985

F.B. 985

FIELD BOOK

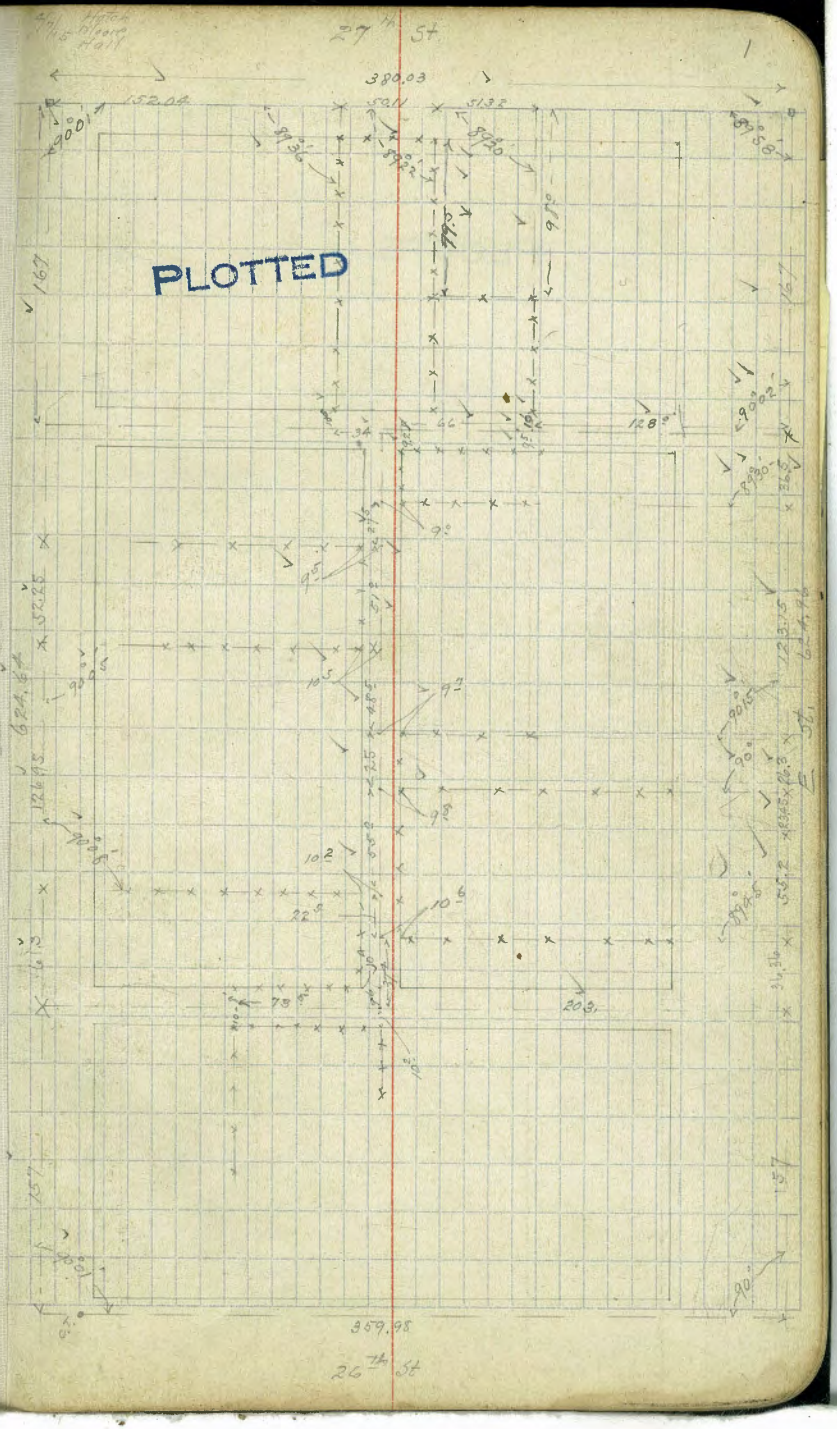
360

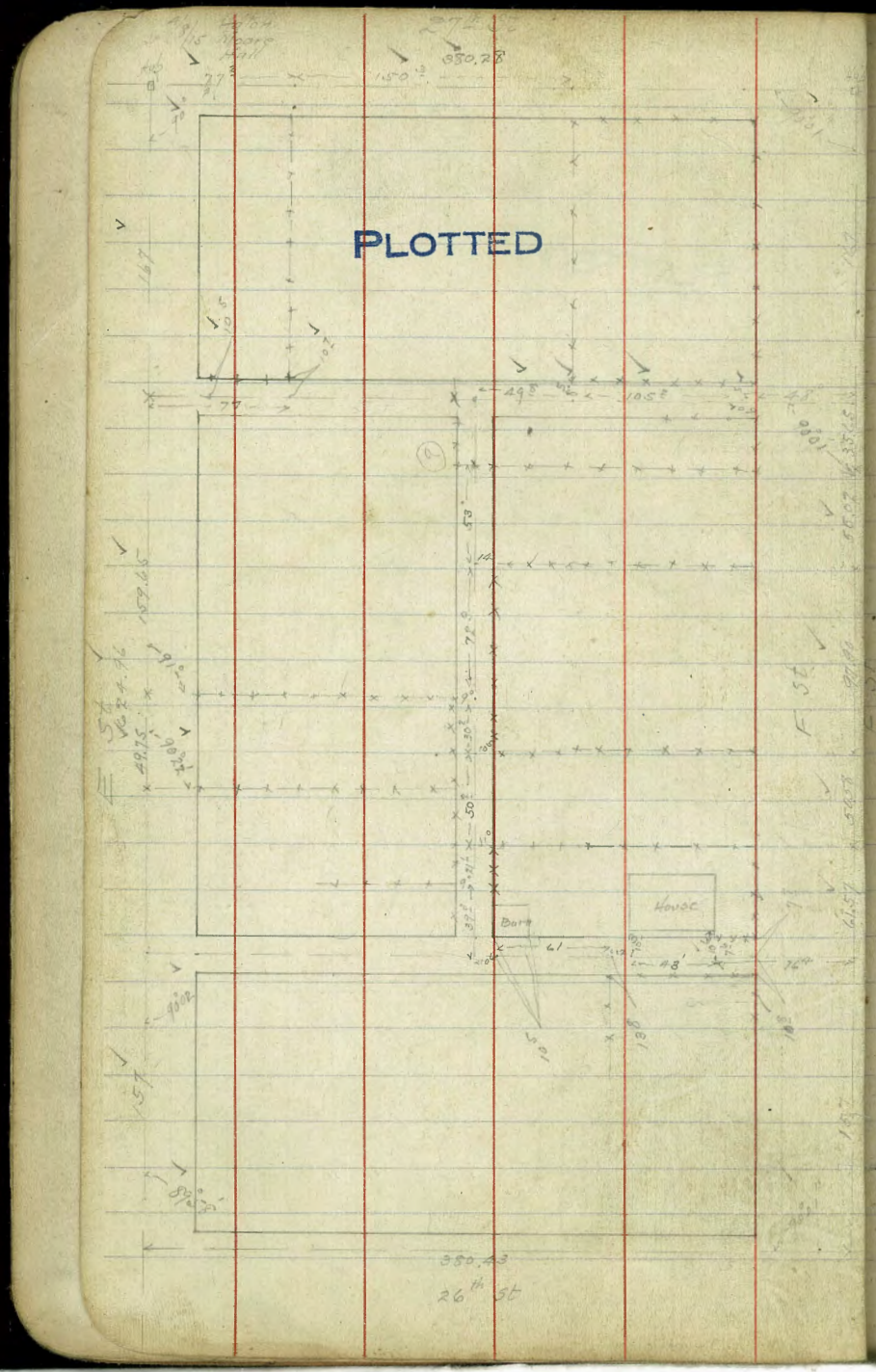
TABLES FOR EXCAVATIONS AND EMBANKMENTS.

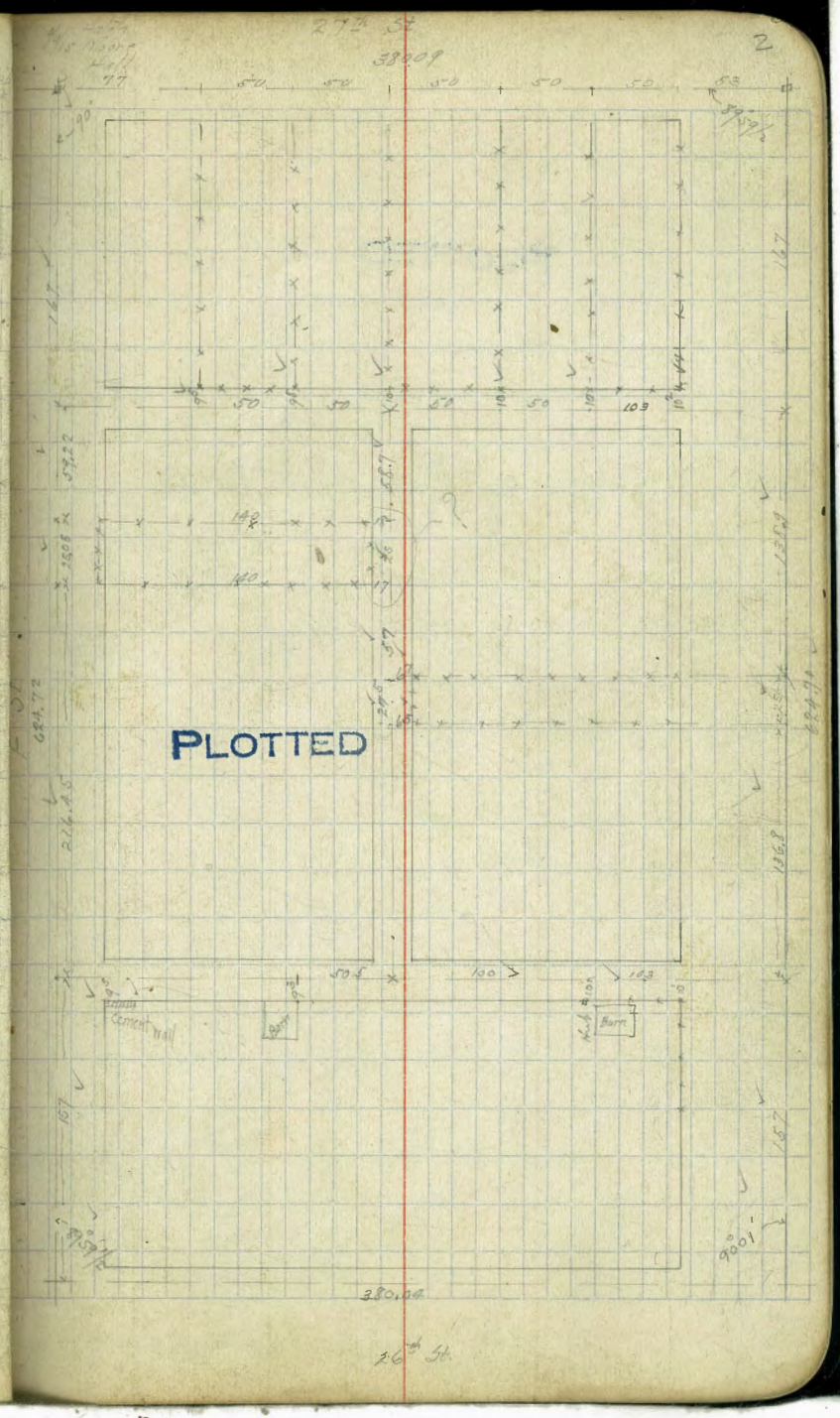
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

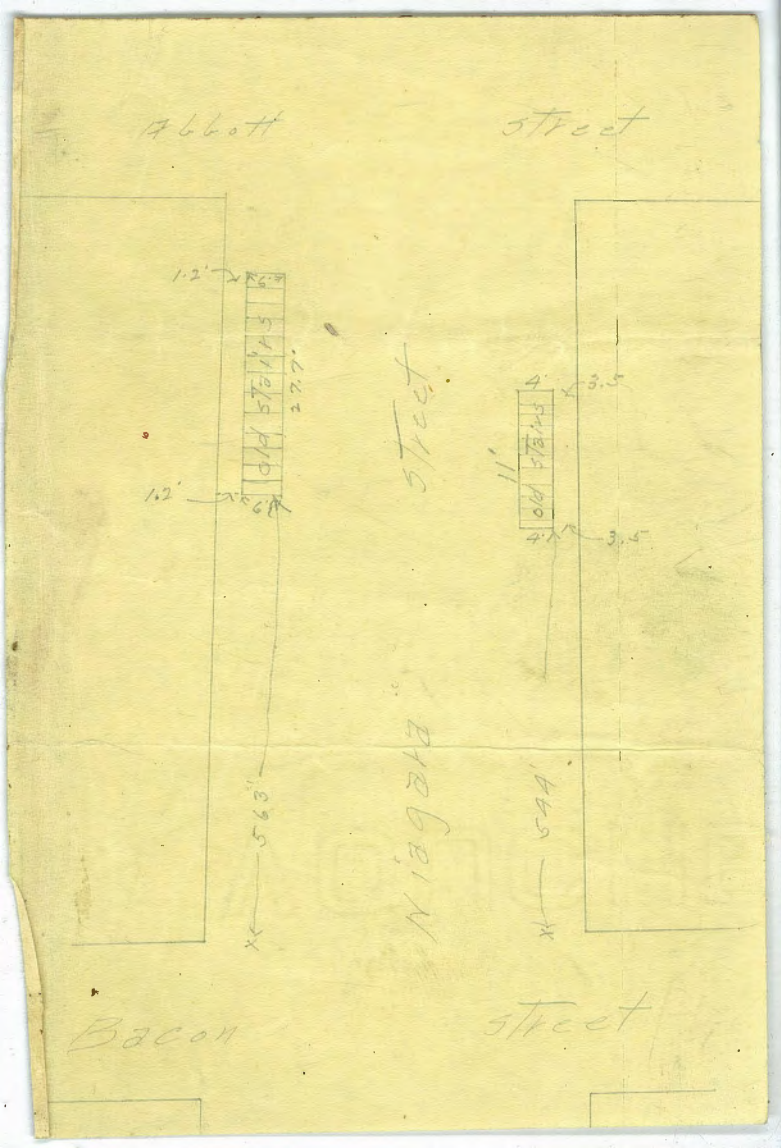
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

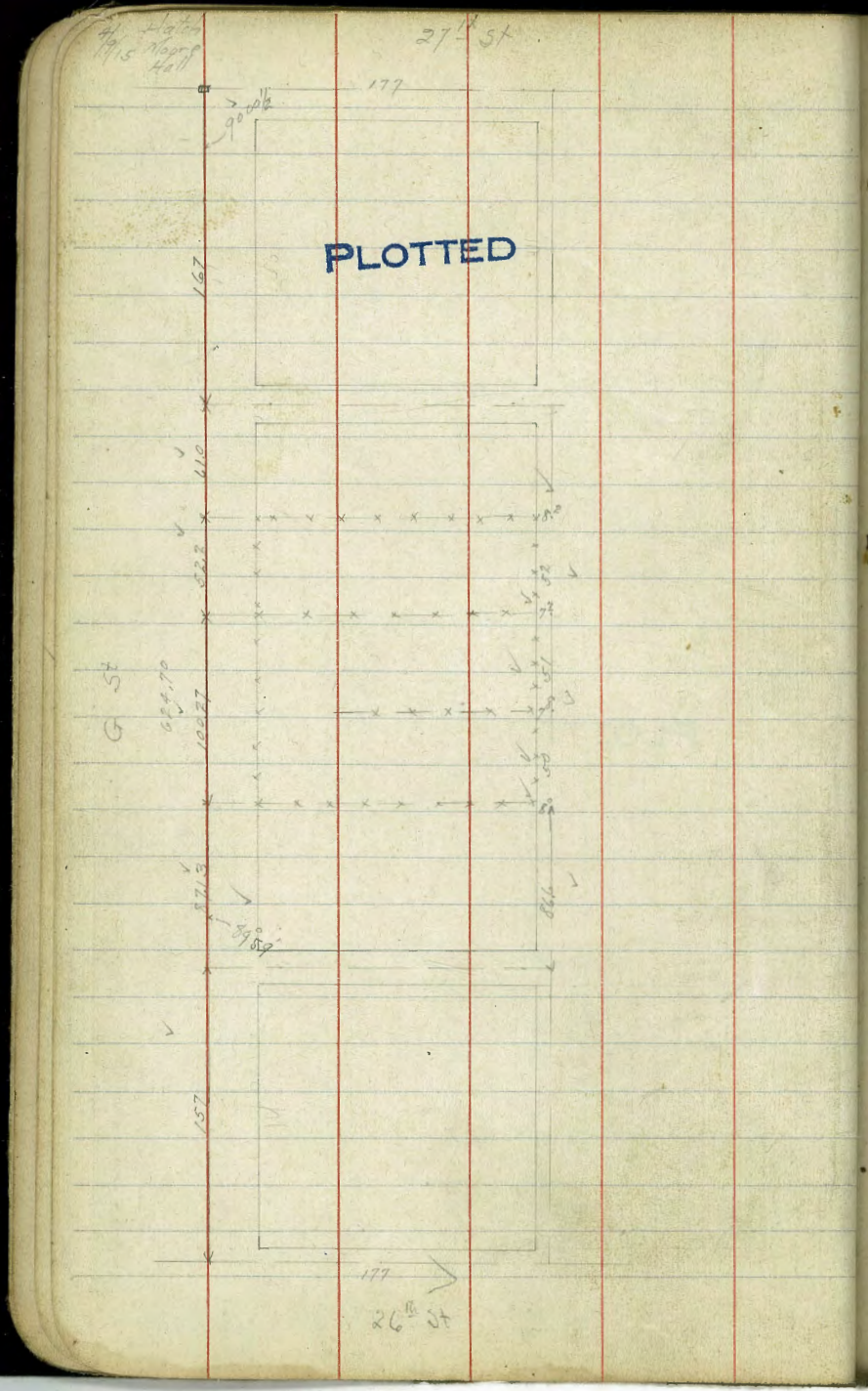
Calculated by Julien A. Hall, M. Am. Soc. C. E.

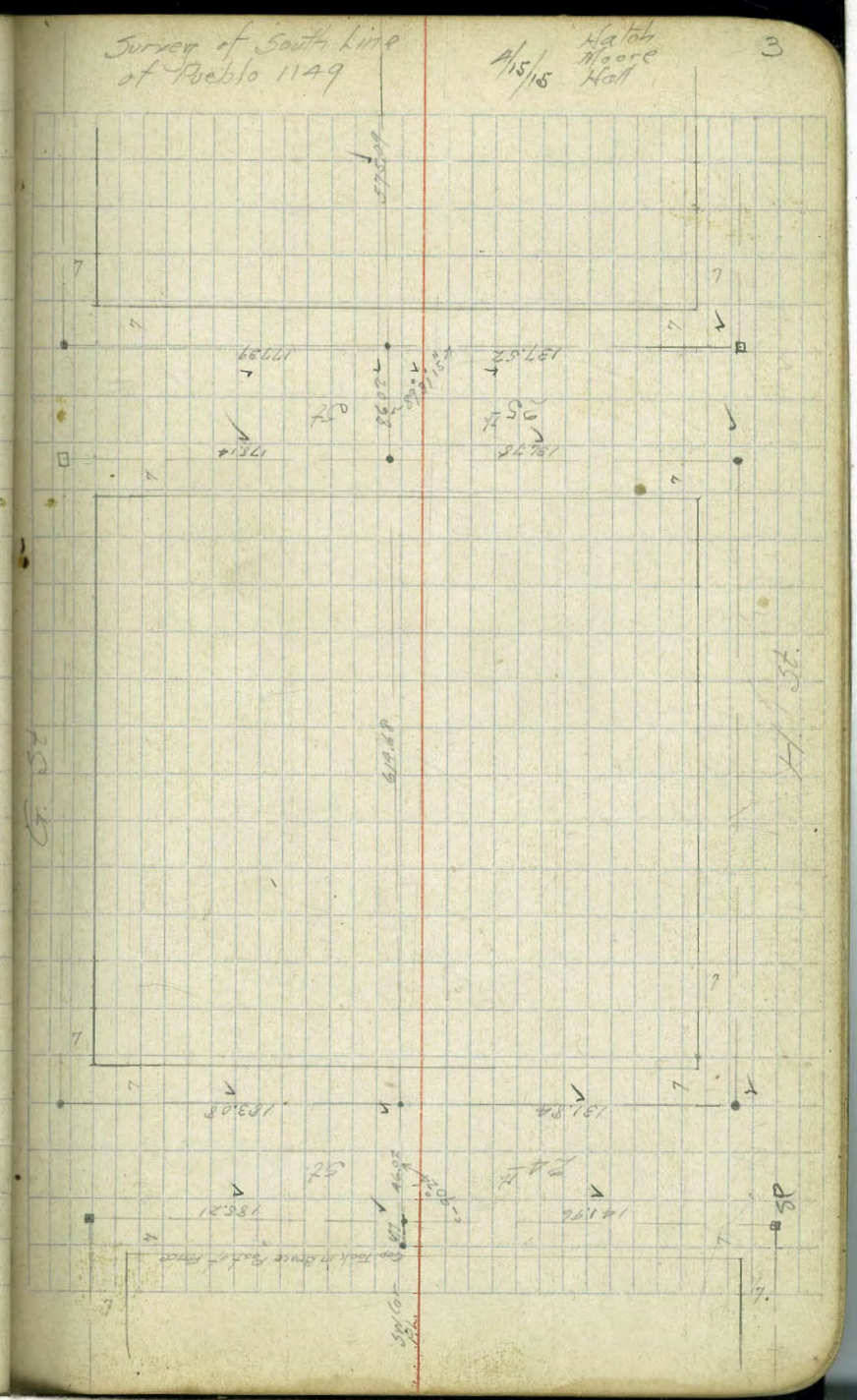

PLOTTED
27th St
380.03
959.98
26th St


PLOTTED
House
Barn
350.43
26th St


PLOTTED
Barn
380.04
26th St


Abbott
Street
1.2'
1.2'
old steps
2.7'
5.63'
Street
11'
4'
3.5'
4'
3.5'
5.44'
Bacon
Street


Hatch Moore Hall
1915
27th St
177
PLOTTED
167
610
522
713
157
G St
177
26th St


Survey of South Line of Pueblo 1149
4/15/15
Hatch Moore Hall
3
G St
137.84
SP

719.30

27th St

187.38

89°32'45"

20309

G St

H St

624.47

162.49

26th St

89°37'30"

162.85

140.93

575.09

G St

Gas

183.53

89°20'42"

89°55'24"

91°16'

43'

27th St

Tk in E end of Skid of Bridge being 20.5' S. of E of H St.

6/2/15 Gregory Moore Miller

CROSS SECTION OF M ST 40' WIDE
FROM 37th to 38th

B.M. spk	3.69	102.75	99.06	NE 37th M
		E.L. 37th St.		
S.			3.1	
+5			4.4	
+10			4.4	
+20			3.8	
+30			3.6	
N			4.3	
		50' E		
N			4.2	
+10 = So. Rail			3.85	
+20			3.8	
+30			4.3	
+36			4.7	
S			3.5	
		75' E		
S			3.1	
+4			4.8	
+10			4.4	
+20			3.8	
+30 = So. Rail			3.85	
N			4.1	
		100' E		
N			4.1	
+10 = So. R			3.83	

+20		3.8
+30		4.6
+36		5.0
S		2.7
	140' E	
S		0.9
+4		4.7
+10		4.7
+20		3.9
+30 So. Rail		4.0
N		3.8
	143' E	3.8
N		
+10' So. Rail		4.0 1
+20		3.9
+30		4.7
+35		4.9
S		4.5
	180' E	
S		4.4
+4		5.1
+10		4.7
+20		4.2
+30 = So. Rail		4.3
N		4.5

200' E	
N	4.8
+10 = So Rail	4.6
+20	4.2
+30	4.8
+37	5.2
S	4.5
250' E	
S	5.0
+10	5.0
+20	4.4
+30 = So Rail	4.8
N	5.1
275' E	
N	5.1
+10 = So Rail	5.0
+20	4.5
+30	5.0
+36	5.0
S	6.3
300' E	
S	6.0
+4	5.1
+10	5.0
+20	4.7
+30 = So Rail	5.1

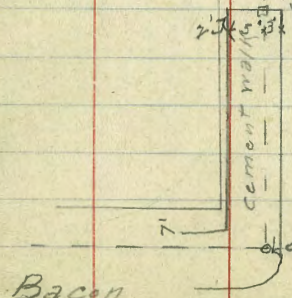
N	5.4
350' E	
N	5.5
+10 = So Rail	5.3
+20	4.9
+30	5.4
S	5.6
400' E	
S	5.1
+10	5.5
+20	5.1
+30 = So Rail	5.5
N	5.8
450' E	
N	6.6
+2	5.9
+10 = So Rail	5.7
+20	5.5
+30	5.9
+38	5.9
S	5.4
500' E	
S	5.8
+10	5.8
+20	5.6
+30 = So Rail	5.9
N	6.0

	550' E		
N		7.0	
+10 = So Rail		6.4	
+20		6.1	
+30		6.2	
+37		6.5	
S		6.0	
	575' E		
S		5.2	
+3		6.5	
+10		6.5	
+20		6.4	
+30 = So Rail		6.7	
N		6.9	
	600.5' E = W.L. 38th St.		
N		7.0	
+10 = So Rail		6.9	
+20		6.5	
+30		6.7	
+37		6.9	
S		6.6	
On BM.		6.60	96.15 = 9611

Levels for proposed steps foot of Niagara St

B.M. N.W. B.P. Bacon & Niagara	9.55	22.54		12.99
T.P.	7.36	29.53	0.37	22.17
0+00 = 7' pt Bacon St				
		5+66.56 = end of cement walk		
South			3.40	26.13
N	on cement walk		3.48	26.05
		5+75		
N			12.0	17.5
S			9.0	20.5
T.P.	0.67	17.56	12.64	16.89
		5+85		
South			3.0	14.6
+05			4.3	13.3
N			7.8	9.8
		5+94.54 = W.L. toilet produced		
N			10.4	7.2
+03			9.0	8.6
South			8.8	8.8
		6+01		
South			14.6	3.0
N			14.2	2.4
		6+07		
N			14.8	2.8
South			14.9	2.7

Abbott 7' St



Bacon St

5+66.56 = end of cement walk taken

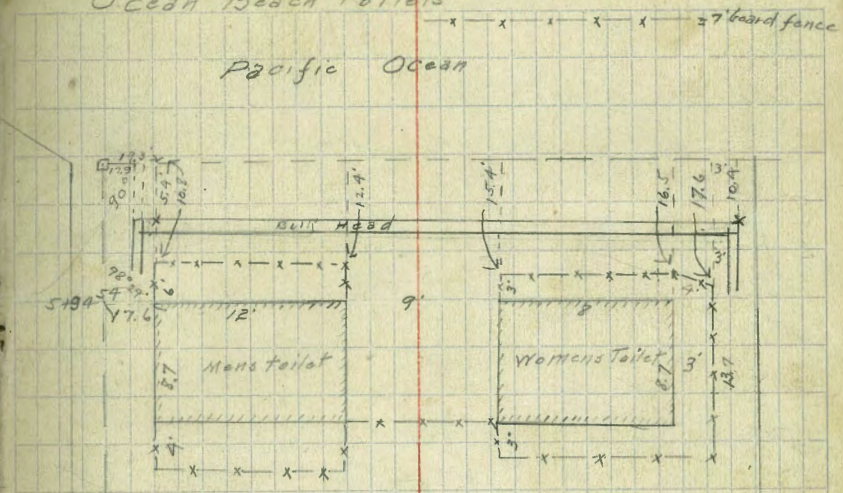
Note - X-sections, centre line of cement walk produced

8

3/14/19 Dunkle Shaw Evans

9

Ocean Beach toilets



Note - embankment back of toilet 5' above floor level

				2.56
				2.74
				5.30
	9.09	22.08		12.99
	10.53	31.28	1.63	20.45
			4.76	27.02

7' pt

Bacon St

6/3/15 Buckle
Shaw
Bunker

X-section West End of Niagara St See Sketch on opposite Page.

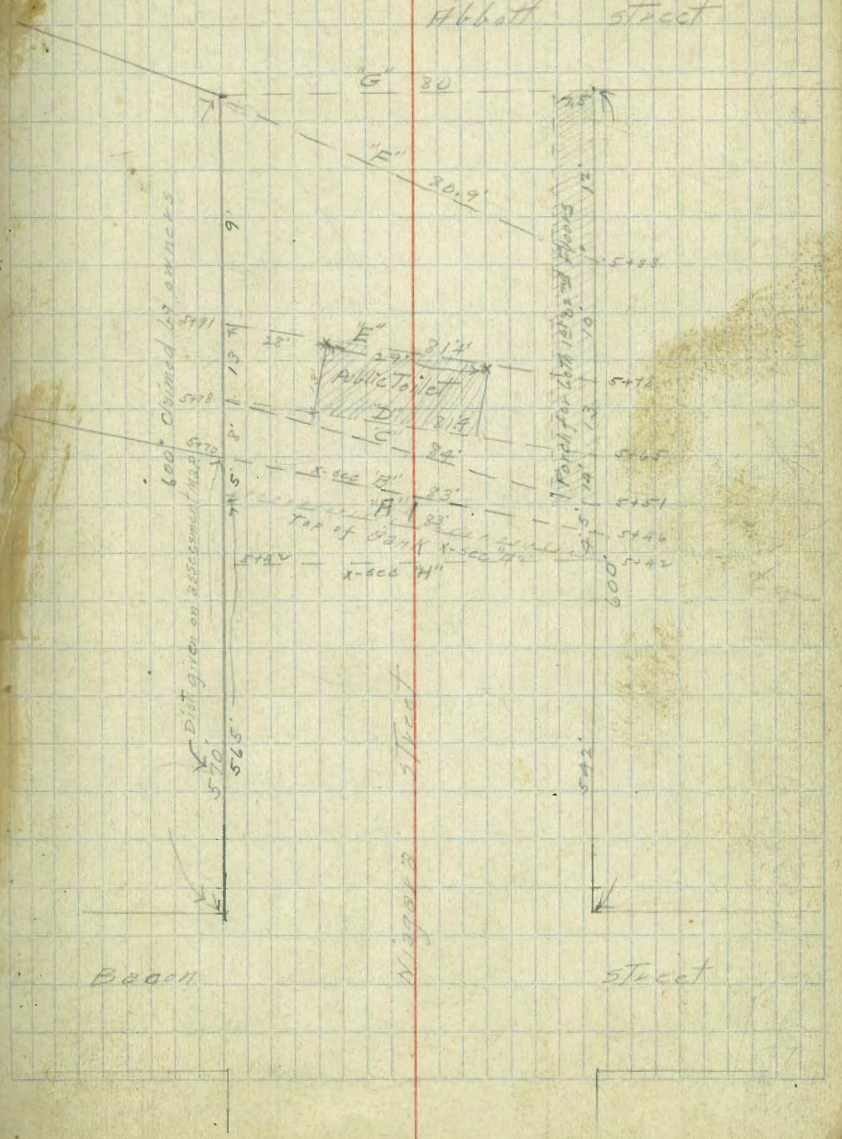
B.M. N.W. Cor Pig Niagara & Bacon				12.99
B.M.	10.37	23.36		
T.P.	8.66	30.17	1.85	21.51

X-section "H"

South			4.3	25.9
+10			4.5	25.7
+20			4.6	25.6
+30			4.4	25.8
+40			4.1	26.1
+50			4.3	25.9
+60			3.8	26.4
+70			4.3	25.9
North			4.9	25.3

X-section "A"

North			4.9	25.3
+10			4.4	25.8
+20			4.3	25.9
Top of curb			3.8	26.4
+30			4.5	25.7
+40			4.1	26.1
+50			4.2	26.0
+60			4.4	25.8
Top of curb			4.3	25.9
+70			4.7	25.5
South			4.9	25.3



30.17

x-section "B"

South			11.2	19.0
+10			11.9	18.3
+20			11.5	18.7
+30			12.7	17.5
+38			12.1	18.1
40			9.9	20.3
+50			10.4	19.8
+60			10.3	19.9
+70			13.0	17.2
+73			10.4	19.8
North			10.3	19.9
T.P.	0.86	18.02	13.01	17.16

x-section "C"

North			0.9	17.1
+10			6.4	11.6
+17			4.3	13.7
+20			0.7	17.3
+30			1.3	16.7
+40			3.5	14.5
+50			5.4	12.6
+58			5.4	12.6
+60			3.7	14.3
+70			5.9	12.1
+74			7.4	10.6
+76			3.4	14.6
South			3.7	14.3

18.02

x-section "D"

South			3.7	14.3
+05			4.1	13.9
+07			8.0	10.0
+10			7.6	10.4
+17			6.3	11.7
+20			7.4	10.6
+23			7.4	10.6
+24			12.4	5.6
+30			12.4	5.6
+40			12.4	5.6
+50			12.4	5.6
+55			12.4	5.6
+56			8.9	9.1
+60			8.0	10.0
+64			8.2	9.8
+70			10.6	7.4
North			11.3	6.7
T.P.		4.22	9.61	12.63	5.39

9.61

X-section "E"

North	2.9	6.7
+10	3.0	6.6
+20	2.8	6.8
+30	2.9	6.7
+40	4.2	5.4
+50	4.4	5.2
+60	4.3	5.3
+70	2.9	6.7
South	2.8	6.8

X-section "F"

South	5.0	4.6
+10	4.6	5.0
+20	4.4	5.2
+30	4.8	4.8
+31	5.9	3.7
+40	6.0	3.6
+49	5.9	3.7
+45	4.7	4.9
+50	4.5	5.1
+60	4.4	5.2
+62	5.3	4.3
+70	3.9	5.7
North	3.7	5.9

9.61

North	8.2	1.4
+10	8.1	1.5
+20	8.1	1.5
+30	7.8	1.8
+40	7.7	1.9
+50	7.3	2.3
+60	6.4	3.2
+67	5.0	4.6
+70	5.2	4.4
South	5.0	4.6

	+R	H.I	− R	Elev
B.M. Grass p/g N.E. Abbott & Newport				6.50
	4.89	11.39		
Elev curb So end Benbough Bldg			5.43	6.26
T.P.	1.56	3.32	9.63	1.76
"A"			1.56	1.76
"B"			11.30	0.02
No end curb concrete Bldg			0.49	2.83
So " " " "			0.00	3.32
"C"			2.02	1.30
No end concrete Bldg			3.57	−0.27
So " " " "			3.51	−0.19
"D"			4.32	−1.00
"E"			3.06	+0.26
"O"				−2.20
Rock at N End wall				−2.00
Approx Sand				−6.00

See End of Book

10/2/18 Dunkle Shaw Evans

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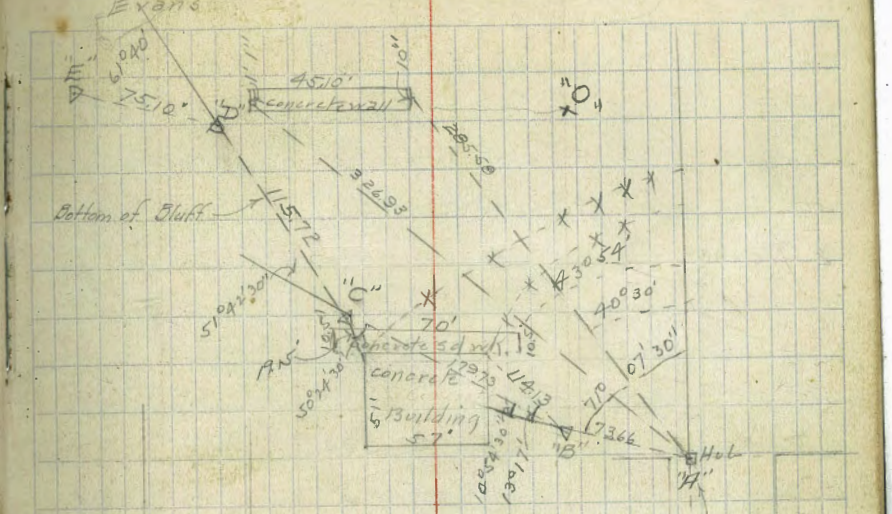


See End of Book

Gregory
Moore
Miller

X-SECTION OF FILL ON
H 5
Between Pascoe and

B.M.	0.80.	138.65		137.85
T.P.	1.18	128.31	11.52	127.13

50' East of Pascoe = 00' on North

70' " " "

40' No. of ℄		8.4	119.9
31' " "		7.6	120.7
24' " "		4.6	123.7
15' " "		3.5	124.8
℄		3.0	125.3
15' So. of ℄		3.5	124.8

80' East of Pascoe = 00' on South

95' " " "

30' So. of ℄		5.6	122.7
15' " "		3.8	124.5
℄		3.2	125.1
19' No. of ℄		3.8	124.5
30' " "		10.0	118.3
46' " "		10.3	118.0
54' " "		11.6	116.7

120' E

55' " "		14.1	114.2
50' " "		12.5	115.8
28' " "		12.8	115.5
15'		3.8	124.5
℄		3.3	125.0

50' tie hub No. of H at Pascoe

128.3 N9.

14

15' So. of ℄		3.8	124.5
13' " "		9.6 = toe	118.7

145' E.

29' So. of ℄		15.6 = toe	112.7
15' " "		4.2	124.1
℄		3.6	124.7
15' No. of ℄		4.2	124.1
35' " "		12.8	115.5
40' " "		15.2	113.1
54' " "		15.2	113.1
58' " "		18.4	109.9

170' E.

61' No. of ℄		21.6	107.3
53' " "		17.9	110.4
40' " "		18.2	110.1
28' " "		14.5	113.8
16' " "		4.4	123.9
℄		4.1	124.2
15' So. of ℄		4.4	123.9
T.P.	4.28 124.37	8.22	120.09
40' So. of ℄		17.2	107.2

195' E.

43' So. of ℄		21.6	102.8
15' " "		0.7	123.7
℄		0.3	124.1
15' No. of ℄		0.7	123.7

30' No. of ℄		11.8	112.6
40' " "		15.4	109.0
53' " "		15.7	108.7
62' " "		21.0	103.4
	220' E		
60' No. of ℄		19.9	104.5
53' " "		16.9	107.5
40' " "		15.4	109.0
30' " "		12.8	111.6
15' " "		1.0	123.4
℄		0.5	123.9
15' So. of ℄		1.0	123.4
50' " "		28.3	96.1
	245' E		
42' So. of ℄		21.7	103.2
15' " "		1.3	123.1
℄		0.8	123.6
15' No. of ℄		1.3	123.1
30' " "		12.7	111.7
38' " "		15.6	108.8
	270' E		
32' No. of ℄		12.1	112.3
37' " "		10.8	113.6
15' " "		1.6	122.8
℄		1.1	123.3
15' So. of "		1.6	122.8

33' So. of ℄		15.2	109.2
	295' E		
29' So. of ℄		12.0	112.4
15' " "		1.9	122.5
℄		1.4	123.0
15' No. of "		1.9	122.5
28' " "		11.3	113.1
	320' E		
27' No. of ℄		11.3	113.1
15' " "		2.3	122.1
℄		1.8	122.6
15' So. of "		2.3	122.1
27' " "		11.6	112.8
	345' E		
28' So. of ℄		12.3	112.1
15' " "		2.8	121.6
℄		2.3	122.1
16' No. of "		2.8	121.6
26' " "		10.4	114.0
	370' E		
27' No. of ℄		12.4	112.0
15' " "		3.2	121.2
℄		2.7	121.7
15' So. of ℄		3.2	121.2
28' " "		12.6	111.8

	124.37		H ST.
	395' E		
29' So. of ℄		14.1	110.3
15' " "		3.4	121.0
℄		2.9	121.5
15' No. of "		3.4	121.0
28' " "		12.3	112.1
	420' E		
28' No. of ℄		12.9	111.5
15' " "		3.6	120.8
℄		3.1	121.3
15' So. of "		3.6	120.8
30' " "		15.3	109.1
	445' E		
31' So. of ℄		16.4	108.0
15' " "		3.9	120.5
℄		3.4	121.0
16' No. of "		3.9	120.5
27' " "		12.5	111.9
	470' E.		
30' No. of ℄		15.2	109.2
15' " "		4.2	120.2
℄		3.7	120.7
15' So. of "		4.2	120.2
34' So. of ℄		18.8	105.6

	1244 K.9.		
	495' E		
37' So. of ℄		21.5	102.9
15' " "		4.4	120.0
℄		3.9	120.5
15' No. of "		4.4	120.0
37' " "		17.1	107.3
	520' E		
33' No. of ℄		17.8	106.6
15'		4.6	119.8
℄		4.1	120.3
15'		4.6	119.8
41' So.		24.6	99.8
	535' E		
42' So. of ℄		25.3	99.1
15' " "		4.9	119.5
℄		4.4	120.0
15' No. of "		4.9	119.5
32' " "		17.6	106.8
	545' E		
32' No. of ℄		17.4	107.0
15'		5.0	119.4
℄		4.5	119.9
15' So. of "		5.0	119.4
41' " "		23.6	100.8

		124.37		H ST.
		560' E		
39' So. of ℄			23.0	101.4
15'			5.2	119.2
℄			4.7	119.7
15' No. of ℄			5.2	119.2
30' " " "			16.5	107.9
		570' E		
30' No. of ℄			16.2	108.2
15' " " "			5.2	119.2
℄			4.7	119.7
15' So. of "			5.2	119.2
37' " " "			19.8	104.6
42' " " "			21.6	102.8
		595' E		
34' So. of ℄			19.3	105.1
15' " " "			5.5	118.9
℄			5.0	119.4
15' No. of "			5.5	118.9
28' " " "			12.5	111.9
		620 E		
24' No. of ℄			11.9	112.5
15' "			5.8	118.6
℄			5.3	119.1
15' So. of "			5.8	118.6
32' " " "			17.5	106.9

		103.1 163		124.4 [illegible] 21 16.6
		645 E		
33' So. of ℄			16.7	107.7
15' " " "			6.0	118.4
℄			5.5	118.9
15' No. of "			6.0	118.4
25' " " "			13.9	110.5
		670 E		
28' No. of ℄			15.0	109.4
15' No. of ℄			6.3	118.1
℄			5.8	118.6
15' So. of "			6.3	118.1
21' " " "			7.9	116.5
37' " " "			19.3	105.1
T.P.	6.59	123.62	7.3	117.03
		695' E		
44' So. of ℄			25.7	97.9
18' " " "				115.9
15' " " "			5.9	117.7
℄			5.3	118.3
16' No. of "			5.9	117.7
31' " " "			16.6	107.0
		720' E		
40' No. of ℄			21.4	102.2
16' " " "			6.2	117.4
℄			5.7	117.9
15' So. of "			6.2	117.4
21' " " "			6.3	116.3

	12362		H ST.
53 So. of ℄		31.1	92.5
	730' E		
53 So. of ℄		31.6	92.0
21' " "		8.5	115.1
15' " "		6.1	117.5
℄		5.6	118.0
16 No. of "		6.1	117.5
41' " "		23.4	100.2
	745' E		
41 No. of ℄		25.0	98.6
17' " "		6.1	117.5
℄		5.6	118.0
15 So. of "		6.1	117.5
22' " "		7.1	116.5
51' " "		28.9	94.7
	760 E		
43 So. of ℄		25.3	98.3
18' " "		6.1	117.5
15' " "		6.0	117.6
℄		5.5	118.1
16 No. of "		6.0	117.6
45' " "		26.3	97.3
	770' E		
47 No. of ℄		27.6	96.0
16' " "		5.6	118.0
℄		6.1	117.5

	12369		
15 So. of ℄		5.6	118.0
18' " "		5.9	117.7
41' " "		23.3	100.3
	795' E		
36 So. of ℄		20.0	103.6
18' " "		5.9	117.7
15' " "		5.6	118.0
℄		5.1	118.5
15' No. of "		5.6	118.0
35' " "		19.3	104.3
	820' E		
27' No. of ℄		14.5	109.1
15' " "		5.3	118.3
℄		4.8	118.8
15 So. of "		5.3	118.3
17' " "		5.9	117.7
	845' E		
28 So. of ℄		14.1	109.5
15' " "		5.0	118.6
℄		4.5	119.1
15' No. of "		5.0	118.6
21' " "		9.6	114.0
	870' E		
20' No. of ℄		8.1	115.5
15' " "		4.7	118.9
℄		4.2	119.4

123.62

H ST.

15' So. of ℄	4.7	118.9
27' " "	13.9	109.7
895' E		
32' So. of ℄	16.4	107.2
15' " "	4.1	119.5
℄	3.6	120.0
15' No. of "	4.1	119.5
20' " "	7.9	115.7
920' E		
23' No. of ℄	9.2	114.4
15' " "	3.6	120.0
℄	3.1	120.5
15' So. of "	3.6	120.0
36' " "	19.4	104.2
945' E		
40' So. of ℄	21.7	101.9
15' " "	3.0	120.6
℄	2.5	121.1
15' No. of "	3.0	120.6
26' " "	10.9	112.7
951' E		
27' No. of ℄	11.3	112.3
15' " "	2.9	120.7
℄	1.4	121.2
15' So. of "	2.9	120.7
47' " "	26.2	97.4

123.6H.S

970' E.

42' So. of ℄	21.5	102.1
15' " "	2.5	121.1
℄	2.0	121.6
15' No. of "	2.5	121.1
31' " "	13.8	109.8
995' E		
35' No. of ℄	16.2	107.4
15' " "	1.9	121.7
℄	1.4	122.2
15' So. of ℄	1.9	121.7
42' " "	20.6	103.0
1012' E		
38' So. of ℄	18.1	105.5
15' " "	1.5	122.1
℄	1.0	122.6
15' No. of "	1.5	122.1
35' " "	15.8	107.8
1020' E		
32' No. of ℄	13.3	110.3
15' " "	1.3	122.3
℄	.08	122.8
15' So. of "	1.3	122.3
36' " "	17.1	106.5

	1236℄		H ST.
	1045 E		
31'50.0 X ℄		12.9	110.7
15' " "		0.8	122.8
℄		0.3	123.3
15' No.0 X "		0.8	122.8
26' " "		8.9	114.7
	1070 E		
20' No.0 X ℄		3.0	120.6
15' " "		0.3	123.3
℄		+ 0.2	123.8
15'50.0 X "		0.3	123.3
26' " "		8.6	115.0
	1095 E = 0.0		
Ctr B.M.		4.50	1191.2 = .0

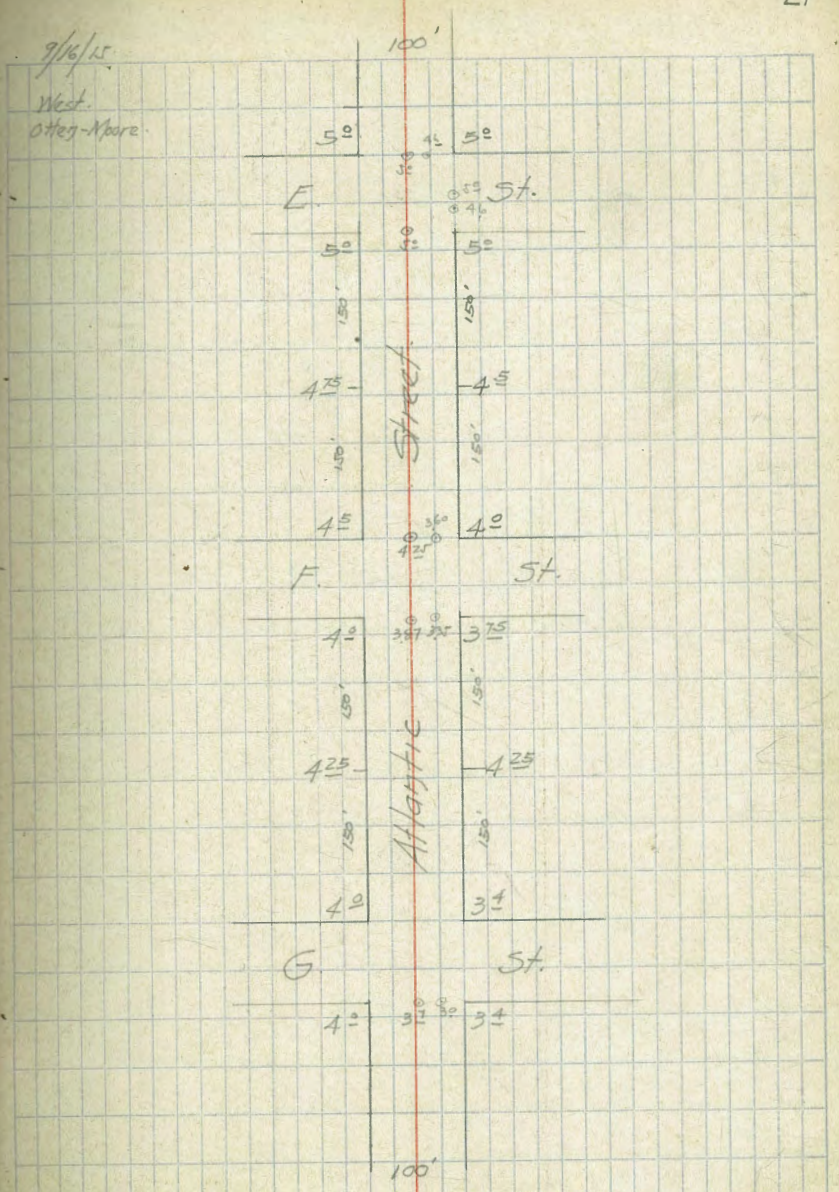
Levels for Valve Casings for Water Dept
on Atlantic at E, F, & G Sts.

BM SE #8 Atlantic Plug.			3.20
	4.84	8.04	
Grade SL G St; Approx E ¼ Atlantic		5.04	3.00 ✓
" " F " " " "		4.69	3.35 ✓
" NL " " " " "		4.44	3.60 ✓
T.P.		3.29	4.75
	4.07	8.82	
Grade EL Atlantic, aprox ¼ of E		4.22	4.60 ✓
" NL E St. " E ¼ Atlantic		4.22 ✓	4.60 ✓

Casings average from 17ft to 20ft E of E Atlantic, so set stakes 0.4' below curb grade.

9/16/15

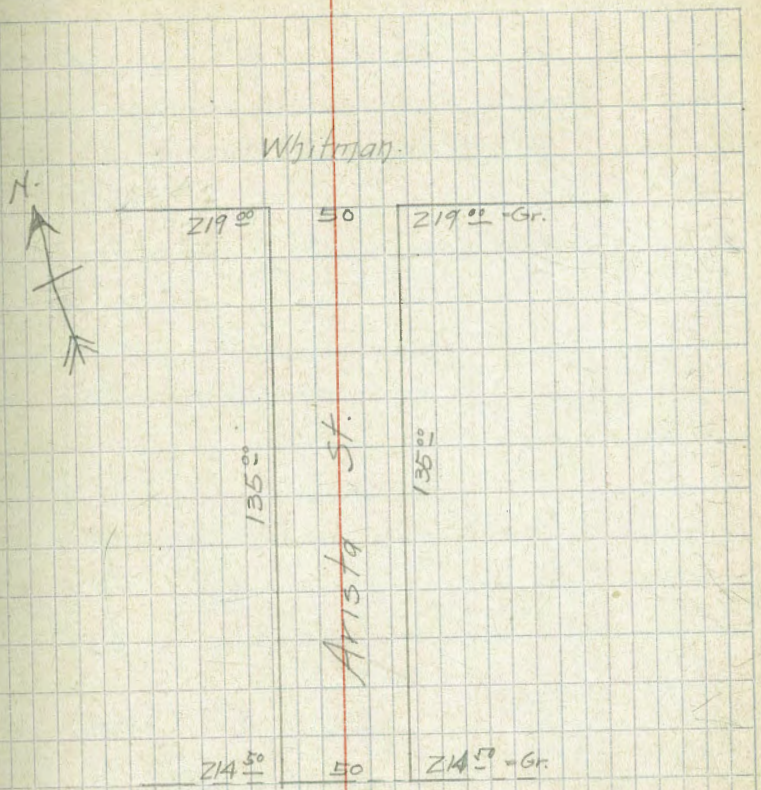
West.
Otteg-Moore



Arista Street levels for grade.
S/ Whitman to 135 ft South

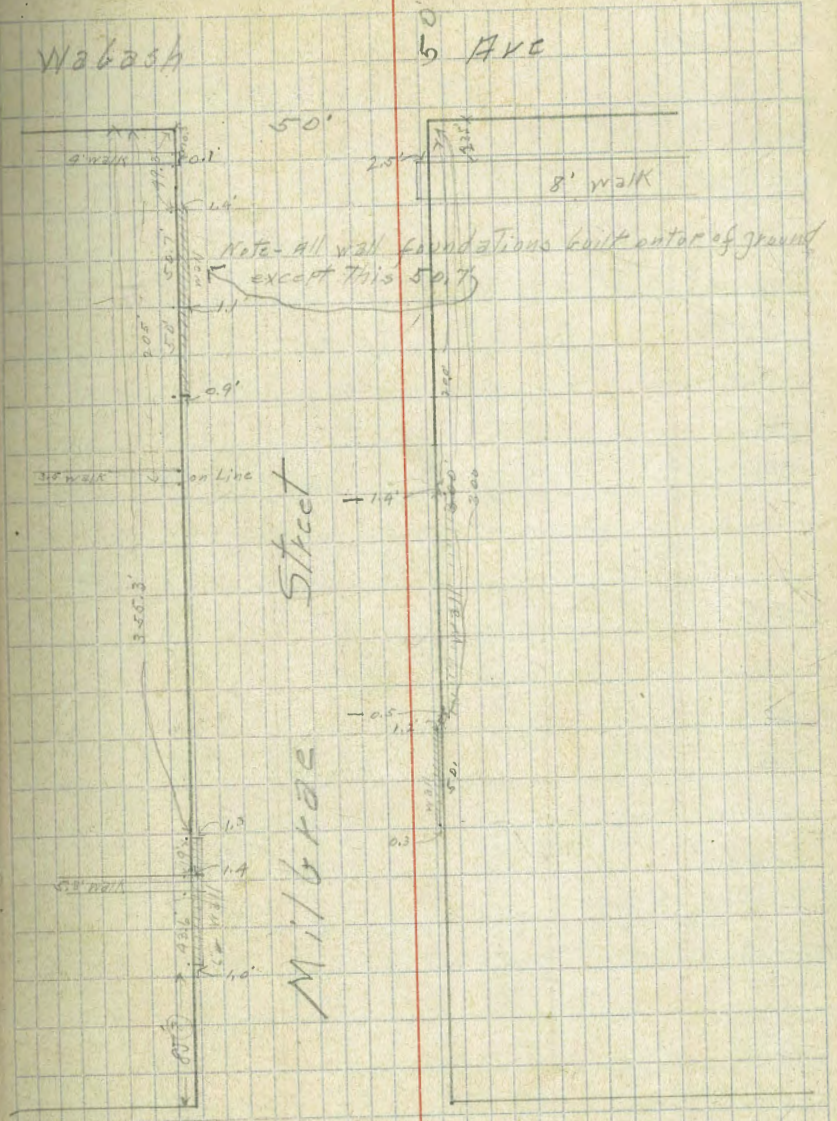
B.M. NE Trias 8 Ft	Stockton Flag			267.06	
T.P.	1.78	268.84	12.29	256.55	
T.P.	0.96	257.51	11.82	245.69	
T.P.	1.76	247.45	12.07	235.38	
T.P.	1.66	237.04	12.68	224.36	
	1.75	226.11			Gr.
	S/ Whitman				
W. Curb			7.2	218.9	219.00
E "			7.3	218.8	219.00
	50' S.				
E Curb.			8.8	217.3	217.33
W "			8.7	217.4	217.33
	100' S.				
W Curb			10.5	215.6	215.67
E "			10.4	215.7	215.67
	135' S = end grading				
E Curb.			11.6	214.5	214.50
W. "			11.9	214.2	214.50

Plan of W. West-Otten-Moore.



X-Section of Milvae Street from S.L. Wabash Ave to N.L. "D" Street

B.M. R.R. Spk	N.E. 37th & Sigel	2.59	101.65	99.06
T.P.	0.52	89.23	12.94	88.71
T.P.	8.39	91.95	6.67	82.56
	0+00 = S.L. Wabash Ave			
W	10' Curb		6.6	84.9
Crb	7½ 1/4		7.1	84.4
41			7.8	83.7
1.05			8.0	83.5
1/4			7.7	83.8
M			7.9	83.6
1/4			7.4	83.1
+05			8.7	82.8
Crb			8.5	83.0
E			9.0	82.5
	0+10.3 = Sdwk N.L.			
			6.9	84.6
	0+25 S of Wabash			
E=Topwalk			10.5	81.0
Crb			10.5	81.0
1/4			10.3	81.2
M			9.5	82.0
1/4			9.2	82.3
Crb			9.1	82.4
+1			8.8	82.7
+08			8.5	83.0
W			8.0	83.5
T.P.	5.19	85.07	11.27	79.88



MILGRAE ST.

85.07

		0+50		
W-top wall			1.9	83.2
+21.4 ground			3.9	81.2
+1.4 bottom wall			4.9	80.2
crb			4.3	80.8
+0.3			4.8	80.3
1/4			4.8	80.3
M			4.9	80.2
1/4			5.8	79.3
crb			6.1	79.0
E			5.8	79.3
		0+75		
E			8.3	76.8
crb			7.8	77.3
1/4			7.6	77.5
M			6.6	78.5
1/4			6.2	78.9
crb			6.1	79.0
+0.9			6.1	79.0
W-step			5.4	79.7
T.P.	2.39	82.27	5.19	79.88

82.27+1

	1+0		
west top wall		0.5	81.8
+0.1 - ground		4.7	77.6
+0.1 - bottom wall		5.4	76.9
crb		5.0	77.3
+0.5		6.0	76.3
1/4		5.8	76.5
M		5.9	76.4
1/4		6.7	75.6
crb		6.7	75.6
E		7.0	75.3
	1+25		
E		8.9	73.4
crb		8.6	73.7
1/4		8.6	73.7
M		7.9	74.4
1/4		8.1	73.2
crb		7.3	75.0
+0.9		6.4	75.9
W-top wall		4.2	77.1
			78.1

MILBRAE ST.

		NO. 82.27		
NE. Top nail		1+50	6.4	75.9
+01			8.6	73.7
Crk			9.4	72.9
+03			10.0	72.3
"4			10.1	72.2
M			10.0	72.3
"4			10.6	71.8
crk			10.4	71.9
E			10.6	71.7
		1+75		
E			12.1	70.2
crk			12.3	70.0
+03			12.6	69.7
"4			12.1	70.2
M			11.6	70.7
"4			12.2	70.1
+05			12.4	69.9
crk			11.5	70.8
+09			11.2	71.1
W			10.3	72.0
T.P.	0.34	70.18	12.43	69.34

70.18

2+0

W	0.6	69.6
+02	1.2	69.0
Crk	1.5	68.7
+02	1.9	68.3
"4	1.5	68.7
M	1.0	69.2
"4	1.4	68.8
+05	2.0	68.2
crk	1.4	68.8
E	1.1	69.1
Top nail	+ 0.7	70.9
2+05		
West nail	0.7	69.5
2+25		
Top nail	0.2	70.0
E	2.0	68.2
crk	2.3	67.9
"4	2.4	67.8
M	2.2	68.0
"4	2.9	67.3
crk	2.8	67.4
+08	2.5	67.7
W	1.8	68.4

70.18 N9 — MILBRAE ST.

2+50		
W	3.9	66.3
Crb	3.9	66.3
to 4	4.3	65.9
1/4	3.9	66.3
M	3.9	66.3
1/4	3.4	66.8
Crb	3.1	67.1
E	2.8	67.4
Top wall	1.0	69.2
2+75		
Top wall		
E	3.5	66.7
Crb	3.9	66.3
1/4	4.1	66.1
M	4.0	66.2
1/4	4.7	65.5
crb	4.8	65.4
W	5.2	65.0
3+0		
W	6.3	63.9
Crb	5.7	64.5
+0.2	6.1	64.1
1/4	5.6	64.6
M	4.9	65.3
1/4	5.2	65.0
Crb	5.3	64.9
+0.8	4.9	65.3
E Top wall	3.4	66.8

70.2 N9

3+25		
E Top wall	4.1	65.1
+0.08	5.3	64.9 / 64.0
Crb	6.2	63.0
1/4	6.4	63.8
M	6.0	64.2
1/4	6.6	63.6
Crb	6.5	63.7
W	6.7	63.5
3+50		
W	7.4	62.8
Crb	7.0	63.2
1/4	7.2	63.0
M	6.7	63.5
1/4	7.0	63.2
Crb	6.6	63.6
+0.9.7	6.2	64.0
E Top wall	4.4	65.8
3+75		
E	6.0	64.2
Top	6.6	63.6
Crb	6.9	63.3
1/4	7.6	62.6
M	7.2	63.0
1/4	7.6	62.6
Crb	7.7	62.5
W Top wall	7.6	62.6
3+85.3		63.1
Top wall	7.1	63.2

MILBRAE ST.

70.18 HG

3+74		
Top Wall	7.0	63.2
4+0		
W	8.5	61.7
+00 Top Wall	7.0	63.2
Crb	8.4	61.8
1/4	8.4	61.8
M	8.0	62.2
1/4	8.0	62.2
Crb	7.4	62.8
+07	7.0	63.2
E	6.6	63.6
4+25		
E	7.5	62.7
+03	8.2	62.0
Crb	8.4	61.8
1/4	8.9	61.3
M	8.8	61.4
1/4	9.2	61.0
Crb	9.0	61.2
W	9.4	60.8

70.18

4+40 = MILBRAE "Q" ST

W	10.3	59.9
Crb	9.8	60.4
1/4	10.0	60.2
M	9.3	60.9
1/4	9.1	61.1
Crb	9.0	61.2
E	8.6	61.6

Elev. checked To Bench 37 B Woolman

X-section Wabash Ave from E.L. 37th to N.L. 38th
Wabash 50' wide 10' walks 7½ 11½
B.M. 10.76 Elev carried from page 28 82.56

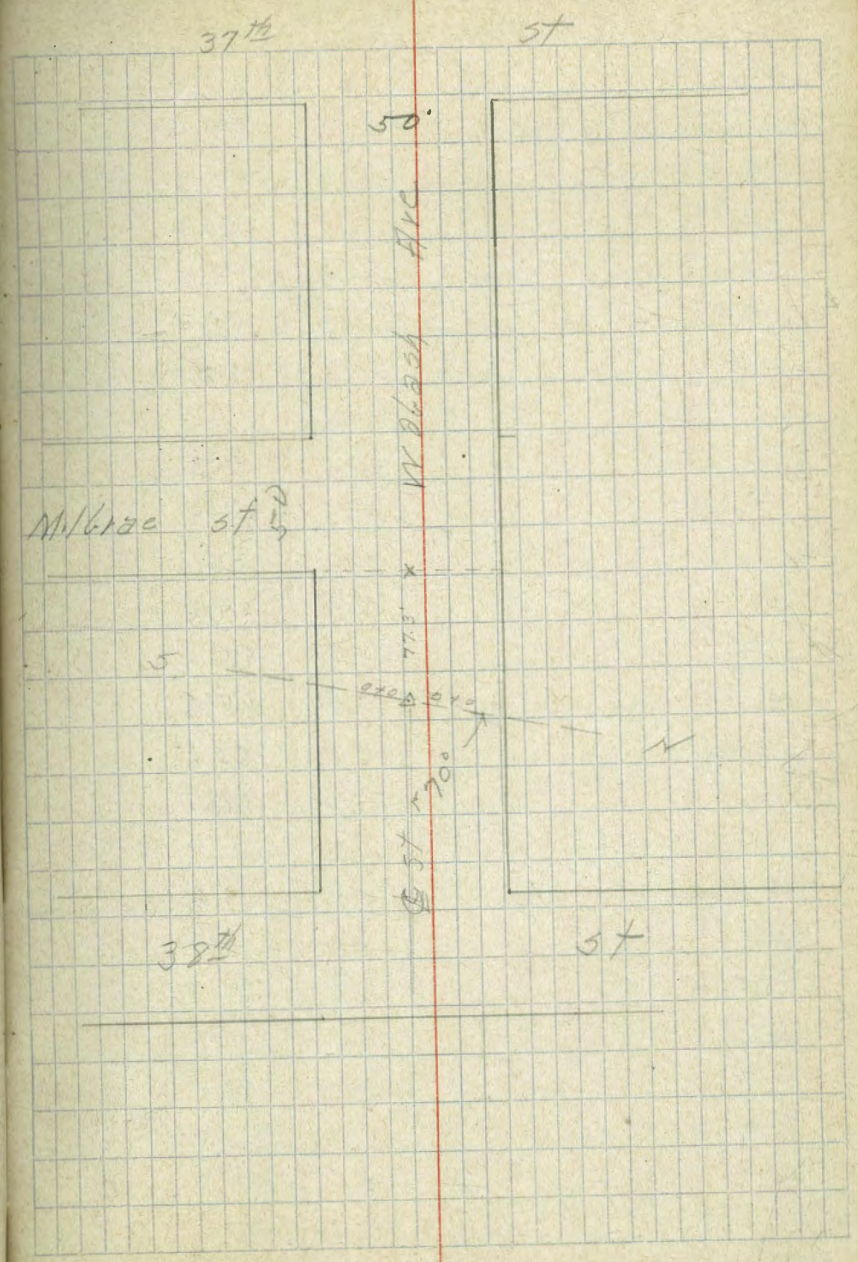
0+02 E.L. 37th St

N		10.7	82.6
cnlr		11.3	82.0
+02		12.2	81.1
¼		12.2	81.1
M		12.2	81.1
¼		12.7	80.6
+05		13.3	80.0
cnlr		13.0	80.3
S		13.9	79.4

0+25 E

S		12	81.3
cnlr		11.6	81.7
¼		11.6	81.7
M		11	82.3
¼		11.2	82.1
+03		11.1	82.2
cnlr		10.3	83.0
N		10.0	83.3

28



93.32

0+50

N	8.0	85.3
Crk	9.1	84.2
¼	10.0	83.3
M	10.0	83.3
¼	10.3	83.0
Crk	10.3	83.0
S	11.1	82.2

0+75

S	10.0	83.3
Top of Crk	9.3	84.0
Crk	8.9	84.4
¼	8.8	84.5
M	8.2	85.1
¼	8.4	88.9
Crk	7.5	85.8
N	6.9	86.4

1+00

N	4.7	88.6
Crk	5.0	88.3
¼	6.2	87.1
M	6.2	87.1
¼	6.8	86.5
Crk	6.9	86.4
Top of Crk	7.6	85.7
S	8.3	85.0

93.32

1+25

S	6.7	86.6
Crk	5.4	87.9
¼	5.0	88.3
M	4.8	88.5
¼	4.3	89.0
Crk	3.5	89.8
N	2.8	90.5

1+50

N	1.5	91.8
Crk	2.6	90.7
¼	3.5	89.8
M	3.7	89.6
¼	4.0	88.3
Crk	4.2	89.1
S	4.5	88.8

1+75

S	4.3	89.0
Crk	4.1	89.2
¼	4.1	89.2
M	3.9	89.4
¼	3.7	89.6
Crk	2.7	90.6
Top of Crk	2.5	90.8
N	1.6	91.7

		93.32		
		2+10		
N			2.5	90.8
Crk			3.7	89.6
1/4			4.6	88.7
M			4.8	88.5
1/4			4.9	88.4
Crk			5.1	88.2
S			5.3	88.0
		2+25		
S			6.3	87.0
Crk			6.0	87.3
1/4			6.3	87.0
M			6.0	87.3
1/4			5.6	87.7
Crk			4.9	88.4
+06			4.8	88.5
N			3.8	89.5
		2+50		
N			5.4	87.9
Crk			6.2	87.1
1/4			6.6	86.7
M			6.8	86.5
1/4			7.2	86.1
Crk			7.2	86.1
S			7.2	86.1

2+24.5 = w.t. Mileage

S		8.4	84.9
Crk		8.1	85.2
1/4		8.3	85.0
N		7.7	85.6
1/4		7.2	86.1
Crk		6.7	86.6
N		6.6	86.7
	W. Crk		
N		6.9	86.4
Crk		7.4	85.9
1/4		7.6	85.7
M		8.0	85.3
1/4		8.9	84.4
Crk		9.5	83.8
S		8.9	84.4
	W 1/4		
S		9.6	83.7
Crk		9.3	84.0
1/4		8.9	84.4
M		8.4	84.9
1/4		7.9	85.4
Crk		7.2	86.1
N		7.2	86.1

93.32

E. Milbrae

N		8.1	85.2
curb		7.9	85.4
1/4		8.3	85.0
M		8.7	84.6
1/4		9.2	84.1
curb		9.6	83.7
S		9.8	83.5
	E 1/4		
S		10.2	83.1
curb		10.0	83.3
1/4		9.5	83.8
M		9.0	84.3
1/4		8.7	84.6
curb		8.0	85.3
N		8.4	84.9
	E Curb		
N		9.2	84.1
curb		10.2	83.1
1/4		9.3	84.0
M		9.4	83.9
1/4		9.8	83.5
curb		10.2	83.1
S		10.4	82.9

93.32

E. L. Millbrae

S			10.9	82.4
curb			10.5	82.8
1/4			10.4	82.9
M			10.0	83.3
1/4			10.0	83.3
curb			10.8	82.5
N			10.3	830
T.R.	11.56	92.93	11.95	81.37
		0+25	E of Millbrae	
N			12.2	80.7
curb			12.1	80.8
1/4			11.5	81.4
M			11.7	81.2
1/4			11.8	81.1
curb			11.6	81.3
S			11.6	81.3
		0+50		
S			13.3	79.6
top			12.5	80.4
curb			12.5	80.4
1/4			12.8	80.1
M			12.8	80.1
1/4			12.4	80.5
top			12.5	80.4
curb			14.1	78.8
N			14.1	78.8

		92.93		
		0+75 E of Milvale		
N			15.0	77.9
calc			14.2	78.7
+0.4			12.7	80.2
1/4			13.1	79.8
M			13.0	79.9
1/4			13.1	79.8
calc			12.6	80.3
+0.8			12.8	80.1
S			13.7	79.2
		1+00		
S			12.9	80.0
calc			12.6	80.3
1/4			12.6	80.3
M			12.5	80.4
1/4			12.5	80.4
calc			13.0	79.9
N			14.1	78.8
		1+25		
N			11.4	81.5
calc			11.9	81.0
1/4			11.7	81.2
M			11.5	81.4
1/4			11.4	81.5
calc			11.4	81.5
S			11.4	81.5

	1+50		
S		9.8	83.1
calc		10.4	82.5
1/4		9.9	83.0
M		9.9	83.0
1/4		9.8	83.1
calc		10.5	82.4
N		10.8	82.1
	1+75		
N		9.1	83.8
calc		8.4	84.5
1/4		8.0	84.9
M		8.0	84.9
1/4		7.8	85.1
calc		8.1	84.8
+0.8		7.8	85.1
S		7.0	85.9
	2+00		
S		4.9	88.0
calc		5.4	87.5
1/4		5.8	87.1
M		6.0	86.9
1/4		6.0	86.9
calc		7.0	85.9
N		7.5	85.4

		92.93		
		2+25		
N			5.5	87.4
cab			4.9	88.0
1/4			4.0	88.9
M			3.2	89.7
1/4			3.3	89.6
cab			3.1	89.8
S			2.5	90.4
T.P.	9.97	101.34 ✓	1.56	91.37 ✓
		2+50		
S			8.4	92.9
cab			8.8	92.5
1/4			8.9	92.4
M			9.0	92.3
1/4			9.4	91.9
cab			10.2	91.1
N			11.3	90.0
		2+74.8 = W.L. 38.7 St		
N			3.0	93.3
cab			6.4	94.9
1/4			6.5	94.8
M			6.0	95.3
1/4			6.0	95.3
cab			5.5	95.8
S			5.3	96.0

Levels for proposed Storm drain Wabash See page 28 for sketch

	4.95	84.95		80.00	9/30/34 L. Shaw Bunker
		North			
0+0 = ℄			4.95	80.0	✓
0+12			4.8	80.2	✓
0+17			6.5	78.5	✓
0+30			6.5	78.5	✓
0+45			6.1	78.9	✓
		South			
0+0 = ℄			4.95	80.0	✓
0+24			4.8	80.2	✓
0+30			7.2	77.8	✓
0+45			7.9	77.1	✓

Plan No. 1

Cross-Section of 1st St. Maple to Olive (80' wide)

16/7 (Dorn Hennie
11 (Hennie

B.M. Brass Pin NW. 1st Maple

	+	H.I.	−	Elev.
	4.25	228.84		224.59
	No line Maple			
			4.8	224.0 ✓
W. Ct			gutr 5.5	223.3 ✓
½			5.0	223.8 ✓
C			4.3	224.5 ✓
½			3.9	224.9 ✓
			gutr 3.7	225.1 ✓
E Ct			2.8	226.0 ✓
	25' No			
			3.15	225.69 ✓
E Ct			gutr 3.8	225.0 ✓
½			3.9	224.9 ✓
C			4.2	224.6 ✓
½			5.2	223.6 ✓
			gutr 4.9	224.9 ✓
W Ct			5.2	223.6 ✓
	50' No			
W. Ct			5.4	223.4 ✓
			gutr 6.1	222.7 ✓
½			5.5	223.3 ✓
C			4.6	224.2 ✓
½			4.2	224.6 ✓
			gutr 4.0	224.8 ✓
E Ct			3.4	225.4 ✓
	75' N.			
E. Ct			3.7	225.1 ✓
			gutr 4.5	224.3 ✓
½			4.9	223.9 ✓
C			5.2	223.6 ✓
½			5.9	222.9 ✓
			gutr 6.3	222.5 ✓
W Ct			5.7	223.1 ✓

	100' No. Maple		
		6.0	222.8 ✓
W. Ct		gutr 6.6	222.2 ✓
½		6.3	222.5 ✓
C		6.0	222.8 ✓
½		5.4	223.4 ✓
		gutr 5.0	223.8 ✓
E Ct.		3.96	224.89 ✓
	125' N.		
		4.2	224.60 ✓
E Ct		gutr 6.1	223.7 ✓
½		5.9	222.9 ✓
C		6.8	222.0 ✓
½		6.9	221.9 ✓
		gutr 6.9	221.9 ✓
W Ct		6.23	222.61 ✓
	(So) 145' No - End Ct W side		
W. Line		6.0	222.8 ✓
Ct		6.3	222.5 ✓
		gutr 10.7	218.1 ✓
	(W o) 145' W.		
W. L		11.9	216.9 ✓
Ct.		10.7	218.1 ✓
	150' W.		
W.		12.2	216.6 ✓
Ct.		11.1	217.7 ✓
½		9.7	219.1 ✓
C		7.3	221.5 ✓
½		4.9	223.9 ✓
		gutr 5.2	223.6 ✓
E Ct		4.55	224.2 ✓

1st St 80' Wide

228.84

158 No Maple

W.L.		17.3	216.5
ct		17.0	217.8
¼		17.5	217.3
C		17.5	217.3
+10		5.4	223.4
½		5.0	223.8
gutter - In driveway - No ct.		5.2	223.6
147 No - End ct on E. Side			
ct		4.56	224.28
E. Line		4.3	224.5
168' No			
W.L.		17.7	211.1
ct		17.0	211.8
¼		16.8	212.0
+10		16.6	212.2
C		17.0	214.8
175' No			
E		4.7	224.1
ct		4.9	223.9
+5		4.9	223.9
¼		9.6	219.2
C		17.4	211.4
¼		17.5	211.3
ct		19.7	209.1
W		19.8	209.0

Note- Where no slopes are taken fig level from property line elev.

41

T.P.	5.75	229.46	5.13	223.71	
200' No					
E			6.0		223.5
+9			6.1		223.4
ct			9.3		220.2
¼			12.5		211.0
C			24.5		205.0
¼			25.9		203.6
ct			27.3		202.2
W			27.1		201.4
			25.7		203.8
50 W			25.7 South		203.8
			32.5 North		197.0
225' No					
E			5.2		224.3
+6			5.5		224.0
ct			11.2		218.3
¼			20.5		209.0
C			24.8		204.7
¼			28.8		200.7
ct			31.1		198.4
W			34.4		195.1
22' W			37.4		192.1
50 W			37.5		192.0

1st St 80' Wide

229.41

		2+0 1/2 No.	Maple	
E			3.7	225.8
+2			3.8	225.7
Ct.			11.4	218.1
H			17.4	212.1
C			21.8	207.7
H			27.1	202.4
Ct.			30.0	199.5
W			30.9	198.6
25 N			34.9	194.6
50 W			41.7	187.8
		2+5 No.		
E			1.9	227.6
+1			1.9	227.6
Ct			10.0	219.5
H			15.2	214.3
C			18.4	211.1
H			19.5	211.0
Ct.			19.5	210.0
W			22.0	207.5
25 W			21.6	202.9
T.P.	10.00	233.71	5.75	223.71

233.71 39

300 No. 50 line Nutmeg

E	4.2	229.4
Ct.	5.1	228.6
H	13.3	220.4
C	12.3	221.4
H	13.8	219.9
Ct.	15.6	218.1
W	16.7	217.0
25 W	24.9	208.8

7 No. 50 line

E	4.6	229.1
Ct.	4.5	229.2
H	5.3	228.4
C	7.5	226.2
H	9.1	224.6
Ct.	10.6	223.1
W	15.0	218.7
25 W	23.5	210.2

50 Ct. Nutmeg

E	4.7	229.0
Ct.	4.2	229.6
H	5.5	228.2
C	6.9	226.8
H	8.1	225.6
Ct.	10.1	223.6
W	14.0	219.7
25 W	21.2	212.5

1st St 80' wide

233.71

So ½ Nutmeg

E		3.3	230.4
ch		3.0	230.7
½		4.0	229.7
c		5.0	228.7
¼		6.2	227.5
ch		8.3	225.4
W		12.1	221.6
10 W		14.2	219.5

CH Nutmeg

W		9.0	224.7
ch		7.1	226.6
½		4.1	227.6
c		4.6	229.1
¼		3.9	229.8
ch		3.6	230.1
E		3.1	230.6

No ¼ Nutmeg

E		3.4	230.3
ch		3.5	230.2
½		3.7	230.0
c		4.4	229.3
¼		5.3	228.4
ch		6.3	227.4
W		7.5	226.2

2337 ft.

No CH. Nutmeg

W		6.7	227.0
ch		5.6	228.1
¼		4.7	229.0
c		4.1	229.6
¼		3.5	230.2
ch		3.4	230.3
E		3.6	230.1

No. line Nutmeg

E		2' No 3' So.	231.6 230.6
ch.		3.1	230.6
½		3.1	230.6
c		3.6	230.1
¼		4.1	229.6
ch		4.8	228.9
W		5.7	228.0
T.P	8.67	238.77	3.61	230.10

26' No Nutmeg

E		5.8	233.0
ch		6.6	232.2
¼		7.0	231.8
c		7.5	231.3
¼		27	231.1
ch		8.7	230.1
W		9.6	229.2

2388

		2388.77		
		50' N.	Autumn 9	
W			8.6	230.2
Ch			7.2	231.6
H			6.8	232.0
C			6.6	232.2
Ic			6.7	232.1
Ch			5.5	233.3
E			4.8	234.0
		75' N.		
E			3.9	234.9
Ch			5.0	233.8
H			6.2	232.6
C			6.5	232.3
H			6.7	232.1
Ch			7.0	231.8
W			7.6	231.2
		100' N.		
W			7.1	231.7
Ch			6.5	232.3
Ic			6.4	232.4
C			5.9	232.9
Ic			5.4	233.4
Ch			4.6	234.2
E			3.0	235.8

		125' N.	
E	4.7		236.1
Ch	4.1		234.7
H	5.2		233.6
C	5.8		233.0
H	6.4		232.7
Ch	6.3		232.5
W	7.1		231.7
	150 N.		
W	7.5		231.3
Ch	6.7		232.1
Ic	6.6		232.2
C	6.0		232.8
H	5.0		233.8
Ch	4.3		234.5
E	2.8		236.0
	175 N.		
W	8.5		230.3
Ch	7.9		230.9
	175 N.		
E	2.4		235.4
Ch	4.5		234.3
H	5.5		233.3
C	6.1		232.7
H	7.0		231.8
Ch	8.1		230.7
W	9.2		229.6

		238.77		
		200 N. Nutmeg		
10 W			13.5	225.9
W			12.5	225.3
Ch			12.0	226.8
H			9.1	229.7
C			7.6	231.2
H			6.2	232.6
Ch			5.0	233.8
E			4.0	234.8
		203 N.		
10 W			16.9	221.9
W			16.0	222.8
Ch			12.9	225.9
		225 N.		
E			5.6	233.2
Ch			6.9	231.9
T			7.6	231.2
H			9.6	229.2
C			14.3	224.5
		241		
E			7.9	230.9
Ch			13.0	225.8
T.P	0.02	226.09	12.70	226.07
		225 N.		
W H			4.8	221.3
Ch			6.9	219.2
W			8.6	217.5
10 W			{8.5 So {10.2 No	217.6 215.9

226.14 9

40

250 N.

E	9.1	226.0
Ch	4.2	221.9
H	7.4	218.7
C	9.9	216.2
H	12.9	213.2
Ch	15.0	211.1
W	16.9	209.2
25 W	22.2	203.9
T.P 6.46	213.67	12.98	213.11
	275 N.	
25 E	1.6	212.0
E	3.1	210.5
Ch	5.0	208.6
H	6.3	207.3
C	9.2	204.4
H	10.8	202.8
Ch	12.9	200.7
W	15.6	198.0
25 W	20.4	193.2
TP 1.06	201.74	12.89	200.68
	301 N. S. Line Olive	
25 E	5.1	196.6
E	6.0	195.7
Ch	7.5	194.2
H	9.1	192.6
C	11.2	190.5
H	12.3	189.4
Ch	14.3	187.4
W	17.3	184.4
25 W	24.2	177.4

Cross Section of 1st St. From 125' No of Maple to So. line Olive St. Plan No. 2

Note South of Nutmeg St. 1st St is 66' wide - 15' taken off of west side. 14' Sidewalk on E. Side & 5' Sidewalk on west - quarters 11.5'
North of Nutmeg St is 80' wide - 15' taken off each side - Sidewalks 5' quarters 10'

	2.95	226.94	2.2399 NW 15 Maple
		125 No Maple	
E		2.0	224.9
ct		2.33	224.6
gutr		3.1	223.8
4		3.9	223.0
c		4.8	222.1
4		4.9	222.0
cl		4.8	222.1
W		5.1	221.8
	150' No		
10 W		10.1	216.8
W		9.2	217.7
ct		9.2	217.7
4		7.2	219.7
c		4.8	222.1
4		3.2	223.7
gutr		3.3	223.6
ct.		2.65	224.3
E		2.1	224.8

226.9 std. See Book 1008 Grades. - Bk 91 41

	158' No	
10 W	9.7	217.2
W	9.0	217.9
ct.	8.8	218.1
4	9.9	217.0
	168' No	
15 W	15.9	211.0
W	15.1	211.8
ct	14.9	212.0
4	14.8	212.1
+6	14.8	212.1
c	11.2	215.7
	158' No	
ctr	8.5	218.4
+7	3.5	223.4
4	2.8	224.1
gutr	3.0	223.6
	167' No. End Ct. E. Side	
E	2.1	224.5
cl.	2.66	224.2
	175 No	
E	2.8	224.1
cl.	3.0	223.9
+5	3.0	223.9
4	6.8	220.1
c	1.46	212.3

2294

175 N. Maple

W 4			16.4	210.5
Ck			17.2	209.7
W			17.6	209.3
15 W			17.8	209.1
T. P	6.21	229.92	3.20	223.71
		200 N.		
E			6.5	223.4
+ 9			6.6	223.3
Ck			9.7	220.2
4			12.0	211.9
C			24.8	205.1
4			26.0	203.9
Ck			27.7	202.2
W			27.9	202.0
15 W			28.8	201.1
		225 N.		
E			5.6	224.3
+ 6			5.9	224.0
Ck			11.6	218.3
W			20.0	209.9
C			24.5	205.4
4			28.0	201.9
Ck			30.1	199.8
W			31.0	198.9
25 W			36.0	193.9

2299 49

175 N. Nutmeg

E			4.1	225.8
+ 2			4.3	225.6
Ck.			11.8	218.1
4			17.1	212.8
C			21.0	208.9
4			25.8	204.1
Ck			25.9	200.0
W			30.4	199.5
25 W			32.7	197.2
		275 N.		
E			2.3	227.6
+ 1			2.3	227.6
Ck			10.4	219.5
4			10.5	214.4
C			14.9	211.0
4			20.0	209.9
Ck			19.8	210.1
W			19.9	210.0
25 W			24.8	205.1
T. P	5.30	234.54	6.68	229.24
		300 N. S. Line Nutmeg		
E			5.2	229.3
Ck			5.9	228.6
4			14.0	220.5
C			13.3	221.2

~~234.54~~

5. Line Nutmeg.

WW-H	15.9	218.6
Ch.	17.2	217.3
W	17.0	217.5
25 W	21.9	212.6

7' N. 5. Line

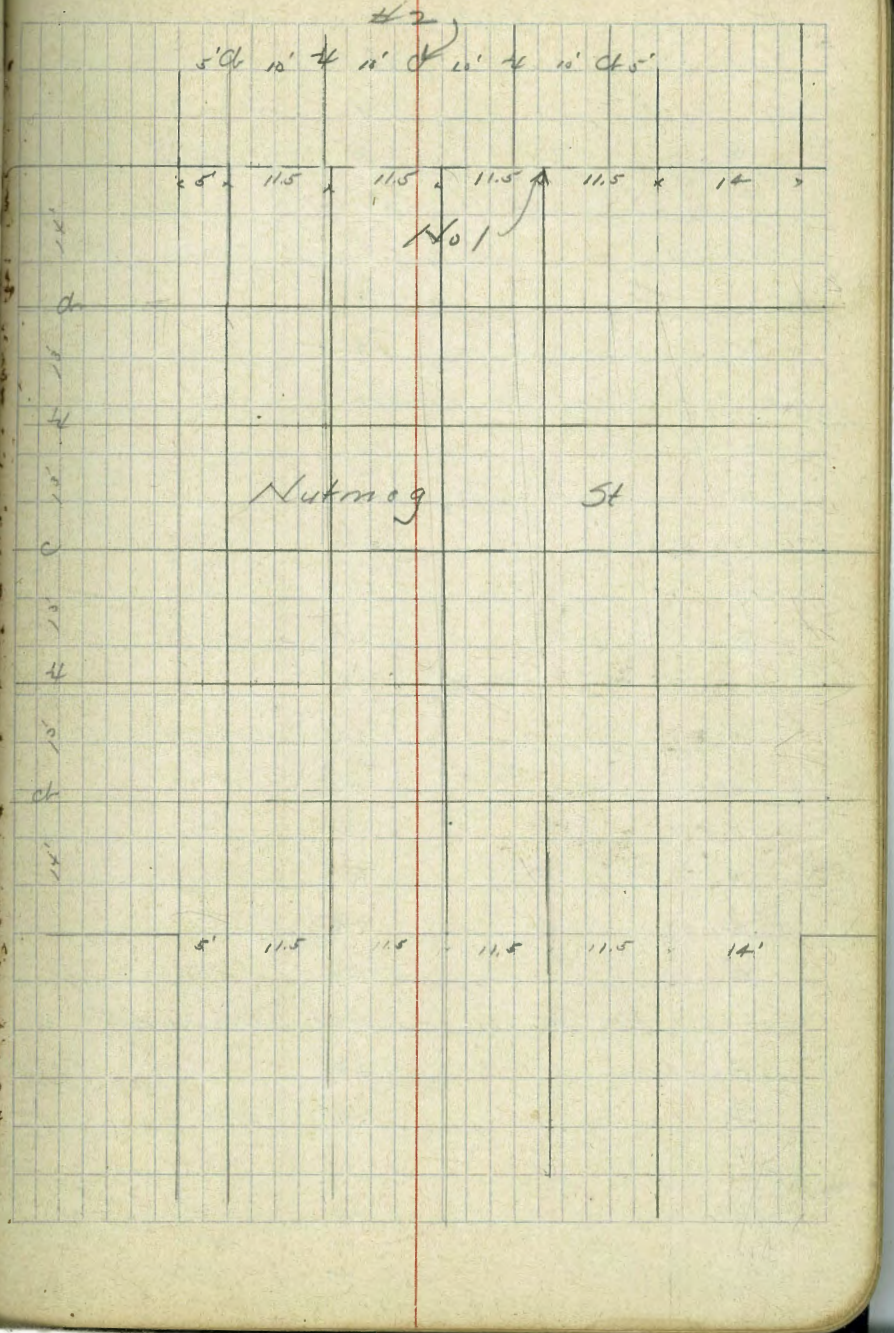
E	5.4	229.1
Ch.	6.3	229.2
H	6.8	227.7
C	7.6	226.9
H	10.6	223.9
Ch	11.2	223.3
W	11.5	223.0

5 Ch. Nutmeg.

W.	10.8	223.7
Ch.	9.9	224.6
H	8.3	226.2
C	7.6	226.9
H	6.5	228.0
Ch	5.0	229.5
E	5.5	229.0

50 H Nutmeg

E	41	230.4
Ch	3.8	230.7
H	4.6	229.9
C	5.4	229.1
H	6.5	228.0
Ch	8.0	226.5
W	8.6	225.9



CA Nutmeg

W	7.8	226.7
Cl	7.4	227.1
H	5.9	228.6
C	5.6	228.9
H	4.7	229.8
Cl	4.3	230.2
E	3.9	230.6

No 4 Nutmeg

E	4.3	230.2
Cl.	4.3	230.2
H	4.5	230.0
C	5.0	229.5
H	5.7	228.8
Cl.	4.7	227.8
W	7.1	227.4

No Cl.

W	6.3	228.2
Cl	6.1	228.4
H	5.4	229.1
C	5.0	229.5
H	4.4	230.1
Cl	4.2	230.3
E	4.5	230.0

#1 No line Nutmeg - (Int) 65' wide

E	3.8	230.7
Cl.	3.9	230.6
H	3.9	230.6
C	4.2	230.2
H	4.8	229.7
Cl	5.2	229.3
W	5.7	228.8

#1 No line Nutmeg 50' wide

E	3.8	230.7
Cl	3.8	230.7
H	3.9	230.6
C	4.3	230.2
H	4.8	229.7
Cl	5.2	229.3
W	5.6	228.9

50' No.

W	4.4	230.1
Cl	4.1	230.4
H	3.7	231.3
C	3.7	231.3
H	3.8	231.7
Cl	3.0	231.5
E	2.6	231.9

50' No

E	1.5	233.0
Cl	2.3	232.2
H	2.5	232.0
C	2.3	232.2
H	2.4	232.1
Cl	3.0	231.5
W	3.2	231.3

234.52

75 N.

W			2.7	231.8
Ch			2.6	231.9
Ls			2.1	232.4
C			2.2	232.3
Ls			1.9	232.6
Ch			1.5	233.0
E			0.9	233.6
		100' N.		
E			0.5	234.0
Ch			1.0	233.5
Ls			1.2	233.3
C			1.6	232.9
W			2.0	232.5
Ch			2.2	232.3
W			2.2	232.3
		125 N.		
W			2.1	232.4
Ch			2.0	232.5
Ls			1.7	232.8
C			1.5	233.0
Ls			1.1	233.4
Ch			0.6	233.9
E			0.1	234.4
T.P.	3.13	237.15	0.52	234.02

237.2 Jf.9.

150 N.

E	2.9	234.3
Ch	2.0	234.2
Ls	3.4	233.8
C	4.2	232.8
Ls	4.6	232.4
Ch	5.0	232.2
W	5.1	232.1
	175 N.	
W	6.5	230.7
Ch	6.0	231.2
Ls	6.1	232.1
C	4.5	232.7
Ls	4.0	233.2
Ch	3.2	234.0
E	2.5	232.7
	200 N.	
E	3.6	233.6
Ch	4.0	233.2
Ls	4.9	232.3
C	6.0	231.2
W	7.0	230.2
Ch	9.3	227.9
W	10.1	227.1

		237.5		
		225 N.		
E			6.2	232.0
cl			6.7	231.5
sy			9.6	228.6
c			12.6	225.6
T.P.	0.03	237.19	12.99	224.16
sy			22	215.0
cl			3.9	220.3
W			4.7	219.5
		250 N.		
W			12.9	211.3
cl			12.0	212.2
sy			10.8	213.9
c			8.2	216.0
sy			4.3	219.9
cl			4.0	220.2
E			2.4	221.8
T.P	0.07	211.21	13.05	211.14
		275 N.		
E			2.9	208.3
cl			3.3	207.9
sy			4.1	207.1
c			6.8	204.4
sy			8.0	203.2
cl			8.9	202.3
W			10.1	201.1

211.2

301' N. 6 Line Olive

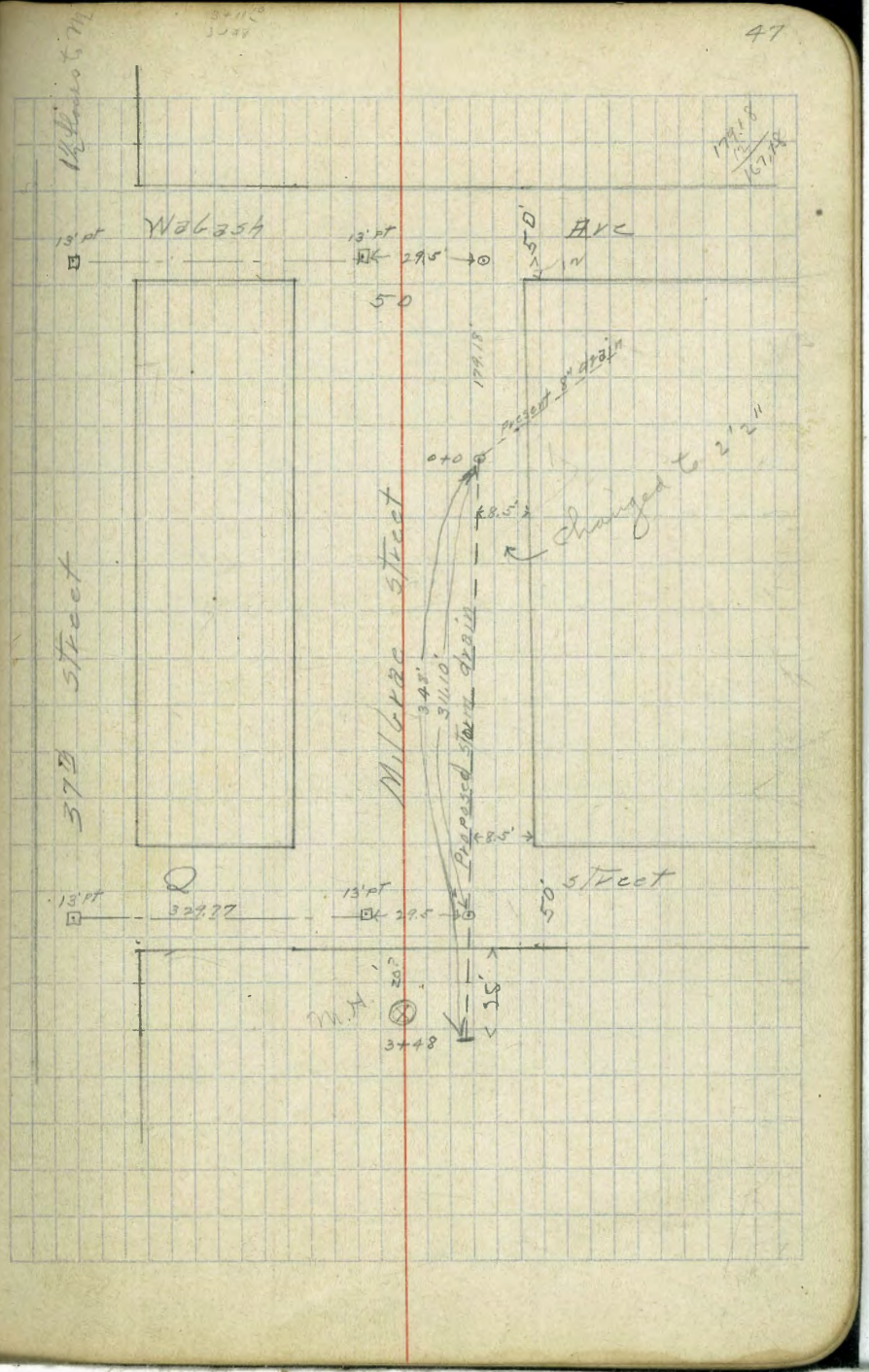
W	23.8	187.4
cl	23.0	188.2
sy	21.4	189.8
c	20.9	190.3
sy	19.0	192.2
cl	17.1	194.1
E	16.3	194.9

Levels for Proposed storm drain - Sketch opp page. 11/29/05 Dunkle Shaw Bunker.

B.M.	2.20	91.26		82.56
T.P.	0.36	79.07	13.05	78.71
0+0 = Bottom of pipe at present S drain Line 2.5 W of E.L. Milsbae			10.63	68.44
0+0 ground			8.4	70.7
+25 South			9.8	69.3
+50			10.9	68.2
+75			11.6	67.5
1			12.4	66.7
T.P.	1.45	67.94	12.58	66.49
+25			2.5	65.4
+50			3.5	64.4
+75			4.2	63.7
2			4.5	63.4
+25			4.9	63.0
+50			5.8	62.1
+75			6.7	61.2
3			6.9	61.0
+11.0 = 13 Line Q St			7.5	60.4
+25			7.9	60.0
+44			9.1	58.8
+48			10.3	57.6
+52	No sl.	576		
+62		586		

up about 10 ft

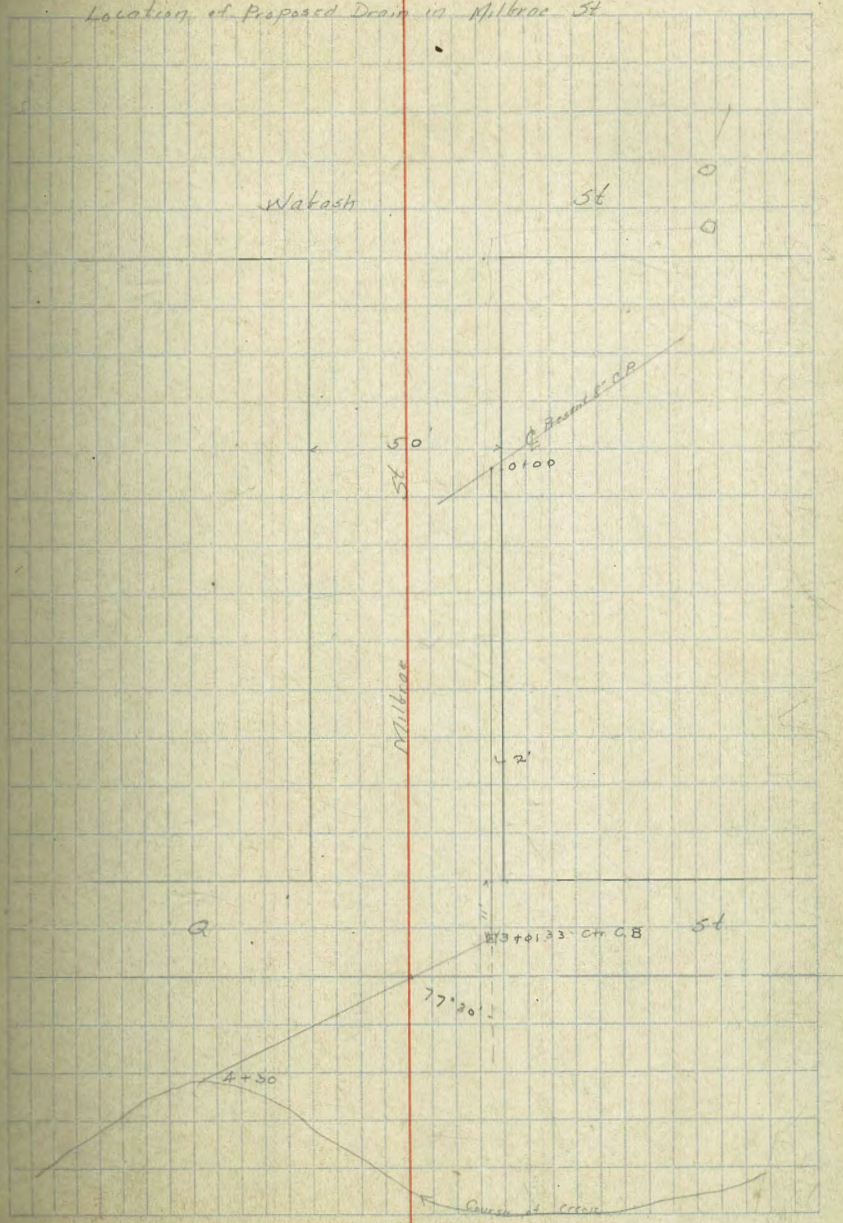
See next page



Levels over Proposed Milbrae St Drain

	4.48	100.26		95.78 RR Spike Elev. Pole NE corner
T.P	0.66	88.30	12.52	87.74
T.P	0.64	75.96	12.98	75.32
0+00			{4.48 Top pipe; 11.6 ground}	69.48 7.14
+50			7.2	68.7
1			8.9	67.1
+50			11.1	64.9
2			12.5	63.5
T.P	2.62	65.91	12.67	63.29
+50			3.1	62.8
3			5.0	60.9
+01.33	C.B.		4.7	61.2
+50			8.2	57.7
4			11.1	54.8
+30			12.0	53.9
B.M. Spike tel pole S.E. Milbrae & Q			5.64	60.27

Location of Proposed Drain in Milbrae St



4/6/16 Gregory Maple Miller

CROSS-SECTION OF LARK ST. (80' wide 13 & 14 curbs) from S.L. of Marine View to E.L. of Middletown

(Note: 17.5 17.5 Varies for 80' St due to use of Varying curbs)

on B.M.	0.48	266.04 ✓		265.56	N/W Lark & Puterbaugh
on hub			12.77	253.27 ✓	hub S.L. Marine View & E.L. Lark
		S.L. Marine View			
E.			12.7	253.3 ✓	
+10			13.4	252.6	
⌀			13.4	252.6	
+3.5			(13.3)	252.7	
+11			(13.2)	252.7	
⌀			12.2	253.8	
T.P.	0.52	253.60 ✓	12.96	253.08 ✓	
+5.5			(4.8)	248.8	
C			10.5	243.1 ✓	
+10			17.3	236.3	
⌀			18.2	235.4	
⌀			25.6	228.0	
W			30.2	223.4 ✓	
+10			32.0	220.6	
+20			37.7	215.0	
+45			51.2	202.4	
+80			63.4	190.2	
+95			66.0	187.6	
		10 · 50.			
-100			69.3	184.3	
-65			61.3	192.3	
-45			53.9	199.7	
-25			42.6	211.0	

LARK ST. 30

Note Clock extensions before using Eqpt.

-10	36.5	217.1 ✓
W.	35.2	218.4
⌀	27.7	225.9
⌀	19.2	234.4
+3	(17.5)	236.1
C.	12.7	240.9 ✓ 235.9
+7.5	(7.2)	246.4
⌀	1.8	252.8
+2	1.2	252.4
+9.5	(1.4)	252.2
⌀	1.5	252.1
+4	1.8	251.8
E.	0.7	252.9 ✓
	20 · 30	
E	1.4	252.2 ✓
+10	2.1	251.2
⌀	2.1	251.5
+3.5	2.1	251.5
+11	2.5	251.1
⌀	3.8	249.8
+5.5	(7.7)	245.9
C	13.3	240.3 ✓
+10	(20.0)	233.6
⌀	21.6	232.0
⌀	29.3	224.3

		353.60		
W			38.2	215.4 ✓
+20			45.9	207.7
+40			53.7	199.9
+55			59.7	193.9
+80			66.5	187.1
+110			72.3	181.3
		26' 30.		
-110			73.3	180.3
-80			66.7	186.9
-60			61.3	192.3
-40			55.3	198.3
-20			47.6	206.0
-10			44.0	209.6
W			37.7	215.9 ✓
cb			29.4	224.2
1/4			22.2	231.4
+3			(20.3)	233.3
C			13.4	240.2 ✓
+7.5			8.4	245.2
1/4			4.7	248.6
+2			3.3	250.3
+9.5			(2.6)	251.0
cb			2.5	251.1
+4			(2.0)	251.0
E			1.9	251.1 ✓

		35' 30.		
E			2.7	250.9 ✓
+10			(3.2)	250.4
cb			3.4	250.2
+35			(3.5)	250.1
+11			3.9	249.7
1/4			4.7	248.9
+5.5			(8.0)	245.6
C			11.6	242.0 ✓
+10			(17.3)	236.3
1/4			19.2	234.4
cb			25.8	227.8
T.P. 394	250.68 ✓		6.86	246.74 ✓
W			29.1	221.6 ✓
+20			43.4	207.2
+45			54.2	196.4
+65			60.6	190.0
+80			64.7	185.9
+100			69.0	181.6
		50' 30.		
-100			70.5	180.1
-75			64.8	185.8
-41			48.4	202.2
-16			38.1	212.5
W			28.2	222.5 ✓
cb			19.4	231.2

		350.68		
1/4			13.8	236.8
+3			(12.6)	238.0
C			8.9	241.8 ✓
+7.5			6.6	244.0
1/4			3.6	247.0
+2			2.5	248.1
+9.5			(1.7)	248.9
cb			1.7	248.9
+4			1.6	249.0
E			1.0	249.7 ✓
		60'50.		
E			2.0	248.7 ✓
+10			(2.5)	248.1
cb			2.6	248.0
+3.5			2.8	247.8
+11			(5.6)	245.0
1/4			5.9	244.7
5.5			(7.7)	242.9
C			9.3	241.4 ✓
+10			(12.2)	238.2
1/4			13.6	237.0
cb			15.7	231.9
W			25.8	224.9 ✓
+17			37.2	213.4
+30			44.0	206.6
+50			57.3	198.3

+63	56.6	194.0
+95	71.1	179.5
+105	73.0	177.6
	70'50.	
-105	73.5	177.1
-97	73.3	177.3
-65	58.0	192.6
-40	50.0	200.6
-23	42.0	208.6
W	26.0	224.7 ✓
cb	18.9	231.9
1/4	13.5	237.1
+3	(12.6)	238.0
C	9.8	240.9 ✓
+7.5	8.5	242.1
1/4	6.8	243.8
+2	(6.0)	244.6
+9.5	(4.9)	245.7
cb	4.7	245.9
+4	(4.0)	246.6
E	3.8	246.9 ✓
	80'50.	
E	5.0	245.7 ✓
+10	(6.2)	244.4
cb	6.4	244.2

		250.68		
+3.5			7.4	243.2
+11			7.9	242.7
1/4			8.2	242.4
+5.5			9.3	241.3
C			11.0	239.7 ✓
+10			12.8	237.8
1/4			13.6	237.0
dr.			17.1	233.5
W			23.6	227.0 ✓
+10			28.9	221.9
+20			37.2	213.4
+45			51.4	199.2
+45			58.7	191.9
+80			64.4	186.2
+98			73.5	177.1
+105			74.5	176.1
		100' So.		
-105			72.4	178.2
-80			63.8	186.8
-65			57.6	193.0
-30			37.0	213.6
W			21.0	229.7 ✓
+5			18.8	231.8
dr			16.4	234.2
1/4			13.9	236.7
+3			13.5	237.1

C			12.6	238.0 ✓
+7.5			11.4	239.2
1/4			10.9	239.7
+2			10.5	240.1
+9.5			9.2	241.4
dr			9.0	241.6
+4			8.2	242.4
E			7.2	243.5 ✓
		115' So.		
E			8.8	241.9 ✓
+10			9.7	240.9
dr.			10.1	240.5
+3.5			10.6	240.0
+11			11.9	238.7
1/4			12.4	238.2
+5.5			13.2	237.4
C			14.0	236.7 ✓
+10			15.5	235.1
1/4			16.1	234.5
dr			18.3	232.3
W			21.5	229.2 ✓
+20			30.0	220.6
+27			32.0	218.6

		250.68		
		125' So.		
-25			29.6	221.0
-15			28.1	225.5
W			23.1	227.6 ✓
cb			19.4	231.2
1/4			16.8	233.8
+3			(15.9)	234.7
C			15.0	235.7 ✓
+7.5			14.2	236.4
1/4			13.1	237.5
+12			(12.8)	237.8
+9.5			(11.5)	239.1
cb			11.1	239.5
+4			(10.5)	240.1
E			9.5	241.2 ✓
		150' So.		
E			11.0	239.7 ✓
+10			(12.9)	237.7
T.P.	0.71	234.06 ✓	12.33	238.35 ✓
cb			1.8	237.26
+3.5			(2.7)	236.36
+11			(3.8)	235.26
1/4			4.1	234.96
+5.5			4.9	234.16
C			5.7	233.4 ✓
+10			7.2	231.86

1/4	7.9	231.1	
cb	11.4	227.6	
W	14.9	224.1 ✓	
+2	15.0	224.0	= top of wall
+2	17.2	221.8	= bot. of wall + top of concrete walk.
+12	17.0	222.0	
	156' So.		
-10	17.0	222.0	= at house.
W	(17.1	222.0 ✓	= bot. of wall
	15.0	224.1 ✓	= top of wall
cb	11.9	227.1	
1/4	9.2	229.8	
+3	8.4	230.6	
C	5.9	233.2 ✓	
+7.5	(5.4)	233.6	
1/4	4.6	234.4	
+2	(2.8)	234.8	
+9.5	(3.1)	235.9	
cb	2.3	236.7	
+4	(1.8)	231.2	
E	0.0	239.1 ✓	
	175' So.		
E	1.9	237.2 ✓	
+10	(3.4)	235.6	
cb	3.8	235.2	

		239.06			
+3.5			4.3	234.7	
+11.			5.1	233.9	
1/4			5.7	233.3	
+5.5			(7.2)	231.8	
C			8.5	230.6 ✓	
+10			(10.6)	228.4	
1/4			11.1	227.9	
ab			15.2	223.8	
+7.5			17.0	222.0	
W			17.6	221.5 ✓	
+16.0			22.2	216.8	= house
		200' SO.			
-35			30.0	209.0	
W			20.9	218.2 ✓	
ab			17.0	222.0	
1/4			13.5	225.5	
+3			(12.7)	226.3	
C			10.0	229.1	
+7.5			(8.8)	230.2	
1/4			7.2	231.8	
+2			(6.8)	232.1	
+9.5			(5.4)	233.6	
ab			4.8	234.2	
+4			(4.0)	235.0	
E			3.3	235.8 ✓	

		225 SO.			
E			4.0	235.1 ✓	
+10			(5.5)	233.5	
ab			6.4	232.6	
+3.5			(7.2)	231.8	
+11			(9.3)	229.7	
1/4			9.8	229.2	
+5.5			10.8	228.2	
C			12.6	226.5 ✓	
+10			(16.2)	222.8	
1/4			17.0	222.0	
ab			21.2	217.8	
W			24.4	214.7 ✓	
+25			30.7	208.3	
+40			33.7	205.3	
		2575 on E 2588 - W	=	N.L. Willow St 80' wide	
-35			39.0	200.0	
-27			34.4	204.6	
W			27.3	211.7 ✓	
ab			24.7	214.3	
1/4			20.8	218.2	
+3			(19.8)	219.2	
C			16.5	222.6 ✓	
+7.5			(14.1)	224.9	
1/4			12.9	226.2	
+2			(12.1)	226.6	

		239.06		
+9.5			11.0	228.0
d			10.0	229.0
+4			8.9	230.1
E			6.1	233.0 ✓
		No. Curb.		
E			7.7	231.4 ✓
+10			10.4	228.6
d			11.5	227.5
+3.5			12.5	226.5
+11			14.8	224.2
1/4			15.2	223.8
+5.5			17.0	222.0
C			18.9	220.2 ✓
+10			21.8	217.2
1/4			22.6	216.4
d			26.2	212.8
W			29.1	209.7 ✓
+15			33.0	206.0
+30			40.1	198.9
		No. Quarter		
-80			61.0	178.0
-60			60.7	178.3
-15			33.6	205.4
W			30.1	209.0 ✓
d			27.4	211.6
1/4			24.1	214.9

LARK ST.

+3			23.2	215.8
C			20.7	218.4 ✓
+7.5			18.7	220.3
1/4			17.2	221.8
+2			16.6	222.4
+9.5			13.8	225.2
d			12.9	226.1
+4			11.5	227.5
E			8.8	230.3 ✓
T.P.	0.0	229.09 ✓	9.97	229.09 ✓
		Center		
E			0.1	229.0 ✓
+10			2.5	226.6
d			3.9	225.2
+3.5			5.1	224.0
+11			7.7	221.4
1/4			8.4	220.7
+5.5			10.1	219.0
C			11.8	217.3 ✓
+10			14.0	215.1
1/4			14.8	214.3
d			18.3	210.8
W			20.9	208.2 ✓
+22			26.6	202.5
+50			42.6	186.9

229.09

+70	56.5	172.6	
+80	58.8	170.8	
So. Quarter			
-32	33.3	195.8	
-22	27.8	201.8	
W	22.3	206.8	✓
cb	19.2	209.9	
1/4	16.1	213.0	
+3	(15.4)	213.7	
C	12.8	216.3	✓
+7.5	(10.5)	218.6	
1/4	9.0	220.1	
+2	(8.1)	221.0	
+9.5	(6.1)	223.0	
cb	5.0	224.0	
+4	(3.8)	225.3	
E	1.0	228.1	✓
So. Curb			
E	2.3	226.8	✓
+10	(4.7)	224.4	
cb	5.6	223.5	
+3.5	(6.5)	222.6	
+11	(7.9)	221.2	
1/4	8.6	220.5	
+5.5	(10.1)	219.0	

C	13.3	215.8	✓
+10	(16.1)	213.0	
1/4	16.9	212.2	
cb	19.7	209.4	
W	23.3	205.8	✓
+25	30.0	199.1	
So. Line of Willow			
-25	30.7	198.4	
-15	28.4	200.7	
W	22.5	206.3	✓
cb	20.1	209.0	
1/4	17.3	211.8	
+3	(16.5)	212.6	
C	13.4	215.7	✓
+7.5	(10.5)	218.6	
1/4	8.7	220.4	
+2	(8.2)	220.9	
+9.5	(6.6)	222.5	
cb	6.1	223.0	
1/4	(5.3)	223.8	
E	3.4	225.7	✓
35' So.			
E	3.8	225.3	✓
+10	(6.1)	223.0	
cb	6.8	220.3	

229.09

+3.5			(7.6)	221.5
+11.			(9.2)	219.9
1/4			9.6	219.5
5.5			(11.0)	218.1
C			12.9	216.2 ✓
+10			(16.1)	213.0
1/4			17.0	212.1
cb			20.7	208.4
W			24.6	204.5 ✓
+15			29.1	200.0
+30			33.7	195.4
		50' So.		
-30			34.6	194.5
W			25.2	203.9 ✓
cb			21.1	208.0
1/4			16.4	212.7
+3			(15.4)	213.7
C			13.3	215.8 ✓
+7.5			(11.5)	217.6
1/4			10.4	218.7
+2			(10.2)	218.9
+9.5			(8.4)	220.7
cb			7.8	221.3
+4			(7.3)	221.8
E			5.1	224.0 ✓

75' So.

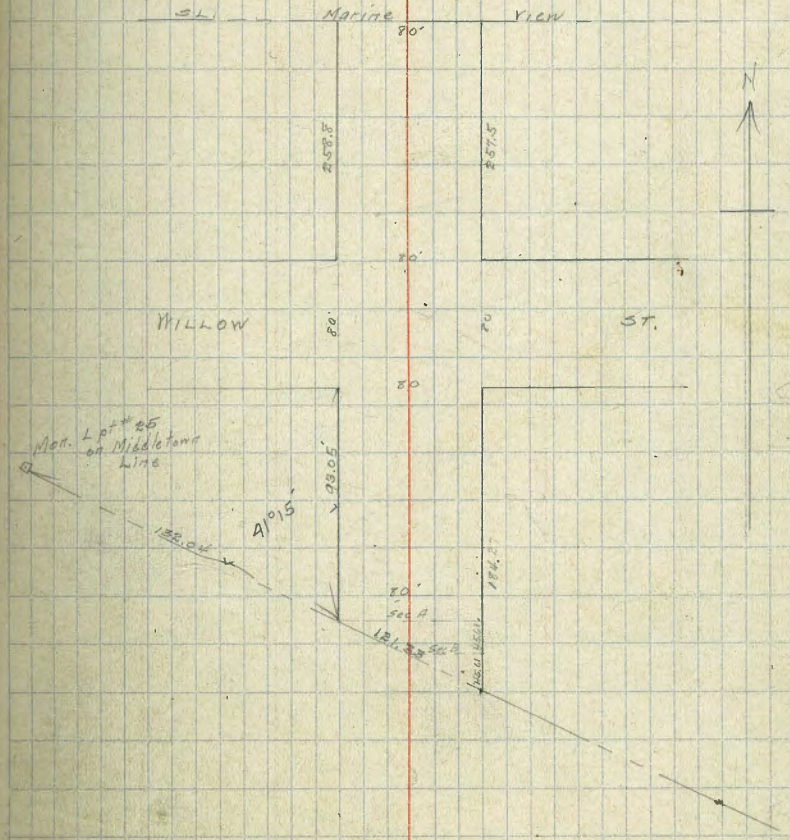
E		5.5	223.6 ✓
+10		(7.3)	221.8
1/4		7.8	221.3
+3.5		(8.6)	220.5
+11		(10.3)	218.8
1/4		10.6	218.5
+5.5		(11.6)	217.5
C		12.9	216.2 ✓
+10		(14.7)	214.4
1/4		15.3	213.8
cb		20.0	209.1
W		24.6	204.5 ✓
+20		30.5	198.6
+40		37.2	191.9
	93.05' So. = 500.7.		
-30		34.4	194.7
-15		28.0	201.1
W		23.7	205.4 ✓
cb		19.0	210.1
1/4		15.1	214.0
+3		(14.4)	214.7
C		12.8	216.3 ✓
+7.5		(11.6)	217.5
1/4		10.5	218.6
+2		(10.1)	219.0

		229.09		
+9.5			(9.0)	220.1
cb			7.8	221.3
+4			(6.7)	222.4
E			4.3	224.8 ✓
		120' So. of Willow		
E			4.6	224.5 ✓
+10			(6.3)	222.5
cb			7.0	222.1
+3.5			(7.5)	221.6
+11			(8.6)	220.5
1/4			9.0	221.1
+5.5			(10.1)	219.0
C			11.7	217.4 ✓
+10			(13.3)	215.8
1/4			13.6	215.5
+13.4=Middletown Line			14.9	214.2
		Sec. B		
C			10.4	218.7 ✓
+7.5			(9.1)	220.0
1/4			7.3	220.8
+2			(8.0)	221.1
+9.5			(6.7)	222.4
cb			6.2	222.9
+4			(5.6)	223.5
E			3.1	226.0 ✓

LARK ST. 59

Int. E.L. Lark with Middletown Line

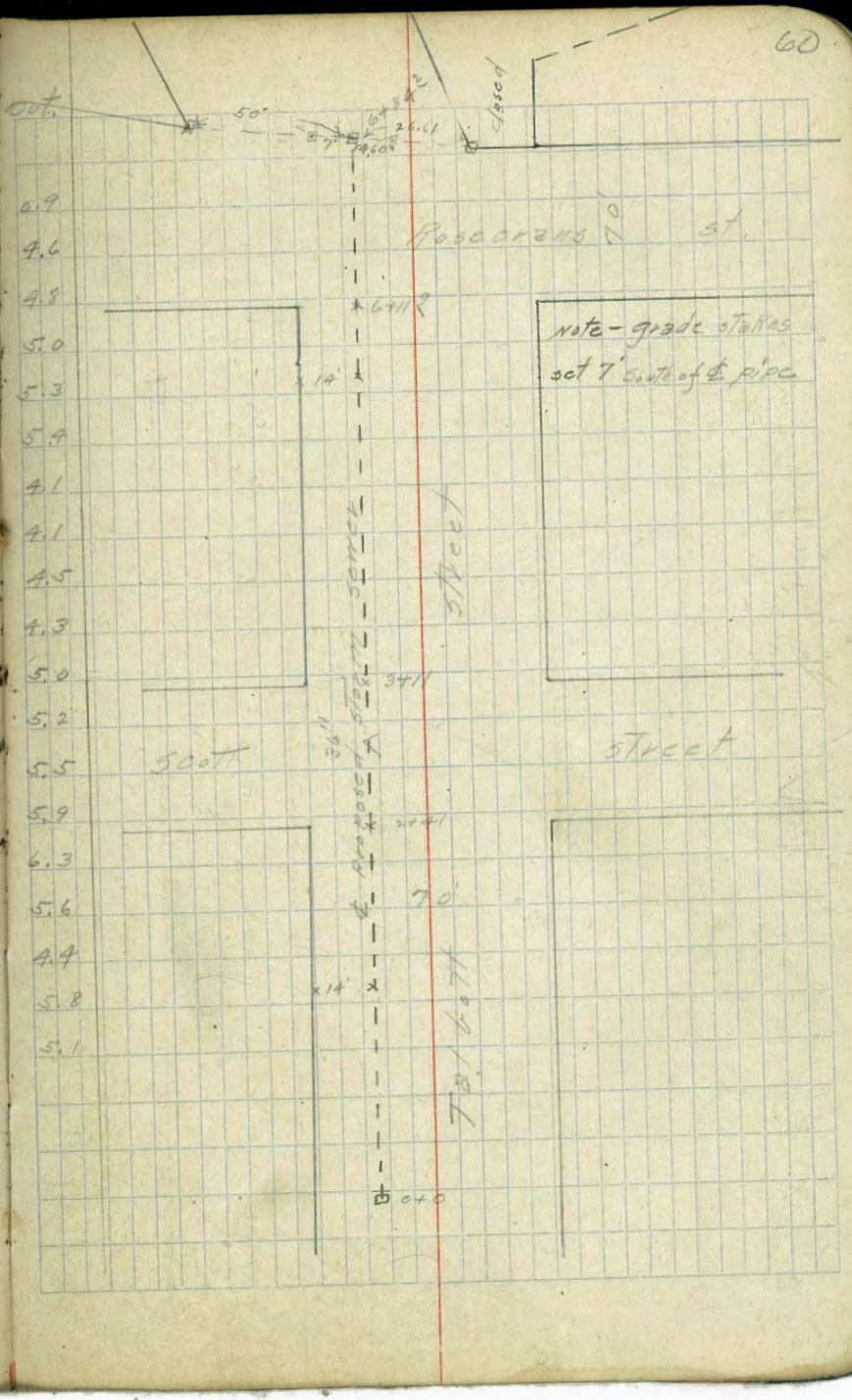
E			1.2	227.9 ✓
T.P.	13.14	248.23 ✓	00	229.09 ✓
T.P.	12.71	253.70 ✓	1.24	240.99 ✓
T.P.	1.282	265.91 ✓	9.61	253.09 ✓
on B.M.			0.35	265.56 ✓



Levels for proposed storm sewer - off Page 4 — by Shaw & Bunker — Dunkle grade

B.M. Man N.E. Talbott & Rosecrans — 2.48 — 28.80 — 21.32 Elev.

T.P.	7.20	13.28	12.72	11.08	
0+0			15.39	− 2.11	− 3.00
+50			10.20	2.98	− 1.64
1			8.78	4.50	− 0.77
+50			7.16	6.12	+ 1.09
2			5.54	7.74	2.46
+41 = E.L. Scott			9.30	8.98	3.58
+50			5.34	7.94	3.82
3			4.00	9.28	5.19
+11 = W.L. Scott Break in grade			3.23	10.06	5.50
+50			2.70	11.08	6.80
T.P.	12.59	26.11	0.76	12.52	
4			11.70	13.41	8.46
+50			9.76	15.35	10.13
5			7.78	17.33	11.79
+50			5.75	19.36	13.46
6			3.71	21.40	15.12
+21.9 = E. Curbline Rosecrans			3.63	21.48	15.85
+56.5 = W. rail & bottom of Tile			3.7	21.4	17.02
+60			3.23	21.88	17.17
+84.2 = W.L. Rosecrans,			2.14	23.00	17.92



8/21/16 Gregory Moore Miller

LEVELS ON 10TH ST
Xfrom University Av.
To Determine grade points
All distances taken Xfrom ~~N.E.~~ Univ. Ave. west of X 10th.

B.M.	7.30 curb	289.39		282.09	SW 10th & Univ.
N.E. Univ. Ave N.L. 10th			6.62	282.77	on cement
" " " E.L. curb			5.95	283.+	" "
100' No. of Univ N.L.			5.63	283.76	" "
150' " " " " "			5.13	284.76	" "
200' " " " N.Cb "			4.98	284.41	" "
230' " " " " "			4.82	284.57	" "
248 " " 0.3 E of EL. 10th			4.50	284.59	on walk to house
300 " " " W.Cb L. 10th			5.41	283.98	on cement
337 " " 0.4 E of EL. 10th			5.56	283.83	on walk to house
380.5 " " " W Cb L. 10th			6.13	283.26	E of X Walk
T.P.	4.25	287.93	5.71	283.68	
20' N. of X. Hendricks EL of 10			8.60	279.33	Top step.

Sidewalk on West Side 10th 5' wide

8/28/14 Gregory Moore Miller

CROSS SECTION OF HENDRICKS ST. 60' wide. 10' walks 10' gutters
Xfrom E.L. 10th to N.L. Vermont

B.M.	7.30	289.39 ✓		282.09	Sq. 10E Vale
T.P.	5.63	287.31 ✓	5.71	283.68 ✓	
	E.L. 10th St.				
S			41	283.2 ✓	
ab			41	283.2 ✓	
1/4			42	283.1 ✓	
C			45	282.8 ✓	
1/4			49	282.4 ✓	
ab			56	281.7 ✓	
N			61	281.2 ✓	
	{18.06'E on So. 00 E on No = Section A				
N			61	281.2 ✓	
ab			55	281.8 ✓	
1/4			51	282.2 ✓	
C			46	282.7 ✓	
1/4			44	282.9 ✓	
ab			43	283.0 ✓	
S			42	283.1 ✓	
	25' E of Sec. A				
S			44	282.9 ✓	
ab			46	282.7 ✓	
1/4			48	282.5 ✓	
C			48	282.5 ✓	
1/4			57	282.2 ✓	
ab			54	281.9 ✓	
N			58	281.5 ✓	

HENDRICKS

	50' E		
N		51	282.2 ✓
ab		54	281.9 ✓
1/4		49	282.4 ✓
C		46	282.7 ✓
1/4		43	283.0 ✓
ab		43	283.0 ✓
S		41	283.2 ✓
	75' E		
S		40	283.3 ✓
ab		43	283.0 ✓
1/4		45	282.8 ✓
C		48	282.5 ✓
1/4		51	282.2 ✓
ab		58	281.5 ✓
N		57	281.6 ✓
	100' E		
N		57	281.6 ✓
ab		54	281.9 ✓
1/4		51	282.2 ✓
C		46	282.7 ✓
1/4		43	283.0 ✓
ab		41	283.2 ✓
S		43	283.0 ✓
	125' E		
S		42	283.1 ✓

		287.31		
dc			4.5	282.8
1/4			4.5	282.8
c			4.7	282.6
1/4			4.8	282.5
dc			4.9	282.4
N			5.7	281.6
		150' E		
N			5.3	282.0
dc			5.1	282.2
1/4			4.9	282.4
C			4.7	282.6
1/4			4.7	282.6
dc			4.5	282.8
S			4.0	283.3
		175' E		
S			3.6	283.7
dc			3.7	283.6
1/4			3.9	283.4
C			4.2	283.1
1/4			4.4	282.9
dc			4.7	282.6
N			4.7	282.6
		200' E		
N			3.6	283.7
dc			3.6	283.7
1/4			3.5	283.8

HENDRICKS

C		3.2	284.1
1/4		3.3	284.0
dc		3.0	284.3
S		2.9	284.4
	225' E		
S		2.4	284.9
dc		2.5	284.8
1/4		2.7	284.6
C		2.9	284.4
1/4		2.8	284.5
dc		3.2	284.1
N		3.4	283.9
	255' E		
N		4.3	283.0
dc		3.9	283.4
1/4		3.4	283.9
C		2.8	284.5
1/4		2.6	284.7
dc		2.6	284.7
S		2.4	284.9
	265' E		
S		7.4	278.9
dc		7.2	280.1
1/4		5.8	281.5
C		4.0	283.3
1/4		4.6	282.7

		287.31			
dc			6.3	281.0	✓
+2			4.7	282.6	✓
N			5.9	281.4	✓
		275' E			
N			11.1	276.2	✓
dc			9.9	277.4	✓
1/4			9.6	277.7	✓
C			9.5	277.8	✓
1/4			10.8	276.5	✓
dc			11.9	275.4	✓
S			13.1	274.2	✓
T.P.	0.16	274.65 ✓	12.82	274.49 ✓	
		300' E			
-20			9.0	265.7 ✓	
S			9.6	265.1 ✓	
dc			10.6	264.1 ✓	
1/4			10.7	264.0 ✓	
C			10.5	264.2 ✓	
1/4			10.2	264.5 ✓	
dc			10.3	264.4 ✓	
N			11.4	263.3 ✓	
+20			12.6	262.1 ✓	
T.P.	3.27	265.71 ✓	12.81	261.84 ✓	
		315' E			
-30			11.6	254.1 ✓	
-20			10.6	255.1 ✓	

HENDRICKS

N		10.2	255.5	✓
dc		9.2	256.5	✓
1/4		8.3	257.4	✓
C		6.9	258.8	✓
1/4		7.8	257.9	✓
dc		9.7	256.0	✓
S		10.1	255.6	✓
+20		7.6	258.1	✓
+30		6.5	259.2	✓
	335' E			
-35		9.3	256.4	✓
-10		11.9	253.8	✓
S		12.4	253.3	✓
dc		12.9	252.8	✓
1/4		12.4	253.3	✓
C		12.7	253.0	✓
1/4		13.1	252.6	✓
T.P.	1.27	254.10 ✓	252.83	✓
dc		2.0	252.1	
N		2.5	251.6	
+20		1.1	253.0	
+40		4.3	249.8	
	395' E			
-50		10.5	243.6	
-30		6.5	247.6	

		254.10		
N			2.7	246.4
dr			6.8	247.3
1/4			5.4	248.7
C			4.9	249.2
1/4			4.6	249.5
dr			5.0	249.1
S			5.7	248.4
+7			1.4	252.7
+12			4.1	250.0
+40			1.5	252.6
+50			+1.8	255.9
		342' E		
-50.0			0.7	253.4
-40.0			2.8	251.3
-25			2.0	252.1
-13			3.5	250.6
-10			1.8	252.3
S			6.6	247.5
dr			8.0	246.1
1/4			7.4	246.7
C			6.8	247.3
1/4			7.7	246.4
dr			9.5	244.6
N			10.5	243.6
+25			10.3	243.8
+40			11.0	243.1
+55			14.7	239.4

HENDRICKS

		352' E		
-55			17.7	236.4
-40			14.7	239.4
-20			15.7	238.4
N			13.8	240.3
dr			12.8	241.3
1/4			10.8	243.3
C			10.2	243.9
1/4			8.3	245.8
dr			5.2	248.9
S			3.5	250.6
+12			0.3	253.8
+40			+1.5	255.6
		355' E		
-12			6.0	254.1
-40			+2.0	256.1
S			2.5	251.6
dr			3.9	250.2
1/4			7.1	247.0
C			9.8	244.3
1/4			11.6	242.5
dr			12.8	241.3
N			12.5	241.6
+10			13.5	240.6
+15			15.9	238.2
+25			17.5	236.6

		254.10		
+40			16.0	238.1
+55			18.8	235.3
		365'E		
-55			22.2	231.9
-35			19.7	234.4
-15			11.4	242.7
N			9.6	244.5
dr			9.5	244.6
1/4			9.2	244.9
C			7.2	246.9
1/4			3.9	250.2
dr			0.8	253.3
TP	12.01	265.91 ✓	0.20	253.90 ✓
S			11.0	254.9
+12			7.8	258.1
+40			5.8	260.1
		385'E		
-16			+1.6	267.5
S			-3.1	262.8
dr			6.2	259.7
1/4			9.6	256.3
C			13.6	252.3
1/4			15.7	250.2
dr			15.5	250.4
N			15.7	250.2
+25			18.9	247.0
+35			21.9	244.0

HENDRICKS

		400'E		
-20			12.6	253.3
N			8.3	257.6
dr			8.3	257.6
1/4			9.2	256.7
C			9.8	256.1
1/4			4.6	261.3
dr			0.9	265.0
TP	13.16	278.75 ✓	0.32	265.59 ✓
S			10.0	268.8
+12			5.2	273.6
		425'E		
-6			0.0	278.8
S			2.6	276.2
dr			7.4	271.4
1/4			11.8	267.0
+5			13.6	265.2
C			13.3	265.5
1/4			10.0	268.8
dr			9.0	269.8
N			9.3	269.5
+15			11.7	267.1
TP	12.32	290.69 ✓	0.38	278.37 ✓
		445'E		
-5			11.4	279.3
N			10.5	280.2

		290.69		
+5			9.6	281.1
cl			10.5	280.2
1/4			12.8	278.9
C			15.1	275.6
1/4			15.8	274.9
cl			13.5	277.2
S			10.1	280.6
+5			7.9	282.8
		450'E		
-5			6.6	284.1
S			8.9	281.8
cl			11.1	279.6
1/4			12.8	277.9
C			12.5	278.2
1/4			10.8	279.9
cl			8.1	282.3
N			8.5	282.2
+5			10.2	280.5
		467'E		
N			6.8	283.9
cl			6.3	284.4
1/4			6.3	284.4
C			7.1	283.6
+5			7.9	282.8
1/4			6.6	283.9
cl			5.7	285.0

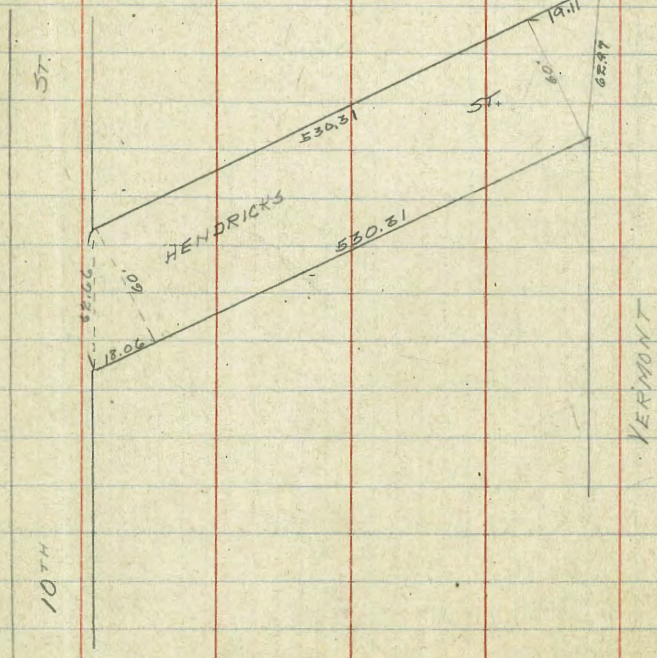
HENDRICKS

S		4.8	285.9
	470'E		
S		3.8	286.9
cl		4.3	286.4
1/4		4.4	286.3
C		4.8	285.9
1/4		5.2	285.5
cl		5.6	285.1
N		5.6	285.1
	500'E		
N		4.4	286.3
cl		4.6	286.1
1/4		4.4	286.3
C		3.9	286.8
1/4		3.6	287.1
cl		3.6	287.1
S		3.0	287.7
	530 E = SECTION B		
S		1.6	289.1
cl		2.7	288.0
1/4		2.4	288.3
C		2.6	288.1
1/4		3.0	287.7
cl		3.1	287.6
N		2.9	287.8

290.69

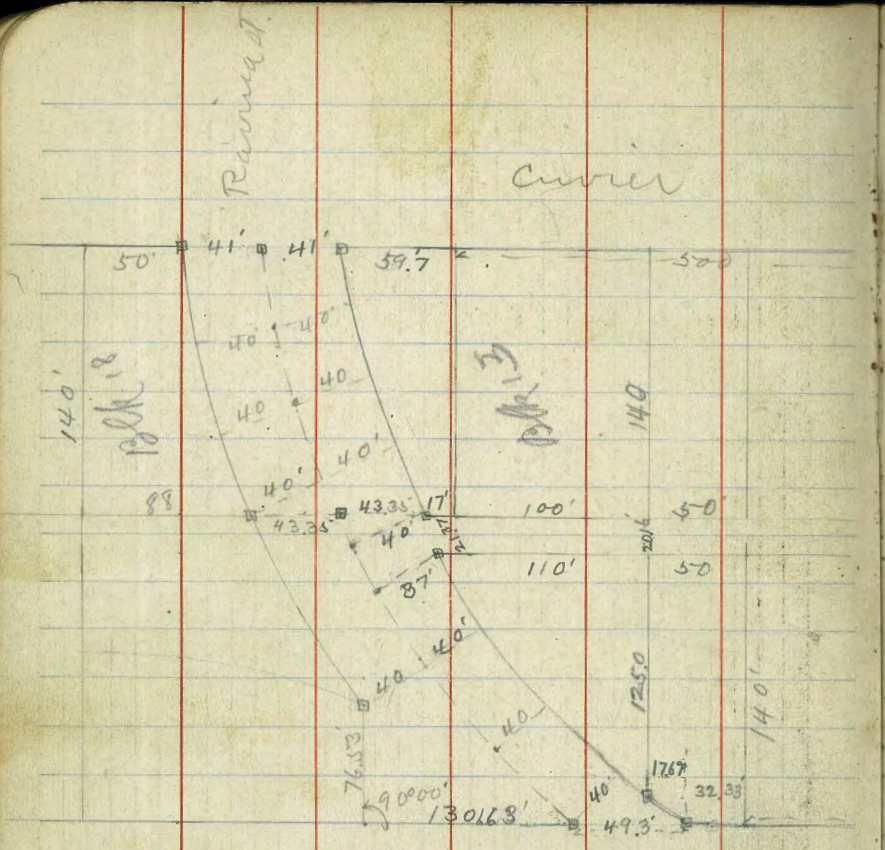
N.L Vermont St.

N			1.6	289.1
ob			2.2	288.5
1/4			2.2	288.5
C			2.0	288.7
1/4			2.1	288.6
ob			2.5	288.2
S			2.5	288.2
T.P.	5 W	291.45	1.65	289.04
C&H or B.M.			4.65	289.83 .79



Survey of center line of Ravina Street from Curran to Lajolla Boulevard.

Calculated Dept. 11 7/12/16 by Evans & Shaw

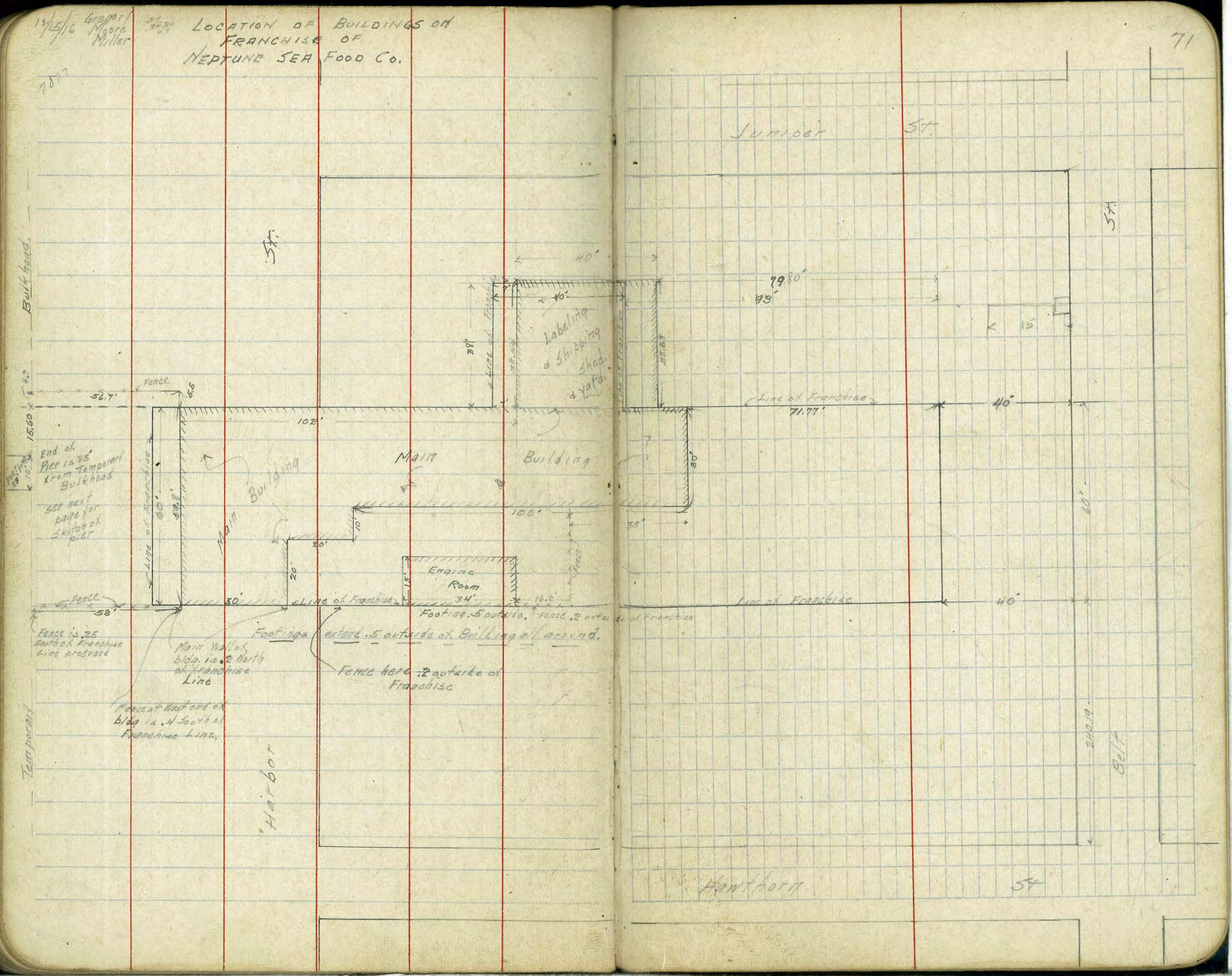


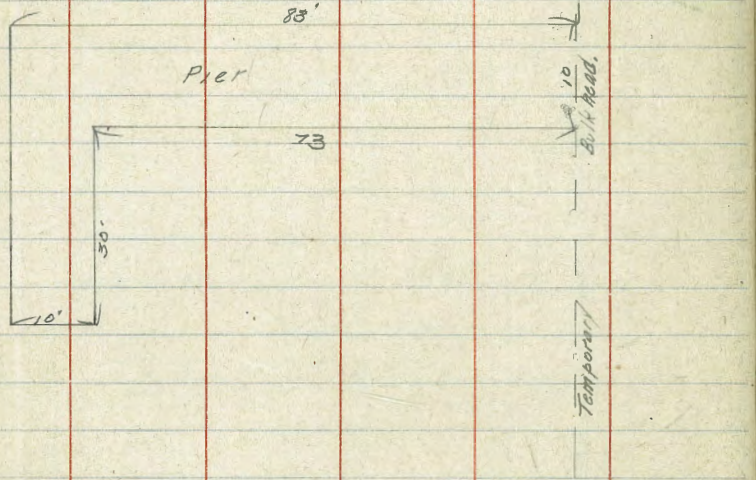
350.00'

Lajolla Blvd.

12/15/16 Gregori Moore Miller

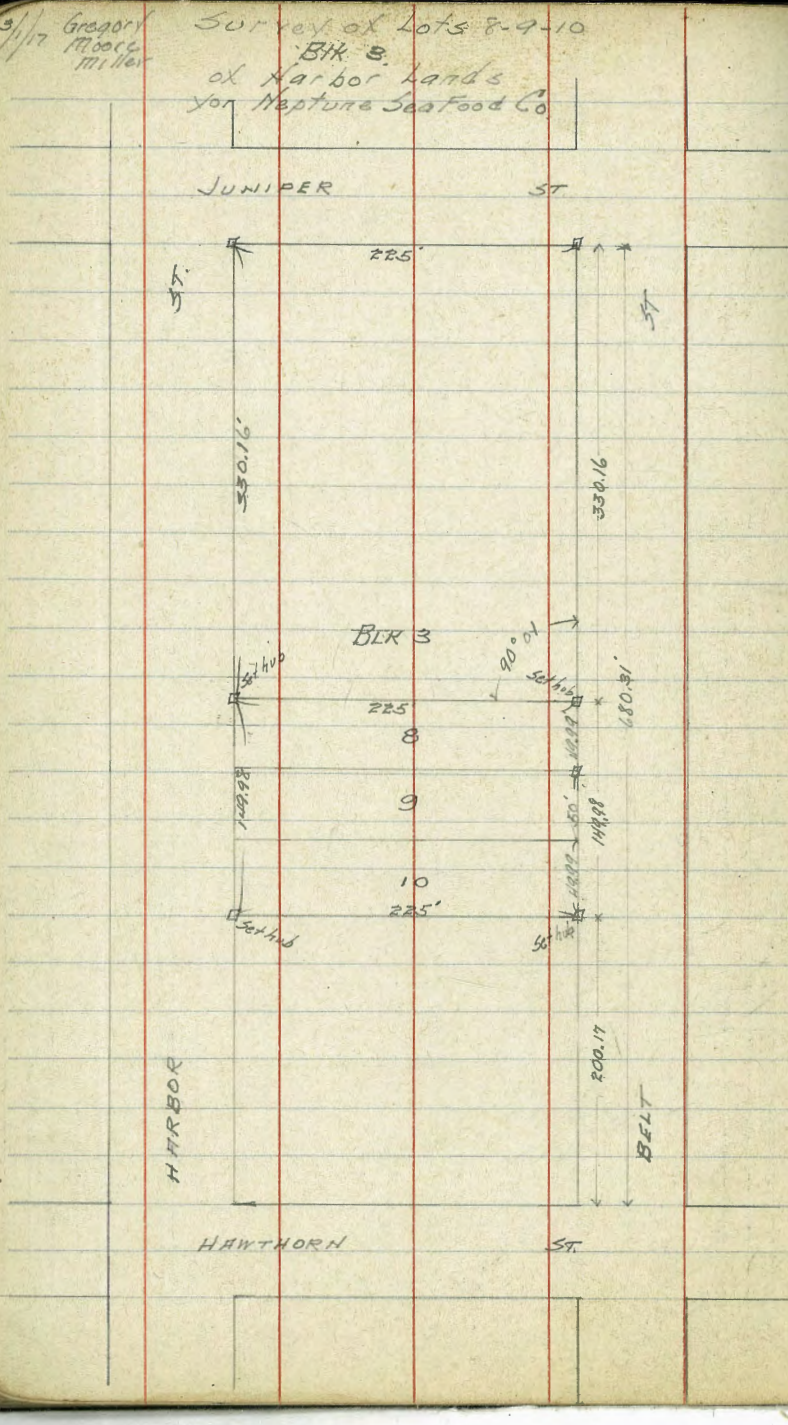
LOCATION OF BUILDINGS ON FRANCHISE OF NEPTUNE SEA FOOD Co.




Line of Franchise
150'
10
Bulk Head.
Temporary
83'
Pier
73
30'
10'

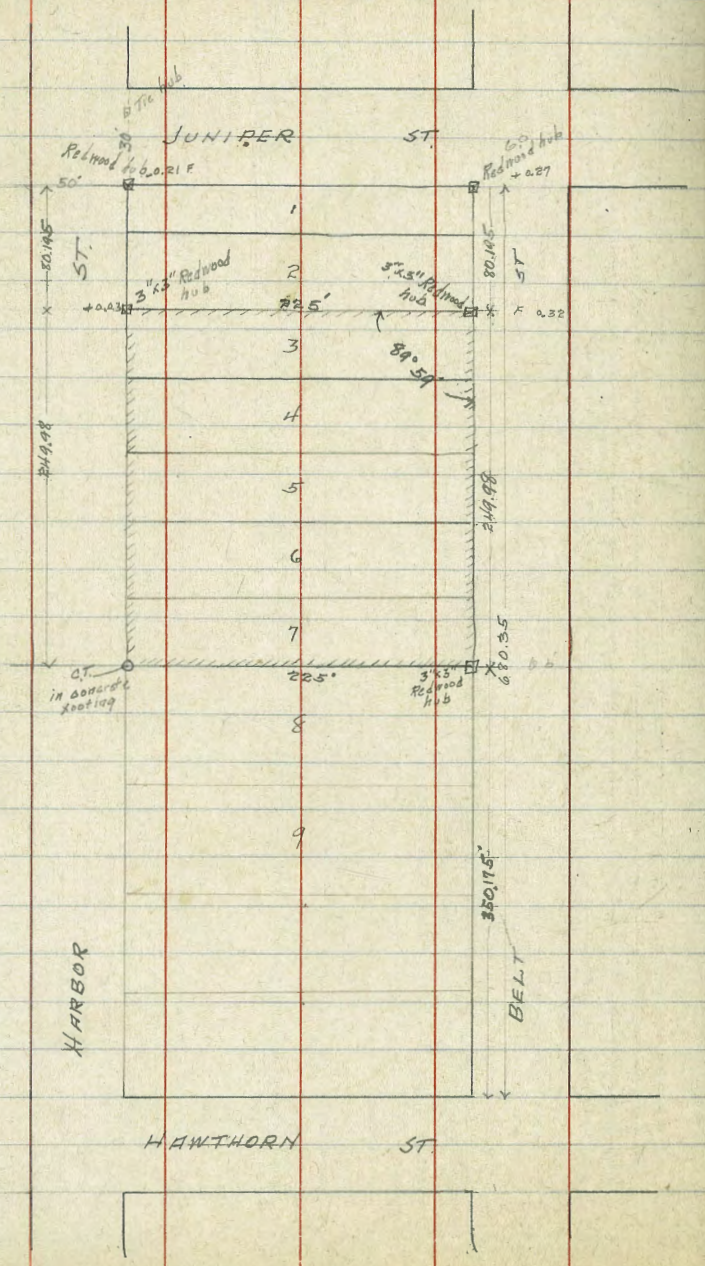
3/1/17 Gregory Moore Miller

Survey of Lots 8-9-10 Blk 3. of Harbor Lands for Neptune Seafood Co.



2/21/18 Gregory Moore Miller

Survey of Lots 3-4-5-6-7
BLOCK 3
of Harbor Lands
for Neptune Sea Food Co.



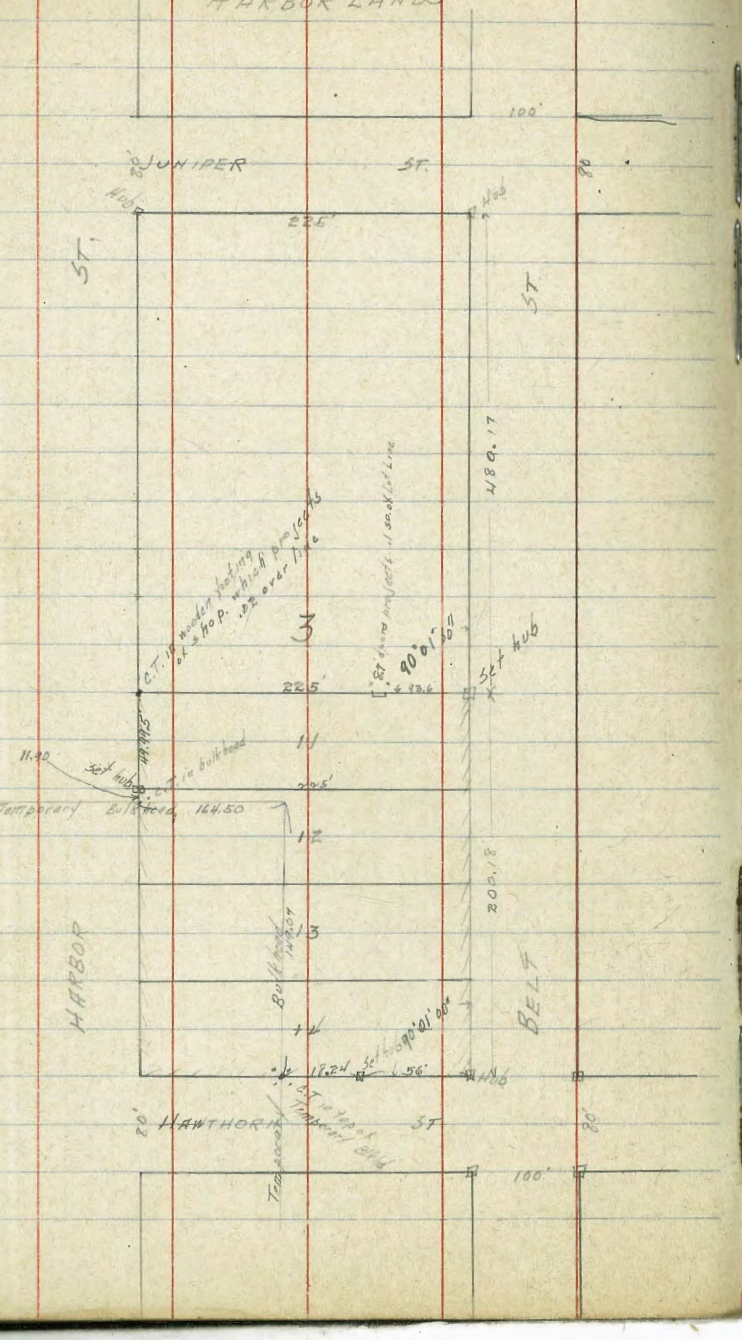
8.20 Top Hydrant type Atlantic
1.05
9.25
6.0 4.17
330 500 (.00152 80 .12160
330
1700
1500
500

405	385	506	485
4.80	4.27	4.79	5.03
0.32	0.00	5.00	5.00
5.12	4.27	-.21	+.03

75

10/8/18 Gregory

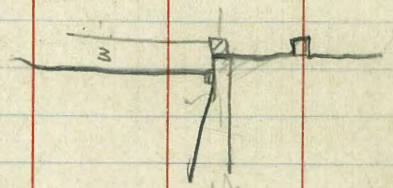
Survey of Lots H-12-13-14
BLOCK 3
HARBOR LANDS



Ocean Beach Plunge see P13

Oct 18/1918

Stg	Rod	⊖	Elev	
B.M.			+2.83	N. End Con. Curb
	+2.95	5.78	0.68	
	-5.92		-0.14 .87	N End Wall
	-5.82		-0.04	S End Wall
"A"	-5.95		-0.17	
"B"	-8.00		-2.22	
"C"	-4.15		+1.63	
"D"	-7.00		-1.22	
"E"	-3.55		+1.23	
"F"	-0.5		+5.28	
"G"				



119-17

189-44

143.47

Cromwell
Hoopes
Schwartz

81

359-60
281-45
78-15

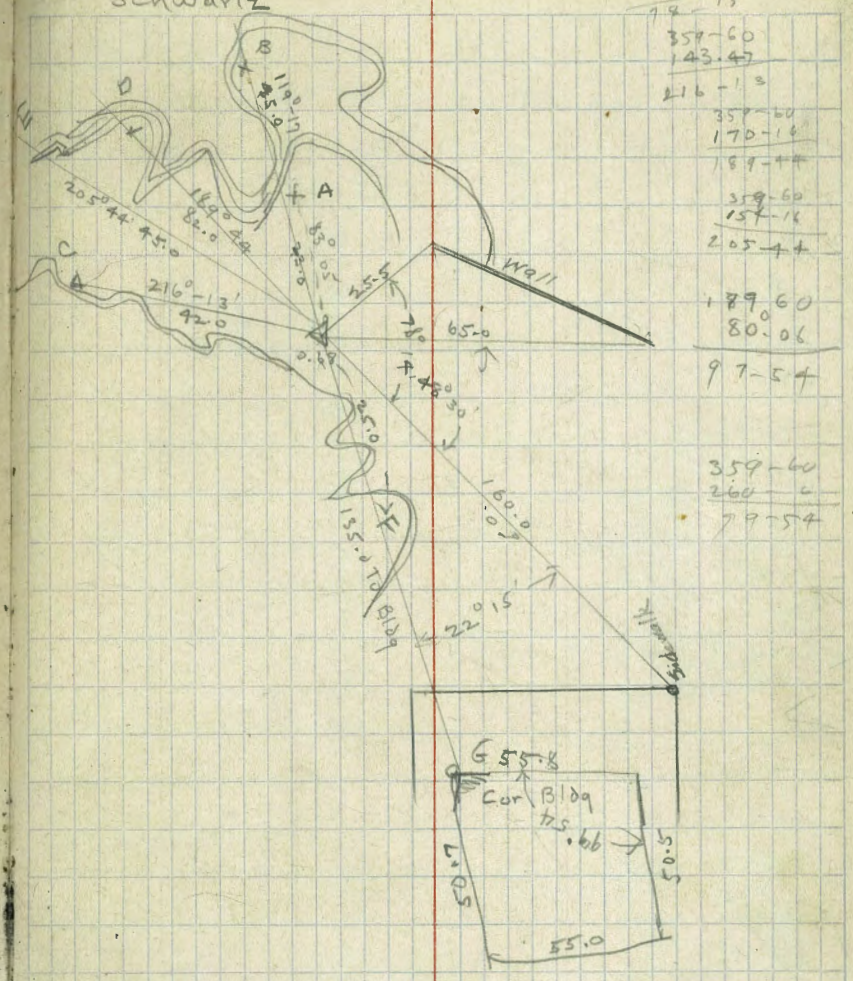
359-60
143.47
216-13

359-60
170-16
189-44

359-60
154-18
205-44

189-60
80.06
97-54

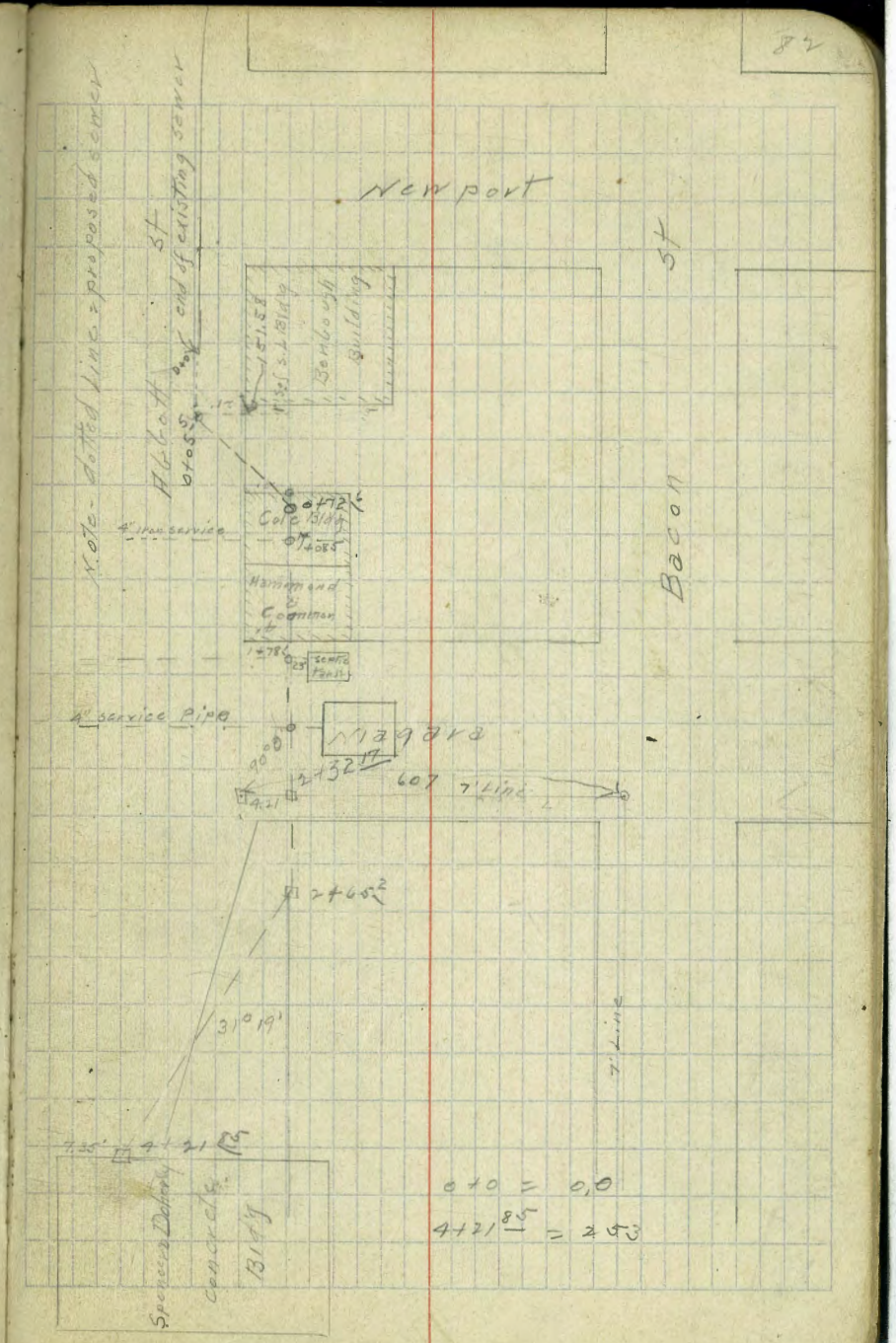
359-60
260-6
99-54



216-13
150
36-13

I

B.M. 6+33.3 pig Newport & Abbott				6.50
T.P.	5.09	11.39	5.03	6.30
0+0 = end of existing sewer			9.1	2.3
0+05.5 = 1'3 of S.L. Bamboogh Bldg			9.1	2.3
0+25			8.3	3.1
0+50			8.4	3.0
0+72.6			8.7	2.7
T.P.	2.68	4.73	9.34	(2.05)
0+78.5			2.2	2.5
1+03 IG			2.2	2.5
+08.5 = bottom 4" iron service			1.4	3.3
1+28 IG			2.0	2.7
1+33.5 = Rock surface			8.6	— 3.9
1+53 IG			2.0	2.7
T.P.	10.38	11.40	3.71	(.02)
1+78' = bottom 3" service pipe			12.5	— 1.1
1+78 IG			8.5	2.9
1+99+ = 4" service			11.7	— 0.3
2+03 IG			8.5	2.9
2+28 IG			8.4	3.0
2+30 IG Rock surface			14.5	— 3.1
2+53			7.2	4.2
2+65.2 R 31°19'			3.0	8.4
2+78 IG			5.8	5.6
2+96 IG			7.7	3.7
3+03 IG			7.0	4.4
3+28 IG			5.9	5.5
3+53 IG			6.1	5.3
3+78 IG			7.1	4.3
+85.5 IG			7.0	4.4
+92.4 IG			10.6	0.8
4+03 IG			6.0	5.4
4+21.85 Floor level & No wall of Spencer & Doherty Bldg			6.50	4.90



Sew Abbott St see page 82

I					
B.M.	4.87	11.37		6.50	
T.P.	3.30	5.20	9.47	1.90	
0+00 end existing sewer see page 82					0.00
0+06			2.75	2.50	0.04
0+50			1.98	3.22	0.30
0+72 6	Right Angles Two hubs 2ft	N. Hub	2.21	2.99	0.44
T.P.	3.13	S. hub	2.26	2.94	0.44
1+03 5		5.11	3.32	1.98	
			2.28	2.83	0.62
1+35 5			2.21	2.90	0.92
	4.99	6.97	3.13	1.98	
2+03 5			1.49	5.48	1.22
2+53.5	5.27	11.98	0.26	6.71	1.53
2+65 2	R 31° 19'	2 Hubs	N Hub 1.53 S Hub 1.60	10.45 10.38	1.59
2+96 5			5.95	6.03	1.78
3+53 5			2.74	8.24	2.12
3+92 5			10.10	1.88	2.35
4+21 85	= Metcalf Spencer Daybert		6.09	5.89	2.53

2.71

2.92

2.45

2.50

2.21

1.88

4.26

5.18

8.86

8.79

4.25

6.12

- 0.37

3.36

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P.=23° 20′ to the R. at Station 542+72.

Ext. in Tab. IV opposite 23° 20′=120.87
120.87+12=10.07. Say a 10° Curve.

Tan. in Tab. IV opp. 23° 20′=1183.1
1183.1+10=118.31.

Tab. V. correction for A. 23° 20′ for a 10° Cur.=0.16
118.31+0.16=118.47=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. 23° 20′=23.33°÷10=2.3333=L. C.

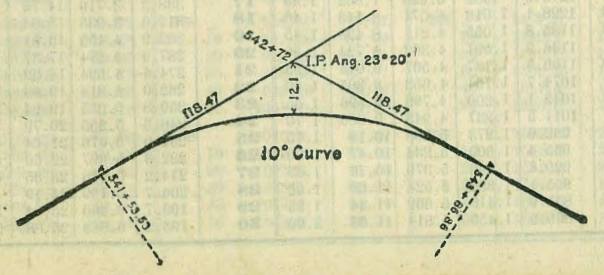
2° 19½′=def. for sta.	542	I. P.=sta.	542+72
4° 49½′= " " "	+50	Tan.=	1.18.47
7° 19½′= " " "	543	B. C.=sta.	541+53.53
9° 49½′= " " "	+50	L. C.=	2.33.33
11° 40′= " " "	543+	E. C.=sta.	543+86.86
	86.86		

100—53.53=46.47×3′(def. for 1 ft. of 10° Cur.)=139.41′=
2° 19½″=def. for sta. 542.

Def. for 50 ft.=2° 30′ for a 10° Curve.

Def. for 86.86 ft.=1° 50½′ for a 10° Curve

(These tables are published in Field Books of KEUFFEL & ESSER Co., New York, N. Y.)



Natural Tangents

deg.	0′	10′	20′	30′	40′	50′	deg.	deg.	0′	10′	20′	30′	40′	50′	deg.
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1 0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1 1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1 1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3452	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4785	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2 1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2 6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3 1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3 3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4 1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
deg.	60′	50′	40′	30	20′	10′	deg.	deg.	60′	50′	40′	30′	20′	10′	deg.

deg.	0′	10′	20′	30′	40′	50′	deg.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.77	0
deg.	60′	50′	40′	30′	20′	10′	deg.

Natural Cotangents

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.