

GRADE 127 BOOK

POSTS

FIELD BOOK

No. 385

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

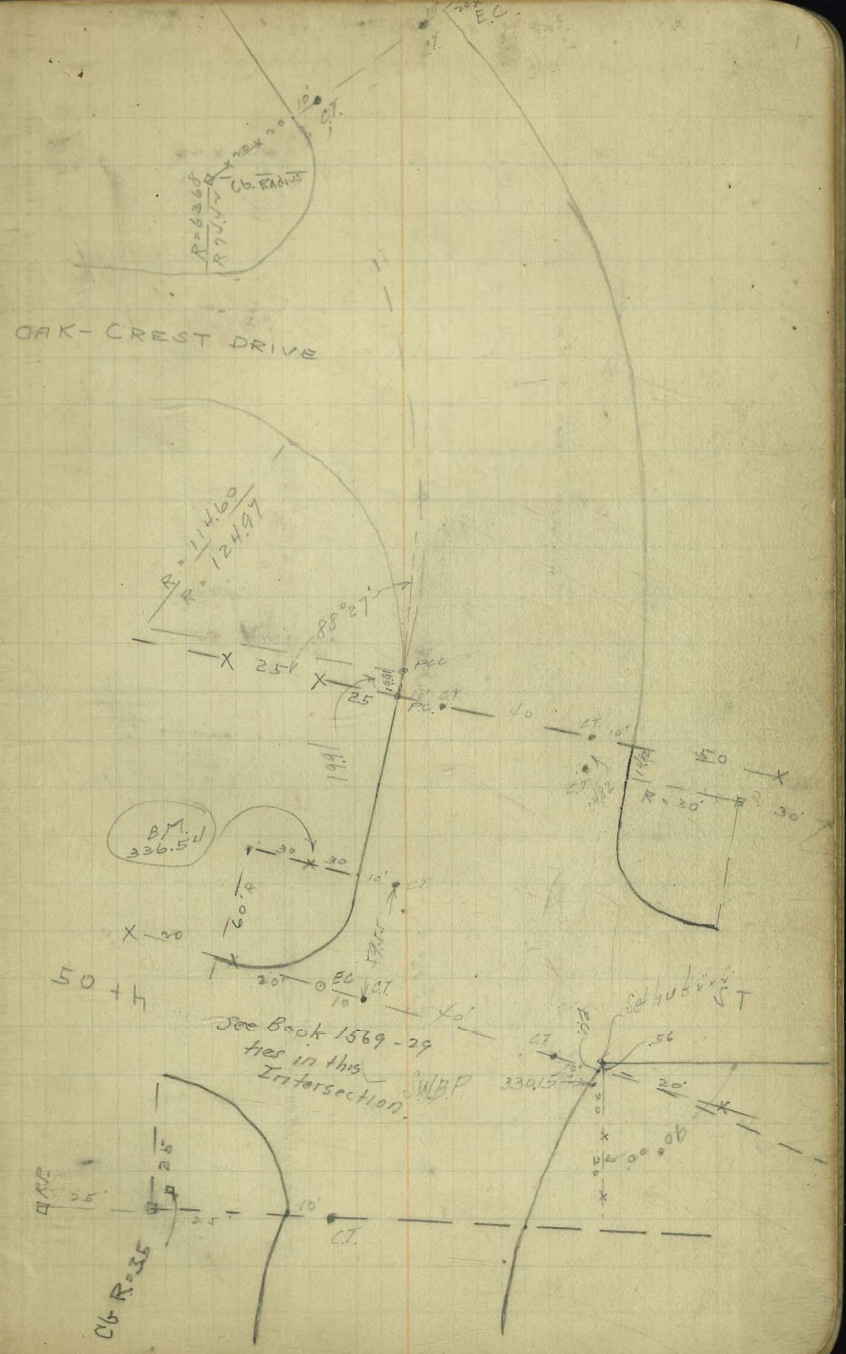
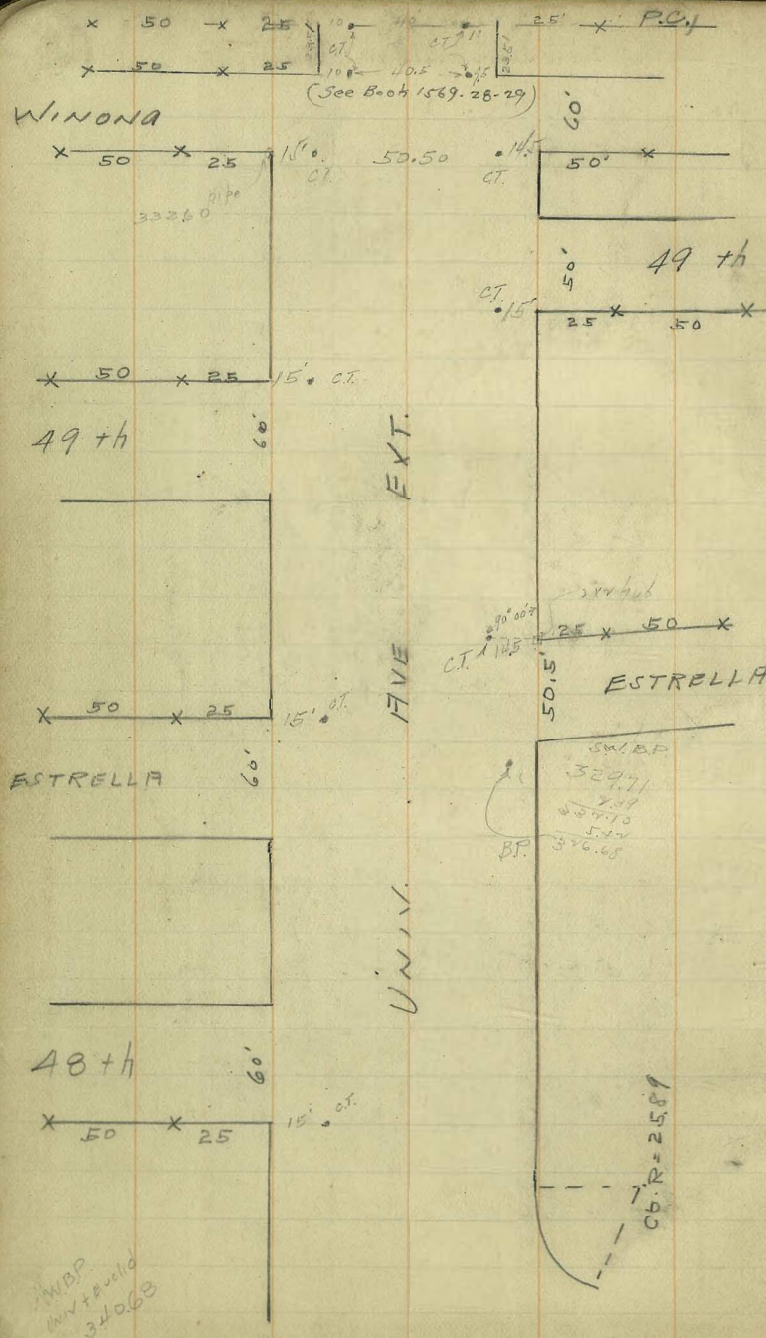
We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.
MICROFILMED

APR 8 1965

Induced
12/27/21
1926



UNIV Ave. Ties

332.03
3.21
335.44
13.24
348.68
0.51
348.17
7.1
315.57

52nd

HVB

EC

NWBP

315.57

PC x 15

98.00 40.50

CT

70.70
95

15 x 20

50' x 50' hub
51.66

51 ST

B.M. 25039
NE Cor Cem porch

This is the Rail
Used for Construction
for New Ties
See Book 1876-11

HVB

795

54th

B.M. 317.98 Spike

317.98
2.17
320.17
13.15
3100.00

STUD IN 2" iron pipe

32.30

50.00

64.69

B.P. 310.00

Cap lock

210.50
R 400

x 30

Cap lock

30' x PC

x 20

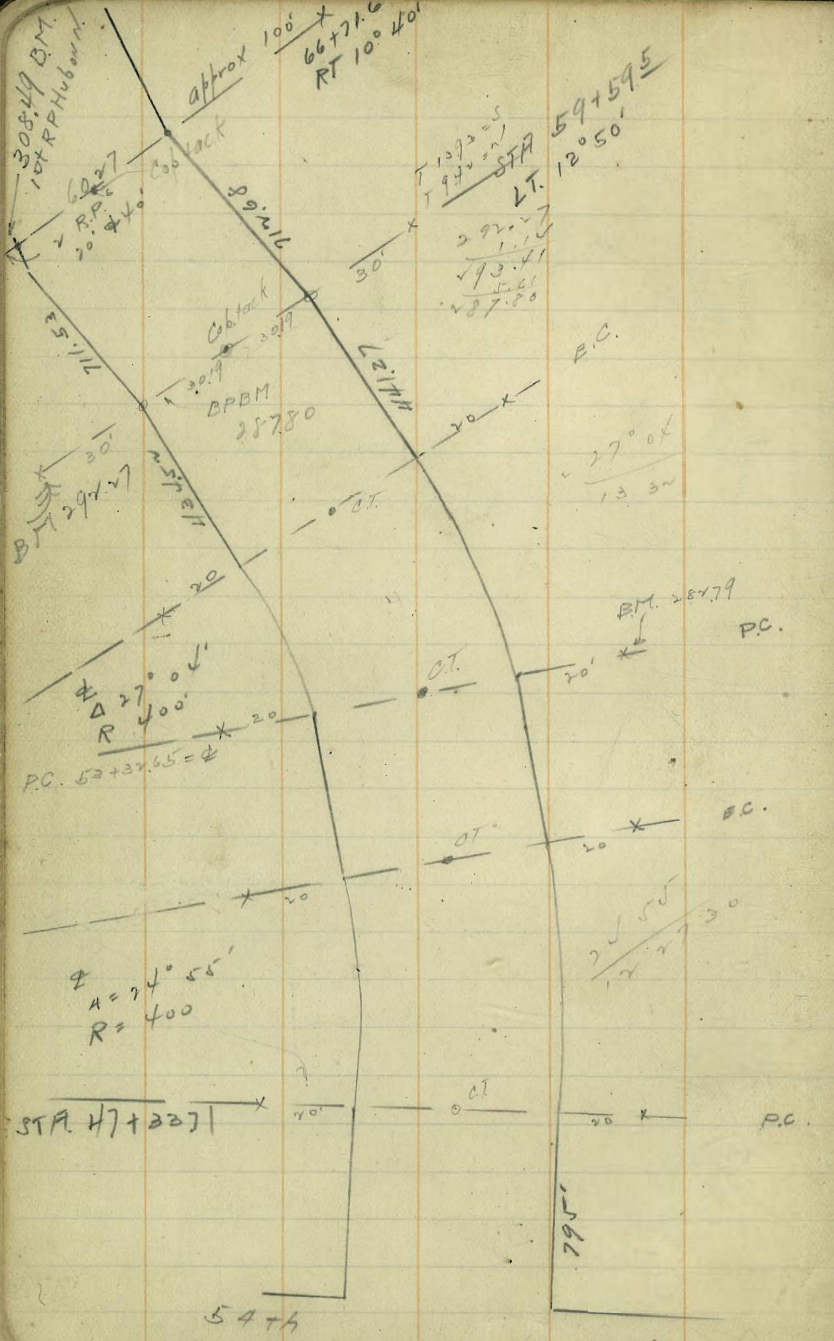
P.O.T.

40 x 35 (10.4)

CT

45 x 50

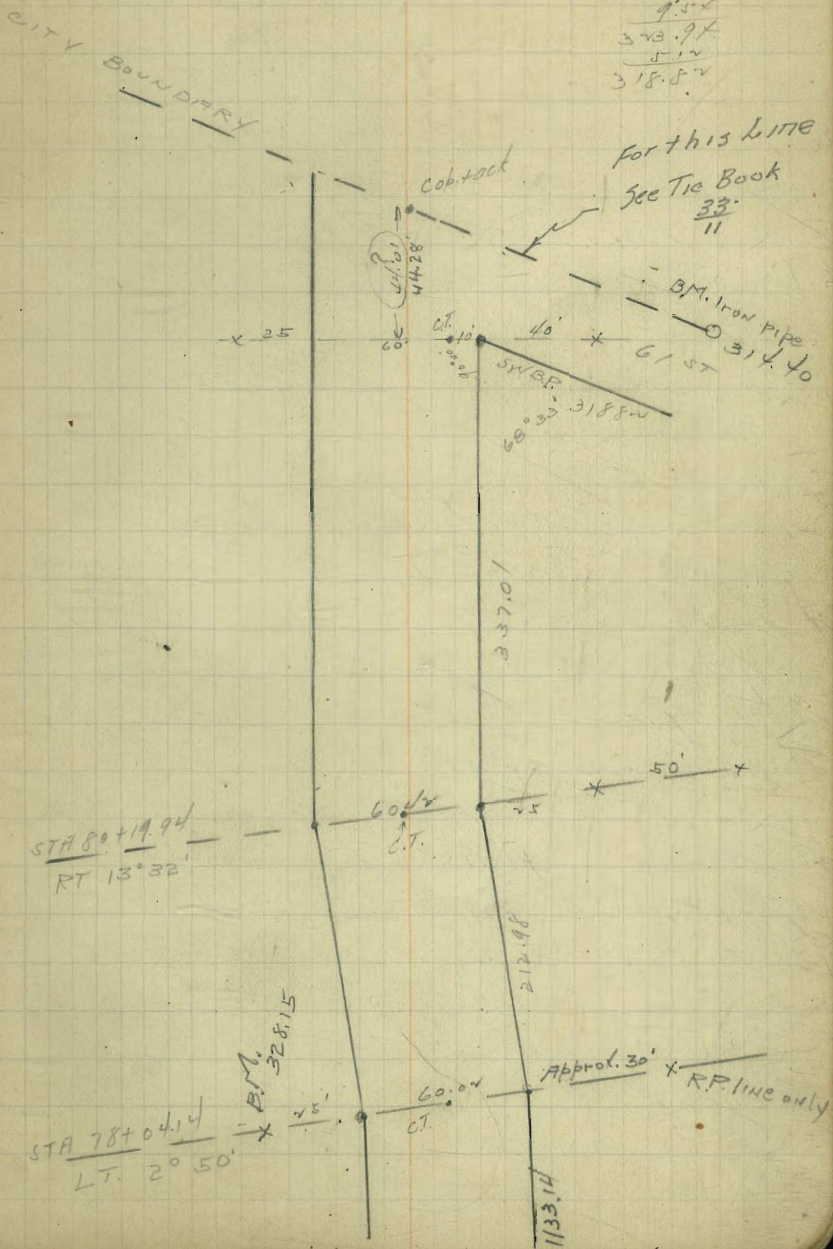
SHILOH Rd.



UNIV. AVE. TIES

31.70
4.52
373.94
5.14
318.82

For this Little
See Tie Book
33.
11



UNIV. FIVE EXT.

	N 66	506	90-509
14300 of Euclid = 0.700	342.91	342.91	PC.
0+47	343.60	343.53	
0+97	344.21	344.13	
1+47 = WL 48th	345.05	344.74	
1+07 = EL ✓ = PC. of VC.	345.95	345.50	85 qut.
1+4767	346.10	345.59	
1+4.33	345.95	345.43	
+60	345.50	345.01	
+77.67	344.80	344.35	
+95.33	343.80	343.45	
3+13 = EC of VC	342.55	342.20	85 qut.
+67.67	338.20	338.35	
4+22.33	333.85	334.40	
+77 = WL Estrella 2nd	329.50	330.45	85 qut.
5+13.54 = 1st		326.50	
+37 = EL Estrella N.L.	327.50		
+84.00 ✓ ✓ SL	323.33	324.0	87 qut
6+21.00	319.70	320.20	
6+60 = PC. of VC.	316.08	316.49	
+80	314.81	315.20	
7	313.73	314.30	
+20	312.84	313.49	
+40	312.16	312.80	
+60	311.67	312.43	
+80	311.27	312.18	87 qut

342.50					329.71	327.50	
1099					588	506 518	4
351.60					335.56		
12.00							
339.60							
0.45							
339.15	NL 43.6	42.25	44.57	45.30	46.20	45.75	
12.30		7.8	7.0	6.3	5.4	5.4	
276.14		4.2	3.4	3.0	3.0	3.0	
342.43		13.2	13.6	13.2	12.7	12.7	5.7
12.30							5.7 35
330.14							6.0
12.30	SL 43.1	43.8	44.4	45.0	45.75	45.92	
342.88		8.5	7.8	7.0	6.6	6.2	
12.30		4.5	4.2	4.0	3.7	3.3	
301.49		17.0	17.1	17.2	17.2	17.1	
12.30							
300.87	NL 42.8	38.45	39.1	39.75	40.75	40.6	20.0
12.30		8.8	13.4	17.5	19.3	18.4	15.4
300.67		5.7	5.8	5.7	5.7	5.7	5.1
0.55		12.1	12.2	12.1	12.1	12.0	12.0
300.07		3.7	3.7	3.7	3.7	3.7	3.7
11.35		15.7	15.7	15.7	15.7	15.7	15.7
311.73							
	NL 41.3	314.0	313.3	311.5			
		1.9	1.7	1.9			
		7.0	10.0	11.8			
		-8.9	-17.8	-17.5			
	SL 42.5	28.6	30.6	30.7	29.75	29.4	20.6
		9.1	13.9	17.3	18.3	17.7	6.0
		3.7	5.2	11.6	5.8	11.7	5.1
		15.7	17.9	18.3	19.5	19.0	18.9
	NL 40.6	314.0	313.3	311.5			
		1.9	1.7	1.9			
		7.0	10.0	11.8			
		-8.9	-17.8	-17.5			
	SL 42.5	28.6	30.6	30.7	29.75	29.4	20.6
		9.1	13.9	17.3	18.3	17.7	6.0
		3.7	5.2	11.6	5.8	11.7	5.1
		15.7	17.9	18.3	19.5	19.0	18.9
	NL 40.6	314.0	313.3	311.5			
		1.9	1.7	1.9			
		7.0	10.0	11.8			
		-8.9	-17.8	-17.5			
	SL 42.5	28.6	30.6	30.7	29.75	29.4	20.6
		9.1	13.9	17.3	18.3	17.7	6.0
		3.7	5.2	11.6	5.8	11.7	5.1
		15.7	17.9	18.3	19.5	19.0	18.9
	NL 40.6	314.0	313.3	311.5			
		1.9	1.7	1.9			
		7.0	10.0	11.8			
		-8.9	-17.8	-17.5			
	SL 42.5	28.6	30.6	30.7	29.75	29.4	20.6
		9.1	13.9	17.3	18.3	17.7	6.0
		3.7	5.2	11.6	5.8	11.7	5.1
		15.7	17.9	18.3	19.5	19.0	18.9
340.68							
515							
345.36							
	NL 45.95	45.50	44.90	43.80	42.55	39.50	
		4.91	3.36	4.06	5.08	6.31	7.50
329.71							
1.79		41.42	45.01	44.35	43.45	42.30	327.50
321.00		3.73	3.84	4.51	5.41	6.56	5.50
329.71							
0.66							
330.37							
12.00							
317.87							
1.44							
318.91							
		320.00	324.70	324.0	20.20	16.49	15.30
		7.00	6.30	6.37	10.8	10.4	10.6
319.28							
5.51							
313.75							
12.00							
310.73							
310.73							
		12.56	12.16	11.67	11.27		
		6.05	7.61	7.61	8.01		
		8.07	6.48				
		13.49	12.56	12.16	11.27		
		8.44	6.05	6.48	6.73		

UNIV. FIVE EXT.

	300.59 ↑	
Culvert # 1	300.64 ↑	Grade Howline
00	311.70 ↑	304.60
0 + 45	317.21 ↑	303.75
1 + 00		302.70
+ 47.5 = cb inlet		301.80
+ 48.5 = Existing 4" Conc. pipe		297.90

Culvert # 2

0 + 00 intake =	294.80	
at 29' oval catch basin	294.6	+2.6 12.0
Sand = Existing pipe	291.40	11.0
Sand + 46' 2" v-outlet	289.60	10.2

4' Cor. Iron Culvert Pipe EXTRA

20' N. of NL = intake = 0 + 00	294.6	12.0
+ 26.2 = NL	293.8	11.2
+ 90	291.53	10.3
+ 20.5 = outlet	290.6	8.8

Culvert # 3

INLET = 70' N of EXISTING Box Culvert	279.07	7.34
OUTLET = 14' S	277.6	8.18

Culvert # 4

0 + 00 = SL UNIV. Ave = A	301.55	6.65
0 + 14.25 = curb inlet	301.0	2.88
0 + 36.72 = UNIV.	300.37	0.7
+ 60 = Junction # 4A	299.0	7.86
+ 73.44 = NL UNIV.	297.0	7.21

0 + 96.7 = N end pipe (outlet)	295.75	12.45
Culvert # 4A		12.10
cb inlet = 0 + 00 top cb	306.18	3.57
v v Howline	304.0	6.20
0 + 23.6	299.86	3.87
0 + 67.2	297.71	7.23

Culvert # 5 Moved 15' West

INLET = 0 + 00	304.0	5.11
+ 16 Ncb inlet	301.58	4.76
+ 56 S v	300.51	5.53
0 + 75 outlet	300.0	4.86

Culvert # 6

inlet = 0 + 00	277.0	10.4
Ncb inlet	276.65	9.7
S v	275.71	10.75
= outlet	275.20	5.10

Culvert # 7

inlet = 0 + 00	283.50	10.1
0 + 16.7 Ncb inlet	282.45	8.8
0 + 46.3 Break	282.0	11.6
0 + 59.8 S cb inlet	281.04	9.7
0 + 81.5 outlet	279.50	14.1

Culvert # 8

0 + 00 = inlet	313.30	8.9
0 + 24.5 Ncb inlet	312.20	10.0
0 + 47.6 Break	311.0	11.2
0 + 68.7 S cb inlet	310.69	9.5
0 + 94.2 outlet	310.3	11.5

UNIV. FIVE EXT.

	NCB	S CB
9° 19' 39" (1)	331.37	330.95
10° 29' 36" (2)	331.28	330.84 ✓
11° 59' 33" (3)	331.17	330.73 ✓
13° 08' 33" (4)	331.10	330.61 ✓ 60 qut.
14° 33' 55" (5)	331.0	330.48 ✓
15° 59' 17" (6)	330.9	330.34 ✓
17° 24' 39" (7)	330.8	330.24 ✓
18° 50' 00" (8)	330.7	330.10
14+84.05 = Wh 50 ft	330.6 ✓ 75 qut.	330.10 60. qut.
14+83.49 = E.C. & C	330.54	
15+62.71 = E.C. 60'R	330.40 ✓	
+75.80 Break	330.30	
+45.8 "	329.99	
0+15.8 "	329.55	
+35.8 = P.C. 40'R	328.94 ✓ 75 qut	328.10 = P.C. 30'R
+55.24 = 370'R P.C.	328.11 ✓ P.C.	327.55
1° 25' 56" Break	327.33 ✓	326.77
2° 51' 52" "	326.31 ✓	325.87
4° 17' 48" "	325.13 ✓	324.85 ✓
5° 43' 44" "	323.83	323.72
7° 09' 40" "	322.37	322.47 ✓
8° 37' 13" "	320.96	321.00
10° 04' 46" "	319.53	319.54 ✓
11° 32' 19" "	318.15 ✓	318.07 ✓
12° 59' 52" "	316.75 ✓	316.60 ✓
14° 27' 25" "	315.35	315.13

NCB chords = 195.4
 SL chords = 218.9
 NCB = 185.4
 del. = 1° 27' 33"
 NCB = 185.4
 del. = 1° 27' 33"
 SL ch = 218.9

33974T

	NL	SL	PC	PC	PC	PC	PC	PC	PC
33974T	31.6	31.5	31.4	31.35	31.3	31.25	31.2	31.15	31.1
Sub	8.1	8.0	7.9	7.8	7.7	7.6	7.5	7.4	7.3
Total	23.5	23.5	23.5	23.5	23.5	23.5	23.5	23.5	23.5
33974T	31.4	31.1	31.0	30.8	30.7	30.6	30.5	30.4	30.3
Sub	8.1	8.0	7.9	7.8	7.7	7.6	7.5	7.4	7.3
Total	23.3	23.1	23.1	23.0	23.0	23.0	23.0	23.0	23.0
33974T	30.50	30.20	29.8	29.4	29.2	29.0	28.8	28.6	28.4
Sub	9.2	9.1	9.0	8.9	8.8	8.7	8.6	8.5	8.4
Total	21.3	21.1	20.8	20.5	20.4	20.3	20.2	20.1	20.0
33974T	24.0	23.7	23.4	23.1	22.9	22.8	22.7	22.6	22.5
Sub	7.3	7.2	7.1	7.0	6.9	6.8	6.7	6.6	6.5
Total	16.7	16.5	16.3	16.1	16.0	15.9	15.8	15.7	15.6

NL
 SL
 PC
 PC
 PC
 PC
 PC
 PC
 PC

UNIV. AVE

Angle	Chord	Notes	Station	Offset	Station
7° 19' 29"	15° 54' 58"	189.99' = chords	N 06		5 06
10° 29' 36"	17° 24' 31"	100.43	312.93		312.67
11° 59' 33"	18° 50' 04"		312.53		312.20
13° 08' 33"	20° 17' 17"		311.12		310.75
14° 33' 55"	21° 45' 10"		309.72		309.27
15° 59' 17"	23° 12' 43"		308.31		307.80
17° 24' 29"	24° 40' 20"		306.91		306.33
18° 50' 00"	26° 08' 00"	191.93 = P.C.	305.50		304.86
20° 14' 48"	27° 35' 45"	185' quarter	304.10		303.40
21° 38' 49"	29° 03' 30"		302.18		301.64
23° 02' 50"	30° 31' 15"		300.75		300.42
24° 26' 51"	32° 00' 00"		299.52		299.41
25° 51' 52"	33° 28' 45"		298.51		298.57
27° 16' 53"	34° 57' 30"		297.69		297.94
28° 41' 54"	36° 26' 15"		297.08		297.48
30° 06' 55"	37° 55' 00"		296.66		297.23
31° 31' 56"	39° 23' 45"		296.45		297.15
32° 56' 57"	40° 52' 30"	85' cut	296.45		297.27
34° 21' 58"	42° 21' 15"		296.60	22+00	297.57
35° 46' 59"	43° 50' 00"			+20	298.08
37° 11' 60"	45° 18' 45"		297.60	+40	298.76
38° 35' 1'	46° 47' 30"		298.42	+60	299.64
39° 59' 2'	48° 16' 15"		299.42	+80	300.70
41° 23' 3'	49° 45' 00"		300.62	22+00 = E.A.V.C.	301.96
42° 47' 4'	51° 13' 45"		303.11	+35.27	304.54
44° 11' 5'	52° 42' 30"		305.60	85' cut	307.13

443.9' = 4 Radius

Station	Offset	Station	Offset	Station	Offset	Station	Offset
290.37	N 06	296.45	80	296.45	80	296.45	80
327.94	N 06	297.15	80	297.15	80	297.15	80
312.93	N 06	297.15	80	297.15	80	297.15	80
312.53	N 06	297.15	80	297.15	80	297.15	80
311.12	N 06	297.15	80	297.15	80	297.15	80
309.72	N 06	297.15	80	297.15	80	297.15	80
308.31	N 06	297.15	80	297.15	80	297.15	80
306.91	N 06	297.15	80	297.15	80	297.15	80
305.50	N 06	297.15	80	297.15	80	297.15	80
304.10	N 06	297.15	80	297.15	80	297.15	80
302.18	N 06	297.15	80	297.15	80	297.15	80
300.75	N 06	297.15	80	297.15	80	297.15	80
299.52	N 06	297.15	80	297.15	80	297.15	80
298.51	N 06	297.15	80	297.15	80	297.15	80
297.69	N 06	297.15	80	297.15	80	297.15	80
297.08	N 06	297.15	80	297.15	80	297.15	80
296.66	N 06	297.15	80	297.15	80	297.15	80
296.45	N 06	297.15	80	297.15	80	297.15	80
296.45	N 06	297.15	80	297.15	80	297.15	80
296.60	N 06	297.15	80	297.15	80	297.15	80
297.60	N 06	297.15	80	297.15	80	297.15	80
298.42	N 06	297.15	80	297.15	80	297.15	80
299.42	N 06	297.15	80	297.15	80	297.15	80
300.62	N 06	297.15	80	297.15	80	297.15	80
303.11	N 06	297.15	80	297.15	80	297.15	80
305.60	N 06	297.15	80	297.15	80	297.15	80

303.47 Top of S side at P.C. 19+93.0

UNIV. AVE. EXT.

	Ncb	S cb
30+00	309.45	310.48
+50	311.10	312.10
31	312.71	313.71
+50	314.32	315.84
32	315.93	316.93
+17.43 w/2 SHILOH	316.50 60	317.50 75
+67.73 PL ✓ on SL		319.0 ✓
33+05.84 = SL 34+83.84 = NL STA 34+07.6	321.78	321.78
+50.21 = P.C.V.C.	325.03 75 qut	324.57 60 qut
+70.21	326.22	325.82
+90.21	327.43	326.88
34+10.21	328.06	327.75
+30.21	328.70	328.44
+50.21	329.16	328.92
+70.21	329.44	329.22
+90.21	329.53	329.33
35+10.21 = P.O.T.	329.45	329.25
+30.21	329.18	328.98
+50.21	328.72	328.51
+70.21	328.09	327.85
+90.21	327.28	327.01
36+10.21	326.28	325.96
SL STA = +14.63 = P.C.	326.01	325.68
36+30.21 EC.V.C.	325.10 75 qut	324.74 60 qut
⊙	324.04	323.81
⊙	322.98	322.89

9 points

316.64										
316.64										
329.75	NL	309.7	11.30	313.0	14.6	16.2	16.8	271.0	25.3	
329.45		6.7	5.3	3.6	2.8	0.4	12.7	8.7	4.4	
311.32		7.9	8.0	3.8	2.4	0.3	12.3	8.3	3.1	
311.32		-0.4	-2.7	-1.3	-0.4	-0.1	+0.6	+0.2	+0.5	
311.32										
311.32	SL	10.7	12.3	314.00	15.6	17.2	17.8	19.2	20.0	20.8
311.32		5.1	4.3	2.6	14.45	12.6	11.9	10.5	7.5	7.7
311.32		2.5	3.9	0.2	1.1	1.2	1.0	0.7	0.5	0.4
311.32		-1.6	+0.4	+2.2	+1.4	+1.4	+1.5	+3.1	+5.2	+6.6
311.32										
311.32	NL	326.5	274	283	290	294	297	298	297	
311.32		3.2	2.3	13.0	12.3	11.7	11.6	11.5	11.5	11.5
311.32		1.4	2.1	11.3	8.7	7.7	6.7	5.8	5.2	5.2
311.32		+0.3	+1.2	+1.7	+2.0	+2.7	+2.7	+6.0	+5.8	+5.8
311.32										
311.32	SL	26.5	27.1	28.0	28.7	29.5	29.6	29.8	29.8	
311.32		7.2	4.1	13.3	12.6	12.1	11.7	11.5	11.5	11.5
311.32		6.9	3.7	12.6	11.1	10.7	10.6	10.4	10.4	10.4
311.32		+0.3	+10.1	+10.6	+10.0	+10.0	+10.1	+10.3	+11.6	
311.32										
311.32	NL	329.4	328.9	328.3	327.5	326.5	325.3	324.3	323.2	
311.32		12.9	13.0	14.0	4.6	5.8	6.8	7.8	8.7	
311.32		8.3	10.2	12.3	4.1	5.3	6.3	7.0	7.9	
311.32		+4.6	+3.2	+1.8	+0.5	-0.3	-0.5	-1.1	-1.0	
311.32										
311.32	SL	329.2	328.8	328.1	327.3	326.2	325.0	324.1	323.1	
311.32		13.1	12.5	14.2	15.0	16.1	17.1	18.1	19.0	
311.32		8.7	10.2	12.3	14.1	16.1	17.1	18.1	19.0	
311.32		+12.4	+11.8	+9.4	+6.9	+5.0	+4.5	+3.5	+3.5	

deflections
 ECVC = 1° 10' 30"
 2° 15' 53"
 3° 21' 16"
 4° 26' 29"
 5° 31' 04"
 6° 37' 25"
 7° 42' 43"
 8° 48' 11"
 9° 53' 34"
 10° 59' 00" = EC

chord = SL NL
 15.17 17.63 = ECVC

Balance ✓ = 14.06 16.26

Univ. Ave. Ext.

S.L. Station	N. Ista	N. cl	S. cl
47+22.05	47+45.33	286.75 = PC	287.28
①	1°14'45"	286.57	287.10
②	2°29'36"	286.39	286.91
③	3°44'15"	286.21	286.73
④	4°59'00"	286.02	286.54
⑤	6°13'45"	285.84	286.36
⑥	7°28'30"	285.66	286.17
⑦	8°43'15"	285.48	285.99
⑧	9°58'00"	285.29	285.80
⑨	11°12'45"	285.11	285.62
49+09.09	12°27'30"	284.93 = EC	285.43 = EC
49+50	49+47.15	284.47	285.03
50+00	+97.15	283.91	284.53
51+50	50+47.15	283.34	284.04
51+00	50+97.15	282.78	283.54
5450	51+47.15	282.22	283.05
52+00	51+97.15	281.64	282.55
52+55	52+52.15	281.0	282.00 = Bk. 1/6
	+91.68	281.40	282.33
53+34.07	53+31.27	281.79	282.67
	① 1°21'12"	281.96	282.84
	② 2°42'24"	282.14	283.01
	③ 4°03'36"	282.31	283.18
	④ 5°24'48"	282.48	283.35
	⑤ 6°46'00"	282.64	283.52

10 hrs 15
 defl. 10 11 12
 S.L. 20.3
 N.L. 17.45 chords

286.60 = BM RP - Sta 47+45.33

4.84 +
 291.44
 8.65

287.79

S	287.5	287.5	287.6	287.0	286.80	286.60	286.4	286.24	286.05	285.9
	3.9	4.1	4.3	4.4	4.6	4.8	5.0	5.2	5.4	5.5
	-1.2	-2.3	-3.3	-4.8	-7.5	-9.6	-12.0	-14.4	-17.5	-20.7

286.60
 2.56
 291.16

N

287.0	286.82	286.7	286.46	286.27	286.10	285.9	285.73	285.54	285.36
4.4	4.6	4.7	5.1	5.3	5.5	5.7	5.9	6.1	6.2
3.4	4.2	5.0	6.2	7.7	9.2	10.7	12.2	13.7	15.1

= EC

S	285.7	285.3	284.8	284.3	283.8	283.3	282.8	282.4	282.0
	3.7	3.9	4.1	4.4	4.7	5.0	5.3	5.6	5.9
	-5.3	-10.0	-14.4	-18.8	-23.1	-27.4	-31.7	-36.0	-40.3

N

285.2	284.7	284.1	283.6	283.0	282.5	281.9	281.4	280.8
6.2	6.5	7.1	7.6	8.2	8.7	9.3	10.0	10.5
+0.7	+0.8	+1.1	+1.5	+1.1	+0.7	+0.1	-0.4	-1.0

S

284.6	284.9	285.1	285.3	285.4	285.6	285.8	286.0	286.2
8.6	8.3	8.1	7.9	7.8	7.6	7.4	7.2	7.0
+1.0	+0.9	+0.8	+0.7	+0.6	+0.5	+0.4	+0.3	+0.2

N

281.4	282.0	282.4	282.8	283.2	283.6	284.0	284.4	284.8
9.6	9.4	9.0	8.8	8.7	8.5	8.3	8.1	7.9
+4.6	+5.2	+5.8	+6.4	+7.0	+7.6	+8.2	+8.8	+9.4

287.79
 5.61
 291.43

N

287.0	286.75	286.52
4.3	4.6	4.9

S

287.50	287.25	287.03
3.93	4.15	4.38

287.79
 3.94
 286.71

17.76 = 1/1
 200 = 5 } = 4' from c/b

UNIV. AVE. EX.

29116

SL STA	NL STA	N CB	S CB
6	8° 07' 17"	282.83	283.70
7	9° 28' 24"	283.00	283.87
8	10° 49' 36"	283.18	284.05
9	12° 10' 48"	283.35	284.21
10	13° 37' 00"	283.53	284.39
55+50	55+50	283.93	284.77
56		284.43	285.20
+50		284.93	285.62
57		285.43	286.03
+55		285.93	286.48
58		286.43	286.91
+50		286.92	287.34
59		287.41	287.78
59+47.8 = Δ 59+40.53		287.80	288.70
60+00		288.40	288.651
+50		288.91	289.08
61		289.43	289.51
+54.99 = BREAK		290.0	290.0
62		290.74	290.46
+50		291.56	291.27
63		292.38	292.09
+50		293.21	292.91
64		294.04	293.731
+50		294.86	294.56
65		295.69	295.37

25.479 10.33 14.147 7.18 288.79	S	83.9 7.3 8.8 -1.5	84.1 7.1 8.0 -0.9	84.3 6.9 8.2 -1.3	84.4 6.5 8.2 -1.4	84.6 6.6 8.2 -1.7	85.0 8.0 9.6 -1.6	85.4 7.6 8.8 -1.2
27.547 1.14 11.6 205.95	N	82.1 9.1 4.6 +4.5	83.2 8.0 4.1 +3.9	83.4 7.8 4.4 +3.4	83.6 7.6 3.7 +3.9	83.8 7.4 3.8 +3.9	84.2 8.8 3.5 +3.3	84.7 8.3 3.6 +5.7
	S	85.8 7.2 8.3 -1.1	86.3 6.7 7.0 -0.3	86.7 6.3 4.5 +1.8	87.2 5.8 6.3 -0.5	87.6 5.4 7.0 -1.6	88.0 8.1 9.1 -4.1	88.4 4.6 10.6 -6.0
	N	85.2 7.8 1.2 +6.8	85.7 7.3 1.2 +2.1	86.2 6.8 1.1 +5.7	86.7 6.3 6.3 0.0	87.2 5.8 5.8 -3.0	87.6 5.4 7.1 +1.6	88.0 8.0 8.5 +3.5
	S	89.0 6.2 10.8 -4.6	89.7 5.8 9.9 -5.1	90.2 4.8 1.9 -7.6	90.7 4.0 1.9 -5.1	91.5 4.0 12.5 -9.3	92.3 3.2 12.5 -11.5	93.2 2.3 13.3 -11.8
	N	89.1 6.4 3.0 +2.8	89.6 5.9 3.0 +2.9	90.2 5.3 2.2 +3.1	91.0 4.5 1.5 +2.7	91.8 3.7 3.3 +1.4	92.6 2.9 2.3 +0.6	93.4 2.0 0.8 +1.2
	S	94.8 0.7 11.5 -10.8	95.6 0.0 6.5 -6.5					
	N	95.1 10.5 10.9 +2.9	95.9 10.0 4.6 +5.4					

6.59 ut 7.59 ut

7.0 ut 7.09 ut

Univ. Five EV.

305.95

14

	N. 06	S. 06
65+50	296.51	296.38
66	297.35	297.10
+52.06 Δ 10°40' RT.	298.85 ✓	297.95 ✓
67	299.11	298.73
+50	299.94	299.55
68	300.76	300.35
+50	301.59	301.16
69	302.41	301.97
+50	303.24	302.78
70	304.06	303.59
+50	304.89	304.39
71	305.71	305.20
+50	306.53	306.00
72	307.36	306.81
+50	308.18	307.62
73	309.01	308.42
+50	309.83	309.23
74	310.66	310.04
+50	311.48	310.85
75	312.31	311.65
+50	313.13	312.45
76	313.95	313.26
+50	314.75	314.07
77	315.56	314.88
+50	316.37	315.67

308.49 0.27 308.96	N	96.7	97.6	98.5	99.3	300.2	301.0	301.8	
0.33 308.63		9.4	8.3	7.4	9.6	8.7	7.9	7.1	
8.88 317.51		+6.9	+7.5	+7.1	+5.3	+5.5	+2.2	+1.5	
2.88 314.63	S	96.5	97.3	98.2	99.0	99.8	300.6	301.4	
12.4 327.09		9.4	8.6	7.7	9.9	9.1	8.3	7.5	
		14.4	13.8	12.8	15.5	14.6	14.1	14.4	
		-8.0	-5.2	-5.1	-5.6	-5.0	-5.8	-6.9	
	N	302.6	303.5	304.3	305.1	305.9	306.8	307.6	
		6.3	5.4	4.6	12.4	11.6	10.7	9.9	
		5.4	1.2	2.0	7.5	6.1	4.7	3.9	
		+0.8	+1.2	+3.6	+4.9	+5.5	+6.0	+6.8	
	S	302.2	303.0	303.8	304.6	305.4	306.2	307.0	
		6.7	5.9	5.1	4.3	3.5	2.7	1.9	
		13.3	13.1	11.7	10.0	8.1	5.6	5.0	
		-7.6	-7.2	-6.6	-5.7	-4.6	-2.9	-3.1	
	N	308.4	09.3	10.3	10.9	11.7	12.5	13.4	14.2
		9.1	8.4	7.2	6.6	5.8	5.0	4.1	3.3
		1.9	1.4	2.1	3.1	3.1	2.9	2.0	1.2
		+7.2	+6.8	+5.1	+4.5	+2.7	+2.1	+2.1	+2.1
	S	07.9	08.6	09.5	10.3	11.1	11.9	12.7	13.5
		1.0	0.3	8.0	7.2	6.4	5.6	4.8	4.0
		4.9	3.7	12.3	16.5	16.0	14.1	11.2	8.1
		-3.8	-3.4	-2.3	-9.3	-9.6	-8.5	-6.4	-4.1
	N	315.0	15.8	16.8					
		12.1	11.3	10.3					
		6.1	4.7	3.6					
		+4.0	+0.6	+7.7					
	S	14.3	15.1	15.9					
		3.2	14.0	11.7					
		5.5	12.5	11.0					
		-2.3	-0.5	2.0					

UNIV FIVE F

Scb

Scb

77+86.66 = Δ 2° 50' LT 316.92

316.23

78+00

317.95

317.23

+50

79

318.75

318.02

+50

319.56

318.82

80+08.54 = Δ 13° 31' RT 320.52

319.48

+50

321.25

320.84

81+11.4 = BREAK

322.30

321.30

+50

321.94

320.90

82

321.44

320.36

+50

320.95

319.82

83

320.45

319.29

+49.4

319.95

318.75

Cityline

319.40

318.40

759 ft

318.88 = φ

659 ft

327.09

1.42

325.17

3.98

329.15

1.00

328.15

1.99

330.14

12.2

317.92

7.25

325.18

16.28

314.40

N

317.4

18.2

19.0

19.8

20.8

21.5

22.5

9.9

11.9

11.1

10.3

9.3

8.6

7.6

4.9

5.3

4.4

4.9

3.6

3.0

3.5

+8.0

+6.1

+6.2

+5.4

+4.7

+5.0

+4.1

S

16.5

17.5

18.2

19.1

19.9

20.8

21.5

11.6

12.6

11.8

11.0

5.3

4.6

3.7

19.6

18.1

18.2

18.1

7.3

7.4

6.9

+0.0

-0.5

-1.1

-1.1

-2.0

-2.5

-5.2

N

22.2

21.7

21.2

20.7

20.2

19.6

318.88

7.9

8.4

4.0

4.5

5.0

5.6

6.30

2.2

2.0

7.5

9.8

4.6

0.9

6.20

+5.7

+6.4

+3.5

-5.2

+6.4

+4.7

0.10

S

21.1

20.6

20.1

19.5

19.0

18.6

Low

4.1

4.6

5.1

5.7

6.4

6.6

padding

8.3

7.7

7.2

14.4

9.2

9.3

-

-7.7

-3.1

-2.6

-8.7

-3.0

-4.7

-

11/16/66 Moore
 ST PAVING 15th to 16th

10906 SW 7' tack
 223 FI + 16th
 11179

15th paving elev = 97.5 ✓
 starting C.B. to be raised PAVED
 97.4 97.3 97.2 97.1 97.0 96.9 96.8 96.7

98.20 97.7 99.0 99.7 BREAK
 98.86 98.6 99.86 100.66 BREAK
 100.50 99.90 101.65 102.45 BREAK

16th paved ST
 10906
 10907
 10908
 10909
 10910
 10911
 10912
 10913
 10914
 10915
 10916
 10917
 10918
 10919
 10920

97.50
 6.23
 103.73 π
 5-96
 -72
 34
 5+6
 48.77



Alley Paving

BIR 176 S.D. & 47 Co. Add.

EL Dewey	51.85	52.15
	51.70	52.00
+ 43.33	52.26	52.56
+ 86.67	52.83	53.13
1 + 30 BREAK	53.10	53.70
+ 74	55.52	55.62
8 + 15	57.24	57.54
+ 62	59.16	59.46
3 + 06	61.08	61.38
+ 50 BREAK	63.0	63.30
+ 70 "	63.70	64.0
+ 90 "	64.10	64.40
4 + 40	64.53	64.83
+ 90	64.97	65.27
5 + 40 BREAK	65.70	65.70
+ 70	66.15	66.45
6 + 00 W. EVANS	66.90	67.20

Dewey to Evans
Logan to Kearney

630 N NW Logan & Evans

630 N						
SW						
71.23						
64.26	N	67.20	66.45	65.70	65.27	64.83
3.28		4.03	4.78	5.53	5.96	6.40
67.34		3.23	3.78	4.53	5.96	6.40
11.60		41.0	41.0	41.0	41.0	41.0
55.72	S	66.90	66.15	65.40	64.97	64.53
2.28		7.03	5.88	5.83	6.26	6.70
58.00		0.0	2.08	0.0	7.17	5.70
			41.0	0.0	-0.91	41.0
	N	64.0	63.30	61.98	59.46	57.52
		3.24	4.04	5.96	7.88	9.50
		2.34	3.04	4.96	6.88	8.50
		41.0	41.0	41.0	41.0	41.0
	S	63.70	63.0	61.08	59.16	57.24
		3.64	4.04	6.26	8.18	10.10
		4.23	3.24	5.50	7.75	8.90
		-0.59	41.0	40.46	40.73	41.0
	N	53.70	53.13	52.56	52.10	51.70
		4.30	4.87	5.44	6.00	6.30
		3.30	3.87	4.44	5.00	5.30
		41.0	41.0	42.0	42.0	42.0
	S	53.40	52.83	52.26	51.70	51.20
		4.60	5.17	5.74	6.30	6.30
		3.60	4.87	5.44	6.00	6.30
		41.0	40.80	40.73		

sub cuts

32nd ST

baved

Thorn

paving

305.27		304.44
307.10	40	301.50

7580	645	746.10
265	427	390
1.85	257	210
0.32	126	0.78
948	100	935
861	918	915
8246	857	85.46
8736	846	8836
840	942	890

120

PEVE

5' breaks

Cb inlet

Cb inlet

ECVC

Cb inlet 394.70 432.5 431 431 433 434 395.0

(31) (32) (30)

shallow

425.17 460

470 510 (304)
 480 510 (311)
 485 515 (321)

Redwood

Cb inlet 394.70 432.5 431 431 433 434 395.0

shallow

470 510 (304)
 480 510 (311)
 485 515 (321)

32nd ST

18

Quince

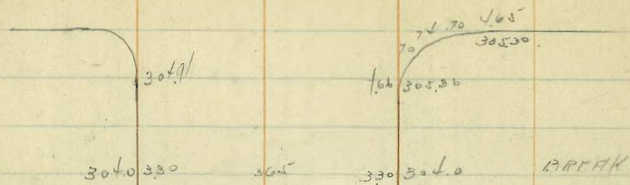
397.99
 395.08 16.16
 5.40
 8.63 8.50
 8.77
 398.83 67
 398.80

307.95 120 787 315 328 and 302.0
 260 275 280 290 120 2900

370 370
 380 330 350
 390 360
 370 37
 380 397 394 392 390

Pd/M

FELTON ST



Break 30050

TERESITA

97.57 6.97

7.25 9.00 Break

91.8 0.55
90.30 9.65
89.03 8.40

1.70 9.25
0.48 9.25 V.C.
9.08 9.00

276.38 7.57
Cb in 12'

6.40 277.45

Nutmeg

Felton + Upas + + -

	WL	EL
353.57 No of 1/1000 = PC = 0.000	322.25	322.25
① 2° 36' 20" = do fl.	321.75	
② $\pi = 255.9$	221.25	
③	320.75	
1407.6 (4) = PPC	320.25	320.25
① ^{EL} 2° 53' 26" = do fl.	319.55	318.25
② 1987 = ch	318.85	316.25
③	318.15	314.25
④ EL on E = Slupas	317.25	EL 312.25
⑤ EL on West Slupas	316.75	EL Felton on = 311.47
	317.25	
= PC on 330 = Slupas	317.75	

318.65
5.29
313.74

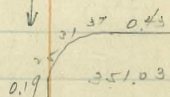
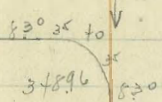
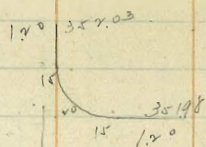
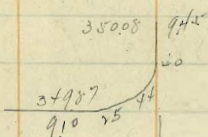
20 21

W	224.2	21.7	21.2	20.7	20.2	19.5	18.8
	1.5	2.0	2.5	3.0	3.5	4.2	5.0
			2.3	2.6	3.2	3.8	4.2
			+0.2	+0.4	+0.3	+0.4	+0.8
E	1.5	2.0	2.5	3.0	3.5	18.2	16.2
	1.9	1.9	2.1	2.5	3.3	5.5	7.5
	-0.1	+0.1	+0.4	10.5	+0.2	4.2	5.7
						47.3	47.8
W	18.1	17.4	16.7	17.2	17.7		
	5.6	6.3	7.0	6.5	6.0		
	4.6	4.7	4.9	4.9			
	+7.0	+1.6	+2.1	+1.6			
E	17.2	17.2	11.4				
	9.5	11.5	14.3				
	6.5	4.9	11.7				
	+2.7	+1.6	+0.6				

Oregon ST.

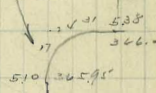
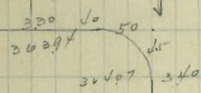
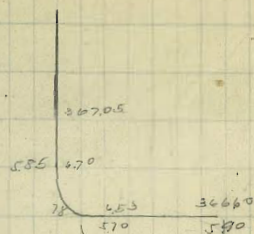
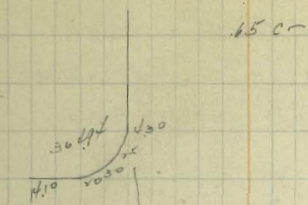
Oregon ST.

21



Lincoln

PAIK



8 cr.

8 cr.

336.0570

325 32910 Break

361.11 0.18

310.3696 BRECK

BRK →
156

Howard

374.10 345
374.05
345

35.5 374.26

334.40

327.16

374.5 32
374.00 32.5

300 373.76

UNIV. Ave

slight BRK

Filley Paving
 BIK 25 Park Villas

15' wide

	W	E
SL Myrtle - paving	328.23 ✓	328.01 ✓
50' S	328.50	328.30
70' S	328.46	328.06
120' S	328.02	327.82
170' S	327.78	327.58
220' S	327.54	327.34
270' S = BREAK	327.30	327.10
300 = NEUPAS - paving	326.15	325.82

NEUPAS - paving 326.15 325.82

327.90
 327.20
 327.02
 326.46
 326.97
 327.85

327.90

	W	E
25.50	25.26	25.02
4.33	4.57	4.81
4.03	4.37	3.26
0.0	+0.20	+1.05
27.85	27.55	27.34
5.05	5.45	5.73
3.25	3.19	2.32
21.50	22.12	22.01
+1.67	+1.67	+1.67

INGRAHAM Grading

See Pac. Beach Tie Pt. Book for ties page 24

	W CB	E CB
NL Grand	57.0	56.0
54' ✓	57.60	56.80
408'	58.20	57.60
1 + 6 ✓	58.80	58.40
2 + 16	59.40	59.20
✓ + 70 = SL Hornblende	60.0	60.0
0 + 100 NL ✓	60.46	60.46
0 + 54	60.81	60.86
1 + 08	61.16	61.26
1 + 6 ✓	61.51	61.66
2 + 16	61.86	62.06
2 + 70 = SL Garnet	62.21	62.46
0 + 100 = NL ✓	63.28	63.25
754	64.00	64.00
1 + 08	64.74	64.75
1 + 6 ✓	65.49	65.50
✓ + 16	66.23	66.25
✓ + 70 = SL Feldspar	67.0	67.0
0 + 100 = NL ✓	68.0	68.0
0 + 54	69.2	69.7
1 + 08	70.4	70.8
1 + 6 ✓	71.6	72.2
2 + 16	72.8	73.6
2 + 70 = SL Emerald	74.0	75.0

55% NEEP Grand + Ingraham

12.00

65.00

5.00

62.60 = SEBP Garnet + Ingraham

4.76

74.36

3.07

70.29

12.56

82.85 x

WL	64.2	65.0	65.7	66.5	67.2	68.0	69.4
	5.2	7.4	6.7	5.9	5.2	4.2	3.0
	9.2	7.9	6.5	5.1	4.0	1.8	2.0
	-7.0	-0.5	+0.2	+0.5	+1.2	+2.4	+1.8
EL	8.2	7.4	6.7	5.9	5.2	4.2	69.6
	9.1	8.5	7.1	6.1	5.2	4.9	2.8
	-0.9	-1.1	-0.4	-0.4	0.0	+1.3	+0.2
WL	70.6	71.8	73.0	74.2	75.4	76.6	77.8
	12.3	11.1	9.9	8.7	7.5	6.3	5.1
	11.2	10.7	9.6	8.5	7.4	6.3	5.2
	+1.1	+0.4	+0.3	+0.2	+0.2	+1.0	+1.6
EL	71.0	72.4	73.8	75.2	76.6	78.0	79.4
	11.9	10.5	9.1	7.7	6.3	4.9	3.5
	11.8	10.0	8.5	7.3	6.0	4.8	3.5
	+0.2	+0.5	+0.3	+0.2	+0.1	+0.6	+1.7
WL	60.7	60.2	59.6	59.0	58.4	57.8	57.2
	7.6	8.1	8.7	9.3	9.9	10.5	11.1
	4.9	4.9	5.2	5.6	6.0	6.4	6.8
	+2.7	+2.2	+3.5	+2.7	+3.0	+2.4	+0.5
EL	60.7	60.2	59.6	59.0	58.4	57.8	57.2
	7.6	8.1	8.7	9.3	9.9	10.5	11.1
	3.8	4.3	4.7	5.0	5.4	5.8	6.2
	+3.8	+4.8	+4.2	+1.7	+1.5	+1.1	

INGRAHAM Grading

	N/C6	E/C6
NL Emerald	75.0	76.0
0+5 ✓	76.1	77.4
1+08	77.8	78.8
1+6 ✓	79.2	80.2
2+16	80.6	81.6
✓ +70 = SL Diamond	82.0	83.0

82.85
2.00
80.16
5.61
85.77

	WL	EL	NL	SL
	75.2 7.7 7.5 +0.2	76.6 6.3 6.4 -0.1	78.0 4.9 5.3 -0.4	79.40 3.5 3.7 -0.2
	76.2 6.7 5.4 +1.3	77.6 5.3 3.9 +1.4	79.0 3.9 3.9 +1.0	80.40 2.5 1.7 +0.8
	62.5 5.8 1.9 +3.7	64.4 3.9 0.9 +3.0	66.2 2.2 1.9 2.8	
	61.9 6.4 0.7 +1.7	63.6 4.7 3.8 +0.9	65.2 3.1 2.7 +0.4	

24

HORNBIEND Regrading

	N/C6	S/C6
New EL Ingraham 2010	60.46	60.0
0+61.67	62.30	61.67 ✓
1+23.33	64.15	63.33
1+85	66.0	65.0

INGRAM Sewer

Sewer #	Description	Grade	Calcs	Final
Sewer #1	plug = 0+00	73.8	52.85 X 8.93 2.51 +6.42	73.8
0+42.5	MH #1	73.58	9.27 3.72 +5.55	73.58
0+56.25		72.6	10.24 4.74 +5.50	72.6
1+30	Sewer #2	71.65	11.20 5.91 +5.29	71.65
1+73.5		70.69	12.16 6.31 +5.85	70.69
7+17.5	MH #2	69.73	13.12 7.40 +5.72	69.73
7+61.25		68.76	14.08 8.60 +5.48	68.76
3+05		67.80	15.05 9.88 +5.17	67.80
3+48.75		66.84	16.01 11.23 +4.78	66.84
3+92.5	MH #3	65.88	16.97 12.65 +4.32	65.88
67.5 E = EL (plug)		66.32	17.93 14.13 +3.80	66.32
37.5 W = WL (plug)		65.62	18.93 15.53 +3.40	65.62
Sewer #4				
MH #4		58.94	72.36 X 14.42 8.16 +6.26	58.94
67.5 E = EL Ingraham		59.38	12.88 6.72 +6.16	59.38
37.5 W = WL		58.79	13.57 7.22 +6.35	58.79
Sewer #5				
MH #5		56.64	116.1 67.4 +48.7	56.64
67.5 E = EL Ingraham		56.39	118.6 49.7 +68.9	56.39
37.5 W = WL		56.90	113.5 67.8 +45.7	56.90
Sewer #6				
MH #6		45.02	55.87 10.65 +5.66	45.02
67.5 E = EL Ingraham		44.77	13.62 7.50 +6.12	44.77
37.5 W = WL		45.77	17.84 9.53 +8.31	45.77
31.75 E of MH		44.89	13.77 7.41 +6.48	44.89

Sewer #	Description	Grade	Calcs	Final
Sewer #7	Grade	38.07		
31.75 E of MH		41.26	51.79 X 10.53 3.66 +6.87	41.26
67.5 E = EL		38.20	13.59 5.25 +8.34	38.20
D.M.H. #7 = 0+00	#8 Sewer	41.00	10.79 4.25 +6.54	41.00
0+00 = Drop in MH #7		37.95	13.84 4.85 +8.99	37.95
0+43.75		37.77	14.02 6.00 +8.02	37.77
0+57.50		37.60	14.19 6.76 +7.43	37.60
1+31.25		37.42	14.37 7.25 +7.12	37.42
1+75 = M.H. #8		37.25	14.54 7.80 +6.74	37.25
2+18.75		37.08	14.71 8.31 +6.40	37.08
2+62.50		36.91	14.88 8.85 +6.03	36.91
3+06.25		36.73	15.06 9.47 +5.59	36.73
3+50 = M.H. #9		36.56	15.24 10.11 +5.13	36.56
Sewer #9				
67.5 E = EL Ingraham		38.00	14.48 5.14 +9.34	38.00
37.5 W = WL		36.41	14.66 5.89 +8.77	36.41
M.H. #9		36.56	14.84 6.72 +8.12	36.56
31.75 E		37.45	15.02 7.60 +7.42	37.45
Sewer #10				
67.5 E = EL Ingraham		41.19	10.81 4.05 +6.76	41.19
37.5 W = WL		40.79	11.11 4.57 +6.54	40.79
M.H. #10		40.94	11.06 4.47 +6.59	40.94
31.75 E		41.06	11.35 4.65 +6.70	41.06

11.00
5.0625
+5.9

52.00 X

- 55.54
- 55.66
- 55.84
- 56.04
- 56.24
- 56.44
- 56.64
- 56.84
- 57.04
- 57.24
- 57.44
- 57.64
- 57.84
- 58.04
- 58.24
- 58.44
- 58.64
- 58.84
- 59.04
- 59.24

Ingraham Grading

	W CB	E CB		
SL Grand	55.0	54.0		
54's	54.0	53.0		
108	53.0	52.0		
16v	52.0	51.0		
216	51.0	50.0		
270 = NL Thomas 80' wide	50.0	49.0		
0+00 SL ✓	49.0	48.0		
54's	48.10	47.10		
108	47.20	46.20		
16v	46.30	45.30		
216	45.40	44.40		
270 = NL Reed 80' wide	44.50	43.50	45.0	
0+00 SL ✓	44.50	43.50	44.65	
54's	45.20	44.40		
108	45.90	45.30		
16v	46.60	46.20		
216	47.30	47.10		
270 = NL Oliver 80' wide	48.0	48.0		
00 = SL ✓	48.0	48.0		
50's	47.70			
100	47.40			
150	47.10			
200	46.80			
250 = NL Pacific	46.50	46.50		

5/28 4/2 part

5585

211

57.96

5.33

52.63

1.70

54.33

5.91

48.42

4.55

54.97

7.52

47.45

5.26

52.19

4.7

47.49

4.2

43.29

3.4

40.89

4.2

36.69

3.8

32.89

3.0

29.89

2.2

27.69

1.6

26.09

1.0

25.09

0.4

24.69

0.0

24.69

0.4

24.29

0.0

24.29

0.4

23.89

0.0

23.89

0.4

23.49

0.0

23.49

0.4

23.09

0.0

23.09

0.4

22.69

0.0

22.69

0.4

22.29

0.0

22.29

0.4

21.89

0.0

21.89

0.4

21.49

0.0

21.49

0.4

21.09

0.0

21.09

0.4

WL	55.0	54.0	53.0	52.0	51.0	50.0	49.0
	2.7	3.7	4.7	5.7	6.7	7.7	8.7
	2.8	1.3	3.0	5.3	6.6	8.1	9.7
	10.9	+2.4	3.7	+1.9	+1.7	+1.9	+1.4
FL	54.00	53.0	52.0	51.0	50.0	49.0	48.0
	4.7	5.7	6.7	7.7	8.7	9.7	10.7
NITON	39.4	4.2	3.4	2.8	2.4	2.1	1.9
Pacific		4.0	4.3	-0.3	-0.4	-0.4	-0.4
WL	48.3	47.4	46.5	45.6	44.7	43.7	42.7
	6.0	2.9	7.8	8.7	9.6	10.6	11.6
	4.4	4.1	5.9	6.7	7.6	8.6	9.6
	41.6	+1.8	+1.9	+2.0	+2.1	+2.2	+2.3
BL	47.3	46.4	45.5	44.6	43.7	42.7	41.7
	12.6	11.5	10.3	9.7	10.6	11.6	12.6
	12.8	12.9	13.0	13.1	13.2	13.3	13.4
	12.8	-1.4	-1.5	-1.0	0.0	-0.5	-1.0
WL	45.4	46.6	46.8	47.5	48.2	48.9	49.6
	5.9	8.0	7.5	6.8	6.1	5.4	4.7
	5.2	5.0	4.8	4.6	4.4	4.2	4.0
	40.6	+0.4	+0.1	+1.5	+3.5	+4.6	+5.7
BL	44.6	45.5	46.4	47.3	48.2	49.1	50.0
	4.7	8.5	7.9	7.0	6.1	5.2	4.3
	4.8	5.3	5.8	6.1	6.3	6.5	6.7
	0.1	+0.5	+0.7	+0.9	+1.0	+1.1	+1.2
WL	42.9	42.60	42.30	42.0	41.7	41.4	41.1
	5.0	5.3	5.6	5.9	6.2	6.5	6.8
	4.9	4.8	4.7	4.6	4.5	4.4	4.3
	42.1	+3.2	3.0	+1.9	+0.5	-0.8	-2.2
FL	5.0	5.3	5.6	5.9	6.2	6.5	6.8
	4.6	5.1	5.5	6.1	6.7	7.3	7.9
	+0.4	+0.2	-0.2	-0.2	-0.5	-0.8	-1.1

Ingraham grading

	wc6	EC6
SL Pacific	46.0	46.0
+50 S	45.90	
1	45.80	
+50	45.71	
✓	45.62	
+50	45.53	
3	45.43	
+50	45.34	
✓	45.24	
+50	45.15	
5	45.05	
+50 = NL Sunset	45.0	45.0 pot + hub
0+00 SL ✓	44.50 75' wide	44.50 ON EAST = BM 43.65
+50	43.80	
1	43.08	
+50	42.37	
W	41.67	
+50	40.95	
3	40.24	
+50	39.54	
✓	38.83	
+50	38.12	
5	37.41	
+50	36.71	
6 = NL Roosevelt	36.0 75' wide	36.0

45.55									
43.7									
47.82									
3.81									
46.01									
3.77									
46.01	WL	46.0	46.1	46.0	45.9	45.8	45.75	45.65	45.55
46.3		3.0	3.7	3.8	3.7	4.0	4.1	4.2	4.3
47.35		4.2	3.9	4.2	4.7	5.4	5.6	4.4	3.7
1.76		-0.6	-0.2	-0.4	-1.5	-1.4	-1.5	-0.2	+0.6
43.11									
5.27	EL	3.6	3.7	3.8	3.9	4.0	4.1	4.2	4.4
37.74		3.7	3.7	3.9	4.7	4.5	4.3	3.8	3.6
		-0.1	0.0	-0.1	-0.8	-0.5	-0.2	+0.4	+0.5
	WL	45.5	45.4	45.3	45.2	44.7	44.7	44.0	43.3
		4.3	4.4	4.6	4.7	5.2	5.2	5.9	6.6
		2.5	2.0	2.1	2.1	3.3	3.3	4.1	4.5
		+1.8	+2.2	+2.5	+2.6	+1.9	+1.9	+1.8	+2.1
	EL	4.4	4.5	4.2	4.7	5.2	5.2	5.9	6.6
		3.4	3.0	4.0	4.7	5.0	5.0	5.0	6.3
		+1.0	+0.9	+0.6	0.0	+0.2	+0.2	+0.9	+0.3
	WL	42.7	41.9	41.4	40.5	39.8	38.6	38.4	37.60
		7.2	8.0	8.7	9.4	10.1	11.3	11.5	12.3
		5.2	5.6	6.2	6.2	6.3	6.9	7.8	8.7
		+2.0	+2.4	+2.5	+3.2	+3.8	+4.4	+3.7	+3.6
	EL	7.2	8.0	8.7	9.4	10.1	11.3	11.5	12.3
		2.2	2.6	3.2	3.8	4.0	4.9	5.6	6.0
		0.0	+0.4	+0.3	+0.6	+1.1	+1.4	+0.9	+1.3

WL	36.9	36.2
	13.0	12.7
	9.6	10.7
	+2.4	+3.0
EL	12.0	13.7
	11.5	13.0
	+0.5	+0.7

Ingraham grading

75' wide	wc6	EC6
SL Roosevelt	35.50	35.00
+50	34.77	34.29
1	34.04	33.58
+50	33.31	32.87
2	32.58	32.16
+50	31.85	31.45
3	31.12	30.75
+50	30.39	30.04
4	29.67	29.33
+50	28.94	28.62
5	28.21	27.91
+50	27.48	27.21
6 = N.L. 75' wide La Playa	26.75	26.50
0+00 SL ✓ ✓	26.75	26.50
+50	26.95	26.75
1	27.15	27.00
+50	27.36	27.25
N	27.57	27.50
+50	27.78	27.75
3 = BREAK	28.0	28.0
+50	29.0	
4 +04	30.0	
+56	31.0	
5 +08	32.0	
+60 = SL Fortuna	33.0	33.0

37.74 1st tie hub on West at Roosevelt

37.74	35.7	35.0	34.3	33.5	32.8	32.1	31.4	30.6
1.78	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7
34.55	31.14	30.60	30.10	29.60	29.10	28.60	28.10	27.60
16.44	8.8	8.5	8.2	7.9	7.6	7.3	7.0	6.7
49.10	47.54	47.10	46.70	46.30	45.90	45.50	45.10	44.70
2.02 WL	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7
31.14	29.60	29.10	28.60	28.10	27.60	27.10	26.60	26.10
3.60	2.0	1.8	1.6	1.4	1.2	1.0	0.8	0.6
27.54	27.10	26.70	26.30	25.90	25.50	25.10	24.70	24.30
7.60	4.1	4.1	4.1	4.1	4.1	4.1	4.1	4.1
35.16 EL	35.4	34.8	34.3	33.8	33.3	32.8	32.3	31.8
4.3	4.3	4.0	3.7	3.4	3.1	2.8	2.5	2.2
4.1	4.1	3.8	3.5	3.2	2.9	2.6	2.3	2.0
10.2	10.2	10.2	10.2	10.2	10.2	10.2	10.2	10.2
29.9	29.9	29.9	29.9	29.9	29.9	29.9	29.9	29.9
7.6	7.6	7.3	7.0	6.7	6.4	6.1	5.8	5.5
10.3	10.3	11.6	12.8	14.0	15.2	16.4	17.6	18.8
0.7	0.7	1.3	1.7	2.1	2.5	2.9	3.3	3.7
29.6	29.6	28.9	28.2	27.5	26.8	26.1	25.4	24.7
4.9	4.9	4.6	4.3	4.0	3.7	3.4	3.1	2.8
4.8	4.8	4.7	4.6	4.5	4.4	4.3	4.2	4.1
1.7	1.7	1.9	2.1	2.3	2.5	2.7	2.9	3.1
27.6	27.6	27.8	28.0	28.2	28.4	28.6	28.8	29.0
7.5	7.5	7.3	7.1	6.9	6.7	6.5	6.3	6.1
2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.5	2.6
1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7
27.5	27.5	27.7	28.0	28.2	28.4	28.6	28.8	29.0
7.6	7.6	7.4	7.1	6.9	6.7	6.5	6.3	6.1
2.3	2.3	2.4	2.6	2.6	2.6	2.6	2.6	2.6
1.7	1.7	1.6	1.5	1.4	1.3	1.2	1.1	1.0
32.2	32.2	33.2	33.2	33.2	33.2	33.2	33.2	33.2
4.9	4.9	4.9	4.9	4.9	4.9	4.9	4.9	4.9
10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8
2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9
2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7

75+75
E of E
89° 51' NE

Culverts 8-9-10 ALTADENA

INlet = 0+00 279.0
 0+43 = angle 276.57
 1 - 273.36
 +30 271.68
 +60 = BREAK 270.0
 +97.5 268.35
 2 +25 = END of 12" pipe Junction of 30" 266.70
 +59 264.45
 +99 = outlet of 36" pipe 262.40

Culverts # 1 # 3 # 5
 0+00 = SLT Horn 298.30
 +50 294.88
 1 287.47
 +50 282.06
 +98.8 = Junction 276.74

#3 = 0+00 E/O ELB wud
 +30 278.89
 +60 = Junction 277.78
 276.74
 #8 OUT 275.80
 1+0 = Junction with #4 274.90
 +43.5 273.72
 1+77 272.55

Culvert #4
 E ob inlet 282.0
 W x ✓ 274.90

Culverts # 11 # 13

INlet = 0+00 260.50
 0+47 257.75
 0+94 Junction 30" 255.0
 1+22 " of 18" 253.30
 1+64 outlet of 30" 251.0

Culvert # 12
 0+00 = grating inlet #9 274.50
 0+00 Bottom of chimney 258.0
 0+08 Junction with 30" 253.30

Culvert # 12 = 18" Conc pipe
 0+00 grating ob inlet #8 274.50
 0+00 bottom chimney 268.0
 0+44 Junction with 30" 255.0

NEBD Nut
 294.08
 2.64
 13.20
 51.72
 1.00
 284.72
 12.64
 270.08
 10.44
 259.47

Top Hd
 3072.6
 016
 3074.2
 13.28
 294.64
 0.71
 295.35
 11.56
 283.79
 1.32
 285.13

NW Hub 29
 Nutmag 7.50
 271.93
 6.40
 276.73
 12.05
 265.25
 2.50
 265.10
 7.35
 257.75
 1.80
 255.0
 1.80
 253.30
 14.1
 23.4
 251.0
 275.74

NUTMEG ST GRADING

	Ncb	5 06
WL Bancroft on south	291.0	294.0
0+50	289.44	290.0
1'	287.87	288.0
+50	286.30	286.0
1+9/30 on NL + 700 SL	285.0	284.0

Bancroft S. of Nutmeg grading

	Ncb	5 06
SL Nutmeg	292.0	293.0
50	292.50	293.17
100	293.0	293.33
150	293.50	293.50
200	294.0	293.67
250	294.50	293.83
300 = NL Maple	295.0	294.0
New SL "	295.50	294.50
55' S	297.25	
110' Break	299.0	298.0
160' S	299.25	
210' S Break	299.50	298.5

29408

NL	91.2	89.7	88.1	86.5	85.4
	3.0	5.4	7.1	8.7	10.0
	12.8	11.6	12.9	13.5	14.7
	-5.9	-6.1	-4.8	-5.1	-4.3
SL	92.2	90.2	88.2	86.2	84.2
	3.0	5.0	7.0	9.0	10.5
	12.8	11.6	12.9	13.0	14.5
	-0.3	-0.1	-0.9	-7.0	-9.9

29408
12.22
30646

WL	92.2	92.7	93.2	93.7	94.2	94.7	95.2
	12.3	13.5	13.9	12.5	12.3	11.8	7.3
	15.0	14.7	14.1	13.6	12.4	12.2	10.0
	-0.7	-0.9	-0.8	-0.6	-0.1	+0.2	+1.3
EL	93.2	93.4	93.6	93.7	93.9	94.0	94.5
	12.3	13.1	12.9	12.5	12.6	12.4	12.3
	10.6	12.2	12.5	11.4	11.4	15.6	15.8
	+2.7	+1.9	+0.3	-1.6	-2.8	-3.2	-3.5
WL	95.7	97.5	99.2	99.5			
	10.8	9.0	7.3	7.3			
	2.0	4.0	4.2	4.2			
	+3.8	+5.0	+3.1				
	285.00	284.00	291.0	291.0			
	10.00	11.0	4.0	3.00			

32nd ST Grading Palm to Laurel

	WCB	ECB
SL Palm	303.0	303.50
+58.07	302.33	302.67
1 +16.1	301.67	301.83
+74.70 = BREAK	301.0	301.0
✓ 124.2		299.50
+74.2		298.0
3 +24.2		296.50
+74.2		295.0
✓ +24.2 = BREAK	293.50	293.50
+49.2	292.70	292.70 ✓
+74.2	291.60	291.60
+99.2	290.30	290.40
5 +24.2	288.90	289.10
5 +44.2 on west = 8.	287.65	287.65
5 +94.2 = NL NUTMEG	284.50	285.0
SL NARROW ST ON WEST	284.0	284.0
0+00 SL NUTMEG	283.50	284.0
	283.70	284.50
N.L. SAN MARCUS	282.90	285.00
SL " "	285.95	286.50
		291.50
NL MAPLE ON EAST	Raise to 297.55 on EL 32 nd	296.50 .75 in return
SL " "	301.15	299.75
		299.61
		299.47
		299.33

31

EL	300.0	299.7	298.7	296.7	295.2
	8.4	2.0	3.5	5.0	6.5
	3.6	5.1	3.9	5.3	5.3
	+4.8	-0.1	-0.2	-0.3	+1.2
EL	303.50	292.9	292.1	291.2	290.2
	9.9	10.1	11.0	12.1	13.0
	7.0	9.1	11.4	13.0	15.0
	11.1 High	13.4	12.1	10.7	8.0
					+0.6
					-1.1
EL	297.7	297.9	296.8	294.7	293.8
	5.0	5.9	6.9	7.9	8.8
	4.3	4.7	5.3	6.0	6.3
	+3.7	+4.1	+4.6	+4.5	+4.5
EL	297.7	296.9	295.8	294.6	293.3
	5.0	5.5	6.1	6.7	7.3
	4.3	4.4	4.5	4.9	5.0
	+0.2	+1.1	+1.5	+2.1	+2.5
304.03					
307.7	303.0	303.50			
	4.2	4.2			
304.03					
	1.6				
305.19					
	12.49				
✓ 174.70					
✓ 20.57					
✓ 193.27					
EL	296.15	295.5	294.75	293.75	292.75
	11.4	10.9	9.4	7.4	5.4
	10.4	12.4	6.7	3.0	1.9
	-0.8	-0.5	+2.7	+1.4	+3.8
EL	300.0	298.6	297.2	295.8	294.4
	8.4	8.6	8.7	8.9	9.0
	3.6	3.7	4.3	5.0	6.7
	+4.8	+4.9	+4.9	+5.9	+6.3
					+0.3
					299.05
					9.29
					299.19
					299.05

0.75 in return on EL 201.50

32nd ST UPAS TO THORN

	WCB	ECB
ST UPAS = 0+00	324.0	325.0
+50	322.30	323.10
1	320.60	321.20
+50	318.90	319.30
2	317.20	317.40
+50	315.50	315.50
3	313.80	313.60
+50	312.10	311.70
4	310.40	309.80
+50	308.70	307.90
5 = BREAK	307.0	306.0
+50	306.75	305.25
6 = N4 THORN	306.50	304.50

32390: SURBP UPAS + 32nd

32

317								
327.07								
12.56								
314.51								
1.29								
315.71	WL	324.00	22.50	20.50	19.10	17.40	15.70	14.00
1.53			4.6	6.3	8.0	9.7	11.4	13.1
308.13			3.9	5.1	6.6	8.3	10.0	11.6
2.59			4.7	5.7	6.6	7.4	8.2	9.0
303.74			10.7	11.4	11.4	11.4	11.0	10.5
	EL	325.0	23.30	21.40	19.50	17.60	15.70	13.80
			3.8	5.1	7.6	9.5	11.4	13.3
			3.9	4.8	5.3	6.5	8.5	10.5
			11.1	11.7	12.3	13.0	13.7	14.3
	WL	12.30	110.60	305.90	207.20	307.00		306.50
		3.0	6.9	5.4	3.5	8.7		
		3.2	5.6	8.7	4.5	10.0		
		10.4	12.5	-13.7	-14.7	1.3		
	EL	11.90	310.00	08.10	06.20	05.50		304.50
		3.3	5.7	7.6	9.5	10.2		11.5
		1.5	4.8	8.0	11.7	12.3		
		12.5	12.8	-2.1	-1.7	-2.1		
307.26								
11.4								
311.40								
		304.50		307.0		306.0		
		6.90		11.40		5.70		

32nd ST Grading Redwood to Palm
 WCB E.C.B

SL Redwood = 0+00	295.0	295.0	295.40
+50	295.67	295.75	
1	296.33	296.50	
+50	297.00	297.25	
2	297.67	298.00	
+50	298.33	298.75	
+70 = N.W. QUINCO	298.60	299.05	
3 +30 = SL "	299.40	299.95	
+50	299.67	300.25	
4	300.33	301.00	
+50	301.00	301.75	
5	301.67	302.50	
+50	302.33	303.25	
+98.6 = N.W. PALM	303.0	304.0	
600			

294.64
 0.49
 295.13
 13.69
 305.44
 1.20
 303.96

W.L.	95.2	95.9	96.6	97.3	97.9	98.6	98.8
	4.6	3.3	4.0	5.1	7.5	6.8	1.6
10+00 N.W. PALM	5.3	16.2	14.0	14.6	11.7	10.3	3.4
	-7.9	-19.5	18.0	-6.5	4.2	-3.5	-2.8
E.L.	95.00	96.0	96.7	98.0	98.2	99.0	99.3
	10.44	9.5	8.7	7.4	7.2	6.4	6.1
	10.44	5.2	4.8	5.0	3.9	2.3	1.9
	4 High	14.2	13.9	4.4	13.2	4.1	4.2
W.L.	99.7	99.9	300.6	301.2	301.9	302.6	303.4
	4.7	5.5	4.8	4.2	5.5	2.8	2.2
	6.7	-0.6	5.8	4.8	3.5	1.9	1.2
	-1.0		-1.0	-0.3	11.0	10.9	11.0
E.L.	300.2	300.5	301.2	302.0	302.7	303.5	304.00
	5.2	4.9	4.2	3.4	2.7	1.9	1.2
	2.0	1.7	1.0	1.3	0.7	0.7	1.2
	+3.2	+3.2	+3.0	+2.1	2.0	+1.2	
304.03							
309.51							
297.6	304.0	303.0	295.0				
299.75	5.51	6.1	5.96				
1.21							
300.96							

33 d 5T Grading Palm To Nutmeg

	W C6	F C6
Sl Palm - 0+00	305.50	306.00
0+60	303.58	303.83
1+20	301.67	301.67
1+80	299.75	299.50
2+40	297.83	297.32
3+00	295.91	295.17
3+60 BRK	294.00	293.00
4+10	292.79	
4+60	293.58	
5+10	293.37	
5+60	293.15	
5+95 NL Nutmeg	293.00	292.00

296.00 1000 Nutmeg + Bancroft

5.66
297.63
0.46
298.97

WIL	305.50	03.3	01.9	300.0	98.1	96.2	94.2
		3.5	5.7	7.6	9.5	3.2	5.2
		3.2	11.1	5.6	2.6	1.6	5.0
		+0.6	+1.6	+2.0	+1.9	+1.6	+0.7
EL	306.0	04.1	01.9	297.7	97.6	95.4	93.2
		3.5	5.7	7.9	1.8	1.0	6.2
		3.5	4.5	5.0	4.0	7.7	11.3
		+0.7	+1.2	-0.2	-2.2	-3.7	-5.1
WIL	94.0	93.5	93.6	93.4	92.2		
	5.4	5.6	5.8	6.0	6.2		
	4.9	5.3	4.8	4.2	5.2		
	+0.5	+0.3	+1.0	+1.3	+1.0		
EL	6.4	6.6	6.8	7.0	7.2		
	12.6	15.0	12.2	6.0	6.9		
	-7.2	-8.4	-5.4	+1.0	+0.3		
	295.0	294.0	294.0	293.0			
	663	5-13	5.22	6.42			

305.60
32.0
308.70
22.51
296.09
3.23
299.72

35

Bancroft Grading

	w.c.b.	EC6
SL Palm	304.50	304.50
Jr S	304.14	
105	303.74	
157.5	303.37	
210	Break	303.0
250	301.75	
290	300.50	
330	299.25	
370	Break	295.0
Jr S	296.75	297.0 ✓
Jr S	295.50	296.0
28.75	294.25	295.0
295 = w.c. nutmeg	293.0	294.0

30403 1417 + 32nd

449

305.47

12.91

292.56

8.10

297.65

4.22

292.12

294.08

1417 + 32nd

NEBR

304.50	04.3	304.0	03.0	03.2	307.0
4.2	4.2	4.5	4.9	5.3	6.5
3.5	4.6	5.1	5.5	7.1	
10.7	-0.1	-0.2	-0.5	-0.6	
FL	4.2	4.5	4.9	5.3	6.5
	3.9	4.2	4.7	5.0	5.8
	10.3	10.3	10.7	10.7	11.1

WIL	300.7	99.5	98.2	97.0	95.7	94.5	93.2
	7.5	9.0	10.3	11.5	12.0	12.2	12.5
	8.1	9.4	10.9	12.2	13.1	13.2	13.3
	-0.3	-0.4	-1.7	-0.7	-1.1	0.0	10.2

FL	7.8	9.0	98.2	97.2	96.2	95.2	294.0
	6.4	7.6	10.3	11.1			
	41.1	41.4	10.8				

29408

411

295.19

30403

395

305.01

293.0	303.0	295.00
5.17	5.01	10.01

Felton ST Grading

EL-STM.

	WCB	ECB
St Point = 0100	305.50	305.50
50	304.75	304.75
100 BREAK	304.00	304.0
+50	302.60	1+45 302.75
200 BREAK	301.20	1+85 301.60 = PC 301.21
+50	299.40	2+50 299.60 301.00=EL
300 BREAK	297.60	3+00 298.00
+50	295.20	295.83
4	292.86	293.67
+50 BREAK	290.50	291.50
+98.5	285.83	286.83
577.0	281.17	282.17
595.5 = NL Not Meq	276.50	278.47
	276.20 ←	277.50 = NL Not Meq
SL "	275.50	276.50

Sw 7' track
Palin + Felton

	WCB	ECB	304.2	302.8	301.4	99.6	97.8
	305.50	305.0	304.2	302.8	301.4	99.6	97.8
WL	305.50	305.0	304.2	302.8	301.4	99.6	97.8
EL	305.7	305.0	304.2	302.8	301.7	99.8	98.2
WL	95.4	93.1	90.7	86.1	81.4	76.4	
FL	96.1	93.9	91.7	87.1	82.4	77.2	
ECB	304.90	305.15	305.21	305.27	305.25		
ECB	304.75	304.0	302.60	301.60	301.31	301.0	
ECB	304.00	+50	1+00	1+50	1+85	2+00	
ECB	299.50	299.56	300.08	300.8	300.2	300.20	
ECB	298.0	+50	1+00	PCVC 1+50	PCVC 1+50	PCVC 1+50	
ECB	286.83	282.17	277.30	277.30	277.30	277.30	
6 parts	76.95	76.51	76.94	77.20	77.73	78.46	

Redwood + 32nd

Return High 4.70 5.20 5.45 5.15 4.40

7.20 7.75 7.90 7.75 7.30

9.96 0.41 0.56 0.41 9.96

2.52 2.97 3.13 2.99 2.55

4.73 5.21 5.39 5.17 4.56

6.03 6.51 6.69 6.57 6.16

7.55 8.03 8.21 8.11 7.70

8.64 9.12 9.30 9.19 8.78

0.16 0.26 0.36 0.26 0.37

1.60 2.12 2.35 2.19 1.90

4.60 3.13 3.37 3.01 2.95

3.34 3.96 4.10 4.15 3.38

3.71

3.75

4.25

4.25

4.25

4.25

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.70

4.56

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

4.75

Bancroft

25' BREAKS

Redwood

V PAS

ST

X

70'

X

10'

X

15'

X

18'

75'

O

ST

O

ST

330

FELTON ST

70' 2.40 0.10 2.50

IN MAIL

X

16'

ST

X

40'

ST

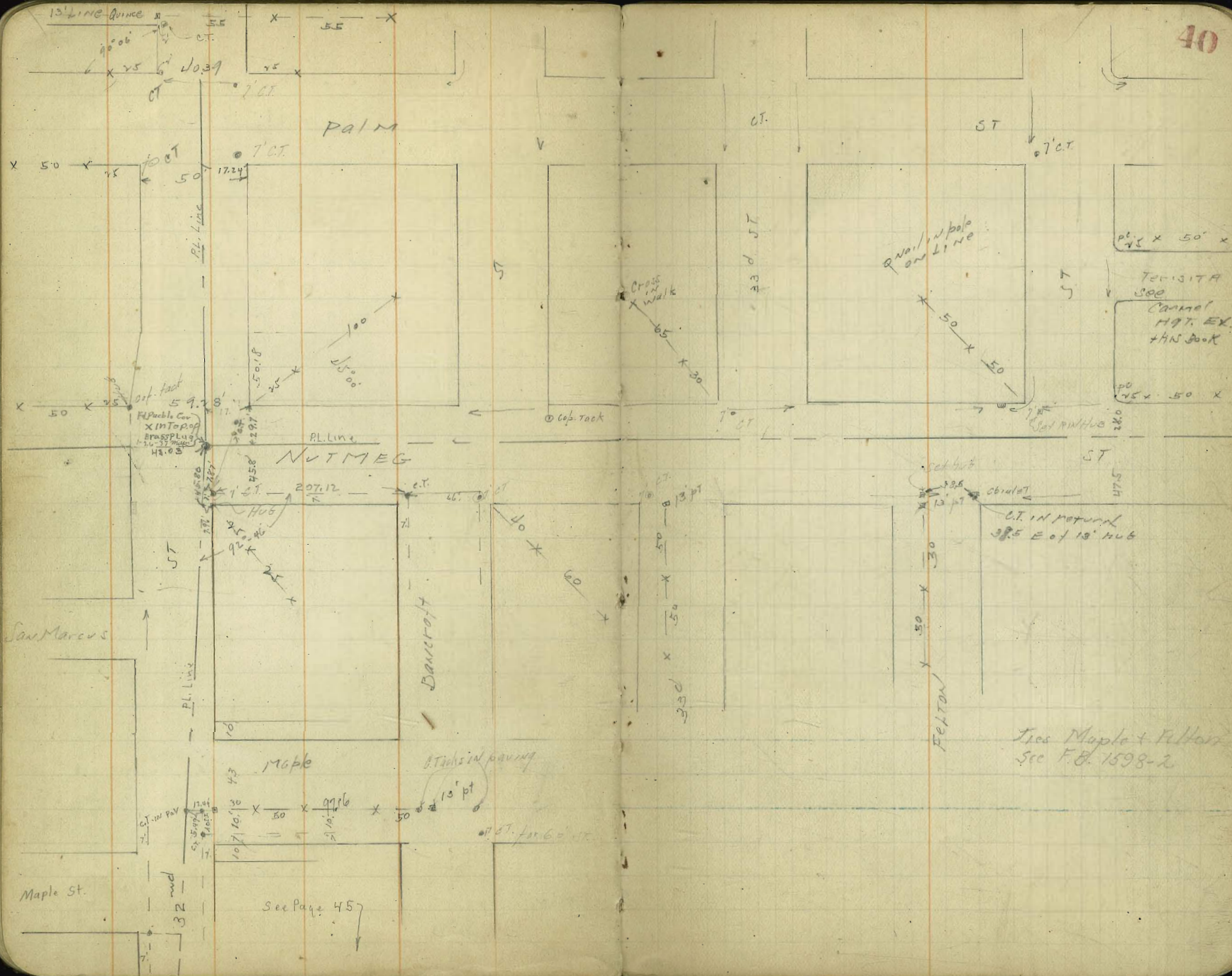
X

10'

ST

39

Redwood to 490 ST



Sewer Construction
32nd St Maple to Palm

(Carmel Hqts)

#1	
DE. S. of Maple = 0700	296.0
0+49	295.40
0+98	294.80
1+47	294.20
1+96	293.60
2+45 = M.H. E Maple #1	293.0
2+92.75	290.0
3+40.50	286.99
3+88.25	283.98
4+36 = M.H. E San Marcus #2	280.97
4+76	281.24
5+16 = beginning C.I. pipe	281.50
5+64	281.82
6+12	282.14
6+60 = END C.I. pipe	282.46
6+98	282.73
7+36 = M.H. #3	283.07
7+90	284.60
8+42	286.20
8+98	287.80
9+52	289.40
10+06 = M.H. #4	291.0
10+54.75	292.37
11+02.50	293.75
11+52.25	295.12
12+01 = DE. #2	296.50

Tied out
50' E & W

294.08
21.0
273.08
12.66
283.56
6.95
290.51
9.00
290.51
13.12
303.63

Not Meg + Bancroft
NEP

Sept. 29, 26
Moore

41

283.0	52.73	52.46	52.14	51.82	51.50
13.22	13.49	13.76	8.37	8.69	9.01
3.23	7.53	12.66	11.87	10.52	6.80
79.79	+5.96	+1.10	-3.50	-7.73	+2.21
812.4	50.97	53.98	56.99	290.0	293.0
9.27	9.54	6.53	16.62	13.63	10.63
5.73	5.96	2.52	12.70	8.80	5.48
+3.53	+3.58	+3.71	+3.94	24.83	15.75
293.60	94.20	94.80	95.40	296.0	
32nd + Palm 10.03	9.43	8.83	8.73	7.63	
304.63	4.85	4.80	4.69	5.20	
0.90	+5.78	+7.63	+4.26	+3.51	+2.40
304.73					
13.23					
291.70	296.50	95.12	93.75	92.37	291.0
9.36	8.43	9.81	11.18	12.56	15.93
292.06	2.72	3.46	4.05	3.24	15.53
	+5.69	+6.35	+7.13	+7.32	17.13
					10.04
					+7.09
86.20	84.60	283.0	282.73	52.46	52.14
18.73	7.16	9.06	9.33	9.60	9.92
11.68	1.03	3.50	5.25	7.80	9.58
+7.05	+6.43	+5.56	+3.55	+1.80	+0.34
81.82	81.50				
10.24	10.56				
10.98	8.29				
-0.74	+2.27				
	2.21				

QUINCE ST

Carmel Hgts. Annex

2905
1269
303.40

NL STA	N CB	SL STA	S CB
	293.60		295.1 ✓
0+00 = P.C.	294.44 ✓		294.93
0+55	295.18 ✓		295.68
1+10	Break		296.4 ✓
+30	"		296.61
+50	"		296.63
+70	"		296.49
+90	"		296.15
2+10	"		295.71
+30	"		294.5 ✓
+50	"		293.76
+70	"	2+70	293.31
3+79.31	RL P.C.		292.21
3+85	" EC	3+02.48	291.50 W. Boundary

NL	94.7	95.4	96.2	96.3	96.3	96.2	95.9
	$\frac{5.5}{15.2}$ -6.7	$\frac{7.0}{10.2}$ -3.6	$\frac{7.0}{7.5}$ -0.5	$\frac{6.9}{7.0}$ -0.1	$\frac{6.9}{6.5}$ +0.4	$\frac{6.1}{6.1}$ +0.9	$\frac{7.3}{6.1}$ +1.2
SL	95.1	95.9	96.6	96.8	96.5	96.7	96.4
	$\frac{6.1}{7.5}$ +1.4	$\frac{7.3}{5.2}$ +2.1	$\frac{6.6}{9.4}$ +2.8	$\frac{6.4}{11.1}$ +4.7	$\frac{6.2}{12.6}$ +16.4	$\frac{6.5}{12.0}$ +5.5	$\frac{6.4}{13.5}$ +7.1
NL	95.4	94.8	94.0	93.0	92.4	90.2	
	$\frac{7.3}{6.3}$ +1.0	$\frac{6.4}{6.8}$ +0.4	$\frac{7.3}{7.3}$ +0.0	$\frac{7.3}{11.9}$ +4.6	$\frac{6.3}{11.5}$ +5.2	$\frac{9.2}{13.3}$ +4.1	
SL	96.0	95.3	94.5	93.5		91.70	
	$\frac{7.2}{3.0}$ +4.2	$\frac{7.9}{4.0}$ +3.9	$\frac{8.7}{11.0}$ +2.3	$\frac{9.7}{14.2}$ +4.5		$\frac{11.5}{13.1}$ +1.6	
N	94.4 = P.C.	92.58	91.88	91.38	90.78	89.17	88.45
S	91.93 = P.C.	91.81	91.56	91.49	91.30	91.20	

Carmel Hqts Palm St GRADING

ANNEX

N 66

S 66

305.67
305.51
306.15

EL FOLION	306.0	305.50
0+10	305.45	304.90
55 E	302.96	302.45
110 BREAK	299.90	299.40
130	298.86	298.35
150	297.84	297.41
170	297.09	296.55
190	296.38	295.85
210	296.19	295.78
230	296.12	295.71
250	296.23	295.85
270	296.39	296.0
300 = WL Cooper	296.74	296.34
3+70.87 = PC EL.	297.50	297.21
500	297.83	297.56
450	298.38	298.17
500	298.94	298.75
5+40 = PC WL MCK.	299.39	299.28
6+10 = V BL ✓	299.43	299.28
+60	299.10	298.97
7+10	298.75	298.65
+60	298.42	298.35
8+10	298.09	298.04
+60	297.76	297.74
9+00 = BREAK.	297.50	297.50
+51.15 = PC ON N.L.	297.74	295.65
ARC		
8.55 = WL BOUNDARY	297.0	297.50

Palm + Folion
305.67
307.67
307.15

43

N	305.7	303.4	300.10	29.1	28.1	27.3	26.6
		2.4	7.5	8.5	2.8	2.0	1.3
		3.9	6.1	7.9	1.9	7.9	7.4
		11.1	17.4	20.6	-2.7	-9.9	-8.7
S	306.1	302.7	29.4	28.6	27.6	26.8	26.1
	2.5	2.9	8.0	7.0	10.0	1.5	0.8
	40.3	17.4	21.8	21.3	1.6	-6.0	-12.0
N	26.4	26.3	26.5	26.6	27.0		
	11.3	11.3	11.1	11.0	10.6		
	13.7	10.6	9.4	8.1	7.4		
	41.5	10.7	11.8	12.9	13.4		
30336 X	26.0	26.0	26.1	26.4	26.6		
	0.7	0.7	11.5	11.4	11.0		
	10.3	5.4	13.3	11.4	10.1		
	-11.0	-6.2	-7.8	0.0	10.9		
N	27.7	28.1	28.6	29.2	29.6	29.6	29.3
	6.2	5.4	5.3	4.7	4.3	3.3	3.0
	1.6	1.7	2.2	3.1	3.2	3.3	3.0
	17.6	16.1	13.0	11.6	10.7	10.5	11.3
S	27.4	27.5	28.4	29.0	29.5	29.5	29.2
	6.4	6.1	5.5	4.9	4.5	4.4	4.1
	3.4	3.5	3.2	3.2	3.1	3.1	3.2
	13.1	12.3	12.3	11.3	10.7	10.5	11.2
N	28.6	28.3	28.0	27.7	28.0		
	5.3	5.6	5.9	6.2	5.9		
	3.7	3.9	3.8	4.2	4.0		
	11.6	11.7	12.0	12.0	12.5		
S	28.6	28.3	28.0	27.7	28.0		
	5.3	5.6	5.9	6.2	5.9		
	3.7	3.9	3.8	4.2	4.0		
	11.6	11.7	12.0	12.0	12.5		

Culverts - Carmel Hgts Fresno

295.017

#4 #5 #6

#4 = Bottom Box 289.0 $\begin{matrix} 6.3 \\ 5.4 \\ +1.1 \end{matrix}$

① = Junction 283.50

#6 = Bottom Box 287.40 $\begin{matrix} 8.1 \\ 0.5 \\ +7.6 \end{matrix}$

② = Junction 282.60

#5 inlet 284.6 $\begin{matrix} 10.7 \\ 10.5 \\ +0.2 \end{matrix}$

outlet 281.5 $\begin{matrix} 2.8 \\ 1.3 \\ +1.5 \end{matrix}$

#1 inlet flowline 283.6 $\begin{matrix} 12.87 \\ 10.67 \\ +2.2 \end{matrix}$ 296.57

outlet 274.6 $\begin{matrix} 17.1 \\ 13.3 \\ +3.8 \end{matrix}$ 291.70

#4 Side bottom Box 285.30 $\begin{matrix} 11.7 \\ 6.0 \\ +4.7 \end{matrix}$ 296.77

#3 Side " " 285.3 $\begin{matrix} 11.7 \\ 6.7 \\ +4.0 \end{matrix}$ 296.77

#11 inlet 287.6 $\begin{matrix} 266.35 \\ 8.75 \end{matrix}$

Junction #11 w/cb 254.5 $\begin{matrix} 8.86 \\ -0.18 \end{matrix}$

" #10 ECB 251.7 $\begin{matrix} 266.85 \\ 18.88 \end{matrix}$

outlet 247.51 $\begin{matrix} 15.80 \\ +3.05 \end{matrix}$

#12 bottom box west 267.9 $\begin{matrix} 278.87 \\ 10.97 \end{matrix}$

#10 bottom box East 261.5 $\begin{matrix} 278.87 \\ 17.27 \\ 13.25 \\ +3.51 \end{matrix}$

Culvert #7

W. end inlet 293.00 E. end outlet 274.6

$\begin{matrix} 7.3 \\ 6.4 \\ +0.7 \end{matrix}$

296.47
 di inlet #3 S of McKinley 10 S of Bar 292.60
 $\begin{matrix} 3.87 \\ 5.13 \\ -1.26 \end{matrix}$ di grade 292.60
 $\begin{matrix} 10.42 \\ 5.25 \\ +4.87 \end{matrix}$ Bottom 292.56
 $\begin{matrix} 3.71 \\ 6.45 \\ -2.74 \end{matrix}$ di grade 292.56

di inlet #4 W of McKinley 10 S of Bar 293.37

$\begin{matrix} 3.10 \\ 1.32 \\ +1.80 \end{matrix}$ Bottom 293.37
 $\begin{matrix} 7.82 \\ 1.98 \\ +5.84 \end{matrix}$ 10 N of Bar 293.37
 $\begin{matrix} 3.10 \\ 2.86 \\ +0.24 \end{matrix}$

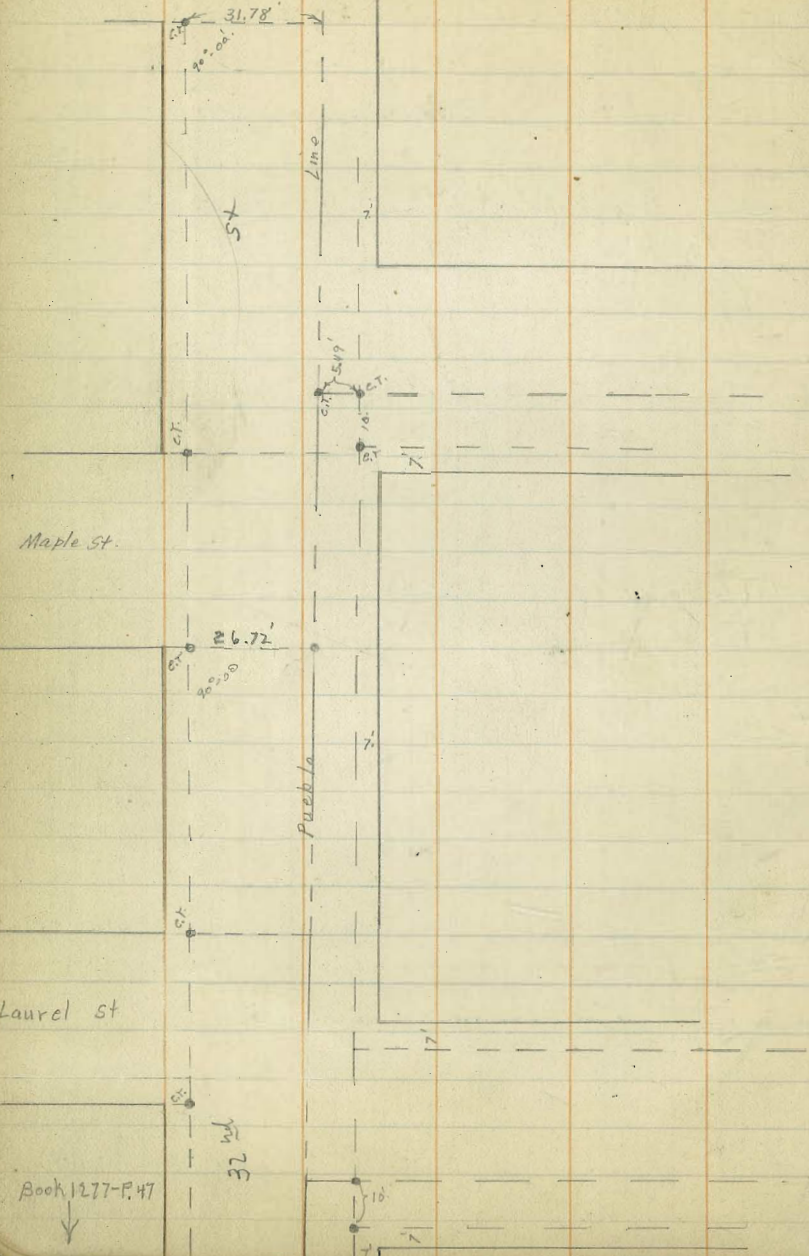
$\begin{matrix} 287.82 \\ 9.40 \\ 8.64 \\ +0.78 \end{matrix}$ $\begin{matrix} 292.72 \\ 9.43 \\ 11.04 \\ -1.63 \end{matrix}$ $\begin{matrix} 294.04 \\ 5.15 \end{matrix}$ $\begin{matrix} 290.00 \\ 9.2 \\ 8.9 \\ +0.3 \end{matrix}$ chk

$\begin{matrix} 282 \\ 6.18 \\ 10.98 \\ +3.74 \end{matrix}$ $\begin{matrix} 289.40 \\ 9.82 \\ 10.44 \\ -0.69 \end{matrix}$ $\begin{matrix} 292.37 \\ 9.85 \\ 10.44 \end{matrix}$ $\begin{matrix} 296.6 \\ 7.4 \\ 9.1 \\ +0.9 \end{matrix}$

52.025
 27.1
 19.88
 73.6
 24.6
 88.3
 71.1
 50.5
 20.6
 104.6

305
 $\begin{matrix} 47.16 \\ 14.3 \\ +2.0 \end{matrix}$
 Prop 274.6
 15.7

San Marcos St



Book 1277-P.47

Laurel St

Maple St.

0 46 0 7167

UT

PalM

McKinley

Hub 70.87 C.T. Hub 90°00'

Cooper

70°00'

Hub

C.T.

70°00'

Cooper

70°00'

C.T.

70°00'

Cooper

70°00'

C.T.

70°00'

Cooper

70°00'

C.T.

70°00'

Cooper

70°00'

C.T.

70°00'

Cooper

70°00'

C.T.

70°00'

Felton

EL. = 014

R = 30'

60'

19°07' = Δ

30'

UT

C.T.

30'

UT

C.T.

30'

UT

C.T.

30'

UT

C.T.

30'

TERESITA

C.T. W. TEL

R = 25'

Lot Line

Δ = 65°00'

3.20

PMH

7 C. Tacks

60'

60'

60'

60'

60'

60'

7 C.T. 30' 30' UT

Carmel 46
Hqrs.
EXTENSION

ST

75.52

Hub C.T.

90°00'

7'

90°00'

60'

65°10'

65°10'

65°10'

65°10'

65°10'

65°10'

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Cooper

NUTMEG

WOOD LINE

BOUNDARY

F.L.

B.M. 29627

100'

90°00'

30'

24.55

S. LINE

7' C.T.

90°00'

30'

UT

C.T.

30'

UT

C.T.

30'

UT

C.T.

30'

Lot Line

50' 4100'S on C.T. LINE

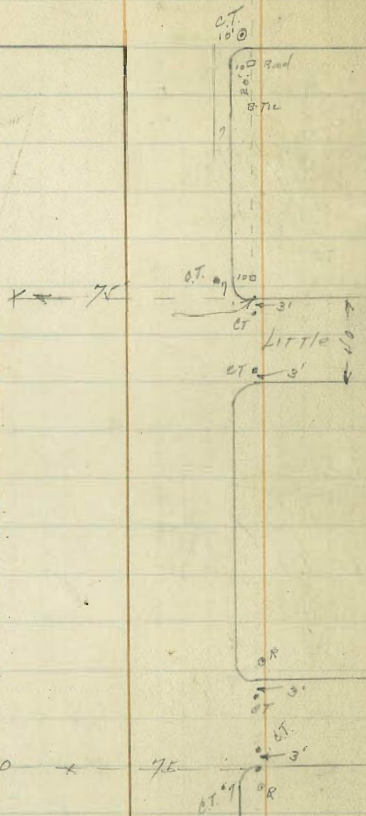
Hub 100'

Hub 50' 4100'S on C.T. LINE

Hub 50' 4100'S on C.T. LINE

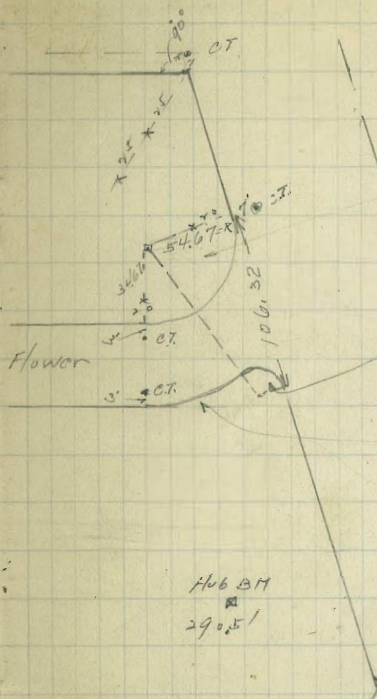
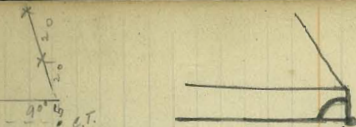
opt tack
Gregory

Redwood



School

McKinley



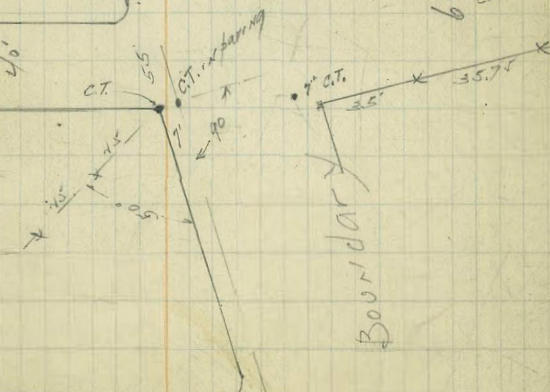
$$\begin{aligned} a &= 106^{\circ} 17' \\ R &= 54.67 \\ T &= 72.92 \end{aligned}$$

$$\begin{aligned} A &= 109^{\circ} 05' \\ R &= 17.79 \end{aligned}$$

$$\begin{aligned} A &= 35^{\circ} 22' \\ R &= 94.67 \end{aligned}$$

Quince

Hub BM
29.51



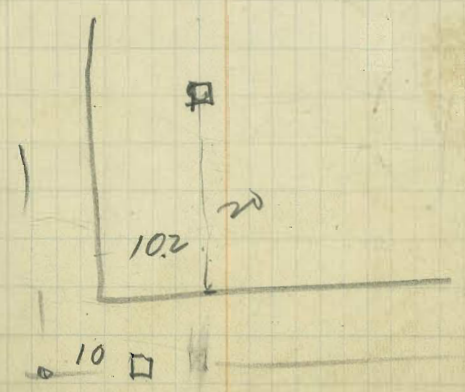
Boundary

Palm

BOUNDARY ST.

WL STA.	W CB	EL STA.	ECB	
NL Redwood -67.50	293.0	-45.0	291.45	NL Redwood produced
SL " = 0+00	291.0	-0+00	290.0	at right Δ
0+52.09	288.0	0+55	286.89	
1+04.18 = NL Flower	285.0	1+10	283.75	
(55.80)				
+30		1+30	282.76	
+50		+50	281.96	
+70		+70	281.39	
+90		+90	281.04	
2+10.50 = SL Flower = EC	281.88	2+10	280.91	
+30	281.94	+30	281.0	
+50	282.21	+50	281.31	
+70	282.72	+70	281.85	
+90	283.44	+90	282.61	
3+10	284.38	3+10	283.59	
+30	285.54	+30	284.79	
+50	286.94	+50	286.22	
3+91.50 = PL NL Quince	290.0	3+59.89	286.93	
↑		+79.89	288.31	
↓		+99.89	289.37	ON EAST NL Quince
↓		+119.89	290.13	
↓		+139.89	290.57	
4+46.50 = SL Quince	291.50	4+59.89	290.85	ON EAST SL Quince
5+01.09	292.33	5+09.89	291.55	
+55.65	293.17	+59.89	292.26	
6+10.27 = PC NL Palm	294.0	6+09.89	292.96	

Station	W CB	EL STA.	ECB	Notes
295.76 x				
13.00				
282.76				
0.35				
283.05				
12.11				
269.94	W	90.0	91.2	88.2
0.01		0.5	0.5	1.0
269.95		1.0	1.0	2.0
0.55		1.5	1.5	3.0
269.07		2.0	2.0	4.0
12.36		2.5	2.5	5.0
281.43	E	91.7	90.2	87.7
0.42		0.0	0.5	1.7
281.01		1.0	1.0	2.7
12.91		1.5	1.5	3.7
283.92		2.0	2.0	4.0
	W	82.1	82.1	82.5
		0.9	1.4	1.6
		1.8	2.8	3.1
		-1.6	-1.6	-1.6
	E	81.1	81.2	81.5
		11.2	11.3	11.6
		4.4	14.0	14.7
		-15.6	-15.2	-15.2
290.51				
95.0	W	90.0		
300.03		0.7		
		0.0		
		+3.7		
290.51				
0.31	E	87.0	88.6	89.6
291.32		6.1	5.3	4.3
		12.0	10.0	9.0
		-5.3	-5.0	-4.7



BOUNDARY ST

WCB.

ECB

ELSTH

6+86.11 = SL Palm	294.50	6+59.89	293.67
7+51.14	295.60	7+09.89	294.37
8+16.13	296.70	+59.89	295.08 ✓
8+81.14 = PC NL Olive	297.80	8+09.89	295.78
9+46.56 = SL "	298.50	+59.89	296.50
10+02.67	298.77	8+94.48	297.00 BREAK
+58.78	299.03	9+56.28	297.57 ✓
11+14.90 = PC NL Cooper	299.30	10+18.08	298.73
12+07.01 = SL Cooper	299.50	10+79.89	299.60 EAST NL Cooper
+52.43	299.10	11+39.89	300.50 SL "
12+97.86 = PC NL	298.70	+97.13	300.17 ✓
31	298.20	12+54.37	299.83 ✓
		13+11.63	299.50 = NL Nutmeg
		14	299.10 = SL "

1311.61
1139.89
181.72
42
223.72

30003 T

799.79
6.80
206.64

W	94.7 5.3 +2.5	95.8 4.2 +2.0	96.9 3.1 +1.8	98.0 2.0 +1.7	98.7 2.9 +1.7	99.0 2.6 +1.1	99.3 2.3 +0.7
E	93.9 6.1 -4.3	94.6 5.4 -3.1	95.3 4.7 -2.2	96.0 4.0 -0.6	96.7 3.3 +1.0	97.4 2.6 +1.7	98.1 2.5 +2.2
W	99.50 2.1 +0.5	99.7 0.9 -0.1	99.3 7.3 -0.3	98.9 2.7 -0.4	98.4 0.4 -0.2		
E	99.0 2.6 -2.2	99.8 6.8 +1.7	300.7 5.9 +1.1	300.4 6.1 +1.3	300.1 6.5 +1.4	99.7 6.9 +0.8	99.2 2.3 +0.5
W	299.00 4.18 +1.2	98.6 0.84 +1.2	98.00 5.09 +1.8	97.24 6.15 +1.0	96.68 6.21 +0.8	96.0 6.29 +0.9	

NUTMEG ST

297.2 x
1160
185.63
1.63
287.26

NL STA	NCB	SL STA.	SCB	
EL Felton PC = 0+00	278.46	0+00	276.50	EL Felton
+29.96	281.3 ✓	0+40	280.3 ✓	
+49.96	283.1 ✓	0+60	282.1 ✓	
+69.96	284.68	0+80	283.68	
+89.96	286.00	1+00	285.0	
1+09.96	287.08	+20	286.08	
+27.96	287.9 ✓	① +28.67	286.44	South EL Gregory
+47.96	288.5 ✓	+40	286.9 ✓	
+67.96	288.88	+60	287.5 ✓	
1+50.00 = PC WL	289.00 ✓	+80	287.88	
2+57.96 = PC	285.80	2+00	288.0	opp. WL Teresita
		① +08.67	287.80	South EL Gregory
end of work		2+40	287.50	opp. EL Teresita
		+65.10	285.08	" PC on N

	N	28.7	81.6	83.4	84.9	86.2	87.3	88.2	88.8
		8.5	15.6	12.8	12.3	11.0	9.9	9.0	8.4
		4.1	11.6	9.8	8.1	6.9	6.1	5.4	5.1
		24.1	70	74.0	74.2	74.7	73.8	73.6	73.3
	S	76.7	80.6	82.4	83.9	85.2	86.3	86.7	87.2
		10.5	6.6	4.8	3.3	2.0	10.9	10.8	10.0
		10.5	9.6	6.4	4.1	11.7	9.8	9.0	8.8
		5.8	-3.0	-1.4	-0.8	+0.3	+1.1	+1.6	+1.5
	N	89.1	89.2	86.0					
		5.1	8.0	X					
		2.9	4.7	.					
		23.2	23.3						
	S	87.8	88.1	88.2	EL Gregory	87.7	85.2		
		9.4	9.1	9.0	8.0	7.4			
		7.7	7.0	6.5	6.5	7.2			
		11.7	12.1	12.5	12.7	12.3			

192488

TERESITA ST

	N 06	S 06
EL FELTON EC	30148	299.60
+ 10 = PC	300.70	300.20
	299.54	299.04
1+07.7=PC	298.38	297.88
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	297.75	297.59
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	297.12	297.29
R=30' ③=EC	296.50	297.0
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	295.37	295.87
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	294.25	294.74
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	293.12	293.61
= 4 pt. ④	292.0	292.78
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	290.95	291.40
$\frac{1}{2} \frac{1}{2} \frac{1}{2}$ 0	289.91	290.31
③ PC	288.87	289.23 = PC
Middle curve	287.33	289.0 = EC
NLN + Meq = EC	285.80	NLN + Meq

51
EC

305.64 0.6 306.26 12.24 294.00 2.23 297.33	N 301.7 2.5 4.1 +0.4	S 301.0 5.2 4.2 +1.0	99.8 6.1 6.5 +1.7	98.6 7.6 5.3 +2.3	98.0 8.2 6.6 +1.6	97.4 8.8 5.0 +1.8	96.7 9.5 4.8 +1.3
S 299.8 6.1 5.7 +0.7	S 300.5 5.7 5.4 +0.3	99.3 6.9 5.7 +1.2	98.1 8.1 6.3 +1.2	97.8 8.4 6.6 +1.8	97.5 8.7 6.9 +1.5	97.2 9.0 7.2 +1.8	96.7 9.5 7.7 +1.3
N 98.6 10.6 4.7 -1.1	S 94.0 11.7 10.1 -1.4	93.4 3.8 4.1 -0.3	92.2 5.0 4.2 +1.1	91.4 6.0 4.9 +1.1	90.2 7.0 5.8 +1.5	89.1 8.1 6.3 +1.8	88.5 7.7 6.6 +1.1
N 87.4 9.6 6.7 +2.9	S 86.0 11.2 7.5 +3.7	80.70 6.26	80.00 6.76	80.70 6.26	80.00 6.76	79.8 6.0 4.0 +1.0	79.8 6.0 4.0 +1.0
305.64 1.2 306.86 9.10 297.76 12.24 297.54 8.5 298.71 10.70 288.01 1.00 292.59 3.27 295.86 1.81 297.67	S 89.2 8.0 4.7 +3.3 98.3 8.5 8.5 +0.4 89.2 8.5 8.5 +0.4 N 89.2 8.5 8.5 +0.4	91.2 9.3 8.1 +1.0 91.2 9.3 8.1 +1.0	90.6 9.6 8.1 +1.5 90.6 9.6 8.1 +1.5	90.0 10.2 8.6 +1.6 90.0 10.2 8.6 +1.6	89.4 10.4 8.8 +1.6 89.4 10.4 8.8 +1.6	88.8 10.4 8.8 +1.6 88.8 10.4 8.8 +1.6	88.2 10.4 8.8 +1.6 88.2 10.4 8.8 +1.6
305.64 1.2 306.86 9.10 297.76 12.24 297.54 8.5 298.71 10.70 288.01 1.00 292.59 3.27 295.86 1.81 297.67	S 88.8 8.1 4.7 +3.3 97.9 8.0 8.0 +0.4 88.8 8.1 8.1 +0.4 N 88.8 8.1 8.1 +0.4	91.2 9.3 8.1 +1.0 91.2 9.3 8.1 +1.0	90.6 9.6 8.1 +1.5 90.6 9.6 8.1 +1.5	90.0 10.2 8.6 +1.6 90.0 10.2 8.6 +1.6	89.4 10.4 8.8 +1.6 89.4 10.4 8.8 +1.6	88.8 10.4 8.8 +1.6 88.8 10.4 8.8 +1.6	88.2 10.4 8.8 +1.6 88.2 10.4 8.8 +1.6

PC on drop frame

288.30 = PC curve

287.40 End curve

OLIVE ST

	N 06	S 06
-39.01 = EL Cooper	295.0	295.00 = R.
0+00 = PT ON SL	295.16	294.60
+50	295.37	294.90
1.	295.59	295.25
+50	295.80	295.57
2	296.02	295.90
+50	296.23	296.20
3	296.45	296.55
+50	296.66	296.87
4	296.88	297.20
+50	297.10	297.50
5	297.32	297.85
+40.17 = PC NL	297.50	298.11
+68.09 = A. SL		298.30

1/4 = 0.0043%
 7/8 =

296.80
295.80
303.86

N	95.0	95.4	95.6	95.8	96.0	96.2	96.5	96.7
	8.7	5.5	8.3	8.1	7.9	7.8	2.4	7.0
	7.0	6.7	6.3	6.0	5.8	5.8	6.4	6.6
	+1.5	+1.8	+1.0	+1.9	+2.0	+1.5	+1.1	+0.6
S		94.8	95.0	95.5	95.8	96.1	96.5	96.8
		8.1	8.7	8.5	8.1	7.8	7.1	7.1
		8.8	7.4	8.1	7.0	7.0	2.1	6.6
		+0.8	+1.3	+1.3	+1.1	+0.6	+0.3	+0.5
N	96.9	97.1	97.3	97.5	97.7			
	7.0	6.5	6.6	6.4	6.2			
	6.9	6.5	6.1	5.8	5.6			
	-0.4	+0.2	+0.5	+1.6	+2.0			
S	97.1	97.4	97.7	98.1	98.3	98.5		
	6.8	6.5	6.2	5.8	5.6	5.4		
	7.4	6.2	6.1	6.2	6.2	5.9		
	-0.6	-1.9	-1.9	-0.4	+1.2	+1.5		
N	97.50 = PC OLIVE	97.70	97.80	97.80	97.80 = EC. 80V			
	7.0	6.8	6.7	6.7	6.7			
	7.0	6.8	6.7	6.7	6.7			
	+1.7	+1.9	+1.3	+1.5	+1.7			
S	98.00 = PC OLIVE	98.10	98.10	98.10	98.10			
	6.8	6.8	6.8	6.8	6.8			
	6.8	6.8	6.8	6.8	6.8			
	+1.0	+1.0	+1.0	+1.0	+1.0			

	NE CB	SW CB
-39.01		296.34
0+00 = P.C. on EL	296.70	296.20
+50	296.48	295.77
1	295.86	295.23
+50	295.45	294.76
2 + 04.98 N/O L.V.	295.0	294.22
+75.85 P.C. SL "	294.11	293.56
3 + 25.85	293.45	293.09
+75.85	292.79	292.62
4 + 25.85	292.14	292.15
+74.46 = P.C. = Sec A	291.50	291.70
Sec B	291.25	291.50
0+00 = E.C. = Sec C	291.40	291.30
+50	291.17	291.07
1	290.95	290.75
+50	290.70	290.47
2	290.48	290.20
+50	290.25	289.93
3	290.03	289.66
+54.04 = BREAK	289.79	289.37
+74.04 = P.C.V.C.	289.83	289.38
+94.04	290.13	289.68
4 + 14.04	290.69	290.27
+34.04	291.51	291.14
+54.04	292.60	292.29

291.00
6.50
300.50

291.00
5.50
304.80

296.20
13.71
337.91
16.0

294.00
10.66
98.66

14.0
4.26

13.50
7.36

297.11 x
15.50
294.91
16.25
301.66

W	96.6	96.4	96.0	95.5	95.0	94.5	93.5	93.3	92.9
	5.3	6.5	6.9	7.4	7.9	8.4	9.1	9.6	10.0
	5.2	6.0	6.7	7.0	7.8	8.9	10.3	10.6	11.0
	+1.0	+0.5	+0.7	+0.1	+0.1	-0.5	-1.7	-0.5	-1.0

E	97.0	96.5	96.1	95.7	95.2	94.4	93.7	93.0
	5.7	6.4	6.3	7.2	7.7	8.5	9.2	9.9
	2.0	3.7	4.4	5.3	6.4	7.5	8.5	9.5
	+2.0	+2.7	+2.7	+1.7	6.4	11.0	11.0	11.0

W	92.4	92.0	91.7	91.5
	10.5	10.9	11.4	
	12.0	12.0	12.1	
	-1.5	-1.7	-0.7	

E	92.4	91.75	91.7	91.65
	10.5	11.7	9.0	
	7.0	9.0		
	+1.1	+1.6		

E	91.6	91.4	91.2	90.9	90.7	90.5	90.3	90.0	90.1
	5.8	6.0	6.2	6.5	6.7	6.9	7.1	7.4	7.3
	4.0	3.9	3.3	3.9	3.5	3.5	3.6	3.7	3.7
	+1.2	+2.4	+2.9	+2.6	+3.2	+2.0	+3.5	+0.3	+3.7

W	91.5	91.3	91.0	90.7	90.4	90.2	89.9	89.6	89.6
	5.9	6.1	6.3	6.7	7.0	7.2	7.5	7.8	7.8
	4.0	5.2	5.7	6.9	6.9	5.4	5.9	7.2	7.8
	+0.2	+0.7	+0.7	+1.5	+2.1	-1.2	+1.6	0.0	-2.0

E	90.4	90.9	91.7	92.5	94.2	96.3
	7.0	6.5	5.7	4.6	3.2	7.1
	1.0	6.2	5.0	3.8	2.3	0.0
	-3.0	+0.3	+0.7	+0.8	+0.7	+1.1

E C B W C B

4 + 74.04 = ECVC 293.96

5 + 02.56 = PC on North 296.04

5 + 47.58 = 17. Middle Curve 297.66

5 + 57.18 = EC w/L Boundary 299.30

5 + 74.58 = P.C. 299.00 opp. P.I.

5 + 57.18 = 299.50 w/L Boundary

W	89.9	90.5	91.1	92.5	94.0	99.2	99.7
	7.8	6.9	6.0	7.9	3.2	2.5	2.0
	15.3	14.5	9.8	7.3	5.2	3.7	2.4
	-7.5	-7.5	-3.8	-2.4	-2.0	-0.6	-0.4

REDWOOD ST

	N 66	5 66	
EL Felton = 0200	313.25	312.50	
+50	313.44	312.67	
1 717 = BREAK W/ ALLEY	312.59	312.84	
+50	313.65	312.90	
2	313.14	312.30	
3	311.30	311.40	
+50 = W/ Gregory	311.50	310.50	
4 = EL "	311.0	310.0	
+50	310.50	309.50	
5	310.0	309.0	
+50	309.50	308.50	
6 +50 = PC 06	309.0	308.0	
+50 = W/ McKinley	308.50	307.50	
7 = EL "	307.50	306.50	
+60	302.67	301.26	
7 + 20	297.83	296.03	
W/ Boundary out.			
+80.30 = BREAK	293.0	291.0	
W/ Boundary south			
EL Boundary at RT. Angles	292.0	290.0	at right angle with SW. cor.
N/ Redwood produced	291.45		

3130 Redwood + Felton W/ WAD

3130							
316.04	N	13.65	13.5	13.90			
10.68							
305.36							
127.3							
145.70							
127.7							
255							
145.70							
127.9	S	13.1	13.15	12.5	11.6	10.70	
3.1							
3.3							
-0.7							
11.4	N	10.7	10.2	09.7	09.2	08.7	07.7
5.3							
5.3							
-0.5							
10.2	S	09.7	09.2	08.7	08.2	07.7	06.7
5.8							
5.8							
+0.4							
02.9	N	95.0	93.2	91.7			
13.1							
10.2							
+2.4							
21.5	S	96.4	91.7	90.2			
14.5							
11.8							
14.7							
3130							
315							
316.20							
3130							
314.75							
307.50							
4.25							
311.50							
13.25							
278.25							
13.25							
291.50							
305.75	S	12.50	12.90	10.50	10.0	307.50	307.00
2.09							
304.9							
306.37							
306.34							
306.0							
305.6							
305.6	N	3.50	3.10	3.53		307.00	306.70
3.24							
3.31							
3.31							
292.50	S	22.0	21.5	21.0	20.50		
291.7							
292.50							
291.7							

LITTLE FLOWER ST

SL STA.	S CB	NL STA	NCB
WL MC = EC	294.20		297.38
0+00 PC	294.30	0+00	294.90
+51.68	291.70		291.77
1+00.36	289.10		288.65
1+55.04 = PC	286.50	1+54.96	285.53
4° 25' 15" @	285.75	1+69.96 (B)	284.63
8° 50' 30" @	285.01		283.71
13° 15' 45" @	284.25		283.37
17° 41' 00" @ PRC	283.50		283.61
PL 11.29	282.96		284.41
WL Down to by @ = EC	281.88		285.0

1968
 Laurel 6.20
 = PC
 CH = 14.45
 7° 51' 31"
 10 25 39
 18° 20' 25"
 28° 49' 14"
 39° 18' 03"
 49° 46' 52"
 53° 08' 30"

55

30320									
12.55									
290.65									
3.20									
293.85									
13.05									
280.80	N 92.6	95.1	92.0	88.9	85.8	84.9	83.9	83.6	
2.15		8.1	11.2	12.3	17.4	2.9	7.9	10.2	
282.95		5.6	8.7	10.5	13.3	4.6	5.4	4.7	
		+2.5	+3.0	+3.8	+4.1	+4.1	+4.7	+5.5	
	S 94.4	94.5	91.9	89.3	86.7	86.0	85.2	84.5	
		5.7	7.3	4.5	7.1		2.3		
		11.8	12.5	6.2	13.2		2.8		
		-3.1	-7.4	-7.9	-6.2		-10.7		
	N 83.8	84.7	85.2						
	10.0	7.1	5.6						
	3.3	1.7	2.3						
	+6.2	+6.4	+6.3						
	S 83.7	83.2	82.9	82.1					
	0.8		0.0	0.8					
	6.8		8.5	14.3					
	-7.6		-8.5	-11.5					
29051									
324									
29375	N 85.8	84.3	83.7	83.2	83.6	84.4	85.0		
225		7.2	10.0	10.2	7.1		9.3		
296.50									
11.87									
298.37									
	S 84.5	84.0	83.5	83.0	82.5	82.0	81.5		
	7.2	7.0	6.5	6.0	5.5	5.0	4.5		
	N 84.0	83.6	83.8	83.7	83.6	83.6	83.6		
	3.7	8.6	8.6	7.0	7.4				
	S 84.5	84.0	83.5	83.0	82.5	82.0	81.5		
	7.2	7.0	6.5	6.0	5.5	5.0	4.5		
	N 84.0	83.6	83.8	83.7	83.6	83.6	83.6		
	3.7	8.6	8.6	7.0	7.4				
	S 84.5	84.0	83.5	83.0	82.5	82.0	81.5		
	7.2	7.0	6.5	6.0	5.5	5.0	4.5		

McKinley ST

	wob	EC6
-10 = SL Redwood	307.50	
0+00 = PC EL McKinley	307.10	306.0
0+65 BREAK	304.50	303.50
1+25 Break	300.0	299.00
+45 "	298.58	297.59
+50 = PC NL Flower		297.35
+65 "	297.34	LITTLE FLOWER
+85 "	296.76	
2+05 "	295.35	
+10 = PC SL Flower		294.20
+25 Break	294.64	293.68
+45 "	294.05	293.13
+65 "	293.65	292.76
+85 "	293.41	292.57
3+05 "	293.35	292.55
+25 "	293.46	292.70
+45 "	293.74	293.03
+65 "	294.28	
3+68.60 = PC NL Quince		293.60
4+28.60 = PC SL "	295.83	295.14
+78.60	296.97	296.50
5+28.60	298.11	297.87
+78.60 = PC CB radius	299.27	299.23
EC NL Pq/17 ST.	299.39	299.43
NW Con. grade	= 299.50	

56

2905 12.53 303.04 30.71 305.21 1.60 295.71 2.01 297.80 1.74 296.07 2.22 303.30	w/ 07.4 0.7 3.6 2.9 4.0 4.7	04.7 3.6 2.9 4.7	00.2 5.1 5.4 4.7	95.8 9.5 6.0 3.5	97.6 10.7 5.2 12.4	96.5 17.5 13.0 7.0	95.6 2.2 7.2 5.5
296.07 2.22 303.30	E 06.2 2.1 2.1 -2.3	03.7 4.6 2.9 -2.1	99.2 9.1 7.2 +1.4	92.2 10.1 4.6 10.7	97.6 10.7 2.9 10.7	94.4 3.0 5.0 -7.0	93.9 3.9 1.5 1.5
	w/ 96.4 4.9 -1.5	94.3 3.5 2.1	93.9 2.9 5.2 -7.5	93.6 7.2 3.7 +1.5	93.6 7.2 1.5 +2.4	93.7 9.1 6.5 +3.3	94.0 3.5 0.8 +3.8
	E 93.4 4.4 15.7 -12.3	93.0 4.5 15.3 -10.3	92.8 5.0 11.7 -6.7	92.8 7.0 9.0 -4.0	92.9 7.9 8.0 -3.1	93.3 4.5 8.7 -2.2	93.8 4.0 8.5 -8.5
	w/ 94.6 3.7 2.0 +2.7	96.1 7.2 5.6 +1.6	97.2 6.1 4.1 +2.0	98.3 5.0 3.2 +1.7	99.6 3.7 2.5 +0.9		
2905 12.53 303.04 30.71 305.21 1.60 295.71 2.01 297.80 1.74 296.07 2.22 303.30	E 96.7 6.6 5.1 +11.5	98.1 5.2 3.3 +7.4	99.6 3.7 2.2 +0.5				
	w/ 97.38 6.33 10.1	96.76 6.05 10.1	96.4 7.57 5.2 +2.02	95.5 5.19 6.3 +1.85	94.0 8.8 6.0	NL Flower	
	w/ 94.20 9.51	44.0 7.31	45.0 9.71	44.0 9.31	42.0 9.51	SL "	
	w/ 94.64 8.77	95.0 9.5	95.10 10.2	10.2		NL Quince	
	w/ 94.24 8.77	94.80 8.91 3.7 +0.1	94.70 9.01 3.65 +1.36	95.20 8.51 8.5	95.4 8.3	SL "	
	w/ 99.27 3.88	94.4 3.73	97.50 3.65	99.4 3.74	99.30 3.85	West = NW MC Palm	
	Found 99.43 3.74	99.27 3.82	99.1 3.94	99.2 4.04	99.3 4.14		

SEWER CONSTRUCTION
CARRIAGE L Hqts E.C.

M.H. #12=00 248.50
 0+50 249.86
 1 - 251.23
 +50 252.59
 2 253.96
 +50 255.32
 3 256.70
 +46.93 = M.H. #8 258.0
 4 261.41
 +50 264.64
 5 267.84
 +36.54 = M.H. #14 270.20
 +50 271.04
 6 274.05
 +35 276.16
 +73.38 = D.D. M.H. #7 278.50

M.H. #14 to #15

M.H. #14=00 270.20
 +50 277.95
 1 285.70
 +37.5 = #15 M.H. 293.50

M.H. #15 to D.E. #10

M.H. #15=0+00 295.0
 +30 295.50
 +60 = D.E. #10 296.0

272.50
 2.51
 268.39
 11.67
 280.56
 1.21
 279.35
 9.67
 288.94
 0.73
 288.11
 12.13
 300.36
 0.96
 299.40
 6.96
 306.36
 0.70
 305.64

Palm & Felt on
 SW 7' track
 305.6

57

248.50 198.6 512.3 52.59 529.6 55.32
 +11.0 24.54 21.17 14.81 18.44 17.05
 272.50 22.58 9.95 14.93 9.60 5.38
 29.66 41.19 44.83 28.75 13.00
 56.70 258.0 61.41 64.62 67.84 70.20
 15.70 14.40 19.15 15.94 12.74 15.74
 4.20 4.50 11.01 3.65 1.50 7.51
 +11.50 29.87 25.14 12.26 110.92 111.31
 71.02 74.05 76.16 78.50
 17.90 14.87
 6.10 10.30
 +11.50 44.57

270.20 277.95 85.70 291.50 DE #9
 +11.21 22.41 17.66 14.86 295.50
 11.25 6.16 5.56 10.56
 +11.22 14.50 19.36 6.21
 295.50 296.0 = DE #10 296.5
 10.86 10.36
 +5.8 5.26
 15.81 15.10

M.H. #15 to D.E. #9
 = 00

0+10 = DE #9 295.0
 295.5

SEWER CONSTRUCTION /
CERRAJO HATS. EV

MH #12 to MH #11 to DMH #10
 MH #12 = 0100 248.50 = EN. ON STUD 259.50
 0 + 36.53 264.0
 0 + 73.07 = MH #11 275.50
 1 + 19.3 277.83
 + 65.53 280.7
 2 + 11.75 = DMH #10 282.20
 ✓ ✓ ✓ ✓ ✓ 285.50

244.00
 6.32
 244.36
 13.08
 281.48
 0.98
 282.46
 13.05
 269.18
 3.32
 272.40
 12.90
 259.50
 9.77
 269.77
 1.00
 268.77
 13.00
 281.77
 1.10
 280.17
 11.46
 291.63

M.H. #12 to M.H. #13
 MH #12 = 0100 248.50
 0 + 40 = BREAK 250.0
 0 + 50 263.10
 1 + 20 = BREAK 276.20
 1 + 48 276.44
 1 + 76 = Δ PT 276.68
 2 276.88
 + 50 277.30
 3 277.74
 + 31 = M.H. #13 278.0

298.27
 10.63
 287.74
 3.75
 291.49

248.50 262.0 275.50 278.25 281.7 282.20
 23.90 20.26 18.86 16.53 14.19 12.16
 12.90 10.81 13.08 7.16 4.65 3.45
 +11.00 29.45 +5.78 +9.37 +9.54 +9.71

248.50 250.0 63.10 76.20 76.44 76.68
 +11.0 19.07 18.14 15.53 15.19 14.95
 12.00 8.89 9.69 3.86 1.85
 +6.67 +9.30 +5.74 +11.33 +12.17

282.20 280.17 277.83 275.50
 16.77 18.20 20.54 15.99
 3.75 3.26 10.63 10.15
 291.49 29.94 29.91 25.81

285.50
 8.86
 3.45
 46.41

58

= Dros

Redwood Sewer CONSTRUCTION
+ McKinley 31498

	Elev.	Grade	
High NE Redwood = 00	5.60	309.38	303.80 + 5.58
0+30 MH #1	6.16	308.82	303.30 + 5.52
0+80.17	6.21	308.77	302.70 + 6.07
1+30.37	7.20	307.78	302.10 + 5.68
1+80.50 MH #2	8.09	306.89	301.50 + 5.39
2+38	10.07	304.91	299.25 + 5.66
2+45.50 DMH #3	12.51	302.47	297.00 + 5.47
" " " " Drop 302.95	"	302.47	288.60 + 13.87
3+48	5.49	298.46	288.25 + 10.21
4+00.50 MH #4	8.92	295.03	287.90 + 7.13
4+55.15	11.49	294.46	287.67 + 6.79
5+09.10	11.82	294.13	287.45 + 6.68
5+64.45	11.22	294.63	287.22 + 7.41
6+19.10 = MH #5	10.15	293.80	287.00 + 6.80
31.43			286.84
22.00			286.68
			286.53
			286.37
			286.21
			286.06
8+39.10 DMH #6			285.90
			285.62
			285.35
			285.07
			284.80
			284.53

con. p 63

31301 NWBP
197 Redwood + Felton
31498
12.51
302.47
1.48
303.95
12.44
290.76

MH #5					
7.23	287.00	86.84	86.68	86.53	86.37
7.24	16.17	16.33	16.49	16.64	16.80
7.25	303.46	8.90	7.85	2.08	5.68
		17.53	45.66	17.56	17.14
		86.21	86.06	85.90	85.75
		16.94	17.11	17.27	17.42
		4.85	4.85	5.00	5.15
		+12.01	+12.23	+12.44	+12.66
		85.07	84.80	84.53	84.26
		18.10	18.37	18.64	18.90
		5.95	6.25	6.53	6.80
		+72.15	17.74	+11.21	

Sewer Construction
B.I.K.H. to D.E.

Carriaf. Hgts

60

DMH. #	3 = 00	303.95		Grades	
0+50		1.30	302.65	288.95	+13.87
1		2.40	301.55	289.30	+14.75
450		3.61	300.34	289.65	+10.69
4 = DE #1		6.67	297.48	290.00	+7.28

Sewer & Little Flower ST

M.H. #	4 = 00	303.95		Grades	
0+45		10.75	293.40	288.25	+4.95
0+90 = DE #2		14.85	291.10	288.60	+4.50

Sewer & Service ST

M.H. #	5 = 00	303.95		Grades	
0+51.67		10.15	293.80	287.00	+6.80
1+03.33		10.03	293.94	287.25	+6.67
1+55		8.85	295.10	287.50	+7.60
2+06.67		8.35	295.60	287.75	+7.85
2+58.33		8.28	295.67	288.00	+7.67
3+10 = DE #3		9.65	294.30	288.25	+6.05
		11.41	292.54	288.50	+4.04

303.17
287.25
15.92
9.15
4.77

Cooper Sewer Line

294.0
293.0
298.27

61

R.M.H #10=00

285.50 = flow from North

285.50	822.0	824.5	827.1	829.6	832.2	834.8
14.83	16.17	15.47	15.06	15.41	15.15	12.89
	7.00	7.41	7.84	8.45	8.57	8.66
	19.17	15.51	17.87	17.16	16.58	16.73

" " " Drop

282.20 = " ENT

40 E

282.45

837.4	284.0	284.31	284.63	284.94	285.26
14.63	14.37	14.06	13.74	13.43	13.11
890	887	10.28	9.89	9.17	7.00
15.73	15.50	+3.78	+4.21	+4.76	+6.11

80

282.71

120

282.96

845.8	849.0	285.00	846.6	846.2	848
14.77	14.47	12.87 = MH #10	12.31	11.75	11.19
2.37	0.43	7.00	6.79	5.97	5.00
+9.02	+12.04	+5.87	+5.54	+5.78	+5.69

160

283.22

200

283.48

877.4	285.20
13.63	10.07 = MH #9
5.10	2.21
+5.53	+5.65

240

283.74

280 = MH #17

284.00

294.04	86.00	85.58	85.27	84.15
913	17.37	17.59	17.30	17.07
303.17	9.00	8.69	9.00	8.19
	+5.67	+5.90	+5.76	+5.30

326.11

284.31

372.22

284.63

418.33

284.94

464.44

285.26

510.55

285.58

556.66 = DE #7

285.90

Cooper Sewer to Olive

DMH #10=00

285.50

286.06

286.62

287.18

287.74

50 MH #9 to Olive

288.30

288.58

288.87

289.15

50/0

Cooper + Olive Sewer

30317

1	289.44
2	289.72
3	290.01
4 = MH #16 @ Olive E of Cooper	290.30
5	290.57
6	290.84
7	291.11
8	291.38
9	291.65
10	291.93
11 = DE #6	292.20

Sewer thru BIK G

#13 MH = 0+00	278.00
46' N	280.18
96'	282.36
1+10	284.54
1+92 = A	286.73
1	288.84
26.3' N	290.95
15.73	293.00
= DE #8	
# Nut req to A pt	
MH #13	278.00
51.67	277.58
51.67	277.15
15.5' = 3' A pt.	276.72
215' E = BREAK	276.40

89.22	89.74	90.01	MH 16	90.30	90.57	90.84
13.73	13.45	13.16	12.87	12.60	12.33	12.06
7.65	7.37	7.08	6.81	6.54	6.27	6.00
+6.09	+5.59	+5.09	+4.59	+4.09	+3.59	+3.09
91.1	91.38	91.65	91.93	92.20	92.47	92.74
12.06	11.79	11.52	11.24	10.97	10.70	10.43
7.10	7.07	6.50	5.93	5.36	4.79	4.22
+4.96	+4.72	+4.02	+3.37	+2.72	+2.07	+1.42

30559

27.66	28.00	28.15	28.36	28.54	28.73	28.84
1.81	16.47	14.79	13.53	11.05	15.86	16.75
27.44	27.0	29.1	12.93	11.33	10.20	9.06
+6.77	+12.35	+10.38	+9.72	+8.66	+7.79	+6.92
22.85	23.00	23.58	24.15	24.48	24.80	25.12
14.64	12.59	16.89	17.34	17.79	17.79	17.79
6.36	7.09	6.80	6.80	6.70	4.67	4.67
+6.25	+5.50	+4.95	+4.62	+4.06	+3.51	+2.96

Palm St Sewer from page 57

6
 7-DDMH#7
 200 = " " " " " "
 5 d. 5
 105 West = DE#5

287.25
 283.98
 290.00
 290.35
 294.70

McKinley + Palm = DMH #6 EAST to DE#4

1
 2
 3
 4
 5
 6
 7 = DE#4

289.00
 290.01
 290.43
 290.84
 291.25
 291.67
 292.08
 292.50

303.6
 3.10
 300.36
 7.25
 307.61
 1.94
 305.67
 3.55
 303.71
 287.60
 13.57
 1.20
 28.57
 92.28
 11.69
 6.42
 4.61

2850 = Cotton Flow Line
 78.96
 7.54
 71.54
 DMH 7
 283.98
 19.48
 7.25
 17.00
 290.01
 13.16
 4.61
 8.55
 92.50
 10.67
 8.45
 2.22
 290.00
 92.35
 73.46
 1.20
 46.24
 290.43
 12.72
 4.61
 28.07
 90.84
 72.33
 5.23
 47.10
 91.25
 11.72
 5.34
 +6.60
 292.70 = DE#5
 8.76
 3.10
 5.66
 91.67
 11.50
 5.43
 2.57

1/24/46
Moore

ALLEY PAVING BIK 44 CITY HQTS

20' wide

WENTHROP ST
NW DP

	W	E
		352.57 7.30 <u>357.76</u>
Sl Polk - 20	361.0	361.30 <u>356.82</u> 5.89
+40	361.20	361.50 <u>362.71</u> 1.67
+60 = BREAK	361.40	361.70 <u>358.04</u> 4.82
120	361.07	361.37 <u>362.86</u> 3.23
160	360.74	361.04 <u>359.63</u> 6.78
200	360.40	360.70 <u>366.41</u> 6.55
240	360.07	360.37 <u>361.86</u> 0.82
280	359.73	360.03 <u>365.70</u>
320 = BREAK	359.40	359.70
360	359.18	359.42
400	358.94	359.15
440	358.71	358.87
480	358.48	358.60
520	358.25	358.33
560	358.03	358.05
600 = N. V. ST	357.80	357.78

	W	E	W	E
	361.0	61.20	61.40	61.07
	4.70	4.50	5.01	5.24
	2.70	3.28	4.01	4.99
	0.0	1.22	1.0	10.24
				10.24
	61.30	61.50	61.70	61.37
	4.10	4.70	4.71	5.02
	1.40	1.06	4.58	4.79
	0.0	10.10	10.12	10.24
				10.24
	60.07	59.73	59.40	59.18
	6.24	6.68	7.01	5.94
	6.24	6.57	6.87	3.68
	0.0	-0.19	+0.12	3.43
				10.24
	60.37	60.03	59.70	59.40
	6.04	6.38	6.71	3.44
	5.0	6.68	6.63	3.60
	11.0	-0.30	+0.05	10.78
				10.78
	58.48	58.25	58.03	57.80
	4.38	4.61	4.68	3.94
	4.38	4.76	4.76	3.71
	0.0	-0.18	1.22	4.07
				10.24
	58.60	58.33	58.05	57.78
	4.26	4.53	4.66	3.94
	3.29	4.34	3.06	3.71
	10.37	10.19	11.0	4.07
				10.24

11/10/66
Muro

WIGHTMAN ST Grados NEMAN

	N 66	338.55	338.55
		6.60	345.15
E.L. Parshing	338.0	7.40	338.01 BP
50 E	340.25	11.20	349.03
100 - BREAK	342.50		
151.87	343.0		
203.73	343.50		
255.5 = w/L 2547	344.0		

3380 / BM
2.29
340.30

Break 6.75 w/L w/L Parshing 333.55
7.15

332.90
6.40

W. & Oregon

W. Wightman + Parshing

N	335.0	40.50	42.7	43.2	43.7	344.0
		8.5	6.3	5.4	5.3	5.0
		8.6	5.6	4.6	3.8	
		11.9	20.7	11.2	11.5	
S	339.0	41.2	43.4	43.2	43.6	345.0
		7.8	5.8	5.6	5.1	5.5
		6.2	3.9	4.6	4.1	5.2
		11.6	11.4	11.0	11.3	11.3
N	347.0	40.50	42.7	43.4	43.7	
		6.5	4.2	3.3	3.3	
		4.5	3.5	2.7	2.7	
		7.0	7.7	6.0	5.7	
S	341.0	41.2	43.4	43.4	43.6	
		5.8	3.8	3.4	2.4	
		4.1	1.9	2.1	2.1	
		7.7	1.9	2.1	2.1	
N	338.0	40.50	42.50	42.7	43.0	43.1
		9.1	8.8	4.4	4.3	4.1
				4.4	3.6	3.0
				4.4	3.6	3.0
				4.4	3.6	3.0
				4.4	3.6	3.0
S	339.0	41.0	43.0	43.0	43.0	43.0
		4.0	4.0	4.0	4.0	4.0
		4.0	4.0	4.0	4.0	4.0
		4.0	4.0	4.0	4.0	4.0
		4.0	4.0	4.0	4.0	4.0
N	344.0	43.4	44.0	43.4	43.4	43.4
		3.6	3.7	3.6	3.6	3.6
S	343.7	43.7	43.7	43.7	43.7	43.7
		3.6	3.6	3.6	3.6	3.6

38th St Grading
Woolman North

Moore 80' wide
12/2/26. 20 cbs

17th SE of Hyd
Woolman road

66

	WCB	ECB
		17.00
		0.07
		17.07
11 Woolman	14.50 11	15.00 14
		13.75
		16.47
		3.78
		17.05
		4.00
0 + 40	14.00 1.79	14.58 1.91
		7.01
		20.39
0 + 60	13.20 1.55	13.86 0.63
0 + 80	11.57 5.90	12.23 5.26
1	9.40 8.07	10.17 7.31
+ 20	7.63 9.66	8.49 9.00
+ 40	6.58 10.91	7.53 11.66
+ 60	6.50 10.99	7.36 10.03
+ 80	7.37 10.5	7.95 9.54
2	9.00 8.49	9.28 8.71
+ 20	10.40 9.05	10.64 8.85
+ 40	11.25 6.26	11.25
3	11.97 5.00	
+ 50	12.57 1.91	
4	13.18 1.31	
+ 50	13.78 6.61	20.39
5	14.39 0.01	
+ 50	15.00 5.39	
6 = Slatlev	15.60 1.99	
+ 70 = NL "	15.84 1.55	
+ 60	16.31 4.08	
7	16.80 3.59	
+ 50	17.40 1.99	
8	18.00 1.39	18.00

17.65	W 14.50	14.47	13.50	11.50	9.67	7.58	6.53	6.75
7.64		7.11	5.15	6.83	7.0	10.8	11.5	11.9
11.04		4.1	5.0	6.5	1.0	5.6	11.5	11.7
7.15			0.6	0.0	+0.6	+1.2	0.0	+0.7
15.19								
1.77								
16.47								
3.78								
17.05								
4.00								
17.00	E 15.00	14.83	14.11	12.48	10.40	8.74	7.78	7.61
3.65		3.8	7.5	6.2	5.0	7.7	10.7	11.0
17.00		2.5	3.1	8.1	7.4	7.0	9.0	11.3
4.80		+1.3	+1.0	-1.9	+0.8	+1.9	11.9	-0.7
	W 7.60	9.25	10.50	11.50	12.00	12.50	13.00	
	11.0	7.9	7.8	7.1	6.4	5.8	5.2	
	7.2	6.9	5.9	5.6	5.0	5.0	5.0	
	15.8	11.5	11.9	+1.5	+1.0	+2.2	-0.3	
	E 8.50	9.53	10.59	11.50	12.00	12.50	13.43	
	10.4	9.1	7.8	6.7	6.0	5.4	4.8	
	8.4	5.0	7.6	6.9	6.0	4.8	3.9	
	+1.5	+1.1	+0.2	-0.2	-1.0	+0.6	+0.9	
	W 14.03	14.64	15.25	15.85	16.09	16.56		
	4.2	3.6	3.0	2.4	2.1	1.7		
	4.0	4.6	5.7	5.3	3.5	2.9		
	-0.6	-1.0	-1.7	-1.3	-1.4	-0.9		
	E 14.03	14.64	15.25	15.85	16.09	16.56		
	4.2	3.6	3.0	2.4	2.1	1.7		
	4.0	4.6	5.7	5.3	3.5	2.9		
	-0.1	-1.0	-1.7	-1.3	-1.4	-0.9		
	W 17.05	17.65	18.25					
	4.2	3.6	3.0					
	3.4	3.2	2.5					
	+0.8	+0.4	+0.5					

ALLEY PAVING
BIX 141 CITY Hgts rowide

Moore
1949

	W	E
SLVWV Ave	359.95	360.05
0+60	359.50	359.60
0+80	359.10	359.16
1+00	358.67	358.74
1+60	358.25	358.28
2+00	357.84	357.84
2+40 BREAK	357.40	357.40
2+85	357.05	357.05
3+30	356.70	356.70
3+75	356.35	356.35
4+20 BREAK	356.00	356.00
4+60	355.20	355.20
5+00 BREAK	354.40	354.40
5+20	353.60	353.60
5+40	352.33	352.40
5+60	350.50	350.60
5+80	348.00	348.20
6+00 NW Wightman	345.30	345.60

Wightman & Swift

NWBP

337.4
11.62
1160 = 0.00 error

Wightman & Swift
NWBP

358.86	359.45	359.50	359.10	358.67	358.25
6.00	7.93	5.36	5.78	6.71	6.63
364.86	✓	4.36	5.34	6.25	6.46
6.51		5.26	2.04	0.04	10.17
358.37					
3.14					
361.77		359.60	359.16	358.74	358.28
5.89	4.83	5.28	5.74	6.16	6.60
365.80		4.28	5.14	5.04	6.00
2.83		7.30	10.58	10.31	10.63
358.73					
12.13					
346.60					
3.14					
349.04					
W 357.84	357.40	357.05	356.70	356.35	356.00
7.06	2.58	4.74	5.09	5.44	5.79
6.70	7.5	4.90	5.25	5.50	6.20
10.36	0.06	-0.16	10.07	0.06	-0.07
E 357.84	357.40	357.05	356.70	356.35	356.00
7.04	7.28	6.74	5.09	5.44	5.79
6.31	7.60	3.74	4.71	4.50	5.21
10.72	-0.17	11.0	10.38	10.61	10.85
358.86	358.20	357.40	356.60	355.80	355.00
6.00	3.83	4.33	5.13	6.23	5.93
364.91	4.06	4.94	5.60	6.21	6.21
1.40	-0.33	-0.12	10.77	10.33	11.01
357.84					
6.70					
E 357.84	357.40	357.05	356.70	356.35	356.00
6.75	3.53	4.33	5.13	6.33	5.13
357.84	2.74	3.26	4.22	4.91	5.51
357.84	10.34	10.47	10.65	10.84	11.61
357.84					
357.84					
W 348.00	345.30	set back	345.45		
10.73	3.78		3.79		
6.88					
358.86					
5.58					
348.86					
7.16					
E 348.20	345.60				
357.48	10.53	3.44 set back			
5.40	5.23				
360.68	11.70				

Restaked 3d time 5/10/47

Alloy v20 Univ. Hgts 20 wide
Cont. Hansen

28000 JEBF
Richardson

68

EL VERMONT = 00 279.55 (out bearing) 279.63 ✓
 0 + 40 BREAK 280.70 280.70
 0 + 90 280.90
 1 + 40 281.10
 + 90 281.30
 2 + 40 281.50
 + 90 281.70
 3 + 40 = BREAK 281.90 281.91
 + 33.33 282.53
 4 + 26.67 283.17
 4 + 70 = BREAK 283.50 283.50
 5 + 13.33 283.10 283.00
 + 56.67 282.40 282.21
 6 + 00 = WLT Richardson 281.71 281.72

28000
2771
287.75
3.51
280.70
2.45
286.37

S 279.55 280.70 280.90 281.10 281.30 281.50
 6.84 5.69 5.49 5.29 5.09 4.89
 5.50 5.22 4.95 4.67 4.40 4.13
 +0.17 +0.15 +0.08 +0.74 +0.25

N 279.63 5.69 5.49 5.29 5.09 4.89
 6.76 5.50 4.75 4.51 4.25 4.01
 +0.13 +0.11 +0.08 +0.14 +0.11 +0.08

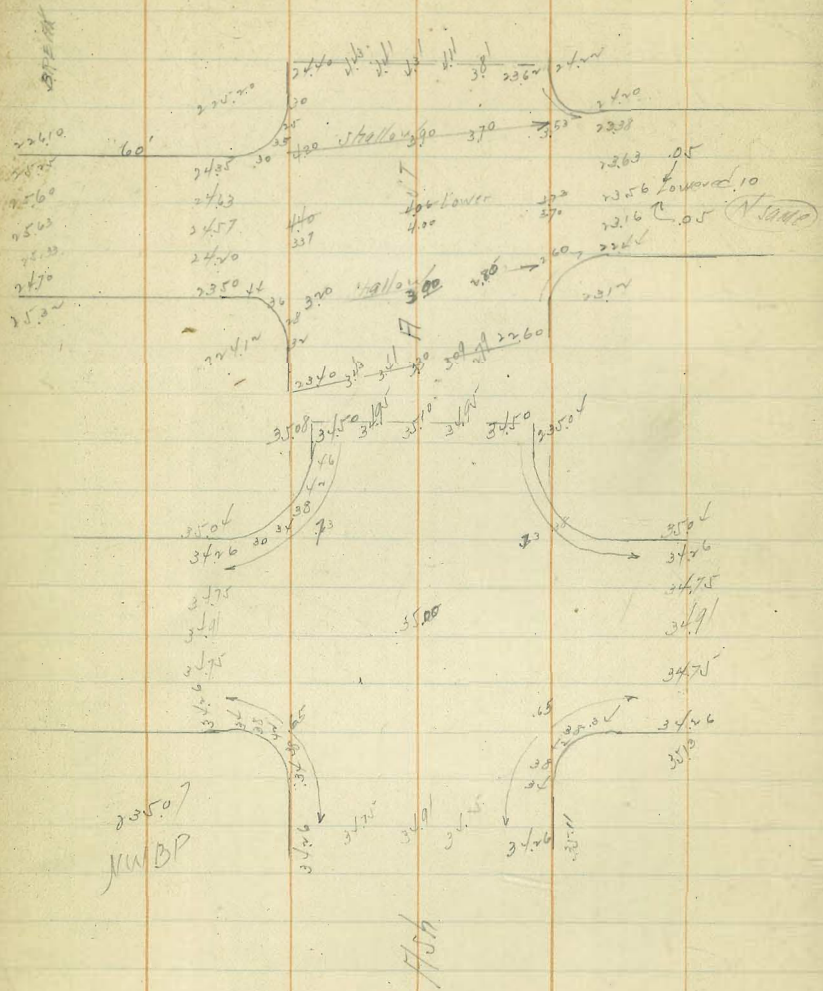
S 281.70 281.90 282.53 283.17 283.50
 4.69 4.49 3.86 4.18 3.95
 4.97 4.63 4.80 4.10 3.70
 -0.30 -0.14 +2.0 +0.45 +0.15

N 4.69 4.49 3.86 283.17 283.50
 4.86 4.55 3.55 3.22 3.95
 -0.17 -0.06 +0.31 +0.00 +0.10

S 283.10 282.40 281.71
 4.65 5.35 6.04
 3.92 5.11 5.73
 +0.67 +0.34 +0.31

N 283.00 282.21 281.72
 4.75 4.54 6.33
 4.01 4.00 6.24
 +0.11 +0.09 +0.07

3 1/2" PAVING 8" CROWN
B. to Beech Sts

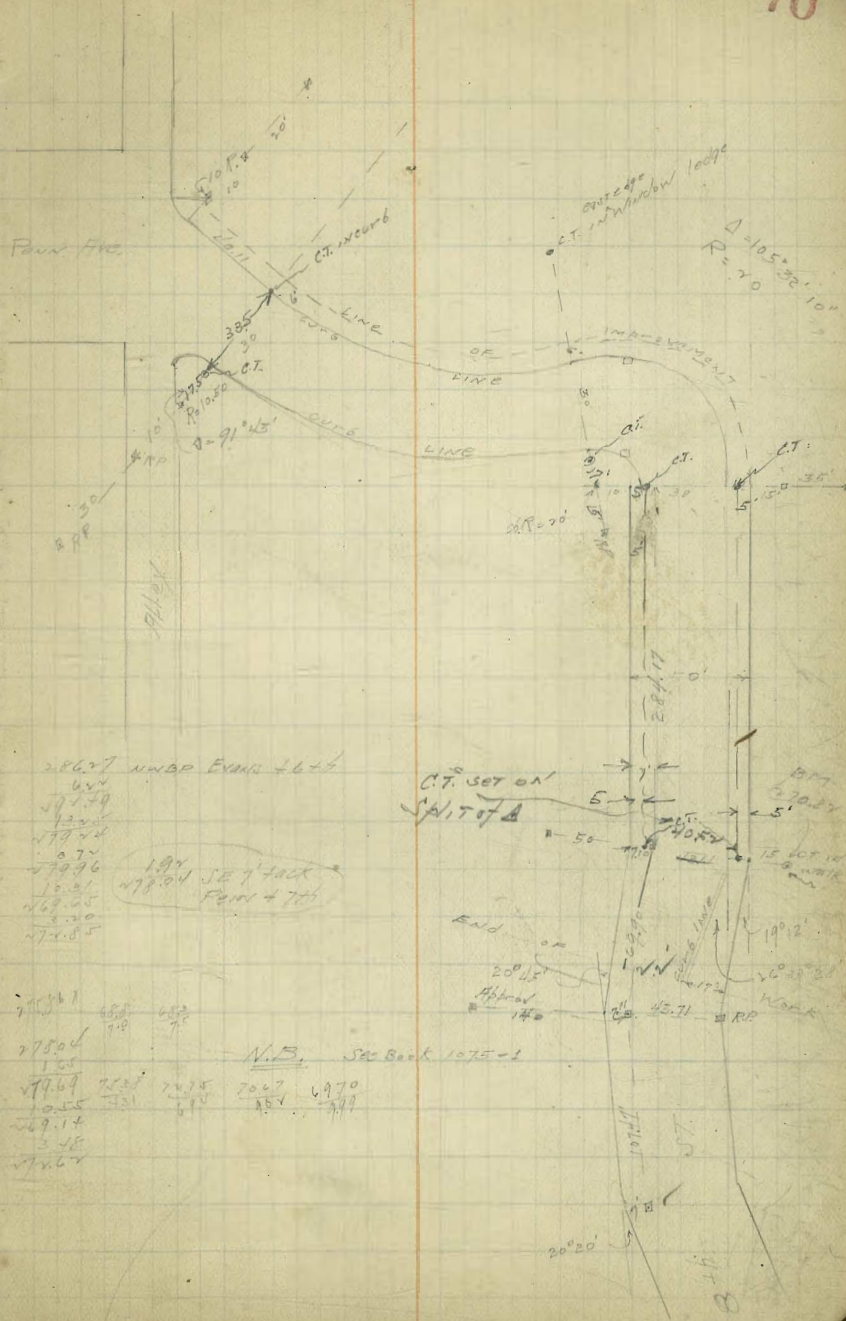


22466 SE A + Grove
410
22876

8th & PENN. AVE.
Grading & Paving

Mooring
12/19/12

	Sc6	N 06
EL 74 = 0400	278.00	278.00
0+50		275.38
1		277.75
+40 = ELLATED	269.50	270.67
+86 = P.C.	269.13	269.70
		268.60 V
1	268.93	268.48
2	268.74	268.36
3	268.55	268.24
4	268.36	268.11
3+07.8 = 5 P.R.C.	268.17	268.00
+228 = 66 m/pt #1 = EL 8th	268.00	267.50
1		267.76
2		268.03
3		268.30
4		268.56
103 = 1st set #5 = EL	268.33	268.83
N 2780	75.6	70.9
	7.3	8.7
	6.6	9.1
	7.1	8.1
	6.8	8.1
S 1	69.0	69.0
	6.5	6.5
	5.4	5.4
	4.1	4.1
	3.3	3.3
	2.3	2.3
	1.6	1.6
N 68.3	68.7	67.7
	4.6	4.6
	4.8	4.8
	3.1	3.1
	2.6	2.6
	2.5	2.5
S 68.5	68.3	68.3
	4.6	4.6
	4.8	4.8
	3.1	3.1
	2.6	2.6
	2.5	2.5



286.27	UNAD	EVANS	± 6.2
6.4			
77.29			
12.2			
17.24			
0.72			
77.96			
12.2			
16.25			
3.20			
77.05			
77.267	68.2	68.2	
77.500			
77.69	70.7	70.7	
10.55	73.1	73.1	
269.14	70.2	70.2	
3.48	75.4	75.4	
77.67			

N.S. See Book 1075-1

Plan of Penn. Ave Paving

	W CB	E CB
10.5 of 1/2 8th = EC = 0+00	268.33	268.53
0+40 = BREAK	269.68	270.20
0+90	270.709	271.20
1+40	271.03	271.50
1+90	270.70	271.20
2+40	269.68	270.20
2+84.7 = A on west	268.20	268.50 = BREAK
2+90 = BREAK NOT SET	268.0	266.10 = BREAK
3+40 = " end of work	265.63	265.40 ENDWORK

Culvert #1

	#1	#2
0+00 = Top cb	268.00	
" " " " inlet #1 bottom box	264.50	
0+30 top cb	267.50	
" " " " = cb inlet #2 = lowline	263.50	end of Culk #1
" " " " " " bottom box	255.0	inlet " #2
0+54 = BREAK	242.9	
0+73 = outlet Culvert #2	240.7	

4.94 B.M. on 45' R.P.
70.57 Cap took in walk

	W	68.6	69.9	70.9	71.3	70.9	69.9	68.4	65.9
	7.1	5.3	4.3	4.4	5.8	5.8	7.3	9.3	
	2.6	4.8	4.3	0.0	4.7	5.2	6.5	10.0	
	11.5	10.1	8.6		10.1	10.2	13.8	19.3	
	68.1	70.4	71.4	71.7	71.4	70.4	68.7	65.6	
	10.9	5.3	4.3	4.0	4.3	5.3	7.0	10.1	
		11.5	10.1	8.6	3.2	3.7	5.1	7.0	
		10.8	10.4	10.8	10.6	11.0	11.9	14.5	
	68.3	69.8	70.70	71.03	70.70	69.65	68.20	65.63	
	7.5	6.7	5.16	4.17	4.50	5.54	7.00	9.57	
							6.00	7.57	
							1.00		
	68.3	70.20	71.20	71.50	71.20	70.20	68.50	65.40	
	7.03	5.86	4.80	3.70	4.00	5.00	6.70	9.10	

	265.0	264.50	267.50	263.50	265.0	242.9	240.70
		3.35		9.25	17.85	16.91	19.11
		4.35		13.41	13.51	14.17	17.04
		13.60		22.66	27.37	30.14	36.15

Alley Paving
BIR 48 City Hqts

Restaked
4/27/27
Floors

	W	E
SL UNIV - 00	358.60	358.60
0.451	358.43	358.40
1.	358.25	358.20
+50	358.08	358.0
2	357.91	357.80
+50	357.74	357.60
3	357.57	357.40
+50 = BREAK	357.40	357.20
4	356.78	356.60
+50	356.16	356.0
5	355.54	355.40
+56	354.92	354.80
6+00 = NL Watermain	354.30	354.20

	W	E	W	E	W	E	W	E
35461	5860	5843	5825	5808	5791	5774	5757	
4.59	5.00	5.17	5.37	5.54	5.71	5.88	6.05	
35720		4.19	4.45	4.71	4.97	5.23	5.49	
35721		10.98	-0.08	-5.17	10.20	0.36	10.77	
35722								
35723								
35724								
35725								
35726								
35727								
35728								
35729								
35730								
35731								
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35790								
35791								
35792								
35793								
35794								
35795								
35796								
35797								
35798								
35799								
35800								

ALLEY PAVING BIK 4 20' wide
City Hq's Annex #1

	W	E
SL UNIV = 0200-	357.77	357.62
50	357.56	357.41
1	358.35	357.21
+50	357.14	357.01
2	356.93	356.81
+50	356.72	356.61
3	356.52	356.41
+50	356.31	356.21
4	356.11	356.01
+50	355.90	355.81
5	355.70	355.61
+50	355.50	355.4
6 - 24 Wightman	355.29	355.21

355.33 Wightman
5.31 FAIRMONT
360.64 KNIBP
357.16
361.74
357.81
362.33

	W	E	Moore	Osborn	Flood
	57.77	57.56	57.35	57.14	56.93
	5.56	5.77	5.98	5.19	5.20
		3.77	3.95	3.19	4.74
		4.10	4.10	4.00	4.66
	57.62	57.41	57.21	57.01	56.81
	4.71	4.92	5.12	5.32	5.52
		3.92	4.12	4.32	4.52
		4.10	4.10	4.10	4.10
	56.74	56.52	56.31	56.11	55.90
	5.02	5.22	5.43	5.63	5.84
	4.22	5.10	4.91	5.20	5.57
	40.80	40.12	40.52	40.32	40.92
	56.61	56.41	56.21	56.01	55.81
	5.11	5.33	5.53	5.73	5.93
	4.11	5.01	5.02	3.72	4.52
	4.10	4.22	4.02	4.22	4.11
	55.70	55.50	55.30	55.10	54.90
	4.92	5.12	5.32	5.52	5.72
	4.32	5.12	5.12	5.12	5.12
	40.80	40.80	40.80	40.80	40.80
	55.61	55.41	55.21	55.01	54.81
	5.03	5.23	5.43	5.63	5.83
	4.03	3.23	3.03	2.83	2.63
	4.00	4.00	4.00	4.00	4.00

57.8
57.7
57.6

Alley Paving
 BIK 1 Hartley's N. Park

15' wide

EL RAY	353.79	353.96	
50 E	354.64	354.78	
100 E - WL N & S alley	355.50	355.60	BREAK
115 E - CL "	355.50	355.60	"
165	355.15	355.25	"
215	354.80	354.90	"
270 = WL GRIM	354.49	354.52	

Put slight break
 have out. acct of paving as
 laid on WL GRIM

Wrightman + Ray 11/19
 Swamp

Moore
 Osborn
 Flood

351.64
 8.71
 360.56
 352.32
 360.75

N	53.96	54.78	55.60	55.60
	6.60	5.78	4.90	5.15
		3.01	4.04	3.15
		+2.00	+2.94	+2.00
S	53.79	54.64	55.50	55.50
	6.77	5.94	5.06	5.35
		4.65	4.03	4.32
		+1.24	+1.03	+0.93
N	55.25	54.90	54.52	
	5.50	5.85	6.23	in High connect
	4.75	5.13		
	+0.75	+0.74		
S	55.15	54.80	54.49	of patch put
	5.60	5.95	6.26	in by old Crim
	4.81	5.05		
	+0.79	+0.70		

351.64
 8.71
 360.19

S	53.79	54.64	55.50	55.50	55.15	54.80	54.49
	6.40	5.55	4.69	4.69	4.04	5.39	
			3.76	3.76	3.20	4.23	
			+0.75	+0.75	0.75	0.75	
N	53.96	54.78	55.60	55.60	55.25	54.90	54.52
	6.60	5.78	4.90	4.90	4.94	5.09	
			3.01	3.01	4.04	3.15	
			+2.00	+2.00	2.00	2.00	

ALLEY PAVING
 BIK IN UNIV. HATS 20 in dia

Moore
 08 Board
 Flood
 1/5/27

Mad. + Idaho SEBP

	W	E
14 Adams on paving	385.70	385.70
405	384.71	384.97
60	385.01	384.25
140	383.33	383.53
160	382.60	382.81
200	381.95	382.09
240	381.22	381.36
280	380.57	380.6
320	379.89	379.92
360 = BREAK	379.20	379.20
400	379.03	
440	378.86	
480	378.70	
520	378.53	
560	378.36	
600 N. Madison	378.20	378.20

378.85	85.70	84.71	84.01	83.33	82.60	81.95
378.31	4.37	5.01	5.71	3.43	4.16	4.81
378.08		4.75	5.14	1.83	3.32	4.71
378.78		+0.26	+0.57	+1.60	+0.29	+0.10
378.71	E	85.70	84.97	84.25	83.53	82.81
378.78		4.02	4.75	5.47	3.23	3.95
378.78			5.14	5.22	2.11	4.01
378.76			-0.39	-0.35	+0.11	-0.06
378.76	W	81.26	80.57	79.89	79.20	78.53
378.76		5.50	6.19	6.87	4.71	4.89
378.76		5.78	6.10	6.71	4.48	4.45
378.92		-0.28	+0.09	+0.16	+0.24	-0.21
378.92	E	81.36	80.64	79.92	79.20	78.53
378.92		5.40	6.14	6.84	4.71	4.89
378.92		5.01	5.92	6.05	4.28	5.46
378.92		+0.39	+0.19	+0.19	+0.49	-0.29
378.92	W	78.56	78.70	78.53	78.36	78.20
378.92		+1.0	+1.0	-0.31	-0.10	
378.85	E	78.56	78.70	78.53	78.36	78.20
378.85		5.06				
378.85		5.40				
378.85		-0.24	-0.37	+1.0	-0.10	
378.85	W	85.40	84.71	84.01	83.33	82.60
378.85		3.77	4.46	5.19	3.02	3.74
378.85		4.11	4.81	5.58	2.07	4.10
378.85		+0.22	+0.52	+1.24	+0.27	+0.21
378.85	E	85.70	84.97	84.25	83.53	82.81
378.85		3.47	4.00	4.92	3.46	4.18
378.85		4.22	4.63	5.13	3.36	4.30
378.85		-0.75	-0.21	-0.21	-0.12	+0.78
378.85	W	79.89	79.20	78.53	78.70	78.53
378.85		4.97	5.65	5.22	6.02	4.08
378.85		4.25	4.85	5.23	5.05	4.75
378.85		+0.22	+0.21	-0.23	0.0	0.35
378.85	E	79.89	79.20	78.53	78.70	78.53
378.85		4.96	5.63	5.25	6.01	4.22
378.85		4.20	4.70	5.18	6.08	4.22
378.85		-0.16	-0.29	-0.23	-0.21	-0.11

Restarted 1/5/27 Moore

ALLEY PAVING 20' wide
 BIK 171 Univ. Hqts.

	W	E
Alhambra 11-00	318.60	318.60
0440 BREAK	319.00	319.20
0475	320.25	320.50
1.10 Break	321.50	321.80
"	322.70	322.87
11.5	323.90	323.95
"	325.10	325.02
3400 BREAK	326.30	326.10
"	326.60	326.48
38	326.90	326.86
"	327.30	327.24
"	327.66	327.62
5440 BREAK	328.00	328.00
470	327.80	327.80
6:54 P.M.	326.65	326.65

Mosco
 20' wide
 Flood
 light

32405 Park + Texas
 J.E.C.P.

	W	E	(B)	(B)
32405	334.37	334.37	19.00	20.25
5.16	5.16	5.16	5.10	5.09
318.60	318.60	318.60	4.10	4.09
319.20	319.20	319.20	4.04	4.00
320.50	320.50	320.50	4.00	3.97
321.80	321.80	321.80	4.00	3.94
322.87	322.87	322.87	4.00	3.91
323.95	323.95	323.95	4.00	3.88
325.02	325.02	325.02	4.00	3.85
326.10	326.10	326.10	4.00	3.82
326.48	326.48	326.48	4.00	3.79
326.86	326.86	326.86	4.00	3.76
327.24	327.24	327.24	4.00	3.73
327.62	327.62	327.62	4.00	3.70
328.00	328.00	328.00	4.00	3.67
327.80	327.80	327.80	4.00	3.64
326.65	326.65	326.65	4.00	3.61

0.4

Euclid Grading

UNIV. to EL Cajon

	web	ECB
St. Anna-Polk	345.00	345.00
50' S	343.40	
1	341.80	
450	340.80	
7+00 = BREAK	338.60	338.60
+50	337.40	337.50
3	337.50	337.60
+50	338.00	338.11
J	338.50	338.63
+50	339.00	339.15
5	339.50	339.66
+50	340.00	340.19
6 = VL UNIV	340.50	340.70

340.68
157
34.55

$\frac{313}{10.60} = 29.5$

$\frac{323}{310.70} = 1.04$ web orange on West

W $\frac{337.50}{5.05}$ $\frac{337.40}{5.15}$ $\frac{338.60}{3.85}$

E $\frac{337.60}{5.05}$ $\frac{337.50}{5.05}$ $\frac{338.40}{3.85}$

340.68	6.41								
347.07	12.10								
337.99									
357 WL	45.5	43.65	42.05	40.65	39.85	37.65	37.75	38.55	
	8.5	10.1	11.0	10.1	9.3	8.4	7.8	7.8	
335.20	6.1	10.5	11.6	10.4	9.5	8.5	7.7	7.5	
340.68		6.7	7.4	7.6	7.3	6.7	6.1	5.8	
237						10.7	11.6	12.2	
340.68	45.5	43.65	42.05	40.65	39.85	37.65	37.75	38.55	
	8.5	10.1	11.7	11.0	10.0	9.3	8.4	8.7	
347.07	12.10	12.6	13.2	12.3	11.4	10.4	9.7	9.1	
353.73	16.7	17.3	18.7	17.5	16.3	15.3	14.0	13.1	
351.20 WL	38.75	39.75	39.75	40.25	40.50 = CB				
	8.3	7.8	7.3	6.5	5.4				
	6.3	7.5	6.6	6.1	5.4				
	4.5	5.3	4.9	4.4	4.0				
EL 338.88	39.40	39.90	40.25	40.70 = CB					
	8.4	7.7	7.1	6.5	6.8				
345.80	11.4	10.7	10.0	9.3	8.3				
8.90	13.5	16.4	16.4	15.3	14.3				

77

Total length of cut 137'

228' S = Wedge grading
244' S = S. II CB inlet
close ECB wedge inlet #1 337.65
" " " N " " " " 338.00
" " " N " " " " #2 337.57
" " " N " " " " 338.01

inlet	327.70	325.70	324.45	
	327.00	17.86	14.11	
	11.56	+12.05	0.75	
351.30			+13.86	
220				
353.53	338.01	338.00		
10.53	0.55	0.55		
342.96	0.50	0.50		
342.46	0.54	0.54		

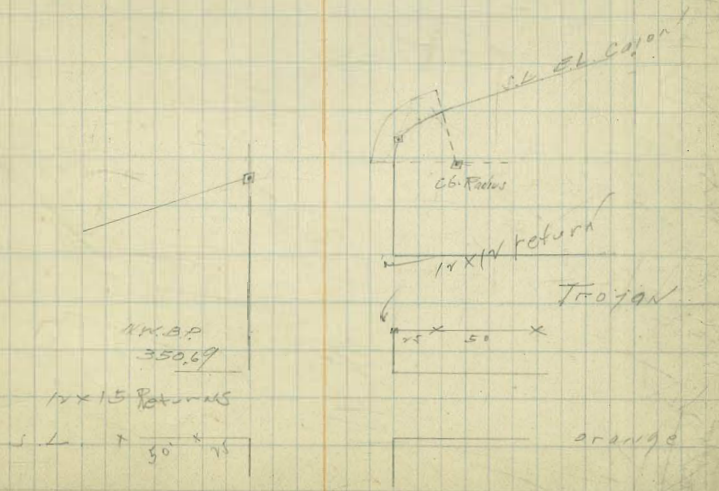


Evold & Paving
Polk to El Cajon

	Wob	ECB
NL Polk	345.50	345.50
50	345.94	345.84
1	346.38	346.19
50	346.82	346.53
50	347.26	346.81
50	347.70	347.22
50	348.14	347.57
50	348.58	347.91
50	349.01	348.26
50	349.46	348.60
50	349.90	348.95
50	350.34	349.30
+ 7756 Orange	350.60	349.50
NL 1000	350.70	349.50
50	350.10	348.91
1	349.54	348.41
50	348.94	347.87
50	348.33	347.33
50	347.75	346.78
50	347.15	346.24
50	346.55	345.70
50	345.96	345.16
50	345.37	344.62
50	344.78	344.08
+ 50	344.19	343.54

35/30
456
35.86
413
30.73
3.27
353.00

W	457	462	466	471	475	479	484	488
	10.1	7.6	7.4	5.7	5.3	7.1	5.4	7.0
	6.2	4.1	3.4	3.3	3.5	3.4	3.0	4.2
	10.1	15.5	15.7	15.4	14.3	14.3	13.5	14.8
F	457	461	464	468	471	475	478	481
	10.1	9.1	7.4	9.0	5.7	5.3	5.0	7.1
	6.2	4.3	3.9	4.0	5.1	7.7	7.5	7.0
	10.1	15.4	15.4	14.0	11.6	10.0	10.5	10.7
W	492	497	501.0	506	50.80	50.9	50.3	49.7
	6.5	6.1	5.7	5.2	5.0	5.1	5.7	5.3
	4.1	3.3	5.0	4.3	5.4	2.3	3.3	5.0
	10.1	11.1	13.9	10.2	0.4	0.2	0.3	0.7
F	485	488	492	495	497	497	495	486
	7.3	7.0	6.4	6.3	3.3	3.3	3.6	5.0
	6.8	6.1	5.3	5.3	2.3	3.5	2.7	4.2
	10.1	10.5	10.2	10.6	0.0	0.2	4.9	11.0
W	491	495	498	47.4	468	462	456	444
	5.7	7.5	5.0	5.6	6.2	6.3	7.4	5.4
	5.0	0.1	7.1	2.4	7.2	3.8	1.9	5.0
	10.1	11.7	11.1	11.6	11.6	11.0	10.5	10.4
F	481	476	470	465	459	454	448	443
	4.7	5.4	6.0	6.5	7.1	7.6	5.4	7.0
	4.6	6.0	6.9	7.1	5.1	5.3	5.5	7.5
	10.2	10.4	10.7	10.4	11.0	10.7	10.3	10.6



Euclid Paving

	wcb		Fcb
600-Si Tropan	343.60	Jan	343.0
00=NL "	346.00		343.60
50	344.15		343.99
1	344.31		344.39
50	344.61		344.77
5	344.77		345.16
50	344.93		345.55
3 1/2 x 7 1/2 FC on Ecb	345.00		346.00
3 1/2 x 5 = wcb. J. E. 1/2			
3 w. 30. Measured to SE EL Canyon			46.10

353.00
 1.50
 343.50
 6.00
 349.50

	w	43.80	44.2	44.4	44.5	44.8	45.0	45.00	45.0
		0.2	0.3	0.3	0.2	0.2	0.2	0.2	0.2
		1.7	6.0	5.7	6.8	6.0	5.8	5.0	0.7
			-0.5	-0.4	-1.3	-1.1	-1.1	-0.0	
		43.2	43.8	44.2	44.6	45.0	45.4	45.8	46.2
		0.8	0.9	0.8	0.9	0.9	0.9	0.9	0.9
		1.00	0.5	0.5	0.0	0.6	0.1	0.4	0.7
		0.20	-0.6	-1.0	-0.9	-0.9	-0.9	0.0	-0.2
		345.51	346.00	346.0	346.4				
		345.1	346	346	346				
		2.88							
		347.09	346.3						
			0.69						

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1/2 to 1
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
last column and top row. The number in both

from side stake to slope stake. If ground is not

IMPROVED TABLES

AND

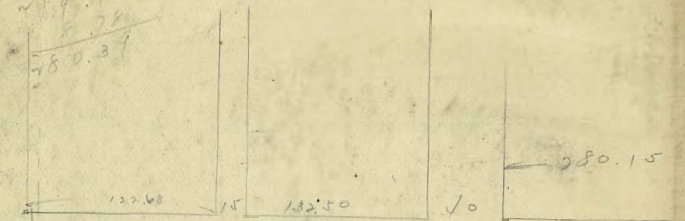
INFORMATION

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external) of point L by
given tangent (or external).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

11898 v NE BP N + 244

257.57
10.00
147.17
8.78
780.39



10
30
40
40.1
37
33

2' - 6"

4039
9039

2.52

1-11
6

CITY H915 Add

101 285 N Quince

1586
6100
555

106.50
551.14
644.64

Harry Davis

5139 Kansas

J. H. Regent and Div

H. E. W. Co.

Frank Luke Post #1

Francis B. ...

Brummett

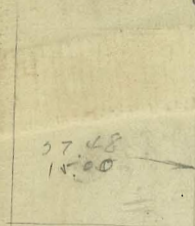
Grant

3788 natl.

297
271

43 - 44
407

Helpingsteins Add



4

310.58

P = 400

T = 776.2

307.00
0.53
307.03
2
31.71
50.37

26.57

3510.21
104.4
3614.61

33.22

Fleister add

lots 32 - 34

133
123
208

314.40

900
660
240

900
610
290

9448
5989
3459