

990

F.B. 990

FIELD BOOK

360

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

RETURN TO CITY ENGINEER'S OFFICE  
CITY HALL, SAN DIEGO, CAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

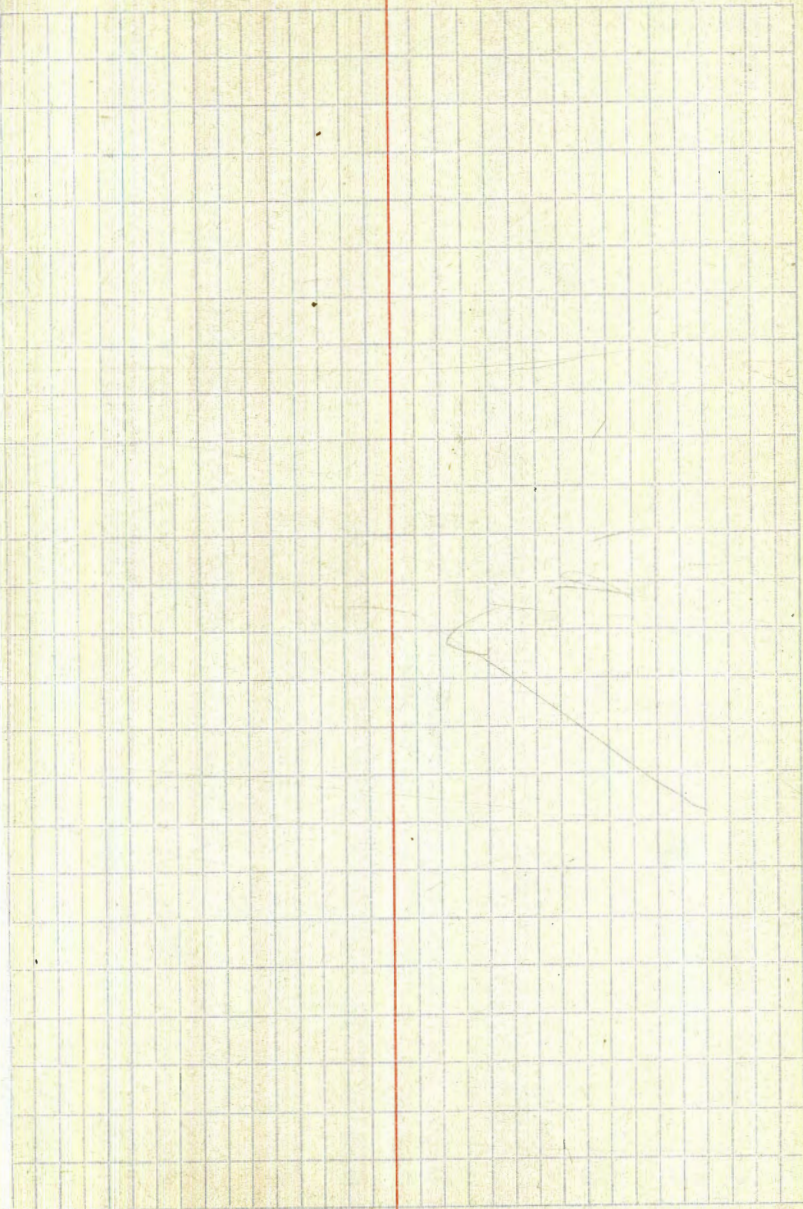
"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

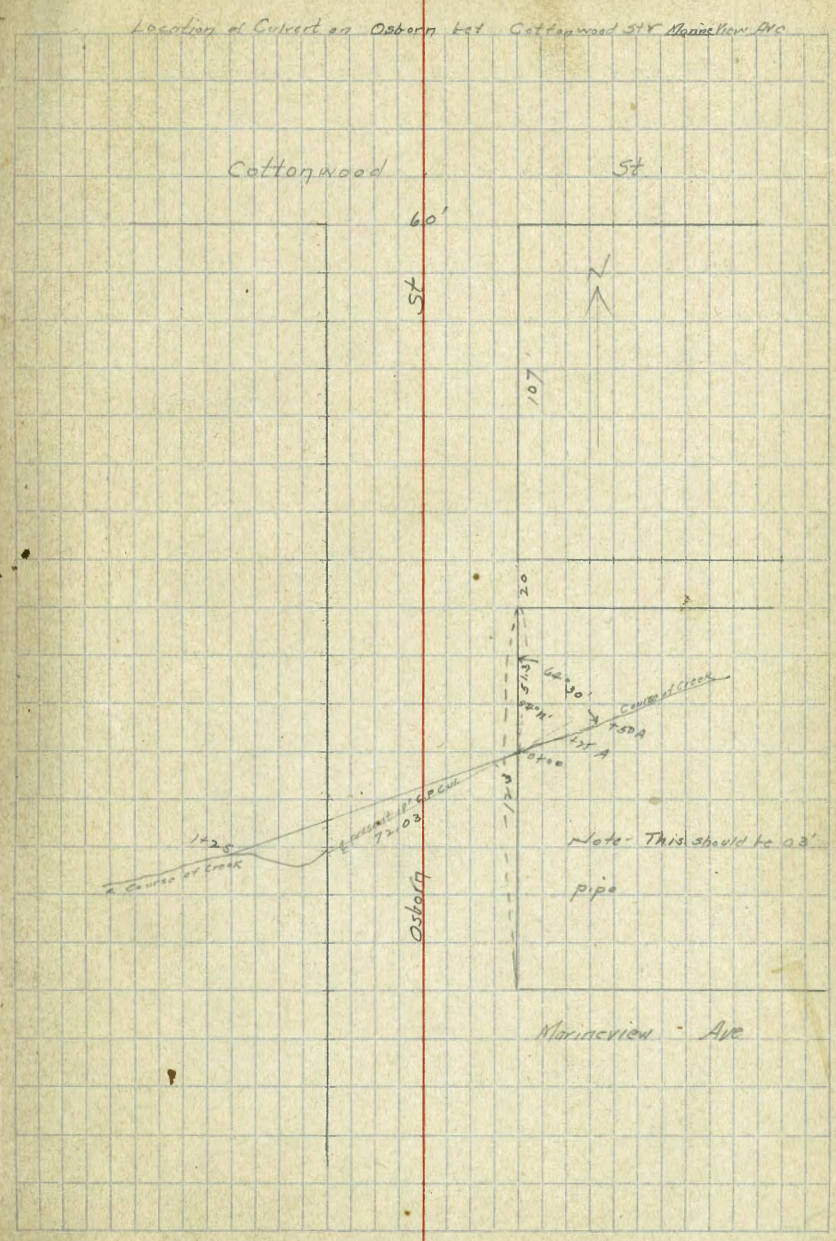
0.51  
0.07  
0.44

MICROFILMED  
JUL 10 1964



3 (Days)  
 21 (Hours)  
 15 (Minutes)

Sta	Levels over	Proposed	Osborn St	Current
	+	Nt.	-	Elev
	1300	2611		1311 B.M. N. Side Main? Cr. 14
T.P	10.34	34.50	192	2419
T.P	0.27	25.35	1295	21.58
T.P	2.17	14.50	1304	12.31
+55A			76	6.9
+55A			78	6.7
0+00 E. End Cul. bed			86	5.9
+00 Top Callac.			63	8.2
+03			49	9.6
+25			46	9.9
+50			45	100
+57			47	9.8
+56			622	8.3
+58			64	8.1
+60			48	7.7
+63			76	6.9
+66 <sup>27</sup> W. line Osborn			82	6.5
+75			72	7.5
+76			56	8.9
+100			70	7.5
+04			74	7.1
+05			81	6.4
+25			83	6.2
W. End present Cul.			96	4.9
B.M. Sp. K. Elev. pole SW Osborn & Cottonwood			489	9.61



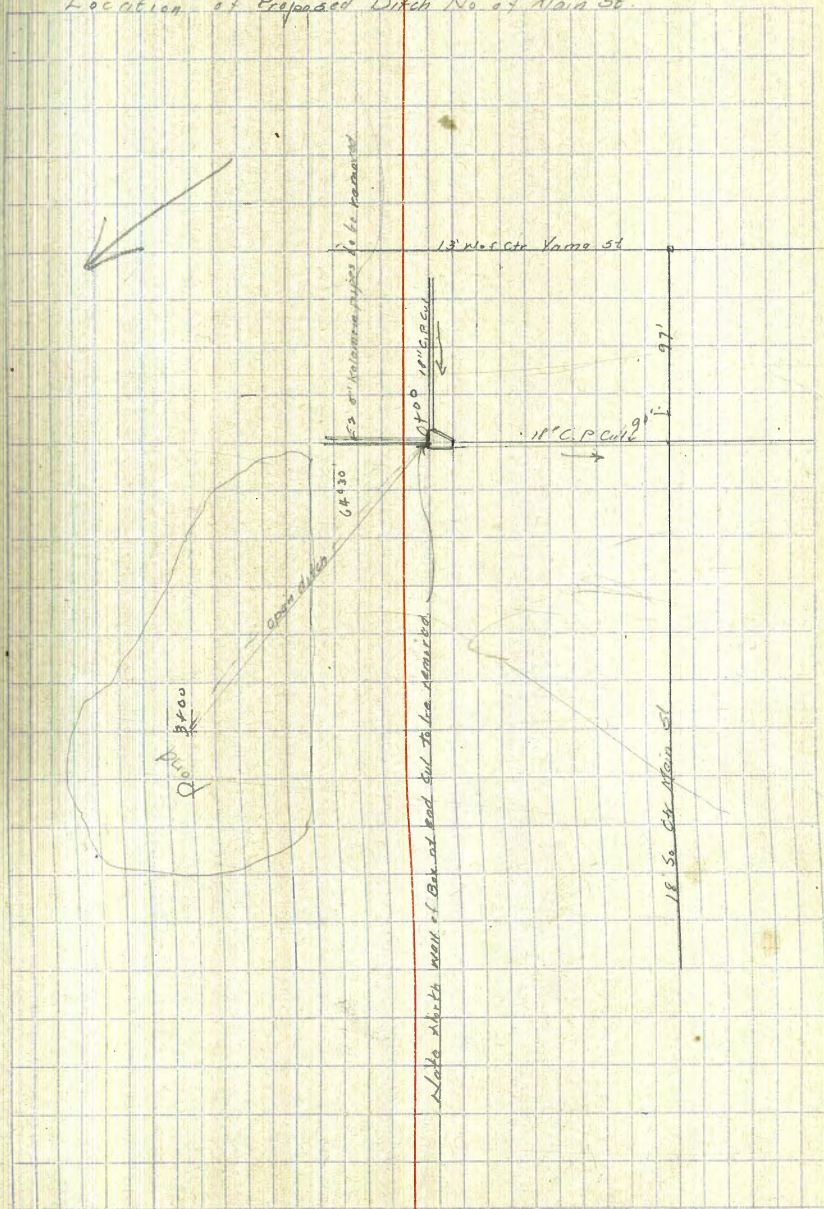
Note - This should be 03' pipe

Levels for ditch No. of Main St West of Yama

Davis  
Hansen  
Harris

	7.21	10.11	20.01	End Cul. N. End
0+00 - End Cul			7.21	3.8
Top Wall at N. end cul			4.9	5.2
+45 - Edge water			6.2	3.9
+75			6.5	3.6
+100			6.4	3.7
+150			6.7	3.4
2			6.2	3.9
150			6.7	3.4
3			7.0	3.1

Location of Proposed Ditch No. of Main St



Cross Sections for Proposed Drain

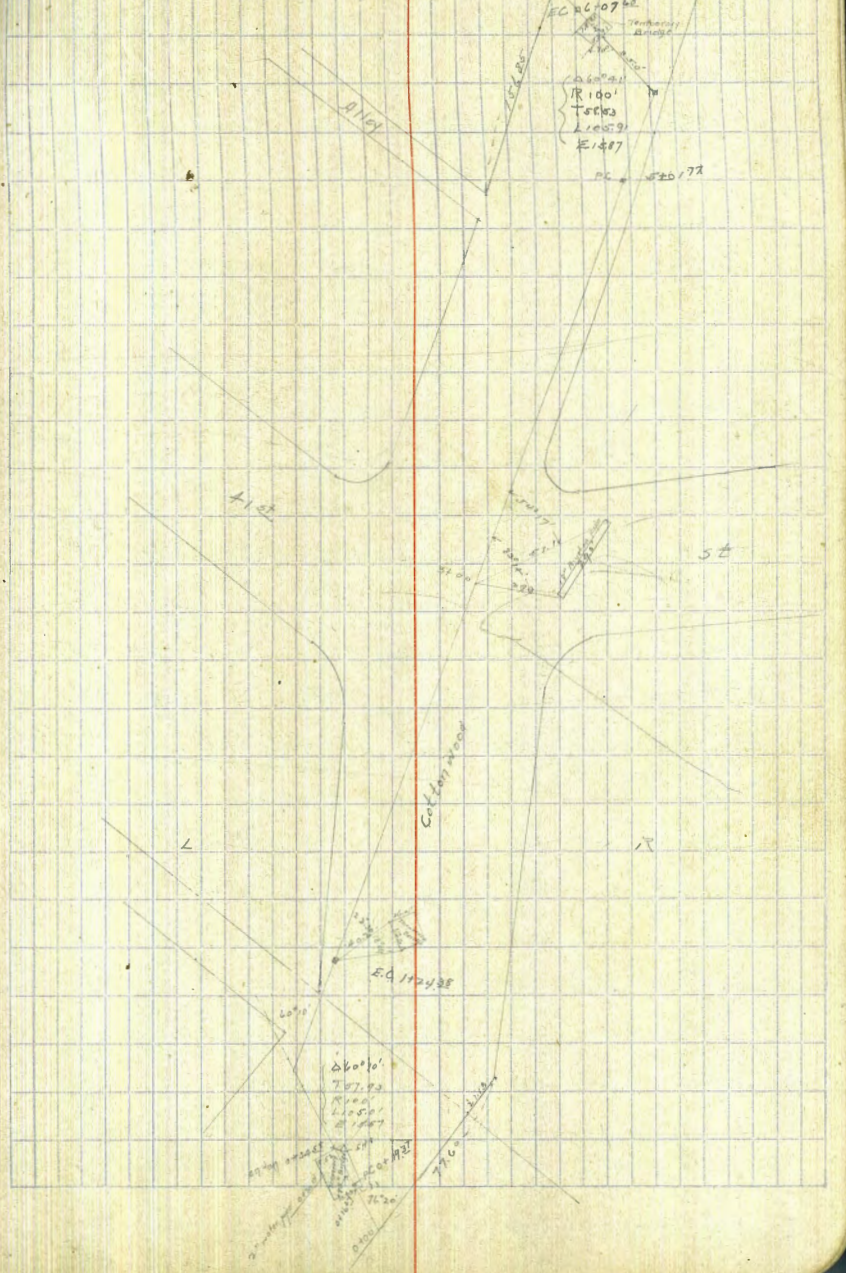
5th E. 1st St.

	6.48	16.09		9.61	BRIDGE	
T.P.	7.15	19.44	3.80	12.27		
Stg			C	R		
± 0.00	12.8 25	13.4 13	8.7 5	8.5	11.1 10.9	12.3 25
So end Bridge and 100'				12.2		
P.C. ± 19.27	12.4 25	12.7 11	8.9	8.5	11.9 11.7	12.7 25
+ 30" Top 2" water pipe				10.0		
+ 50	12.9 25	12.4 12	8.7 5	9.9	11.5 11.4	12.4 25
+ 75	13.8 25	12.5 13	11.0 10	9.3	10.7 10.5	12.4 25
+ 100	12.6 25	12.7 13	8.9 5	8.9	11.6 11.1	12.3 25
E.C. 1st St	12.4 25	12.3 12		9.2	11.2 11.0	12.5 25
+ 50	13.7 25	13.0 10		12.7	11.9 11.7	12.0 25
+ 75	14.2 25	13.0 10		13.0	12.1 11.9	12.0 25
2	14.3 25	14.1 12	11.2 11	13.1	12.0 11.8	12.0 25
+ 10				13.6	12.4 12.2	12.0 25
+ 75	14.2 25	14.1 10		13.9	12.7 12.5	12.0 25
+ 50	14.7 25	14.2 10		14.2	13.0 12.8	12.0 25
+ 75	14.6 25	14.6 10		14.6	13.1 12.9	12.0 25
3		14.4 25		14.1	13.4 13.2	12.0 25
+ 05				14.0	13.4 13.2	12.0 25
+ 20				14.4	13.8 13.6	12.0 25
+ 25	14.8 25			14.7	14.1 13.9	12.0 25
+ 50	15.4 25			15.0	14.4 14.2	12.0 25
+ 75	15.7 25			15.0	14.7 14.5	12.0 25
4	16.2 25			15.3	15.0 14.8	12.0 25

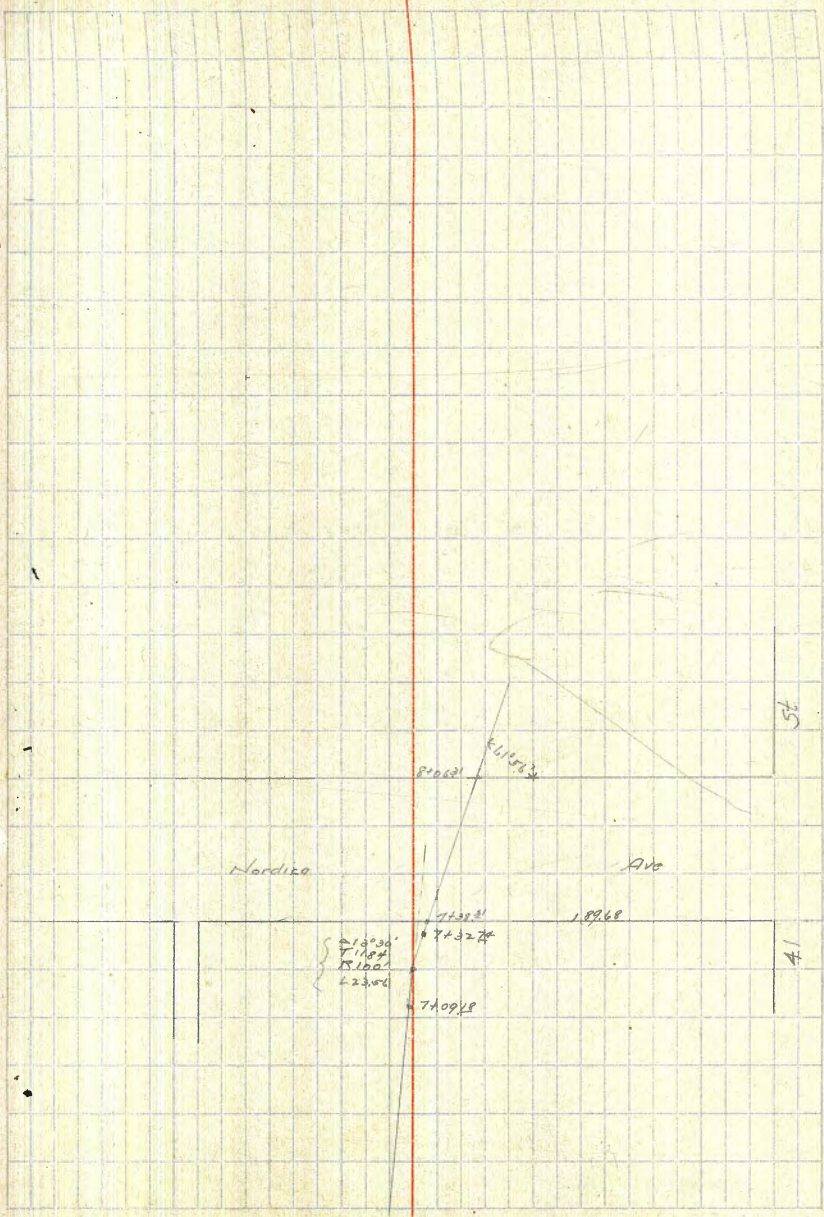
B.M. 5th brace pile NE corner of 4th

Location of Drain in Nardica Heights

Don  
Hancock  
Henick



Sta	L	1944	C	R
4+2.5		$\frac{15.5}{25}$	$\frac{15.4}{28}$ $\frac{14.5}{27}$ $\frac{11.1}{27}$ $\frac{11.1}{27}$ $\frac{13.4}{27}$	$\frac{14.2}{20}$
650		$\frac{15.6}{25}$	15.6	$\frac{15.1}{16}$ $\frac{14.9}{27}$ $\frac{13.1}{25}$ $\frac{14.1}{29}$ $\frac{14.2}{20}$
+75		$\frac{15.6}{25}$	15.6	$\frac{15.4}{8}$ $\frac{14.1}{10}$ $\frac{13.7}{24}$ $\frac{14.1}{22}$ $\frac{14.5}{20}$
PC 6+01.72		$\frac{15.6}{25}$	15.5	$\frac{15.5}{12}$ $\frac{14.6}{17}$ $\frac{14.2}{22}$ $\frac{14.8}{21}$ $\frac{15.1}{15}$
+25		$\frac{15.5}{25}$	15.0	$\frac{14.6}{29}$ $\frac{12.7}{24}$ $\frac{10.6}{21}$ $\frac{14.2}{20}$ $\frac{14.4}{20}$ $\frac{15.9}{25}$
+50		$\frac{16.0}{25}$	15.7	$\frac{14.6}{18}$ $\frac{13.1}{29}$ $\frac{11.1}{26}$ $\frac{14.7}{22}$ $\frac{15.2}{20}$ $\frac{16.2}{20}$
T.P. on BI Hub 629		21.31	5.02	14.42
+75		$\frac{15.8}{25}$ $\frac{15.6}{2}$	14.8	$\frac{12.2}{7}$ $\frac{11.9}{14}$ $\frac{14.6}{20}$ $\frac{15.7}{20}$
Floor of Bridge			15.06	
EC 6+07.68		$\frac{16.4}{25}$ $\frac{15.9}{12}$ $\frac{4.1}{7}$ $\frac{10.9}{2}$	10.9	$\frac{11.3}{3}$ $\frac{15.0}{8}$ $\frac{15.3}{25}$
+25		$\frac{16.6}{25}$ $\frac{16.3}{12}$ $\frac{15.1}{7}$ $\frac{11.7}{2}$	11.5	$\frac{12.9}{6}$ $\frac{15.3}{12}$ $\frac{15.5}{25}$
+50		$\frac{16.2}{25}$ $\frac{15.9}{10}$ $\frac{14.1}{2}$	11.9	$\frac{14.8}{3}$ $\frac{15.6}{13}$ $\frac{15.6}{25}$
+75		$\frac{15.8}{25}$ $\frac{15.7}{12}$ $\frac{12.6}{3}$	12.4	$\frac{15.3}{10}$ $\frac{15.9}{25}$
PC 7+09.8		$\frac{16.9}{25}$ $\frac{16.2}{15}$ $\frac{13.0}{3}$	12.6	$\frac{12.8}{3}$ $\frac{15.8}{11}$ $\frac{16.4}{25}$
EC 7+32.0		$\frac{16.9}{25}$ $\frac{16.5}{14}$ $\frac{13.5}{6}$	12.9	$\frac{15.8}{9}$ $\frac{16.0}{25}$
TS 21		$\frac{16.8}{25}$ $\frac{16.7}{16}$ $\frac{13.6}{6}$	11.8	$\frac{12.8}{1}$ $\frac{15.5}{15}$ $\frac{16.1}{25}$
End 3rd Pipe		$\frac{15.6}{9}$ $\frac{13.9}{3}$ $\frac{11.6}{1}$	11.8	$\frac{14.9}{1}$ $\frac{15.9}{25}$
+68		$\frac{16.3}{25}$	15.8	$\frac{15.8}{25}$
+75		$\frac{16.1}{25}$	15.9	$\frac{15.4}{25}$
+86		$\frac{16.9}{25}$	15.9	$\frac{16.6}{25}$
+93		$\frac{17.0}{25}$ $\frac{16.6}{4}$	12.4	$\frac{12.2}{9}$ $\frac{16.3}{10}$ $\frac{16.6}{25}$
P + 06.21 N.L. Nordica		$\frac{16.2}{25}$ $\frac{15.9}{10}$ $\frac{13.9}{6}$	12.2	$\frac{12.7}{6}$ $\frac{15.6}{10}$ $\frac{16.9}{25}$
101.2 Parallel with N.L. line		$\frac{16.9}{25}$ $\frac{16.6}{9}$ $\frac{13.7}{7}$	12.2	$\frac{12.7}{7}$ $\frac{15.8}{15}$ $\frac{17.5}{25}$
B.M. BIK Cor. Hub S.W. Nordica 41.2			3.25	18.06
I.P. 6.50		25.63	2.18	19.13
B.M. BIK Cor. Hub N.W. Nordica 42.9			40.4	21.59

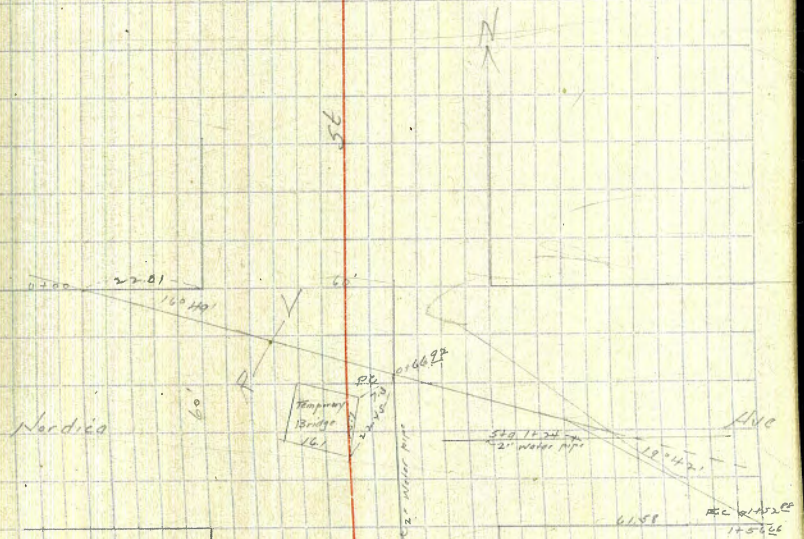


Cross Sections for Proposed Drain

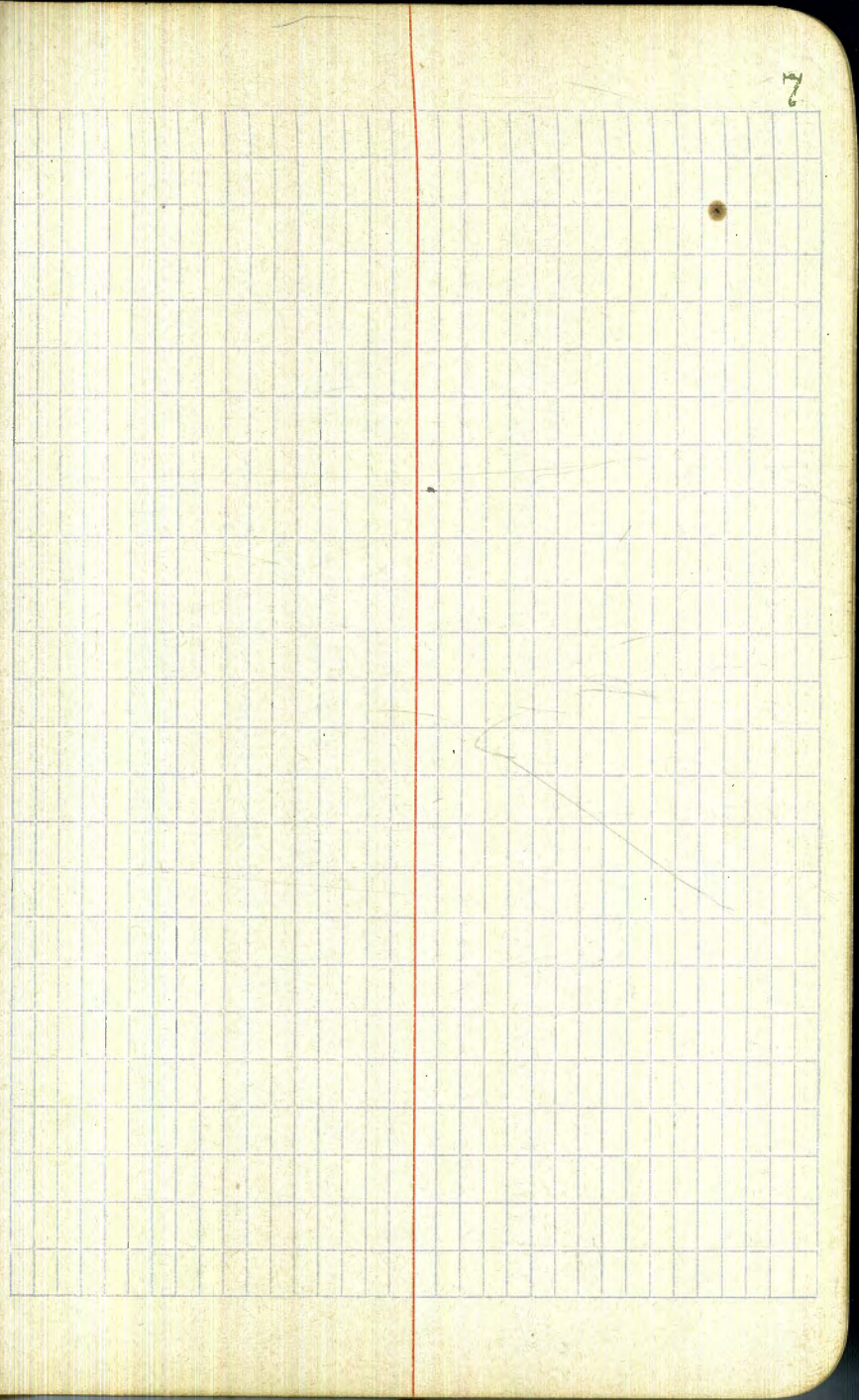
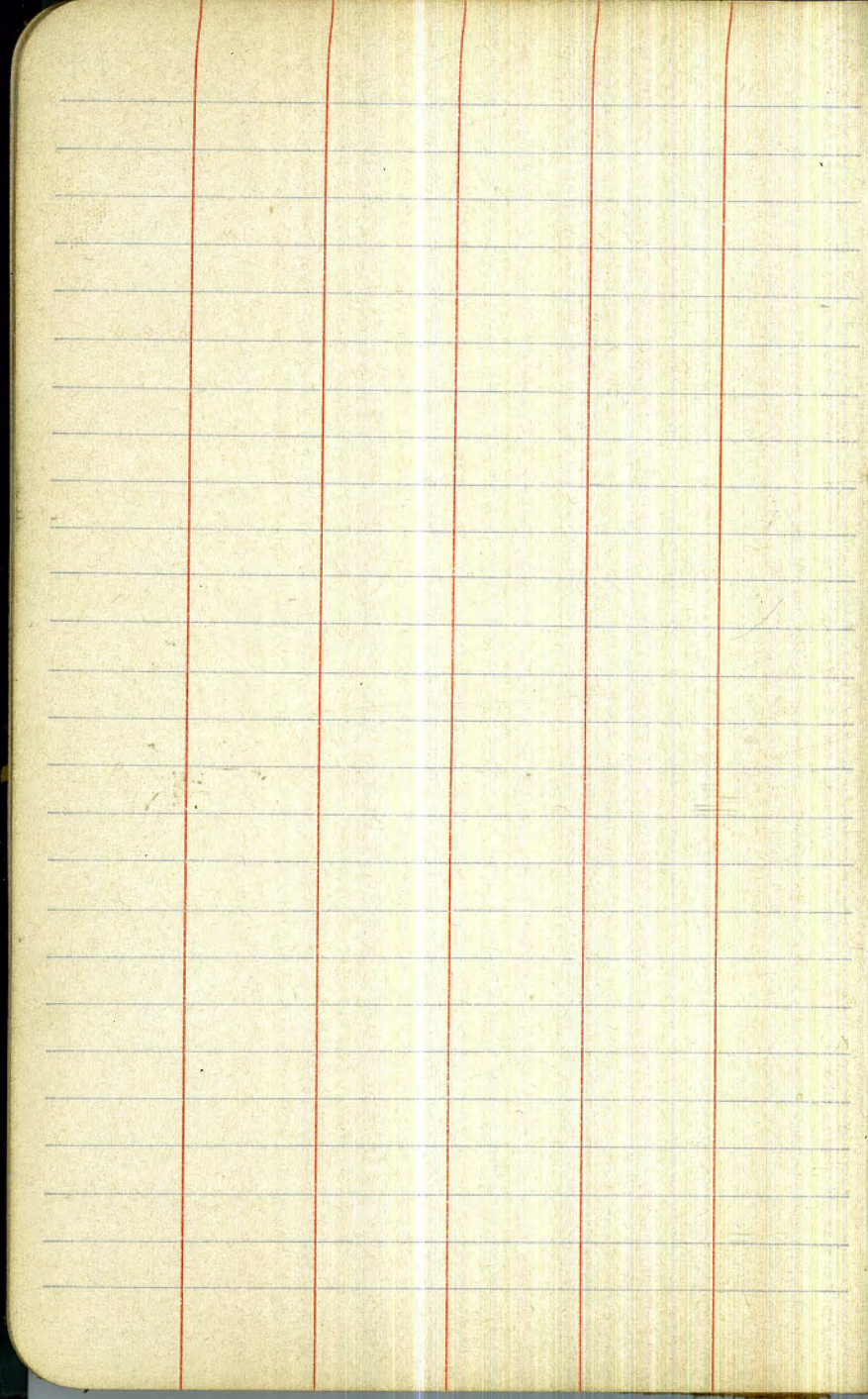
Station	Left	Center	Right
5+84	27.42		21.57
5+90			
0+00 Along Line	$\frac{21.7}{18} \frac{21.7}{18}$	18.8	$\frac{19.7}{17} \frac{22.7}{20} \frac{22.7}{20}$
0+00 At Right Angles	$\frac{22.1}{25} \frac{21.8}{25}$	18.9	$\frac{18.1}{3} \frac{22.7}{10} \frac{22.0}{25}$
+25	$\frac{22.3}{25}$	20.8	$\frac{19.0}{6} \frac{18.9}{13} \frac{22.7}{16} \frac{22.4}{25}$
+50	$\frac{22.2}{25}$	22.2	$\frac{22.2}{5} \frac{18.8}{15} \frac{18.9}{17} \frac{22.0}{20} \frac{22.7}{25}$
Floor of Bridge		21.7	
P.C. +66.92	$\frac{22.2}{25}$	21.9	$\frac{22.5}{7} \frac{19.2}{10} \frac{19.8}{20} \frac{22.4}{20} \frac{22.7}{30}$
1+00	$\frac{22.3}{25} \frac{22.4}{25}$	19.9	$\frac{19.3}{2} \frac{19.3}{1} \frac{22.9}{17} \frac{22.5}{25}$
+25 on 2" Pipe		19.6	
+75	$\frac{22.4}{25} \frac{22.4}{9} \frac{22.6}{9}$	19.2	$\frac{20.1}{5} \frac{22.9}{11} \frac{22.6}{25}$
E.C. +52.99	$\frac{22.5}{25}$	19.3	$\frac{19.2}{2} \frac{22.1}{10} \frac{22.7}{25}$
Stone St +36.44	$\frac{22.5}{25}$	19.2	$\frac{19.2}{2} \frac{22.1}{10} \frac{22.7}{25}$
+56.66 Along St. Line	$\frac{22.3}{25} \frac{22.1}{17} \frac{19.3}{2}$	19.2	$\frac{19.2}{2} \frac{22.3}{15} \frac{22.7}{30}$

Location of Proposed Drain - Nerdica & 42<sup>nd</sup> St

Hand  
Traced







4/12/14  
Graham  
Thorne  
Miller

CROSS-SECTION OF VOLTAIRE ST. 70' WIDE 10' WALKS  
FROM THE WEST LINE OF CHATEAUX BLVD  
TO THE EAST - Point Loma Villas  
(SEE SKETCH PAGE 1A)

B.M.	837	105.02	96.65	511 Tennessee + Chateaux
T.P.	18.95	117.24	107.89	
T.P.	805	123.19	115.14	
W.L. of Chateaux = 500 ft (126 ft.?)				
So. = P.C.		5.1	118.1'	
cb on Curve		4.3	118.9'	
So. Line prod. East		3.9	119.3'	
Cb ✓ ✓ ✓		3.5	119.7'	
So. 1/4 ✓ ✓		2.8	120.4'	
Ctr ✓ ✓		2.4	120.8'	
No. 1/4 ✓ ✓		2.2	121.0'	
cb line ✓ ✓		1.7	121.5'	
No. ✓ ✓ ✓		1.0	122.2'	
cb on Curve		1.0	122.2'	123.1
No. = E.C.		0.1	123.1'	123.6

SEC. B.

No.	1.4	121.8'
cb	1.8	121.4'
1/4	2.2	121.0'
c	2.7	120.5'
1/4	3.4	119.8'
cb	3.9	119.3'
So.	4.5	118.7'

SEC. C

So.	4.5	118.7'
-----	-----	--------

Point about 1 ft. 30

VOLTAIRE

123.2 H3

No.	4.0	119.2'
1/4	3.5	119.7'
1/4	2.6	120.6'
1/4	2.4	120.8'
cb	1.8	121.4'
No.	1.4	121.8'
25' West.		
No.	1.9	121.3'
cb	2.2	121.0'
1/4	2.5	120.7'
c	3.1	120.1'
1/4	3.6	119.6'
cb	4.5	118.7'
So.	5.1	118.1'
50' W.		
So.	5.4	117.8'
cb	4.9	118.3'
1/4	4.2	119.0'
c	3.6	119.6'
1/4	3.1	120.1'
cb	2.9	120.3'
No.	2.6	120.6'
75' W.		
No.	3.0	120.2'
cb	3.6	119.6'

123.19

1/4		4.1	119.1
c		4.5	118.7
1/4		5.2	118.0
cb		5.5	117.7
So.		5.9	117.3
	100' W		
So.		6.1	117.1
cb		5.6	117.6
1/4		5.6	117.6
c		5.1	118.1
1/4		4.5	118.7
cb		4.2	119.0
No.		3.9	119.3
	125' W		
No.		4.9	118.3
cb		5.4	117.8
1/4		6.0	117.2
c		6.4	116.8
1/4		6.8	116.4
cb		7.1	116.1
So.		7.7	115.5
	150' W		
So.		9.4	113.8
cb		8.8	114.4
1/4		8.5	114.7
c		8.2	115.0

123.2

VOLTAIRE

1/4		7.5	115.7
cb		6.9	116.3
No.		6.8	116.4
	175' W		
No.		8.3	114.9
cb		8.7	114.5
1/4		8.8	114.4
c		9.3	113.9
1/4		9.7	113.5
cb		10.2	113.0
So.		10.7	112.5
	200' W		
So.		12.6	110.6
cb		12.4	110.8
1/4		12.1	111.1
c		11.3	111.9
1/4		10.7	112.5
cb		10.3	112.9
No.		9.7	113.5
	225' W		
No.		12.4	110.8
cb		12.5	110.7
1/4		12.7	110.5
T.P.	2.20	112.81	112.58
c		3.3	109.5

1/4		3.8	109.0 ✓
cb		3.8	109.0 ✓
So		3.8	109.0 ✓
250' W			
So		5.6	107.2
cb		5.5	107.3
1/4		5.5	107.3
C		5.3	107.5
1/4		4.6	108.2
cb		4.1	108.7
No		3.9	108.9
275' W			
No		5.9	106.9
cb		6.1	106.7
1/4		6.0	106.8
C		6.8	106.0
1/4		7.5	105.5
cb		7.1	105.7
So		7.4	105.4
296.87' W = SEC. D			
So		9.4	103.4
cb		9.2	103.6
1/4		8.9	103.9
C		8.3	104.3
1/4		7.8	105.0
cb		7.1	105.7

No.		7.1	105.7
SEC. E			
No.		7.7	105.1
cb		8.2	104.6
1/4		8.6	104.2
C		9.1	103.7
1/4		9.5	103.3
cb		9.5	103.3
So		9.4	103.4
East Line of Villa Drive (70' wide) 128.94' from Z to Y			
S = EC = pt Z		14.6	98.2
Co. on Curve		13.1	99.7
So Line prod. W		12.9	99.9
Cb ✓ ✓ ✓		12.9	99.9
1/4 ✓ ✓ ✓		12.7	100.1
C ✓ ✓ ✓		12.2	100.6
1/4 ✓ ✓ ✓		11.7	101.1
cb ✓ ✓ ✓		11.0	101.8
No ✓ ✓ ✓		10.5	102.3
No. = E.C. - pt Y		9.4	103.4
Curve (127.17 from No to So)			
No = on line XY		10.2	102.6
No Line prod. W		11.9	100.9
Cb ✓ ✓ ✓		12.4	100.4
T.P.	1.14	101.62'	12.33 100.48'

101.62

1/2 line prod. west	1.8	99.3
c - - -	2.2	99.4
1/4 - - -	2.8	98.8
cb - - -	3.2	98.4
So. - - -	3.6	98.0
on line WZ	4.6	97.0
Quarter (120.95 from WZ to XY)		
on line WZ	6.0	95.6
So. - prod. West.	5.0	96.6
cb - - -	4.5	97.1
1/4 - - -	4.4	97.2
c - - -	4.4	97.2
1/2 - - -	4.8	96.8
cb - - -	4.5	97.1
No. - - -	3.0	98.6
on line XY	0.9	100.7
Center (122.74 from XY to WZ)		
on line XY	4.2	97.4
No. - prod. West.	5.8	95.8
cb - - -	5.5	96.1
1/4 - - -	6.4	95.2
c - - -	6.2	95.9
1/2 - - -	5.4	96.2
cb - - -	4.9	96.7
So. - - -	5.5	96.1
on line WZ	7.2	94.4

101.6

VOLTAIRE

11

West Quarter (120.53 from WZ to XY)

on line WZ	8.2	93.4
So. - prod. West.	6.6	95.0
cb - - -	6.5	95.1
1/4 - - -	7.1	94.5
c - - -	7.7	93.9
1/2 - - -	7.3	94.3
cb - - -	6.2	95.4
No. - - -	6.7	94.9
on line XX	7.0	94.6
Curb (117.32 from XY to WZ)		
on line XY	10.2	91.4
No. - prod. west	9.2	92.4
cb - - -	8.8	92.8
1/4 - - -	9.5	92.1
c - - -	9.2	92.4
1/2 - - -	8.5	93.1
cb - - -	8.0	93.6
So. - - -	8.1	93.5
on line WZ	9.7	91.9
West Line of Killa Drive (116.55 from W to X)		
on point W	11.0	90.6
+10	9.6	92.0
So. line prod.	9.1	92.5
+32 = cb on curve	9.1	92.5
cb line prod.	9.2	92.4

1/4 line prod		9.7	919
c - -		10.2	914
1/4 - v		10.6	910
cb - -		11.2	904
No. v -		11.9	897
+ 13 = cb on Curve		11.8	898
on point X		12.7	889
T.P.	467	<u>93.66</u>	12.63 8899

= T.P. on NE  
end of curve  
07-11-19

## Sec. F.

No.		6.0	877
cb		4.9	888
1/4		4.1	896
c		3.8	899
+ 5		3.4	903
1/4		2.4	913
cb		1.3	924
So.		1.4	923

## Sec. G.

So.		1.8	919
cb		1.6	921
1/4		2.7	910
+ 7.5		3.5	902
c		3.7	900
1/4		4.0	897
cb		4.9	888
No.		6.0	877

## 25' west.

No.		62	875
cb		51	886
1/4		42	895
c		39	898
1/4		33	904
cb		23	914
So.		26	911

## 50' west.

So.		43	894
cb		39	898
1/4		39	898
c		43	894
1/4		49	888
cb		54	883
No.		60	877

## 75' west.

No.		62	875
cb		58	879
1/4		52	885
c		44	893
1/4		40	897
cb		40	897
So.		50	887

100' west

So	5.7	88.0'
cb	4.9	88.8'
1/4	4.5	89.2'
c	5.5	88.2'
1/4	6.4	87.3'
cb	5.6	88.1'
No	5.5	88.2'

110' west

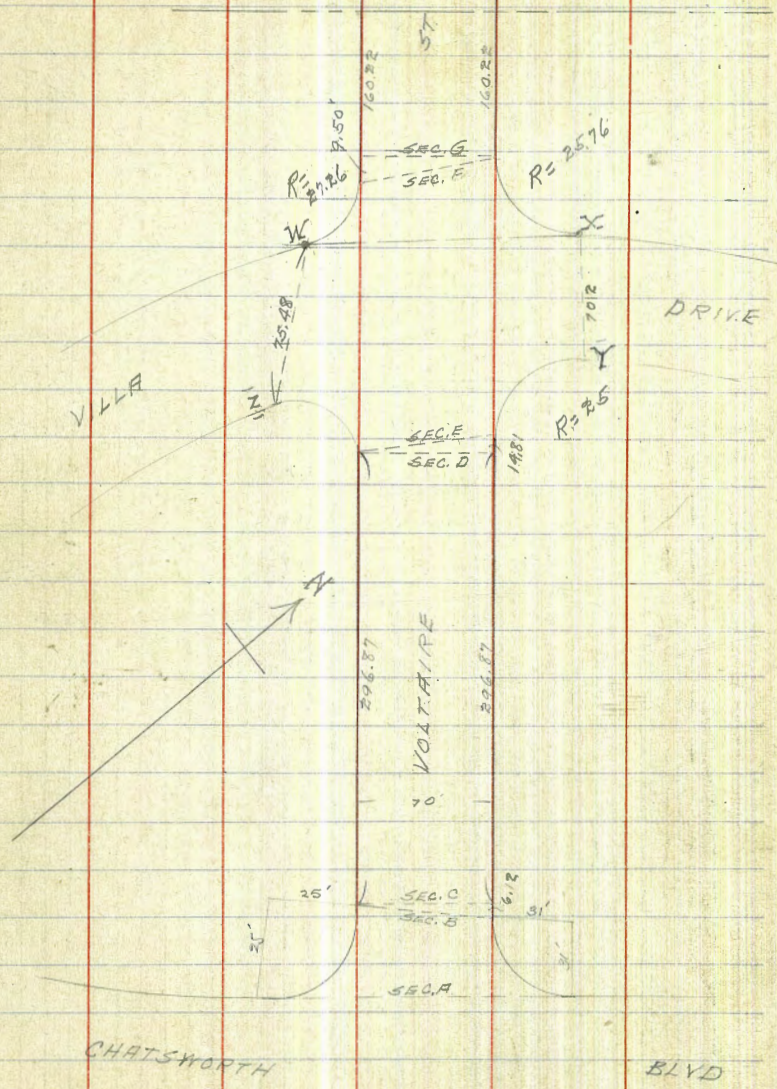
No.	6.8	86.9'
cb	6.8	86.9'
1/4	7.8	85.9'
c	7.1	86.6'
1/4	6.4	87.3'
cb	6.5	87.2'
So.	7.2	86.5'

125' W

-15	12.5	81.2'
So.	11.0	82.7'
cb	10.2	83.3'
1/4	9.9	83.8'
c	9.1	84.6'
1/4	8.9	84.8'
cb	9.7	84.0'
No.	10.3	83.4'
+15	11.5	82.2'

T.P.	1.76	88.59	12.83	80.83
100.88' M = Pt. of Pt. Loma Villas				
-20			8.2	74.4'
No.			6.4	76.2'
cb			5.5	77.1'
1/4			5.6	77.0'
c			6.3	76.3'
1/4			7.1	75.5'
cb			8.2	74.4'
So			10.6	72.0'
+30			14.0	68.6'
T.P.	12.78	93.61	1.76	80.83'
T.P.	9.49	103.05	0.03	93.58
			6.41	96.64 = 65.819

Continued on page 36





Gregory Moore Miller

Levels on Chatsworth Blvd (Graded) 20' wide  
 from No. of Tennyson  
 to N.E. of Dumas St.

SEE SKETCH PAGE 28

B.M. 932 105.97 96.65 SW Tennyson & Chatsworth  
 149.0 on West }  
 144.45 on East } = No. of Tennyson = end of curb.

E cb 8.1 97.9 on cement Co.

c 8.5 97.5

W cb 8.4 97.6 on cement Co.

Sect. A

W 7.9 98.1

cb 8.1 97.9

c 8.3 97.7

cb 8.1 97.9 on cement.

Sect B

E 7.6 98.4

cb 7.8 98.2

c 8.0 98.0

cb 7.8 98.2

W 7.7 98.3

Sect C = at end of Villa Drive

W 6.7 99.3 1 foot of sand washed in or West side walk

cb 6.7 99.3

c 6.7 99.3

cb 6.1 99.6

E 6.3 99.7

Sect D

E 4.6 101.4

cb 4.4 101.6

106.0

CHATS WORTH BLVD

15

c	4.7	101.3
cb	4.7	101.3
W	4.6	101.4

Sect. E = R.O.

W	3.9	102.1
cb	4.1	101.9

c	3.9	102.1
---	-----	-------

cb	3.8	102.2
----	-----	-------

E	3.9	102.1
---	-----	-------

Sect F

E	1.0	105.0
---	-----	-------

cb	1.3	104.7
----	-----	-------

c	1.2	104.8
---	-----	-------

cb	1.1	104.6
----	-----	-------

W	1.4	104.6
---	-----	-------

T.P.	12.98	118.57
------	-------	--------

Sect G

W	10.4	108.2
---	------	-------

cb	10.5	108.1
----	------	-------

c	10.3	108.3
---	------	-------

cb	9.8	108.8
----	-----	-------

E	9.5	109.1
---	-----	-------

Sect H.

E	5.6	113.0
---	-----	-------

cb	6.1	112.5
----	-----	-------

c		6.8	111.8	
d		6.7	111.9	
W		6.5	112.1	
Sect J = E.C. of Curve on Voltaire				
W		2.2	116.4	
d		2.4	116.2	
c		2.5	116.1	
d		1.0	117.6	
E		0.7	117.9	
T.P.	12.63	121.12	0.08	118.49
Sect. J = E.C.				
E		10.8	120.3	
d		11.2	119.9	
c		12.2	118.9	
d		12.0	119.1	
W		12.0	119.1	
81.19' No = Sect K = E.C. of Curve on Voltaire				
W		8.7	121.4	
d		9.3	121.8	
c		8.9	122.2	
d		8.4	122.7	
E		8.0	123.1	
18.81' No of K = Sect L				
E		7.3	123.8	
d		7.7	123.4	
c		8.0	123.1	

d		8.1	122.7	
W		8.0	123.1	
50' No. of Sect L				
W		6.1	125.0	
d		6.0	125.1	
c		6.0	125.1	
d		5.8	125.3	
E		5.4	125.7	
100' No. of Sect. L				
E		3.7	127.4	
d		4.0	127.1	
c		4.0	127.1	
d		3.5	127.6	
W		3.3	127.8	
135' No. of Sect. L = P.C.				
W		1.9	129.2	
d		1.9	129.2	
c		2.5	128.6	
d		2.9	128.2	
E		2.6	128.5	
T.P.	12.99	143.98	0.13	130.99
Sect M				
E		12.9	131.1	
d		13.3	130.7	
c		12.9	131.1	

cb	12.3	131.7
W	12.0	132.0
Sect N		
W	9.5	134.5
cb	9.7	134.3
c	10.5	133.5
cb	10.6	133.4
E	10.2	133.7
Sect O		
E	7.7	136.3
cb	8.1	135.9
c	7.9	136.1
cb	7.2	136.8
W	6.9	137.1
Sect P		
W	4.3	139.7
cb	4.5	139.5
c	5.3	138.7
cb	5.4	138.6
E	5.0	139.0
Sect Q		
E	2.5	141.5
cb	2.8	141.2
c	2.7	141.3
cb	1.6	142.4
W	1.6	142.4

T.P.	12.65	156.40	0.23	143.75
Sect R = So Line Terrace Walk. <small>500' wide on West side of road.</small>				
W			11.4	145.0
cb			11.5	144.9
c			12.5	143.9
cb			12.6	143.8
E			12.3	144.1
No. Line Terrace Walk.				
E			9.7	146.7
cb			10.1	146.3
c			9.9	146.5
cb			9.0	147.4
W			8.6	147.8
Sect S				
W			6.2	150.2
cb			6.5	149.9
c			7.3	149.1
cb			7.6	148.8
E			7.1	149.3
Sect T				
E			4.6	151.8
cb			5.1	151.3
c			4.8	151.6
cb			4.1	152.3
W			3.9	152.5

156.40

sect U

W	1.5	154.9
dt	1.8	154.6
C	2.5	153.9
dt	2.7	153.7
E	2.4	154.0
T.P.	11.83	167.74
	0.49	155.91

sect V = EC

E	11.1	156.6
dt	11.3	156.2
C	11.30	156.4
dt	10.5	157.2
W	10.2	157.5

50' No. of sect V

W	8.2	159.5
dt	8.6	159.1
C	9.0	158.7
dt	9.2	158.5
E	8.8	158.9

100' No. of V

E	6.5	161.2
dt	6.8	160.9
C	6.9	160.8
dt	6.2	161.5
W	5.9	161.8

167.749. CHATSWORTH BLVD

18

125' No. of V

W	5.1	162.6
dt	5.4	162.3
C	6.0	161.7
dt	6.0	161.7
E	5.6	162.1

150' No. of V

E	4.6	163.1
dt	5.1	162.6
C	5.3	162.4
dt	4.9	163.0
W	4.4	163.3

175' No. of V

W	4.2	163.5
dt	4.5	163.2
C	4.8	162.9
dt	4.5	163.2
E	4.2	163.5

200' No. of V

E	3.8	163.9
dt	4.3	163.4
C	4.6	163.1
dt	4.3	163.4
W	3.8	163.9

225' No. of V

W	3.9	163.8'
cb	4.3	163.4'
C	4.5	163.2'
cb	4.1	163.6'
E	3.6	164.1'

250' No. of V

E	3.9	163.8'
cb	4.2	163.5'
C	4.5	163.2'
cb	4.6	163.1'
W	4.2	163.5'

300' No. of V

W	5.0	162.7'
cb	5.4	162.3'
C	5.0	162.7'
cb	4.7	163.0'
E	4.4	163.3'

350' No. of V

E	4.6	163.1'
cb	5.0	162.7'
C	5.5	162.2'
cb	5.6	162.1'
W	5.3	162.4'

370' No. of V = P.C

W	5.1	162.3'
cb	6.0	161.7'
C	5.7	162.0'
cb	5.3	162.4'
E	4.9	162.8'
47.58 on West } 57.83 on East } = Sect W = end of Curb. on west		
E	5.2	162.5'
cb	5.3	162.4'
C	6.2	161.5'
cb	6.15	161.59' on cement curb
TP.	2.34	163.90
	6.18	161.56 B.M.

Sect X

cb	2.6	161.3' on cement
C	2.6	161.3'
cb	2.0	161.9'
E	1.7	162.2'

Sect Y

E	1.7	162.2'
cb	2.1	161.8'
C	2.8	161.1'
cb	2.9	161.0' on cement

Sect Z

cb	3.3	160.6'
C	3.3	160.6'
cb	2.7	161.2'

E	24	161.5	
Sect AB = EC			
E	26	161.3	
cb	31	160.8	
C	37	160.2	
cb	36	160.3	on cement
50' No. of AB			
cb	40	159.9	on cement
C	40	159.9	
cb	34	160.5	
E	30	160.9	
100' No. of AB			
E	34	160.5	
cb	37	160.2	
C	43	159.6	
cb	44	159.5	on cement
127.83' No. = AC = EC on Alcott St			
cb	46	159.3	on cement
C	45	159.4	
cb	40	159.9	
E	36	160.3	
50' No. of AC ctr of Alcott			
E	37	160.2	
cb	42	159.7	
C	47	159.2	
cb	37	160.2	

W	31	160.8	
West end of Curve on So side Alcott			
W	25	161.4	
ctr of Alcott + 25' n. of Chatsworth			
	21	161.8	
West end of Curve on No. side Alcott			
W	25	161.4	
39.83' No. of ctr of Alcott = AD			
C	50	158.9	
cb	50	158.9	
E	44	159.5	
10.17' No. of AD = A.E.			
W	51	158.8	on cement
W	57	158.2	on
ctr of Browning			
E	67	157.2	
cb	65	157.4	
C	60	157.9	
cb	59	158.10	on cement
4' No. of ctr of Browning			
Wob.	60	157.9	on cement
17' No. of ctr of Browning			
Wob.	63	157.6	on cement
30' No. of ctr of Browning			
Wob.	67	157.2	on cement

60' No. of ctr of Bronning = Sect A.G.

Web	7.9	156.0	on cement.
C	8.0	155.9	
Ecb	8.0	155.9	on cement.

East end of Curve on Bronning

	8.0	155.9	on cement.
--	-----	-------	------------

Cement Curb - walk all in on both sides from Bronning North.  
150' No. of A.G. = A.H.

TP	210	153.04	12.91	150.99	
on BM			4.21	149.88	SE Curtis + City's north
Ecb			3.2	149.9	
C			3.5	149.6	
Web			3.1	150.0	

47' No. of A.H.

Web	4.9	148.2		
			ctr of Curtis	6.1

Web	5.3	147.8		5.6
C	5.1	147.7		
at line	6.0	147.1		
E	6.1	147.0		

2' No. of ctr of Curtis

Web	5.4	147.7		
-----	-----	-------	--	--

17' No. of ctr of Curtis

Web	5.6	147.5		
-----	-----	-------	--	--

60' No. of Ctr of Curtis = Sect A.I

Web	5.6	147.5		
e	6.0	147.1		
Ecb	6.4	146.7		

121.53' No. = Sect A.J

Web	4.9	148.2		
5.91' N. on curb into Curtis	4.6	148.5		
5.91' - of last	3.9	149.2		
5.91' - - -	3.1	150.0		
5.91' - - -	2.1	151.0		
5.91' - - -	1.0	152.1		
5.91' - - -	+ 0.1	153.2		

28.47' No. of A.I = A.K

Ecb	6.1	147.0		
End of curve So. side of Dumas	7.8	145.3		
- - - - No. - - -	9.2	143.9		

120' No. of A.K = A.L

E. ct	8.1	145.0		
-------	-----	-------	--	--

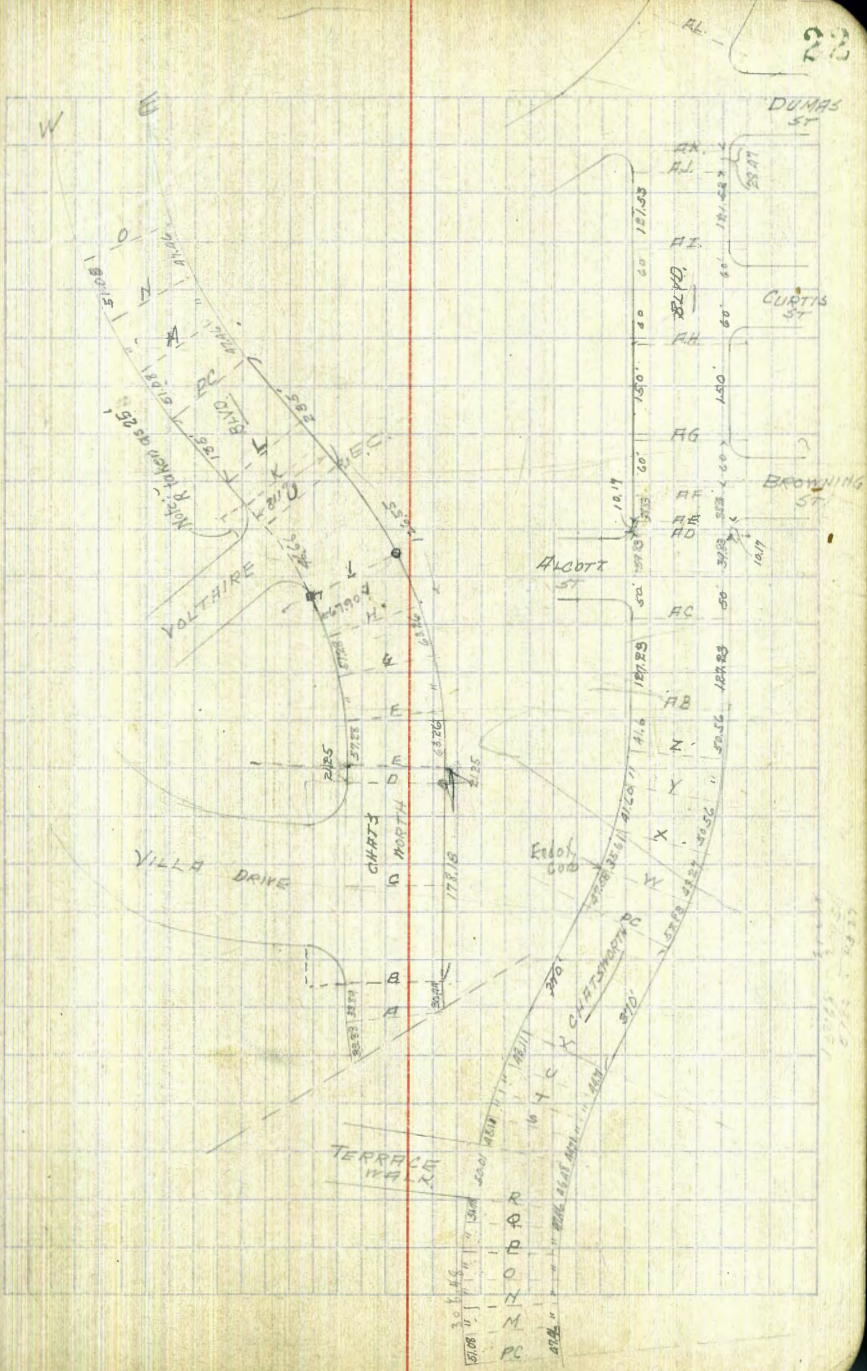
PRC on West

Web	6.7	146.4		
19.90 So. on curve into Curtis or West	6.1	147.0		
- - of 173'	5.6	147.5		
- - - -	4.8	148.3		
- - - -	3.7	149.4		
- - - -	2.1	151.0		
- - - -	0.1	153.0		

on Peab's Line

Feb	8.1	143.0
Eds	9.7	143.4

LL77





5/3/6

Gregory  
Moore  
MillerCROSS-SECTION OF (SEE SKETCH)  
VILLA DRIVE PAGE 25  
FROM VOLTTHIRE ST No.

## N. L. VOLTTHIRE ST = SECTION A

T.P.	1317	10 2.16	88.99
W		132	89.0
cb		108	91.4
1/4		76	94.6
C		48	97.4
1/4		14	100.8
T.P.	396	105.23	0.89
cb		26	102.6
E		18	103.4
		15.88 ON E 25.28 ON W from last Section	
E		16	103.6
cb		21	103.1
1/4		31	102.1
C		48	100.4
1/4		96	95.6
cb		144	90.8
W		193	85.9
+25		255	79.7
		21.68 ON E 25.29 ON W from last Section	
-30		322	73.0
-15		290	76.2
W		226	82.6
cb		176	87.6
1/4		129	92.3

1052

23

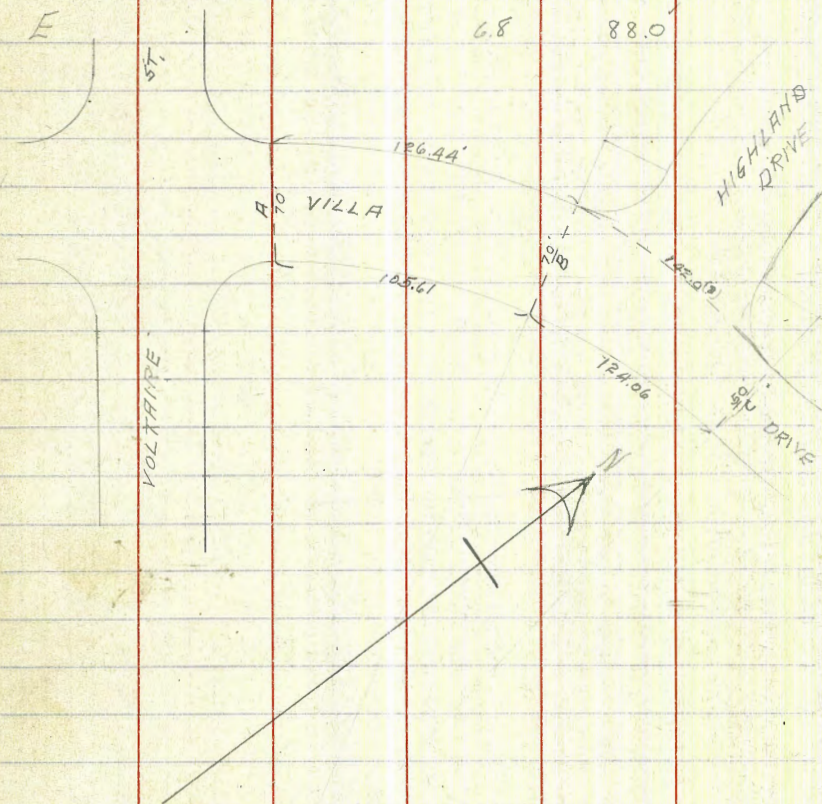
C	71	98.1
+5	49	100.3
1/4	40	101.2
cb	29	102.3
E	23	102.9
	21.68 ON E 25.29 ON W from last Section	
E	44	100.8
cb	57	99.5
1/4	74	97.8
C	133	91.9
1/4	183	86.9
cb	239	81.3
W	290	76.2
+25	380	67.2
+35	370	67.2
	21.69 ON E 25.29 ON W from last Section	
-20	319	73.3
W	390	66.2
cb	325	72.7
1/4	248	80.4
C	123	86.9
1/4	129	92.3
cb	92	96.0
E	80	97.2

21.68 on E from last Section = Section B  
25.29 on W

E		10.4	94.8'
T.P.	0.54	94.23	109.4
cb		4.5	90.3'
1/4		11.2	83.6'
C		15.7	79.1'
1/4		22.5	72.3'
+4		25.7	69.1'
+7		26.0	68.8'
cb		23.4	71.4'
W		15.6	76.2'
	24.81 on E from Sect B 28.4 on W		
W		8.6	86.2'
cb		11.7	83.1'
1/4		18.7	76.1'
+6		23.1	71.7'
+9		23.1	71.7'
+2.5 = C		19.5	75.3'
+11.5 = 1/4		12.2	82.6'
+11.5 = cb		5.0	89.8'
+10 = E		0.9	93.9'
	24.81 on E from last Section 28.4 on W		
E		3.5	91.3'
+10 = cb		7.6	87.2'
+10.5 = 1/4		13.3	81.5'
+7.5		12.7	77.1'
		20.3	74.5'

+3 = C		21.0	73.8'
+10.5 = 1/4		12.4	82.4'
+10.5 = cb		5.0	86.8'
+10 = W		3.1	91.7'
	24.82 on E from last Section 28.4 on W		
W		2.5	92.3'
+10 = cb		5.2	89.6'
+9.5 = 1/4		9.0	85.8'
+9.5 = C		13.3	81.5'
+9.5 = 1/4		16.2	78.6'
+4		16.9	77.9'
+9.5 = cb		12.4	82.4'
+10 = E		7.6	87.2'
	24.81 on E from last Section 28.4 on W		
E		10.2	84.6'
+10 = cb		13.3	81.5'
+5		13.2	81.6'
+9.5 = 1/4		12.2	84.6'
+9.5 = C		9.5	85.3'
+9.5 = 1/4		6.8	88.0'
+5.5 = cb		4.4	90.4'
+10 = W		2.1	92.7'
	24.81 on E from last Section = End of Curve 28.4 on W		
W		5.0	92.8'
cb		4.3	90.5'
1/4		6.5	88.3'

C	9.2	85.6
1/4	11.5	83.3
cb	11.6	83.2
E	6.8	88.0



Cross Section Alley, Block 783 Univ. Hgts.  
Between Ohio + Illinois From N. Univ. to S. Lincoln

20' Wide

SPRING  
UNIVERSITY  
LAND

BM	717	863.67	356.50
TP	594	362.90	356.96
		0.0 = 1 Line University Ave.	
E	Top Pavng	5.83	357.07
Z	" "	6.18	356.78
N	" "	6.00	356.90
		10' N	
N		5.4	357.5
Z		5.4	357.5
17		5.5	357.4
E		5.3	357.6
		50' N	
E		4.6	358.3
12		5.0	357.9
Z		4.9	358.0
13		5.2	357.7
N		5.2	357.7
		90' N	
N		5.0	357.9
Z		4.7	358.2
19.5	Garage Area	4.54	358.36
E		4.5	358.4
15.5	Garage Conc. Floor	4.52	358.37
		100' N	
E		4.7	358.2

Plotted  
Sept 21-  
1977

9-21-76  
5:55 PM  
9/25/76  
Northward

26

362.90

Z		4.9	358.2
N		4.6	358.3
		133' N	
N	Conc. Drive Lumber	4.5	358.4
Z	" "	4.2	358.7
E		4.4	358.5
		150' N	
E		4.1	358.5
13		4.6	358.3
Z		4.6	358.3
N		4.3	358.6
		170' N	
N	Conc. Drive Lumber	4.57	358.33
13	" "	4.5	358.4
16		4.3	358.6
Z		4.2	358.7
17		4.1	358.5
E		4.0	358.9
		190' N	
-5	Garage Dr. Floor	3.7	359.2
E		4.0	358.9
Z		4.6	358.3
N		4.1	358.8
		210' N	
N		4.0	358.9

	362.9		
E		40	358.9
E		39	359.0
	215 W		
E		38	359.1
E		37	359.2
N		35	359.4
TP	460	364.68	2.82 360.08 ✓
	270 W		
N	Center 30' Deck Planning Mill Conc Floor	514	359.54
E		49	359.8
E		50	359.7
	300 W		
E		46	360.1
E		52	359.5 <sup>309'</sup>
N		48	359.7 <sup>Garage on floor GREEN 115</sup>
	355 W		
N		41	360.6
E		41	360.6
E	Conc Apron	416	360.52
+1	Garage Conc Floor	404	360.64
	382 W		
E		39	360.8
+4		42	360.5
E		38	360.9
N		40	360.7
+1.5	Driverhood Floor	390	360.8

Plotted  
scope 215 W  
Larry

	400 W		
N		38	360.9
E		43	360.6
E		40	360.7
TP	702	367.45	4.85 360.43 ✓
	415 W		
E		65	361.0
E		66	360.9
N		66	360.9
+3	Driverhood Floor	625	361.2
	457 W		
N		62	361.3
+1	Garage Dir Floor	62	361.3 <sup>Garage on W side of block</sup>
E		62	361.3
E		60	361.5
	492		
+2	Garage Conc Floor	54	361.1
E		56	361.9
+3		60	361.5
E		57	361.8
N		59	361.6
	505		
N		58	361.7
+7		59	361.4
E		56	361.9
+5		56	361.9
E		52	362.2

Cross Section Alley  
Block 208 36745

28

535' N

-2 Garage 2nd Floor 55 367.0

E 55 367.0

± 56 361.9

N 56 361.9

557' N

N 48 362.7

± 51 362.4

E.L. Conc Apron 51 362.4

115 Can Do Garage  
Anchor

570' N

E 50 362.5

± 47 362.8

N 47 362.8

591' N - 36 inch concrete

N Top Curb 40 362.85

Gutter 52 362.3

+7 53 632.2

± 48 362.7

Gutter 53 362.7

E Top Curb 47 362.64

B.M. 535 362.10

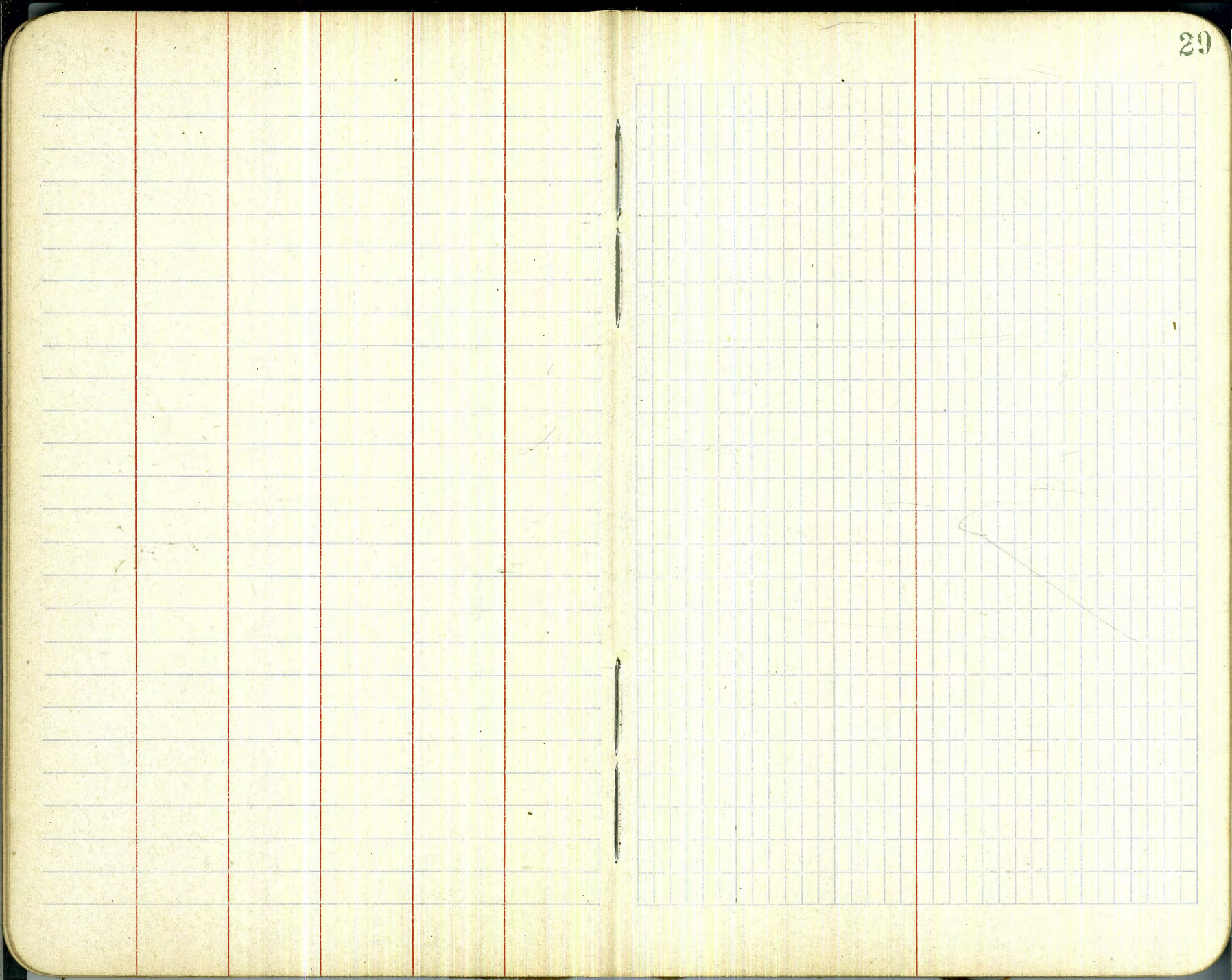
SE. Linden  
+ Ohio

T.P. 334 364.03 676 360.69

T.P. 655 707 356.96

N.H. Cor  
adv. for  
362.5

B.M. 708 356.49

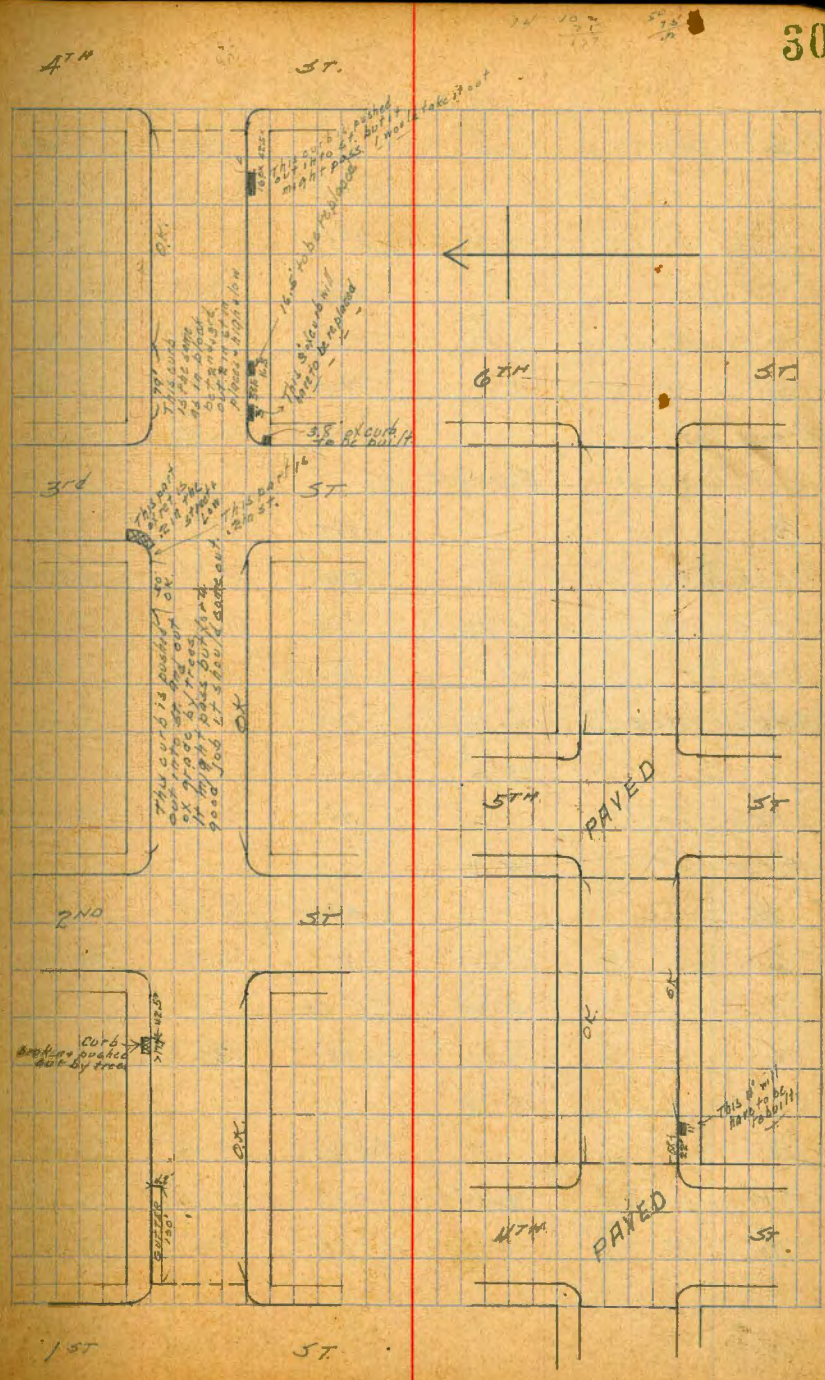


Gregory  
Moore  
Miller

Levels on Curb on  
Laurel Street from  
EL 1st to W.L. 6th  
xor paving

Elvs. of curb  
shown by

BM.	1016	232.16	222.0	Elvs. with shown by 11th 1st Laurel
EL. 1st St				
No.		8.21	23.95	24.00
So.		9.26	22.90	23.00
25' E				
So.		8.47	23.69	23.75
No.		7.70	24.46	24.63
50' E				
No.		7.09	25.07	25.25
So.		7.70	24.46	24.50
75' E				
So.		6.07	25.19	25.25
No.		6.42	25.74	25.88
100' E				
No.		5.69	26.47	26.50
So.		6.25	25.91	26.00
125' E				
So.		5.51	26.65	26.75
No.		4.86	27.30	27.38
140' E = West end of Bad Curb				
No.		4.35	27.81	27.90
150' E				
No.		3.95	28.21	28.25
So.		4.23	27.43	27.50
157.5' E = East end of Bad Curb				
No.		3.70	28.46	28.51





232.16

125' E

So		40	28.16	28.25
No		312	29.02	29.13

300' E = K.L. End

No		225	29.91	30.00
Around Ref.		224	29.92	30.00
So		324	28.92	29.00
Around Ref.		327	28.89	29.00

E.L. 2nd St.

So		217	29.99	30.00
Around Ref.		221	29.95	30.00
No		0.90	31.26	31.00
Around Ref.		110	31.06	31.00
Half Way Around Ref.		120	30.96	31.00

8' E

No		.90	31.26	31.26
----	--	-----	-------	-------

25' E

No		0.95	31.81	31.81
So		1.37	30.79	30.81

39' E

No		± 0.22	<del>32.38</del>	32.27
----	--	--------	------------------	-------

50' E

So		0.53	31.63	31.63
----	--	------	-------	-------

T.P.	9.14	240.63	0.67	231.49
------	------	--------	------	--------

No		8.03	32.60	32.63
----	--	------	-------	-------

240.63

63' E

No		760	233.03	33.05
----	--	-----	--------	-------

72.7' E

No		707	33.56	33.36
----	--	-----	-------	-------

75' E

No		204	33.59	33.44
----	--	-----	-------	-------

So		821	32.41	32.44
----	--	-----	-------	-------

83' E

No		692	33.71	33.70
----	--	-----	-------	-------

100' E

So		741	33.22	33.25
----	--	-----	-------	-------

No		622	34.41	34.25
----	--	-----	-------	-------

112' E

No		603	34.60	34.64
----	--	-----	-------	-------

125' E

No		557	35.06	35.06
----	--	-----	-------	-------

So		670	33.93	34.06
----	--	-----	-------	-------

135' E

No		530	35.33	35.39
----	--	-----	-------	-------

150' E

So		584	34.79	34.88
----	--	-----	-------	-------

No		479	35.84	35.88
----	--	-----	-------	-------

175' E

No		402	36.61	36.69
----	--	-----	-------	-------

So		504	35.59	35.69
----	--	-----	-------	-------

31

200' E = N.L. 3rd St

So.		4.25	236.38	236.50
Around Ref		4.30	36.33	36.50
No.		3.19	37.44	37.50
92' Around Ref		3.31	37.32	37.50
Around Ref.		3.35	37.28	37.50

E.L. 3rd St.

No.		3.12	37.51	37.50
Around Ref		3.17	37.46	37.50
So.		4.10	36.53	36.50
9' from ✓ Around Ref		4.33	36.30	36.50
		4.30	36.33	36.50

T.P.	7.90	245.21	3.32	237.51
------	------	--------	------	--------

So.		7.58	36.63	36.57
No.		7.65	37.56	37.58

So.		8.60	36.61	36.64
-----	--	------	-------	-------

No.		7.38	37.83	37.75
-----	--	------	-------	-------

No.		7.25	37.96	37.93
-----	--	------	-------	-------

So.		8.30	36.91	37.06
-----	--	------	-------	-------

No.		7.09	38.12	38.13
-----	--	------	-------	-------

No.		6.78	38.43	38.38
-----	--	------	-------	-------

So.		7.90	37.31	37.43
-----	--	------	-------	-------

50' E

No.		6.57	238.64	38.75
So.	58' E	7.51	37.70	37.81
So.	60' E	7.46	37.75	37.81
No.		6.27	38.94	39.00
No.	75' E	6.00	39.21	39.38
So.		7.10	38.11	38.19
No.	79' E	5.85	39.36	39.48
So.	100' E	6.56	38.65	38.75
No.		5.30	39.91	40.00
No.	125' E	4.78	40.43	40.63
No.		6.05	39.16	39.31
So.	141.5' E	5.58	39.63	39.68
So.	150' E	5.27	39.94	39.88
No.		4.05	41.16	41.25
So.	157.5' E	5.22	39.99	40.04
No.	175' E	3.45	41.76	41.88
So.		4.65	40.56	40.44

245.21

N.L. 4<sup>th</sup> St (Paved)

So		4.25	240.96	41.00
No		2.80	42.31	42.50
B.M.	10.85	253.36	2.68	<del>242.53</del> = 51.89
	E.L. 4 <sup>th</sup>			
So		11.44	41.92	42.00
No		9.85	43.51	43.50
	22' E			
So		10.76	42.60	42.77
	25' E			
No		9.14	44.22	44.31
So		9.96	43.40	42.88
	33' E			
So		10.22	43.14	43.16
	50' E			
So		9.72	43.64	43.75
No		8.38	44.98	45.13
	75' E			
No		7.50	45.86	45.94
So		8.83	44.53	44.63
	100' E			
So		8.0	45.36	45.50
No		6.77	46.59	46.75
	125' E			
No		5.88	47.48	47.56
So		7.08	46.28	46.38

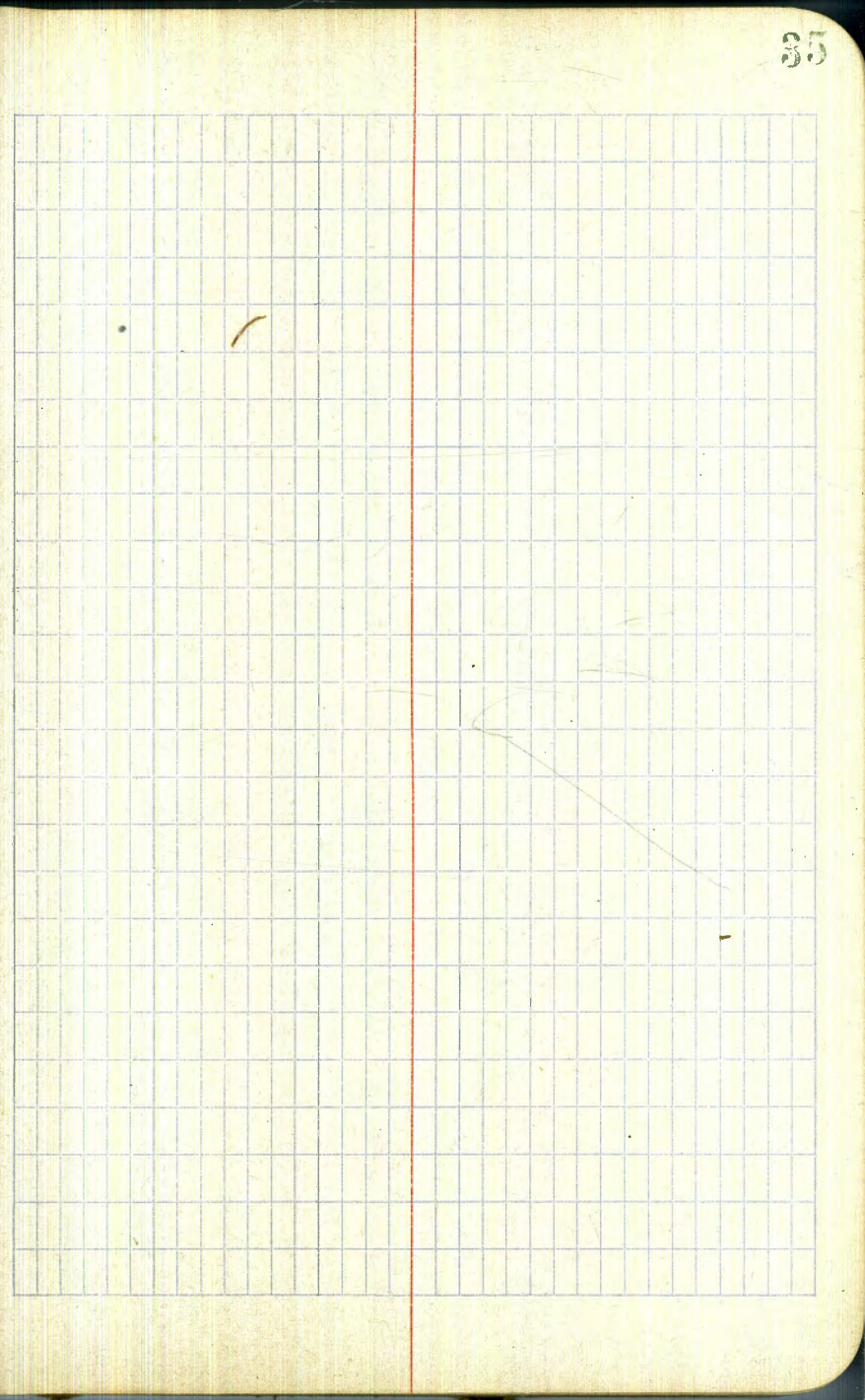
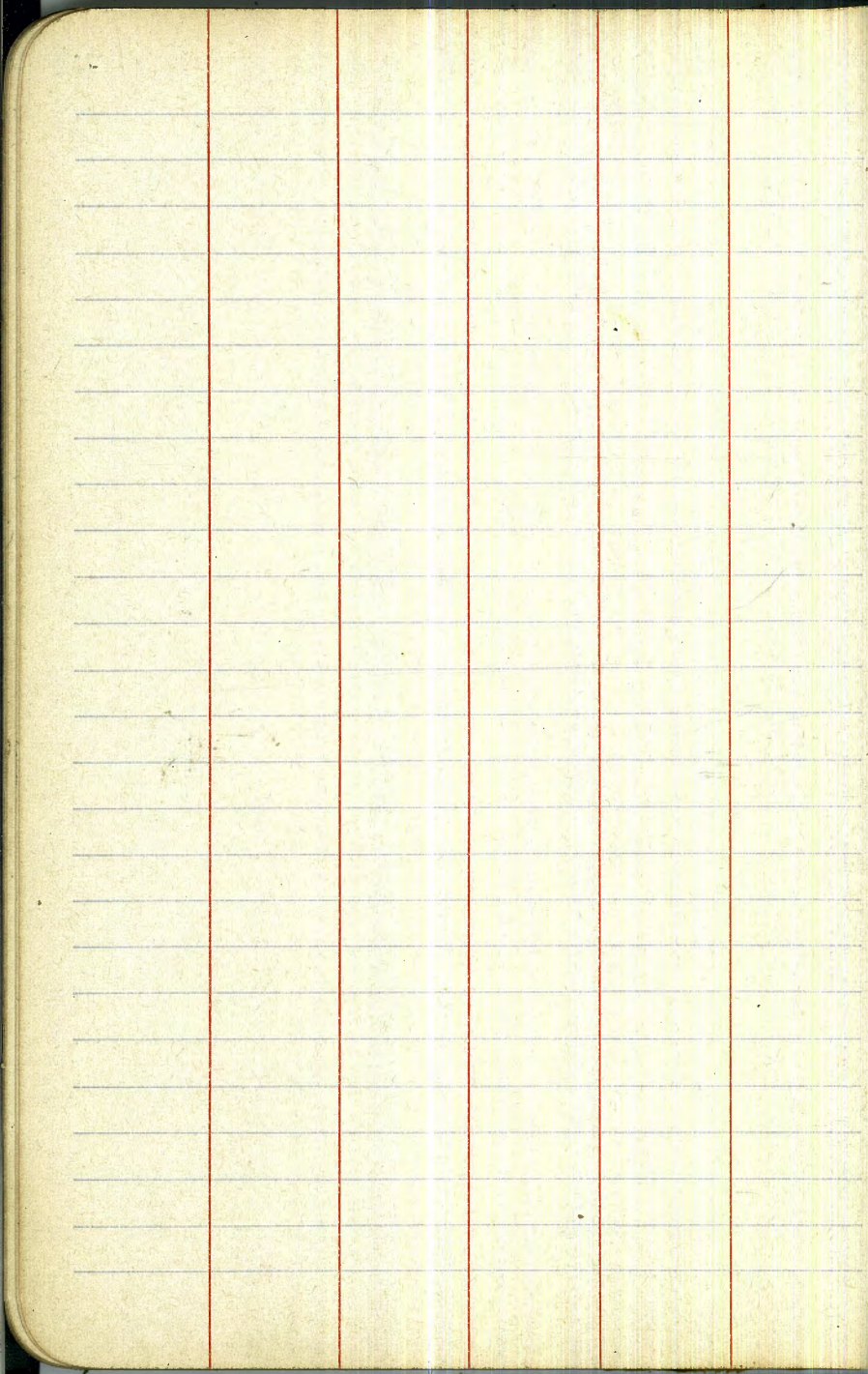
253.36

150' E

33

So		6.25	247.11	47.25
No		5.15	48.21	48.38
	175' E			
No		4.33	49.03	49.19
So		5.40	47.96	48.13
	200' E = N.L. 5 <sup>th</sup> St (Paved)			
So		4.43	48.93	49.00
No		3.54	49.82	50.00
	E.L. 5 <sup>th</sup> St			
No		2.45	50.91	51.00
So		3.49	49.87	50.00
	25' E			
So		3.40	49.93	50.14
No		2.35	51.01	51.14
	50' E			
No		2.18	51.18	51.28
So		3.23	50.13	50.28
	75' E			
So		3.08	50.28	50.42
No		2.02	51.34	51.42
	100' E			
No		1.94	51.42	51.55
So		2.91	50.45	50.55
	125' E			
So		2.83	50.53	50.69

No.		1.80	251.56	51.69
	150' E			
No.		1.65	51.71	51.83
So		2.66	50.70	50.23
	175' E			
So		2.52	50.84	50.97
No.		1.54	51.82	51.97
	180.5 E = 141.6 <sup>th</sup> SE			
No.		1.50	51.86	52.00
So		2.48	50.88	51.00
BM		3.18	249.88 = 141.5 <sup>th</sup> ↓ Level .95	



10/19/6  
Granger  
Massey  
Miller

CROSS-SECTION OF  
VOLTAIRE ST.  
from the West Line of Point Loma Villas  
to East San Clemente St.

70.11/66  
12.2 1/2

Sr. Tennison  
& Chatsworth

BM	3.51	10.016	96.65
T.P.	0.47	88.09	12.54
		West Line Pt Loma Villas	
N		11.8	76.3
cl		11.1	77.0
1/2		11.2	76.9
C		11.7	76.4
1/2		12.8	75.3
cl		13.9	74.2
S		16.1	72.0
+30		19.5	68.6
		5' W	
-30		21.3	66.8
S		17.8	70.3
cl		16.2	71.9
1/2		14.0	74.1
C		13.2	74.9
1/2		12.8	75.3
cl		13.0	75.1
N		13.6	74.5
+20		14.9	73.2
T.P.	0.53	76.18	12.11
		25' W	
-30		10.7	66.1
N		10.1	66.1

From page 13 (76.2)

VOLTAIRE

36

cl		9.9	66.3
1/2		9.2	66.8
C		9.0	67.2
1/2		9.3	66.9
cl		9.5	66.7
S		9.7	66.5
+30		12.9	63.3
+40		13.2	63.0
		45' W	
T.P.	2.28	66.51	11.95
-45		4.9	61.6
-30		5.7	60.8
S		6.2	60.3
cl		5.8	60.7
1/2		5.9	60.6
C		5.9	60.6
1/2		5.8	60.7
cl		6.0	60.5
N		6.1	60.4
+30		6.5	59.7
		58' W	
-40		8.7	57.8
-30		10.0	56.5
N		10.2	56.3
cl		9.8	56.7

66.51

1/4		9.1	57.4
C		9.7	56.8
1/4		8.5	58.0
cb		6.8	59.7
S		6.5	60.0
+30		5.0	61.5
+45		3.8	62.7
	64' W		
-45		9.6	62.9
S		6.6	59.9
cb		10.1	56.9
1/4		10.9	55.6
C		11.5	55.0
1/4		11.9	54.6
cb		10.2	56.3
N		10.6	55.9
+30		10.9	55.6
+40		9.0	57.5
	73' W		
-40		9.7	56.8
-25		11.6	54.9
-10		11.5	55.0
N		12.6	53.9
cb		11.5	55.0
1/4		8.9	57.6
C		7.5	59.0

66.5

VOUTAIRE

37

1/4		7.2	59.3
cb		6.4	60.1
S		5.5	61.0
+15		4.0	62.5
+40		3.1	63.4
	85' W		
-30		2.4	64.1
S		3.9	62.6
cb		4.7	61.8
1/4		5.4	61.1
C		5.5	61.0
1/4		7.3	59.2
cb		8.4	58.1
N		9.0	57.5
+15		12.2	54.3
+40		13.0	53.5
+60		12.6	53.9
	100' W		
-60		13.6	52.9
-40		13.3	53.2
-20		11.6	54.9
N		7.9	58.6
cb		6.5	60.0
1/4		4.9	61.6
C		3.5	63.0

(66.51)

1/4			2.7	63.8
ob			2.0	64.5
S			1.6	65.1
+30			0.0	66.5
T.P.	11.58	76.91	1.18	65.33
		125' W		
-20			5.2	71.7
S			5.7	71.2
ob			7.0	69.9
1/4			8.3	68.6
C			9.3	67.6
1/4			10.8	66.1
ob			12.9	64.0
N			15.0	61.9
+15			18.7	58.2
+30			20.7	56.2
+45			22.5	54.6
		150' W		
-30			17.8	59.1
-15			16.0	60.9
N			11.3	65.6
ob			8.7	68.2
1/4			5.7	71.2
C			4.3	70.6
1/4			3.8	73.7
ob			1.3	75.6

VOLTAIRE

38

T.P.	11.42	88.01	0.32	76.59
S			11.1	76.9
+15			10.7	77.3
		175' W		
-15			6.2	81.8
S			6.8	81.2
ob			7.1	80.9
1/4			9.8	78.2
C			11.2	76.8
1/4			12.6	75.4
ob			15.9	72.1
N			20.6	67.4
+15			23.4	64.6
+25			24.0	64.0
		260' W		
-20			17.8	70.2
N			15.9	72.1
ob			13.8	74.2
1/4			10.4	77.6
C			6.5	81.5
1/4			4.5	83.7
ob			2.6	85.4
S			2.1	85.9
T.P.	10.80	92.04	0.77	89.24



98.04

225' W

S	86	89.4
cb	92	88.8
1/4	98	88.2
C	112	86.8
1/4	141	83.9
cb	170	81.0
N	186	79.4
±15	188	79.2

250' W

-10	126	85.4
N	117	86.3
cb	104	87.6
1/4	88	89.2
C	80	90.0
1/4	72	90.8
cb	67	91.3
S	65	91.5

260' W

S	57	92.3
cb	60	92.0
1/4	66	91.4
C	69	91.1
1/4	77	90.3
cb	81	89.9
N	87	89.3

98.0

VOLTAIRE

39

270' W = E. L. Warrington St. 50' wide

N	7.0	91.0
cb	67	91.3
1/4	66	91.4
C	62	91.8
1/4	59	92.1
cb	54	92.6
S	48	93.2
E. Curb		
S	42	93.8
cb	47	93.3
1/4	50	93.0
C	56	92.4
1/4	52	92.8
cb	56	92.4
N	59	92.1
E. Quarter		
N	5.1	92.9
cb	4.8	93.2
1/4	4.5	93.7
C	4.7	93.3
1/4	4.5	93.5
cb	4.0	94.0
S	3.5	94.5
Center		
S	3.1	94.9

cb	31	94.9
1/4	36	94.4
C	43	93.7
1/4	42	93.8
cb	41	93.9
N	45	93.5

## N. Quarter

N	41	93.9
cb	39	94.1
1/4	38	94.2
C	39	94.1
1/4	30	95.0
cb	28	95.2
S	28	95.2

## N. Curb

S	28	95.2
cb	27	95.3
1/4	23	95.7
C	36	94.4
1/4	36	94.4
cb	37	94.3
N	39	94.1

## N. Line Washington St.

N	37	94.3
cb	33	94.7
1/4	31	94.9

C	3.0	95.0
1/4	2.4	95.6
cb	2.2	95.8
S	2.0	96.0

## 25' W

S	0.7	97.3
cb	0.5	97.5
1/4	1.2	96.6
C	1.9	96.1
1/4	2.5	95.5
cb	2.2	95.6
N	2.6	95.4

## 50' W

N	1.9	96.1
cb	1.9	96.1
1/4	1.5	96.5
C	1.5	96.5
1/4	0.7	97.3
TP	10.90	107.90
cb	10.1	97.8
S	9.9	98.0

## 75' W

S	10.1	97.8
cb	10.4	97.8
1/4	10.5	97.6

107.90

c	10.3	97.6
1/4	10.7	97.2
cb	11.0	96.9
N	11.1	96.8
100' W		
N	9.6	98.3
cb	9.2	98.7
1/4	9.4	98.5
c	9.3	98.6
1/4	9.6	98.3
cb	9.4	98.5
S	9.5	98.4
125' W		
S	8.8	99.1
cb	8.7	99.2
1/4	8.6	99.3
c	8.2	99.7
1/4	8.6	99.3
cb	8.4	99.5
N	8.3	99.6
150' W		
N	6.2	101.7
cb	6.5	101.4
1/4	6.6	101.3
c	7.0	100.9
1/4	7.1	100.8

107.90

VOLTAIRE

41

cb	7.7	100.2
S	7.9	100.0
175' W		
S	6.9	101.0
cb	6.7	101.2
1/4	5.8	102.1
c	5.6	102.3
1/4	5.4	102.5
cb	4.5	103.4
N	4.3	103.6
200' W		
N	2.8	105.1
cb	3.2	104.7
1/4	4.0	103.9
c	4.1	103.8
1/4	4.7	103.7
cb	5.0	102.9
S	5.5	102.4
225' W		
S	5.2	102.7
cb	4.7	103.2
1/4	4.2	103.7
c	3.5	104.4
1/4	3.2	104.7
cb	2.2	105.7

107.90

N			116	1063
T.P	402	108.71	3.21	104.69
		250 W		
N			23	106.4
db			25	105.9
1/4			37	105.0
c			41	104.6
1/4			47	104.0
db			51	103.6
S			57	103.0
		275 W		
S			59	102.8
db			50	103.7
1/4			45	104.2
c			40	104.7
1/4			36	105.1
db			35	105.2
+1			26	106.1
N			21	106.6
		300 W = E.L. Warden St 50' m. da		
N			20	106.7
+6			21	106.6
+7			3.4	105.3
db			3.5	105.2
1/4			37	105.0
c			44	104.3

108.7

VOLTAIRE

42

1/4			51	103.6
db			58	102.9
S			63	102.4
		E. Corb		
S			66	102.1
db			61	102.6
1/4			57	103.0
+10			53	103.4
c			44	104.3
1/4			38	104.9
db			37	105.0
+5			3.5	105.2
N			23	106.4
		E. Quarter		
N			39	104.8
db			39	104.8
1/4			39	104.8
+9			40	104.7
c			55	103.2
1/4			62	102.5
db			67	102.0
S			71	101.6
		Center		
S			9.8	100.9
db			74	101.3

1/4	6.8	101.9
C	6.2	102.5
+8	4.2	104.3
1/4	4.2	104.5
cb	4.1	104.6
N	4.1	104.6

W. Quarter

N	4.1	104.6
cb	4.1	104.6
1/4	4.2	104.5
C	6.5	102.2
1/4	7.2	101.5
cb	8.0	100.7
S	8.2	100.5

W. Curb

S	8.6	100.1
cb	8.3	100.4
1/4	7.4	101.3
C	6.8	101.9
1/4	5.5	103.2
+7	4.5	104.2
cb	4.3	104.4
N	4.1	104.6

W.L. Korden St.

N	6.40	102.31	on Ave
cb	7.3	101.4	

1/4	7.5	100.9
C	7.6	101.1
1/4	8.0	100.7
cb	9.0	99.7
S	9.3	99.4

25' W

S	12.4	96.3
cb	12.6	96.1
1/2	12.0	96.7
C	11.8	96.9
1/4	11.5	97.2
cb	10.5	98.2
N	9.6	99.1

50' W

N	12.8	95.8		
T.P.	0.61	96.65	12.67	96.04
cb	1.5	95.1		
1/4	2.0	94.6		
C	2.4	94.2		
1/2	2.8	93.8		
cb	3.2	93.4		
S	3.7	93.0		

75' W

S	7.5	89.2
cb	6.7	90.0

1/4	56	91.0
C	50	91.6
1/4	45	92.1
cl	39	92.7
N	37	93.0
100' W		
N	67	90.0
cl	70	89.6
1/4	73	89.3
C	79	89.7
1/4	87	88.0
cl	96	87.0
S	103	86.3
125' W		
S	123	84.3
cl	117	85.0
1/4	111	85.5
C	106	86.0
1/4	101	86.5
cl	97	87.0
N	91	87.5
150' W		
N	109	85.7
cl	109	85.7
1/4	113	85.3
C	122	84.4

TP	100	85.80	12.45	84.20
1/4			23	83.5
cl			30	82.8
S			36	82.2
175' W				
S			80	77.8
cl			65	79.3
1/4			49	80.9
C			35	82.3
1/4			25	83.0
cl			23	83.5
N			22	83.6
200' W				
N			51	80.7
cl			56	80.2
1/4			61	79.7
C			78	78.0
1/4			104	75.4
cl			118	74.0
S			123	73.5
225' W				
S			145	71.3
cl			141	71.7
1/4			135	72.3
C			122	73.6

85.80

1/4			10.6	75.2
cb			9.0	76.8
N			8.1	77.7
		250' W		
N			11.6	74.2
cb			12.2	73.6
1/4			12.6	73.2
T.P.	0.54	73.85'	12.44	73.31'
C			1.2	72.6
1/4			2.5	71.3
cb			4.5	69.3
S			5.2	68.6
+10			5.5	68.3
		275' W		
-10			7.1	66.7
S			6.8	67.0
cb			6.2	67.6
1/4			3.8	70.0
C			2.1	71.7
1/4			1.6	72.2
cb			1.6	72.2
N			1.7	72.1
		300' W = E.L. Wells St 50' wide		
N			2.7	71.2
cb			2.6	71.2
1/4			2.6	71.2

738

VOLTAIRE

45

C			3.0	70.8
1/4			4.8	69.0
cb			7.0	66.8
S			8.0	65.8
+10			8.6	65.2
		E. Curb		
-10			9.1	64.4
S			8.2	65.6
cb			7.1	66.7
1/4			5.1	68.4
C			3.1	70.4
1/4			2.9	70.9
cb			2.9	70.9
N			3.0	70.8
		E. Quarter		
N			3.2	70.6
cb			3.3	70.5
1/4			3.3	70.5
C			4.8	69.0
1/4			6.7	67.1
cb			8.0	65.8
S			8.8	65.0
+10			9.9	63.9

## Center

-10	10.8	63.0
S	9.8	64.0
cb	8.2	65.6
1/4	7.2	66.6
C	5.7	68.1
1/4	3.7	70.1
cb	3.6	70.2
N	3.6	70.2

## W Quarter

N	3.9	70.0
cb	3.8	70.0
1/4	4.1	69.7
C	6.1	67.7
1/4	7.4	66.4
cb	8.9	65.0
S	10.6	63.2
+15	11.9	62.0

## W Curb

-15	12.6	61.2
S	10.7	63.1
cb	9.3	64.5
1/4	7.4	66.4
C	5.7	68.1
1/4	4.1	69.7
cb	3.8	70.0

N	4.0	69.8
W.L. Wells St		
N	4.8	69.97 on hub
cb	4.0	69.8
1/4	4.5	69.3
C	5.8	68.0
1/4	7.9	65.9
cb	9.5	64.3
S	10.8	63.0
+15	13.4	60.4
10' W		
-15	14.2	59.6
S	11.3	62.5
cb	10.1	63.7
1/4	8.9	64.9
C	2.6	66.2
1/4	4.9	68.9
cb	4.4	69.4
N	4.7	69.1
25' W		
N	5.1	68.7
cb	4.9	68.9
1/4	6.3	67.5
C	9.0	64.8
1/4	10.7	63.1



73.85

dt			11.8	62.0
S			13.9	60.0
+30			19.3	54.5
		50' W		
-30			21.6	52.2
S			17.6	56.2
dt			14.8	59.0
1/4			12.3	61.5
C			10.3	63.5
1/4			7.5	66.3
dt			5.5	68.3
N			5.7	68.1
		60' W		
N			6.4	67.4
dt			6.5	67.3
1/4			8.7	65.1
C			10.8	63.0
1/4			12.6	61.2
TP	1.45	62.83	12.47	61.38
dt			4.4	58.4
S			8.2	54.6
+30			12.3	50.5
		75' W		
-40			15.2	47.6
-30			14.9	47.9
S			10.6	52.2

628

VOLTAIRE

47

dt			7.7	55.1
1/4			4.8	58.0
C			1.9	60.9
1/4			0.5	62.3
dt			+0.4	63.2
N			+0.6	63.4
		85' W		
N			2.0	60.8
dt			2.4	60.4
1/4			3.0	59.8
C			4.2	57.9
1/4			7.3	55.5
dt			10.8	52.0
S			12.6	50.2
+35			15.8	47.0
+40			14.6	48.2
		110' W		
-40			12.0	50.8
-10			16.6	46.2
S			17.1	45.7
dt			15.8	47.0
1/4			14.2	48.6
C			12.7	50.1
1/4			10.6	52.2
dt			7.1	55.7

62.23

N			5.5	57.3
+ 15°			5.9	56.9
-15		130' W	9.6	53.2
N			11.8	51.0
df			12.8	50.0
T.P.	409	54.12	12.70	50.3
1/4			5.8	48.3
C			6.8	47.3
1/4			8.1	46.0
+8			9.0	45.1
df			8.9	45.2
S			8.0	46.1
+30			3.7	50.4
		150' W		
-30			0.2	53.9
-15			4.5	49.6
S			6.0	48.1
df			7.9	46.2
+7			9.4	44.7
1/4			9.8	44.3
C			9.8	44.3
1/4			8.9	45.2
df			6.9	47.2
N			5.8	48.3
+20			1.6	52.5
		175' W		
-30			8.1	46.0

54.1

VOLTAIRE

48

-15			10.2	43.9
N			11.3	42.8
df			11.6	42.5
1/4			11.0	43.1
C			9.4	44.7
1/4			7.2	46.9
df			5.2	48.9
S			3.3	50.8
+15			0.0	54.1
+25			+3.3	57.4
		200' W		
-15			+4.0	58.1
S			+6.1	54.2
df			2.3	51.8
1/4			5.9	48.4
C			7.8	46.3
1/4			10.2	43.9
df			11.6	42.5
N			12.0	42.1
+10			12.0	42.1
+30			10.4	43.7
+40			9.2	44.9
		225' W		
-45			13.6	40.5
-25			13.4	40.9

54.12

N			10.9	43.2
db			8.2	45.7
1/2			5.6	48.5
C			2.2	51.7
T.P.	11.36	65.14	0.34	52.78
1/2			9.6	55.5
db			5.9	59.2
S			2.8	62.3
+10			0.3	64.8
T.P.	11.66	74.57	2.23	62.91
		240' W		
-10			4.0	70.6
S			8.3	66.3
db			11.2	63.2
1/2			15.0	59.6
C			19.5	55.1
1/2			22.2	52.4
db			25.6	49.0
N			28.9	45.7
+15			31.1	43.5
+40			33.6	41.0
+50			34.4	40.2
		252' W		
-50			34.5	40.3
-20			31.2	43.4
N			26.6	48.0

74.6

VOLTAIRE

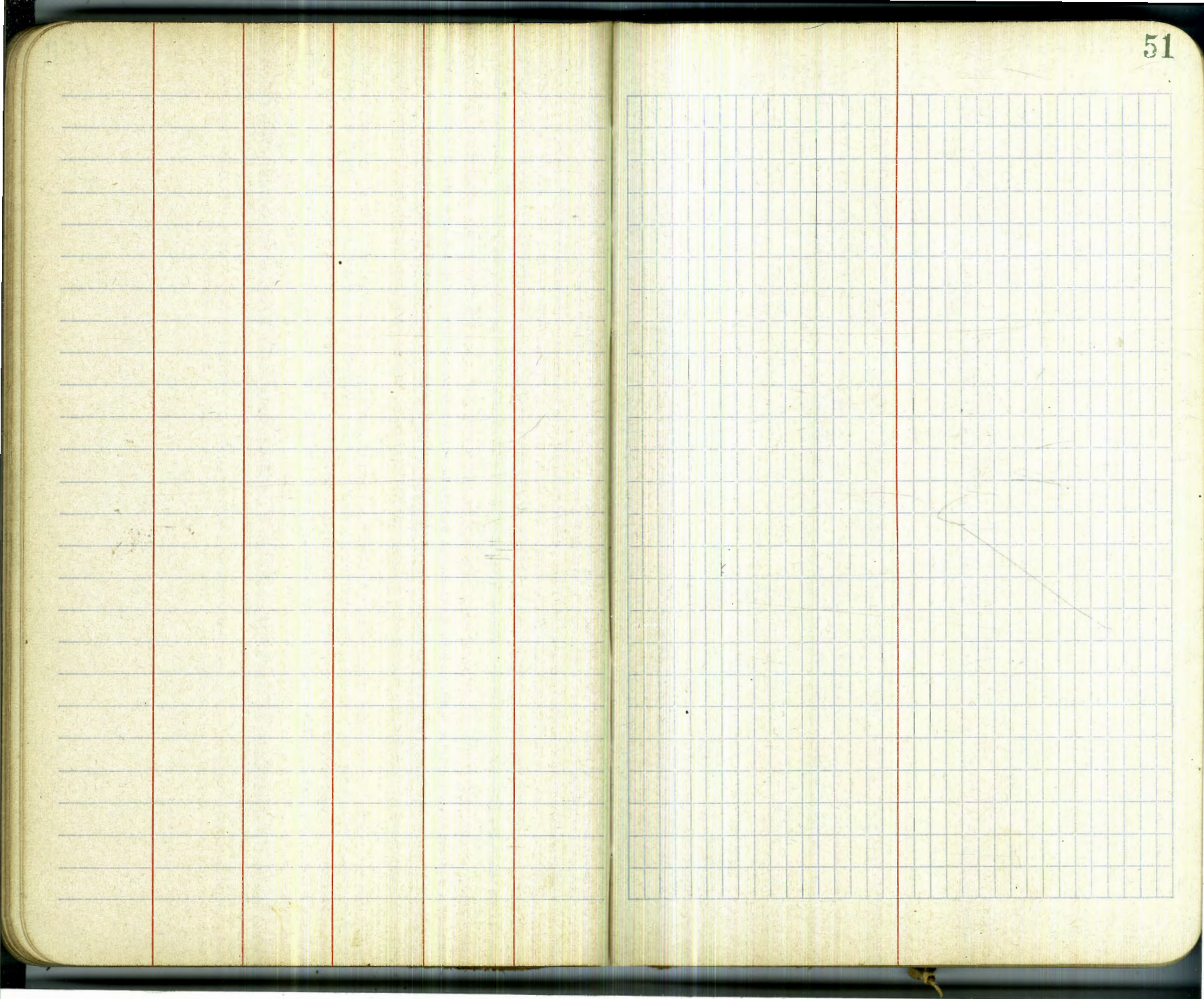
49

db			23.7	50.9
1/2			20.6	54.0
C			17.0	57.6
1/2			15.0	62.6
db			8.1	66.5
S			2.6	72.0
		275' W		
S			2.2	72.4
db			2.7	71.9
+3			3.2	71.2
1/2			8.2	66.4
C			11.0	63.6
1/2			14.5	60.1
db			17.7	56.9
N			20.1	54.5
+30			25.5	49.1
+40			29.0	45.6
		300' W		
-25			16.5	58.1
N			12.2	62.4
db			10.0	64.6
1/2			4.9	66.7
C			6.0	68.6
1/2			2.6	72.0
db			2.4	72.2

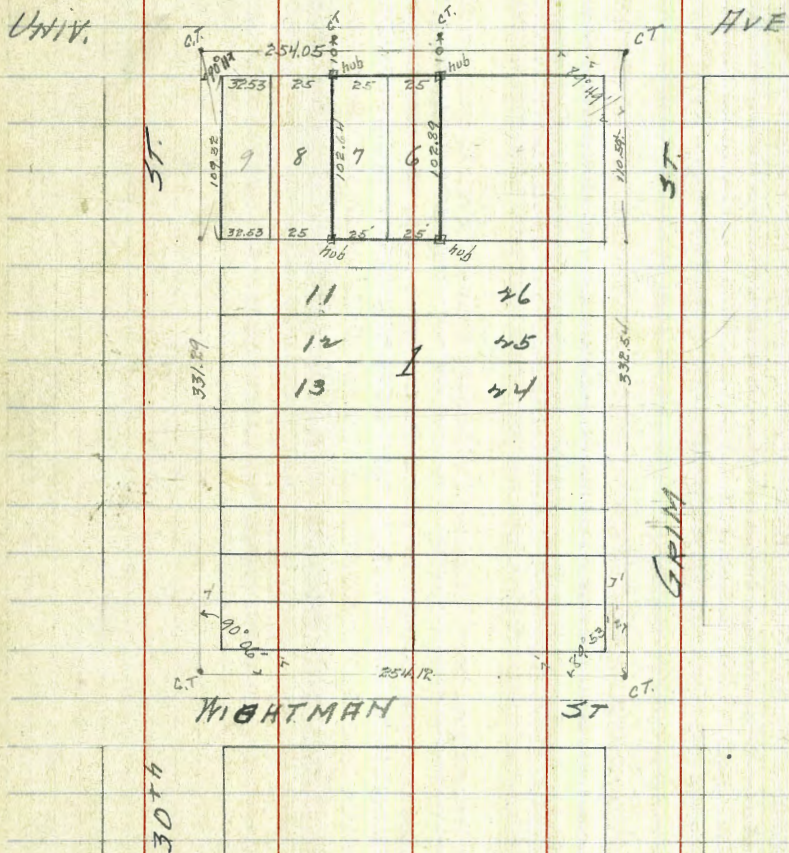
S		2.8	71.8
	325' W		
S		2.3	72.3
cb		2.6	72.0
1/4		2.7	71.9
C		2.8	71.8
1/2		2.9	71.7
cb		3.1	71.5
+5		4.5	70.1
N		7.4	67.2
+10		9.5	65.1
	350' W		
-10		6.5	68.1
N		5.1	69.5
+3		3.3	71.3
cb		2.1	71.5
1/4		2.7	71.9
C		2.7	71.9
1/2		2.8	71.8
cb		2.9	71.7
S		2.2	72.4
	375' W		
S		2.1	72.5
cb		3.0	71.6
1/4		3.0	71.6
C		2.8	71.8

1/2		2.9	71.7
cb		2.6	72.0
N		3.6	71.0
+10		5.6	69.0
	400' 300' W = E.L. San Clemente St.		
N		2.8	71.8
cb		2.7	71.9
1/4		3.1	71.5
C		3.0	71.6
1/2		3.0	71.6
cb		2.8	71.8
S		2.1	72.5
cb		2.09	

72.18 - 200' Clemente  
71.12 - 400' Voltaire



1/2/17 Gregory Miller DT67  
 Survey of Fire Station Site  
 Being Lots 6+7 Bk 1  
 Hartley's No. Park.



Handies  
 Elevations on foundation of Fire Station 30th University 1/17/17 Gregory Miller

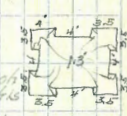
355.31 NW Corner  
 350.07

N.E. Cor App Room Bottom of Excavation 5.64  
 354.45 = elev  
 S.E. ✓ ✓ ✓ ✓ ✓ ✓ 5.60  
 354.49 ✓ ✓  
 S.W. ✓ of Bldg. ✓ ✓ ✓ ✓ 5.66  
 354.43 ✓ ✓  
 N.W. ✓ of Trk ✓ ✓ ✓ ✓ 5.56  
 354.53 ✓ ✓  
 N.W. ✓ App Room ✓ ✓ ✓ ✓ 5.77  
 354.32 ✓ ✓  
 Int Office ✓ ✓ ✓ ✓ ✓ ✓ 5.58  
 354.54 ✓ ✓

Elevations of Ditto (tranches) 1/2/17 Gregory Miller

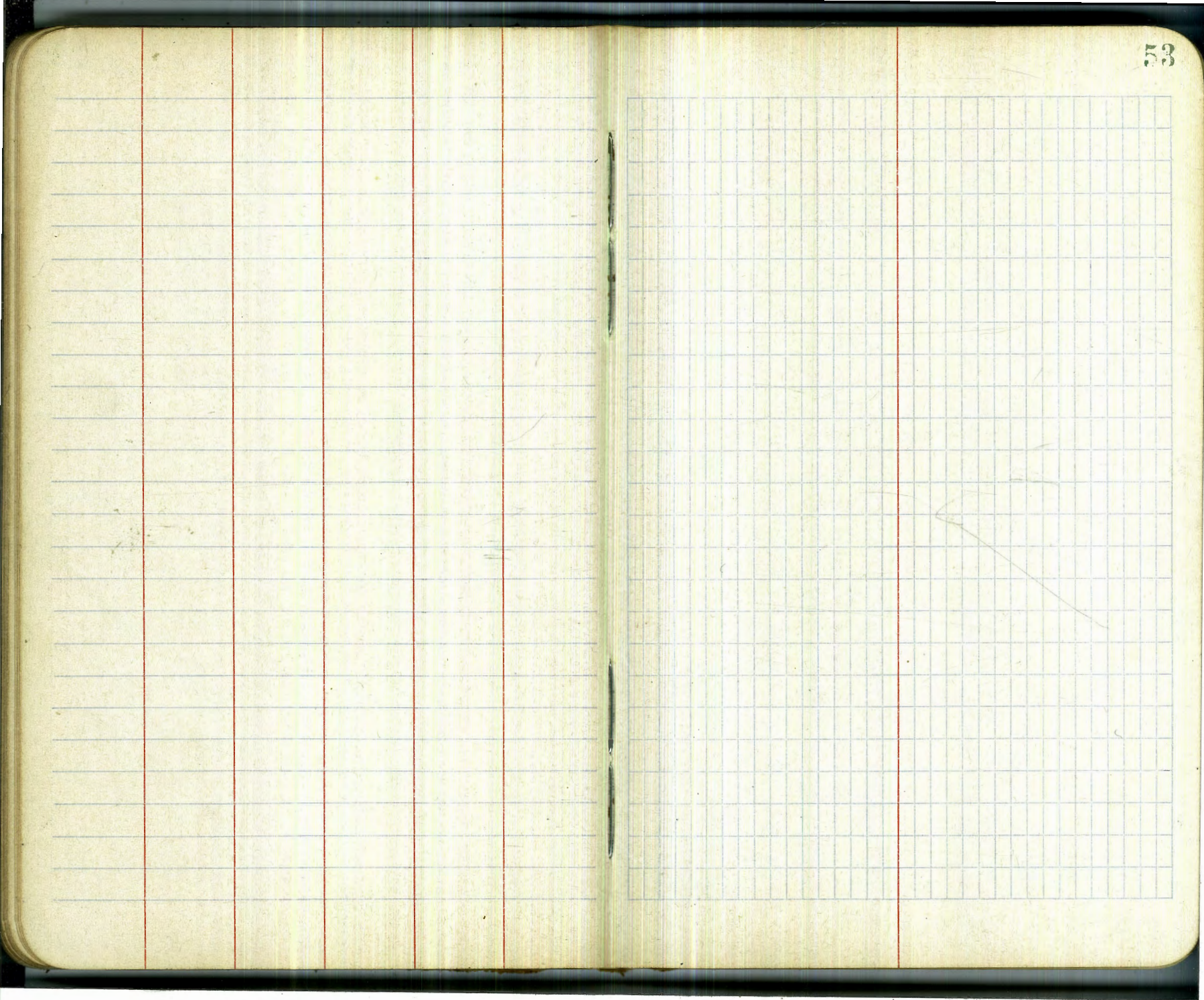
355.21 N.E. Cor App Room 5.66  
 354.49  
 350.13 5.62  
 354.51  
 S.E. ✓ ✓ ✓ ✓ ✓ ✓ 5.55  
 354.58  
 S.W. ✓ Bldg 5.55  
 354.58  
 N.W. ✓ Office 5.57  
 354.56  
 N.W. ✓ App Room 5.66  
 354.56  
 Int Office ✓ ✓ ✓ ✓ ✓ ✓ 5.56  
 354.57  
 Ctr of Clock Tower 5.82  
 353.31

These elevations are some higher than those taken at 1/17/17 due to sloughing in.



355.31 NW. Office 1/4 SW Bldg 1/4 SE + 1/4 Int Trunk of Trk.  
 350.78 5.58 4.70 4.70 5.10 4.60 4.60 4.60 4.60 4.60  
 350.78 356.13 356.13 356.13 356.13 356.13 356.13 356.13  
 NE low Int Top NE Bldg NW low  
 54.11 350.86 356.93 350.86

355.31 353 359.53 nails mark app above finish 5.66 Elev of Top of Foundation



1/22/17 Gage Levels of Elliot St. (18' curbs)  
 from Chatsworth to Villa Drive (The East 8 or 9' not graded)  
 Curb is in on West Side all through

B.M.	4.39	153.25	148.86	SE Chatsworth + 20.713
		20' So. of E.C. No. of Chatsworth (measured on curb)		
W cb		13.81	139.5	on cement
		10' So. of -		
Wcb		13.20	140.1	on cement
		E.C.		
Wcb		12.38	140.87	on cement
T.P.	10.85	153.22	142.87	
E cb		14.0	139.7	
		44.5' No. of E.C.		
Ecb		10.1	143.6	
W ✓		9.2	144.5	on cement
		25' No. of last section		
W ✓		7.4	146.3	on cement
E ✓		8.2	145.5	
		25' No. of last		
E ✓		6.9	146.8	
W ✓		6.07	147.6	on cement
		25' No. of last		
Wcb		5.17	148.5	on cement
E ✓		6.20	147.5	
		25' No. of last		
E ✓		5.7	148.0	
W ✓		4.67	149.0	on cement

Ecb graded off line.

153.77  
 100' No. of last sect.

Wcb		3.87	149.8	on cement
E ✓		4.7	149.0	
		100' No. of last		
E ✓		3.2	150.3	
W ✓		2.90	150.8	on cement
		60' No. of last		
W ✓		1.60	152.1	on cement
E ✓		2.2	151.5	
T.P.	10.18	162.77	1.13	152.59
		60' No. of last		
Ecb		2.9	152.9	
W ✓		2.13	153.7	on cement
		60' No. of last		
W ✓		2.26	155.5	on cement
E ✓		2.2	154.6	
		30' No. of last		
E ✓		6.8	156.0	
W ✓		6.15	156.6	on cement
		30' No. of last		
Wcb		4.92	157.9	on cement
E ✓		5.6	157.2	
		30' No. of last		
E ✓		4.2	158.6	
W ✓		3.65	159.1	on cement



20' No. of last sect.		
Web	2.64	160.2 on cement
E ✓	2.8	160.0
25' No. of last		
E ✓	2.1	160.7
W ✓	2.11	160.1 on cement
25' No. of last		
Web	1.76	161.0 on cement
E ✓	1.5	161.3
50' No. of last		
E ✓	1.4	161.4
W ✓	1.45	161.3 on cement
20' No. of last		
Web	1.5	161.3 on cement
E ✓	1.6	161.2
20' No. of last		
E ✓	2.1	160.7
W ✓	1.71	161.1 on cement
20' No. of last		
W ✓	2.12	160.7 on cement
E ✓	2.5	160.3
20' No. of last		
E ✓	3.1	159.7
W ✓	2.73	160.1 on cement

3217' No. of last		
Web	3.92	159.9 on cement
E ✓	4.3	159.5
100' No. of last		
E	7.8	155.0
Web	7.75	155.0 on cement
100' No. of last = P.C.		
Web	11.63	151.2 on cement
E ✓	11.4	151.4
T.P.	1.47	152.62
		11.62
		151.15
10' West of P.C. measured on curb (radius = ?)		
cb	1.86	150.8 on cement
20' - - - - -		
cb	2.18	150.4 - -
30' - - - - -		
cb	2.57	150.0 - -
40' - - - - -		
cb	3.02	149.6 - -
50' - - - - -		
cb	3.62	149.0 - -
60' - - - - -		
cb	4.38	148.2 - -
68.8 - - - - -		
cb	5.27	147.3 end of cement
INT of Curb & W. of Pt Loma Villas		
Ecb	3.1	149.5

152.62

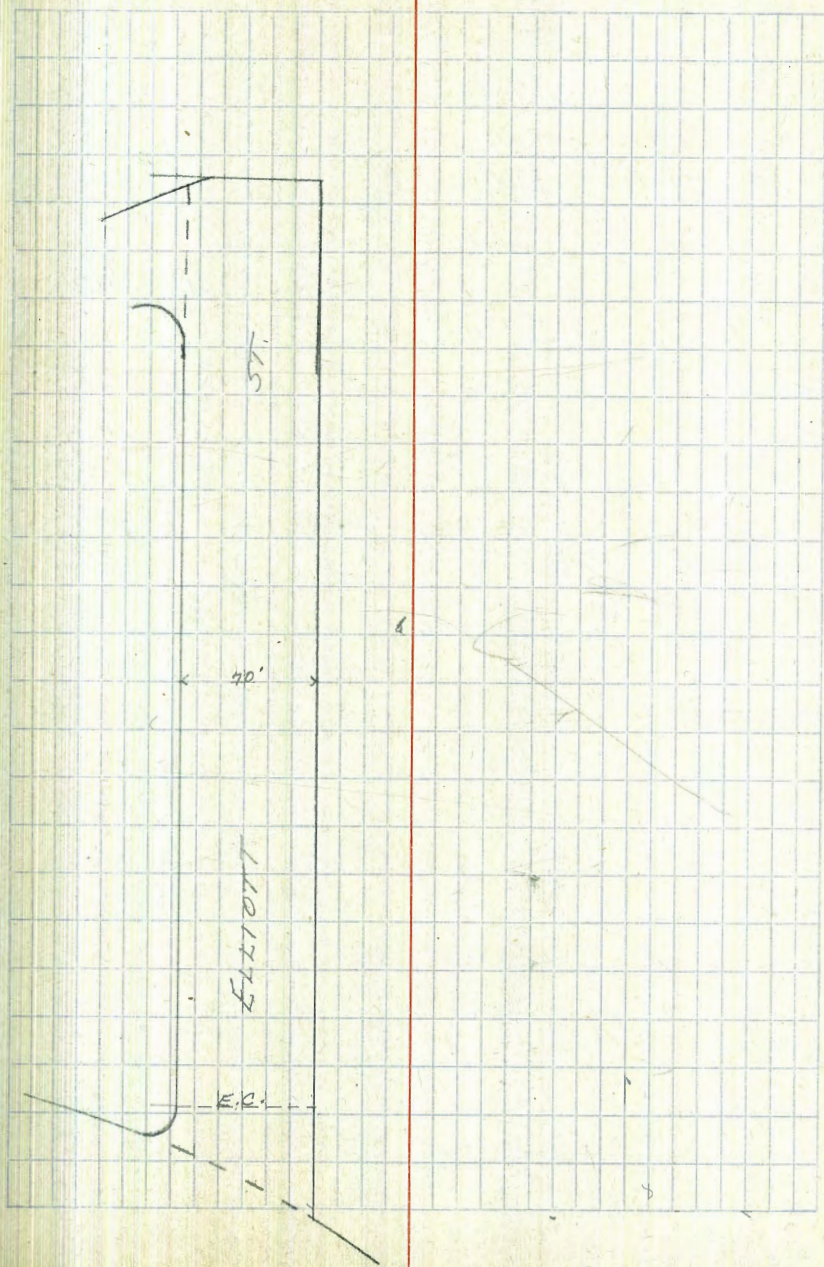
INT. OF W.L. Elliott + N.L. Villa Drive

No. Curb

3.7

148.9

56



1/22/17  
Gregory  
Moore  
Miller

Larals on Villa Drive 50' wide  
from W.L. Elliott to  
E. Alcott St  
12' curbs

	152.62		
	M.L. Elliott		
No. Cb.	3.7		148.9
	Section A		
✓ ✓	6.5		146.1
So. Cb.	5.7		146.9
	38.6 Mon So } Hairs V - No. } = B		
So Cb.	8.4		144.2
No. ✓	9.3		143.3
	25' W on So } 26' W - No. } = C		
No. ✓	10.9		141.7
So ✓	9.9		142.7
	25' W on So } 26' W - No. } = D		
So ✓	11.3		141.3
No. ✓	12.3		140.3
	25' W on So } 26' W - No. } = E		
No. ✓	13.2		139.4
So ✓	12.2		140.4
T.P.	10.00	150.38	140.38
	25' W on So } 26' W - No. } = F		
So Cb.	10.6		139.8
No. ✓	11.6		138.8
	25' W on So } 26' W - No. } = G		
No. Cb.	11.9		138.5
So ✓	10.8		139.6

Posted

VILLA DRIVE  
57

	25' W on So } 26' W - No. } = H	
So Cb.	150.38	10.8
No. ✓		11.8
	25' W on So } 26' W - No. } = I	
No. Cb.		11.3
So ✓		10.3
	25' W on So } 26' W - No. } = J	
So Cb.		9.6
No. ✓		10.7
	25' W on So } 26' W - No. } = K	
No. ✓		10.6
So ✓		9.6
	71.28 W. of K on No.	
No. Cb.		8.3
	INT of N.L. Villa Drive & No. Curb on East curb of Curtis & N.L. Villa Dr.	
Cb.		8.6
	25' W. of K on So.	
So Cb.		5.7
	INT of N.L. Villa Dr & W curb of Curtis St.	
No. Cb.		7.1
	E.C. west of Curtis on No. = Sect L	
No. Cb.		5.6
	E.C. ✓ - ✓ on So. = Sect M.	
So Cb.		4.2
T.P.		4.17
	146.21 ✓	or end of ret. SW Curtis & Villa Dr

117.49 Vol. 11 No. 1 = N = P.C.C.

No. 06 4.8 145.6

So ✓ 3.7 146.7

with 144 W on No. 1 = 0 -

So ✓ 2.6 147.8

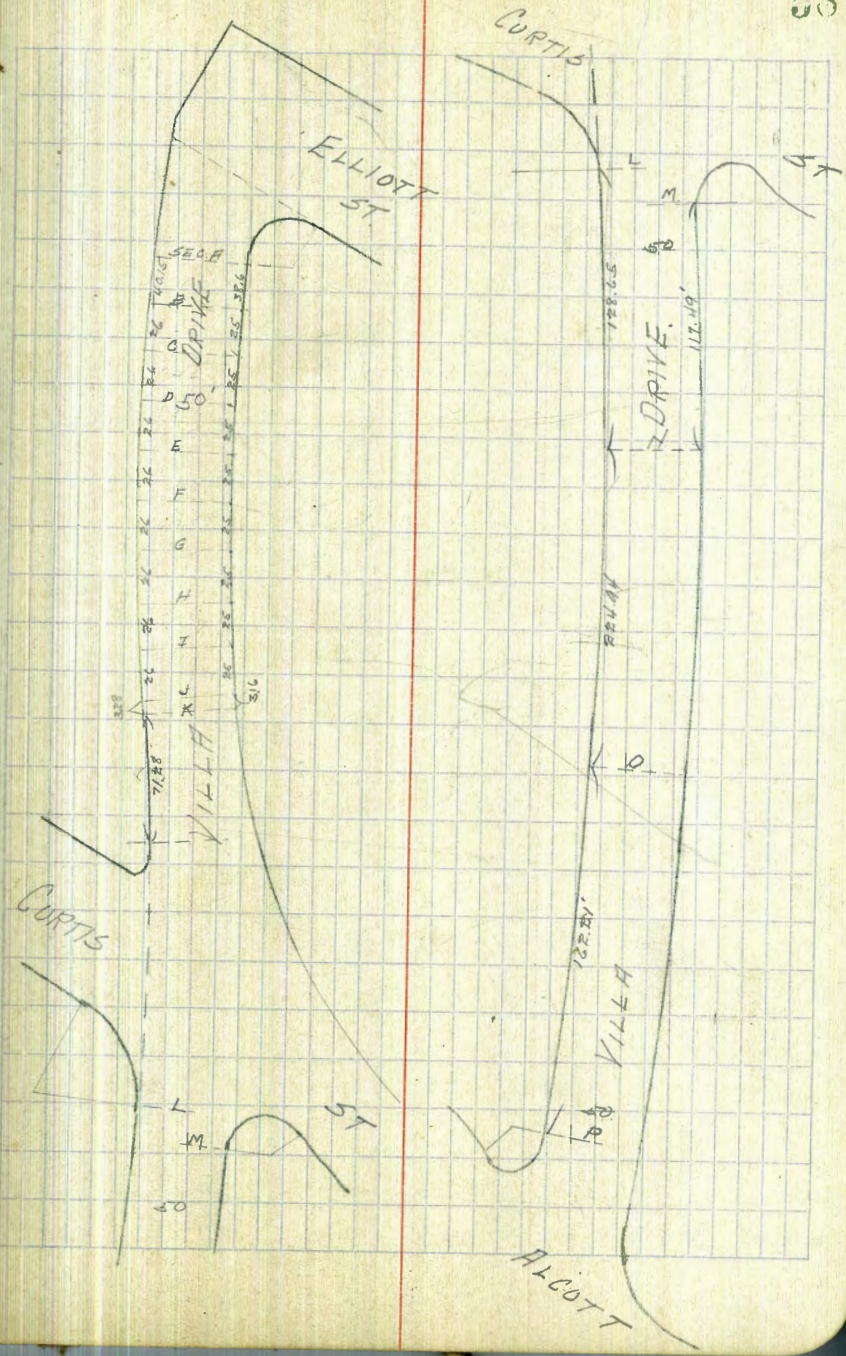
No ✓ 3.5 146.9

158.28

from H I page 64

162.21 No. 1007 No. = P.

No. 06 1 7.05 151.23



This page features a grid of blue horizontal lines. Three vertical red lines are positioned to create four columns of varying widths. The columns are approximately 15%, 35%, 35%, and 15% of the page width from left to right. The page is otherwise blank.

This page features a grid of blue horizontal lines. A single vertical red line is positioned to create two columns of approximately 65% and 35% of the page width from left to right. The page is otherwise blank.

7/24/17 Gregory  
Moore  
Miller

Levels on Curtis St  
from Chatsworth Blvd  
to Villa Drive  
Curbs in on Both Sides

50 wide  
18' walks  
Distances are prop. line  
dis.

SE Curtis  
4 Chatsworth

B.M.	736	156.22	148.86	
		End of Curve Just No. of Chatsworth = A.		
Wcb		2.11	153.11	
Ecb		3.04	153.18	
T.P.	1327	169.45	0.04	156.18
		141.92' No. of A.		
Ecb		1.82	167.63	
		155.96' No. of A.		
Wcb		1.41	168.04	
		161.92' No. of A.		
Ecb		0.11	169.34	
		175.96' No. of A.		
T.P.	956	178.74	0.27	169.18
Wcb		9.14	169.60	
		181.92' No.		
Ecb		7.92	170.82	
		195.96' No.		
Wcb		2.74	171.0	
		201.92' No.		
Ecb		6.68	172.06	
		215.96' No.		
Wcb		6.57	172.17	
		221.92' No.		
Ecb		5.64	173.10	

Platted  
7/30/17

178.14

235.96' No.

60

Wcb		5.65	173.09	
		241.92' No.		
Ecb		4.92	173.82	
		255.96' No.		
Wcb		4.94	173.80	
		Curb on West Turns in to Driveway here		
		261.92' No.		
Ecb		4.44	174.30	
		281.92' No.		
Ecb		4.16	174.58	
		301.92' No.		
Ecb		4.17	174.57	
		348.74' = E.C. into Driveway		
Wcb		3.74	174.80	
		404.96' No. of B 430.56' - W } = SECT. B		
Wcb		5.37	173.37	
Ecb		5.64	173.10	
		INT. of Wcb into Creston Dr with N.L. of Curtis		
W		4.87	173.87	
		44.76' No. of B		
Ecb		6.83	171.91	
		49.76' No.		
Ecb		7.38	171.36	
		119.76' No.		
Ecb		8.38	170.36	

139.76 No

Ecb 9.75 168.99

159.76 No

Ecb 11.53 167.21

INT. of Web as constructed into Creston Dr. with M.L. Curtis

5.90 172.84

127.4 No. of B = E.C. out of Creston Dr.

Web 7.63 171.11

No. End of Curve out of Creston Dr. as shown on map.

Web 9.13 169.61

T.P. 0.16 166.05 128.5 165.89

218.37 No. of B

Ecb 4.81 161.24

238.37 No.

Ecb 6.81 159.24

258.37 No

Ecb 8.74 157.31

278.37 No

Ecb 10.50 155.55

298.37 No

Ecb 12.03 153.02

T.P. 3.24 156.24 13.05 153.0

318.37 No

Ecb 3.58 152.66

338.37 No

Ecb 4.70 151.54

358.37 No

Ecb 5.70 150.54

378.37 No

Ecb 6.68 149.56

397.56 No

Ecb 11.58 144.66

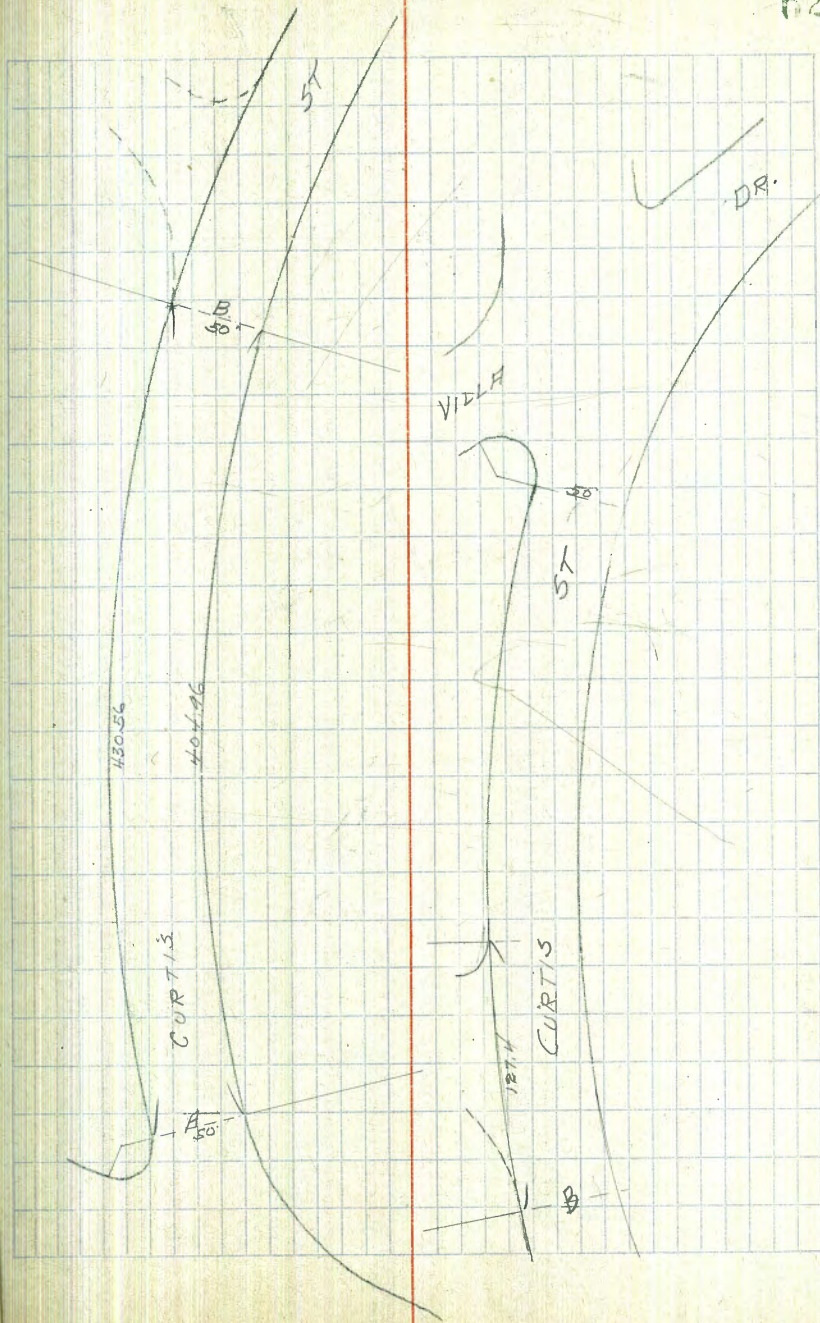
So. End Curve on St. Villa Dr + Curtis

Web 6.78 149.46

42.25' So. of above reading

Web 3.88 152.36

T.P. 8.46 147.78





7/25/17  
Gregory  
Moore  
Miller

Levels on Albott St  
from Chatsworth Blvd  
to a point No. of  
Villa Drive

Posted  
7/20/17

SE. Chatsworth  
+ Curtis

B.M.	13.07	161.93	168.86	
	for levels back from this pt see page 20			
	SECTION A			
Wcb.		0.52	161.41	
T.P.	12.66	174.52	0.07	161.86
Ecb		13.20	161.32	
	73.59' No. = SECT. B = P.C.			
Ecb		2.56	165.96	
Wcb		8.49	165.03	
	75.27' No. of B. on E = P.C. of curve into driveway			
Ecb		3.59	170.93	
	101.38' No. of B. on W			
Wcb		1.40	173.12	
	121.38' - - - W			
Wcb		0.11	174.41	
T.P.	3.96	178.37	0.11	174.71
	144.94' No. of B. on E = E.C. of curve into driveway			
Ecb		3.00	175.37	
	141.38' No. of B. on W			
Wcb		2.97	175.40	
Ecb		1.49	175.58	
	151.38' No. of B. on W = E.C. = SECT. C			
Wcb		2.64	175.73	
Ecb		7.27	177.10	
	10' No. of Cor W			
Wcb		2.39	175.98	
	30' No. of Cor W			
Wcb		2.04	176.33	

63

80' No. of Cor W = SECT. D = P.C.

Wcb	178.37	2.24	176.13
	1/3 of dis. bet SECT. C + PT X		
Ecb		0.71	177.66
	2/3 of dis. bet - - - -		
Ecb		0.50	177.87
	INT. of E.L. Albott with <sup>curve</sup> Baldwin Creston = Point X		
Ecb		0.58	177.99
	INT. of E.L. Albott with No curb line Creston as graded.		
Ecb		1.33	177.04
	20		
	40		
	52.48' No. of SECT. D on E = E.C. out of Creston as graded.		
Ecb		2.13	176.24
	E.C. of Curve on No Side Creston as shown on map. = PT Y		
Ecb		2.79	175.58
	20.0' No. of PT Y on E		
Ecb		4.07	174.30
	40' No. - - - - E		
Ecb		5.74	172.63
	20' No. of SECT. D on W		
Wcb		2.35	176.02
	40' No. of SECT. D on W		
Wcb		2.60	175.73

60' No. of Don W

Web 178.37 3.19 175.18

80' No. of Don W

Web 4.00 174.32

T.P.

100' No. of Don W

Web 5.21 173.16

120' No. of Don W

Web 6.63 171.74

T.P. 00 165.36 13.01 165.36

40' So. of SECT F on F

Ecb 6.62 158.74

20' - - - F - -

Ecb 8.26 157.10

SECT. F

Ecb 9.56 155.80

SECT E

Web 9.89 155.47

INT. C.B. Line + So L. Villa Dr.

Web 11.66 153.70

20' No. of SECT F

Ecb 11.11 154.25

40' - - - F

Ecb 12.24 153.12

6009 - - - F = E.C

Ecb 12.84 152.52

T.P. 5.76 158.28 12.84 152.52

SECT G

Ecb 7.05 151.23

12.84 No. of G

Ecb 6.75 151.53

35.63 No. of G = A

Ecb 6.34 151.94

Web 6.05 152.23 ✓

20' So. of A on W

Web 6.30 151.98

40' So. of A on W

Web 6.20 152.08

SECT. I

Web 4.74 154.14

Ecb 5.50 152.88

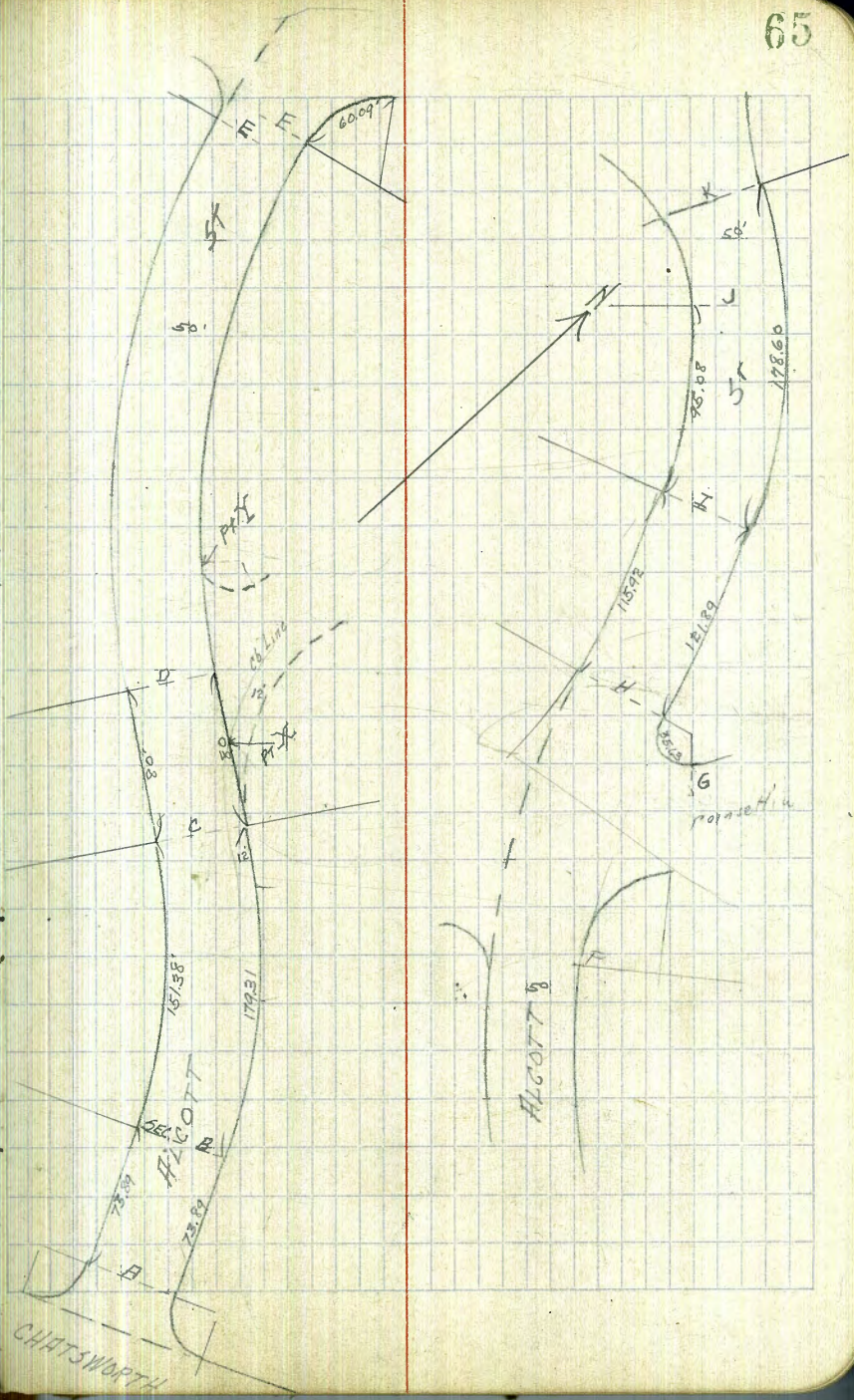
SECT J = P.C.C.

Web 2.80 155.48

SECT A = End

Web 1.16 157.12

Ecb 2.76 155.52



x-section Jack dam st from S.L. Washington st  
 South for 150' - Jack dam 50' wide 10 walks 75' 1125

B.M. S.E. brass plg Washington & Ivis 260.54

B.M. 1.86 262.40  
 0+0 = S.L. Washington

E.L.	4.7	257.7
+07	5.1	257.3
CR6	5.7	256.7
"4	5.9	256.5
CTV	5.8	256.6
"4	6.0	256.4
CR6	6.2	256.2
+02	5.5	256.9
W.L.	5.5	256.9 ✓
0+25 South		
W.L.	5.3	257.1 ✓
+08	5.5	256.9
CR6	6.8	255.6
"4	6.3	256.1
CTV	5.9	256.5
"4	6.3	256.1
CR6	6.1	256.3
+02	5.6	256.8
E.L.	5.2	257.2 ✓

7/28/19 Dunkle  
 EVANS  
 Folcke

262.40

66

0+50

E.L.	5.6	256.8 ✓
+07	5.8	256.6
CR6	6.7	255.7
"4	6.5	255.9
CTV	6.2	256.2
"4	6.6	255.8
CR6	6.8	255.6
+02	6.2	256.2
W.L.	5.5	256.9 ✓
0+75		
W.L.	5.8	256.6 ✓
CR6	7.2	255.2
"4	6.8	255.6
CTV	6.7	255.7
"4	6.7	255.7
CR6	6.8	255.6
E.L.	5.9	256.5 ✓
1+0		
E.L.	6.3	256.1 ✓
CR6	6.1	256.3
"4	5.7	256.7
CTV	5.4	257.0
"4	6.1	256.3
CR6	6.6	255.8
W.L.	6.4	256.0

262.40

#16

W.L.	7.5	254.9	✓
CR6	6.6	255.8	
1/4	5.4	257.0	
CTR	4.8	257.6	
1/4	5.8	256.6	
CR6	7.3	255.1	
E.L.	7.9	254.5	✓

#150

-15'	23.1	239.3	
E.L.	18.7	243.7	
CR6	15.7	246.7	
1/4	14.0	248.4	✓
CTR	13.3	249.1	
1/4	13.2	249.2	
CR6	13.7	248.7	
W.L.	15.0	247.4	
#15	12.2	244.2	

67

10/11/19  
 600 ft  
 17.16  
 32W

CROSS SECTION OF  
 LAUREL ST 80' wide in obs  
 1.4th to 30th

291.33

FS

	1.42	291.33	289.71	BP SE 30th + 1/2 way
		N. L. 30th		
S		5.3	286.01	
cb		5.8	285.51	= cement
1/6		6.9	84.4	
c		7.4	283.91	
1/2		8.0	83.3	
cb		7.8	283.5	
		(8.8)	282.5	cement
N		8.5	282.81	
				5' W
N		2.1	289.21	
+3		6.1	85.2	
+7		7.1	84.2	
cb		7.2	284.11	
1/2		7.7	83.6	
c		6.8	284.51	
1/4		4.6	86.7	
cb		1.5	289.81	
S		1.1	290.21	
				10' W
S		0.5	290.81	
cb		1.2	290.11	
1/4		1.0	90.3	
+8		1.1	90.2	

Sections for 80' street, 15' cleared  
 on each side 1/5/20

2		5.5	285.81	
+4		7.0	84.3	
1/4		8.0	83.3	
cb		7.2	284.11	
+8		7.0	84.3	
+12		5.6	85.7	
N		2.5	288.81	
				15' W
N		0.9	290.41	
+2		0.9	290.4	
+3		4.1	287.2	
cb		8.8	282.51	
1/4		8.3	283.0	
+9		5.5	285.8	
+10		1.0	290.3	
c		1.0	290.31	
1/5		1.1	290.2	
cb		1.1	290.21	
S		1.0	290.31	
				20' W
S		1.1	290.21	
cb		0.8	290.51	
1/4		0.8	290.5	
c		0.9	290.41	
+8		0.9	290.4	

291.33

+8.1	5.7	285.6
1/4	8.1	283.2
cb	8.3	283.0
+1	1.2	290.1
N	1.0	290.3

25' W

N	0.9	290.4
cb	1.2	290.1
1/4	1.0	290.3
C	0.7	290.6
1/4	0.7	290.6
cb	0.9	290.4
S	1.0	290.3

50' W

T.P.	4.50	291.97	0.86	290.47
s			4.6	290.4
cb			4.5	290.5
1/4			4.4	290.5
C			4.3	290.7
1/4			4.5	290.5
cb			4.3	290.7
N			3.6	291.4

100' W

N	4.3	290.7
cb	4.1	290.9
1/4	4.3	290.7

294.97

Lauric

69

C	46	290.4
1/4	45	290.4
cb	43	290.7
S	43	290.7

150' W

S	40	291.0
cb	39	291.1
1/4	37	291.2
C	41	290.9
1/4	47	290.2
cb	48	290.2
N	48	290.2

175' W

N	47	290.3
cb	48	290.2
1/4	45	290.4
C	41	290.9
1/4	38	291.1
cb	40	291.0
S	35	291.2

200' W

S	38	291.2
cb	41	290.9
1/4	43	290.6
C	45	290.5

294.97

1/4		53	289.6	
cl		55	289.5	
N	sidewalk to house at 225'	53	289.7 ✓	= 1/2 way
	250' W			= 1/2 way
N		60	289.0 ✓	
cl		61	288.9 ✓	
1/4		55	289.4	
c		4.7	290.3 ✓	
1/4		4.2	290.7	
cl		3.7	291.3	
S		3.0	292.0 ✓	291.5 ✓
	300' W			
S		2.6	292.4 ✓	291.8 ✓
cl		2.1	291.6	
1/4		50	289.9	
c		53	289.7 ✓	
1/4		60	288.9	
cl		61	288.9 ✓	
N		63	288.7 ✓	= 1/2 way
	350' W			
N		66	288.4 ✓	= 1/2 way
cl		66	288.4 ✓	
1/4		6.2	288.7	
c		53	289.7 ✓	
1/4		4.2	290.8	
cl		3.7	291.3	291.6 ✓

294.97

LAUREL

70

S		2.7	292.3 ✓	
	400' W			
S		2.5	292.5 ✓	292.0 ✓
cl		3.2	291.8	
1/4		4.5	290.4	
c		5.0	290.0 ✓	
1/4		6.4	288.5	
cl		7.0	288.0	287.8 ✓
N		7.7	287.3 ✓	
	417.6' W = E. side of house which projects			
	10.5 into st. house is 86.4' wide. cl. floor = 289.0			
	450' W			
N		9.4	285.6 ✓	286.4 ✓
cl		8.3	286.7	
1/4		6.9	288.1	
c		4.4	290.6 ✓	
1/4		4.2	290.7	
cl		3.6	291.4	291.6 ✓
S		3.0	292.0 ✓	
	500' W			
S		4.6	290.4 ✓	290.0 ✓
cl		5.1	289.9	
1/4		6.2	288.7	
c		7.4	287.6 ✓	
1/4		9.1	285.9	



cl	10.6	284.4	286.1
N	13.2	281.8	✓
+7	14.1	280.9	
+20	20.5	274.5	
550' W.			
-20	25.8	269.2	
-10	19.6	275.4	
N	17.5	277.5	✓
cl	15.3	279.7	279.1
1/4	11.9	283.1	
C	9.9	285.1	✓
1/4	8.7	286.3	✓
cl	7.7	287.3	
S	6.7	288.3	289.0
575' W			
S	2.7	287.3	✓
cl	4.1	285.9	286.3
1/4	10.3	284.6	
C	11.9	283.1	✓
1/4	14.1	280.9	
cl	16.6	278.5	
N	20.5	274.5	277.4
+40	27.8	267.2	
601.3' W = E.L. 29 <sup>th</sup> St 80' wide			
-20	33.6	261.5	
N	24.1	270.9	

cl	19.1	275.6	274.3
1/4	15.8	279.2	
C	13.3	281.7	
1/4	11.6	83.3	
cl	10.4	284.6	
S	8.7	286.3	
E. Cb.			
S	9.2	285.8	✓
N	26.3	268.7	✓
E 1/4			
N	27.8	267.2	✓
S	9.5	285.5	✓
C			
S	10.5	284.5	✓
N	29.4	265.6	✓
W 1/4			
N	30.6	264.4	✓
S	12.2	282.8	✓
cl			
S	13.2	281.5	✓
N	33.6	261.4	✓
M.L. 29 <sup>th</sup> St			
N	37.0	258.0	✓
S	15.0	280.0	
500' so. of Laurel on 29 <sup>th</sup> St			
E	5.7		
W	10.8		
over			

24/97

100' So. of Laurel on 49

W

70

E

4.6

72

1/29/00 Gregory Miller Shaw  
 CROSS SECTION OF  
 KALMIA ST 20' wide in cbs  
 14th to 30th

6.91

296.6<sup>v</sup>

289.71

SE Kalmia  
 +30' W

W. L. 30th ST.

s	6.7	289.9 <sup>v</sup>
cb	6.9	89.7 <sup>v</sup>
1/4	7.1	89.5 <sup>v</sup>
c	7.2	89.4 <sup>v</sup>
1/4	7.1	89.5 <sup>v</sup>
cb	7.1	89.5 <sup>v</sup>
	(6.70)	289.9 <sup>v</sup> = 66'
N	6.6	90.0 <sup>v</sup>
	50' W	
N	6.5	90.1 <sup>v</sup>
cb	6.7	89.9 <sup>v</sup>
1/4	7.0	89.6 <sup>v</sup>
c	7.0	89.6 <sup>v</sup>
1/4	7.0	89.6 <sup>v</sup>
cb	7.0	89.6 <sup>v</sup>
s	7.0	89.6 <sup>v</sup>
	80' W	
s	7.0	89.6 <sup>v</sup>
cb	7.0	89.6 <sup>v</sup>
1/4	7.0	89.6 <sup>v</sup>
c	6.9	89.7 <sup>v</sup>
1/4	6.7	89.9 <sup>v</sup>
cb	6.7	89.9 <sup>v</sup>

296.6<sup>v</sup>

28

N	6.7	289.9 <sup>v</sup>
	100' W	
N	6.4	90.2 <sup>v</sup>
cb	6.4	90.2 <sup>v</sup>
1/4	6.5	90.1 <sup>v</sup>
c	6.8	89.8 <sup>v</sup>
1/4	6.9	89.7 <sup>v</sup>
cb	6.4	90.2 <sup>v</sup>
s	6.3	90.3 <sup>v</sup>
	125' W	
s	6.2	90.4 <sup>v</sup>
cb	6.2	90.4 <sup>v</sup>
1/4	6.3	90.3 <sup>v</sup>
c	6.3	90.3 <sup>v</sup>
1/4	6.2	90.4 <sup>v</sup>
cb	6.1	90.5 <sup>v</sup>
N	5.6	91.0 = 91.6 to hood
	160' W	
N	4.3	92.3 <sup>v</sup>
cb	4.5	92.1 <sup>v</sup>
1/4	4.7	91.9 <sup>v</sup>
c	4.8	91.8 <sup>v</sup>
1/4	4.9	91.7 <sup>v</sup>
cb	4.8	91.8 <sup>v</sup>
1/3	4.3	92.3 <sup>v</sup>
s	4.0	292.6 <sup>v</sup>

296.62

200' W

212' W on S = opp. to house 34

293.0

S	36	293.0
db	31	93.5
1/4	31	93.5
C	35	93.1
1/4	36	93.0
db	35	93.1
N	32	93.4

per of lawn

235' W

N	33	93.3
db	35	93.1
1/4	34	93.2
C	36	93.1
1/2	37	92.9
db	38	92.8
S	37	92.9

255' W

S	40	92.6
db	41	92.5
1/4	37	92.9
C	29	93.7
1/4	34	93.2
db	37	92.9
N	23	293.3

270' W on S = opp. to house db 292

296.62

KALHIA

4

280' W

N	39	292.7
db	35	92.8
1/4	42	92.4
C	44	92.2
1/4	45	92.1
db	44	92.2
S	43	92.3

300' W

S	44	92.2
db	48	91.8
1/4	47	91.9
C	45	92.1
1/4	43	92.3
db	32	93.4
N	32	93.4

320' W

N	45	92.1
db	46	92.0
1/4	47	91.9
C	50	91.6
1/4	50	91.6
db	51	91.5
S	50	91.6

296.62

370' W

S	52	291.4	✓
cb	55	91.1	✓
1/4	55	91.1	✓
C	52	91.4	✓
1/4	51	91.5	✓
cb	48	91.8	✓
N	45	92.1	✓

400' W

N	42	92.4	✓
cb	51	91.5	✓
1/4	51	91.5	✓
C	49	91.7	✓
1/4	50	91.6	✓
cb	56	91.0	✓
S	54	91.5	✓

450' W

S	57	90.9	✓
cb	57	90.9	✓
1/4	55	91.1	✓
C	53	91.3	✓
1/4	48	91.8	✓
cb	50	91.6	✓
N	47	291.9	✓

296.62

KALMIA

75

500' W

N	53	291.3	✓
cb	54	91.2	✓
1/4	57	90.9	✓
C	57	90.9	✓
1/4	61	90.5	✓
cb	65	90.1	✓
S	65	90.1	✓

550' W

S	83	88.3	✓
cb	77	88.9	✓
1/4	75	89.1	✓
C	69	89.7	✓
1/4	65	90.1	✓
cb	65	90.1	✓
N	61	90.5	✓

601.5 - F.A 294.5 50' wide 14 obs

N	72	89.2	✓
cb	79	88.7	✓
1/4	85	88.1	✓
C	90	87.6	✓
1/4	95	87.1	✓
cb	99	86.7	✓
S	102	86.4	✓

296.62

E. ob

S	11.2	285.4	✓
ob	10.9	85.7	✓
1/4	10.3	86.3	✓
C	9.7	86.9	✓
1/4	9.0	87.6	✓
ob	8.5	88.1	✓
N	8.1	88.5	✓
50' N	6.7	89.9	✓
100' N	6.5	90.1	✓

E 1/4

N	8.6	88.0	✓
ob	8.9	87.7	✓
1/4	9.2	87.2	✓
C	10.2	86.4	✓
1/4	10.5	86.7	✓
ob	11.1	85.5	✓
S	11.6	85.0	✓

center 29th

S	12.6	84.0	✓
ob	11.7	84.9	✓
1/4	11.2	85.4	✓
C	10.6	86.0	✓
1/4	9.9	86.7	✓
ob	9.5	87.1	✓
N	9.0	87.6	✓

296.62

KALMIA

76

W. 1/4

N	9.6	287.0	✓	
ob	10.0	86.6	✓	
1/4	10.6	86.0	✓	
C	11.2	85.2	✓	
1/4	11.8	84.8	✓	
ob	11.9	284.6	✓ on 13/100	
543	270.0	12.8	83.8	✓
S	7.2	82.7	✓	
S	8.7	81.8	✓	
ob	7.5	82.5	✓	
1/4	8.2	83.8	✓	
C	5.5	84.5	✓	
1/4	4.7	85.3	✓	
ob	4.0	86.0	✓	
N	3.5	86.8	✓	
50' N	2.1	87.9	✓	
100' N	1.6	88.4	✓	
N	4.6	85.4	✓	
ob	5.2	84.9	✓	
1/4	5.8	84.3	✓	
C	6.6	83.4	✓	
1/4	7.8	82.2	✓	

190.06

dt

5

+ 10

9.2

10.7

12.2

80.8<sup>9</sup>

279.4

11.8<sup>9</sup>

77

Cross Section Alley Block 57 City Heights  
 Between Cherokee + Reed From University to Kluber  
 26' Wide

BM	719	352.28	352.09	NW Cor University + Reed
- Stone University Ave. = 0 + 0				
F	Top Cb	5.31	353.90 ✓	
L	" Parking	5.37	353.91 ✓	
H	" Cb	4.84	354.44 ✓	
10' S				
H		5.1	54.2 ✓	
L		5.3	57.0 ✓	
E		5.0	59.3 ✓	10' S Tap 11" 55
33' S				
E	Garage Dirt Floor	5.7	53.6 ✓	
L		5.7	53.6 ✓	
H		5.4	53.9 ✓	
51' S				
H		5.7	53.6 ✓	
L		6.0	53.3 ✓	
+7		6.4	52.9 ✓	
E		5.7	53.6 ✓	
94' S				
-1	Garage Dirt Floor	7.2	52.1 ✓	
EL		7.2	52.1 ✓	
L		6.9	52.4 ✓	
+6		6.7	52.6 ✓	112' S 3.54 112
H		6.3	53.0 ✓	Can Do Garage 6.53
180' S				

359.78				
H		7.0 ?	52.9	48.3 ✓
L		7.0 ?	52.3	48.3 ✓
+6		7.1 ?	52.2	48.2 ✓
F	Conc Apron	7.40	51.88 ✓	181' S
+5	Garage Conc Floor	7.45	51.83 ✓	Garage 30' x 42' Curb 1' x 2' 69' S
150' S				
E		7.6	51.7 ✓	
E		7.6	51.7 ✓	
H		7.8	51.5 ✓	
+7		7.95	351.30 ✓	
185' S				
-5	Garage Conc Floor	8.33	51.41 ✓	
H		8.9	50.8 ✓	
L		8.7	51.0 ✓	
E		8.7	51.0 ✓	
207' S				
E		8.4	50.3 ✓	
L		8.1	50.6 ✓	
H		8.1	50.6 ✓	
+7	Can Garage Conc Floor	8.95	50.79 ✓	
238' S				
-5	Can Garage Dirt Floor	8.5	50.2 ✓	
H		8.9	49.8 ✓	
L		8.4	50.3 ✓	
E		8.8	49.9 ✓	
282' S				



353.74

-5	Garage Dirt Floor	46	49.1 ✓
F		47	49.0 ✓
S		43	49.4 ✓
N		42	49.5 ✓
75	Garage Conc Floor	381	49.93 ✓

381.5

N		48	48.9 ✓
S		49	48.8 ✓
E		49	48.8 ✓

367.5

E		51	48.6 ✓
S		49	48.8 ✓
N	Garage Conc Floor	447	49.27 ✓

400.5

N		55	48.2 ✓
74		55	48.2 ✓
S		53	48.4 ✓
74		54	48.3 ✓
E1		58	47.9 ✓

450.5

E		55	48.2 ✓
S		55	48.2 ✓
N		53	48.4 ✓

500.5

N		62	47.5 ✓
---	--	----	--------

Fence  
10' 10" Alley

Fence  
10' 10" Alley

353.74

+8		65	47.2 ✓
S		67	47.0 ✓
E		69	46.9 ✓
70	222	34295	706
			346.68 ✓

520.5

72	Col 16 Ganges Conc Floor	266	46.68 ✓
E		22	46.7 ✓
S		22	46.7 ✓
74		21	46.8 ✓
N		16	47.3 ✓

560.5

N		20	46.9 ✓
74		22	46.7 ✓
76		28	46.1 ✓
S		29	46.0 ✓
E		27	46.2 ✓

590.5

E		29	46.0 ✓
71		29	46.0 ✓
72		33	45.3 ✓
S		40	44.9 ✓
76		36	45.3 ✓
N		29	46.0 ✓

597

N		33	45.6 ✓
---	--	----	--------

3489

77		55	43.4 ✓
2		56	43.3 ✓
15		54	43.5 ✓
18		40	44.9 ✓
E		37	45.2 ✓

6015

E		58	43.1 ✓
2		60	42.9 ✓
M		54	43.5 ✓

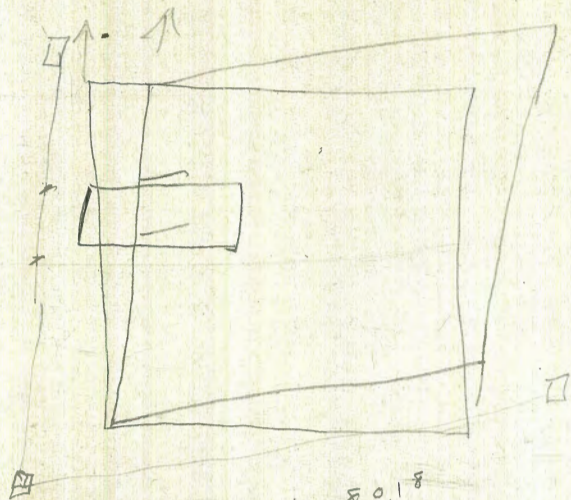
6015 N Edge Walk - N2 W 60°

M	Top Walk	58	43.02 ✓
2	"	60	42.50 ✓
E	"	650	42.40 ✓
T.P.	718	354.50	158 447.32 ✓
T.P.	701	359.07	251 351.99 ✓
B.M.		690	352.10 ✓

4015  
 4014  
 352.29

Page 26

80



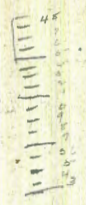
$$\begin{array}{r}
 80,18 \\
 \hline
 79840 \\
 16000 \\
 \hline
 9950 \\
 70200
 \end{array}$$

100.22  
 121.05  
 10220  
 10569

262.4  
 + 71  
 257.9

388

9595  
 222  
 9719  
 37837  
 47756



15928  
 1736  
 14192

SE K+30  
 289.71

1120  
 9421  
 18625

15928  
 5861  
 21837

50  
 80  
 100  
 125  
 150  
 175  
 200  
 225  
 250  
 275  
 300  
 325  
 350  
 375  
 400

RETURN TO CITY ENGINEER'S OFFICE  
 CITY HALL, SAN DIEGO, CAL.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.