4.2	764

9.4 N. of N. ¼ = S. Rail of S.P. + R.R. on W.

℄		5.2	754
+2		5.2	754
+5		6.9	737
cb		7.0	736
¼		6.5	741
+5		5.9	747
℄		7.6	730
¼		10.4	707
cb		10.0	706
W		9.19	7140 on S. Rail

N. cb

W		9.9	701
cb		9.9	701
¼		10.3	703
℄		10.6	700
+7		10.7	699
¼		9.4	712
cb		7.2	734
+4		6.7	739
℄		6.9	737

80.59

5'. N. 80.6

61

℄		7.5	731
cb		9.7	709
+4		11.0	696
¼		10.8	698
℄		10.4	702
+1 = S. Rail		9.74	7085 No yardage
¼		10.5	701
cb		11.0	696
W		10.3	703

11' N. of N. cb

W		9.2	716
+4		7.9	717
cb		9.5	711
+5		11.3	693
¼		11.5	691
℄		10.9	697
¼		10.5	701
cb		11.1	695
℄		11.3	693
+5		9.1	715

00 = N. Hm ℄ N. St

-5		11.4	694
℄		11.4	694
+9	S. Rail	10.24	7035 no yardage
cb		10.7	699
¼		11.2	691

80.59

806

C		11.7	689
+4		11.6	690
1/4		9.5	711
CB		4.2	747
+5		5.8	728
W		7.7	709

4.4 N. of N. Line = S. Rail on E

W		6.7	739
+8		5.4	75
CB		5.5	751
+7		6.1	745
1/4		6.8	738
C		9.6	710
+6		11.8	688
1/4		11.8	688
CB		11.2	691
E		11.0	696
E		10.41	70.18 on mail no yardage
+5		11.4	691

16' N

-5		12.2	687
E		12.2	688
CB		8.2	771
+5		6.6	740
1/4		6.3	743
C		6.5	741
1/4		6.7	739

80.59

806

32nd St

62

CB		6.1	745
W		6.5	741

25' N

W		6.3	743
CB		6.2	744
1/4		6.3	743
C		7.1	735
1/4		7.6	730
+5		7.8	728
CB		7.3	733
E		7.3	733

32' N

E		8.3	723
CB		7.9	727
1/4		7.5	731
C		6.8	738
1/4		6.4	742
CB		6.3	743
W		6.3	743

63' N

W		6.7	739
CB		7.0	736
1/4		7.0	736
C		7.0	736
1/4		7.5	731
CB		8.0	726
E		8.5	721

80.59

75' N 806

E	8.7	719
cb	8.3	723
1/4	7.7	729
c	7.3	733
1/4	7.1	735
cb	7.0	736
w	8.3	723

93' N.

w	9.3	713
cb	9.4	712
1/4	9.1	715
c	9.2	714
1/4	8.5	721
cb	8.9	717
E	8.9	717

105' N

E	9.8	708
cb	9.9	707
1/4	9.7	709
c	9.8	708
1/4	9.5	711
cb	9.0	716
w	8.9	717

120' N

w	8.0	726
cb	8.3	723

1/4	8.7	719
c	9.2	714
1/4	9.3	713
cb	9.8	708
E	10.1	705

150' N

E	9.8	708
cb	9.7	709
1/4	9.5	711
c	9.3	713
1/4	9.0	716
cb	8.8	718
w	8.6	720

200' N

w	7.8	728
cb	8.1	725
1/4	8.0	726
c	8.1	725
1/4	8.2	724
cb	8.2	724
E	8.3	723

250' N

E	7.5	731
cb	7.7	729
1/4	7.4	732
c	7.2	734

80.59

806

¼			7.1	73.5
cb			7.0	73.6
W			6.6	74.0
T.P.	6.78	75.90	11.47	69.12

298' N 75.9

W			1.2	74.7
cb			2.1	73.8
¼			1.7	74.2
C			1.3	74.6
¼			1.4	74.5
cb			1.5	74.4
E			1.6	74.3

300' N. = S Line Imperial on W = Sec A Page 65

E			1.7	74.2
cb			1.4	74.5
¼			1.4	74.5
C			1.6	74.3
¼			2.1	73.8
cb			3.2	72.7
+5			2.0	73.9
W			5.7	70.2

6' N of S Line Imperial - Sec B Page 65

W			6.9	69.0
cb			4.9	71.0
+5			3.2	72.7
¼			2.7	73.2

75.90

32nd ST

64

75.9

C			2.0	73.9
¼			1.4	74.5
cb			1.3	74.6
E			1.5	74.4

10' N of N Line Imperial = Sec C Page 65

E			1.4	74.5
cb			1.4	74.5
¼			1.4	74.5
C			1.8	74.1
¼			2.7	73.2
+7			3.2	72.7
cb			4.1	71.8
W			6.8	69.1

10' N of S Line Imp on W to 24' N of Imp. on E = Sec D Page 65

W			6.8	69.1
cb			3.6	72.3
¼			2.8	73.1
C			1.6	74.3
¼			1.4	74.5
cb			1.4	74.5
E			1.6	74.3

14' N of S. Line Imp on W to 28' N on E = Sec E Page 65

E			10.4	65.5
cb			9.8	66.1
¼			9.5	66.4
C			9.2	66.7

on Paving

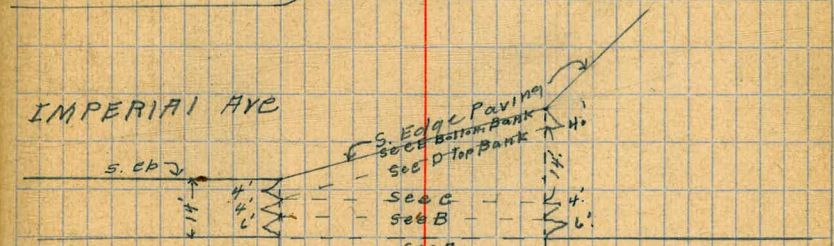
75.90

75.6

'y	9.1	668	on paving
cb	9.1	668	" "
w	8.71	6719	" curb
w	9.4	66.5	" paving
T.P.	8.70	67.20	=67.03 BMNW 32 & Hom.

32nd St

65



June 26 At Bound N. Sight Highway for 0 Az Rt

1 ✓	710	25 20	Test Well 1st North of 3	
2 ✓	665	22 5	" "	
3 ✓	630	19 10	" " Post	
4 ✓	593	15 50	" "	
5 ✓	575	14° 0	" " Auger	
6 ✓	560	12° 5	" " Holes	
7 ✓	543	10° 0	" "	
8 ✓	480	10 45	" "	
9 ✓	440	10 50	" "	
10 ✓	395	17 20	" "	
" ✓ 43 14	385	22 15	43 - 14	
12 ✓	355	21° 50	Test Well	
13 ✓ 14 ✓	450	325 25	Test Well # 3	
Bound N.a	680	291 57		

Colored

At Bound N. a Sight Bound N for 0 Az Rt

A3 22	165	95 30	in River bed	✓ 1
A3. 26	290	111 10	Bott. Bank	✓ 2
Wind Mill	525	95 20	N E Cor	✓ 3
Oil Pump H.	338	150 40		✓ 4
" Well	200	148 5	In River Bott.	✓ 5
" "	75	140 5	on South Bank	✓ 6
Test Well	145	146 10	Stake for Well in R bed	✓

July 1

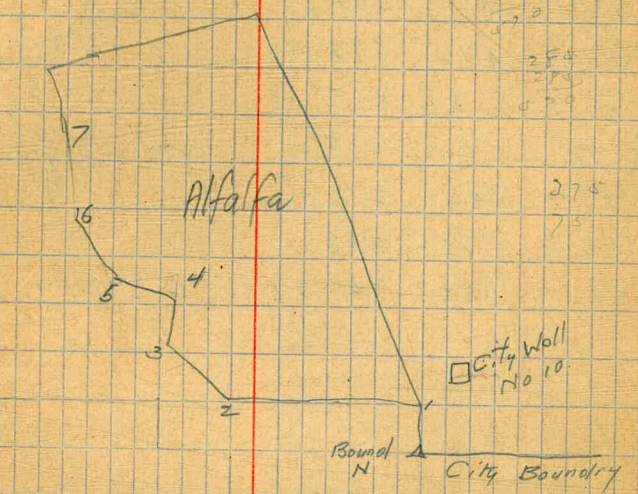
At Boundry N Sight Highway for zero Az

F. Cor. 1	10	340 50		✓	1
43 17	55	195 30		✓	2
F. Cor 2	95	256 40		✓	3
F Cor 3	335	278 20		✓	4
F Cor 4	470	289 35		✓	5
F Cor 5	700	290 15		✓	6
F Cor 6	750	293 25		✓	7
F Cor 7	830	297 35		✓	8
43 15	140	326 0	On F. line	✓	9
43 18	170	265 20	Head of Draw	✓	10
43 19	148	196 10	Top Bank	✓	11
43 16	250	107 30	Top Bank	✓	12
43 13	360	61 40		✓	13
43 12	480	82 20		✓	14
43 10	570	81 30		✓	15
43 11	568	73 15		✓	16
City Well	70	270 0	# 10	✓	17
E. EHO Bridge	107	134 0		✓	18
Bound. N B	290	149 13	On Bridge	✓	19

Checked.

At Bound N. B Sight Peck for zero Az

Bound N	290	44° 49'		
Well	140	309 20		1
NE Cor	118	300 50	Pump House	✓
43 RC 2	255	273 30		3



Checked.

At Bound N B

City Well No II	155	228 35		✓	✓
W. End	110	233 30	Bridge	✓	5
43 RC 3	150	220 10		✓	6
43 RC 1	520	249° 5'		✓	7
City Well No IV	490	241 45		✓	8
43 RC 5	630	227 10		✓	9
39 IV	520	208° 0	Head of 39	✓	10
43 RC 4	345	218 15'		✓	11
43 RC 6	870	238 10		✓	✓
Well	880	241 20	12" Casing	✓	13

Offset

Bub HR E. Schieback CL Nichols

18	8	8	8
18	8	8	8
19	8	8	8
20	0	0	0
21	8	8	
22	8	8	8
23	8	8	8
24	8	8	8
25	8	8	8
26	8	8	8
27	0	0	0
28	8	8	8
29	8	8	8
30	8	8	8
July 1	8	0	8
2	8	0	0
3	8		
4	0		
5	0		
6			

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P.=23° 20′ to the R. at Station 542+72.

Ext. in Tab. IV opposite 23° 20′=120.87
120.87÷12=10.07. Say a 10° Curve.

Tan. in Tab. IV opp. 23° 20′=1183.1
1183.1÷10=118.31.

Tab. V. correction for A. 23° 20′ for a 10° Cur.=0.16
118.31+0.16=118.47=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. 23° 20′=23.33°÷10=2.3333=L. C.

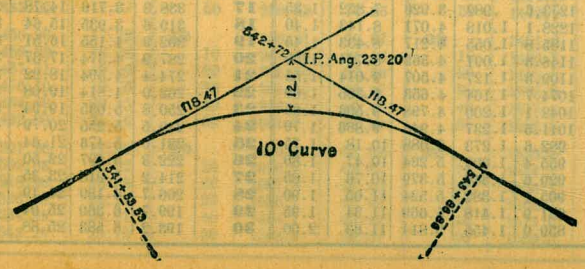
2° 19½′=def. for sta.	542	I. P.=sta.	542+72
4° 49½′= " " "	+50	Tan.=	1.18.47
7° 19½′= " " "	543	B. C.=sta.	541+53.53
9° 49½′= " " "	+50	L. C.=	2.33.33
11° 40′= " " "	543+	E. C.=sta.	543+86.86
	86.86		

100—53.53=46.47×3′(def. for 1 ft. of 10° Cur.)=139.41′=
2° 19½″=def. for sta. 542.

Def. for 50 ft.=2° 30′ for a 10° Curve.

Def. for 86.86 ft.=1° 50½′ for a 10° Curve

(These tables are published in Field Books of KEUFFEL & ESSER Co., New York, N. Y.)

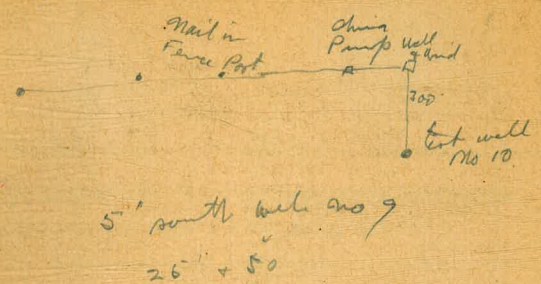


Natural Tangents

deg.	0′	10′	20′	30′	40′	50′	log.	deg.	0′	10′	20′	30′	40′	50′	deg.
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
deg.	60′	50′	40′	30	20′	10′	log.	deg.	60′	50′	40′	30′	20′	10′	deg.

deg.	0′	10′	30′	30′	40′	50′	log.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.77	0
deg.	60′	50′	40′	30′	20′	10′	deg.

Natural Cotangents



00
8
42
48
66
88
100
130

156
192
250

No 5 m.P.
Test W 6-59-11 to East.
69.12 at Gug Bridge
59.14 at upper Bridge

180
180
360

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 14 feet wide. Side Slopes 1½ to 1.

For Single Track Embankment.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44 2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.