

G-114



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ENGINEERS'  
FIELD BOOK  
No. 404

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# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.1  | 8.2  | 8.3  | 8.4  | 8.5  | 8.6  | 8.7  | 8.8  | 8.9  | 0  |
| 1  | 9.0  | 9.1  | 9.2  | 9.3  | 9.4  | 9.5  | 9.6  | 9.7  | 9.8  | 9.9  | 1  |
| 2  | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 2  |
| 3  | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 3  |
| 4  | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 4  |
| 5  | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 5  |
| 6  | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 6  |
| 7  | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 7  |
| 8  | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 8  |
| 9  | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 9  |
| 10 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 10 |
| 11 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 11 |
| 12 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 12 |
| 13 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 13 |
| 14 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 14 |
| 15 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 15 |
| 16 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 16 |
| 17 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 17 |
| 18 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 18 |
| 19 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 19 |
| 20 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 20 |
| 21 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 21 |
| 22 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 22 |
| 23 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 23 |
| 24 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 24 |
| 25 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 25 |
| 26 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 26 |
| 27 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 27 |
| 28 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 28 |
| 29 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 29 |
| 30 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 30 |
| 31 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 31 |
| 32 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 32 |
| 33 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 33 |
| 34 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 34 |
| 35 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 35 |
| 36 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 36 |
| 37 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 37 |
| 38 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 38 |
| 39 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 39 |
| 40 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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MICROFILMED

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|                                                     |        |      |
|-----------------------------------------------------|--------|------|
| SWBP ELLIOTT + NARCISSUS                            | 157.4  |      |
| SEBP ✓ + VILLA DRIVE                                | 150.35 |      |
| NE. PAINSETTIA + AMARYLLIS 1 <sup>st</sup> 25' R.P. | 157.40 |      |
| <sup>SE</sup> ON Radius Hub ✓ Not Lotus             | 139.61 |      |
| ELLIOTT + CHATSWORTH                                | 128.13 | SEBP |
| SEBP FREEMAN + ✓                                    | 108.61 |      |
| SE. Radius Pipe Jonquil + Lotus                     | 159.80 |      |

POINSETTIA Dr. Grades

|                            |        |             |
|----------------------------|--------|-------------|
| W.L. STA.                  | W.C.   | EC          |
| N. L. ELLIOTT              | 147.88 | 149.25      |
| 25' N ONE = EC             |        | 149.78      |
| 50 N                       | 148.93 | 150.24      |
| 100                        | 149.98 | 151.17      |
| 150                        | 151.03 | 152.11      |
| 200                        | 152.08 | 153.04      |
| 250                        | 153.13 | 153.98      |
| 300 N = PC                 | 154.18 | 154.91      |
| 251.60 = W.L.              | 154.70 | 155.50      |
| 318.5 = EL                 | 155.24 | 156.10      |
| 318.5 = EL                 | 155.77 | 156.68      |
| 400.69 = EC & Nipoma BREAK | 156.30 | 157.27      |
| 465.20 = N.W.              | 157.50 | 158.50      |
| 475.69 = PC                | 157.52 | 158.56      |
| 3123.20                    | 157.72 | 158.67      |
| 5000 W.L.                  | 157.78 | 158.78      |
| 4737 W.L.                  | 158.04 | 158.89      |
| 1412                       | 158.04 | 159.00      |
| 585.26 = EC                | 158.20 | 159.20      |
| 624.631                    | 158.50 | 159.20      |
| 674.631                    | 157.97 | 159.20      |
| 694.63                     | 157.39 | 159.20      |
| 714.63                     | 156.61 | 159.20      |
| 734.63                     | 155.63 | 159.20      |
| 754.63                     | 154.45 | 159.20      |
| 774.63                     | 153.09 | 154.50 = EC |

15025 ELLIOTT CROP  
9.17 VALM DRIVE

|        |       |       |       |       |       |       |
|--------|-------|-------|-------|-------|-------|-------|
| 1545.2 | 51.30 | 52.30 | 53.30 | 54.30 | 55.1  | 55.5  |
| 1547.5 | 5.7   | 7.0   | 4.1   | 5.1   | 12.7  | 12.7  |
| 1547.7 | 12.2  | 13.3  | 13.8  | 70.6  | 16.5  | 16.5  |
| 1547.9 | 1.8   | 0.7   | 2.0   | 5.5   | 3.8   | 2.0   |
| 1548.5 |       |       |       |       |       |       |
| 1548.4 | 50.0  | 50.5  | 51.4  | 52.3  | 53.20 | 54.30 |
| 1548.7 | 9.5   | 9.0   | 8.1   | 7.4   | 6.7   | 5.7   |
| 1548.8 | 3.9   | 3.2   | 3.0   | 2.7   | 2.0   | 1.3   |
| 1548.9 | 2.6   | 2.8   | 2.1   | 2.5   | 2.7   | 2.3   |
| 1549.0 |       |       |       |       |       |       |
| 1549.1 | 50.0  | 50.5  | 51.7  | 52.0  | 52.1  | 52.3  |
| 1549.2 | 11.7  | 11.3  | 10.0  | 9.7   | 8.6   | 7.4   |
| 1549.3 | 14.0  | 14.2  | 12.0  | 12.5  | 10.0  | 9.6   |
| 1549.4 | 3.8   | 3.0   | 2.6   | 2.8   | 2.0   | 2.0   |
| 1549.5 |       |       |       |       |       |       |
| 1549.6 | 56.9  | 57.5  | 58.7  | 59.0  | 59.1  | 59.3  |
| 1549.7 | 15.8  | 18.4  | 17.0  | 15.7  | 15.6  | 15.5  |
| 1549.8 | 2.1   | 2.2   | 2.3   | 2.5   | 2.6   | 2.7   |
| 1549.9 | 2.7   | 2.8   | 2.7   | 2.9   | 2.6   | 2.7   |
| 1550.0 |       |       |       |       |       |       |
| 1550.1 | 56.9  | 57.7  | 58.3  | 59.0  | 59.1  | 59.3  |
| 1550.2 | 10.8  | 3.6   | 5.0   | 5.7   | 5.6   | 5.5   |
| 1550.3 | 11.8  | 6.3   | 8.6   | 7.8   | 7.7   | 7.6   |
| 1550.4 | 2.1   | 3.2   | 2.6   | 2.9   | 2.6   | 2.7   |
| 1550.5 |       |       |       |       |       |       |
| 1550.6 |       |       |       |       |       |       |
| 1550.7 |       |       |       |       |       |       |
| 1550.8 |       |       |       |       |       |       |
| 1550.9 |       |       |       |       |       |       |
| 1551.0 |       |       |       |       |       |       |
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| 1567.0 |       |       |       |       |       |       |
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| 1568.0 |       |       |       |       |       |       |
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| 1568.9 |       |       |       |       |       |       |
| 1569.0 |       |       |       |       |       |       |
| 1569.1 |       |       |       |       |       |       |
| 1569.2 |       |       |       |       |       |       |
| 1569.3 |       |       |       |       |       |       |
| 1569.4 |       |       |       |       |       |       |
| 1569.5 |       |       |       |       |       |       |
| 1569   |       |       |       |       |       |       |

POINSETTIA GRADES

|                         | W CB     | ECB      |
|-------------------------|----------|----------|
| 810.61 = BREAK ✓        | 15088    | 151.88   |
| 829.50 = FC ✓           | 149.54   | 150.54   |
| 849.27                  | 148.44   | 149.44   |
| 868.79 ✓                | 147.60   | 148.60   |
| 888.21                  | 147.01   | 148.18   |
| 907.63                  | 146.67   | 147.88   |
| 910.08 = FC ✓           |          |          |
| 927.40 ✓                | 146.58   | 147.59 ✓ |
| 947.40                  | 146.75   | 147.77 ✓ |
| 967.40                  | 147.17 ✓ | 148.20 ✓ |
| 1017 Jo = 5L Amery 1.33 | 149.0    | 148.54   |
| NL ✓                    | 150.80   | 151.34   |
| NL Sub.                 | 151.86   | 152.99   |

15826  
389  
15088  
105  
155.50

|        | W CB   | ECB    | FC     | AC     | Sub    |
|--------|--------|--------|--------|--------|--------|
| 15826  | 151.0  | 152.10 |        |        |        |
| 389    | U.5    | 3.0    |        |        |        |
| 15088  | U.5    | 3.0    |        |        |        |
| 105    | -1.0   | +0.4   |        |        |        |
| 155.50 |        |        |        |        |        |
| 122    |        |        |        |        |        |
| 159.48 |        |        |        |        |        |
| 12.34  |        |        |        |        |        |
| 147.09 |        |        |        |        |        |
| 120    |        |        |        |        |        |
| 145.89 |        |        |        |        |        |
| W CB   | 51.6   | 53.2   |        |        |        |
| EV     | 7.8    | 6.2    |        |        |        |
| 154357 | 5.7    | 2.2    |        |        |        |
| W CB   | 150.88 | 149.54 | 148.44 | 147.60 | 147.01 |
|        | 8.87   | 10.21  | 11.51  | 12.15  | 12.72  |
| FC     |        | 150.54 | 149.44 | 148.60 | 148.18 |
|        |        | 9.11   | 10.31  | 11.15  | 11.57  |
| 146.67 |        |        |        |        | 11.67  |
| 840    |        |        |        |        | 7.79   |
| 155.87 |        |        |        |        |        |
| W CB   | 146.58 | 146.75 | 147.17 | 149.0  |        |
|        | 8.49   | 8.32   | 7.90   | 6.07   |        |
| ECB    | 147.57 | 147.77 | 148.20 | 149.00 |        |
|        | 7.48   | 7.30   | 6.87   | 6.53   |        |
| FC     |        |        |        |        |        |
|        |        |        |        |        |        |
| ECB    | 149.48 | 150.48 | 150.97 | 151.50 |        |
|        | 8.14   | 7.61   | 7.10   | 6.57   |        |

JONQUILL DRIVE

| W.L. STA.     | W of   | E of   |
|---------------|--------|--------|
| N L ELLIOTT   | 157.43 | 158.37 |
| 20 N          | 158.86 | 159.48 |
| 40            | 160.21 | 160.52 |
| 60            | 161.41 | 161.44 |
| 80            | 162.42 | 162.22 |
| 100           | 163.34 | 162.89 |
| 120           | 164.01 | 163.42 |
| 140           | 164.57 | 163.83 |
| 160 N = P.C.  | 164.47 | 164.11 |
| 18116 BK      | 165.36 | 164.27 |
| 20232 BK      | 165.28 | 164.29 |
| 223.48 BK     | 165.19 | 164.19 |
| 258.82 = EC   | 164.74 | 163.74 |
| 318.20 = P.C. | 164.0  | 162.0  |
| 333.37        | 162.80 | 162.80 |
| 348.56        | 163.61 | 162.61 |
| 363.71        | 163.41 | 162.41 |
| 378.88        | 163.22 | 162.22 |
| 394.05        | 163.03 | 162.03 |
| 409.22        | 162.83 | 161.83 |
| 424.39        | 162.64 | 161.64 |
| 439.56        | 162.44 | 161.44 |
| 454.73        | 162.25 | 161.25 |
| 469.90        | 162.06 | 161.06 |
| 485.07        | 161.86 | 160.86 |

Def 106.30  
57.21.16  
41.21.15

1003.38  
C = 157.6 = 2

157.14  
155  
169.65

| E of  | 58.6                | 60.75              | 62.5               | 63.65               | 64.25                | 64.5                 | 64.6                 | 64.7                 |
|-------|---------------------|--------------------|--------------------|---------------------|----------------------|----------------------|----------------------|----------------------|
|       | 11.6<br>7.9<br>+3.1 | 8.9<br>6.3<br>+1.6 | 7.7<br>5.3<br>+1.8 | 6.8<br>4.7<br>+0.7  | 5.3<br>3.1<br>+1.5   | 5.1<br>3.0<br>+1.9   | 5.0<br>3.0<br>+2.0   | 5.2<br>3.2<br>+2.1   |
| W of  | 57.7                | 60.5               | 62.25              | 64.25               | 65.2                 | 65.6                 | 65.5                 | 65.45                |
|       | 11.4<br>9.0<br>+2.9 | 9.1<br>7.2<br>+1.9 | 7.0<br>4.7<br>+2.3 | 5.4<br>3.2<br>+2.2  | 4.2<br>2.2<br>+2.0   | 2.0<br>2.2<br>+1.1   | 2.1<br>2.1<br>+1.0   | 2.2<br>2.5<br>+1.7   |
| E of  | 124.0               | 62                 | 68                 | 71                  | 76                   | 79                   | 81.3                 | 83.3                 |
|       | 5.6<br>7.9<br>+2.3  | 8.6<br>5.2<br>+1.2 | 7.8<br>4.0<br>+1.0 | 6.6<br>3.0<br>+0.5  | 8.0<br>4.4<br>+0.4   | 7.9<br>4.0<br>+2.1   | 8.3<br>4.3<br>+1.9   | 8.3<br>4.3<br>+2.6   |
| W of  | 165.0               | 164.25             | 163.55             | 163.5               | 163.05               | 162.7                | 162.5                | 162.5                |
|       | 5.6<br>1.9<br>+2.7  | 5.4<br>1.0<br>+2.6 | 5.8<br>1.6<br>+4.2 | 6.7<br>3.2<br>+3.4  | 6.6<br>3.0<br>+3.6   | 6.9<br>4.0<br>+2.9   | 7.1<br>4.7<br>+2.4   | 7.1<br>4.7<br>+2.4   |
| E of  |                     |                    |                    |                     |                      |                      |                      |                      |
| 15035 | 1520                | 1515               | 1510               | 1505                | 1500                 | 1495                 | 1490                 | 1485                 |
|       | 13.15<br>6.3        | 12.15<br>6.3       | 11.15<br>6.3       | 10.15<br>6.3        | 9.15<br>6.3          | 8.15<br>6.3          | 7.15<br>6.3          | 6.15<br>6.3          |
| W of  | 162.10              | 162.0              | 161.9              | 161.8               | 161.7                | 161.6                | 161.5                | 161.4                |
|       | 7.5<br>5.8<br>+1.7  | 6.5<br>4.8<br>+1.7 | 5.5<br>3.8<br>+1.7 | 4.5<br>2.8<br>+1.7  | 3.5<br>1.8<br>+1.7   | 2.5<br>0.8<br>+1.7   | 1.5<br>-0.2<br>+1.7  | 0.5<br>-1.2<br>+1.7  |
| E of  | 158.7               | 159.85             | 160.52             | 161.14              | 162.23               | 162.84               | 162.84               | 162.84               |
|       | 7.5<br>5.8<br>+1.7  | 6.5<br>4.8<br>+1.7 | 5.5<br>3.8<br>+1.7 | 4.5<br>2.8<br>+1.7  | 3.5<br>1.8<br>+1.7   | 2.5<br>0.8<br>+1.7   | 1.5<br>-0.2<br>+1.7  | 0.5<br>-1.2<br>+1.7  |
| W of  | 163.0               | 164.25             | 164.85             | 164.63              | 164.97               | 165.36               | 165.25               | 165.25               |
|       | 2.6<br>1.6<br>+1.0  | 3.2<br>2.2<br>+1.0 | 3.7<br>2.7<br>+1.0 | 3.9<br>2.9<br>+1.0  | 3.6<br>2.6<br>+1.0   | 3.3<br>2.3<br>+1.0   | 3.3<br>2.3<br>+1.0   | 3.3<br>2.3<br>+1.0   |
| E of  | 163.22              | 163.67             | 164.08             | 163.87              | 164.11               | 164.27               | 164.27               | 164.27               |
|       | 5.7<br>3.7<br>+2.0  | 4.7<br>2.7<br>+2.0 | 3.7<br>1.7<br>+2.0 | 2.7<br>0.7<br>+2.0  | 1.7<br>-0.3<br>+2.0  | 0.7<br>-1.3<br>+2.0  | 0.7<br>-1.3<br>+2.0  | 0.7<br>-1.3<br>+2.0  |
| W of  | 165.14              | 164.97             | 164.74             | 164.63              | 164.57               | 164.51               | 164.51               | 164.51               |
|       | 3.0<br>2.0<br>+1.0  | 2.0<br>1.0<br>+1.0 | 1.0<br>0.0<br>+1.0 | 0.0<br>-1.0<br>+1.0 | -1.0<br>-2.0<br>+1.0 | -2.0<br>-3.0<br>+1.0 | -3.0<br>-4.0<br>+1.0 | -4.0<br>-5.0<br>+1.0 |
| E of  | 164.9               | 164.7              | 164.5              | 164.3               | 164.1                | 163.9                | 163.7                | 163.5                |
|       | 4.0<br>3.0<br>+1.0  | 3.0<br>2.0<br>+1.0 | 2.0<br>1.0<br>+1.0 | 1.0<br>0.0<br>+1.0  | 0.0<br>-1.0<br>+1.0  | -1.0<br>-2.0<br>+1.0 | -2.0<br>-3.0<br>+1.0 | -3.0<br>-4.0<br>+1.0 |
| W of  | 163.22              | 163.67             | 164.08             | 164.63              | 164.97               | 165.36               | 165.25               | 165.25               |
|       | 5.1<br>4.1<br>+1.0  | 4.1<br>3.1<br>+1.0 | 3.1<br>2.1<br>+1.0 | 2.1<br>1.1<br>+1.0  | 1.1<br>0.1<br>+1.0   | 0.1<br>-0.9<br>+1.0  | -0.9<br>-1.9<br>+1.0 | -1.9<br>-2.9<br>+1.0 |
| W of  | 162.06              | 161.86             | 161.66             | 161.46              | 161.26               | 161.06               | 160.86               | 160.66               |
|       | 4.6<br>3.6<br>+1.0  | 3.6<br>2.6<br>+1.0 | 2.6<br>1.6<br>+1.0 | 1.6<br>0.6<br>+1.0  | 0.6<br>-0.4<br>+1.0  | -0.4<br>-1.4<br>+1.0 | -1.4<br>-2.4<br>+1.0 | -2.4<br>-3.4<br>+1.0 |

JONQUILL DRIVE

|                 | wcb    | ECB    |
|-----------------|--------|--------|
| 5002 ✓          | 161.67 | 160.67 |
| 5154 ✓          | 161.47 | 160.47 |
| 53058 ✓         | 161.28 | 160.28 |
| 54575 ✓         | 161.09 | 160.09 |
| 5609 ✓          | 160.89 | 159.89 |
| 57609 ✓         | 160.70 | 159.70 |
| 5914 ✓          | 160.50 | 159.50 |
| 616.14          | 160.66 | 158.75 |
| 6408 ✓ = PCE.   | 160.84 | 158.0  |
| 666.68          | 161.0  |        |
| 692.48          | 161.17 |        |
| 718.31          | 161.34 |        |
| 744.14 = BREAK  | 161.50 |        |
| 768.01          | 161.25 |        |
| 791.88 ✓        | 161.0  |        |
| 815.75          | 160.75 |        |
| 839.6 ✓ = BREAK | 160.50 |        |
| 859.20          | 160.30 |        |
| 875.78          | 160.2  |        |
| 898.36 ✓        | 159.94 |        |
| 917.94          | 159.75 |        |
| 927.5 ✓         | 159.57 |        |
| 957.10          | 159.38 |        |
| 976.68 = BREAK  | 159.20 |        |

Panseller.

4

| ECB             | 60.90  | 60.50  | 60.15  | 59.75  | 159.0  | 158.25 |
|-----------------|--------|--------|--------|--------|--------|--------|
|                 | 8.7    | 9.1    | 9.5    | 9.9    | 10.6   | 11.2   |
|                 | 10.6   | 9.7    | 9.3    | 9.4    | 10.3   | 10.4   |
|                 | -1.9   | -0.6   | +0.2   | +0.5   | +0.3   | +1.0   |
| wcb             | 61.70  | 61.15  | 60.75  | 60.40  | 61.05  | 61.25  |
|                 | 7.9    | 11.1   | 11.5   | 11.3   | 11.2   | 11.0   |
|                 | 6.9    | 9.1    | 9.5    | 9.8    | 9.7    | 9.5    |
|                 | +1.6   | +2.0   | +2.0   | +1.5   | +1.5   | +1.5   |
| wcb             | 61.60  | 61.25  | 61.5   | 61.25  | 61.0   | 60.75  |
|                 | 10.6   | 10.2   | 10.7   | 11.0   | 11.2   | 11.5   |
|                 | 8.8    | 8.6    | 8.4    | 8.2    | 8.2    | 8.2    |
|                 | +1.8   | +1.9   | +2.3   | +2.8   | +3.3   | +3.3   |
| wcb             | 60.20  | 160.0  | 59.5   | 59.6   | 59.45  |        |
|                 | 14.0   | 14.2   | 14.4   | 14.6   | 14.8   |        |
|                 | 5.1    | 5.1    | 4.9    | 5.1    | 5.2    |        |
|                 | +6.9   | +7.1   | +7.5   | +7.5   | +7.8   |        |
| 15740 DM        |        |        |        |        |        |        |
| wcb             | 160.90 | 161.15 | 160.95 | 161.29 | 161.25 | 161.50 |
|                 | 3.63   | 3.38   | 3.58   | 3.47   | 3.37   | 3.17   |
| wcb             | 161.10 | 160.80 | 160.70 | 160.50 | 160.30 | 159.90 |
|                 | 3.49   | 3.63   | 3.73   | 4.03   | 4.21   | 4.59   |
| wcb             | 159.57 | 159.35 | 159.20 |        |        |        |
|                 | 3.46   | 3.17   | 3.38   |        |        |        |
| 16000 ✓         |        |        |        |        |        |        |
| wcb             | 161.67 | 161.47 | 161.28 | 161.09 | 160.89 | 160.70 |
|                 | 2.45   | 2.85   | 3.04   | 3.23   | 3.43   | 3.62   |
| wcb             | 160.50 | 160.67 | 160.74 | 160.96 | 160.96 | 160.70 |
|                 | 5.65   | 5.85   | 6.04   |        |        |        |
| wcb             | 161.67 | 161.47 | 161.28 | 161.09 | 160.89 | 160.70 |
|                 | ✓      | ✓      | ✓      | ✓      | ✓      | ✓      |
| wcb             | 160.61 | 160.73 | 161.0  |        |        |        |
|                 | 5.71   | 5.89   | 5.37   |        |        |        |
| SP Return       | 158.50 | 159.00 | 158.90 | 158.60 | 158.00 | 158.0  |
| Jonquil + botug | 6.8    | 7.0    | 7.4    | 7.7    | 8.0    | 8.2    |

NIPOMA ST

|               |        |        |
|---------------|--------|--------|
|               | S CB   | N CB   |
| WL POINSETTIA | 156.30 | 157.50 |
| 25' W ON SL   | 156.50 |        |
| EL ALLEY      | 144.0  | 145.0  |

FIMARILLIS West of POINSETTIA

|                  |        |        |
|------------------|--------|--------|
|                  | S CB   | N CB   |
| WL POINSETTIA    | 149.00 | 150.80 |
| 23.33' W ON SL   | 149.80 |        |
| 73.3' W          | 146.60 | 145.40 |
| EL ALLEY         | 139.0  |        |
| 101.6' W ON N=PC |        | 140.0  |
| 50.8' W          |        | 139.5  |
| EL ALLEY         |        | 139.0  |

ELLIOTT ST West of POINSETTIA

|                                  |        |        |
|----------------------------------|--------|--------|
|                                  | S CB   | N CB   |
| WL VILVA DR.                     | 148.70 |        |
| PC                               | 147.41 |        |
| 70.90' W = BREAK = WL POINSETTIA | 146.88 | 147.88 |
| +61.30'                          | 140.94 | 141.94 |
| 1+22.65'                         | 135.0  | 136.0  |

148.9

5  
5

|        |       |        |        |        |        |        |        |
|--------|-------|--------|--------|--------|--------|--------|--------|
|        | SC    | 149.45 | 150.0  | 149.65 | 149.45 |        |        |
|        |       | -1.9   | -7.4   | 3.6    | 9.0    |        |        |
|        |       |        |        | 17.1   | 4.3    |        |        |
|        |       |        |        | -7.5   | -5.2   |        |        |
|        | NC    |        |        | 148.65 | 148.65 | 139.85 | 139.45 |
| 157.40 |       |        |        | 14.6   | 8.0    | 8.5    | 9.0    |
| 5.6    |       |        |        | 1.3    | 4.2    | 5.3    | 7.0    |
| 13.06  |       |        |        | 1.1    | 5.6    | 3.3    | 11.0   |
| 12.25  | SC    | 156.40 | 156.07 | 154.89 | 150.25 | 144.0  |        |
| 12.08  |       | 6.46   | 7.00   | 8.17   | 17.81  | 8.23   |        |
| 12.22  |       |        |        |        |        |        |        |
|        | NC    | 157.50 | 157.0  | 155.50 | 151.25 | 144.0  |        |
|        |       | 5.56   | 6.6    | 7.56   | 17.81  | 7.33   |        |
|        |       |        |        |        |        |        |        |
| 155.00 |       |        |        |        |        |        |        |
| 0.97   | SC    | 156.55 | 156.75 | 144.45 |        |        |        |
| 126.5  |       | -3.0   | -6.2   | 17.3   |        |        |        |
|        |       |        |        | 15.8   |        |        |        |
|        |       |        |        | -3.5   |        |        |        |
|        | NC    | 157.75 |        | 145.25 |        |        |        |
|        |       |        |        | 11.3   |        |        |        |
|        |       |        |        | 11.3   |        |        |        |
|        |       |        |        | 2.1    |        |        |        |
| 155.07 |       |        |        |        |        |        |        |
| 10.29  | SC    | 149.0  | 149.2  | 149.6  | 149.5  | 148.8  | 144.68 |
| 14.68  |       | 6.7    | 5.77   | 5.47   | 5.57   | 6.77   | 10.39  |
| 1.39   |       |        |        |        |        |        | 6.50   |
| 146.07 |       |        |        |        |        |        | 7.07   |
|        | NC    | 150.56 | 150.60 | 150.20 | 149.55 | 148.00 | 140.0  |
|        |       | 1.27   | 4.47   | 4.87   | 5.57   | 9.67   | 6.07   |
|        |       |        |        |        |        |        | 6.77   |
|        |       |        |        |        |        |        | 7.07   |
|        |       |        |        |        |        |        |        |
|        | NECOR |        |        |        |        |        |        |
|        | ECT   | 151.2  | 152.99 |        |        |        |        |
|        |       | 3.93   | 4.08   |        |        |        |        |
|        |       |        |        |        |        |        |        |
|        | Wct   | 151.86 |        |        |        |        |        |
|        |       | 3.71   |        |        |        |        |        |
| 150.35 |       |        |        |        |        |        |        |
| 0.07   |       |        |        |        |        |        |        |
| 151.22 | SC    | 149.0  | 147.7  | 147.1  | 141.20 | 135.25 |        |
|        |       | 4.4    | 3.5    | 4.1    | 10.0   | 16.0   |        |
|        |       | 4.5    | 6.9    | 8.0    | 11.4   | 16.9   |        |
|        |       | 2.3    | -3.4   | -3.7   | -1.4   | -0.9   |        |
|        |       |        |        |        |        |        |        |
|        | NC    | 148.10 | 142.20 |        | 136.25 |        |        |
|        |       | 8.1    | 9.0    |        | 15.0   |        |        |
|        |       | 4.9    | 9.0    |        | 15.7   |        |        |
|        |       | -1.8   | 0.0    |        | -2.2   |        |        |



# LOTUS DRIVE

| NL STA                               | SCT   | NCT                        |
|--------------------------------------|-------|----------------------------|
| W. HYACINTH                          |       | 127.20                     |
| Curve                                |       | 128.60                     |
| PC = 0+00 NL STA                     | 131.0 | 130.00                     |
| 25.41 W                              | 132.0 | 131.01                     |
| 50.82 ✓                              | 133.0 | 132.63                     |
| 76.23                                | 134.0 | 133.05                     |
| 101.64                               | 135.0 | 134.06                     |
| 127.05                               | 136.0 | 135.07                     |
| 152.46                               | 137.0 | 136.69                     |
| 177.87                               | 138.0 | 137.11                     |
| 203.78 = C.C. BREAK                  | 139.0 | 138.14                     |
| 243.17 = 1st AMARYLLIS               |       | 139.74                     |
| 304.11 = WV ✓                        |       | 141.0 BREAK                |
| 228.08 W                             | 140.0 | NL STA.<br>354.11 W 142.81 |
| 252.88                               | 141.0 | 404.11 ✓ 144.63            |
| 277.68                               | 142.0 | 454.11 ✓ 146.45            |
| 302.48 = BREAK opposite WV Amaryllis | 143.0 | 483.16 ✓ 147.50            |
| 327.28                               | 143.5 |                            |
| 352.08                               | 144.0 |                            |
| 376.88                               | 144.5 |                            |
| 401.68                               | 145.0 |                            |
| 426.48                               | 145.5 |                            |
| 451.28 = BREAK                       | 146.0 |                            |

R = 270 W  
 R = 270 W  
 R = 270 W

dot = 1' 58" 26"  
 CH = 24.80

150.15  
 0.14  
150.34  
 9.93  
 40.41  
 44.46  
144.87

| SCT | 146.2         | 147.7  | 148.2  | 149.7  | 151.2  | 152.7 | 153.2 | 154.7 | 156.2 |
|-----|---------------|--------|--------|--------|--------|-------|-------|-------|-------|
|     | 4.1           | 1.6    | 5.1    | 5.6    | 6.1    | 6.6   | 7.1   | 7.6   | 8.1   |
|     | 3.7           | 4.5    | 3.1    | 3.1    | 3.7    | 4.1   | 4.9   | 5.4   | 5.1   |
|     | +0.4          |        | +2.0   | +2.5   | +2.7   | +2.5  | +2.2  | +2.2  | +2.2  |
| NCT | 47.7          | 46.7   | 46.9   | 43.0   | 41.25  | 40.0  |       |       |       |
|     | 8.2           | 3.4    | 5.4    | 2.3    | 9.1    | 10.3  |       |       |       |
|     | 0.1           | 0.2    | 0.4    | 0.8    | 3.0    | 1.6   |       |       |       |
|     | +2.5          | +2.8   | +3.0   | +3.5   | +7.1   | -2.2  |       |       |       |
| SCT | 41.2          | 44.2   | 49.2   | 38.2   | 37.2   | 36.2  | 35.2  | 34.2  |       |
|     | 9.7           | 10.1   | 11.1   | 14.1   | 13.1   | 12.1  | 11.1  | 10.1  |       |
|     | 6.9           | 7.0    | 8.0    | 9.2    | 9.8    | 9.2   | 8.2   | 7.2   |       |
|     | +2.2          | +2.7   | +2.2   | +2.5   | +2.3   | +2.2  | +2.2  | +2.2  |       |
| NCT | 27.5          | 28.5   | 30.25  | 32.3   | 29.3   | 28.3  | 27.3  | 26.3  |       |
|     | 12.3          | 11.0   | 9.6    | 8.5    | 7.5    | 6.5   | 5.5   | 4.5   |       |
|     | 11.0          | 10.4   | 10.1   | 9.5    | 9.0    | 8.3   | 7.3   | 6.3   |       |
|     | +1.3          | +0.4   | -1.5   | -1.3   | -1.5   | -1.8  | -1.8  | -1.8  |       |
| SCT | 131.25        | 122.25 | 122.25 | 122.25 | 122.25 |       |       |       |       |
|     | 8.6           | 7.6    | 6.6    | 5.6    | 4.6    |       |       |       |       |
|     | 4.3           | 5.0    | 6.4    | 5.6    | 1.7    |       |       |       |       |
|     | +2.3          | +2.6   | +3.2   | +3.9   |        |       |       |       |       |
| NCT | 25.2          | 26.3   | 27.4   | 28.4   | 29.0   |       |       |       |       |
|     | 4.5           | 3.5    | 2.4    | 1.4    |        |       |       |       |       |
|     | 0.3           | 5.7    | 5.0    | 3.9    |        |       |       |       |       |
|     | -1.8          | 2.2    | 2.6    | -2.5   |        |       |       |       |       |
|     | 139.61        | 142.0  |        | 147.50 |        |       |       |       |       |
|     | 9.23          | 7.84   | raked  | 1.34   |        |       |       |       |       |
|     | 148.84 = H.Z. |        |        |        |        |       |       |       |       |
| NCT | 27.0          | 27.76  | 28.24  | 28.88  | 29.44  | 30.0  | 31.0  | 32.03 | 32.65 |
|     | 7.14          | 7.23   | 6.47   | 6.11   | 5.55   | 4.99  | 3.98  | 2.96  | 1.94  |
| SCT |               |        |        |        |        | 31.0  | 32.0  | 33.0  | 34.0  |
|     |               |        |        |        |        | 3.99  | 4.99  | 5.99  | 6.99  |
| NCT | 34.06         | 35.07  | 36.09  | 37.11  | 38.14  | 39.24 | 40.10 |       |       |
|     | 0.73          | 1.82   | 1.80   | 1.78   | 1.75   | 5.15  | 3.89  |       |       |
| SCT | 35.0          | 36.0   | 37.0   | 38.0   | 39.0   | 40.0  | 41.0  | 42.0  |       |
|     | 8.84          | 7.84   | 6.84   | 5.84   | 4.84   | 3.84  | 2.84  | 1.84  |       |
| SCT | 143.0         | 143.50 | 144.0  | 144.5  | 145.0  | 145.5 | 146.0 |       |       |
|     | 1.84          | 1.34   | 0.84   | 0.34   | 0.70   | 5.70  | 5.20  |       |       |



NARCISSUS DRIVE

| W.L. STA.          | WCB    | ECB    |
|--------------------|--------|--------|
| N L ELLIOTT = 0+00 | 156.40 | 154.03 |
| 50 W               | 154.60 | 152.40 |
| 100 W              | 152.81 | 151.02 |
| 150                | 151.01 | 149.64 |
| 191.94 BREAK       | 149.50 | 148.50 |
| 250                | 149.15 |        |
| 270.32 = P.C.      | 149.03 |        |
| 295.97             | 148.88 |        |
| 321.62             | 148.74 |        |
| 347.27             | 148.60 |        |
| 372.92             | 148.45 |        |
| 398.57             | 148.30 |        |
| 424.22             | 148.16 |        |
| 449.87             | 148.01 |        |
| 475.52             | 147.87 |        |
| 501.17             | 147.72 |        |
| 526.82             | 147.58 |        |
| 552.47             | 147.43 |        |
| 578.12             | 147.28 |        |
| 603.77             | 147.14 |        |
| 629.42 = E.C.      | 147.0  | 146.0  |
| C Curve            | 147.25 |        |
| E.C. =             | 148.50 | 147.50 |

104503.0  
3 20 06 0  
5 15 09 0  
7 00 12 0  
8 45 15 0

2565  
2199

14' 0" DISTANCE  
20' 0" DISTANCE  
15' 0" DISTANCE  
21' 0" DISTANCE  
13' 0" DISTANCE  
25' DISTANCE FROM SL

1571.6

8

| W.L.   | 56.6  | 54.8  | 53.3  | 51.2  | 49.7  | 49.4  | 49.2  | 49.2  | 49.0  |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1571.6 | 1.0   | 2.8   | 4.6   | 6.4   | 7.9   | 8.2   | 8.4   | 8.4   | 8.6   |
| 160.30 | 1.5   | 2.7   | 4.0   | 5.7   | 7.6   | 8.7   | 8.7   | 8.4   | 8.2   |
|        | -0.5  | +0.1  | +0.6  | +0.7  | +0.3  | +1.5  | +1.7  | +1.0  | +1.4  |
| EL     | 54.3  | 52.0  | 51.2  | 49.9  | 49    | 49    | 49.4  | 49.4  | 49.6  |
|        | 3.3   | 5.0   | 5.4   | 7.7   | 14.3  | 9.3   | 12.4  | 14.0  | 9.6   |
|        | -0.7  | -0.5  | -0.7  | -0.9  | -3.4  | -0.6  | -2.8  | -1.6  | 0.0   |
| WL     | 48.8  | 48.6  | 48.5  | 48.4  | 48.2  | 48.1  | 48.0  | 47.8  | 47.65 |
|        | 8.8   | 9.0   | 9.1   | 9.0   | 9.4   | 9.5   | 9.6   | 9.8   | 10.0  |
|        | 7.1   | 7.8   | 8.4   | 9.4   | 9.2   | 9.1   | 9.4   | 9.8   | 10.0  |
|        | +2.7  | +1.4  | +0.7  | -0.4  | +0.2  | +0.4  | +0.2  | 0.0   | 0.0   |
| EL     | 44    | 100   | 10.1  | 10.2  | 10.2  | 10.5  | 10.6  | 10.8  | 11.0  |
|        | 8.9   | 9.4   | 10.0  | 10.6  | 12.0  | 12.0  | 11.6  | 11.8  | 11.7  |
|        | +2.9  | +0.6  | +0.1  | -0.4  | -1.6  | -1.5  | -1.0  | -1.0  | -0.7  |
| WL     | 47.5  | 47.2  | 47.25 | 47.0  | 46.75 | 46.75 | 46.75 | 46.75 | 46.75 |
|        | 10.1  | 10.2  | 10.2  | 9.6   | 8.9   | 8.9   | 8.9   | 8.9   | 8.9   |
|        | 10.0  | 9.9   | 9.3   | 8.8   | 8.2   | 8.2   | 8.2   | 8.2   | 8.2   |
|        | +0.1  | +0.3  | +1.1  | +0.8  | +0.5  |       |       |       |       |
| EL     | 11.1  | 11.2  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  |
|        | 11.7  | 11.4  | 11.1  | 11.1  | 11.1  | 11.1  | 11.1  | 11.1  | 11.1  |
|        | -0.6  | -0.2  | +0.3  |       |       |       |       |       |       |
| 15120  | 117.0 | 125.5 | 125.0 | 127.5 | 148.0 | 148.5 | 148.0 | 148.0 | 148.0 |
|        | 1.0   | 3.5   | 3.7   | 3.5   | 3.0   | 0.9   | 1.7   |       |       |

| WCB    | 156.40 | 149.50 | 149.03 | 48.8 | 48.74 | 48.60 | 48.65 |
|--------|--------|--------|--------|------|-------|-------|-------|
| 1571.6 | 3.89   | 10.09  | 10.56  | 3.19 | 3.33  | 3.33  | 3.27  |
| 159.59 |        |        |        |      |       |       |       |
| 149.03 |        | 149.50 |        |      |       |       |       |
| 157.01 |        | 3.57   |        |      |       |       |       |
| EL     | 154.03 | 149.50 |        |      |       |       |       |
|        |        | 5.57   |        |      |       |       |       |

| WCB | 48.30 | 48.16 | 48.01 | 47.87 | 47.72 | 47.58 | 47.43 | 47.28 |
|-----|-------|-------|-------|-------|-------|-------|-------|-------|
|     | 3.77  | 3.91  | 4.00  | 4.10  | 4.35  | 4.49  | 4.64  | 4.79  |
|     | 47.14 | 47.0  |       |       |       |       |       |       |
|     | 4.9   | 5.0   |       |       |       |       |       |       |



AMARYLLIS DRIVE

|                             | S CB   | N CB   |
|-----------------------------|--------|--------|
| 633.68                      | 148.82 | 147.79 |
| 648.33 = EC                 | 148.92 | 147.89 |
| 700                         | 149.26 | 148.33 |
| 750                         | 149.60 | 148.76 |
| 783.33 = ELHYACINTH         | 149.82 | 149.04 |
| 804.30 = PC                 | 149.96 |        |
| 822.74 A7°33'<br>SLR=1000   | 150.09 |        |
| 841.14 = W. HYACINTH        | 150.20 | 149.50 |
| 859.58 0°31'41"<br>1°03'22" | 150.32 | 149.64 |
| 878.02 1°34'03"<br>2°06'44" | 150.44 | 149.78 |
| 896.46 2°38'25"<br>3°10'06" | 150.56 | 149.93 |
| 914.90 3°46'28"             | 150.68 | 150.07 |
| 936.07 = EC                 | 150.82 | 150.23 |
| 987.01                      | 151.16 | 150.62 |
| 1037.95 = PC ON SV          | 151.50 | 151.0  |
| 1081.93 = NL SL             | 150.0  | 151.34 |
| = EC                        | 148.54 |        |

C=19.54 NL  
C=18.44 SL

Last E =  
NL=22.40  
SL=21.17

AMARYLLIS CULVERT

def. = 23° 50' 55" = Lot Line of 13+14 BKED Ch= 8894

|            |            |        |
|------------|------------|--------|
| Chamber #1 | Flowline = | 133.0  |
|            |            | 131.50 |
|            |            | 131.3  |

156.57

0.50  
126.07  
51.0

161.17

|        |                     |                     |                     |                     |                    |                    |                    |                    |                    |
|--------|---------------------|---------------------|---------------------|---------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| NCL    | 148.0               | 148.1               | 148.6               | 149.0               | 149.3              | 149.5              | 149.9              | 150.0              | 150.2              |
|        | 8.6<br>4.5<br>+4.1  | 8.5<br>4.0<br>+4.3  | 8.0<br>4.4<br>+3.6  | 7.6<br>4.6<br>+3.0  | 7.3<br>4.1<br>+3.2 | 6.9<br>3.8<br>+3.1 | 6.7<br>3.3<br>+3.4 | 6.6<br>2.8<br>+3.8 | 6.5<br>2.3<br>+4.2 |
| SL*    | 149.0               | 149.1               | 149.5               | 149.5               | 150.1              | 150.2              | 150.3              | 150.5              | 150.6              |
|        | 7.6<br>3.3<br>+4.3  | 7.5<br>3.1<br>+4.4  | 7.1<br>3.2<br>+3.7  | 6.7<br>3.2<br>+3.5  | 6.5<br>2.9<br>+3.6 | 6.4<br>2.8<br>+3.6 | 6.3<br>2.7<br>+3.6 | 6.2<br>2.6<br>+3.6 | 6.1<br>2.5<br>+3.6 |
| NCL    | 50.3                | 50.5                | 50.9                | 51.25               | 51.6               |                    |                    |                    |                    |
|        | 6.3<br>3.2<br>+3.1  | 6.1<br>2.8<br>+3.3  | 5.7<br>2.3<br>+3.4  | 5.0<br>2.6<br>+2.4  | 4.6<br>2.3<br>+2.3 |                    |                    |                    |                    |
| SL     | 50.7                | 50.8                | 50.9                | 51.25               | 51.4               | 51.75              | 52.05              | 48.5               |                    |
|        | 10.5<br>8.0<br>+2.5 | 10.2<br>6.5<br>+3.7 | 10.3<br>5.6<br>+4.7 | 10.1<br>5.1<br>+5.0 | 9.8<br>4.7<br>+5.1 | 9.4<br>4.3<br>+5.1 | 9.0<br>3.9<br>+5.1 | 8.5<br>3.8<br>+4.7 |                    |
| 5111 T | Set                 | 43.44               | 43.96               |                     |                    |                    |                    |                    |                    |
|        | 2.19                | 2.19                | 4.36                |                     |                    |                    |                    |                    |                    |
| 147.59 | NCL                 | 47.79               | 47.89 TP            | 49.04               |                    |                    |                    |                    |                    |
| 154.33 |                     | 3.34                | 3.00                | 2.78                |                    |                    |                    |                    |                    |
| 157.10 | N                   | 151.34              | 149.50              | 150.23              |                    |                    |                    |                    |                    |
| 158.37 |                     | 6.95                | 8.82                | 8.09                |                    |                    |                    |                    |                    |
|        | S                   | 151.50              | 150.82              |                     |                    |                    |                    |                    |                    |
|        |                     | 6.82                | 7.50                |                     |                    |                    |                    |                    |                    |

# HYACINTH DRIVE

AT AMARYLLIS

W C6

E C6

N. C. AMARYLLIS

= P.C. 0+00

149.50

1 30° 08' 21" PL  
2 6° 16' 42"  
3 9° 25' 03"  
4 12° 33' 24"  
5 15° 41' 45"

147.94

146.38

144.82

P.L.C. = 21.36

143.26

17.1 = 10.78 more

S = Add. Line = EC

141.70

N. C. AMARYLLIS

= P.C. 0+00

149.04

1 3° 47' 51"

147.61

2 7° 35' 42"

146.18

3 11° 23' 33"

144.76

4 15° 11' 24"

143.33

5 18° 59' 15"

141.91

6 22° 47' 06"

140.48

7 = E.C. 26° 24' 57"

139.06

+ 37.38

136.10

156.57

12.02

144.55

4.78

149.30

11

|    |       |      |      |      |       |      |      |       |
|----|-------|------|------|------|-------|------|------|-------|
| EL | 47.86 | 46.6 | 45.0 | 43.6 | 42.15 | 40.7 | 39.3 | 37.35 |
|    | 8.7   | 10.4 | 11.6 | 13.0 | 14.4  | 15.9 | 17.3 | 20.3  |
|    | 12.0  | 10.0 | 8.8  | 8.0  | 8.8   | 9.8  | 11.4 | 14.1  |
|    | -3.3  | -2.0 | -2.2 | -2.0 | +5.6  | +6.0 | +6.2 | +2.4  |

|    |      |      |      |      |       |  |  |  |
|----|------|------|------|------|-------|--|--|--|
| WL | 48.2 | 46.6 | 45.0 | 43.5 | 41.95 |  |  |  |
|    | 1.1  | 2.7  | 4.3  | 5.8  | 7.4   |  |  |  |
|    | 0.7  | 6.4  | 10.5 | 13.8 | 17.7  |  |  |  |
|    | +0.4 | -3.7 | -6.7 | -8.0 | -10.3 |  |  |  |

158.87

10.10

148.77

1.15

149.37

|   |        |       |       |       |       |       |       |
|---|--------|-------|-------|-------|-------|-------|-------|
| W | 149.40 | 47.94 | 46.38 | 44.82 | 43.26 | 41.70 | 40.92 |
|   | 8.92   | 10.43 | 11.79 | 13.54 | 15.11 | 16.67 | 18.25 |

|   |        |       |       |       |       |       |       |       |
|---|--------|-------|-------|-------|-------|-------|-------|-------|
| E | 149.04 | 47.61 | 46.14 | 44.76 | 43.33 | 41.91 | 40.48 | 39.06 |
|   | 2.33   | 1.76  | 2.19  | 2.61  | 3.04  | 3.46  | 3.89  | 4.31  |

E 361.0  
13.87

W C = 101.31 Meters

Δ 30° 06'

# HYACINTH DRIVE

| W/L STA.                                    | W CB   | EL STA      | E CB   |
|---------------------------------------------|--------|-------------|--------|
| NL WING                                     | 116.75 |             | 115.0  |
| 50' N                                       | 116.55 | ↑ 111.7     | 115.10 |
| 100                                         | 116.34 |             | 115.20 |
| 136.85 = SL PLUMOSA                         | 116.20 | SLAZALEA ↓  | 115.30 |
| 230.30 = NL ✓                               | 117.70 | NL ✓        | 116.67 |
| 250 ✓                                       | 118.37 | 50' N       | 118.32 |
| 300                                         | 120.09 | 100'        | 119.97 |
| 350                                         | 121.80 | 150         | 121.62 |
| 400                                         | 123.52 | 200         | 123.27 |
| 450                                         | 125.23 | 262.9N BK   | 125.36 |
| 466.20 = PC = BREAK<br>A: 35° 57' 20"       | 125.80 | 282.9N BK   | 125.91 |
| 4° 29' 40"                                  | 126.67 | 286.26 = PC | 125.98 |
| 6° 59' 40"                                  | 127.54 | 299.29 BK   | 126.23 |
| 13° 29' 00"                                 | 128.42 | 318.68 BK   | 126.34 |
| 17° 52' 40"                                 |        |             |        |
| 541.60 = PCC<br>C: 1800 A: 5° 45' 45"       | 129.30 | 332.04 BK   | 126.22 |
|                                             | 130.15 | 348.40 BK   | 125.88 |
| SL LOTUS<br>det = 10' 26" 26"<br>5' 25" 50" | 131.0  | 364.76 BK   | 125.31 |
|                                             |        | 370.72 = EC | 125.07 |
| NL LOTUS                                    | 127.20 | 383.89      | 124.53 |
|                                             |        | 400.72 = PC | 123.70 |
|                                             |        | 404.16 BK   | 123.52 |

OVER

# HYACINTH DRIVE NORTH OF LOTUS

WL STA

|                                   | WCB    | ECB    |
|-----------------------------------|--------|--------|
| 41.8' Not in Lotus<br>= PC = 0+00 | 124.81 | 123.70 |
| 396' N (B)                        | 124.60 | 123.54 |
| 08' 57"                           |        |        |
| 24.37                             | 123.42 | 122.39 |
| 10° 03' 54"                       |        |        |
| 41.48 (C)                         | 122.46 | 121.26 |
| 08' 58" 41"                       |        |        |
| 2° 52' 58"                        |        |        |
| 60.59 (B)                         | 121.22 | 120.22 |
| 3° 47' 15"                        |        |        |
| 79.70 (B)                         | 120.24 | 119.32 |
| 4° 42' 02"                        |        |        |
| 5° 36' 49"                        |        |        |
| 98.81 (B)                         | 119.63 | 118.63 |
| 6° 31' 36"                        |        |        |
| 117.94 (D)                        | 119.17 | 118.17 |
| 7° 26' 23"                        |        |        |
| 8° 17' 56"                        |        |        |
| 137.03 (B)                        | 118.69 | 117.69 |
| 9° 09' 29"                        |        |        |
| 156.14 (D)                        | 118.46 | 117.46 |
| 10° 01' 02"                       |        |        |
| 174.10                            | 118.32 | 117.32 |
| 192.06                            | 118.18 | 117.18 |
| 210.02 P.C.C.                     | 118.04 | 117.04 |
| Δ 8° 10' 27"                      |        |        |
| 231.44                            | 117.89 | 116.88 |
| 0° 40' 52"                        |        |        |
| 252.86                            | 117.73 | 116.73 |
| 1° 41' 44"                        |        |        |
| 274.28                            | 117.57 | 116.57 |
| 2° 02' 36"                        |        |        |
| 295.70                            | 117.41 | 116.42 |
| 2° 43' 28"                        |        |        |
| 317.12                            | 117.25 | 116.27 |
| 3° 24' 20"                        |        |        |
| 338.54                            | 117.10 |        |
| 4° 05' 12"                        |        |        |

1257.00  
0.22  
127.09

| WL  | 175.0  | 20.7   | 22.5   | 21.5   | 20.6   | 19.9   | 19.4   | 18.9   | 18.7   |
|-----|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| EL  | 124.0  | 123.6  | 123.5  | 123.5  | 123.4  | 123.3  | 123.2  | 123.1  | 123.0  |
| WCB | 124.81 | 124.60 | 124.40 | 124.20 | 124.00 | 123.80 | 123.60 | 123.40 | 123.20 |
| ECB | 123.70 | 123.54 | 123.39 | 123.26 | 123.12 | 122.98 | 122.84 | 122.70 | 122.56 |
| WCB | 121.22 | 121.22 | 121.22 | 121.22 | 121.22 | 121.22 | 121.22 | 121.22 | 121.22 |
| ECB | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 | 120.22 |
| WCB | 119.63 | 119.63 | 119.63 | 119.63 | 119.63 | 119.63 | 119.63 | 119.63 | 119.63 |
| ECB | 118.63 | 118.63 | 118.63 | 118.63 | 118.63 | 118.63 | 118.63 | 118.63 | 118.63 |
| WCB | 119.17 | 119.17 | 119.17 | 119.17 | 119.17 | 119.17 | 119.17 | 119.17 | 119.17 |
| ECB | 118.17 | 118.17 | 118.17 | 118.17 | 118.17 | 118.17 | 118.17 | 118.17 | 118.17 |
| WCB | 118.69 | 118.69 | 118.69 | 118.69 | 118.69 | 118.69 | 118.69 | 118.69 | 118.69 |
| ECB | 117.69 | 117.69 | 117.69 | 117.69 | 117.69 | 117.69 | 117.69 | 117.69 | 117.69 |
| WCB | 118.46 | 118.46 | 118.46 | 118.46 | 118.46 | 118.46 | 118.46 | 118.46 | 118.46 |
| ECB | 117.46 | 117.46 | 117.46 | 117.46 | 117.46 | 117.46 | 117.46 | 117.46 | 117.46 |
| WCB | 118.32 | 118.32 | 118.32 | 118.32 | 118.32 | 118.32 | 118.32 | 118.32 | 118.32 |
| ECB | 117.32 | 117.32 | 117.32 | 117.32 | 117.32 | 117.32 | 117.32 | 117.32 | 117.32 |
| WCB | 118.18 | 118.18 | 118.18 | 118.18 | 118.18 | 118.18 | 118.18 | 118.18 | 118.18 |
| ECB | 117.18 | 117.18 | 117.18 | 117.18 | 117.18 | 117.18 | 117.18 | 117.18 | 117.18 |
| WCB | 118.04 | 118.04 | 118.04 | 118.04 | 118.04 | 118.04 | 118.04 | 118.04 | 118.04 |
| ECB | 117.04 | 117.04 | 117.04 | 117.04 | 117.04 | 117.04 | 117.04 | 117.04 | 117.04 |
| WCB | 117.89 | 117.89 | 117.89 | 117.89 | 117.89 | 117.89 | 117.89 | 117.89 | 117.89 |
| ECB | 116.88 | 116.88 | 116.88 | 116.88 | 116.88 | 116.88 | 116.88 | 116.88 | 116.88 |
| WCB | 117.73 | 117.73 | 117.73 | 117.73 | 117.73 | 117.73 | 117.73 | 117.73 | 117.73 |
| ECB | 116.73 | 116.73 | 116.73 | 116.73 | 116.73 | 116.73 | 116.73 | 116.73 | 116.73 |
| WCB | 117.57 | 117.57 | 117.57 | 117.57 | 117.57 | 117.57 | 117.57 | 117.57 | 117.57 |
| ECB | 116.57 | 116.57 | 116.57 | 116.57 | 116.57 | 116.57 | 116.57 | 116.57 | 116.57 |
| WCB | 117.41 | 117.41 | 117.41 | 117.41 | 117.41 | 117.41 | 117.41 | 117.41 | 117.41 |
| ECB | 116.42 | 116.42 | 116.42 | 116.42 | 116.42 | 116.42 | 116.42 | 116.42 | 116.42 |
| WCB | 117.25 | 117.25 | 117.25 | 117.25 | 117.25 | 117.25 | 117.25 | 117.25 | 117.25 |
| ECB | 116.27 | 116.27 | 116.27 | 116.27 | 116.27 | 116.27 | 116.27 | 116.27 | 116.27 |
| WCB | 117.10 | 117.10 | 117.10 | 117.10 | 117.10 | 117.10 | 117.10 | 117.10 | 117.10 |
| ECB |        |        |        |        |        |        |        |        |        |

754  
648  
85



# AZALEA DRIVE

N 1/2

S 1/2

| SL. STM.                 |          | N 1/2 | S 1/2    |
|--------------------------|----------|-------|----------|
| EL. HYACINTH = 20100     |          |       | 115.30   |
| 57.57 E Opposite N. side | 114.70   |       | 113.60   |
| 100                      | 113.11   |       | 112.10   |
| 154.09 PC A 40° 36' 00"  | 111.25 ✓ |       | 110.39 ✓ |
| 174.09                   | 110.63   |       | 109.75   |
| 194.09                   | 110.01   |       | 109.12   |
| 214.09                   | 109.38   |       | 108.48   |
| 234.09                   | 108.76   |       | 107.85   |
| 254.09                   | 108.13   |       | 107.22   |
| 274.09                   | 107.51   |       | 106.58   |
| 294.09                   | 106.88   |       | 105.95   |
| 314.09                   | 106.26   |       | 105.31   |
| 334.09                   | 105.63   |       | 104.68   |
| 354.09                   | 105.01   |       | 104.05   |
| 374.09                   | 104.38   |       | 103.41   |
| 394.09                   | 103.76   |       | 102.78   |
| 414.09                   | 103.13   |       | 102.14   |
| 434.09                   | 102.51   |       | 101.51   |
| 454.09                   | 101.88   |       | 100.88   |
| 474.09                   | 101.26   |       | 100.24   |
| 494.09                   | 100.63   |       | 99.61    |
| 514.09                   | 100.01   |       | 98.98    |
| 534.09                   | 99.38    |       | 98.34    |
| 554.09 = E.C.            | 98.76    |       | 97.71    |
| 600                      | 97.17    |       | 96.26    |

1025' - WIL MALLEY  
2406' - WIL MALLEY  
5033' - SEALING  
4494' - 04

WIL CH = 1257  
E.C. = 20100

| SL. STM. |  | N 1/2 | S 1/2 |
|----------|--|-------|-------|
| 12913    |  |       |       |
| 1732     |  |       |       |
| 1744     |  |       |       |
| 1750     |  |       |       |
| 1757     |  |       |       |
| 1758     |  |       |       |
| 1759     |  |       |       |
| 1760     |  |       |       |
| 1761     |  |       |       |
| 1762     |  |       |       |
| 1763     |  |       |       |
| 1764     |  |       |       |
| 1765     |  |       |       |
| 1766     |  |       |       |
| 1767     |  |       |       |
| 1768     |  |       |       |
| 1769     |  |       |       |
| 1770     |  |       |       |
| 1771     |  |       |       |
| 1772     |  |       |       |
| 1773     |  |       |       |
| 1774     |  |       |       |
| 1775     |  |       |       |
| 1776     |  |       |       |
| 1777     |  |       |       |
| 1778     |  |       |       |
| 1779     |  |       |       |
| 1780     |  |       |       |
| 1781     |  |       |       |
| 1782     |  |       |       |
| 1783     |  |       |       |
| 1784     |  |       |       |
| 1785     |  |       |       |
| 1786     |  |       |       |
| 1787     |  |       |       |
| 1788     |  |       |       |
| 1789     |  |       |       |
| 1790     |  |       |       |
| 1791     |  |       |       |
| 1792     |  |       |       |
| 1793     |  |       |       |
| 1794     |  |       |       |
| 1795     |  |       |       |
| 1796     |  |       |       |
| 1797     |  |       |       |
| 1798     |  |       |       |
| 1799     |  |       |       |
| 1800     |  |       |       |

FIZALEA DRIVE

W 06

S 06

624.09 SL Wisteria 96.34 95.50

650.50 NL WISTERIA ON ANGLE 95.50

Opp. E 94.50

Culvert # 1

Flowline @ inlet #1 = 133.0

" " " #2 = 132.0

@ 06 line = Bottom of Basin = 0+00 131.5

+50 E 127.95

100 E 124.40

142.6 121.30

1061.

Handwritten calculations on a grid background:

$$\begin{array}{r} 96.59 \\ 9.6 \\ \hline 106.19 \\ \hline 10.0 \\ \hline 96.19 \\ \hline 10.0 \\ \hline 86.19 \end{array}$$

$$\begin{array}{r} 95.75 \\ 10.0 \\ \hline 105.75 \\ \hline 10.0 \\ \hline 95.75 \end{array}$$

$$\begin{array}{r} 94.75 \\ 10.0 \\ \hline 104.75 \\ \hline 10.0 \\ \hline 94.75 \end{array}$$

$$\begin{array}{r} 95.50 \\ 10.0 \\ \hline 105.50 \\ \hline 10.0 \\ \hline 95.50 \end{array}$$

$$\begin{array}{r} 101.3 \\ 94.7 \\ \hline 6.6 \\ \hline 101.3 \\ \hline 101.3 \\ \hline 6.6 \\ \hline 94.7 \end{array}$$

$$\begin{array}{r} 100.48 \\ 4.2 \\ \hline 104.68 \\ \hline 104.68 \\ \hline 4.2 \\ \hline 100.48 \end{array}$$

$$\begin{array}{r} 95.60 \\ 7.69 \\ \hline 103.29 \\ \hline 7.69 \\ \hline 95.60 \end{array}$$

$$\begin{array}{r} 95.35 \\ 7.94 \\ \hline 103.29 \\ \hline 7.94 \\ \hline 95.35 \end{array}$$

$$\begin{array}{r} 94.50 \\ 10.0 \\ \hline 104.50 \\ \hline 10.0 \\ \hline 94.50 \end{array}$$

$$\begin{array}{r} 127.95 \\ 12.75 \\ \hline 140.70 \\ \hline 12.75 \\ \hline 127.95 \end{array}$$

$$\begin{array}{r} 127.95 \\ 12.75 \\ \hline 140.70 \\ \hline 12.75 \\ \hline 127.95 \end{array}$$

$$\begin{array}{r} 127.95 \\ 12.75 \\ \hline 140.70 \\ \hline 12.75 \\ \hline 127.95 \end{array}$$

$$\begin{array}{r} 127.95 \\ 12.75 \\ \hline 140.70 \\ \hline 12.75 \\ \hline 127.95 \end{array}$$

$$\begin{array}{r} 127.95 \\ 12.75 \\ \hline 140.70 \\ \hline 12.75 \\ \hline 127.95 \end{array}$$

WISTERIA DRIVE

GL. STA.

N 06

S 06

EL AZALIA = 0000

24.20 E opp. N side

+50

100

150

200

223.43 = opp. N. L. BREAK

188.50

94.50

94.50

93.54

92.58

91.62

90.66

90.20

95.50

95.01

94.52

93.53

92.57

91.57

91.05

89.75

100.11

7.12

97.99

0.87

97.81

on RT 25' W of W.L.  
at WISTERIA + HEAD OFF

2032

94.20

91.6

3.61

2.8

20.8

|        |       |       |       |       |       |       |
|--------|-------|-------|-------|-------|-------|-------|
|        | 94.75 | 93.79 | 92.82 | 91.87 | 90.91 | 90.45 |
|        | 5.1   |       | 7.0   | 8.0   | 8.9   | 9.4   |
|        | 4.3   |       | 6.3   | 5.5   | 4.7   | 4.2   |
|        | +0.8  |       | +0.7  | -0.8  | -3.3  | -3.2  |
| SL     | 95.26 | 94.78 | 93.77 | 92.77 | 91.80 | 90.00 |
|        | 4.6   | 0.1   | 7.1   | 8.1   | 8.5   | 9.8   |
|        | 4.8   | 5.0   | 6.7   | 5.0   | 8.4   | 9.6   |
|        | +0.5  | +0.7  | +0.4  | +0.1  | +0.7  | +0.2  |
| 100.59 | 84.75 | 90.00 | 94.50 |       |       |       |
|        | 10.84 | 1.29  | 4.09  |       |       |       |

# PLUMOSA DRIVE

| SL. STA.       | S 06<br>outside | N 06<br>inside |
|----------------|-----------------|----------------|
| NL WING 0000   | 125.00          | 122.00         |
| 1641 N 1040 05 | 124.98          | 122.20         |
| 328 N 3020 10  | 124.80          | 122.46         |
| 49.23 5000 15  | 124.70          | 122.74         |
| 65.64 8020 25  | 124.60          | 122.97         |
| 82.10 = BREAK  | 124.50          | 123.23         |
| 9022 29        | 124.61          | 123.39         |
| 10024 33       | 124.73          | 123.55         |
| 11026 37       | 124.84          | 123.71         |
| 12028 41       | 124.96          | 123.87         |
| 13030 35       | 125.07          | 124.03         |
| 14034 49       | 125.19          | 124.19         |
| 15034 53       | 125.30          | 124.35         |
| 16036 57       | 125.41          | 124.51         |
| 17039 01       | 125.53          | 124.67         |
| 18041 05       | 125.53          | 124.67         |
| 10=1839 PCC    | 125.64          | 124.82         |
| 10038 14       | 125.85          | 125.05         |
| 11016 24       | 126.06          | 125.35         |
| 12054 36       | 126.27          | 125.61         |
| 13032 48       | 126.48          | 125.88         |
| 14049 14       | 126.70          | 126.15         |
| 15047 24       | 126.91          | 126.42         |
| 16050 36       | 127.12          | 126.69         |
| 17043 48       | 127.33          | 126.95         |
| 18022 00       | 127.54          | 127.21         |

12850  
0.59  
128.51  
3.45  
131.96

177

|   | 125.00                       | 25.1                        | 25.0                        | 24.9                        | 24.8                        | 24.7                        | 125.0                       | 25.0                        |
|---|------------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| S | 3.6<br>3.5<br>-0.2           | 3.7<br>4.3<br>-0.6          | 3.8<br>4.7<br>-0.9          | 3.9<br>5.1<br>-1.2          | 4.0<br>5.7<br>-1.7          | 4.1<br>5.1<br>-1.0          | 3.5<br>5.1<br>-1.6          | 3.6<br>4.7<br>-1.1          |
| N | 122.00<br>4.0<br>3.7<br>-0.1 | 22.2<br>6.4<br>10.3<br>-2.9 | 22.4<br>7.2<br>9.9<br>-0.7  | 22.7<br>8.4<br>11.7<br>-3.3 | 23.0<br>8.4<br>11.7<br>-3.3 | 23.2<br>8.4<br>11.7<br>-3.3 | 23.5<br>8.4<br>11.7<br>-3.3 | 23.8<br>7.8<br>13.6<br>-5.8 |
| S | 25.0<br>3.0<br>5.6<br>-2.2   | 25.6<br>3.7<br>5.7<br>-2.1  | 25.9<br>2.9<br>5.1<br>-2.2  | 26.3<br>2.5<br>2.0<br>-0.5  | 26.6<br>2.7<br>0.6<br>-1.6  | 27.1<br>4.5<br>1.5<br>-3.0  | 27.5<br>4.1<br>1.7<br>-2.4  |                             |
| N | 24.5<br>7.1<br>12.5<br>-5.4  | 24.8<br>6.8<br>12.6<br>-5.8 | 25.3<br>6.3<br>10.2<br>-3.9 | 25.8<br>5.8<br>7.2<br>-1.4  | 26.4<br>5.1<br>5.5<br>-0.4  | 26.9<br>4.7<br>7.6<br>-2.9  |                             |                             |
| S | 124.95<br>4.85<br>7.50       | 124.90<br>4.93<br>7.57      | 124.80<br>5.0<br>7.63       | 124.70<br>5.13<br>7.69      | 124.60<br>5.23<br>7.75      | 124.50<br>5.33<br>7.81      | 124.40<br>5.43<br>7.87      | 124.30<br>5.53<br>7.93      |
| N | 122.03<br>7.50               | 122.26<br>7.57              | 122.50<br>7.63              | 122.74<br>7.69              | 122.98<br>7.75              | 123.23<br>7.81              | 123.49<br>7.87              |                             |
| S | 24.73<br>5.10                | 24.84<br>5.17               | 24.96<br>5.23               | 25.07<br>5.29               | 25.20<br>5.35               | 25.34<br>5.41               | 25.53<br>5.47               | 25.64<br>5.53               |
| N | 23.55<br>6.11                | 23.71<br>6.17               | 23.87<br>6.23               | 24.03<br>6.29               | 24.19<br>6.35               | 24.35<br>6.41               | 24.67<br>6.47               | 24.82<br>6.53               |
| S | 125.85<br>3.95               | 126.06<br>3.77              | 126.27<br>3.56              | 126.48<br>3.35              | 126.70<br>3.13              | 126.91<br>2.91              | 127.12<br>2.71              | 127.33<br>2.50              |
| N | 25.05<br>3.75                | 25.25<br>4.43               | 25.41<br>4.22               | 25.58<br>3.95               | 25.75<br>3.68               | 25.92<br>3.41               | 26.09<br>3.14               | 26.25<br>2.87               |

# PLUMOSIA DRIVE

| SL STA.                  | S ct<br>outside    | N ct<br>inside |
|--------------------------|--------------------|----------------|
| 10 373.47 = EC.          | 127.75 ✓           | 127.50 ✓       |
| 398.47 = PC.             | 127.98 ✓           | 127.84         |
| def = 5° 50' 18"         | 128.21 ✓           | 128.0          |
| C = 20.34                | 128.44 ✓           | 128.17         |
| R = 100'                 | 128.68 ✓           | 128.35         |
|                          | 128.91 ✓           | 128.57         |
|                          | 129.14 ✓           | 128.70         |
|                          | 129.38 ✓           | 128.87         |
|                          | 129.61 ✓           | 129.05         |
|                          | 129.84 ✓           | 129.22         |
|                          | 130.07 ✓           | 129.39         |
|                          | 130.31 ✓           | 129.53         |
|                          | 130.55             | 129.70         |
| 644.81 = BREAK           | 130.78 = PC + V.C. | 129.86         |
| 664.12 ✓                 | 130.97             | 130.05         |
| 695.45 ✓                 | 131.03             | 130.13         |
| 712.43 = EC.             | 130.98             | 130.29         |
| 719.5 = BREAK            | 130.94             | 130.06         |
| 737.43 = PC.             | 130.77             | 129.89         |
| 739.56 = BREAK           | 130.74             | 129.86         |
| ✓                        | 130.37 ✓           | 129.54         |
| ✓                        | 129.89 ✓           | 129.08         |
| ✓                        | 129.28 ✓           | 128.50         |
| 5200 81.00 = END of V.C. | 128.54             | 127.78         |
| ✓                        | 127.71             | 127.00         |

131.66  
0.50  
131.16 TP  
5.75  
130.87

18

| SL STA.                  | S ct<br>outside    | N ct<br>inside |
|--------------------------|--------------------|----------------|
| 10 373.47 = EC.          | 127.75 ✓           | 127.50 ✓       |
| 398.47 = PC.             | 127.98 ✓           | 127.84         |
| def = 5° 50' 18"         | 128.21 ✓           | 128.0          |
| C = 20.34                | 128.44 ✓           | 128.17         |
| R = 100'                 | 128.68 ✓           | 128.35         |
|                          | 128.91 ✓           | 128.57         |
|                          | 129.14 ✓           | 128.70         |
|                          | 129.38 ✓           | 128.87         |
|                          | 129.61 ✓           | 129.05         |
|                          | 129.84 ✓           | 129.22         |
|                          | 130.07 ✓           | 129.39         |
|                          | 130.31 ✓           | 129.53         |
|                          | 130.55             | 129.70         |
| 644.81 = BREAK           | 130.78 = PC + V.C. | 129.86         |
| 664.12 ✓                 | 130.97             | 130.05         |
| 695.45 ✓                 | 131.03             | 130.13         |
| 712.43 = EC.             | 130.98             | 130.29         |
| 719.5 = BREAK            | 130.94             | 130.06         |
| 737.43 = PC.             | 130.77             | 129.89         |
| 739.56 = BREAK           | 130.74             | 129.86         |
| ✓                        | 130.37 ✓           | 129.54         |
| ✓                        | 129.89 ✓           | 129.08         |
| ✓                        | 129.28 ✓           | 128.50         |
| 5200 81.00 = END of V.C. | 128.54             | 127.78         |
| ✓                        | 127.71             | 127.00         |

# PLUMOSA DRIVE

S.C.B.  
outside

N.4  
inside

|    |            |          |          |
|----|------------|----------|----------|
| 7  | 2° 42' 20" | 126.88   | 126.20 ✓ |
| 8  | 3° 09' 00" | 126.06 ✓ | 125.40 ✓ |
| 9  | 3° 25' 36" | 125.24 ✓ | 124.61 ✓ |
| 10 | 4° 02' 12" | 124.41 ✓ | 123.82 ✓ |
| 11 | 4° 28' 48" | 123.59 ✓ | 123.02 ✓ |
| 12 | 4° 55' 24" | 122.76 ✓ | 122.23 ✓ |
| 13 | 5° 22' 00" | 121.94 ✓ | 121.42 ✓ |
| 14 | 5° 48' 36" | 121.11 ✓ | 120.64 ✓ |
| 15 | 6° 15' 12" | 120.29 ✓ | 119.85 ✓ |
| 16 | 6° 46' 07" | 119.47 ✓ | 119.05 ✓ |
| 17 |            |          | 118.10 ✓ |
| 18 |            |          | 117.15 ✓ |
| 19 |            |          | 116.20 ✓ |

check min  
90.84

1109.43 = E.C. on SL

1109.23 = E.C. on inside

10857 T  
1234  
123.73  
123.85

|         |                              |                               |                               |                               |                               |                               |                               |                               |
|---------|------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| 10871 S | 27.1<br>9.8<br>9.0<br>+0.8   | 26.20<br>10.6<br>9.8<br>+0.8  | 25.5<br>11.4<br>10.7<br>+0.7  | 24.66<br>12.2<br>12.1<br>+0.1 | 23.82<br>13.0<br>12.9<br>+0.1 |                               |                               |                               |
| N       | 26.0<br>10.7<br>11.3<br>-0.6 | 25.40<br>11.5<br>11.3<br>+0.2 | 24.61<br>12.2<br>12.5<br>+0.1 | 23.82<br>12.1<br>12.0<br>+0.1 | 23.02<br>12.9<br>12.8<br>+0.1 | 22.23<br>13.7<br>13.5<br>+0.2 | 21.44<br>14.5<br>14.8<br>-0.3 | 20.64<br>15.3<br>15.5<br>-0.2 |
| S       | 22.2<br>2.9<br>3.0<br>-0.1   | 20.2<br>3.7<br>3.9<br>-0.2    | 21.4<br>4.5<br>5.2<br>-0.7    | 20.0<br>5.3<br>5.8<br>-0.1    | 19.7<br>6.2<br>7.0<br>-0.8    | 17.95<br>8.0<br>7.0           |                               |                               |
| N       | 18.85<br>6.1<br>6.1<br>0.0   | 19.05<br>6.9<br>6.8<br>0.0    | 18.10<br>7.8<br>7.5<br>+0.3   | 17.15<br>8.76<br>8.8<br>-0.04 | 16.25<br>9.46<br>9.4<br>-0.06 |                               |                               |                               |

13134  
1233  
119.85  
119.7  
121.15

outside

|        |                |                |                |                 |                 |                 |                 |                 |
|--------|----------------|----------------|----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| S      | 126.58<br>7.80 | 126.06<br>7.27 | 125.24<br>6.14 | 124.41<br>6.7   | 123.59<br>7.19  | 122.76<br>8.64  | 121.94<br>9.54  | 121.11<br>10.37 |
| inside | 126.20<br>8.18 | 125.40<br>8.98 | 124.61<br>9.77 | 123.82<br>10.56 | 123.02<br>11.34 | 122.23<br>12.13 | 121.44<br>12.94 | 120.64<br>13.73 |

S

|               |                 |
|---------------|-----------------|
| 2029<br>11.01 | 119.47<br>11.21 |
|---------------|-----------------|

- BREAK = PC of 10' R Curve on PL

|   |                 |                 |                 |                 |                 |                 |                 |                 |                 |
|---|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| N | 119.85<br>11.53 | 119.05<br>12.33 | 118.24<br>13.14 | 117.41<br>13.91 | 116.58<br>14.73 | 115.75<br>15.55 | 114.92<br>16.37 | 114.09<br>17.01 | 113.26<br>17.65 |
|---|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|

|        |                 |                 |                 |                 |                 |                 |                 |                 |                 |
|--------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| 10' PC | 119.47<br>11.75 | 119.05<br>12.57 | 118.24<br>13.38 | 117.41<br>14.19 | 116.58<br>15.01 | 115.75<br>15.83 | 114.92<br>16.65 | 114.09<br>17.47 | 113.26<br>18.30 |
|--------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|

12136

|                |
|----------------|
| 119.47<br>1.89 |
|----------------|

ELLIOTT GRADES

Nct

|                       |          |
|-----------------------|----------|
| PC on SL=0400 = BREAK | 139.60 ✓ |
| 134.5 W               | 142.58 ✓ |
| 1044.5 = BREAK        | 143.72 ✓ |
| 154.5                 | 144.40 ✓ |
| 84.5                  | 146.20 ✓ |
| 1094.5 = BREAK        | 146.70 ✓ |
| 104.5                 | 147.04 ✓ |
| 154.5 = BREAK         | 148.9 ✓  |
| 204.5                 | 148.55 ✓ |
| 154.5                 | 149.10 ✓ |
| 304.5 W               | 149.65 ✓ |
| 354.5 W = BREAK       | 150.20 ✓ |
| 414.5 = BREAK         | 151.50 ✓ |
| 474.5                 | 152.05 ✓ |
| 511.5 = EL Narcissus  | 154.00 ✓ |
| 534.5 = BREAK (OUT)   | 154.60 ✓ |
| 574.5 = WL Narcissus  | 156.40 ✓ |
| 594.5                 | 157.44 ✓ |
| 654.5 = BREAK         | 160.20   |
| 704.5 = BREAK         | 161.40 ✓ |
| 724.5                 | 161.65 ✓ |
| 754.5 = BREAK         | 161.40 ✓ |
| 794.50 BREAK          | 160.70 ✓ |
| 834.50 BREAK          | 159.50 ✓ |
| 867.50 = EL Jonquil   | 158.37   |
| 927.50 = WL ✓         | 156.30   |

158.37 = WL Return  
157.43

12013  
13200  
14092  
133  
139.60  
142.58  
143.72  
144.40  
146.20  
146.70  
147.04  
148.9  
148.55  
149.10  
149.65  
150.20  
151.50  
152.05  
154.00  
154.60  
156.40  
157.44  
160.20  
161.40  
161.65  
161.40  
160.70  
159.50  
158.37  
156.30

|        |        |        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 145.0  | 139.60 | 144.40 | 143.72 | 146.20 | 146.70 | 147.04 | 148.9  | 148.55 | 149.10 | 149.65 | 150.20 | 151.50 | 152.05 |
| 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   |
| 147.04 | 148.9  | 148.55 | 149.10 | 149.65 | 150.20 | 151.50 | 152.05 | 154.00 | 154.60 | 156.40 | 157.44 | 160.20 | 161.40 |
| 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   |
| 147.04 | 148.9  | 148.55 | 149.10 | 149.65 | 150.20 | 151.50 | 152.05 | 154.00 | 154.60 | 156.40 | 157.44 | 160.20 | 161.40 |
| 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   |
| 147.04 | 148.9  | 148.55 | 149.10 | 149.65 | 150.20 | 151.50 | 152.05 | 154.00 | 154.60 | 156.40 | 157.44 | 160.20 | 161.40 |
| 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   |

142.8  
144.40  
148.9  
157.44  
160.20  
161.40  
161.65  
161.40  
160.70  
159.50  
158.37  
156.30

ELLIOTT

GRADES

|                 |        |        |
|-----------------|--------|--------|
| 984.5           | 154.34 |        |
| 1034.5          | 152.64 |        |
| 1066.67 BREAK   | 151.50 |        |
| 1103            | 150.65 |        |
| 1140 = PC BREAK | 149.80 | 149.78 |

EC ON SLELLIOTT

|    |        |        |
|----|--------|--------|
| VC | ① = EC | 147.70 |
|    | ②      | 147.84 |
|    | ③      | 148.01 |
|    | ④      | 147.70 |
|    | PC ⑤   | 147.43 |

= PC ON SL

|        |                 |           |
|--------|-----------------|-----------|
|        |                 | 147.16    |
|        | INL ELLIOTT     | 147.88 VC |
| 0+00   | = WL Powissetia | 147.38    |
| +613   |                 | 141.69    |
| 1+2267 | = WL Tract      | 136.0     |

16000  
8.12  
154.30  
136  
157.66  
10.75  
157.35  
1.42  
156.32  
9.45  
151.67  
1.08  
152.37

157.65  
1.08  
158.73

|   |        |        |        |        |             |        |
|---|--------|--------|--------|--------|-------------|--------|
|   | 154.24 | 152.62 | 151.50 | 150.65 | 149.80      | 149.53 |
|   | 3.32   | 5.04   | 6.18   | 7.01   | 7.86        | 8.13   |
|   | 149.39 | 149.37 | 149.39 | 149.52 | 149.78 = EC |        |
|   | 8.27   | 8.29   | 8.27   | 8.14   | 7.88        |        |
|   | 147.88 | 147.38 |        |        |             |        |
|   | 9.78   | 10.28  |        |        |             |        |
| S | 142.70 | 147.84 | 145.01 | 147.70 | 147.43      | 147.16 |
|   | 5.62   | 4.50   | 2.01   | 2.62   | 2.89        | 3.16   |
| S | 145.84 | 140.94 | 135.0  |        |             |        |
|   | 2.26   | 9.38   | 7.37   |        |             |        |
| N | 141.69 | 136.0  |        |        |             |        |
|   | 8.63   | 6.37   |        |        |             |        |

9.38  
1.22  
1.75



SUNSET GROVE Sowers R/4/22

Moore

|                               |        |
|-------------------------------|--------|
| ALLEY BIK v = 0100 = DE.      | 126.85 |
| 50 N                          | 119.65 |
| 100 N                         | 112.44 |
| 110 N BREAK                   | 111.0  |
| 140 N = # Muir's MH & LT      | 110.0  |
| 200                           | 109.65 |
| 250                           | 109.35 |
| 300                           | 109.06 |
| 350                           | 108.76 |
| 400                           | 108.47 |
| 450                           | 108.17 |
| 480 BREAK                     | 108.0  |
| 518.8                         | 103.50 |
| 557.6 = Flysh Tank            | 99.0   |
| FLUSH TANK ALLEY BIK v = 0100 | 111.82 |
| 50 E                          | 116.71 |
| 100                           | 121.60 |
| 150                           | 126.56 |
| 175.6 E BREAK                 | 129.0  |
| 227.8                         | 131.25 |
| 280 E = DE                    | 133.50 |
| ALLEY BIK 1                   |        |
| 5' east w/ lots = 0100 = DE.  | 146.65 |
| 42.5' E of House              | 145.7  |
| 67.9 w v ✓                    | 144.61 |
| 115' w' = End of pipe.        | 143.20 |

557.6  
280.0  
277.6

3.35  
6.28

71.00 N.W. Man Voltaire + Mendocino

|        |        |        |       |
|--------|--------|--------|-------|
| 126.85 | 119.65 | 112.44 | 111.0 |
| 3.21   | 10.91  | 18.12  | 7.92  |
| 130.26 | 10.91  | 18.12  | 7.92  |
| 3.0    | 5.24   | 11.53  | 2.81  |
| 130.56 | 14.97  | 16.59  | 2.81  |

|        |        |        |       |
|--------|--------|--------|-------|
| 126.85 | 119.65 | 112.44 | 111.0 |
| 4.16   | 9.81   | 15.08  | 11.00 |
| 3.21   | 10.91  | 18.12  | 7.92  |
| 3.21   | 10.91  | 18.12  | 7.92  |
| 112.44 | 10.91  | 18.12  | 7.92  |
| 111.0  | 10.91  | 18.12  | 7.92  |
| 110.0  | 10.91  | 18.12  | 7.92  |
| 109.65 | 10.91  | 18.12  | 7.92  |
| 109.35 | 10.91  | 18.12  | 7.92  |
| 109.06 | 10.91  | 18.12  | 7.92  |
| 108.76 | 10.91  | 18.12  | 7.92  |
| 108.47 | 10.91  | 18.12  | 7.92  |
| 108.17 | 10.91  | 18.12  | 7.92  |
| 108.0  | 10.91  | 18.12  | 7.92  |
| 103.50 | 10.91  | 18.12  | 7.92  |
| 99.0   | 10.91  | 18.12  | 7.92  |
| 111.82 | 10.91  | 18.12  | 7.92  |
| 116.71 | 10.91  | 18.12  | 7.92  |
| 121.60 | 10.91  | 18.12  | 7.92  |
| 126.56 | 10.91  | 18.12  | 7.92  |
| 129.0  | 10.91  | 18.12  | 7.92  |
| 131.25 | 10.91  | 18.12  | 7.92  |
| 133.50 | 10.91  | 18.12  | 7.92  |
| 146.65 | 10.91  | 18.12  | 7.92  |
| 145.7  | 10.91  | 18.12  | 7.92  |
| 144.61 | 10.91  | 18.12  | 7.92  |
| 143.20 | 10.91  | 18.12  | 7.92  |

5.78  
103.87 = Nick BM  
103.94 = Rest of MH

174.5  
Moore

ALLEY PAVING  
BIK & PARK ADD.

|                             | SL      | NL     |
|-----------------------------|---------|--------|
| 160 w of WL of 20th to 0+00 | 291.0 ✓ | 291.27 |
| 20 w BREAK                  | 291.17  | 291.42 |
| 40 w BREAK                  | 291.15  | 291.40 |
| 80                          | 290.96  | 291.21 |
| 120                         | 290.76  | 291.01 |
| 160                         | 290.57  | 290.82 |
| 200                         | 290.38  | 290.63 |
| 240                         | 290.19  | 290.44 |
| 280 w BREAK                 | 290.0   | 290.25 |
| 310                         | 289.0   | 289.25 |
| 340 w BREAK                 | 288.0   | 288.25 |
| 380                         | 285.62  | 285.87 |
| 420 w BREAK                 | 283.25  | 283.50 |
|                             | 278.78  | 279.18 |
| 490.5 = SL<br>= NL          | 274.31  | 274.86 |

289.71 SEBP Kalmia + 30th

23

|  | SL | 91.8 ✓ | 91.17 | 91.15 | 90.96 | 90.74 | 90.57 | 90.38 | 90.19   |
|--|----|--------|-------|-------|-------|-------|-------|-------|---------|
|  |    | 5.53   | 5.40  | 5.30  | 5.68  | 5.81  | 6.00  | 6.28  | 6.42    |
|  |    | 0.52   | 0.43  | 0.33  | 0.56  | 0.81  | 1.04  | 1.26  | 1.42    |
|  |    | +1.0   | +0.47 | +0.08 | +0.05 | +1.0  | +1.48 | +1.27 | +1.0    |
|  | NL | 91.17  | 91.12 | 91.40 | 91.21 | 91.01 | 90.82 | 90.63 | 90.44   |
|  |    | 5.30   | 5.15  | 5.17  | 5.86  | 5.56  | 5.75  | 5.78  | 5.77    |
|  |    | 0.52   | 0.55  | 0.72  | 0.36  | 0.40  | 0.96  | 0.88  | 0.59    |
|  |    | +0.46  | +0.60 | +1.0  | +1.0  | +1.16 | -0.21 | +1.30 | +0.78   |
|  | SL | 288.0  | 89.0  | 88.0  | 85.62 | 82.25 | 78.78 | 74.31 |         |
|  |    | 0.61   | 5.01  | 0.61  | 8.99  | 11.36 | 3.96  | 8.43  |         |
|  |    | 1.22   | 1.17  | 5.26  | 6.42  | 10.00 | 0.82  | 7.70  | checked |
|  |    | +1.22  | +1.22 | +0.85 | +0.57 | +1.36 | +3.11 | +0.78 | STAKE   |
|  | NL | 90.25  | 89.25 | 88.25 | 85.87 | 83.50 | 79.18 | 74.86 |         |
|  |    | 5.36   | 5.36  | 6.36  | 8.74  | 11.11 | 3.56  | 7.88  |         |
|  |    | 1.22   | 5.29  | 6.15  | 8.38  | 11.14 | 2.95  | 6.75  |         |
|  |    | +0.89  | +0.07 | +0.71 | +0.36 | -0.03 | +0.61 | +1.13 |         |





POINSETTIA SEWER

POINSETTIA  
+ ELLIOTT = MH #1 = 0+00

|                 |        |
|-----------------|--------|
| 50 ~            | 143.00 |
| 100 ~           | 144.12 |
| 150 ~           | 145.24 |
| 200 ~           | 146.36 |
| 250 ~           | 147.48 |
| 300 ~           | 148.60 |
| 350 ~           | 149.72 |
| 385 ~ = MH #3 A | 150.53 |
| 385 ~           | 151.49 |
| 425 ~           | 152.45 |
| 485 ~           | 153.42 |
| 525 ~           | 154.39 |
| 566.53 ~ = D.E. | 155.0  |

|               | Main   | BREAK  | Prop   | from Main |
|---------------|--------|--------|--------|-----------|
| Sewer LAT# 13 | 152.60 | 153.0  | 153.70 | 1         |
| ✓ # 24        | 153.60 | 154.40 | 155.20 | 1         |
| ✓ # 23        | 155.10 | 155.5  | 156.20 | 1         |

156.96  
220  
156.76  
5.17  
161.93

|        |       |       |       |       |       |        |
|--------|-------|-------|-------|-------|-------|--------|
| 104.12 | 152.6 | 163.6 | 174.8 | 186.0 | 197.2 | 150.53 |
| 10.84  | 11.72 | 10.60 | 9.48  | 8.36  | 7.24  | 6.13   |
| 5.67   | 7.60  | 6.70  | 5.71  | 4.78  | 3.75  | 3.05   |
| 24.17  | 24.12 | 23.90 | +3.77 | +3.58 | +3.49 | +3.38  |
| 51.49  | 52.65 | 53.44 | 54.37 | 55.0  |       |        |
| 5.47   | 5.51  | 3.54  | 7.54  | 6.93  |       |        |
| 2.09   | 1.13  | 0.20  | 4.30  | 1.13  |       |        |
| +3.38  | +3.88 | +3.38 | +3.20 | +2.80 |       |        |

156.6 HI

ALLEY SEWER BETWEEN  
ELLIOTT + PLUMOSA DR.

|                                  |         |
|----------------------------------|---------|
| M.H. #21 = 0+00<br>PLUMOSA DRIVE | 117.50  |
| H958 W                           | 120.33  |
| 9916                             | 123.17  |
| H875 = M.H. #26 = A              | 126.0   |
| 200                              | 127.73  |
| 250                              | 129.41  |
| 300                              | 131.09  |
| 350                              | 132.77  |
| 400                              | 134.45  |
| 450                              | 136.13  |
| 500                              | 137.86  |
| 518 W = D.M.H. #15 A             | 138.50  |
| 574 W                            | 142.17  |
| 630.48                           | 144.33  |
| 686.7 W = M.H. #17 & Narraquis   | 146.50  |
| 738.7 W                          | 148.5 W |
| 790.7 W                          | 150.54  |
| 842.7 W                          | 152.56  |
| 894.7 W                          | 154.58  |
| 946.7 W = DE.                    | 156.60  |
| PLUMOSA WAY TO EXISTING SEWER    |         |
| EX. Sewer = 0+00                 | 116.5 W |
| 50 W                             | 116.79  |
| 100 W                            | 117.06  |
| 150                              | 117.33  |
| 180 = M.H. #21.                  | 117.50  |

117.50  
5.01  
7.13  
12.9 ✓

27

|        |        |        |        |        |       |        |        |        |
|--------|--------|--------|--------|--------|-------|--------|--------|--------|
| 1571.4 | 117.50 | 20.33  | 22.17  | 126.0  | 27.73 | 29.41  | 31.09  | 32.77  |
| 165.00 | 11.20  | 2.47   | 16.4 W | 12.59  | 11.86 | 10.18  | 8.50   | 6.8 W  |
| 148.47 | 10.53  | 2.84   | 12.20  | 7.45   | 3.91  | 3.15   | 3.25   | 1.77   |
| 128.47 | 11.79  | 3.62   | 14.2 W | 7.94   | 16.17 | 2.03   | 6.24   | 4.00   |
| 117.47 | 2.25   | 3.65   | 37.56  | 38.50  | DMH   | 140.0  | 12.17  | 14.33  |
| 105.47 | 16.49  | 14.79  | 13.08  | 12.24  | 12.90 | 8.77   | 6.61   | 6.61   |
| 97.37  | 12.05  | 10.43  | 7.74   | 6.50   | 6.50  | 3.25   | 2.31   | 1.37   |
| 97.30  | 14.22  | 2.36   | 25.24  | 5.74   | 2.84  | 15.31  | 4.52 W | 4.52 W |
|        | 46.50  | 48.5 W | 50.54  | 52.56  | 54.58 | 156.60 |        |        |
|        | 16.50  | 14.78  | 12.46  | 10.4 W | 8.4 W | 6.00   |        |        |
|        | 11.47  | 9.8 W  | 7.75   | 5.93   | 3.93  | 1.54   |        |        |
|        | 5.03   | 4.66   | 4.71   | 4.51   | 4.49  | 4.56   |        |        |
| 1297.7 |        |        |        |        |       |        |        |        |
| 1282.0 |        |        |        |        |       |        |        |        |
| 1264.0 |        |        |        |        |       |        |        |        |
| 1246.0 |        |        |        |        |       |        |        |        |
| 1228.0 |        |        |        |        |       |        |        |        |
| 1210.0 |        |        |        |        |       |        |        |        |
| 1192.0 |        |        |        |        |       |        |        |        |
| 1174.0 |        |        |        |        |       |        |        |        |
| 1156.0 |        |        |        |        |       |        |        |        |
| 1138.0 |        |        |        |        |       |        |        |        |
| 1120.0 |        |        |        |        |       |        |        |        |
| 1102.0 |        |        |        |        |       |        |        |        |
| 1084.0 |        |        |        |        |       |        |        |        |
| 1066.0 |        |        |        |        |       |        |        |        |
| 1048.0 |        |        |        |        |       |        |        |        |
| 1030.0 |        |        |        |        |       |        |        |        |
| 1012.0 |        |        |        |        |       |        |        |        |
| 994.0  |        |        |        |        |       |        |        |        |
| 976.0  |        |        |        |        |       |        |        |        |
| 958.0  |        |        |        |        |       |        |        |        |
| 940.0  |        |        |        |        |       |        |        |        |
| 922.0  |        |        |        |        |       |        |        |        |
| 904.0  |        |        |        |        |       |        |        |        |
| 886.0  |        |        |        |        |       |        |        |        |
| 868.0  |        |        |        |        |       |        |        |        |
| 850.0  |        |        |        |        |       |        |        |        |
| 832.0  |        |        |        |        |       |        |        |        |
| 814.0  |        |        |        |        |       |        |        |        |
| 796.0  |        |        |        |        |       |        |        |        |
| 778.0  |        |        |        |        |       |        |        |        |
| 760.0  |        |        |        |        |       |        |        |        |
| 742.0  |        |        |        |        |       |        |        |        |
| 724.0  |        |        |        |        |       |        |        |        |
| 706.0  |        |        |        |        |       |        |        |        |
| 688.0  |        |        |        |        |       |        |        |        |
| 670.0  |        |        |        |        |       |        |        |        |
| 652.0  |        |        |        |        |       |        |        |        |
| 634.0  |        |        |        |        |       |        |        |        |
| 616.0  |        |        |        |        |       |        |        |        |
| 598.0  |        |        |        |        |       |        |        |        |
| 580.0  |        |        |        |        |       |        |        |        |
| 562.0  |        |        |        |        |       |        |        |        |
| 544.0  |        |        |        |        |       |        |        |        |
| 526.0  |        |        |        |        |       |        |        |        |
| 508.0  |        |        |        |        |       |        |        |        |
| 490.0  |        |        |        |        |       |        |        |        |
| 472.0  |        |        |        |        |       |        |        |        |
| 454.0  |        |        |        |        |       |        |        |        |
| 436.0  |        |        |        |        |       |        |        |        |
| 418.0  |        |        |        |        |       |        |        |        |
| 400.0  |        |        |        |        |       |        |        |        |
| 382.0  |        |        |        |        |       |        |        |        |
| 364.0  |        |        |        |        |       |        |        |        |
| 346.0  |        |        |        |        |       |        |        |        |
| 328.0  |        |        |        |        |       |        |        |        |
| 310.0  |        |        |        |        |       |        |        |        |
| 292.0  |        |        |        |        |       |        |        |        |
| 274.0  |        |        |        |        |       |        |        |        |
| 256.0  |        |        |        |        |       |        |        |        |
| 238.0  |        |        |        |        |       |        |        |        |
| 220.0  |        |        |        |        |       |        |        |        |
| 202.0  |        |        |        |        |       |        |        |        |
| 184.0  |        |        |        |        |       |        |        |        |
| 166.0  |        |        |        |        |       |        |        |        |
| 148.0  |        |        |        |        |       |        |        |        |
| 130.0  |        |        |        |        |       |        |        |        |
| 112.0  |        |        |        |        |       |        |        |        |
| 94.0   |        |        |        |        |       |        |        |        |
| 76.0   |        |        |        |        |       |        |        |        |
| 58.0   |        |        |        |        |       |        |        |        |
| 40.0   |        |        |        |        |       |        |        |        |
| 22.0   |        |        |        |        |       |        |        |        |
| 4.0    |        |        |        |        |       |        |        |        |

SEWER LAT.

|       |       |        |        |        |        |        |        |        |
|-------|-------|--------|--------|--------|--------|--------|--------|--------|
| #112  | #114  | #111   | #110   | #109   | #115   | #108   | #114   | #107   |
| 155.0 | 155.0 | 163.80 | 162.0  | 150.0  | 129.70 | 144.50 | 142.00 | 142.00 |
| 4.4   | 6.7   | 8.6 W  | 10.4 W | 12.4 W | 14.7 W | 5.78   | 7.03   | 8.08   |
| 1.7 W | 3.00  | 5.7    | 7.36   | 9.25   | 10.46  | 2.73   | 3.83   | 5.00   |
| 3.70  | 3.00  | 3.05   | 3.06   | 3.07   | 4.25   | 3.05   | 4.14   | 5.06   |

|       |       |       |       |       |        |        |        |        |
|-------|-------|-------|-------|-------|--------|--------|--------|--------|
| #106  | #105  | #104  | #103  | #102  | #101   | #100   | #99    | #98    |
| 129.0 | 136.0 | 135.0 | 134.0 | 133.0 | 130.50 | 128.50 | 125.70 | 120.50 |
| 11.2  | 14.9  | 15.5  | 4.3   | 5.23  | 7.83   | 2.83   | 12.63  | 4.1    |
| 8.5   | 10.5  | 13.1  | 0.75  | 0.75  | 4.5    | 3.25   | 5.35   | 2.91   |
| 2.50  | 3.40  | 3.07  | 2.58  | 2.58  | 3.31   | 2.705  | 3.05   | 4.40   |

+5.25 raised

43 W

|        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 117.50 | 116.50 | 115.50 | 114.50 | 113.50 | 112.50 | 111.50 | 110.50 | 109.50 |
| 116.50 | 115.50 | 114.50 | 113.50 | 112.50 | 111.50 | 110.50 | 109.50 | 108.50 |
| 115.50 | 114.50 | 113.50 | 112.50 | 111.50 | 110.50 | 109.50 | 108.50 | 107.50 |
| 114.50 | 113.50 | 112.50 | 111.50 | 110.50 | 109.50 | 108.50 | 107.50 | 106.50 |
| 113.50 | 112.50 | 111.50 | 110.50 | 109.50 | 108.50 | 107.50 | 106.50 | 105.50 |
| 112.50 | 111.50 | 110.50 | 109.50 | 108.50 | 107.50 | 106.50 | 105.50 | 104.50 |
| 111.50 | 110.50 | 109.50 | 108.50 | 107.50 | 106.50 | 105.50 | 104.50 | 103.50 |
| 110.50 | 109.50 | 108.50 | 107.50 | 106.50 | 105.50 | 104.50 | 103.50 | 102.50 |
| 109.50 | 108.50 | 107.50 | 106.50 | 105.50 | 104.50 | 103.50 | 102.50 | 101.50 |
| 108.50 | 107.50 | 106.50 | 105.50 | 104.50 | 103.50 | 102.50 | 101.50 | 100.50 |
| 107.50 | 106.50 | 105.50 | 104.50 | 103.50 | 102.50 | 101.50 | 100.50 | 99.50  |
| 106.50 | 105.50 | 104.50 | 103.50 | 102.50 | 101.50 | 100.50 | 99.50  | 98.50  |
| 105.50 | 104.50 | 103.50 | 102.50 | 101.50 | 100.50 | 99.50  | 98.50  | 97.50  |
| 104.50 | 103.50 | 102.50 | 101.50 | 100.50 | 99.50  | 98.50  | 97.50  | 96.50  |
| 103.50 | 102.50 | 101.50 | 100.50 | 99.50  | 98.50  | 97.50  | 96.50  | 95.50  |
| 102.50 | 101.50 | 100.50 | 99.50  | 98.50  | 97.50  | 96.50  | 95.50  | 94.50  |
| 101.50 | 100.50 | 99.50  | 98.50  | 97.50  | 96.50  | 95.50  | 94.50  | 93.50  |
| 100.50 | 99.50  | 98.50  | 97.50  | 96.50  | 95.50  | 94.50  | 93.50  | 92.50  |
| 99.50  | 98.50  | 97.50  | 96.50  | 95.50  | 94.50  | 93.50  | 92.50  | 91.50  |
| 98.50  | 97.50  | 96.50  | 95.50  | 94.50  | 93.50  | 92.50  | 91.50  | 90.50  |
| 97.50  | 96.50  | 95.50  | 94.50  | 93.50  | 92.50  | 91.50  | 90.50  | 89.50  |
| 96.50  | 95.50  | 94.50  | 93.50  | 92.50  | 91.50  | 90.50  | 89.50  | 88.50  |
| 95.50  | 94.50  | 93.50  | 92.50  | 91.50  | 90.50  | 89.50  | 88.50  | 87.50  |
| 94.50  | 93.50  | 92.50  | 91.50  | 90.50  | 89.50  | 88.50  | 87.50  | 86.50  |
| 93.50  | 92.50  | 91.50  | 90.50  | 89.50  | 88.50  | 87.50  | 86.50  | 85.50  |
| 92.50  | 91.50  | 90.50  | 89.50  | 88.50  | 87.50  | 86.50  | 85.50  | 84.50  |
| 91.50  | 90.50  | 89.50  | 88.50  | 87.50  | 86.50  | 85.50  | 84.50  | 83.50  |
| 90.50  | 89.50  | 88.50  | 87.50  | 86.50  | 85.50  | 84.50  | 83.50  | 82.50  |
| 89.50  | 88.50  | 87.50  | 86.50  | 85.50  | 84.50  | 83.50  | 82.50  | 81.50  |
| 88.50  | 87.50  | 86.50  | 85.50  | 84.50  | 83.50  | 82.50  | 81.50  | 80.50  |
| 87.50  | 86.50  | 85.50  | 84.50  | 83.50  | 82.50  | 81.50  | 80.50  | 79.50  |
| 86.50  | 85.50  | 84.50  | 83.50  | 82.50  | 81.50  | 80.50  | 79.50  | 78.50  |
| 85.50  | 84.50  | 83.50  | 82.50  | 81.50  | 80.50  | 79.50  | 78.50  | 77.50  |
| 84.50  | 83.50  | 82.50  | 81.50  | 80.50  | 79.50  | 78.50  | 77.50  | 76.50  |
| 83.50  | 82.50  | 81.50  | 80.50  | 79.50  | 78.50  | 77.50  | 76.50  | 75.50  |
| 82.50  | 81.50  | 80.50  | 79.50  | 78.50  | 77.50  | 76.50  | 75.50  | 74.50  |
| 81.50  | 80.50  | 79.50  | 78.50  | 77.50  | 76.50  | 75.50  | 74.50  | 73.50  |
| 80.50  | 79.50  | 78.50  | 77.50  | 76.50  | 75.50  | 74.50  | 73.50  | 72.50  |
| 79.50  | 78.50  | 77.50  | 76.50  | 75.50  | 74.50  | 73.50  | 72.50  | 71.50  |
| 78.50  | 77.50  | 76.50  | 75.50  | 74.50  | 73.50  | 72.50  | 71.50  | 70.50  |
| 77.50  | 76.50  | 75.50  | 74.50  | 73.50  | 72.50  | 71.50  | 70.50  | 69.50  |
| 76.50  | 75.50  | 74.50  | 73.50  | 72.50  | 71.50  | 70.50  | 69.50  | 68.50  |
| 75.50  | 74.50  | 73.50  | 72.50  | 71.50  | 70.50  | 69.50  | 68.50  | 67.50  |
| 74.50  | 73.50  | 72.50  | 71.50  | 70.50  | 69.50  | 68.50  | 67.50  | 66.50  |
| 73.50  | 72.50  | 71.50  | 70.50  | 69.50  | 68.50  | 67.50  | 66.50  | 65.50  |
| 72.50  | 71.50  | 70.50  |        |        |        |        |        |        |



Senior ALLEY LINE betw  
Amargliss + Lotus

|                  |        |
|------------------|--------|
| MH #13 = 0100    | 114.75 |
| +40W #53L H84NL  | 115.8W |
| +50              | 116.08 |
| +97 #5V          | 117.36 |
| 100W             | 117.4V |
| 148W #51         | 118.70 |
| 159 = DMH #1VARI | 119.0  |
| 0100W # Lot #45  | 119.18 |
| +50              | 119.40 |
| 77W #47W #46E    | 119.6V |
| 100W             | 119.81 |
| 149W #48E        | 120.04 |
| 150N             | 120.21 |
| 177 #49          | 120.43 |
| 185 = DE         | 120.50 |
| 187 #50          |        |
| 159W = DMH #1V   | 123.50 |
| 200W #44         | 125.38 |
| 250              | 127.68 |
| 25W #43          | 127.77 |
| 300W = MH #11ALT | 130.00 |
| 343W = MH #10ART | 132.00 |
| 400              | 134.35 |
| 450              | 136.4V |
| 500W = DMH #9ALT | 138.50 |

830  
29

|      |        |        |        |        |        |        |
|------|--------|--------|--------|--------|--------|--------|
| 1021 | #53    | #54    | #55    | #56    | #57    | #58    |
| 1022 | 114.75 | 116.84 | 116.08 | 120.36 | 117.4V | 122.70 |
| 1023 | 15.94  | 12.89  | 7.63   | 10.35  | 13.49  | 8.01   |
| 1024 | 15.02  | 7.89   | 7.33   | 2.13   | 1.22   | 5.70   |
| 1025 | 20.75  | 6.50   | 7.34   | 15.22  | 15.07  | 14.91  |
| 1026 |        | 15.39  |        |        |        |        |
| 1027 | DMH    | #45    | #46    | #47    | #48    | #49    |
| 1028 | 119.0  | 123.18 | 119.40 | 120.0  | 119.81 | 120.40 |
| 1029 | 11.71  | 7.53   | 11.31  | 10.71  | 12.40  | 10.31  |
| 1030 | 2.84   | 2.15   | 2.99   | 4.20   | 3.71   | 5.18   |
| 1031 | +8.84  | +5.38  | +9.2V  | +6.51  | +4.0   | +5.10  |
| 1032 |        | DE     | #50    | #51    | DMH    | #52    |
| 1033 | 120.21 | 120.50 | 122.0  | 120.63 | 125.38 | 125.38 |
| 1034 | 10.50  | 10.21  | 8.71   | 7.02   | 5.33   | 12.60  |
| 1035 | 4.22   | 5.72   | 5.71   | 6.87   | 7.21   | 5.69   |
| 1036 | 46.03  | +4.24  | +2.75  | +3.21  | +2.35  | +4.64  |
| 1037 |        | #43    | #44    | #45    | #46    | #47    |
| 1038 | 127.68 | 129.77 | 120.00 | 120.0  | 127.70 | 124.35 |
| 1039 | 14.54  | 12.25  | 14.02  | 70.00  | 7.37   | 9.04   |
| 1040 | +4.54  | 9.50   | 4.56   | 5.07   | 4.36   | 4.89   |
| 1041 |        | +2.70  | +7.46  | +4.95  | +3.96  | +7.13  |
| 1042 |        | DMH    |        |        |        |        |
| 1043 | 136.4V | 138.50 |        |        |        |        |
| 1044 | 14.04  | 13.96  |        |        |        |        |
| 1045 | 8.49   | 6.90   |        |        |        |        |
| 1046 | +7.55  | +7.04  |        |        |        |        |
| 1047 |        |        |        |        |        |        |
| 1048 |        |        |        |        |        |        |
| 1049 |        |        |        |        |        |        |
| 1050 |        |        |        |        |        |        |
| 1051 |        |        |        |        |        |        |
| 1052 |        |        |        |        |        |        |
| 1053 |        |        |        |        |        |        |
| 1054 |        |        |        |        |        |        |
| 1055 |        |        |        |        |        |        |
| 1056 |        |        |        |        |        |        |
| 1057 |        |        |        |        |        |        |
| 1058 |        |        |        |        |        |        |
| 1059 |        |        |        |        |        |        |
| 1060 |        |        |        |        |        |        |
| 1061 |        |        |        |        |        |        |
| 1062 |        |        |        |        |        |        |
| 1063 |        |        |        |        |        |        |
| 1064 |        |        |        |        |        |        |
| 1065 |        |        |        |        |        |        |
| 1066 |        |        |        |        |        |        |
| 1067 |        |        |        |        |        |        |
| 1068 |        |        |        |        |        |        |
| 1069 |        |        |        |        |        |        |
| 1070 |        |        |        |        |        |        |
| 1071 |        |        |        |        |        |        |
| 1072 |        |        |        |        |        |        |
| 1073 |        |        |        |        |        |        |
| 1074 |        |        |        |        |        |        |
| 1075 |        |        |        |        |        |        |
| 1076 |        |        |        |        |        |        |
| 1077 |        |        |        |        |        |        |
| 1078 |        |        |        |        |        |        |
| 1079 |        |        |        |        |        |        |
| 1080 |        |        |        |        |        |        |
| 1081 |        |        |        |        |        |        |
| 1082 |        |        |        |        |        |        |
| 1083 |        |        |        |        |        |        |
| 1084 |        |        |        |        |        |        |
| 1085 |        |        |        |        |        |        |
| 1086 |        |        |        |        |        |        |
| 1087 |        |        |        |        |        |        |
| 1088 |        |        |        |        |        |        |
| 1089 |        |        |        |        |        |        |
| 1090 |        |        |        |        |        |        |
| 1091 |        |        |        |        |        |        |
| 1092 |        |        |        |        |        |        |
| 1093 |        |        |        |        |        |        |
| 1094 |        |        |        |        |        |        |
| 1095 |        |        |        |        |        |        |
| 1096 |        |        |        |        |        |        |
| 1097 |        |        |        |        |        |        |
| 1098 |        |        |        |        |        |        |
| 1099 |        |        |        |        |        |        |
| 1100 |        |        |        |        |        |        |
| 1101 |        |        |        |        |        |        |
| 1102 |        |        |        |        |        |        |
| 1103 |        |        |        |        |        |        |
| 1104 |        |        |        |        |        |        |
| 1105 |        |        |        |        |        |        |
| 1106 |        |        |        |        |        |        |
| 1107 |        |        |        |        |        |        |
| 1108 |        |        |        |        |        |        |
| 1109 |        |        |        |        |        |        |
| 1110 |        |        |        |        |        |        |
| 1111 |        |        |        |        |        |        |
| 1112 |        |        |        |        |        |        |
| 1113 |        |        |        |        |        |        |
| 1114 |        |        |        |        |        |        |
| 1115 |        |        |        |        |        |        |
| 1116 |        |        |        |        |        |        |
| 1117 |        |        |        |        |        |        |
| 1118 |        |        |        |        |        |        |
| 1119 |        |        |        |        |        |        |
| 1120 |        |        |        |        |        |        |
| 1121 |        |        |        |        |        |        |
| 1122 |        |        |        |        |        |        |
| 1123 |        |        |        |        |        |        |
| 1124 |        |        |        |        |        |        |
| 1125 |        |        |        |        |        |        |
| 1126 |        |        |        |        |        |        |
| 1127 |        |        |        |        |        |        |
| 1128 |        |        |        |        |        |        |
| 1129 |        |        |        |        |        |        |
| 1130 |        |        |        |        |        |        |
| 1131 |        |        |        |        |        |        |
| 1132 |        |        |        |        |        |        |
| 1133 |        |        |        |        |        |        |
| 1134 |        |        |        |        |        |        |
| 1135 |        |        |        |        |        |        |
| 1136 |        |        |        |        |        |        |
| 1137 |        |        |        |        |        |        |
| 1138 |        |        |        |        |        |        |
| 1139 |        |        |        |        |        |        |
| 1140 |        |        |        |        |        |        |
| 1141 |        |        |        |        |        |        |
| 1142 |        |        |        |        |        |        |
| 1143 |        |        |        |        |        |        |
| 1144 |        |        |        |        |        |        |
| 1145 |        |        |        |        |        |        |
| 1146 |        |        |        |        |        |        |
| 1147 |        |        |        |        |        |        |
| 1148 |        |        |        |        |        |        |
| 1149 |        |        |        |        |        |        |
| 1150 |        |        |        |        |        |        |
| 1151 |        |        |        |        |        |        |
| 1152 |        |        |        |        |        |        |
| 1153 |        |        |        |        |        |        |
| 1154 |        |        |        |        |        |        |
| 1155 |        |        |        |        |        |        |
| 1156 |        |        |        |        |        |        |
| 1157 |        |        |        |        |        |        |
| 1158 |        |        |        |        |        |        |
| 1159 |        |        |        |        |        |        |
| 1160 |        |        |        |        |        |        |
| 1161 |        |        |        |        |        |        |
| 1162 |        |        |        |        |        |        |
| 1163 |        |        |        |        |        |        |
| 1164 |        |        |        |        |        |        |
| 1165 |        |        |        |        |        |        |
| 1166 |        |        |        |        |        |        |
| 1167 |        |        |        |        |        |        |
| 1168 |        |        |        |        |        |        |
| 1169 |        |        |        |        |        |        |
| 1170 |        |        |        |        |        |        |
| 1171 |        |        |        |        |        |        |
| 1172 |        |        |        |        |        |        |
| 1173 |        |        |        |        |        |        |
| 1174 |        |        |        |        |        |        |
| 1175 |        |        |        |        |        |        |
| 1176 |        |        |        |        |        |        |
| 1177 |        |        |        |        |        |        |
| 1178 |        |        |        |        |        |        |
| 1179 |        |        |        |        |        |        |
| 1180 |        |        |        |        |        |        |
| 1181 |        |        |        |        |        |        |
| 1182 |        |        |        |        |        |        |
| 1183 |        |        |        |        |        |        |
| 1184 |        |        |        |        |        |        |
| 1185 |        |        |        |        |        |        |
| 1186 |        |        |        |        |        |        |
| 1187 |        |        |        |        |        |        |
| 1188 |        |        |        |        |        |        |
| 1189 |        |        |        |        |        |        |
| 1190 |        |        |        |        |        |        |
| 1191 |        |        |        |        |        |        |
| 1192 |        |        |        |        |        |        |
| 1193 |        |        |        |        |        |        |
| 1194 |        |        |        |        |        |        |
| 1195 |        |        |        |        |        |        |
| 1196 |        |        |        |        |        |        |
| 1197 |        |        |        |        |        |        |
| 1198 |        |        |        |        |        |        |
| 1199 |        |        |        |        |        |        |
| 1200 |        |        |        |        |        |        |
| 1201 |        |        |        |        |        |        |
| 1202 |        |        |        |        |        |        |
| 1203 |        |        |        |        |        |        |
| 1204 |        |        |        |        |        |        |
| 1205 |        |        |        |        |        |        |
| 1206 |        |        |        |        |        |        |
| 1207 |        |        |        |        |        |        |
| 1208 |        |        |        |        |        |        |
| 1209 |        |        |        |        |        |        |
| 1210 |        |        |        |        |        |        |
| 1211 |        |        |        |        |        |        |
| 1212 |        |        |        |        |        |        |
| 1213 |        |        |        |        |        |        |
| 1214 |        |        |        |        |        |        |
| 1215 |        |        |        |        |        |        |
| 1216 |        |        |        |        |        |        |
| 1217 |        |        |        |        |        |        |
| 1218 |        |        |        |        |        |        |
| 1219 |        |        |        |        |        |        |
| 1220 |        |        |        |        |        |        |
| 1221 |        |        |        |        |        |        |
| 1222 |        |        |        |        |        |        |
| 1223 |        |        |        |        |        |        |
| 1224 |        |        |        |        |        |        |
| 1225 |        |        |        |        |        |        |
| 1226 |        |        |        |        |        |        |
| 1227 |        |        |        |        |        |        |
| 1228 |        |        |        |        |        |        |
| 1229 |        |        |        |        |        |        |
| 1230 |        |        |        |        |        |        |
| 1231 |        |        |        |        |        |        |
| 1232 |        |        |        |        |        |        |
| 1233 |        |        |        |        |        |        |
| 1234 |        |        |        |        |        |        |
| 1235 |        |        |        |        |        |        |
| 1236 |        |        |        |        |        |        |
| 1237 |        |        |        |        |        |        |
| 1238 |        |        |        |        |        |        |
| 1239 |        |        |        |        |        |        |
| 1240 |        |        |        |        |        |        |
| 1241 |        |        |        |        |        |        |
| 1242 |        |        |        |        |        |        |
| 1243 |        |        |        |        |        |        |
| 1244 |        |        |        |        |        |        |
| 1245 |        |        |        |        |        |        |
| 1246 |        |        |        |        |        |        |
| 1247 |        |        |        |        |        |        |
| 1248 |        |        |        |        |        |        |
| 1249 |        |        |        |        |        |        |
| 1250 |        |        |        |        |        |        |



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|                  |        |
|------------------|--------|
| 500 w = DMH #9   | 140.00 |
| 510'S L#40       | 140.31 |
| 558'S L#44       | 141.83 |
| 563'S MM#8 ART   | 142.00 |
| 576 w/Lat#39     | 142.38 |
| 600 ✓            | 143.09 |
| 610 ✓ LH 38      | 143.40 |
| 630 ✓ ✓ 37       | 143.97 |
| 650 ✓            | 144.54 |
| 658 L#36         | 144.80 |
| 688 ✓ 35         | 145.58 |
| 700              | 146.04 |
| 710 L#34         | 146.34 |
| 750              | 147.51 |
| 760 L#33         | 147.81 |
| 800 w = MM#7 ART | 149.0  |
| 837 L#31         | 149.40 |
| 846 L#32         | 149.50 |
| 850              | 149.55 |
| 900              | 150.09 |
| 946 Lat#30S #29  | 150.59 |
| 950              | 150.63 |
| 1000             | 151.18 |
| 1045 Lat. #28    | 151.67 |
| 1050             | 151.74 |
| 1055 ✓ 27        | 151.79 |

152.46  
0.39  
152.87  
9.82  
161.89

30

| #40    | #40    | #40    | #39    | #39    | #39    |
|--------|--------|--------|--------|--------|--------|
| 140.00 | 142.31 | 142.03 | 142.00 | 143.35 | 143.09 |
| 14.46  | 10.25  | 10.43  | 10.46  | 8.05   | 7.37   |
| 6.92   | 6.32   | 6.32   | 5.46   | 5.00   | 4.32   |
| 6.54   | 13.73  | 4.11   | 7.60   | 43.08  | 16.03  |
| #28    | #37    | #36    | #36    | #35    | #34    |
| 145.40 | 144.20 | 144.56 | 145.80 | 146.58 | 146.04 |
| 7.06   | 8.26   | 7.90   | 6.62   | 6.44   | 6.44   |
| 3.95   | 3.05   | 2.20   | 2.20   | 3.82   | 2.82   |
| 43.11  | 45.41  | 45.70  | 44.60  | 44.92  | 45.64  |
| #34    | #37    | #23    | #29    | #31    | #27    |
| 147.44 | 147.51 | 149.0  | 149.0  | 150.00 | 150.50 |
| 8.12   | 5.61   | 12.89  | 12.89  | 11.49  | 11.39  |
| 0.87   | 75.77  | 8.85   | 7.25   | 7.25   | 6.32   |
| 44.73  |        | 44.04  | 45.14  | 42.89  | 45.07  |
| #34    | #34    | #29    | #29    | #31    | #27    |
| 149.55 | 150.09 | 150.09 | 150.09 | 150.63 | 151.18 |
| 14.34  | 11.80  | 15.25  | 15.08  | 11.26  | 10.71  |
| 6.77   | 6.57   | 9.89   | 11.00  | 6.10   | 5.07   |
| 45.57  | 45.22  | 6.32   | 44.48  | 45.16  | 45.34  |
| #28    | #27    | #27    |        |        |        |
| 152.67 | 151.72 | 152.09 |        |        |        |
| 9.22   | 10.17  | 9.80   |        |        |        |
| 6.50   | 6.22   | 7.41   |        |        |        |
| 42.74  | 42.68  | 42.39  |        |        |        |

CONTINUED

|                            |        |
|----------------------------|--------|
| 10'S                       | 152.10 |
| 1120 = MH # 6              | 152.50 |
| 55' x 1' MH # 6 = Lot # 25 | 153.40 |
| 60' x 1' ✓ ✓ ✓ = DE        | 153.50 |
| 40' S. of MH # 6           | 153.05 |
| 66' ✓ ✓ ✓ = Lot # 26       | 153.40 |
| 80' ✓ ✓ ✓ = DE             | 153.60 |

16189 X

31

|        |        |             |        |        |        |
|--------|--------|-------------|--------|--------|--------|
| 152.10 | 152.50 | 153.50      | #25    | 153.05 | #26    |
| 7.77   | 7.39   | 8.34        | 153.40 | 8.84   | 153.60 |
| 7.10   | 6.87   | 7.53        | 8.79   | 7.30   | 8.79   |
| 17.68  | 4.12   | 23.86       | 41.33  | 4.04   | 3.05   |
|        |        |             | 42.91  |        | 75.24  |
| DE     | 4.51   | 157.40 B.M. |        |        |        |
| 153.60 | 157.38 | Check       |        |        |        |
| 8.29   |        |             |        |        |        |
| 347    |        |             |        |        |        |
| +5.00  |        |             |        |        |        |



# HYACINTH + PLUMOSA SEWER LINE

|                      |        |        |
|----------------------|--------|--------|
| EX. MH = 0+00        | 110.0  |        |
| 50 N                 | 110.78 |        |
| 100 r                | 110.57 |        |
| 105 = Lat # 84       | 110.60 | 111.10 |
| 150                  | 110.85 |        |
| 200                  | 111.1  |        |
| 213.58 = MH # 27 ALT | 111.22 |        |
| 250 w                | 112.73 |        |
| 300                  | 114.89 |        |
| 350                  | 116.90 |        |
| 400                  | 118.98 |        |
| 430 = Lat # 83       | 120.23 |        |
| 450                  | 121.07 |        |
| 495 = Lat # 86       | 122.95 | 125.00 |
| 500                  | 123.15 |        |
| 540 = Lat # 85       | 124.88 |        |
| 543.58 = DE          | 125.00 |        |

12/23/25

33

|        |        | HEV    |         | MH     |        |
|--------|--------|--------|---------|--------|--------|
| 110.28 | 110.57 | 111.10 | 110.55  | 111.14 | 111.22 |
| 14.59  | 14.30  | 13.77  | 14.04   | 13.73  | 13.65  |
| 10.27  | 10.77  | 11.55  | 10.11   | 10.7   | 9.55   |
| +2.22  | +3.53  | +2.22  | +3.61   | 0.7    | +4.10  |
| 114.81 | 116.90 | 118.98 | 121.0   | 121.07 | 121.0  |
| 10.06  | 7.97   | 5.89   | 14.00   | 3.80   | 11.00  |
| 5.84   | 4.13   | 2.13   | 9.14    | 0.3    | 6.96   |
| +2.27  | +3.87  | +3.76  | +1.14   | +3.57  | +4.04  |
| 123.15 | 125.80 | 125.00 | DE      |        |        |
| 11.85  | 9.20   | 10.00  |         |        |        |
| 8.30   | 4.99   | 6.83   |         |        |        |
| +3.55  | +4.21  | +3.17  |         |        |        |
| 10.86  | 110.14 |        |         |        |        |
| 11.00  | 9.49   |        |         |        |        |
| 11.96  | 4.60   |        |         |        |        |
| 119.6  | +4.89  |        |         |        |        |
|        |        | 2.13   | 1220.00 | 0.0057 | 2.0    |
|        |        |        | 10.65   |        |        |
|        |        |        | 155.0   |        | 114.40 |
|        |        |        | 144.1   |        |        |
|        |        |        | 59.0    |        |        |

NARCISSUS SEWER

M.H. #15 = 0700  
 50 SW  
 100  
 150 Lat #67 S  
 195 ✓ #65 N  
 258 ✓ #66 S  
 294 = M.H. #16  
 318 Lat #64  
 350  
 400  
 413 Lat #62 S f #63  
 450  
 500  
 520 #61 N  
 530 #60 S  
 544 = DE.

135.0  
 135.85  
 136.70  
 137.55  
 138.34  
 139.39  
 140.0  
 140.29  
 140.67  
 141.27  
 141.40  
 141.87  
 142.47  
 142.71  
 144.83  
 143.0

1396  
 1271  
 152.2V

M.H. #15

|        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|
| 135.0  | 135.55 | 136.70 | 137.55 | 138.32 | 139.39 | 140.0  |
| 17.32  | 16.47  | 15.62  | 14.77  | 12.00  | 11.93  |        |
| 10.70  | 8.78   | 6.86   | 5.91   | 6.02   | 5.47   |        |
| +6.62  | +7.77  | +5.76  | +5.85  | +7.95  | +7.26  |        |
| #64    |        |        | #62 S  |        |        |        |
| 140.29 | 140.67 | 141.27 | 141.80 | 141.87 | 142.47 | 142.71 |
|        | 11.65  | 11.05  | 142.00 | 10.45  | 9.85   |        |
|        | 5.11   | 5.20   | 10.22  | 5.20   | 4.22   |        |
|        | +6.54  | +5.85  | 4      | +5.45  | +5.62  |        |
| 142.82 | 142.0  | = DE   |        |        |        |        |
|        | 9.32   |        |        |        |        |        |
|        | 3.95   |        |        |        |        |        |
|        | +6.37  |        |        |        |        |        |
| #67    | #65    | #66    | #64    | #62    | #63    | #61    |
| 138.50 | 142.0  | 140.0  | 141.52 | 144.0  | 143.32 | 144.32 |
| 13.82  | 10.22  | 11.22  | 8.00   | 1.632  | 9.00   | 8.00   |
| 5.52   | 4.27   | 5.92   | 3.42   | 3.97   | 2.00   | 1.45   |
| 5.23   | +5.65  | +6.40  | 7.06   | +6.35  | +6.94  | +6.52  |
| #60    |        |        |        |        |        |        |
| 143.50 |        |        |        |        |        |        |
| 8.82   |        |        |        |        |        |        |
| 4.17   |        |        |        |        |        |        |
| +4.65  |        |        |        |        |        |        |

# HYACINTH SEWER

|                 |        |        |
|-----------------|--------|--------|
| #13 MH = 0+00   | 114.75 |        |
| 75 Lat #74      | 114.70 | 115.40 |
| 50              | 114.45 |        |
| 109 S = Lat #75 | 114.10 |        |
| 163 = DMH #14   | 113.75 |        |
| 200 #73 SW      | 120.0  |        |
| 250             | 123.72 |        |
| 265 #72         | 124.36 |        |
| 300             | 125.57 |        |
| 320 #71         | 126.72 |        |
| 350             | 128.01 |        |
| 383 #70         | 129.42 |        |
| 400             | 130.16 |        |
| 442 #69         | 131.96 | 136.0  |
| 450             | 132.30 |        |
| 494 #68         | 134.18 |        |
| 512 = MH #15    | 135.0  |        |

35

|        | #68     | #69    | #70    |
|--------|---------|--------|--------|
| 152.32 | 135.0   | 137.30 | 132.30 |
| 11.95  | 173.27  | 155.32 | 140.02 |
| 140.40 | 15.32   | 6.56   | 11.92  |
| 141.57 | 6.56    | 48.46  | +8.10  |
| 12.97  | 4.71    |        | +7.30  |
| 147.60 | 131.00  | 129.36 | 122.72 |
| 135    | 10.57   | 15.70  | 17.85  |
| 147.88 | 1.27    | 8.22   | 14.57  |
|        | 9.10    | 17.22  | 5.37   |
|        | DMH #14 | +7.70  | 46.20  |
|        | 130.00  | 113.75 | #74    |
|        | 11.57   | 27.82  | 7.5    |
|        | 12.97   | 14.92  | 114.10 |
|        | +8.00   | 114.80 | 15.78  |
|        |         | 15.88  | 15.43  |
|        |         | 4.32   | 6.43   |
|        | 114.75  | +10.78 | +13.62 |
|        | 15.13   |        | +9.00  |
|        | 11.19   |        |        |
|        | 3.94    |        |        |
| 132.91 | 121.58  | 123.72 | 125.57 |
| 132.40 | 11.33   | 9.19   | 128.01 |
| 132.41 | 3.57    | 1.31   | 16.80  |
| 144.81 | +7.46   | +7.88  | 8.14   |
| 144.40 |         |        | +8.56  |
|        |         |        | +8.52  |
|        | 132.30  | 135.0  |        |
|        | 12.51   | 9.81   |        |
|        | 4.57    | 2.7    |        |
|        | +7.74   | +6.64  |        |
| 1813   | #74     | 6.62   | #75    |
| 1875   | 115.40  | 114.45 | 114.10 |
|        | 14.35   | 15.30  | 15.65  |
| 1396   | 10.53   | 7.96   | 14.95  |
| 140.10 | +3.82   | +7.34  | 5.20   |
| 140.08 |         |        | +10.45 |
| 140.65 |         |        |        |
| 141.32 |         |        |        |
| 141.17 |         |        |        |
|        | 115.40  | 114.45 | 114.10 |
|        |         |        | 114.80 |
|        |         |        | 16.37  |
|        |         |        | 5.48   |
|        |         |        | 10.89  |
|        |         |        |        |
|        |         |        | 114.75 |
|        |         |        | 16.42  |
|        |         |        | 11.77  |
|        |         |        | +4.65  |

HAZEL + WISTERIA POWER

|                     |        |
|---------------------|--------|
| DE = 0200           | 107.0  |
| +08 #116 S          | 106.75 |
| +50                 | 105.46 |
| +60 #117 S          | 105.16 |
| 100                 | 103.93 |
| 107 #118 S          | 102.72 |
| 150                 | 102.40 |
| 155 #119 S          | 102.25 |
| 200                 | 100.86 |
| 205 #120 S + #122 N | 100.71 |
| 250 #121 S          | 99.31  |
| 260 = M.H. #23      | 99.00  |
| 270 #123 N          | 98.67  |
| 293 #124 S          | 97.90  |
| 300                 | 97.66  |
| 315 #125 N          | 97.16  |
| 344 #126 N          | 96.20  |
| 350                 | 96.00  |
| 365 #127 N          | 95.50  |
| 390 #128 S          | 94.66  |
| 400                 | 94.33  |
| 420 #129 N          | 93.67  |
| 450                 | 92.65  |
| 470 #130            | 92.00  |
| 496                 | 91.14  |
| 505 #131            | 90.84  |
| 570 #132 N          | 90.30  |

10861 286 P 12/31/45  
500 Chats + Freedland

|                                                      |                                                               |                                                       |                                                      |                                                           |                                                      |                                          |
|------------------------------------------------------|---------------------------------------------------------------|-------------------------------------------------------|------------------------------------------------------|-----------------------------------------------------------|------------------------------------------------------|------------------------------------------|
| 107.0<br>102.9<br>409<br>117.29<br>104.25<br>106.32  | H116 S<br>106.75<br>107.20<br>7.87<br>5.64<br>+2.27           | 105.26<br>11.82<br>3.31<br>28.02                      | H117 S<br>105.16<br>105.86<br>11.03<br>6.01<br>+5.42 | 102.93<br>13.26<br>5.83<br>+7.52                          | H118 S<br>103.72<br>104.02<br>12.87<br>7.77<br>+5.60 | 102.40<br>14.89<br>5.35<br>+6.54         |
| H119 S<br>102.25<br>12.95<br>14.34<br>10.87<br>+3.27 | H120 S<br>100.71<br>16.63<br>10.41<br>15.88<br>75.54<br>+3.75 | H121 N<br>100.71<br>102.71<br>17.58<br>20.05<br>+2.53 | H122 S<br>99.31<br>102.00<br>2.32<br>7.32<br>+5.00   | H123 N<br>99.00<br>7.32<br>1.95<br>+5.34                  | H124 N<br>98.67<br>100.67<br>4.65<br>3.12<br>+5.13   | H125 S<br>98.60<br>7.72<br>3.12<br>+2.60 |
| 97.66<br>8.66<br>2.75<br>+5.91                       | H125 N<br>97.16<br>99.16<br>7.16<br>3.40<br>+5.00             | H126 S<br>96.20<br>97.0<br>9.22<br>5.12<br>+1.00      | H127 N<br>96.00<br>10.32<br>4.32<br>+5.60            | H128 S<br>95.50<br>97.0<br>9.22<br>10.86<br>7.30<br>+2.56 | H129 N<br>93.67<br>90.0<br>10.02<br>5.02<br>+4.95    |                                          |
| 94.65<br>13.67<br>6.02<br>+7.21                      | H130<br>92.00<br>92.00<br>12.32<br>6.72<br>+5.52              | H131 S<br>90.84<br>92.0<br>14.32<br>2.07<br>+6.25     | H132 N<br>90.30<br>92.50<br>13.52<br>7.9<br>+5.90    | 91.14<br>15.15<br>7.95<br>+7.20                           |                                                      |                                          |

AZALEA + WISTERIA SEWERS

|                |       |
|----------------|-------|
| 548 = M.H. #24 | 90.00 |
| 580            | 88.88 |
| 635 #132S      | 8760  |
| 642 #135N      | 8744  |
| 685 #136S      | 865N  |
| 695 #137N      | 865N  |
| 735 #138S      | 8556  |
| 757 #139N      | 8508  |
| 794 #140S      | 8427  |
| 799 #133       | 8415  |
| 805 = M.H. #25 | 84.00 |

1063N

1277  
93.55  
431  
94.26

M.H. #24

90.00 88.88  
16.5N 17.44  
9.19 10.84  
+7.13 +6.60

#132V

8760  
18.7N  
11.25  
+7.00  
90.20  
18.32  
11.32  
+5.00

#135N

8744  
88.40  
17.92  
12.27  
+5.15

#136

865N  
11.8N  
5.2V  
+6.60  
88.0  
10.86  
+4.77  
5.53

#137

865N  
87.00  
17.86  
6.59  
+4.77

#138

8556  
17.80  
6.70  
+8.10  
87.00  
11.86  
5.91  
+5.28

#139

8508

13.78  
7.46  
6.22

8568  
17.68  
10.72  
+1.90

#140

8427

86.0  
12.36  
7.03

+5.03

#133

8415

86.0  
12.36  
7.03

+4.76

M.H. #25

84.00

14.26  
7.97

+6.39



# HYACINTH SEWER

MH #v = 0+00

50' ✓

85' Lat #81

96' ✓ #80

100' ✓

150

189 #79

200

216 #78

250

300

321 #77

350

357 #76

400

422.2 = DMH #14

111.2 ✓

111.5 ✓

111.6 ✓

111.67

111.8 ✓

112.1 ✓

112.35

112.4 ✓

112.5 ✓

112.71 ✓

113.01 ✓

113.13 ✓

113.31 ✓

113.35 ✓

113.61

113.75

10861

1120

100.73

004

120.89

1120

137.91

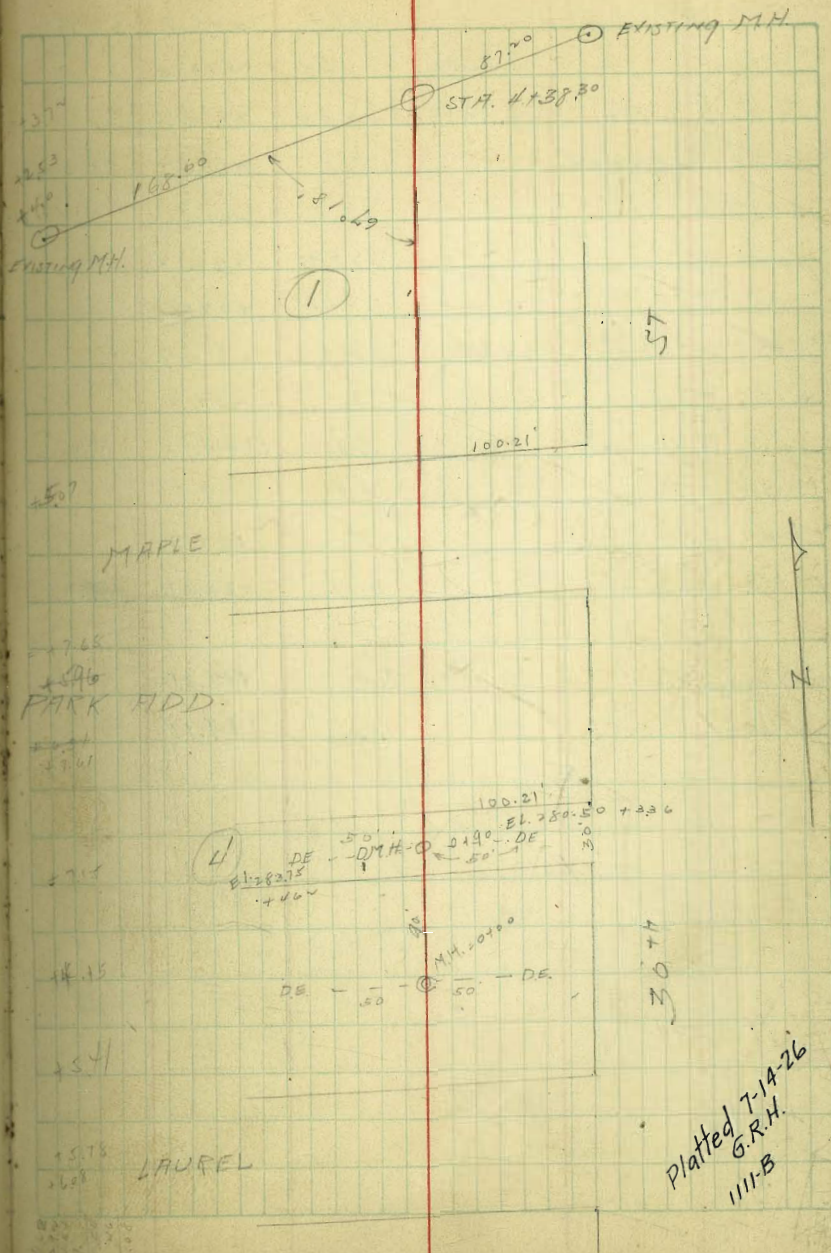
1/6/76

38

|         | #81     | #50    |        |         |         |         |     |
|---------|---------|--------|--------|---------|---------|---------|-----|
| 111.2 ✓ | 111.5 ✓ | 112.20 | 110.0  | 111.8 ✓ | 112.1 ✓ | 112.2 ✓ |     |
| 9.71    | 9.41    | 8.73   | 6.43   | 9.11    | 8.81    | 8.51    |     |
| 5.41    | 4.78    | 3.61   | 1.65   | 3.43    | 1.78    | 0.04    |     |
| +7.10   | +4.63   | 5.12   | +3.78  | +5.68   | +7.03   | +8.47   |     |
| #79     | #78     | 112.71 | 113.01 | #77     | 113.31  | 115.0   | #76 |
| 118.0   | 114.0   | 20.20  | 19.90  | 120.0   | 19.60   | 17.91   |     |
| 14.41   | 18.91   | 10.62  | 8.82   | 12.91   | 6.96    | 2.23    |     |
| 904     | 1087    | +9.58  | +11.07 | 320     | +12.64  | +10.68  |     |
| +5.87   | +5.02   |        |        | +9.71   |         |         |     |
| 112.61  | 112.75  | 120.00 |        |         |         |         |     |
| 19.30   | 19.16   | 12.91  |        |         |         |         |     |
| 5.62    | 5.07    | 5.27   |        |         |         |         |     |
| +13.68  | +13.49  | +7.24  |        |         |         |         |     |

Sewer Location & Construction Thru Moore  
BIRs 1 & 4 Park Add 2/20/26

|                   |      |        |       |        |                  |
|-------------------|------|--------|-------|--------|------------------|
| SE Kalma + 30th   | 5.05 | 294.76 |       | 299.71 |                  |
| DE to EAST        | ✓    |        | 2.52  | 290.22 | 286.5            |
| ✓ V. West         | ✓    |        | 5.73  | 289.03 | 286.5            |
| M.H. BIR 4 = 0700 |      |        | 4.76  | 290.00 | 286.0            |
| 45' W             | ✓    |        | 5.52  | 289.22 | 284.30           |
| 70' W             |      |        | 5.7   | 289.0  |                  |
| 76                |      |        | 7.9   | 286.8  |                  |
| 80                |      |        | 8.2   | 286.5  |                  |
| 81                |      |        | 8.7   | 286.0  |                  |
| 96' x 1 = D.M.H.  |      |        | 8.09  | 286.67 | 281.60<br>280.00 |
| 100               |      |        | 8.6   | 286.1  |                  |
| 101               |      |        | 7.9   | 286.8  |                  |
| 105               |      |        | 6.9   | 287.8  |                  |
| 130               | ✓    |        | 7.37  | 287.39 | 289.70<br>281.43 |
| 165               |      |        | 7.55  | 287.21 |                  |
| 172 = BREAK       | OUT  |        | 8.5   | 286.4  | 280.20<br>279.40 |
| 175               |      |        |       |        |                  |
| T.P.              | 0.58 | 282.71 | 12.63 | 282.12 |                  |
| 185               | ✓    |        | 2.5   | 279.96 | 277.81           |
| T.P.              | 1.47 | 271.35 | 12.83 | 269.85 |                  |
| 200               | ✓    |        | 2.92  | 268.43 | 264.28           |
| T.P.              | 0.12 | 259.15 | 12.32 | 259.03 |                  |
| 275               | ✓    |        | 3.05  | 255.77 | 250.06           |
| T.P.              | 0.20 | 246.25 | 13.07 | 246.08 |                  |
| 250               | ✓    |        | 4.66  | 241.62 | 235.84<br>228.00 |
| 262 = BREAK       |      |        |       |        |                  |
| 265               |      |        | 13.2  | 223.0  |                  |
| T.P.              | 1.39 | 235.53 | 12.12 | 224.12 |                  |





# CRANE PLACE

|                  | Feb    | Mar    |
|------------------|--------|--------|
| SL Sutter = 0100 | 255.00 | 254.50 |
| 60 S             | 255.37 | 254.85 |
| 120 S            | 255.68 | 255.18 |
| 180 S = PC       | 256.0  | 255.50 |
| ± Curvar         | 255.75 |        |

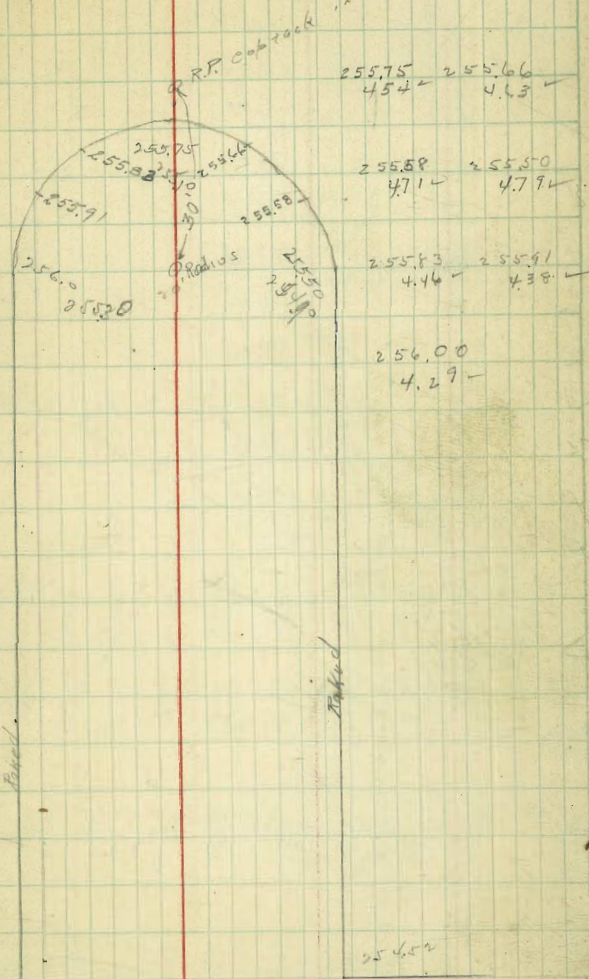
5/17/26  
set cb marks

|           |              |        |       |
|-----------|--------------|--------|-------|
| Sewer lot | at Main      | 250.57 | 9.80  |
|           | at top of EL | 252.0  | 1.1   |
|           |              |        | +1.9  |
|           |              |        | 5.27  |
|           |              |        | 1.9   |
|           |              |        | +6.77 |

Sutter + Goldfinch N.E. CP

|        |    |        |        |        |
|--------|----|--------|--------|--------|
| 256.99 | EL | 255.50 | 255.90 | 256.10 |
| 270    |    | 4.0    | 4.6    | 4.3    |
| 257.69 |    | 2.2    | 1.4    | 4.6    |
| 517    |    | +4.2   |        | -0.3   |
| 257.54 | WL | 254.65 | 255.0  | 255.20 |
| 255    |    | 5.7    | 5.4    | 5.0    |
| 260.27 |    | 6.0    | 3.9    | 6.4    |
|        |    | +1.7   | 1.5    | -1.4   |

256.99  
260 +  
259.59 - HI  
5.75  
255.66  
21.5  
260.27



SUTTER



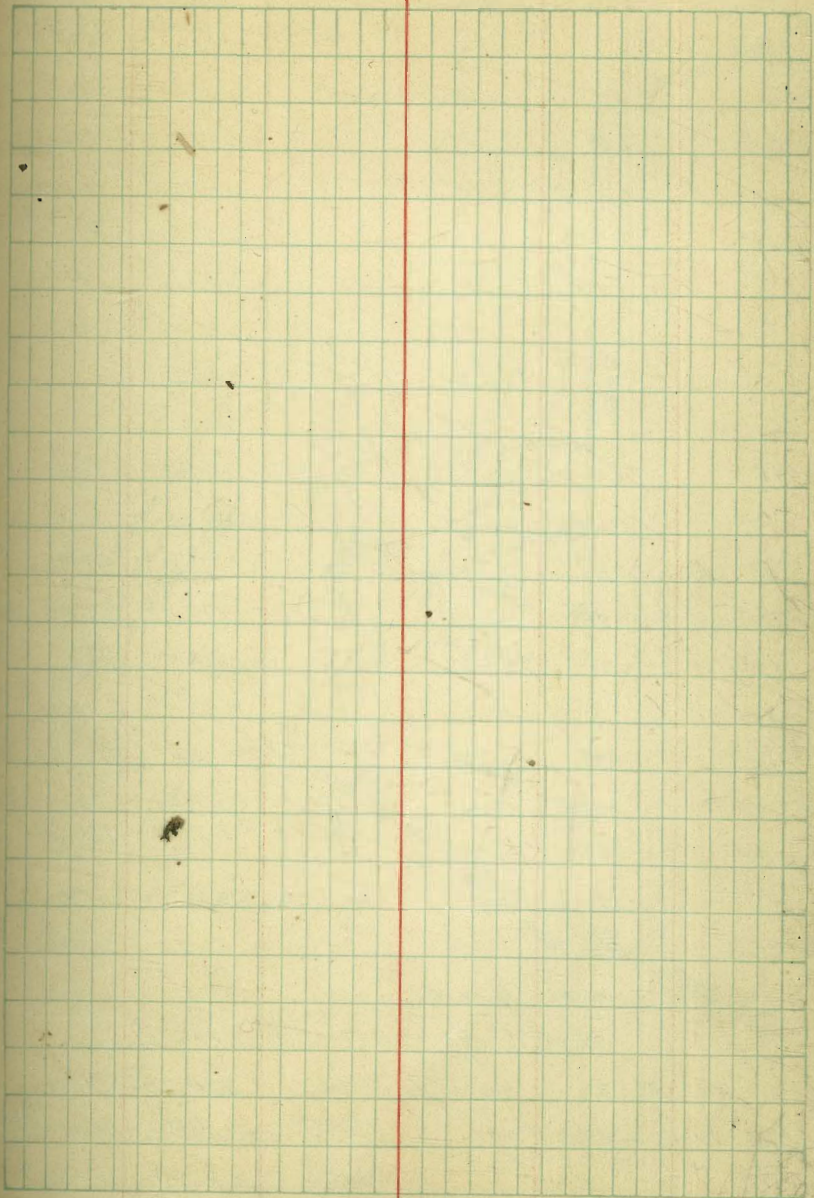


Moist Flow

CONT  
64.84  
6.70  
12.45  
77.15

|                  |      |       |       |      |
|------------------|------|-------|-------|------|
|                  |      | 1106  | 5.06  |      |
| 400              | 6.3  | 58.11 | 59.10 | 5.4  |
| 500              |      | 59.77 | 60.77 | 1.0  |
| 600              | 3.0  | 61.62 | 62.62 | 1.0  |
| 700              | 10.0 | 66.75 | 67.75 | 1.0  |
| 800              | 10.0 | 71.88 | 72.88 | 1.0  |
| 600.2 wt. Gains  |      | 77.0  | 78.0  |      |
|                  |      |       |       |      |
| EL BARRAN = 0000 |      | 8.0   | 7.5   |      |
| 50               | 0.0  | 8.75  | 8.5   | +0.1 |
| 100              | 0.1  | 9.50  | 9.50  | +0.5 |
| 150              | +1.4 | 10.5  |       | +0.2 |
| 200              | +0.4 | 10.80 |       | +0.3 |
| 250              | +0.7 | 11.45 |       | +0.2 |
| 300              | +0.1 | 12.10 |       | 0.0  |
| 350              | +0.1 | 12.76 |       | -0.3 |
| 400              | +0.5 | 13.41 |       | -0.2 |
| 450              | +0.3 | 14.06 |       | +0.2 |
| 500              | +0.4 | 14.71 |       | +0.3 |
| 550              | +0.6 | 15.37 |       | +0.4 |
| wt. cable        | +0.2 | 16.0  | 16.0  | 0.0  |
| PL ✓             | +0.2 | 17.0  | 17.0  | +0.1 |
| 50 F             | +0.4 | 17.69 | 17.69 | +0.1 |
| 100              | +0.5 | 18.38 | 18.37 | +0.5 |
| 150              | +0.4 | 19.01 | 19.06 | +0.5 |

20.0  
17.3  
17.3  
20.0  
17.3  
17.3  
16.1



| Milit Five      |      | Cont. |            |
|-----------------|------|-------|------------|
|                 | NCB  |       | SCB        |
| 200             | +0.7 | 19.76 | 19.35 +0.7 |
| 250             | +0.8 | 20.45 | 20.13 +0.8 |
| 300             | +1.0 | 21.15 | 21.14 +1.1 |
| 350             | +1.0 | 21.85 | 21.81 +1.0 |
| 400             | +1.1 | 22.54 | 22.59 +1.0 |
| 450             | +1.0 | 23.23 | 23.18 +0.9 |
| 500             | +0.6 | 23.94 | 23.87 +1.0 |
| 550             | +0.1 | 24.61 | 23.56 +0.6 |
| 600 = w/L Dalor |      | 25.30 | 25.25      |
| EL ✓            |      | 25.75 | 25.80      |
| 50              | +0.2 | 26.18 | 26.23 +0.5 |
| 100             | +0.1 | 26.62 | 26.66 +0.3 |
| 150             | -0.2 | 27.06 | 27.10 +0.1 |
| 200             | -0.2 | 27.50 | 27.53 -0.2 |
| 250             | -0.2 | 27.93 | 27.96 +0.1 |
| 300             | -0.1 | 28.27 | 28.29 0.0  |
| 350             | -0.3 | 28.81 | 28.83 -0.1 |
| 400             | -0.4 | 29.24 | 29.26 +0.1 |
| 450             | 0.0  | 29.68 | 29.70 -0.1 |
| 500             | 0.0  | 30.14 | 30.12 0.0  |
| 550             | -0.1 | 30.56 | 30.55 +0.1 |
| 600 = w/L Ebers | 0.0  | 31.0  | 31.0 +0.1  |

Sewer Location 8th & Harbor

4.51 6.85

234 = 8" M<sup>6</sup>

chk. Flow DM #1 R-59

12.75 - 5.90 - Floor MH #1

" " MH #1 R-59

12.92 - 6.07 - MH #1

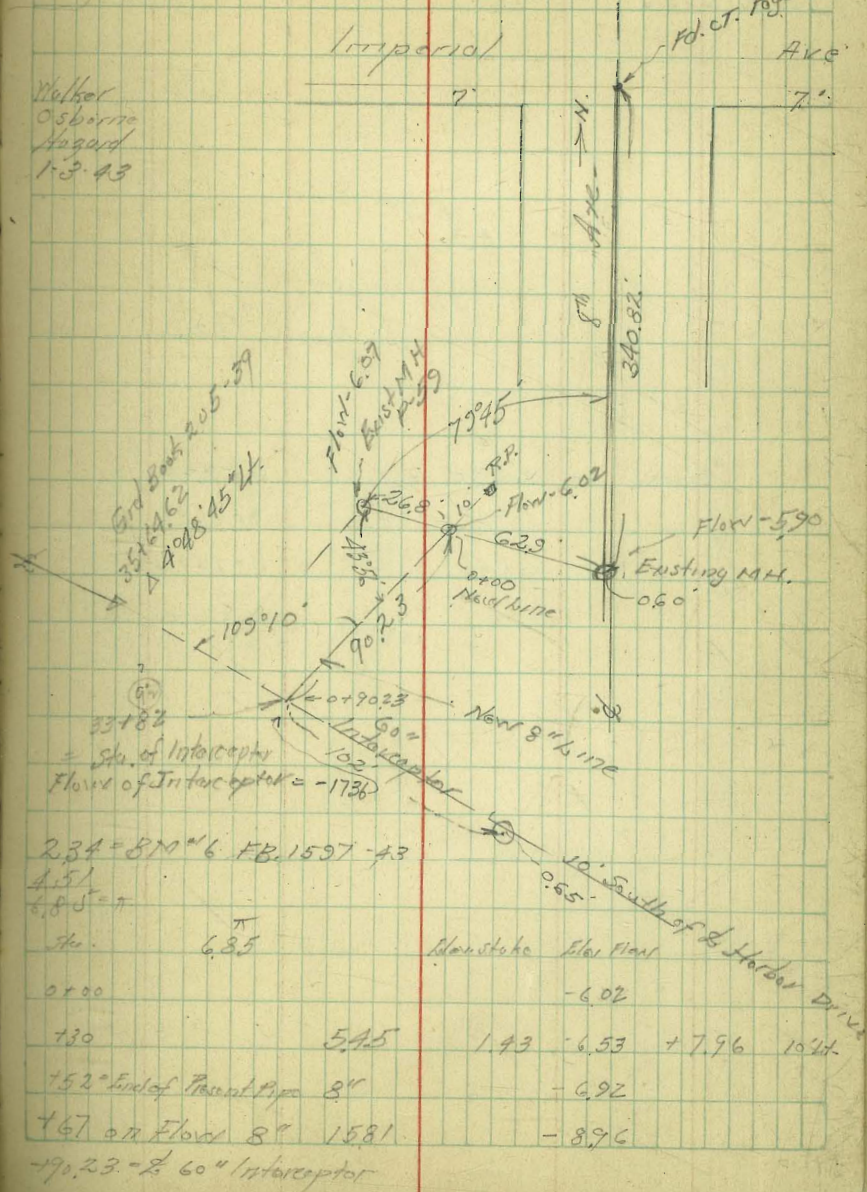
CHK 35+00  
FB Grid 205-39

1.12

5.73 ✓

3500  
2317  
1.54  
1.57  
1.57  
1.54

Location Newly Const. 8<sup>th</sup> & Harbor 45  
8th Ave And Harbor Drive  
Sewer Partly Constructed  
from 0+52 to 0+90.23



234 = 8" M<sup>6</sup> FB 1597-43

4.51

6.85

Flow 6.85

0+00

730

152' End of Present Pipe 8"

+67 on Flow 8" 1581

-190.23 = 2" 60" Interceptor

Flow 6.85

Flow 6.02

5.45

1.43

-6.92

-8.96

10' South of Harbor Drive

1.43

6.53

+7.96

10' H.



Filley Parking  
Bik 208 UNIV AVE.

W

E

SL Lincoln 20400

OK here

by Lorenson

Moore 5/12/46

Break

358.0

358.20

357.29

357.64

356.98

357.07

357.98 NW UNIV 4 1/2  
3.20  
361.70

26

W

358.0

357.49

3.20

4.21

3.71

40.50

E

358.20

357.64

3.50

4.04

W

358.0

E

358.20

356.98

357.07



|      |       | 322.91 | Levels on paving on<br>30th ST. |                                                         |
|------|-------|--------|---------------------------------|---------------------------------------------------------|
|      | 50 W  |        |                                 | 322.60 W<br>2.31<br>322.31<br>6.22<br>328.64 W<br>321.0 |
| E    |       |        | 1.93                            | 320.98                                                  |
| W    |       |        | 1.94                            | 320.99                                                  |
|      |       |        |                                 | 320<br>3.47<br>+0.15                                    |
| W    | 100   |        | 1.47                            | 321.44                                                  |
| E    |       |        | 1.35                            | 321.56                                                  |
|      |       |        |                                 | 321.54<br>3.08<br>2.93<br>+0.15                         |
|      | 150   |        |                                 |                                                         |
| E    |       |        | 0.87                            | 322.10                                                  |
| W    |       |        | 0.87                            | 322.07                                                  |
| T.P. | 763   | 329.45 | 1.09                            | 321.82                                                  |
|      | 200 W |        |                                 | 322.09<br>2.53<br>2.20<br>+0.11                         |
| W    |       |        | 6.90                            | 327.55                                                  |
| E    |       |        | 6.88                            | 327.57                                                  |
|      | 250   |        |                                 | 322.65<br>6.01<br>5.84<br>+0.11                         |
| E    |       |        | 6.37                            | 323.08                                                  |
| W    |       |        | 6.31                            | 323.14                                                  |
|      | 300   |        |                                 | 323.18<br>5.46<br>5.31<br>+0.15                         |
| W    |       |        | 5.77                            | 323.68                                                  |
| E    |       |        | 5.87                            | 323.58                                                  |
|      | 350   |        |                                 | 323.72<br>4.94<br>4.78<br>+0.14                         |
| E    |       |        | 5.23                            | 324.22                                                  |
| W    |       |        | 5.20                            | 324.25                                                  |
|      | 400   |        |                                 | 324.27<br>4.37<br>4.21<br>+0.14                         |
| W    |       |        | 4.68                            | 324.77                                                  |
| E    |       |        | 4.71                            | 324.74                                                  |
|      | 450   |        |                                 | 324.82<br>3.84<br>3.68<br>+0.14                         |
| E    |       |        | 4.16                            | 325.24                                                  |
| W    |       |        | 4.17                            | 325.25                                                  |
|      |       |        |                                 | 325.36<br>3.78<br>3.17<br>+0.11                         |

|      |                   | 329.45 |        |                                                              |
|------|-------------------|--------|--------|--------------------------------------------------------------|
|      | 500               |        |        |                                                              |
| W    |                   | 3.58   | 325.87 |                                                              |
| E    |                   | 3.55   | 325.90 |                                                              |
|      | 550               |        |        | 325.91<br>2.73<br>2.63<br>+0.10                              |
| E    |                   | 3.01   | 326.42 |                                                              |
| W    |                   | 3.03   | 326.42 |                                                              |
|      | 599 = SL U PAS ST |        |        | 326.46<br>2.18<br>2.10<br>+0.08                              |
| W    |                   | 2.57   | 326.88 |                                                              |
| T.P. | 589               | 332.95 | 2.39   | 327.06                                                       |
| E    |                   | 5.96   | 326.99 |                                                              |
|      | check to BM       | 7.28   | 325.67 | 325.52                                                       |
|      |                   |        |        | 327.0<br>BOTH<br>T.P. 589<br>327.00<br>7.44<br>1.53<br>+0.11 |

T 48

328.64  
1.54  
327.05  
4.71  
321.76

ALLEY PAVING  
BIR 50 U.H.

20' wide  
5/13/46 Mosco

|                   | W        |       | E        |       |
|-------------------|----------|-------|----------|-------|
| St. Mont 000 0100 | 348.86 ✓ |       | 348.89 ✓ |       |
| +50               | 348.67   | +0.30 | 348.74   | +0.56 |
| 1                 | 348.50   | +1.0  | 348.58   | +1.02 |
| +50               | 348.33   | +0.38 | 348.42   | +1.0  |
| W                 | 348.17   | +0.63 | 348.27   | +0.62 |
| +50               | 348.00   | +0.20 | 348.12   | +0.28 |
| 3                 | 347.84   | +1.0  | 347.96   | +1.0  |
| +50               | 347.67   | +1.0  | 347.81   | +0.27 |
| 4                 | 347.51   | +0.04 | 347.65   | +0.27 |
| +50               | 347.34   | -0.23 | 347.50   | +1.0  |
| 5                 | 347.18   | +0.09 | 347.31   | +0.50 |
| +50               | 347.01   | +0.91 | 347.19   | +0.68 |
| 6 - N4 Meade      | 346.85 ✓ |       | 347.02 ✓ |       |

60' Campus + Cleveland  
348.00 NE BP Meade + Campus

576  
551.70  
3.10  
346.60  
5.12  
353.72  
4.83  
348.89  
4.04  
344.93  
5.01  
347.94  
3.95  
351.87

|   |        |       |       |       |       |       |
|---|--------|-------|-------|-------|-------|-------|
| W | 348.67 | 485.0 | 473.3 | 481.7 | 481.0 | 476.4 |
|   | 5.05   | 5.12  | 5.34  | 4.76  | 4.93  | 5.09  |
|   | 4.75   | 4.22  | 5.38  | 4.13  | 4.73  | 4.09  |
|   | +0.30  | +1.0  | 5.00  | +0.63 | +0.20 | +1.0  |
|   |        |       | +0.53 |       |       |       |
| E | 487.4  | 485.8 | 484.2 | 482.7 | 481.2 | 479.6 |
|   | 4.98   | 5.14  | 5.30  | 5.25  | 4.81  | 4.77  |
|   | 0.22   | 4.12  | 4.30  | 4.83  | 4.53  | 3.77  |
|   | +0.56  | +1.02 | +1.0  | +0.62 | +0.28 | +1.0  |
| W | 476.7  | 475.1 | 473.6 | 471.8 | 470.1 | 468.5 |
|   | 5.26   | 4.36  | 4.52  | 4.69  | 4.86  | 5.01  |
|   | 4.32   | 4.72  | 4.72  | 4.60  | 3.82  |       |
|   | +1.0   | +0.02 | -0.23 | +0.07 | +0.77 |       |
| E | 478.1  | 476.5 | 475.0 | 473.4 | 471.9 | 470.4 |
|   | 5.14   | 5.28  | 4.87  | 4.53  | 4.68  | 4.83  |
|   | 4.85   | 5.01  | 4.37  | 4.03  | 4.00  |       |
|   | +0.27  | +0.27 | +1.0  | +0.50 | +0.68 |       |



|                             |        |       |        |       |
|-----------------------------|--------|-------|--------|-------|
| ↓ 33+90.6 = EC              | 6.6    | 295.5 | 295.53 | 0.0   |
| 13                          | 4.6    | 297.5 | 296.90 | +0.6  |
| 12                          | 3.4    | 298.7 | 298.25 | +0.5  |
| 11                          | 1.7    | 300.4 | 299.60 | +0.8  |
| TP 094                      | 302.07 | 12.68 | 301.13 |       |
| 10                          | 10.0   | 303.8 | 301.0  | +2.8  |
| 9                           | 6.5    | 307.3 | 302.33 | +5.0  |
| 8                           | 4.9    | 308.9 | 303.67 | +5.3  |
| 7                           | 5.4    | 308.4 | 305.01 | +6.6  |
| 6                           | 6.6    | 307.2 | 306.36 | +10.9 |
| 5                           | 7.6    | 306.2 | 307.70 | -1.5  |
| 4                           | 6.3    | 307.5 | 309.04 | -1.5  |
| 3                           | 1.7    | 312.1 | 310.39 | +1.8  |
| 2                           | 1.7    | 312.1 | 311.73 | +0.4  |
| 1                           | 2.0    | 311.8 | 313.07 | -1.3  |
| 29+90.40 = PC Az 28° 40' RT | 2.2    | 311.6 | 314.42 | -1.8  |
| TP 0.05                     | 313.80 | 12.55 | 313.75 |       |
| 29+50                       | 13.4   | 312.9 | 316.82 | -3.9  |
| 28+90.40 = EC               | 8.9    | 317.4 | 319.12 | -1.7  |
| ① 2855.56                   | 5.2    | 321.1 | 320.60 |       |
| 28+50 = BREAK               | 4.0    | 322.3 | 321.00 |       |
| ② 2826.91                   | 6.7    | 319.6 | 321.82 |       |
| ③ 2795.28                   | 6.4    | 319.9 | 322.30 |       |
| ④ 2763.64                   | 6.4    | 319.9 | 322.38 |       |
| +57                         | 9.0    | 317.3 | 322.42 |       |
| +55                         | 6.0    | 320.3 | 322.47 |       |
| 27+52                       |        |       |        |       |

326.30 π

|            |
|------------|
| 1° 01' 25" |
| 2 02 50    |
| 3 04 15    |
| 4 05 40    |
| 5 07 05    |
| 6 08 30    |
| 7 09 55    |
| 8 11 20    |
| 9 12 45    |
| 10 14 10   |
| 11 15 35   |
| 12 17 00   |
| 13 18 25   |
| 14 19 50   |

A = 28° 40' RT  
 R = 800'  
 S.T. = 204.41  
 chords = 28.57  
 L = 400.26

BREAK

culvert

# Hog Canyon Road

52

|       |               |        |       |        |        |                |
|-------|---------------|--------|-------|--------|--------|----------------|
| 45    | P.O.T. = T.P. |        | 9.3   | 261.19 | 259.34 | +1.9           |
|       | +50           |        | 10.0  | 260.4  | 260.0  | +0.4           |
| 44    |               |        | 10.3  | 260.1  | 260.67 | -0.6           |
|       | +50           |        | 10.7  | 259.7  | 261.33 | -1.7           |
| 43    | BREAK         |        | 10.4  | 260.0  | 262.0  | -2.0 ✓ = BREAK |
|       | +50           |        | 9.1   | 261.3  | 263.73 | -2.4           |
| 42    |               |        | 6.3   | 264.1  | 265.46 | -1.3           |
| T.P.  | 2.35          | 270.42 | 12.09 | 268.07 |        |                |
|       | +50           |        | 13.1  | 267.1  | 267.19 | 0.0            |
| 41    |               |        | 7.3   | 272.9  | 268.92 | +4.0           |
|       | +50           |        | 3.3   | 276.9  | 270.65 | +6.4           |
| 40    |               |        | 3.2   | 277.0  | 272.38 | +4.6           |
|       | +50           |        | 2.0   | 278.2  | 274.11 | +4.1           |
| 39    |               |        | 2.5   | 277.7  | 275.84 | +1.9           |
|       | +50           |        | 3.0   | 277.2  | 277.57 | -0.4           |
| 38    |               |        | 2.7   | 277.5  | 279.30 | -1.8           |
| T.P.  | 2.35          | 280.16 | 12.96 | 277.81 |        |                |
|       | +50           |        | 12.50 | 278.3  | 281.03 | -2.7           |
| 37    |               |        | 10.0  | 280.8  | 282.76 | -2.0           |
|       | +50           |        | 7.8   | 283.0  | 284.49 | -1.5           |
| 36    |               |        | 6.0   | 284.8  | 286.25 | -1.4           |
|       | +50           |        | 3.8   | 287.0  | 288.00 | -1.0           |
| T.P.  | 1.69          | 290.77 | 12.99 | 289.08 |        |                |
| 35    |               |        | 12.7  | 289.4  | 290.36 | -1.0           |
| 34+50 |               |        | 9.8   | 292.3  | 292.72 | -0.4           |

302.07

π

BREAK

Hog Canyon Road

|                 |      |        |        |               |
|-----------------|------|--------|--------|---------------|
| 45              | 1.63 | 262.82 | 261.19 | P.O.T.        |
| +50             |      |        | 2.3    | 260.5 258.67  |
| 46              |      |        | 2.9    | 259.9 258.0   |
| +50             |      |        | 3.9    | 258.9         |
| 47              |      |        | 5.5    | 257.3         |
| +50             |      |        | 6.9    | 255.9         |
| 48              |      |        | 8.4    | 254.4         |
| +50             |      |        | 10.5   | 252.3         |
| 49              |      |        | 12.3   | 250.5         |
| T.P.            | 090  | 251.42 | 12.30  | 250.52        |
| +50             |      |        | 3.2    | 248.2         |
| 49+80.47=PC     |      |        | 4.35   | 247.07 on hub |
| 50+11 = Culvert |      |        | 6.6    | 244.8         |
| 50+17           |      |        | 5.7    | 245.7         |
| ⊙               |      |        | 5.5    | 245.9         |
| ⊙               |      |        | 7.1    | 244.3         |
| ⊙               |      |        | 9.0    | 242.4         |
| ⊙               |      |        | 9.9    | 241.5         |
| ⊙               |      |        | 11.0   | 240.4         |
| ⊙               |      |        | 12.2   | 239.2         |
| 53+35.86 = P.O. |      |        | 13.1   | 238.3         |
| 54              |      |        | 14.4   | 237.0         |
| +50             |      |        | 13.8   | 237.6         |
| 55              |      |        | 14.4   | 237.0         |
| +50             |      |        | 13.6   | 237.8         |
| 56              |      |        | 13.1   | 238.3         |

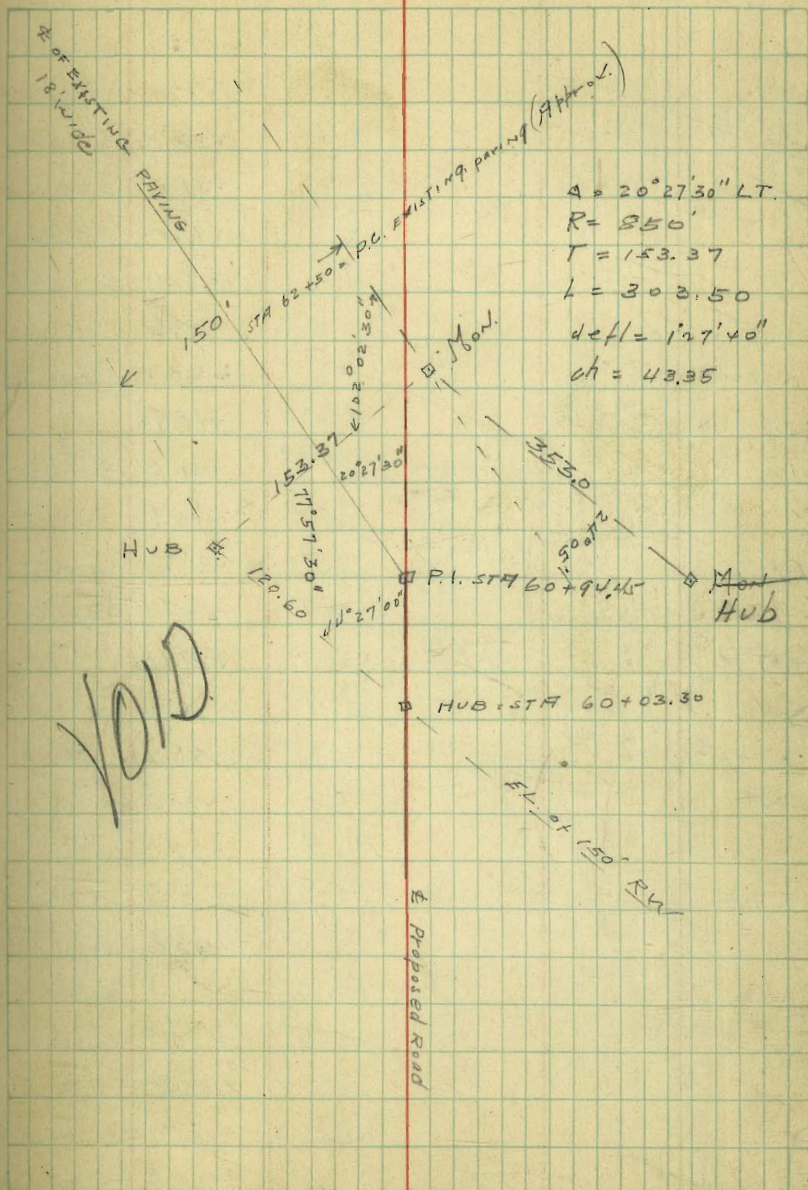
7 pts  
50.76

+11.8  
+19  
← see page 55

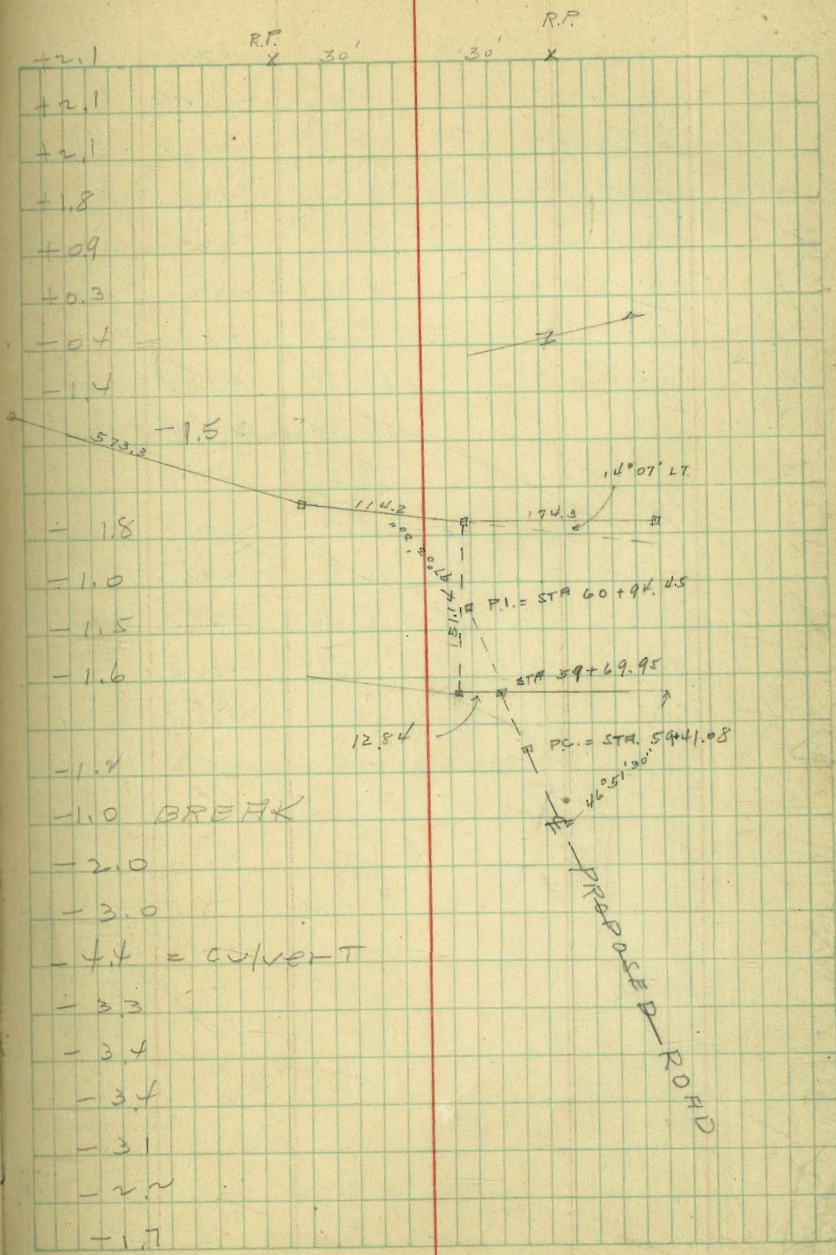
49+80.47 = PC  
 $\Delta$  22° 37' 2"  
 ST = 180.00  
 CO = 355.39  
 ch = 50.76  
 R = 900



| Station                      | Description          | Station | Value  | Notes         |
|------------------------------|----------------------|---------|--------|---------------|
| +50                          |                      | 12.6    | ~38.8  |               |
| 57                           |                      | 12.8    | ~38.6  |               |
| +50                          |                      | 12.2    | ~39.2  |               |
| 58                           |                      | 11.7    | ~39.7  |               |
| +18.60 POT.                  | 386                  | ~43.41  | 11.87  | ~39.55 on hub |
| +50                          |                      | 4.5     | ~38.9  |               |
| 59                           |                      | 6.2     | ~37.2  |               |
| +41.08 = PC                  |                      | 7.4     | ~36.0  |               |
| +54.220                      |                      | 8.4     | ~35.0  |               |
| 60+27.76 @                   |                      | 9.0     | ~34.4  |               |
| 60+40 @                      | culvert              | 11.5    | ~31.9  |               |
| +71.0 @                      |                      | 9.6     | ~33.8  |               |
|                              | 26.5' N to SL paving | 8.1     | ~35.3  |               |
| 61+14.44 @                   |                      | 8.1     | ~35.3  |               |
|                              | 11' N to SL paving   | 6.4     | ~37.0  |               |
| 61+57.78 @                   | on SL paving         | 4.8     | ~38.6  |               |
| 62+01.14 @                   |                      | 3.3     | ~40.1  |               |
| 62+44.58 = E.C.P. = @ E.V. ✓ |                      | 200     | ~41.41 |               |
| TP                           | 9x5                  | ~50.66  | 4.0    | ~46.66        |
| 64+44.58                     | on paving            |         |        |               |



| from page 52    |      |          |        |          |
|-----------------|------|----------|--------|----------|
| 46+55.23 New PC | 18.5 | 263.04   | 201.19 | = P.O.T. |
|                 | 1.5  |          | 258.5  | 256.39   |
|                 | 6.0  |          | 257.0  | 254.90   |
|                 | 7.5  |          | 255.5  | 253.42   |
|                 | 9.3  |          | 253.7  | 251.93   |
|                 | 11.7 |          | 251.3  | 250.45   |
| T.P             | 0.4  | 250.36   | 249.4  |          |
|                 | 1.1  |          | 249.2  | 248.96   |
|                 | 3.2  |          | 247.1  | 247.48   |
| 50+10.72 = EC   | 5.7  |          | 244.6  | 246.0    |
| +50             | 7.0  |          | 243.3  | 244.56   |
| +93 = CULVERT   | 9.4  |          | 240.9  |          |
| 51              | 8.7  |          | 241.6  | 243.40   |
| +50             | 9.4  |          | 240.9  | 241.93   |
| 52              | 11.2 |          | 239.1  | 240.47   |
| +50             | 12.9 |          | 237.4  | 239.01   |
| 53 TP           | 3.7  | 241.61   | 238.14 |          |
| 53              | 5.4  |          | 236.2  | 237.44   |
| +50             | 6.6  |          | 235.0  | 236.0    |
| 54              | 7.9  |          | 233.7  | 235.63   |
| +50             | 9.4  |          | 232.2  | 235.22   |
| +80 = CULVERT   | 10.9 | 236 pipe | 230.7  | 235.10   |
| 55              | 10.0 |          | 231.6  | 234.90   |
| +50             | 10.5 |          | 231.1  | 234.53   |
| 55+89.8 = PC    | 10.8 |          | 230.8  | 234.24   |
|                 | 10.8 |          | 230.8  | 233.94   |
|                 | 10.2 |          | 231.4  | 233.63   |
|                 | 10.0 |          | 231.6  | 233.31   |



4676=ch

241.61

57+5300 ↓

5

6

58+75.12 = EC

59

+50

+85

60

+10

+25

+50

+85

61 paving

+50 ✓

62 ✓

|      |        |              |
|------|--------|--------------|
| 9.4  | ~37.2  | 233.0        |
| 8.9  | ~37.7  | 233.28       |
| 8.6  | ~33.0  | 233.56       |
| 8.6  | ~33.0  | 233.84       |
| 8.6  | ~33.0  | 234.0        |
| 8.6  | ~33.0  | 234.24       |
| 9.0  | ~37.6  |              |
| 10.7 | ~30.9  | 234.68       |
| 11.7 | ~29.9  | 234.75       |
| 9.5  | ~37.1  |              |
| 9.4  | ~37.4  | 235.04       |
| 6.9  | ~34.7  |              |
| 6.4  | ~35.4  | 235.40       |
| 4.8  | ~36.8  |              |
| 2.9  | ~38.7  |              |
| 2.7  | ~34.54 | 239.55 = PVI |

-0.8 = BREAK

-0.6

-0.6

-0.8

-1.0

-1.2

-3.5

-4.8 = CULVERT

-2.6

0.0 = PAVING

at first survey = STA 58+18.60

PC = 55+89.82

Δ = 20° 26'

PI = 57+37.00

EC = 58+75.12

ch = 40.72

L = 285.30

def = 10' 27" 34"

SS = 144.8

56

30th + Redwood Culvert

|                             |      |        |       |        |           |
|-----------------------------|------|--------|-------|--------|-----------|
| SWBP.                       | 207  | 304.13 |       | 302.06 |           |
|                             | 0.89 | √92.15 | 12.87 | √91.76 |           |
| Howline at 105' from outlet |      |        | 14.38 | √77.77 |           |
|                             | 8.50 | √88.94 | 11.71 | √80.44 |           |
| Howline at outlet           |      |        | 12.38 | √76.56 | .015 Rate |

|        |         |
|--------|---------|
| 302.06 | 105     |
| 3.28   | 337     |
| 305.34 | 14.38   |
| 12.87  |         |
| √92.15 | 26      |
| 8.89   | 4       |
| √94.13 | 104     |
| 12.87  |         |
| √80.44 |         |
| 12.38  |         |
| √77.77 | 277.77  |
| 1.5    | 276.56  |
|        | 1.21    |
|        | .01152  |
| 105    | 1.21000 |
|        | 1.05    |
|        | 1.60    |
|        | 1.05    |
|        | 5.50    |
|        | 5.25    |
|        | 2.50    |
| .01152 |         |
| 45     |         |
| 57.60  |         |
| 4008   |         |
| 51840  |         |
| 27722  | 11.0    |
| 27828  | 2.8     |
|        | 13.84   |

S. D. ELEC. RR Co. Grades on K ST.

|                              | S. Track | N. Track |
|------------------------------|----------|----------|
| 36' of EL 5th Ex. rails 5000 | 5.00     | 5.25     |
| +14                          | 5.12     |          |
| +64                          | 5.54     |          |
| +114                         | 5.97     |          |
| +164 = w L 6th               | 6.40     | 6.55     |
| ↓ w L 6th                    | 6.76     |          |
| EL 6th                       | 7.20     | 7.35     |
| 50 E                         | 8.01     |          |
| 100                          | 8.82     |          |
| 150                          | 9.64     |          |
| 200 = w L 7th                | 10.45    | 10.60    |
| 10 w L 7th                   | 10.69    |          |
| EL 7th                       | 11.10    | 11.25    |
| 50                           | 11.90    |          |
| 100                          | 12.70    |          |
| 150                          | 13.50    |          |
| 200 = w L 8th                | 14.30    | 14.45    |
| EL 8th                       | 14.95    | 14.55    |
| 50                           | 14.83    |          |
| 100                          | 15.27    |          |
| 150                          | 15.71    |          |
| 200 = w L 9th                | 16.15    | 16.15    |
| EL 9th                       | 16.68    |          |
| 50                           | 17.11    | 17.25    |
| 100                          | 17.50    |          |

698 SE 3rd K + 6th  
Moore 11/21/25 58

|              |       |       |       |       |       |       |       |       |       |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 36.5         |       |       |       |       |       |       |       |       |       |
| 10.61        |       |       |       |       |       |       |       |       |       |
| 216          |       |       |       |       |       |       |       |       |       |
| 10.85        | 5.12  | 5.54  | 5.97  | 6.40  | 6.76  | 7.20  | 8.01  | 8.82  | 9.64  |
| 14.62        | 5.49  | 5.97  | 6.40  | 6.76  | 7.20  | 7.64  | 8.01  | 8.45  | 8.97  |
| 1.57         |       |       |       |       |       |       |       |       |       |
| 1.08         |       |       |       |       |       |       |       |       |       |
| 1.76         |       |       |       |       |       |       |       |       |       |
| 11.05 NW 7th |       |       |       |       |       |       |       |       |       |
| 10.45        | 10.69 | 11.10 | 11.90 | 12.70 | 13.50 | 14.30 | 15.10 | 15.90 | 16.70 |
| 0.16         | 0.90  | 0.66  | 0.86  | 0.80  | 0.80  | 0.80  | 0.80  | 0.80  | 0.80  |
| 11.05 NW     | 14.40 | 14.85 | 15.27 | 15.71 | 16.15 | 16.68 | 17.11 | 17.50 | 17.93 |
| 15.87        | 3.36  | 3.93  | 4.57  | 5.27  | 6.01  | 6.78  | 7.61  | 8.48  | 9.38  |
| 1.70         |       |       |       |       |       |       |       |       |       |
| 16.17        |       |       |       |       |       |       |       |       |       |
| 1.84         |       |       |       |       |       |       |       |       |       |
| 1.06         |       |       |       |       |       |       |       |       |       |
| 17.21        | 17.80 | 18.39 | 18.98 | 19.50 | 20.00 | 20.50 | 21.00 | 21.50 | 22.00 |
| 3.85         | 0.26  | 0.67  | 0.98  | 1.25  | 1.50  | 1.75  | 2.00  | 2.25  | 2.50  |
| 100 E        |       | 18.29 |       |       |       |       |       |       |       |
| 150          |       | 18.98 |       |       |       |       |       |       |       |
| 100          |       | 19.10 |       |       |       |       |       |       |       |
| 170 E Rail   |       | 19.13 |       |       |       |       |       |       |       |
|              |       |       |       |       |       |       | 19.19 |       |       |

Sewer Outfall Construction  
Foot of 8th St  
690 T

Harbor  
Moore  
4/1/26

|                                           | Flowline                    | Elev.           |       |
|-------------------------------------------|-----------------------------|-----------------|-------|
| 0100s Exist 8" Sewer                      | Flowline                    | 12.88 =         | -5.98 |
| + 72.5                                    | EXISTING 6" Sewer Flowline  | 12.55 = Elev    | -6.08 |
| + 80                                      | 24" Storm Drain Top of pipe | 7.10 = -0.58 MH | -6.17 |
| 1 + 86                                    |                             |                 | -6.23 |
| 1 + 91 = M.H. A 180° to LT                |                             |                 | -6.29 |
| + 50                                      |                             |                 | -6.33 |
| + 75                                      |                             |                 | -6.39 |
| 1 + 72                                    |                             |                 | -6.45 |
| + 50                                      |                             |                 | -6.51 |
| + 75                                      |                             |                 | -6.57 |
| 3                                         |                             |                 | -6.63 |
| + 30                                      |                             |                 | -6.69 |
| + 55                                      |                             |                 | -6.76 |
| + 75                                      |                             |                 | -6.84 |
| 4                                         |                             |                 | -6.87 |
| + 75                                      |                             |                 | -6.93 |
| + 50                                      |                             |                 | -6.99 |
| + 75                                      |                             |                 | -7.05 |
| 5                                         |                             |                 | -7.11 |
| 6 + 00 = water edge                       |                             |                 | -7.17 |
| 11 + 50 = spike in pile at Long Bulk head |                             |                 | -7.51 |
| " about water level 12:00 Noon 6/1/26     |                             |                 | -8.73 |

-0.00239

1011 NWBP L + 10th

16.93  
16.93  
8.70  
2.40  
11.17  
11.17  
4.0  
17.07  
17.07  
11.17  
5.90

131  
125  
178

Nail in Tool House

Ring 7.64  
F.L. 13.47 } below nail

57' line of Imperial

Walker 1-29-43

Flow MW #1 - -6.29

-7.07

978' Elev. Run

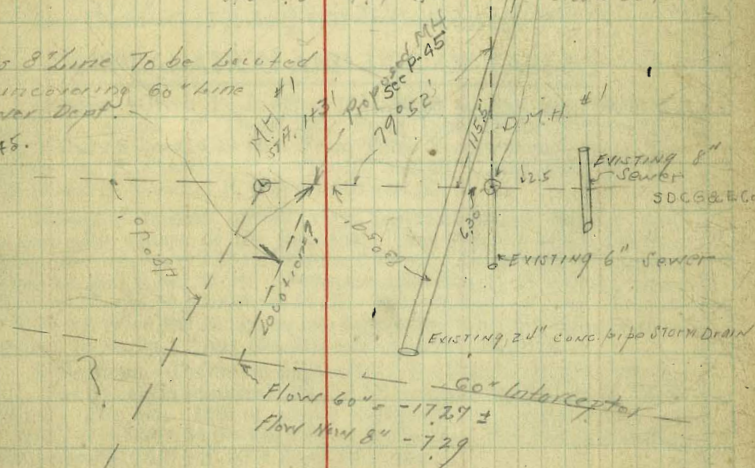
500'

5.18' Foot Elev. Floor Cut

365 2.13 -7.29 + 9.42

2x2 Grouting  
clean out

This 8" line to be located  
after uncovering 60" line  
by Sewer Dept.  
See 45.

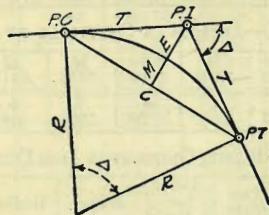


Flow 60" = -17.34 ±  
Flow MW #4 = -7.29

|                                           |       |              |        |                                   |
|-------------------------------------------|-------|--------------|--------|-----------------------------------|
| Chatsworth                                |       |              |        |                                   |
| SE BP DUMS                                | 12.00 | 157.13       | 145.13 |                                   |
| T.P.                                      | 13.19 | 163.45       | 6.87   | 150.26                            |
| ELLIOTT<br>SWBP CHARLESUS Dr.             |       |              | 6.31   | 157.14                            |
| on pipe                                   |       |              | 13.30  | 150.15 on pipe                    |
| T.P.                                      | 5.43  | 159.52       | 9.36   | 154.09                            |
| VILLA DR.<br>SEBP ELLIOTT                 |       |              | 9.17   | 150.35                            |
| Curb Fly. on Woolman at Olivewood Terrace |       |              |        |                                   |
| B.M.                                      | 0.35  | 63.77        | 63.44  | SE top H.V.S.T.<br>27th + Woolman |
| cb 100 w of W.L. 37th                     |       | side Woolman | 9.33   | 54.44                             |
| T.P.                                      | 2.33  | 55.37        | 11.73  | 54.04                             |
| cb return <del>149.7</del>                |       | of W.L. 37th | 3.66   | 51.71                             |
| " " 149.7                                 |       | Woolman      | 3.67   | 51.70                             |
| cb NW cor Olivewood + Woolman at R. angle |       |              | 7.00   | 48.35 with prop cor               |
| SE cor Olivewood + Woolman                |       |              | 7.55   | 47.84                             |
| top of graded dirt return SW cor          |       |              | 6.00   | 49.37                             |

## DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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### CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R(1 - \cos \frac{\Delta}{2}) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{2} - R \quad (8) = R \sec \frac{\Delta}{2} - R \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

### EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{2} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. —  $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 — Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

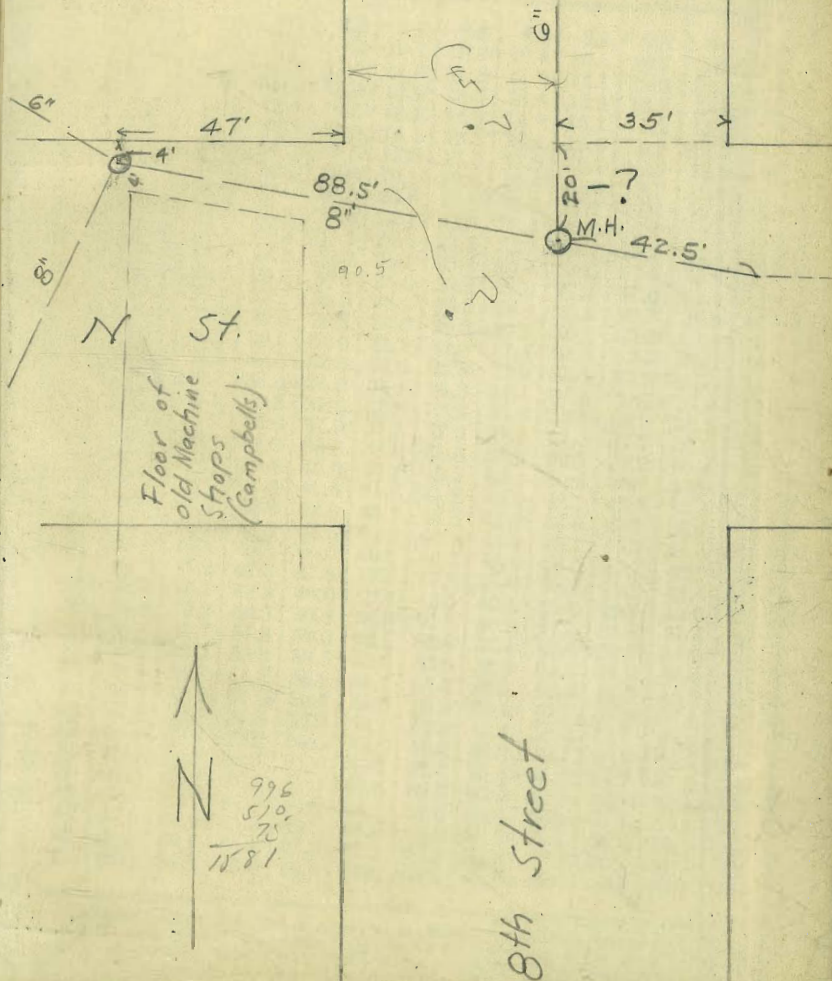
**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$  and from Table V correction = .10 or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

These ties are not correct  
 Location of manholes check very closely with notes on page 59.  
 H.R.B.  
 10-28-30

See Drainage Plans of 8th St. Harbor Dept.

Note: Apparently Banker's measurements were from curb-lines instead of property lines G.P.A.

Location of sewers in the vicinity of 8th & N Sts. by W.E. Banker 11-26-29.





Narcissus  $49^{\circ} 01' 33''$

WL ch = 25.65  
 det  $1^{\circ} 45'$   
 EL ch = 21.99

6" = 6.34  
 8" = 8.34

1893  
 4733

1500  
 993  
 507.7

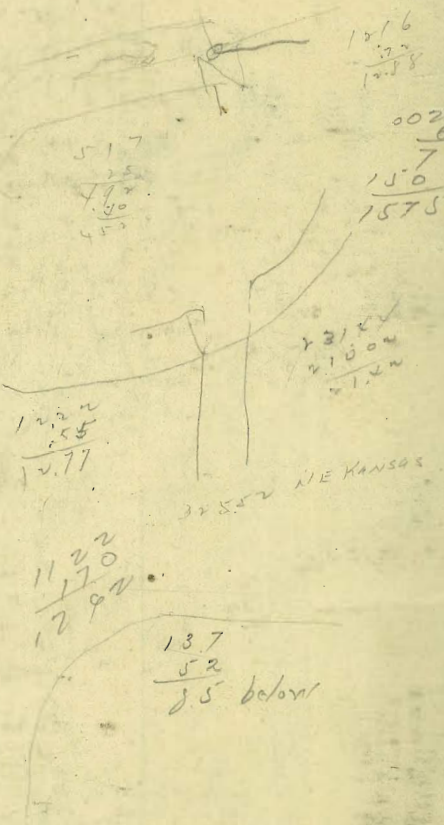
2087  
 526  
 137.61

2135  
 330  
 525.5

600330  
 91.15  
 609245  
 155  
 6250.00

1658  
 1457  
 88

72  
 12.41  
 33.73  
 12.77  
 .36



16030  
 10.5  
 58.15

1673  
 12.20  
 155.20 ON P.H.  
 110000 NW

746  
 1.0  
 4.8

15925  
 208  
 15740

104.00

3450  
 657  
 2218.19

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2.  
 For Single Track Embankment.

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.2  | 8.3  | 8.5  | 8.6  | 8.8  | 8.9  | 9.1  | 9.2  | 9.4  | 0  |
| 1  | 9.5  | 9.7  | 9.8  | 10.0 | 10.1 | 10.3 | 10.4 | 10.6 | 10.7 | 10.9 | 1  |
| 2  | 11.0 | 11.2 | 11.3 | 11.5 | 11.6 | 11.8 | 11.9 | 12.1 | 12.2 | 12.4 | 2  |
| 3  | 12.5 | 12.7 | 12.8 | 13.0 | 13.1 | 13.3 | 13.4 | 13.6 | 13.7 | 13.9 | 3  |
| 4  | 14.0 | 14.2 | 14.3 | 14.5 | 14.6 | 14.8 | 14.9 | 15.1 | 15.2 | 15.4 | 4  |
| 5  | 15.5 | 15.7 | 15.8 | 16.0 | 16.1 | 16.3 | 16.4 | 16.6 | 16.7 | 16.9 | 5  |
| 6  | 17.0 | 17.2 | 17.3 | 17.5 | 17.6 | 17.8 | 17.9 | 18.1 | 18.2 | 18.4 | 6  |
| 7  | 18.5 | 18.7 | 18.8 | 19.0 | 19.1 | 19.3 | 19.4 | 19.6 | 19.7 | 19.9 | 7  |
| 8  | 20.0 | 20.2 | 20.3 | 20.5 | 20.6 | 20.8 | 20.9 | 21.1 | 21.2 | 21.4 | 8  |
| 9  | 21.5 | 21.7 | 21.8 | 22.0 | 22.1 | 22.3 | 22.4 | 22.6 | 22.7 | 22.9 | 9  |
| 10 | 23.0 | 23.2 | 23.3 | 23.5 | 23.6 | 23.8 | 23.9 | 24.1 | 24.2 | 24.4 | 10 |
| 11 | 24.5 | 24.7 | 24.8 | 25.0 | 25.1 | 25.3 | 25.4 | 25.6 | 25.7 | 25.9 | 11 |
| 12 | 26.0 | 26.2 | 26.3 | 26.5 | 26.6 | 26.8 | 26.9 | 27.1 | 27.2 | 27.4 | 12 |
| 13 | 27.5 | 27.7 | 27.8 | 28.0 | 28.1 | 28.3 | 28.4 | 28.6 | 28.7 | 28.9 | 13 |
| 14 | 29.0 | 29.2 | 29.3 | 29.5 | 29.6 | 29.8 | 29.9 | 30.1 | 30.2 | 30.4 | 14 |
| 15 | 30.5 | 30.7 | 30.8 | 31.0 | 31.1 | 31.3 | 31.4 | 31.6 | 31.7 | 31.9 | 15 |
| 16 | 32.0 | 32.2 | 32.3 | 32.5 | 32.6 | 32.8 | 32.9 | 33.1 | 33.2 | 33.4 | 16 |
| 17 | 33.5 | 33.7 | 33.8 | 34.0 | 34.1 | 34.3 | 34.4 | 34.6 | 34.7 | 34.9 | 17 |
| 18 | 35.0 | 35.2 | 35.3 | 35.5 | 35.6 | 35.8 | 35.9 | 36.1 | 36.2 | 36.4 | 18 |
| 19 | 36.5 | 36.7 | 36.8 | 37.0 | 37.1 | 37.3 | 37.4 | 37.6 | 37.7 | 37.9 | 19 |
| 20 | 38.0 | 38.2 | 38.3 | 38.5 | 38.6 | 38.8 | 38.9 | 39.1 | 39.2 | 39.4 | 20 |
| 21 | 39.5 | 39.7 | 39.8 | 40.0 | 40.1 | 40.3 | 40.4 | 40.6 | 40.7 | 40.9 | 21 |
| 22 | 41.0 | 41.2 | 41.3 | 41.5 | 41.6 | 41.8 | 41.9 | 42.1 | 42.2 | 42.4 | 22 |
| 23 | 42.5 | 42.7 | 42.8 | 43.0 | 43.1 | 43.3 | 43.4 | 43.6 | 43.7 | 43.9 | 23 |
| 24 | 44.0 | 44.2 | 44.3 | 44.5 | 44.6 | 44.8 | 44.9 | 45.1 | 45.2 | 45.4 | 24 |
| 25 | 45.5 | 45.7 | 45.8 | 46.0 | 46.1 | 46.3 | 46.4 | 46.6 | 46.7 | 46.9 | 25 |
| 26 | 47.0 | 47.2 | 47.3 | 47.5 | 47.6 | 47.8 | 47.9 | 48.1 | 48.2 | 48.4 | 26 |
| 27 | 48.5 | 48.7 | 48.8 | 49.0 | 49.1 | 49.3 | 49.4 | 49.6 | 49.7 | 49.9 | 27 |
| 28 | 50.0 | 50.2 | 50.3 | 50.5 | 50.6 | 50.8 | 50.9 | 51.1 | 51.2 | 51.4 | 28 |
| 29 | 51.5 | 51.7 | 51.8 | 52.0 | 52.1 | 52.3 | 52.4 | 52.6 | 52.7 | 52.9 | 29 |
| 30 | 53.0 | 53.2 | 53.3 | 53.5 | 53.6 | 53.8 | 53.9 | 54.1 | 54.2 | 54.4 | 30 |
| 31 | 54.5 | 54.7 | 54.8 | 55.0 | 55.1 | 55.3 | 55.4 | 55.6 | 55.7 | 55.9 | 31 |
| 32 | 56.0 | 56.2 | 56.3 | 56.5 | 56.6 | 56.8 | 56.9 | 57.1 | 57.2 | 57.4 | 32 |
| 33 | 57.5 | 57.7 | 57.8 | 58.0 | 58.1 | 58.3 | 58.4 | 58.6 | 58.7 | 58.9 | 33 |
| 34 | 59.0 | 59.2 | 59.3 | 59.5 | 59.6 | 59.8 | 59.9 | 60.1 | 60.2 | 60.4 | 34 |
| 35 | 60.5 | 60.7 | 60.8 | 61.0 | 61.1 | 61.3 | 61.4 | 61.6 | 61.7 | 61.9 | 35 |
| 36 | 62.0 | 62.2 | 62.3 | 62.5 | 62.6 | 62.8 | 62.9 | 63.1 | 63.2 | 63.4 | 36 |
| 37 | 63.5 | 63.7 | 63.8 | 64.0 | 64.1 | 64.3 | 64.4 | 64.6 | 64.7 | 64.9 | 37 |
| 38 | 65.0 | 65.2 | 65.3 | 65.5 | 65.6 | 65.8 | 65.9 | 66.1 | 66.2 | 66.4 | 38 |
| 39 | 66.5 | 66.7 | 66.8 | 67.0 | 67.1 | 67.3 | 67.4 | 67.6 | 67.7 | 67.9 | 39 |
| 40 | 68.0 | 68.2 | 68.3 | 68.5 | 68.6 | 68.8 | 68.9 | 69.1 | 69.2 | 69.4 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \times 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

Made in Germany.