

986

F.B. 986

LEVEL BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO.

SAN FRANCISCO.

ST. LOUIS.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION

"Copyright, 1886, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

30 st X Secs.
 Univ to El Cajon - 80' Wide
 14' Walks - 13' 1/4's

B.M. 3W. Howard & 30 st. Spk. Folk. 367.70

410 371.80

J.L. El Cajon

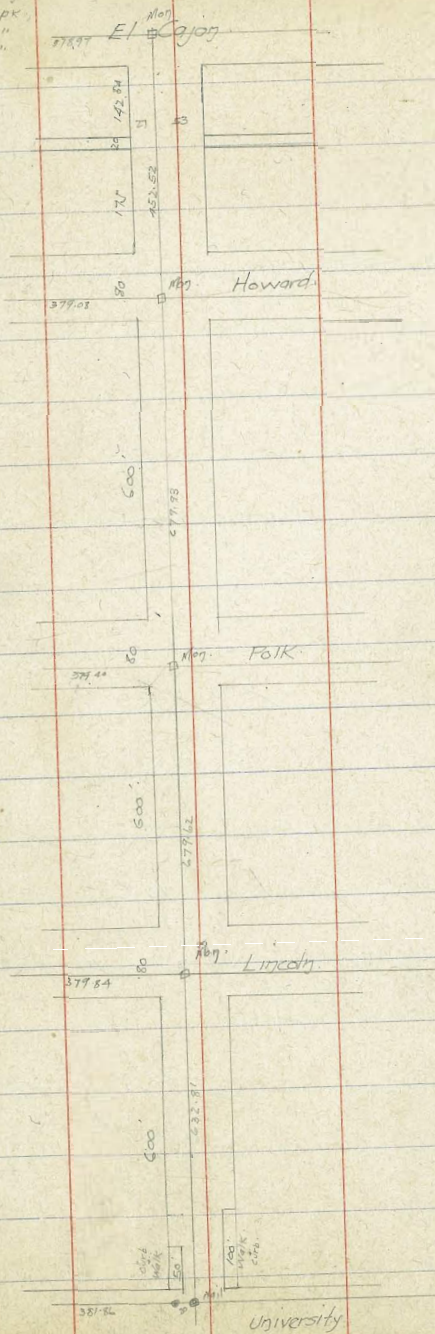
W.L.	6.8	365.0
C.	{ 7.2	364.6
	{ 7.8	364.0
1/4.	7.6	364.2
£.	7.5	364.3
1/4.	7.5	364.3
C.	{ 8.3	363.5
	{ 7.5	364.3
EL.	7.3	364.5

50' South.

EL.	7.0	364.8
C.	7.4	364.4
+1	8.0	363.8
1/4.	7.5	364.3
£.	7.2	364.6
1/4.	7.5	364.3
+11	7.6	364.2
C.	7.0	364.8
W.L.	6.7	365.1

B.M. NW 30 - Univ 356.03 Plug
 SW - Lincoln 361.18 Spk
 " " " " Folk 364.31 "
 " " " " Howard 367.70 "

4/2/15
 West
 Open
 Moore.



30 St

371.80

100' South

W.L.	62	365.6
C.	65	365.3
+2	72	364.6
1/4	7.1	364.7
E.	6.9	364.9
1/4	7.3	364.5
+11	7.6	364.2
C.	6.9	364.9
EL	6.7	365.1
1425 S. N.L. Alley.		
EL	6.3	365.5
C.	6.8	365.0
+2	7.3	364.5
1/4	6.9	364.9
E.	6.5	365.3
1/4	6.6	365.2
+11	6.9	364.9
C.	6.1	365.7
W.L.	5.8	366.0

30 St.

371.80

162⁶ South = S.L. Alley.

3

W.L.	5.6	366.2
C.	6.1	365.7
+2	6.7	365.1
1/4	6.5	365.3
E.	6.3	365.5
1/4	6.7	365.1
+11	7.1	364.7
C.	6.4	365.4
EL	6.1	365.7
187 ⁶ South.		
EL	5.7	366.1
C.	6.2	365.6
+2	6.9	364.9
1/4	6.5	365.3
E.	6.1	365.7
1/4	6.3	365.5
+11	6.6	365.2
C.	5.9	365.9
W.L.	5.4	366.4

30 St.

371.80

237⁶ South

WL.	5.1	366.7
C	5.4	366.4
+2	6.1	365.7
1/4	5.9	365.9
±	5.7	366.1
1/4	6.4	365.4
+11	6.4	365.4
C	5.8	366.0
EL.	5.5	366.3

287⁶ South

EL.	5.0	366.8
C	5.6	366.2
+2	6.0	365.8
1/4	5.8	366.0
±	5.5	366.3
1/4	5.7	366.1
+11	5.9	365.9
C	5.0	366.8
WL.	4.7	367.1

30 St.

371.80

MWKS-13' 1/2

337⁶ South - NL Howard 80' Wide 4

WL.	4.3	367.5
C	4.7	367.1
+2	5.6	366.2
1/4	5.4	366.4
±	5.1	366.7
1/4	5.2	366.6
+11	6.0	365.8
C	5.0	366.8
EL.	4.7	367.1

North Curb.

EL.	5.4	366.4
C	5.9	365.9
1/4	5.4	366.4
±	5.0	366.8
1/4	5.3	366.5
C	5.8	366.0
+6	5.4	366.4
WL.	4.8	367.0

30 St.

371.80

North 1/4 Howard

WL	4.8	367.0
C	5.8	366.0
1/4	5.3	366.5
£	5.0	366.8
1/4	5.3	366.5
C	5.8	366.0
EL	5.3	366.5

£ Howard

EL	4.6	367.2
C	5.8	366.0
1/4	5.4	366.4
£	5.0	366.8
1/4	5.3	366.5
C	6.0	365.8
WL	4.7	367.1

30 St.

371.80

5 1/4 Howard

5

WL	5.0	366.8
C	5.9	365.9
1/4	5.3	366.5
£	5.0	366.8
1/4	5.1	366.7
C	5.8	366.0
EL	5.2	366.6

3 Curb-Howard

EL	5.3	366.5
C	5.8	366.0
1/4	5.5	366.3
£	5.0	366.8
1/4	5.2	366.6
C	5.8	366.0
WL	5.0	366.8

30 St.371.80

J.L. Howard

WL	4.3	367.5
C	5.1	366.7
1/4	5.2	366.6
£	4.9	366.9
1/4	5.2	366.6
+11	5.9	365.9
C	5.0	366.8
EL	4.8	367.0

50' South of Howard

EL	5.1	366.7
C	5.2	366.6
+2	6.1	365.7
1/4	5.4	366.4
£	5.2	366.6
1/4	5.5	366.3
+11	5.9	365.9
C	5.2	366.6
WL	4.7	367.1

30 St.371.80

100' South

6

WL	5.1	366.7
C	5.3	366.5
+2	6.0	365.8
1/4	5.7	366.1
£	5.5	366.3
1/4	5.7	366.1
+11	6.5	365.3
C	5.7	366.1
EL	5.4	366.4

150' South

EL	5.6	366.2
C	6.2	365.6
+2	6.9	364.9
1/4	5.9	365.9
£	5.9	365.9
1/4	6.2	365.6
+11	6.6	365.2
C	5.7	366.1
WL	5.5	366.3

30 St.

371.80

T.P.

5.60

366.20

2.87

369.07

200' South of Howard.

WL.

3.0

366.1

C

3.4

365.7

+2

4.1

365.0

1/4

3.9

365.2

E

3.5

365.6

1/4

3.7

365.4

+11

4.5

364.6

C

3.8

365.3

EL

3.5

365.6

250' South

EL

3.9

365.2

C

4.3

364.8

+2

5.0

364.1

1/4

4.1

365.0

E

4.0

365.1

1/4

4.3

364.8

+11

4.6

364.5

C

3.7

365.4

WL

3.5

365.6

30 St.

369.07

7

300' South.

WL

3.7

365.4

C

4.1

365.0

+2

4.9

364.2

1/4

4.6

364.5

E

4.2

364.9

1/4

4.5

364.6

+11

5.2

363.9

C

4.5

364.6

EL

4.3

364.8

350' South

EL

4.7

364.4

C

4.9

364.2

+2

5.5

363.6

1/4

5.1

364.0

E

4.8

364.3

1/4

5.0

364.1

+11

5.2

363.9

C

4.3

364.8

WL

4.1

365.0

30 St.

369.07

400' South

WL	4.4	364.7
C	4.7	364.4
+Z	5.3	363.8
1/4	5.4	363.7
⊕	5.3	363.8
1/4	5.3	363.8
+11	6.0	363.1
C	5.1	364.0
EL	5.0	364.1

450' South

EL	5.4	363.7
C	5.6	363.5
+Z	6.2	362.9
1/4	5.7	363.4
⊕	5.4	363.7
1/4	5.6	363.5
+11	5.8	363.3
C	5.1	364.0
WL	4.9	364.2

30 St.

369.07

500' South

8

WL	5.3	363.8
C	5.4	363.7
+Z	6.0	363.1
1/4	6.0	363.1
⊕	5.6	363.5
1/4	5.7	363.4
+11	6.3	362.8
C	5.8	363.3
EL	5.7	363.4

550' South

EL	5.9	363.2
C	6.3	362.8
+Z	6.7	362.4
1/4	6.1	363.0
⊕	5.4	363.7
1/4	6.1	363.0
+11	6.2	362.9
C	5.7	363.4
WL	5.5	363.6

30 St.

369.07

600 S = NL Polk 80' wide 14 WKS - 13 1/4 S

WL	5.8	363.3
C	6.1	363.0
+2	6.5	362.6
1/4	6.2	362.9
£	5.5	363.6
1/4	6.2	362.9
C	6.5	362.6
EL	6.2	362.9

N. Curb Polk

EL	6.1	363.0
1/4 C	6.3	362.8
1/4	5.9	363.2
£	5.5	363.6
1/4	6.1	363.0
C	6.4	362.7
WL	6.2	362.9

30 St.

369.07

N 1/4 of Polk

9

WL	5.8	363.3
C	6.2	362.9
1/4	6.1	363.0
£	5.4	363.7
1/4	5.7	363.4
C	5.7	363.4
EL	5.6	363.5

£ Polk

EL	5.5	363.6
C	5.9	363.2
1/4	6.0	363.1
£	5.4	363.7
1/4	5.8	363.3
C	5.7	363.4
WL	5.2	363.9

30 St.

369.07

5.1/4 Polk.

WL	5.1	364.0
C	5.3	363.8
1/4	5.7	363.4
Φ	5.5	363.6
1/4	5.8	363.3
C	5.9	363.2
EL	5.7	363.4

3. Curb of Polk

EL	5.5	363.6
C	6.2	362.9
1/4	5.7	363.4
Φ	5.5	363.6
1/4	5.6	363.5
C	5.9	363.2
WL	5.6	363.5

30 St.

369.07

5.1/4 Polk.

10

WL	5.0	364.1
C	5.7	363.4
+2	6.1	363.0
1/4	5.8	363.3
Φ	5.4	363.7
1/4	6.1	363.0
C	6.3	362.8
EL	5.5	363.6
TP	5.4	363.60

6.13 369.73

5.0' South of Polk.

EL	5.9	363.8
C	6.3	363.4
+2	6.6	363.1
1/4	6.5	363.2
Φ	6.1	363.6
1/4	6.2	363.5
+11	6.4	363.1
C	5.8	363.9
WL	5.6	364.1

30 St369.73

100' South.

WL.	54	364.3
C.	57	364.0
+Z	64	363.3
1/4	61	363.6
±	59	363.8
1/4	63	363.4
+11	65	363.2
C.	63	363.4
EL	56	364.1

150' South.

EL.	53	364.4
C.	56	364.1
+Z	62	363.5
1/4	61	363.6
±	57	364.0
1/4	60	363.7
+11	66	363.1
C.	54	364.3
WL.	53	364.4

30 St369.73

200' South.

11

WL.	52	364.5
C.	57	364.3
+Z	64	363.3
1/4	59	363.8
±	56	364.1
1/4	57	364.0
+11	61	363.6
C.	55	364.2
EL	53	364.4

250' South.

EL.	50	364.7
C.	54	364.3
+Z	61	363.6
1/4	58	363.9
±	54	364.3
1/4	58	363.9
+11	63	363.4
C.	53	364.4
WL.	49	364.8

30 St

369.73

300' South

WL	5.2	364.5
C	5.5	364.2
+Z	6.5	363.2
1/4	5.8	363.9
£	5.4	364.3
1/4	5.7	364.0
+11	5.8	363.9
C	5.3	364.4
EL	5.0	364.7
	350' South	
EL	5.3	364.4
C	5.5	364.2
+Z	6.0	363.7
1/4	6.2	363.5
£	5.8	363.9
1/4	6.2	364.5
+11	6.7	363.0
C	5.6	364.1
WL	5.4	364.3

30 St

369.73

400' South

12

WL	5.7	364.0
C	6.1	363.6
+Z	7.1	362.6
1/4	6.5	363.2
£	6.2	363.5
1/4	6.6	363.1
+11	6.9	362.8
C	6.2	363.5
EL	5.9	363.8
	450' South	
EL	6.5	363.2
C	6.8	362.9
+Z	7.4	362.3
1/4	7.3	362.4
£	6.8	362.9
1/4	7.1	362.6
+11	7.6	362.1
C	6.6	363.1
WL	6.4	363.3

30 St.
369.73

500' South.

WL	6.8	362.9
C	7.3	362.4
+2	8.2	361.5
1/4	7.8	361.9
£	7.5	362.2
1/4	7.8	361.9
+11	8.1	361.6
C	7.5	362.2
EL	7.1	362.6
TP	7.39	362.34

309

365.43

550' South.

EL	3.5	361.9
C	3.8	361.6
+2	4.4	361.0
1/4	4.2	361.2
£	3.9	361.5
1/4	4.1	361.3
+11	4.5	360.9
C	3.5	361.9
WL	3.1	362.3

30 St.

365.43

600' South - N.L. Lincoln, 80' Wide - 14' WKS - 13' 65' 18

WL	3.7	361.7
C	4.4	361.0
+2	5.2	360.2
1/4	4.6	360.8
£	4.4	361.0
1/4	4.7	360.7
+11	5.2	360.2
C	4.4	361.0
EL	4.4	361.0

N. Curb of Lincoln

EL	4.7	360.7
C	5.1	360.3
1/4	5.0	360.4
£	4.5	360.9
1/4	4.7	360.7
C	5.2	360.2
WL	4.6	360.8

30 St

365.43

N. 1/4 Lincoln

WL	4.9	360.5
C	5.3	360.1
1/4	4.7	360.7
£	4.5	360.9
1/4	5.0	360.4
C	5.3	360.1
EL	4.9	360.5

£ Lincoln

EL	4.7	360.7
C	5.0	360.4
1/4	5.1	360.3
£	4.8	360.6
1/4	4.8	360.6
C	5.6	359.8
WL	4.4	361.0

30 St

365.43

S. 1/4 Lincoln

14

WL	4.9	360.5
C	5.5	359.9
1/4	4.9	360.5
£	4.6	360.8
1/4	5.0	360.4
C	5.3	360.1
EL	5.1	360.3

S. Curb of Lincoln

EL	5.2	360.2
C	5.5	359.9
1/4	5.2	360.2
£	4.8	360.6
1/4	5.0	360.4
C	5.5	359.9
WL	5.0	360.4

30 St.365.43S.L. Lincoln.

WL.	45	360.9
C	48	360.6
+Z	53	360.1
$\frac{1}{4}$	52	360.2
£	49	360.5
$\frac{1}{4}$	54	360.0
+11	59	359.5
C	50	360.4
EL.	49	360.5

50' South.

EL	53	360.1
C	54	360.0
+Z	62	359.2
$\frac{1}{4}$	58	359.6
£	54	360.0
$\frac{1}{4}$	55	359.9
+11	61	359.3
C	51	360.3
WL.	48	360.6

30 St.365.43100' South.

15

WL.	53	360.1
C.	56	359.8
+Z	62	359.2
$\frac{1}{4}$	60	359.4
£.	59	359.5
$\frac{1}{4}$	62	359.2
+11	66	358.8
C.	58	359.6
EL.	57	359.7

150' South.

EL.	61	359.3
C.	62	359.2
+Z	70	358.4
$\frac{1}{4}$	66	358.8
£.	62	359.2
$\frac{1}{4}$	64	359.0
+11	67	358.7
C	58	359.6
WL.	58	359.6

30 St.365.43

200' South of Lincoln

WL	60	359.4
C	65	358.9
+Z	6.9	358.5
1/4	6.6	358.8
⊖	6.5	358.9
1/4	7.1	358.3
+11	7.2	358.2
C	6.6	358.8
EL	6.4	359.0

250' South

EL	6.7	358.7
C	6.9	358.5
+Z	7.4	358.0
1/4	7.2	358.2
⊖	6.7	358.7
1/4	6.9	358.5
+11	7.3	358.1
C	6.6	358.8
WL	6.4	359.0

30 St.365.43

6.70

358.70

16

T.P.

347

362.20

300' South

WL	3.8	358.4
C	4.1	358.1
+Z	4.8	357.4
1/4	4.1	358.1
⊖	3.8	358.4
1/4	4.2	358.0
+11	4.6	357.6
C	4.1	358.1
EL	4.0	358.2

350' South

EL	4.3	357.9
C	4.4	357.8
+Z	5.2	357.0
1/4	4.8	357.4
⊖	4.5	357.7
1/4	4.7	357.5
+11	5.1	357.1
C	4.3	357.9
WL	4.1	358.1

30 St.

362.20

400' South

WL	4.6	357.6
C	4.9	357.3
+2	5.5	356.7
1/4	5.1	357.1
£	4.7	357.5
1/4	5.2	357.0
+11	5.8	356.4
C	4.8	357.4
EL	4.7	357.5

450' South

EL	5.1	357.1
C	5.3	356.9
+2	6.2	356.0
1/4	5.7	356.5
£	5.1	357.1
1/4	5.4	356.8
+11	6.0	356.2
C	5.1	357.1
WL	5.1	357.1

30 St.

362.20

500' South

17

WL	5.1	357.1
C	5.6	356.6
+2	6.3	355.9
1/4	5.8	356.4
£	5.4	356.8
1/4	6.0	356.2
C	6.3	355.9
C	5.9	356.3
EL	5.4	356.8

Note: ←

E. Curb in from here

to NL University, also walk.

550' South

EL	5.8	356.4
C	6.1	356.1
C	6.7	355.5
1/4	6.2	356.0
£	5.9	356.3
1/4	6.2	356.0
C	6.4	355.8
C	5.9	356.3
WL	5.7	356.5

Note - from here to
NL Univ, walk & curb in.

30 St.

362.20

600' South - NL University.

WL.	6.0	356.2
C	6.3	355.9
	6.8	355.4
1/A	6.5	355.7
⊕	6.3	355.9
1/A	6.4	355.8
C	6.9	355.3
	6.3	355.9
EL.	6.1	356.1
DM-NW Univ & 30 Plug.	6.24	355.96
		356.03 = OK.
		.07

6/22/15 - West - Otter - Moore.

X Sec. State St. 75' Wide
 10' Wks - 13²⁵/₁₀₀
 from N.L. Laurel to St. Maple.

7/6/15. What
 Other
 Name.

76.72

19

BM. NW Curb State & Laurel Keel		73.00	1/4	154	61.3
	3.72	76.72	±	10.7	66.0
		N.L. Laurel	1/4	5.1	71.6
EL.		1.2	C	2.1	74.6
C		1.6	EL	1.5	75.2
+9		2.1			
1/4		4.8		34' N. = 266' So. Maple	
+11		8.9	EL	2.2	74.5
±		2.7	+4	2.6	74.1
+5		3.3	C	4.8	71.9
1/4		5.5	+6	5.9	70.8
+8		11.2	1/4	9.2	67.5
C		8.9	±	12.9	63.8
+3		7.3	1/4	16.7	60.0
WL		4.6	C	20.9	55.8
			WL	22.6	54.1
		20' N. = 280' So. Maple	+13	26.0	50.7
-27 ¹⁰ = 100'		22.7	+37 = Tol.	29.6	47.1
-23		22.0			
WL		18.9			
C		16.2			
+7		13.3			

50' N. State 01
= 250' So. Maple

76.72 HS.

-49 ² Toc.	39.0	37.7 ✓
-23	29.9	46.8 ✓
WL.	23.8	52.9 ✓
+6	22.0	54.7 ✓
C	24.3	52.4 ✓
1/4	20.8	55.9 ✓
£	17.1	59.6 ✓
1/4	14.1	62.6 ✓
C	9.4	67.3 ✓
EL.	7.3	69.4 ✓

55' N. = 245' So. Maple

EL.	8.3	68.4 ✓
C	10.6	66.1 ✓
1/4	13.4	63.3 ✓
£	17.1	59.6 ✓
1/4	20.7	56.0 ✓
C	24.4	52.3 ✓
WL.	25.3	51.4 ✓
+23	32.5	44.2 ✓
+36	37.0	39.7 ✓
+49	41.6	35.1 ✓
+56 ⁸ Toc.	43.8	37.9 ✓

76.72

60' N. = 240' So. Maple

20

-51 ¹ Toc = top 30" pipe.	43.0	33.7 ✓
-48	42.9	33.8 ✓
-35	42.4	34.3 ✓
-22	35.1	41.6 ✓
WL.	29.0	47.7 ✓
C	24.7	52.0 ✓
1/4	19.0	57.7 ✓
£	16.3	60.4 ✓
1/4	13.3	63.4 ✓
C	11.0	65.7 ✓
EL.	8.6	68.1 ✓
+3.7 = Toc	7.3	69.4 ✓

75' N. = 225' So. Maple

-6 = Toc	7.7	67.0 ✓
EL.	12.5	64.2 ✓
+6	13.4	63.3 ✓
C	17.2	59.5 ✓
1/4	15.7	61.0 ✓
£	17.5	59.2 ✓
1/4	20.0	56.7 ✓
C	22.2	54.5 ✓

State St.

76.72

C	27.8	48.9
W.L.	35.7	41.0
+19	41.8	34.9
+32	42.0	34.7
+40	42.0	34.7
+48.6 Too slope.	39.3	37.4
92' N. = 208' S. Maple		
- 39.8 Too slope	34.3	42.4
- 36	35.1	41.6
-23	40.2	36.5
-6	42.5	34.2
W.L.	42.7	34.0
C	39.2	37.5
1/4	32.5	44.2
⊥	27.6	49.1
1/4	21.0	55.7
C	16.2	60.5
EL.	11.7	65.0
+5 = Too.	10.1	66.6
T.P.	12.70	64.02

236

66.38

66.38

100' N. = 200' S. Maple

21

-5.5 = too	0.5	65.9
EL.	3.2	63.2
C	9.4	57.0
1/4	15.0	51.4
⊥	21.3	45.1
1/4	26.3	40.1
C	30.7	35.7
+6	31.8	34.6
+7	34.7	31.7
W.L.	34.8	31.6
+19	28.4	38.0
+36 = too	21.9	44.5
110' N. = 190' S. Maple		
-33 = too	19.6	46.8
-25	21.8	44.6
W.L.	31.0	35.4
C	33.6	32.8
1/4	30.8	35.6
⊥	27.4	39.0
1/4	21.0	45.4

66.38

State St.

C		13.8	52.6
EL.		6.5	59.9
+ 7 ² toe.		3.2	63.2
	120' N. = 180' S. maple		
- 11 ¹ toe.		5.6	60.8
T.P.		12.96	53.42
	410	57.52	
EL.		6.6	50.9
C.		10.5	47.0
1/4		19.2	38.3
£		23.9	33.6
1/4		24.5	33.0
+5		24.5	33.0
+7		23.0	34.5
C		20.3	37.2
WL.		17.4	40.1
+27 ² toe.		7.8	49.7

57.52

22

	125' N. = 175' S. maple		
-27 ² toe.		7.8	49.7
WL.		15.5	42.0
C		18.1	39.4
1/4		21.9	35.6
+2		24.0	33.5
£		25.3	32.2
1/4		20.0	37.5
C		13.5	44.0
EL. 45° up hill.		6.0	51.5
" " "	143' N. = 157' S. maple		
EL.		7.5	50.0
C		15.8	41.7
+6		19.5	38.0
+9		26.8	30.7
1/4		24.5	33.0
+4		21.5	36.0
£		20.7	36.8
1/4		17.6	39.9
C		12.0	45.5
WL		1.2	50.3
+24 ⁵ toe		7.3	50.2

57.52State St.

150' N. = 150' So. maple

- 29.3 = toe	7.4	50.1
WL	6.7	50.8
+5	7.1	50.4
C	8.9	48.6
1/4	15.4	42.1
E	20.4	37.1
1/4	21.5	36.0
+8	25.3	32.2
C	16.7	40.8
EL. 45° up hill	9.3	48.2

175' N. = 125' So. maple

- 14 ² = toe	1.3	56.2
EL	7.9	49.6
+2	9.3	48.2
+4	11.8	45.7
C	14.5	43.0
1/4	22.3	35.2
+7	24.4	33.1
E	22.2	35.3

57.52

23

1/4	13.5	44.0
C	6.6	50.9
WL	6.9	50.6
+8 = house	7.0	50.5

190' N. = 110' So. maple

- 8 house	7.0	50.5
WL	6.6	50.9
C	6.6	50.9
1/4	16.0	41.5
E	24.4	33.1
1/4	19.3	38.2

C	14.1	43.4
EL	9.5	48.0
+16 toe	3.4	54.1

200' N. = 100' So. maple

- 15 ² toe	5.7	51.8
EL	14.6	42.9
C	17.3	40.2
+5	21.0	36.5
1/4	22.0	35.5
+2	24.0	33.5

57.52

State St

£	236	33.9 ✓
+4	23.2	34.3 ✓
+5	18.3	39.2 ✓
1/4	13.7	43.8 ✓
+12	6.4	51.1 ✓
C	6.3	51.2 ✓
WL	6.4	51.1 ✓
+19 ⁰ toe.	6.3	51.2 ✓

Z16' N = 84' S. maple

-17 ⁸ toe.	6.2	51.3 ✓
WL	6.0	51.5 ✓
C	6.1	51.4 ✓
+11	6.6	50.9 ✓
1/4	7.9	49.6 ✓
£	136	43.9 ✓
1/4	17.3	40.2 ✓
C	20.0	37.5 ✓
EL	238	33.7 ✓
+6	236	33.9 ✓
+8	21.2	36.3 ✓
+20	16.9	40.6 ✓
+28 ⁵ toe.	13.5	44.0 ✓

57.52

Z25' N = 75' S. maple

24

-32 ² toe.	15.5	42.0 ✓
-26	19.3	38.2 ✓
-13	22.5	35.0 ✓
EL	17.7	39.8 ✓
C	14.4	43.1 ✓
1/4	13.3	44.2 ✓
£	9.7	47.8 ✓
+5	6.5	51.0 ✓
1/4	6.2	51.3 ✓
C	6.0	51.5 ✓
WL	5.9	51.6 ✓
+17 ⁸ toe.	6.0	51.5 ✓
TP. 5x. 6x.	5.56	51.76 ✓

6.71 58.67

Z44' N = 56' S. maple

-15 ⁶ toe.	6.5	52.2 ✓
WL	6.8	51.9 ✓
C	6.8	51.9 ✓
1/4	6.8	51.9 ✓
£	6.6	52.1 ✓

State St.

5867

F 1/4		6.4	52.3 ✓
C		6.4	52.3 ✓
EL.		6.9	51.8 ✓
+20		13.1	45.6 ✓
+25 [±] toe.		14.3	44.4 ✓
	250' N. 50' So. from maple		
-			
-	15 [±] toe.	8.1	50.6 ✓
EL.		6.2	52.5 ✓
C		6.2	52.5 ✓
1/4		6.3	52.4 ✓
£		6.4	52.3 ✓
1/4		6.7	52.0 ✓
C		6.7	52.0 ✓
WL		6.7	52.0 ✓
+14 [±] toe.		6.5	52.2 ✓
	275' N. = 25' So maple		
-11 [±] toe.		5.7	53.0 ✓
WL.		6.0	52.7 ✓
C		6.0	52.7 ✓

5867

25

1/4		6.0	52.7 ✓
£		5.8	52.9 ✓
1/4		5.5	53.2 ✓
C		5.3	53.4 ✓
EL		4.7	54.0 ✓
+9 [±] toe.		5.1	53.6 ✓
	Note street taps on intersection 300' N = S.L. Maple from N on SL to 77 [±] N.L. See photo photo.		
- 8 [±] toe		5.7	53.0 ✓
EL		5.2	53.5 ✓
C		5.3	53.4 ✓
1/4		5.0	53.7 ✓
£		5.1	53.6 ✓
1/4		5.2	53.5 ✓
C		5.1	53.6 ✓
WL.		5.2	53.5 ✓
+ 8 [±] toe		4.9	53.8 ✓
	S. Corb.		
+ 7.1 toe		4.6	54.1 ✓
WL.		4.8	53.9 ✓

State St.

5867

C		48	53.9	✓
1/4		50	53.7	✓
£		48	53.9	✓
1/4		52	53.5	✓
C		53	53.4	✓
EL		54	53.3	✓
+5 ³ toe		54	53.3	✓
	5/4			
EL		53	53.4	✓
C		51	53.6	✓
1/4		51	53.6	✓
£		45	54.2	✓
1/4		45	54.2	✓
C		43	54.4	✓
WL		40	54.7	✓
	£ Maple			
-3 ¹ toe		26	56.1	✓
WL		26	56.1	✓
C		35	55.2	✓
1/4		42	54.5	✓

26

5867

£		47	54.0	✓
1/4		50	53.7	✓
C		50	53.7	✓
EL		49	53.8	✓
+5 ¹ toe		50	53.7	✓
	N/4			
EL		47	54.0	✓
C		47	54.0	✓
1/4		47	54.0	✓
£		45	54.2	✓
1/4		42	54.5	✓
C		28	55.9	✓
WL		76	37.1	✓
	N. Curb			
WL		0.7	58.0	✓
+5		0.9	57.8	✓
C +7		2.8	55.9	✓
1/4		3.1	53.6	55.6
1/4		40	54.7	✓
£		40	54.7	✓
1/4		43	54.4	✓
C		46	54.1	✓
EL		47	54.0	✓

58.67

Reynard Way

N. L. Maple. = 30th of sec MP.

-A ² toe.		4.2	54.5	
EL		4.2	54.5	
C		4.4	54.3	
1/4		4.1	54.6	
±		3.8	54.9	
1/4		4.0	54.7	
+5		3.7	55.0	
+10		0.5	58.2	
C		0.1	58.6	
DM. Hub.	58.65	4.00	54.67	54.65
TP.		0.62	58.03	
	12.28	70.31		
WL on N. Maple		7.6	62.7	
TP.		0.39	69.72	
	11.58	81.30		
	Sec MP 30 th N of N.L. Maple.			
WL.		9.0	72.3	
C		15.4	65.7	
1/4		22.7	58.6	
+10		23.4	57.9	
+11		25.3	56.0	
±		25.9	55.4	

81.30

27

1/4		26.0	55.3	
C		25.9	55.4	
EL. Loc. cont.		26.0	55.3	
	Sec. M.O. = 29 th N. on WL. Same pt. EL = 65.9 ^{if Sec IL} " 65.85 E " 65.9 W			
EL		26.0	55.3	
C		25.9	55.4	
1/4		25.9	55.4	
± +3		25.6	55.7	
+5		23.6	57.7	
±		23.1	58.2	
+7		22.5	58.8	
+9		18.8	62.5	
1/4		17.0	64.3	
+7		13.8	67.5	
+8		11.2	70.1	
C		8.3	73.0	
WL.		2.6	78.7	

Reynard Way

81.30
80' Wide from this point North
10' Wks. - 15' 1/4s

Sec MN = 20° 48' N. of N.O. = 638' S. of I.L.

WL.	6.3	75.0
C	10.1	71.2
+6	15.3	66.0
1/4	18.5	62.8
+2	22.1	59.2
£	23.3	58.0
+5	23.4	57.9
+8	25.2	56.1
1/4	25.6	55.7
C	25.9	55.4
EL. Level	26.0	55.3
625' S. of I.L.		
EL. Level	26.0	55.3
C	26.0	55.3
1/4	25.1	56.2
+10	24.8	56.5
+13	23.0	58.3
£	22.8	58.5
1/4	21.3	60.0

Reynard Way
80' Wide
10' Wks.
15' 1/4s

28

81.30

+5	17.1	64.2
C	13.3	68.0
+5	8.5	72.8
WL.	7.0	74.3
600' S. of I.L.		
WL.	5.5	75.8
+2	6.1	75.2
+3	7.1	74.2
C	10.6	70.7
+7	13.5	67.8
+13	16.8	64.5
1/4	20.8	60.5
£	22.9	58.4
+4	22.5	58.8
+6	24.9	56.4
1/4	25.7	55.6
C	26.1	55.2
EL.	26.5	54.8
+3 - to	27.0	54.3

Reynard way

81.30

575' S. of I.L.

-22 ^o toe.	10.5	40.8	✓
-16	40.8	40.5	✓
-13	37.2	44.1	✓
EL	{ 33.9	47.4	✓
	{ 32.5	48.8	✓
C	26.9	54.4	✓
1/4	25.8	55.5	✓
+6	25.3	56.0	✓
+10	21.6	59.7	✓
£	21.7	59.6	✓
1/4	20.2	61.1	✓
+2	16.4	64.9	✓
C	9.6	71.7	✓
+5	6.2	75.1	✓
WL	3.1	78.2	✓
	550' S. of I.L.		
WL	3.9	77.4	✓
C	8.8	72.5	✓
+9	12.4	68.9	✓
1/4	19.6	61.7	✓
£	20.9	60.4	✓
+9	25.2	56.1	✓

81.30

29

1/4	25.5	55.8	✓
+10	25.9	55.4	✓
C	30.5	50.8	✓
EL	35.0	46.3	✓
+3	37.0	44.3	✓
+8	38.0	43.3	✓
+9	40.0	41.3	✓
+19	39.8	41.5	✓
+20 ⁵ toe	39.5	41.8	✓
	521 ⁵⁶ S. of I.L. (E.L. of Plate 8r.)		
-16 ^o toe	36.7	44.6	✓
-7	39.4	41.9	✓
EL	39.6	41.7	✓
+3	37.0	44.3	✓
C	32.3	49.0	✓
1/4	25.4	55.9	✓
+5	24.5	56.8	✓
+7	21.8	59.5	✓
£	18.3	63.0	✓
1/4	19.0	62.3	✓

Reynard Way

81.30

+4	18.4	62.9 ✓
+9	15.4	65.9 ✓
+10	12.8	68.5 ✓
C	9.3	72.0 ✓
WL.	4.8	76.5 ✓

515' S. of I.L.

WL.	4.5	76.8 ✓
C.	8.2	73.1 ✓
+2	12.0	69.3 ✓
+9	16.4	64.9 ✓
1/4	17.1	64.2 ✓
+5	17.3	64.0 ✓
+6	18.7	62.6 ✓
+12	18.7	62.6 ✓
+13	17.7	63.6 ✓
£	17.9	63.4 ✓
1/4	25.1	56.2 ✓
C	31.1	43.6 ✓
+2	39.2	42.1 ✓
EL	39.2	42.1 ✓
+11 I ¹ toe	34.0	47.3 ✓

81.30

500 S. of I.L.

00

-8 ⁵ toe	32.3	49.0 ✓
EL.	36.0	45.3 ✓
+3	37.0	44.3 ✓
+3 ^E	38.8	42.5 ✓
C	39.1	42.2 ✓
+6	38.3	43.0 ✓
1/4	28.2	53.1 ✓
£	18.8	62.5 ✓
+2	18.8	62.5 ✓
+3	19.8	61.5 ✓
+9	19.7	61.6 ✓
+11	16.3	65.0 ✓
1/4	16.1	65.2 ✓
+9	15.4	65.9 ✓
C	11.6	69.7 ✓
+1	9.8	71.5 ✓
WL.	3.2	78.1 ✓

81.30 Reynard Way

475' S of I.L.

WL	3.7	77.6
+2	4.9	76.4
+5	9.7	71.6
C	12.1	69.2
+3	14.0	67.3
+12	14.4	66.9
1/4	16.8	64.5
+8	21.3	60.0
£	21.4	59.9
1/4	30.2	51.1
+91	38.1	43.2
C	38.9	42.4
+6	{ 38.5	42.8
	{ 36.3	45.0
EL	36.0	45.3
+13 = toe	35.5	45.8

455' S of Sec I.L.

-10 ⁸ toe	34.3	47.0
EL	35.6	45.7
+1	38.0	43.3
C	38.8	42.5
+2	38.8	42.5

81.30

01

+A	36.0	45.3
+10	34.8	46.5
+12	32.2	49.1
1/4	30.8	50.5
£	23.0	58.3
+7	23.2	58.1
+12	19.3	62.0
1/4	14.3	67.0
C	13.3	68.0
+4	12.4	68.9
+8	5.4	75.9
WL	4.6	76.7
	450' S	
WL	5.0	76.3
TP	12.73	68.57

4.15 72.72

+4	3.9	68.8
C	4.4	68.3
1/4	5.3	67.4
+9	14.4	58.3

72.72

Reynard way

Φ	14.0	58.7	✓
1/4	21.9	50.8	✓
+1	25.2	47.5	✓
+12	26.6	46.1	✓
+13	28.9	43.8	✓
C	28.9	43.8	✓
EL	29.1	43.6	✓
+10° toe.	25.3	47.4	✓
425' S. of I.L.			
-16?	30.0	42.7	✓
-14	30.0	42.7	✓
EL	26.5	46.2	✓
C	26.3	46.4	✓
+3	23.3	49.4	✓
1/4	17.8	54.9	✓
+6	14.8	57.9	✓
Φ	16.0	56.7	✓
+5	16.3	56.4	✓
+8	7.5	65.2	✓
1/4	4.1	68.6	✓
C	3.5	69.2	✓
WL	3.3	69.4	✓

72.72

400' S. of Sec I.L.

02

WL	3.0	69.7	✓
C	3.3	69.4	✓
+7	4.2	68.5	✓
1/4	10.3	62.4	✓
+2	15.8	56.9	✓
+12	17.0	55.7	✓
Φ	18.8	53.9	✓
1/4	20.0	52.7	✓
+8	19.6	53.1	✓
+13	22.6	50.1	✓
C	25.0	47.7	✓
EL	26.0	46.7	✓
+11° toe.	26.7	46.0	✓
375' S. of I.L.			
-122 toe.	27.2	45.5	✓
-7	27.3	45.4	✓
EL	25.4	47.3	✓
C	25.5	47.2	✓
+8	24.8	47.9	✓
1/4	20.6	52.1	✓

72.72

£	19.3	53.4	✓
1/4	18.2	54.5	✓
C	7.0	65.7	✓
+3	29	69.8	✓
WL	2.6	70.1	✓

364²⁶ S. = SL. Natmeg. on WL.

WL	2.7	70.0	✓
+2	2.7	70.0	✓
C	9.9	62.8	✓
+5	16.0	56.7	✓
1/4	18.6	54.1	✓
£	19.3	53.4	✓
+10	19.8	52.9	✓
1/4	23.2	49.5	✓
+3	24.2	48.5	✓
C	25.6	47.1	✓
EL	26.0	46.7	✓
+9	27.5	45.2	✓
+10 ^s toe	27.0	45.7	✓

72.72

350's of IL.

08

- 11 ^o toe	27.3	45.4	✓
EL	25.7	47.0	✓
C	25.1	47.6	✓
1/4	24.8	47.9	✓
+9	20.1	52.6	✓
£	19.9	52.8	✓
1/4	18.6	54.1	✓
+10	16.4	56.3	✓
C	11.3	61.4	✓
WL	3.8	68.9	✓

330's of IL.

WL	7.0	65.7	✓
C	13.4	59.3	✓
+7	16.8	55.9	✓
+10	19.5	53.2	✓
1/4	20.0	52.7	✓
+6	19.1	53.6	✓
£	24.4	58.3	✓

7272

1/4	25.1	47.6	✓
C	24.0	48.7	✓
EL	24.2	48.5	✓
+9.9 toe	26.8	45.9	✓
TP	11.55	61.17	✓

474 65.91 ✓

315° S of IL - NL Inteq. on West.

WL	2.0	63.9	✓
C	8.6	57.3	✓
+6	9.9	56.0	✓
+10	14.6	51.3	✓
1/4	15.0	50.9	✓
+6	14.3	51.6	✓
±	17.6	48.3	✓
+12	17.5	48.4	✓
1/4	16.3	49.6	✓
C	17.7	48.2	✓
EL	18.2	47.7	✓
+7.3 toe	18.4	47.5	✓

65.91

300's of IL.

04

-6.2 toe	18.0	47.9	✓
EL	17.7	48.2	✓
C	17.6	48.3	✓
1/4	17.5	48.4	✓
±	17.1	48.8	✓
+8	17.0	48.9	✓
+11	15.5	50.4	✓
1/4	15.5	50.4	✓
+6	15.4	50.5	✓
C	9.6	56.3	✓
WL	3.8	62.1	✓

275's of IL.

WL	4.5	61.4	✓
C	11.9	54.0	✓
+6	16.0	49.9	✓
1/4	16.0	49.9	✓
±	16.6	49.3	✓
1/4	17.1	48.8	✓
C	16.1	49.8	✓
EL	17.2	48.7	✓
+6 toe	17.1	48.8	✓

6591

270's

- 5 ^s toe	17.0	48.9 ✓
EL.	17.1	48.8 ✓
C.	16.0	49.9 ✓
+10	15.8	50.1 ✓
1/4	16.0	49.9 ✓
£	16.6	49.3 ✓
1/4	16.1	49.8 ✓
+8	16.2	49.7 ✓
C.	12.2	53.7 ✓
WL.	6.5	59.4 ✓

250's

WL	3.8	62.1 ✓
C	9.1	56.8 ✓
+10	15.7	50.2 ✓
1/4	16.4	49.5 ✓
£	16.2	49.7 ✓
+10	16.2	49.7 ✓
1/4	14.6	51.3 ✓
C	15.2	50.7 ✓
EL	16.8	49.1 ✓
+5 ^s toe.	16.6	49.3 ✓

6591

225's

5

- 5 ^s toe.	16.0	49.9 ✓
EL.	15.9	50.0 ✓
C.	15.1	50.8 ✓
1/4	15.2	50.7 ✓
£	14.9	51.0 ✓
1/4	15.9	50.0 ✓
+5	15.9	50.0 ✓
C	8.7	57.2 ✓
WL.	1.7	64.2 ✓

200's

WL.	4.7	61.2 ✓
C	12.5	53.4 ✓
+4	15.0	50.9 ✓
1/4	13.7	52.2 ✓
£	13.7	52.2 ✓
1/4	14.6	51.3 ✓
C	16.1	49.8 ✓
EL	15.6	50.3 ✓
+ 5 ^s toe.	15.6	50.3 ✓

6591

195's

-5	15.5	50.4	✓
EL.	15.5	50.4	✓
C	15.5	50.4	✓
1/4	14.3	51.6	✓
£	13.7	52.2	✓
1/4	13.4	52.5	✓
+12	14.7	51.2	✓
C	13.0	52.9	✓
WL.	5.4	60.5	✓

186²⁴ S of IL = WL. Union on West.

WL.	9.2	56.7	✓
C	14.1	51.8	✓
1/4	13.9	52.0	✓
£	14.5	51.4	✓
1/4	14.6	51.3	✓
C	14.5	51.4	✓
EL.	14.6	51.3	✓
+5	14.6	51.3	✓

6591

170's

26

-5	13.9	52.0	✓
EL.	13.9	52.9	✓
C	14.3	51.6	✓
1/4	14.9	51.0	✓
£	14.1	51.8	✓
1/4	14.1	51.8	✓
C	13.8	52.1	✓
WL.	13.1	52.8	✓

150's

WL.	12.8	53.1	✓
C	13.3	52.6	✓
1/4	14.5	51.4	✓
£	14.2	51.7	✓
1/4	14.1	51.8	✓
C	14.1	51.8	✓
EL.	14.3	51.6	✓
+4 ⁵ fee.	14.4	51.5	✓

65.91

125's of I.L.

-5	13.7	52.2
EL	13.7	52.2
C	13.3	52.6
1/4	14.4	51.5
±	14.5	51.4
1/4	14.3	51.6
C	12.5	53.4
WL	12.3	53.6
+4	12.2	53.7

100's.

WL	10.7	55.2
C	11.4	54.5
+12	10.4	55.3
1/4	13.0	52.9
+4	15.4	50.5
±	15.9	50.0
+7	8.0	57.9
1/4	8.5	57.4
C	9.4	56.5
EL	10.6	55.3

65.91

85's.

37

EL	9.7	56.2
C	8.5	57.4
1/4	8.3	57.6
±	9.7	56.2
+12	8.5	57.4
1/4	10.6	55.3
C	10.9	55.0
WL	9.7	56.2

75's of I.L.

WL	8.3	57.6
C	9.6	56.3
+12	9.2	56.7
1/4	8.8	57.1
±	9.2	56.7
1/4	8.2	57.7
C	8.3	57.6
EL	9.5	56.4

67's.

EL	8.8	57.1
C	9.5	56.4
1/4	9.6	56.3

65.91

±	9.7	56.2 ✓
1/4	9.8	56.1 ✓
+9	9.0	56.9 ✓
C	3.5	62.4 ✓
T.P.	4.83	61.08 ✓

12.20

73.28

+4	6.0	67.3
WL	5.2	68.1

56.72 S. of I.L. = EL. - 11.00 on West

WL	5.4	67.9 ✓
+6	6.6	66.7 ✓
C	8.4	64.9 ✓
+6	17.2	56.1 ✓
1/4	17.3	56.0 ✓
±	18.0	55.3 ✓
1/4	18.1	55.2 ✓
C	17.7	55.6 ✓
EL	16.9	56.4 ✓

73.28

40'S. of I.L.

38

EL	18.5	54.8 ✓
C	17.0	54.3 ✓
1/4	18.4	54.9 ✓
±	18.3	55.0 ✓
1/4	18.0	55.3 ✓
C	18.5	54.8 ✓
+3	16.4	56.9 ✓
+8	6.6	66.7 ✓
WL	6.1	67.2 ✓

32'S. of I.L.

WL	18.0	55.3 ✓
C	18.0	55.3 ✓
1/4	18.3	55.0 ✓
±	18.2	55.1 ✓
1/4	18.4	54.9 ✓
C	18.8	54.5 ✓
EL	19.1	54.2 ✓

16'S.

-4.8' to	20.2	53.1 ✓
EL	20.2	53.1 ✓
C	19.2	54.1 ✓
1/4	18.5	54.8 ✓

73.28

£	18.3	55.0
1/4	18.0	55.3
C	17.5	55.8
WL	17.4	55.9

Sec I.L. = L. pt on WL - 15.35' L. ST = 10.25

WL	17.5	55.8
C	17.4	55.9
1/4	17.6	55.7
£	17.4	55.9
1/4	18.7	54.6
C	17.4	55.9
EL	15.3	58.0

Sec I.K = sample on W - 10.35' N of E = L. pt.

EL	13.9	59.4
C	16.2	57.1
1/4	18.0	55.3
£	17.5	55.8
1/4	18.2	55.1
C	17.0	56.3
WL	17.5	55.8

73.28

= 626' S. of E.H.

Sec I.J. = 10.95' N of East.

39

WL	17.5	55.8
C	17.0	56.3
1/4	17.3	56.0
£	16.6	56.7
1/4	15.8	57.5
C	14.5	58.8
EL	13.6	59.7

600' S. of L.H.

EL	12.6	60.7
C	13.9	59.4
1/4	16.0	57.3
£	16.2	57.1
1/4	16.2	57.1
C	16.2	57.1
WL	16.4	56.9

575' S. of E.H.

WL	16.4	56.9
C	16.4	56.9
1/4	16.2	57.1
£	16.8	56.5

7328

$\frac{1}{4}$	15.7	57.6 ✓
C	15.1	58.2 ✓
EL	13.2	60.1 ✓
561'S		
EL	12.8	60.5 ✓
C	15.3	58.0 ✓
$\frac{1}{4}$	16.8	56.5 ✓
±	15.5	57.8 ✓
$\frac{1}{4}$	16.7	56.6 ✓
C	16.8	56.5 ✓
WL	16.8	56.5 ✓
550'S		
WL	17.0	56.3 ✓
C	16.6	56.7 ✓
$\frac{1}{4}$	16.8	56.5 ✓
± ¹¹¹	16.5	56.8 ✓
	13.7	59.6 ✓
$\frac{1}{4}$	15.8	57.5 ✓
C	16.7	56.6 ✓
EL	16.2	57.7 ✓

7328

533'S

40

EL	11.8	61.5 ✓
+5	12.4	60.9 ✓
C	14.2	59.1 ✓
+8	15.1	58.2 ✓
$\frac{1}{4}$	12.1	61.2 ✓
+10	15.4	57.9 ✓
±	16.0	57.3 ✓
$\frac{1}{4}$	16.4	56.9 ✓
C	17.7	55.6 ✓
WL	18.2	55.1 ✓
525'S		
WL	18.4	54.9 ✓
C	18.2	55.1 ✓
$\frac{1}{4}$	16.7	56.6 ✓
±	15.7	57.6 ✓
$\frac{1}{4}$	12.7	60.6 ✓
C	11.9	61.4 ✓
EL	12.0	61.3 ✓

73.28

500'S.

EL	14.7	58.6 ✓
C	11.7	61.6 ✓
1/4	12.4	60.9 ✓
£	14.1	59.2 ✓
+6.	14.0	59.3 ✓
1/4	18.5	54.8 ✓
C	19.1	54.2 ✓
WL	19.1	54.2 ✓
+6 ³ toe	19.1	54.2 ✓

475'S.

-6 ⁸ toe	19.1	54.2 ✓
WL.	19.1	54.2 ✓
C	18.9	54.4 ✓
1/4	18.2	55.1 ✓
+6	17.4	55.9 ✓
£	15.1	58.2 ✓
+12	12.5	60.8 ✓
1/4	9.9	63.4 ✓
+10	10.4	62.9 ✓
C	12.7	60.6 ✓
EL.	14.0	59.3 ✓

73.28

450'S.

41

EL	13.6	59.7 ✓
C	11.8	61.5 ✓
1/4	10.9	62.4 ✓
£	7.5	65.8 ✓
+2	17.0	56.3 ✓
1/4	18.0	55.3 ✓
C	18.2	55.1 ✓
WL	18.4	54.9 ✓
+6 ¹ toe	18.4	54.9 ✓

435'S. - 52. Olive on West.

-3 ² toe	16.5	56.8 ✓
WL.	16.4	56.9 ✓
C	16.3	57.0 ✓
1/4	14.1	59.2 ✓
+6	12.8	60.5 ✓
+7	6.5	66.8 ✓
£	8.1	65.2 ✓
1/4	11.7	61.6 ✓
C	12.7	60.6 ✓
EL.	13.0	60.3 ✓

73.28

432'S.

EL.	130	60.3 ✓
C	126	60.7 ✓
1/4	117	61.6 ✓
⊕	85	64.8 ✓
1/4	59	67.4 ✓
C	44	68.9 ✓
WL.	30	70.3 ✓

406' S. = SL Olive on East.

WL.	29	70.4 ✓
C	42	69.1 ✓
1/4	52	68.1 ✓
⊕	73	66.0 ✓
1/4	117	61.6 ✓
C	124	60.9 ✓
EL.	128	60.5 ✓

382' S. = NL Olive on W.

EL.	129	60.4 ✓
C	123	61.0 ✓
1/4	115	61.8 ✓
+8	113	62.0 ✓

73.28

42

⊕	93	64.0 ✓
1/4	63	67.0 ✓
C	44	68.9 ✓
WL.	32	70.1 ✓

350'S.

WL.	32	70.1 ✓
C	47	68.6 ✓
1/4	71	66.2 ✓
⊕	105	62.8 ✓
1/4	112	62.1 ✓
C	126	61.3 ✓
+3	143	59.0 ✓
+7	125	60.8 ✓
EL.	127	60.6 ✓

325'S.

EL.	114	61.9 ✓
C	125	60.8 ✓
+7	142	59.1 ✓
1/4	123	61.0 ✓
⊕	94	63.9 ✓

73.28

+7	9.1	64.2 ✓
1/4	6.1	67.2 ✓
C	4.2	69.1 ✓
WL	3.0	70.3 ✓
TP	4.77	68.51 ✓

12.78 81.29 ✓

300's

WL	10.7	70.6 ✓
C	11.6	69.7 ✓
+11	12.9	68.4 ✓
1/4	15.2	66.1 ✓
⊖	17.6	63.7 ✓
+10	19.8	61.5 ✓
+12	21.5	59.8 ✓
1/4	21.7	59.6 ✓
+2	19.8	61.5 ✓
C	18.8	62.5 ✓
EL	17.8	63.5 ✓

275's

EL	13.5	67.8 ✓
+5	16.8	64.5 ✓
C	17.1	64.2 ✓
1/4	19.4	62.2 ✓

81.29

00

+8	19.7	61.6 ✓
+10	21.5	59.8 ✓
+13	21.4	59.9 ✓
⊖	19.7	61.6 ✓

+4 19.2 62.1 ✓

1/4 13.6 67.7 ✓

C 11.6 69.7 ✓

WL 9.9 71.4 ✓

250's

WL 9.8 71.5 ✓

+7 10.8 70.5 ✓

C 14.1 67.2 ✓

+10 14.0 67.3 ✓

1/4 18.1 63.2 ✓

+6 19.4 61.9 ✓

+10 21.4 59.9 ✓

⊖ 19.3 62.0 ✓

1/4 17.0 64.3 ✓

C 14.9 66.4 ✓

EL 9.2 72.1 ✓

81.29

235²³ S. = WL Horton on West

EL	64	74.9✓
C	146	66.7✓
1/4	173	64.0✓
E	189	62.4✓
+4	194	61.9✓
+8	210	60.3✓
+12	192	62.1✓
1/4	190	62.3✓
+6	183	63.0✓
+9	153	66.0✓
C	153	66.0✓
+4	150	66.3✓
+7	106	70.7✓
WL	100	71.3✓

218¹⁷ S = EL Horton on East

WL	12.1	69.2✓
+3	12.5	68.8✓
+5	14.8	66.5✓
C	15.7	65.6✓
+8	15.5	65.8✓

81.29

04

1/4	208	60.5✓
E	180	63.3✓
1/4	165	64.8✓
+6	155	65.8✓
C	111	70.2✓
EL	4.5	76.8✓

200'S.

EL	06	80.7✓
C	8.7	72.6✓
1/4	160	65.3✓
E	184	62.9✓
1/4	180	63.3✓
C	161	65.2✓
WL	14.1	67.2✓

175' # South

WL	14.3	67.0✓
C	15.9	65.4✓
1/4	170	64.3✓
E	188	62.5✓
+6	183	63.0✓

81-29

+9	16.1	65.2✓
1/4	15.6	65.7✓
curb.	5.5	75.8✓

150's.

E Curb.	5.2	76.1✓
1/4	18.0	63.3✓
£	17.6	63.7✓
1/4	16.9	64.4✓
C	15.2	66.1✓
WL	13.2	68.1✓

125's.

WL	14.9	66.4✓
C	15.6	65.7✓
1/4	16.2	65.1✓
£	17.3	64.0✓
1/4	17.5	63.8✓
Curb.	4.8	76.5✓

81-29

108²⁹ S = E.L. Horton on West

45

E. Curb.	4.0	77.3✓
1/4	13.9	67.4✓
+5	17.0	64.3✓
£	17.0	64.3✓
1/4	16.0	65.3✓
C	15.7	65.6✓
WL	14.6	66.7✓

100's.

WL	15.1	66.2✓
C	16.2	65.1✓
1/4	15.9	65.4✓
£	17.1	64.2✓
+6	16.6	64.7✓
1/4	12.7	68.6✓
E curb.	3.6	77.7✓

75's.

E curb.	3.5	77.8✓
1/4	11.9	69.4✓
£	16.2	65.1✓
1/4	16.0	65.3✓

81.29

C	154	65.9 [✓]
WL	144	66.9 [✓]
50' S.		
WL	140	67.3 [✓]
C	148	66.5 [✓]
1/4	164	64.9 [✓]
10	157	65.6 [✓]
±	146	66.7 [✓]
1/4	104	70.9 [✓]
AA	93	72.0 [✓]
32 ⁸⁸ South of EH = S.L. D.M. both sides.		
10' W. of East Curb.	81	73.2 [✓]
1/4	92	72.1 [✓]
±	128	68.5 [✓]
1/4	148	66.5 [✓]
C	168	64.5 [✓]
WL	144	66.9 [✓]

81.29

Sec E.H. = 2 pt on W. 20' 11' L. ST = 14.24 ⁰⁸

WL	141	67.2 [✓]
C	168	64.5 [✓]
1/4	136	67.7 [✓]
±	97	71.6 [✓]
1/4	63	75.0 [✓]
T.P.	268	78.6 [✓]
1055 89.16 [✓]		
C	105	78.7 [✓]
EL	05	88.7 [✓]
32 ⁸⁸ S. of EH		
EL	20	87.2 [✓]
E Curb	101	79.1 [✓]
50' S. of EH		
E curb	103	78.9 [✓]
EL	25	86.7 [✓]
75' S. of EH		
EL	35	85.7 [✓]
100' S. of EH		
EL	42	85.0 [✓]

89.16

108 3/3 of EH.

EL. 4.3 84.9✓

125' S. of EH.

EL. 5.1 84.1✓

150' S. of EH.

EL. 5A 83.8✓

175' S. of EH.

EL. 5.9 83.3✓

TP. 10.55 78.61✓

12.77

91.38 ✓

Sec EG = 14.24 N. on EL.

EL. 1.88 89.50✓

C 9.2 82.2✓

1/4 13.9 77.5✓

1/2 17.7 73.7✓

1/4 22.1 69.3✓

C 26.5 64.9✓

+5 26.5 64.9✓

WL. 24.9 66.5✓

91.38

391.16
Sec. E.F. = 14.24 N. on E. = 317.165 of Sec. D. 87

WL. 24.9 66.5✓

+6 26.5 64.9✓

C 26.8 64.6✓

1/4 23.0 68.4✓

1/2 18.3 73.1✓

1/4 13.1 78.3✓

C 8.0 83.4✓

EL. 4.3 87.1✓

383.57 S. of AD.

EL. 3.7 87.7✓

C 6.9 84.5✓

1/4 12.8 78.6✓

1/2 17.9 73.5✓

+7 20.3 71.1✓

+9 25.5 65.9✓

1/4 26.5 64.9✓

C 26.5 64.9✓

WL. 24.4 67.0✓

91.38

375'S. of A.D.

WL	23.6	67.8✓
C	24.4	67.0✓
1/4	25.7	65.7✓
£	26.0	65.4✓
+2	17.5	73.9✓
1/4	12.5	78.9✓
C	6.8	84.6✓
EL	2.2	89.2✓

350'S. of A.D.

EL	5.4	86.0✓
C	10.0	81.4✓
+5	12.2	79.2✓
1/4	18.3	73.1✓
+12	26.0	65.4✓
£	26.0	65.4✓
1/4	24.0	67.4✓
C	22.8	68.6✓
WL	23.5	67.9✓

91.38

325'S. of A.D.

08

WL	22.1	69.3✓
C	22.6	68.8✓
1/4	23.3	68.1✓
+6	24.0	67.4✓
+13	26.5	64.9✓
£	25.2	66.2✓
1/4	22.9	68.5✓
C	17.2	74.2✓
EL	12.0	79.4✓
T.P.	12.93	78.45✓

4.76 83.21✓

300'S.

EL	7.8	75.4✓
C	10.4	72.8✓
1/4	13.0	70.2✓
£	14.6	68.6✓
+10	15.7	67.5✓
1/4	18.0	65.2✓
+4	16.2	67.0✓
C	14.0	69.2✓
WL	14.4	68.8✓

83.21

275' S

+3	17.0	66.2✓
WL	17.2	66.0✓
+6	17.6	65.6✓
C	15.2	68.0✓
1/4	13.9	69.3✓
£	13.2	70.0✓
1/4	10.4	72.8✓
C	7.2	76.0✓
EL	5.3	77.9✓

250' S

EL	4.5	78.7✓
C	5.9	77.3✓
1/4	9.6	73.6✓
£	11.8	71.4✓
1/4	12.7	70.5✓
C	14.1	69.1✓
WL	14.8	68.4✓
+4	14.9	68.3✓

233⁵⁹ S

WL	13.1	70.1✓
C	12.9	70.3✓

83.21

49

1/4	120	71.2✓
£	11.2	72.0✓
1/4	100	73.2✓
C	68	76.4✓
EL	4.5	78.7✓

225' S

EL	4.5	78.7✓
H	6.3	76.9 77.0

C	8.6	74.6✓
+13	100	73.2✓
1/4	9.6	73.6✓
£	11.0	72.2✓
1/4	11.8	71.4✓
C	12.8	70.4✓
WL	13.0	70.2✓

220' S

WL	13.2	70.0✓
C	12.8	70.4✓
1/4	11.6	71.6✓
£	10.5	72.9✓

83.21

WL

1/4	9.8	73.4✓
C	7.4	75.8✓
EL	6.8	76.4✓

218'S.

EL	4.6	78.6✓	
C	6.1	77.1✓	
+2	6.3	76.9✓	
+4	8.7	74.5✓	
1/4	9.3	73.9✓	
±	10.4	72.8✓	
1/4	11.4	71.8✓	
C	13.0	70.2✓	
+9	13.5	69.7✓	
WL	15.4	67.8✓	
+5 ² toe	15.6	67.6✓	
↓ - 2 ⁸ toe	200'S.	13.5	69.7✓
WL	15.2	68.0✓	
C	15.5	67.7✓	
1/4	11.3	71.9✓	
±	8.6	74.6✓	

83.21

50

1/4	6.3	76.9✓
C	4.9	78.3✓
EL	4.3	78.9✓

193'S.

EL	4.0	79.2✓
C	5.0	78.2✓
1/4	6.5	76.7✓
±	9.1	74.1✓
+9	10.4	72.9 ^{72.8}
+12	15.2	68.0✓
1/4	15.5	67.7✓
C	15.0	68.2✓
+6	14.8	68.4✓
WL	12.6	70.6✓

175'S.

WL	11.2	72.0✓
C	11.7	71.5✓
+3	13.5	69.7✓
1/4	12.3	70.9✓
±	14.2	69.0✓
+3	15.6	67.6✓

83.21

+6	13.9	69.3✓
1/4	11.3	71.9✓
c	8.3	74.9✓
EL	6.3	76.9✓

150's

EL	10.6	72.6✓
c	12.0	71.2✓
+3	13.4	69.9 ^{69.8}
+11	15.1	68.1✓
1/4	12.6	70.6✓
±	10.9	72.3✓
+10	12.9	70.3✓
1/4	11.7	71.5✓
+6	10.5	72.7✓
c	10.5	72.7✓

133's

WL	10.2	73.0✓
WL	9.0	74.2✓
c	9.2	74.0✓
1/4	9.9	73.3✓

83.21

51

±	11.2	72.0✓
1/4	10.5	72.7✓
c	11.8	71.4✓
+1	15.2	68.0✓
EL	14.2	69.0✓

+6's toe

14.2 69.0✓

125's

EL	11.1	72.1✓
c	10.4	72.8✓
1/4	9.9	73.3✓
±	10.6	72.6✓
1/4	8.7	74.5✓
c	8.3	74.9✓
WL	7.9	75.3✓

100's

WL	3.2	80.0✓
c	4.1	79.1✓
1/4	5.9	77.5✓
±	8.1	75.1✓
1/4	9.4	73.8✓

83.21

C		9.0	74.2✓
EL		9.0	74.2✓
	75'S.		
EL		7.8	75.4✓
C		8.1	75.1✓
1/4		8.0	75.2✓
⊕		5.9	77.3✓
1/4		3.8	79.4✓
C		1.8	81.4✓
WL		0.5	82.7✓
T.P.		1.07	82.14✓
	9.05	91.19✓	
		50' S of A.D.	
WL		6.0	85.2✓
C		7.8	83.4✓
1/4		10.1	81.1✓
⊕		12.6	78.6✓
1/4		14.9	76.3✓
C		15.4	75.8✓
EL		15.4	75.8✓

91.19

25'S.

52

EL		15.0	76.2✓
C		14.6	76.6✓
1/4		12.8	78.4✓
⊕		11.1	80.1✓
1/4		8.6	82.6✓
C		5.4	85.8✓
WL		3.3	87.9✓
		7 ¹² S of A.D. = P.C.	
WL		2.3	88.9✓
C		4.8	86.4✓
1/4		8.2	83.0✓
⊕		10.4	80.8✓
1/4		11.6	79.6✓
C		14.3	76.9✓
EL		14.9	76.3✓
		Sec A.D.	
EL		15.0	76.2✓
C		14.2	77.0✓
1/4		11.1	80.1✓
⊕		9.6	81.6✓

91.19

57

1/4	81	83.1✓
C	4.5	86.7✓
WL	2.1	89.1✓
	= 1424 N of A.D. if produced to P.L. on W.	
	Sec AC thru Lpt = E Curve path sides.	
WL.	2.57	88.62✓
C	4.8	86.4✓
1/4	7.8	83.4✓
E	9.5	81.7✓
1/4	11.3	79.9✓
C	14.5	76.7✓
EL	15.4	75.8✓
	Sec A-B = 1424 N of WL = 743 rd S. of UX.	
EL.	15.4	75.8✓
C	14.5	76.7✓
1/4	11.0	80.2✓
E	9.3	81.9✓
1/4	7.4	83.8✓
C	4.5	86.7✓
WL.	2.8	88.4✓

91.19

58

736.42 S. of O.X = P.C.

WL	2.9	88.3✓
C	4.9	86.3✓
1/4	7.4	83.8✓
E	9.2	82.0✓
1/4	11.3	79.9✓
+5	13.6	77.6✓
C	14.4	76.8✓
EL	14.9	76.3✓
	710 th S. of UX = NL Quince.	
EL	15.1	76.1✓
C	14.1	77.1✓
1/4	13.0	78.2✓
E	10.8	80.4✓
1/4	8.6	82.6✓
C	5.7	85.5✓
WL	3.2	88.0✓
	700's	
WL	3.6	87.6✓
C	6.1	85.1✓
1/4	9.3	81.9✓

91.19

£	11.3	79.9✓
1/4	13.3	77.9✓
C	14.0	77.2✓
EL.	14.8	76.4✓

675's.

EL.	14.1	77.1✓
C	13.7	77.5✓
1/4	13.3	77.9✓
£	12.1	79.1✓
1/4	8.5	82.7✓
C	5.6	85.6✓
WL.	4.1	87.1✓

650's

WL	5.3	85.9✓
C	6.9	84.3✓
1/4	9.6	81.6✓
£	11.8	79.4✓
+8	13.5	77.7✓
1/4	14.2	77.0✓
C	13.7	77.5✓
EL.	14.5	76.7✓

91.19

625's.

54

EL.	13.1	78.1✓
C	13.8	77.4✓
1/4	13.3	77.9✓
£	13.1	78.1✓
+5	12.9	78.3✓
+6	11.4	79.8✓
1/4	10.1	81.1✓
C	8.5	82.7✓
WL.	6.9	84.3✓
T.P. = Keel Rock near E. point	12.61	78.58✓

12.39 90.97✓

600's. of U.X.

EL.	9.1	81.9✓
+7	10.3	80.7✓
C	11.7	79.3✓
1/4	12.9	78.1✓
£	13.3	77.7✓
1/4	14.0	77.0✓
C	11.2	79.8✓
WL.	10.7	80.3✓

90.97

575's

WL	124	78.6✓
+6	13.8	77.2✓
C	12.9	78.1✓
1/4	12.5	78.5✓
£	13.0	78.0✓
1/4	10.3	80.7✓
C	9.4	81.6✓
EL	7.7	83.3✓

565's

EL	7.5	83.5✓
C	8.9	82.1✓
1/4	10.0	81.0✓
+5	10.1	80.9✓
+7	11.8	79.2✓
£	12.2	78.8✓
+8	13.6	77.4✓
1/4	12.7	78.3✓
+3	11.1	79.9✓
C	11.6	79.4✓
WL	13.9	77.1✓

90.97

550's

55

WL	11.5	79.5✓
C	10.8	80.2✓
+9	11.0	80.0✓
1/4	13.3	77.7✓
+7	11.0	80.0✓
£	11.0	80.0✓
+7	11.2	79.8✓
1/4	8.8	82.2✓
C	8.4	82.6✓
EL	7.8	83.2✓

525's

EL	4.6	86.4✓
C	6.5	84.5✓
1/4	8.1	82.9✓
£	9.3	81.7✓
+10	10.3	80.7✓
1/4	12.9	78.1✓
+6	10.5	80.5✓
C	10.4	80.6✓
WL	10.4	80.6✓

90.97

500's

WL.	9.3	81.7✓
C	9.5	81.5✓
+7	9.7	81.3✓
+10	12.0	79.0✓
1/4	11.4	79.6✓
+4	9.8	81.2✓
±	8.3	82.7✓
1/4	6.3	84.7✓
+11	5.6	85.4✓
+12	3.8	87.2✓
C	3.0	88.0✓
EL.	1.4	89.6✓

480's

EL.	+0.5	91.5✓
+2	+0.2	91.2✓
+4	3.6	87.4✓
C	6.4	84.6✓
1/4	6.6	84.4✓
±	7.4	83.6✓
+10	8.9	82.2✓

90.97

56

1/4	10.8	80.2✓
+4	10.8	80.2✓
+5	8.8	82.2✓
C	8.3	82.7✓
WL.	8.6	82.4✓

475's. of 0. X

WL.	8.4	82.6✓
C	8.2	82.8✓
+9	8.4	82.6✓
+11	10.4	80.6✓
1/4	10.6	80.4✓
+5	8.6	82.4✓
±	7.3	83.7✓
1/4	6.9	84.1✓
C	6.8	84.2✓
EL.	4.8	86.2✓

463's

EL.	6.3	84.7✓
C	7.1	83.9✓
1/4	7.1	83.9✓

90.97

£	66	844 ✓
+5	75	835 ✓
+11	100	810 ✓
1/4	104	806 ✓
+3	101	809 ✓
+4	81	829 ✓
C	79	831 ✓
WL	82	828 ✓

450'S.

WL	84	826 ✓
C	77	833 ✓
+13	76	834 ✓
1/4	101	809 ✓
+9	83	827 ✓
+11	70	840 ✓
£	68	842 ✓
1/4	72	838 ✓
C	69	841 ✓
EL	64	846 ✓

90.97

425'S.

57

EL	53	857 ✓
C	66	844 ✓
1/4	77	833 ✓
£	76	834 ✓
1/4	75	835 ✓
C	82	828 ✓
WL	88	822 ✓

409⁰⁶S = 51. Redwood

WL	84	826 ✓
C	82	828 ✓
1/4	95	815 ✓
£	83	827 ✓
1/4	75	835 ✓
C	59	851 ✓
EL	54	856 ✓

400'S.

EL	54	856 ✓
C	65	845 ✓
1/4	78	832 ✓

90.97

£	7.8	832✓
¼	8.2	828✓
C	8.8	822✓
WL	8.7	823✓

395' S. of Ux.

WL	10.5	805✓
C	9.5	815✓
¼	8.0	830✓
£	7.7	833✓
¼	7.5	835✓
C	6.9	841✓
EL	5.4	856✓

385' S.

EL	5.3	857✓
C	6.6	844✓
¼	7.0	840✓
£	7.8	832✓
¼	7.0	840✓
£	6.7	843✓
WL	6.1	849✓

90.97

375' S. of Ux.

58

WL	5.9	851✓
C	5.8	852✓
¼	6.1	849✓
£	7.3	837✓
¼	6.8	842✓
C	6.6	844✓
EL	5.9	851✓

367' S.

EL	6.0	850✓
C	6.6	844✓
¼	6.4	846✓
£	6.4	846✓
¼	5.1	859✓
C	4.6	864✓
WL	4.3	867✓

350' S.

WL	3.9	871✓
C	4.1	869✓
¼	4.6	864✓

90.97

£	54	856✓
1/4	66	844✓
C	66	844✓
EL.	58	852✓
	329 ⁰⁰ S. = N.L Redwood.	
EL.	{6.4	846✓
	{7.3	837✓
+5.	7.8	832✓
+6	6.2	848✓
C	5.8	852✓
1/4	5.8	852✓
£	4.0	870✓
1/4	3.8	872✓
C	3.2	878✓
WL.	3.0	88.0✓
	309 S of O X.	
WL.	1.4	896✓
C	2.2	888✓
1/4	2.9	881✓
£	3.1	879✓
1/4	4.3	867✓

90.97

59

C	5.1	859✓
EL	{5.8	852✓
	{7.1	839✓
	300 S. of O X.	
EL.	5.6	854✓
C	5.2	858✓
1/4	3.9	871✓
£	3.0	880✓
1/4	2.6	884✓
C	1.7	893✓
WL.	1.1	89.9✓
T.P.	1.86	89.11✓
	939 98 50	
	275 S.	
WL.	7.4	81.1✓
C	7.7	90.8✓
1/4	9.0	89.5✓
£	9.6	88.9✓
1/4	10.3	88.2✓
C	12.2	86.3✓
EL.	12.2	86.3✓

98.50

250's of UX

# EL	11.7	86.8✓
C	11.0	87.5✓
1/4	9.1	89.4✓
E	8.2	90.3✓
1/4	7.8	90.7✓
C	6.8	91.7✓
WL	6.7	91.8✓

225's

WL	5.9	92.6✓
C	6.2	92.3✓
1/4	7.0	91.5✓
E	7.1	91.4✓
1/4	7.8	90.7✓
C	10.3	88.2✓
EL	11.4	87.1✓

200's

EL	11.3	87.2✓
C	8.8	89.7✓
1/4	6.8	91.7✓
E	6.2	92.3✓

98.50

60

1/4	6.3	92.2✓
C	5.2	93.3✓
WL	4.9	93.6✓

175's

WL	4.6	93.9✓
C	5.2	93.3✓
1/4	6.3	92.2✓
E	7.0	91.5✓

1/4	7.2	91.3✓
C	9.6	88.9✓
EL	10.8	87.7✓

150's

EL	11.2	87.3✓
C	10.0	88.5✓
1/4	9.8	88.7✓
E	9.4	89.1✓
1/4	7.1	89.4✓
C	7.7	90.8✓
WL	6.0	92.5✓

98.50

147's.

WL.	59	92.6✓
C	79	90.6✓
1/4	9.1	89.4✓
£	9.3	89.2✓
1/4	10.0	88.5✓
C	10.5	88.0✓
EL.	12.6	85.9✓
+3	12.6	85.9✓
+L.	10.6	87.9✓

125's.

EL.	10.5	88.0✓
+4	11.2	87.3✓
+L	12.2	86.3✓
+8	11.1	87.4✓
C	10.4	88.1✓
1/4	10.2	88.3✓
£	9.7	88.8✓
1/4	10.1	88.4✓
C	8.8	89.7✓
WL.	7.4	91.1✓

98.50

100's.

61

WL.	7.6	90.9✓
C	9.6	88.9✓
1/4	9.1	89.4✓
£	8.5	90.0✓
1/4	8.8	89.7✓
C	8.6	89.9✓
+4	9.2	89.3✓
+8	11.4	87.1✓
EL.	11.8	86.7✓

90's. of UX.

EL.	11.5	87.0✓
+4	9.1	89.4✓
C	8.0	90.5✓
1/4	8.4	90.1✓
£	8.3	90.2✓
1/4	8.6	89.9✓
C	9.6	88.9✓
WL.	7.5	91.0✓

98.50

75'S.

WL.	66	919	✓
C	9.1	89.4	✓
1/4	8.3	90.2	✓
£	7.9	90.6	✓
1/4	7.9	90.6	✓
C	8.1	90.4	✓
EL.	8.2	90.3	✓

50'S.

EL.	7.1	91.4	✓
C	6.8	91.7	✓
1/4	6.7	91.8	✓
£	7.1	91.4	✓
1/4	8.1	90.4	✓
#12	8.9	89.6	✓
C	7.8	90.7	✓
WL.	5.5	93.5	✓

29'S. S.L. Spruce

WL.	4.4	94.1	✓
C	6.3	92.2	✓
TL	8.2	90.3	✓

98.50

62

1/4	8.5	90.0	✓
£	7.3	91.2	✓
1/4	6.7	91.8	✓
C	6.6	91.9	✓
EL.	6.7	91.8	✓

10'S. of OX = PC.

EL.	6.4	92.1	✓
C	6.3	92.2	✓
1/4	7.2	91.3	✓
£	7.8	90.7	✓
+10	7.9	90.6	✓
1/4	6.3	92.2	✓
C	4.3	94.2	✓
WL.	3.2	95.3	✓
		95.2	✓

500 O.X.

WL.	2.8	95.7	✓
C	3.5	95.0	✓
1/4	5.2	93.3	✓
£	7.2	91.3	✓
1/4	7.2	91.3	✓

98.50

80 #			
C	7.2	91.3	
EL	6.7	91.8	
T.P. Hub. L pt. E side U.X.	6.75	91.75	
10.36	102.11		
Sec UV = E Curve.			
EL	10.4	91.7	
C	11.0	91.1	
1/4	10.6	91.5	
E	10.0	92.1	
1/4	8.4	93.7	
C	6.9	95.2	
WL	5.7	96.4	
Sec UV = 423 ⁹⁸ S. of QT.			
WL	5.7	96.4	
C	7.0	95.1	
1/4	8.2	93.9	
E	9.6	92.5	
1/4	10.0	91.5	
C	11.2	90.9	
EL	10.4	91.7	

102.11

413.045 = Pt. Tang.

63

EL	10.9	91.2	
C	9.9	92.2	
1/4	9.8	92.3	
E	9.2	92.9	
1/4	8.1	94.0	
C	6.9	95.2	
WL	5.3	96.9	
411 ³⁰ S = NL Spruce on EL.			
WL	5.3	96.8	
C	6.9	95.2	
1/4	8.2	93.9	
E	9.2	92.9	
1/4	9.6	92.5	
C	9.8	92.3	
EL	10.7	91.4	
400' S. of QT.			
EL	9.2	92.9	
C	9.1	93.0	
1/4	8.9	93.2	
E	8.6	93.5	

102.11

1/4	7.8	94.3✓
C	6.3	95.8✓
WL	4.8	97.3✓
375'S.		
WL	4.6	97.5✓
C	5.8	96.3✓
1/4	7.3	94.8✓ 94.9
£	8.3	93.8✓
1/4	8.2	93.9✓
C	8.4	93.7✓
EL	8.5	93.6✓
366'S.		
EL	9.8	92.3✓
C	8.5	93.6✓
1/4	8.2	93.9✓
£	7.7	94.4✓
1/4	7.2	94.9✓
C	6.2	95.9✓
WL	4.7	97.4✓

102.11

354'S.

64

WL	4.9	97.2✓
C	6.3	95.8✓
1/4	7.0	95.1✓
£	7.7	94.4✓
1/4	8.1	94.0✓
C	8.8	93.3✓
+3	9.5	92.6✓
+5	11.8	90.3✓
EL	12.2	89.9✓
352' B of QT.		
EL	9.3	92.8✓
+2	12.3	89.8✓
+5	11.9	90.2✓
+6	10.5	91.6✓
C	9.1	93.0✓
1/4	8.1	94.0✓
£	7.7	94.4✓
1/4	6.9	95.2✓
C	6.3	95.8✓
WL	5.0	97.1✓

102.11

350'S of QT.

WL	5.1	97.0✓
C	6.2	95.9✓
1/4	6.8	95.3✓
£	7.7	94.4✓
1/4	7.9	94.2✓
C	9.8	92.3✓
+1	12.0	90.1✓
+6	12.2	89.9✓
+7	9.3	92.8✓
EL	8.8	93.3✓

335'S of QT.

EL	7.3	94.8✓
C	8.0	94.1✓
1/4	9.3	92.8✓
+2	11.5	90.6✓
+8	11.5	90.6✓
+9	9.8	92.3✓
£	8.0	94.1✓
1/4	6.9	95.2✓
C	5.7	96.4✓
WL	4.8	97.3✓

102.11

325'S.

65

WL	5.6	96.5✓
C	6.1	96.0✓
1/4	7.6	94.5✓
+12	8.2	93.9✓
+13	11.2	90.9✓
£	11.5	90.6✓
+2	11.5	90.6✓
+3	9.1	93.0✓
1/4	7.9	94.2✓
C	6.8	95.3✓
EL	6.7	95.4✓

300'S.

EL	5.3	96.8✓
C	5.9	96.2✓
1/4	6.2	95.9✓
£	6.9	95.2✓
+10	8.0	94.1✓
+12	10.1	92.0✓
1/4	10.4	91.7✓
+2	8.6	93.5✓

102.11

C	6.1	96.0 ✓
WL	6.0	96.1 ✓
	282 ³² = DC. of EL	
WL	6.2	95.9 ✓
C	6.9	95.2 ✓
+4	7.6	^{94.5} 94.6
+7	9.8	92.3 ✓
+13	7.2	94.9 ✓
1/4	6.7	95.4 ✓
⊖	6.2	95.9 ✓
1/4	5.6	96.5 ✓
C	5.2	96.9 ✓
EL	4.9	97.2 ✓
	275' S.	
EL	4.5	97.6 ✓
C	4.6	97.5 ✓
1/4	5.4	96.7 ✓
⊖	5.6	96.5 ✓
1/4	6.5	95.6 ✓
+6	7.6	94.5 ✓

102.11

86

+10	9.7	92.4 ✓
C	7.5	94.6 ✓
WL	6.2	95.9 ✓
	253' S. of AT AT.	
WL	6.9	95.2 ✓
+1	9.1	93.0 ✓
+5	9.2	92.9 ✓
+6	7.3	94.8 ✓
Curb	6.6	95.5 ✓
1/4	5.6	96.5 ✓
⊖	4.7	97.4 ✓
1/4	4.6	97.5 ✓
C	4.3	97.8 ✓
EL	4.3	97.8 ✓
	250' S.	
EL	4.1	98.0 ✓
C	4.3	97.8 ✓
1/4	4.5	97.6 ✓
⊖	4.6	97.5 ✓
1/4	5.5	96.6 ✓

102-11

100 C	59	96.2✓
+5	72	94.9✓
WL	92	92.9✓
+5	59	96.2✓

243'S of QT.

WL	70	95.1✓
C	53	96.8✓
1/4	52	96.9✓
⊖	47	97.4✓
1/4	43	97.8✓
C	42	97.9✓
EL	38	98.3✓

225'S

EL	0.1	102.0✓
+7	34	98.7✓
C	36	98.5✓
1/4	40	98.1✓
⊖	42	97.9✓
1/4	44	97.7✓
C	48	97.3✓
WL	60	96.1✓

102-11

200'S

67

WL	47	97.4✓
C	42	97.9✓
1/4	42	97.9✓
⊖	38	98.3✓
1/4	39	98.2✓
+2	38	98.3✓
+5	1.6	100.5✓
TR	135	100.76✓

10.11 - 110.87

C	8.2	102.7✓
EL	52	105.7✓

185'S of QT.

EL	3.9	107.0✓
C	6.8	104.1✓
+13	10.3	100.6✓
1/4	12.2	98.7✓
⊖	12.4	98.5✓
1/4	12.8	98.1✓
C	12.8	98.1✓
WL	13.2	97.7✓

110.87

175's. of QT.

WL.	130	97.9✓
c	126	98.3✓
1/4	127	98.2✓
±	123	98.6✓
1/4 ⁺¹³	123	98.6✓
	110	99.9✓
+10	88	102.1✓
c	69	104.0✓
EL.	47	106.2✓

148⁸³'s. of QT. = 5 L. Eagle in cut

EL.	65	104.4✓
c	71	103.8✓
+5	93	101.6✓
1/4	97	101.2✓
+2	117	99.2✓
±	118	99.1✓
1/4	119	99.0✓
c	122	98.7✓
WL.	131	97.8✓

110.87

140's.

68

WL.	135	97.4✓
c	120	98.9✓
1/4	113	99.6✓
±	115	99.4✓
1/4	98	101.1✓
c	78	103.1✓
EL.	72	103.7✓

136's.

EL.	75	103.4✓
c	81	102.8✓
1/4	101	100.8✓
±	114	99.5✓
1/4	111	99.8✓
c	120	98.9✓
+8	136	97.3✓
WL.	149	96.0✓
+5	132	97.7✓

110.87

130's of QT.

WL.	136	97.3✓
+2	148	96.1✓
+5	132	97.7✓
C	123	98.6✓
1/4	111	99.8✓
±	112	99.7✓
1/4	100	100.9✓
C	84	102.5✓
EL.	7.8	103.1✓

112's.

EL.	7.4	103.5✓
C	83	102.6✓
1/4	9.7	101.2✓
±	10.5	100.4✓
1/4	10.9	100.0✓
C	133	97.6✓
+2	140	96.9✓
+5	132	97.7✓
WL.	123	98.6✓

110.87

100's. of QT.

69

WL	11.8	99.1✓
C	130	97.9✓
+2	142	96.7✓
+12	113	99.6✓
1/4	109	100.0✓
±	10.1	100.8✓
1/4	9.1	101.8✓
C ⁺¹⁴	80	102.9✓
C	7.1	103.8✓
EL.	5.8	105.1✓

75's.

EL	40	106.9✓
C	54	105.5✓
1/4	7.8	103.1✓
±	9.8	101.1✓
+8	9.3	101.6✓
+9	11.4	99.5✓
1/4	13.8	97.1✓
+4	12.4	98.5✓
C	11.4	99.5✓
WL.	10.6	100.3✓

110.87

62.81 = S.L. Thorn on West

WL	10.5	100.4 ✓
C	10.9	100.0 ✓
1/4	11.9	99.0 ✓
+1	12.4	98.5 ✓
+2	13.2	97.7 ✓
+5	13.4	97.5 ✓
+8	10.8	100.1 ✓
±	9.5	101.4 ✓
+7	8.6	102.3 ✓
1/4	6.4	104.5 ✓
C	4.8	106.1 ✓
EL	3.3	107.6 ✓
50' S		
EL	3.0	107.9 ✓
C	4.6	106.3 ✓
1/4	6.0	104.9 ✓
+5	6.4	104.5 ✓
+7	8.2	102.7 ✓
±	9.0	101.9 ✓
+7	8.5	102.4 ✓

110.87

20

+12	13.2	97.7 ✓
1/4	12.2	98.7 ✓
C	10.9	100.0 ✓
WL	10.2	100.7 ✓
20° 25' of QT = PC		
WL	10.1	100.8 ✓
C	11.1	99.8 ✓
+2	11.6	99.3 ✓
+5	12.8	98.1 ✓
+6	11.2	99.7 ✓
1/4	9.0	101.9 ✓
±	8.2	102.7 ✓
+3	7.8	103.1 ✓
+4	6.5	104.4 ✓
1/4	5.3	105.6 ✓
C	3.2	107.7 ✓
EL	1.1	109.8 ✓

15.64' S = S.L. Thorn on East

EL	0.4	110.5 ✓
C	2.8	108.1 ✓

110.87

1/4	50	1059 ✓
412	65	1044 ✓
±	80	1029 ✓
1/4	83	1026 ✓
+5	94	1015 ✓
+13	128	981 ✓
1/4 C	114	995 ✓
WL	99	1010 ✓
Sec Q.T.		
WL	107	1002 ✓
+1	112	997 ✓
+3	126	983 ✓
+5	116	993 ✓
C	94	1015 ✓
1/4	78	1031 ✓
+10	80	1029 ✓
±	62	1047 ✓
1/4	42	1067 ✓
C	13	1096 ✓
T.P.	042	11045 ✓

EL 8.84

119.29 ✓

60

113.3 ✓

119.29

Q.S. = ± Curve. thru 2 pts.

1

EL	39	115.4 ✓
C	8.1	111.2 ✓
+8	11.1	108.2 ✓
1/4	12.0	107.3 ✓
±	14.9	104.4 ✓
1/4	16.1	103.2 ✓
C	18.0	101.3 ✓
+6	21.0	98.3 ✓
WL	19.1	1002 ✓

Sec QR = 14.5° N. of QS = 373° S. of FMP.

W	19.1	1002 ✓
+4	21.0	98.3 ✓
C	18.0	101.3 ✓
1/4	16.0	103.3 ✓
+11	16.2	103.1 ✓
±	14.3	105.0 ✓
1/4	11.8	107.5 ✓
C	6.8	112.5 ✓
EL	1.9	117.4 ✓

119.29

353³⁶S = P.C.

EL	23	117.0 ✓
C	62	113.1 ✓
+6	87	110.6 ✓
1/4	101	109.2 ✓
+11	122	107.1 ✓
⊖	139	105.4 ✓
+3	153	104.0 ✓
1/4	153	104.0 ✓
C	167	102.6 ✓
WL	182	101.1 ✓
+5	208	98.5 ✓
+6 ^{toe}	194	99.9 ✓
	3A7 ⁰⁶ = NL Thorn on West.	
-6 ^{toe}	193	100.0 ✓
-5	206	98.7 ✓
WL	176	101.7 ✓
C	160	103.3 ✓
1/4	150	104.3 ✓
+13	149	104.4 ✓
⊖	124	106.9 ✓

119.29

1/4	97	109.6 ✓	72
C	63	113.0 ✓	
EL	27	116.6 ✓	
	325' S of MP.		
EL	39	115.4 ✓	
C	61	113.2 ✓	
1/4	90	110.3 ✓	
+10	106	108.7 ✓	
+12	129	106.4 ✓	
⊖	134	105.9 ✓	
+2	147	104.6 ✓	
+7	134	105.9 ✓	
1/4	143	105.0 ✓	
C	157	103.6 ✓	
WL	166	102.9 ✓	
+3 ^{toe}	168	102.5 ✓	
	300' S of MP.		
-3 ^{toe}	160	103.3 ✓	
WL	160	103.3 ✓	
C	151	104.2 ✓	
1/4	133	106.0 ✓	

119.29

15 +13	12.2	107.1	✓
£	13.1	106.2	✓
+6	12.8	106.5	✓
1/4	10.1	109.2	✓
C	6.1	113.2	✓
EL	4.0	115.3	✓

275' S. of M.P.

EL	4.0	115.3	✓
C	6.0	113.3	✓
+7	8.5	110.8	✓
+9	8.1	111.2	✓
1/4	8.8	110.5	✓
+4	9.9	109.4	✓
+5	11.1	108.2	✓
+12	11.1	108.2	✓
£	10.4	108.9	✓
1/4	12.2	107.1	✓
C	12.9	106.4	✓
WL	14.1	105.2	✓

250' S.

WL	12.7	106.6	✓
C	11.7	107.6	✓

119.29

1/4	11.0	108.3	✓
£	9.5	109.8	✓
1/4	9.3	110.0	✓
+2	8.9	110.4	✓
+3	7.0	112.3	✓
C	6.1	113.2	✓
EL	4.5	114.8	✓

225' S. of M.P.

EL	3.4	115.9	✓
C	5.0	114.3	✓
+3	5.8	113.5	✓
+5	7.8	111.5	✓
1/4	8.0	111.3	✓
£	9.6	109.7	✓
1/4	10.7	108.6	✓
C	12.1	107.2	✓
WL	13.3	106.0	✓
+2 ¹ toe	13.5	105.8	✓

215' S.

-5 ¹ toe	14.7	104.6	✓
WL	14.3	105.0	✓

73

119.29

C	134	105.9✓
1/4	11.5	107.8✓
±	100	109.3✓
1/4	8.5	110.8✓
+12	7.9	111.4✓
C	55	113.8✓
EL.	3.5	115.8✓

200's of NP.

EL.	6.3	113.0✓
+2	6.7	112.6✓
+5	8.4	110.9✓
C	8.3	111.0✓
+5	8.1	111.2✓
+10	9.6	109.7✓
1/4	10.4	108.9✓
±	11.7	107.6✓
1/4	12.5	106.8✓
C	12.9	106.4✓
WL.	13.2	106.1✓
+32	13.2	106.1✓

119.29

186's of NP.

74

-3 ⁵ toe.	13.0	106.3✓
WL.	12.9	106.4✓
C	12.7	106.6✓
1/4	12.4	106.9✓
±	11.9	107.4✓
1/4	10.7	108.6✓
C	8.3	111.0✓
EL.	8.2	111.1✓

175's.

EL.	8.1	111.2✓
C	9.3	110.0✓
1/4	10.8	108.5✓
±	11.7	107.6✓
1/4	12.1	107.2✓
C	12.2	107.1✓
WL.	12.2	107.1✓
+2	12.3	107.0✓
+6 ⁶ toe	14.6	104.7✓

57

119.29

150'S.

-8° toe	14.8	104.5 ✓
-5	14.8	104.5 ✓
WL	11.5	107.8 ✓
C	11.4	107.9 ✓
1/4	11.7	107.6 ✓
£	11.7	107.6 ✓
1/4	10.8	108.5 ✓
C	9.4	109.9 ✓
EL	8.1	111.2 ✓

143'S.

EL	8.4	110.9 ✓
C	9.3	110.0 ✓
1/4	10.6	108.7 ✓
£	11.6	107.7 ✓
1/4	11.6	107.7 ✓
C	11.3	108.0 ✓
WL	11.3	108.0 ✓
+3	14.6	104.7 ✓
+8° toe	14.6	104.7 ✓

119.29

139'S.

75

-6.5° toe	13.4	105.9 ✓
-3	13.4	105.9 ✓
WL	14.5	104.8 ✓
+2	11.4	107.9 ✓
C	11.2	108.1 ✓
1/4	11.4	107.9 ✓
£	11.5	107.8 ✓
1/4	10.5	108.8 ✓
C	9.5	109.8 ✓
EL	8.4	109.9 ✓

125'S.

EL	8.6	110.7 ✓
C	9.6	109.7 ✓
1/4	10.0	109.3 ✓
£	11.3	108.0 ✓
1/4	11.0	108.3 ✓
C	10.8	108.5 ✓
+6	10.8	108.5 ✓
WL	14.3	105.0 ✓
+8° toe	14.3	105.0 ✓

119.29

112'S

- 5 ¹ / ₂ toe.	12.2	107.1 ✓
WL	13.0	106.3 ✓
+4	14.1	105.2 ✓
+7	10.4	108.9 ✓
C	10.4	108.9 ✓
1/4	11.2	108.1 ✓
⊕	11.1	108.2 ✓
1/4	9.4	109.9 ✓
C	9.5	109.8 ✓
EL	8.9	110.4 ✓

100'S

EL	8.7	110.6 ✓
C	9.0	110.3 ✓
1/4	9.2	110.1 ✓
⊕	10.7	108.6 ✓
1/4	11.0	109.3 ✓
C	10.4	108.9 ✓
+4	14.1	105.2 ✓
+8	12.1	107.2 ✓
WL	12.0	107.3 ✓
+ 5 ¹ / ₂ toe.	11.8	107.5 ✓

119.29

90'S of NP

76

- 2 ¹ / ₂ toe.	9.6	109.7 ✓
WL	10.6	108.7 ✓
+3	11.7	107.6 ✓
+6	13.6	105.7 ✓
C	11.3	108.0 ✓
1/4	10.8	108.5 ✓
⊕	10.1	109.2 ✓
1/4	8.8	110.5 ✓
C	8.4	110.9 ✓
EL	8.2	111.1 ✓

75'S

EL	7.9	111.4 ✓
C	8.3	111.0 ✓
1/4	8.7	110.6 ✓
⊕	9.4	109.9 ✓
1/4	10.3	109.0 ✓
+12	11.2	108.1 ✓
C	13.4	105.9 ✓
+4	11.6	107.7 ✓
WL	9.4	109.9 ✓

119-29

50'S of N.P.

WL	88	110.5✓
+2	92	110.1✓
+7	124	106.9✓
C	12.1	107.2✓
+2	11.1	108.2✓
+10	9.4	109.9✓
1/4	9.0	110.3✓
±	8.7	110.6✓
1/4	8.1	111.2✓
C	7.7	111.6✓
EL	7.2	112.1✓

40'S

EL	7.0	112.3✓
C	7.6	111.7✓
1/4	8.0	111.3✓
±	8.5	110.8✓
1/4	8.7	110.6✓
+4	9.2	110.1✓
+8	10.3	109.0✓
+12	10.4	108.9✓
C	12.1	107.2✓

119-29

+6

WL

WL

C

+6

+10

1/4

±

1/4

C

EL

EL

C

1/4

±

1/4

+1

+5

C

+5

WL

9.0

85

6.9

9.0

11.7

9.9

9.1

8.2

7.9

7.5

7.0

6.4

7.1

7.7

8.4

9.8

11.1

9.8

8.5

7.6

6.0

110.3✓

110.8✓

112.4✓

110.3✓

107.6✓

109.4✓

110.2✓

111.1✓

111.4✓

111.8✓

112.3✓

112.9✓

112.2✓

111.6✓

110.9✓

109.5✓

108.2✓

109.5✓

110.8✓

111.7✓

113.3✓

77

27⁵⁴S = SL Ups. on East

15'S

119.29

0.96 S. of N.P. - S.L. Ups on W.

WL.	56	113.7 ✓
C	79	111.4 ✓
+10	87	110.6 ✓
1/4	88	110.5 ✓
+10	92	110.1 ✓
±	86	110.7 ✓
1/4	74	111.9 ✓
C	68	112.5 ✓
EL.	62	113.1 ✓

Sec. N.P.

EL.	62	113.1 ✓
C	68	112.5 ✓
1/4	74	111.9 ✓
±	86	110.7 ✓
+5	92	110.1 ✓
1/4	88	110.5 ✓
+5	87	110.6 ✓
C	79	111.4 ✓
WL.	56	113.7 ✓

119.29

Sec. N.O. - 36th N on East. camp pt. W. 78

EL.	62	113.1 ✓
C	64	112.9 ✓
1/4	69	112.4 ✓
±	77	111.6 ✓
1/4	76	111.7 ✓
+6	80	111.3 ✓
C	73	112.0 ✓
WL.	56	113.7 ✓
T.P. Hub. 15' W. of N.O.	173	117.56

ok
117.59

Continued in book 987

29

30



1193
797
1192

Handwritten notes and calculations on the left page, including various numbers and small tables. Some numbers are circled or underlined. There are also some faint sketches or diagrams.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.