Gr. 155

DAST

FIELD BOOK

No. 385

S.L. SD
Bet. Hudney & Twiggs
0+25 = 47 Gut
45
45
47
39
40
41
44
43
43
44

G-155 11

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

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100 15
100 05

200 20
182 3
382 50
98
480 50
158 45
638-95 - 639,68
200 8 200
838 75 839,68
56
895-75

Indexed tip 48. 11/28/29

55
37

49
73

822
700

Walker McGough Eng. Inc. Lake Kiowa 1-30-24

LA SOLLA AVE. PAVING

from Frias St to San Diego Ave.

SL. Sta.	S.L. Grade	NL. Sta.	NL Grade
170° NNW. T. to SL			S 4.5°
= 0+00 = End Exist. cb.	48.30	cb PC on this St.	54.25
(41.63') 4			
0+41.63	47.10	①	53.98
+83.26	45.90	②	53.75
1+24.9	44.70	on Lasolla Blvd.	
SL.LV Cor Ampudia		③ = cb EC = 0+00 =	53.50
+66.52 = End Exist Return	43.50	3-46'	
		0+46	52.34
EC. cb Return. at B see P-3	42.00	+92	51.17
End of cb to be Constructed at NWly Cor Lasolla Blvd. and Congress. Leave out	41.45	1+38 = Brk. = opp Frias St. (48.31')	50.00
= 0+00 = C See P-3	41.20	1+81.81 = cb. P.C.	48.55
0+14.92 = cb. P.C.	40.97		
0+40.7	40.60	①	48.50
+81.4 = Brk. (41') 5	40.00	②	48.55
	.092		
1+22.1	39.08	③	48.82
+63.4	38.16	④ = End Return	49.20
		5131' W cb P.C. on Sta 1+86.37	46.30
2+04.4	37.24	= Δ = Intersection SL. Congress w.c.L. Lasolla Blvd.	
+45.4			
+82.16 = End cb.	36.22		
+86.4 = Brk. = SLV Line Arista (7.47') 1	35.49		
= E Arista = Δ Lt 4°02' (1930')	35.40		
= beginning cb on diag. NLV Line Arista St		= 9' EW Line	
= 0+00 (50.36') 5	34.06	NE Cor Lasolla & Ampudia = Rev. Grade =	43.70
0+50.36	33.68	NW Cor Ampudia & Lasolla Blvd. = 0+00 (41.3') 3	42.70
1+00.72	33.36	0+41.3	41.90
+51.09	33.04	+82.6	41.10
2+01.46	32.72	1+23.9 = Brk. (46') 5	40.30
cb R = 9693	32.40		
+51.83 = PC Lt 2°00' Brk. 11.68' = chd 0.67 from cb Face		1+69.9	39.26
① def = 3°29'15"	32.37	2+15.9	38.22

Cont. on P-2

Note: Sta. 1+38 Brk. is not opposite Frias St.

Note: Sta. 1+38 Brk. is 20.48' Rt. of Sta. 1+86.37 on Lasolla Blvd. (41.63') 4 Southerly of Sta. 1+86.37

Change in Alignment see R8

01

3516 = BM. SE Pole Arista & Lasolla Blvd.

11227

4638 = T

.039 =

45.99 = TP

1170+

57.69 = T

385 =

53.84 = TP

2724

56.56 = T

1273 =

4383 = TP

643'

5026 = T

1247 =

37.79 = TP

2191

3998 = T

8.07 =

31.91 = TP

585 =

37.76 = T

679 =

30.97 = Nails in Pole 3098 - 5M. S.M. Conde & San Diego .001 = Error

5769 385 = SLV Line Frias St Lasolla Blvd 5384

= PC. cb Return

NL	5350	5234	5117	5000	4876	4790	4270	4190	4110	
	3.06	4.72	5.39	6.56	8.66	7.66	13.86	8.36	9.16	
	+.031	.034	.144	.415	.700	.900	1.213	.880	.998	
	+3.37	13.7	+3.95	+2.4	+1.016	+.756	+.113	-.044	-.082	
S	4830	4710	4590	4470	4350	4120	4060	4000	3908	
	1.96	3.16	4.36	5.56	6.76	9.06	9.66	10.26	8.70	
		3.77	4.52	5.61	6.59	9.23	10.59	11.04	4.84	
		-.06	-.016	-.01	+.017	-.017	-.098	-.138	-.414	
N	4030	3926	3822							
	9.96	11.00	1.76							
	1098	1247	3.06							
	-1.0	-.15	-1.3							

300' = 17.2' East of E.L. Congress = PC

N	4476	4390								
	5.26	6.10								
	4.13	4.43								
	+.11	+.167								
S	3816	3724	3682	3540	3400	3368	3336	3304	3272	3240
	1.82	2.74	3.16	4.58	5.98	6.30	6.62	6.94	7.26	7.58
	6.98	6.72	8.21	9.62	7.53	9.15	10.37	11.14	10.08	8.41
	-3.16	-3.98	-4.60	-5.04	-1.55	-2.85	-3.75	-4.2	-2.82	-0.83

5384 = BM. 108+ 5492 = T

N	4855	4630	4370							
	5.77	8.07	10.67							
	5.68	5.74	5.71							
	+.01	+.79	+.191							

FINISH STAKES

N 4830 ← RAKED → 4350

5384 = BM. 108+ 5492 = T 1761 = T 4731 = TP 291 = 4702 = T 1080 = TP 3442 = TP

= EC

S	5425	5398	5275	5350	5234	5117	5000	4855	4850	4855
	0.67	0.94	1.17	1.47	2.58	3.75	4.92	6.37	6.42	6.37
	4200	4185	= 0+14.92	4097	4060	4000	3908	3816	3724	3632	3549
S	3.72	3.87	Brk.	4.25	4.62	4.22	6.14	7.06	7.98	8.90	7.73
	3.14	3.70								
	.061	1.670								
	4882	4930	= EC				0+00			
J	610	5.62				N	4270	4190	4110	4030	3926	3822
							7.52	5.32	4.12	4.92	5.96	7.00

N

PC.

V	3406	3400	3368	3336	3304	3272	3240	3237		
	3.28	3.34	3.66	3.98	4.30	4.62	4.94	4.97		

S

Lasolla Blvd. Con't. from P-1
And San Diego Ave

S.L. sta.		S.L. Grade	N.L. sta.	N.L. Grade
② def	6°58'30"	32.34	2+61.9	37.18
③ "	10°27'45"	32.31	3+07.9	36.14
④ = EC "	13°57'	32.28	+53.9 = Brk = S'LY Line Arista	35.10
			①	34.93
			②	34.76
			③	34.59
			④ = EC, 21.41 E.W.L. on North	34.42
			= 0+00 = WLY Line Arista (38.94')4	34.00
			0+38.94	33.80
			+77.9	33.60
			1+16.8	33.40
			+55.75 Brk (27.12)2	33.20
			1+82.87	33.23
			2+10.0 = End cb. beginning cb on NLY Line San Diego and NLY Line Lasolla Blvd.	33.26
			cb. P.C. N.E. Cor. Conde	33.40
P.C. Return		32.20		33.20
1		32.16	①	33.20
2	S.E.	32.03	② N.E. Cor Conde	33.30
3 = EC "		31.87	③ = EC	33.46
End Return		31.80	End Return	33.50
Beg. Return		31.50	End Return	33.30
P.C. "		31.58	P.C. "	33.25
1	S.W. Conde St	31.80	①	33.13
2		31.93	②	33.04
3				
EC = 0+00 (50')5		32.00	③ = EC = 0+00 (50')6	33.00
+50		31.81 (79)	0+50	32.85
1+00		31.62 (57)	1+00	32.70
+50		31.43 (36)	1+50	32.55

32.15

00.26 %

Cont. on P-5

3998 = T
3098 = BM. P-1
624+
37.22 = T

2

N 3718 3614 3510 3400 3385 3370 3355 3340 3320 3323 3326
280 384 488 598 613 628 643 658 400 396
609 686 746 427 527 348 613 629 353 300
-3.29 -3.02 -2.58 +1.7 +0.86 +2.8 +0.3 +0.3 +0.5 +1.0

= ½ way bet P.C. and Beg = 0+00

S 3230 3220 3200 3181 3162 3143
492 502 522 541 560 58
487 832 870 862 835 78
-3.3 -3.5 -3.2 -2.75 -2.0

3351
357 = cb. PC = 0+00

N 3340 3320 3300 3285 3270 3255
3.82 402 422 437 452 467
3.61 386 566 548 516 389
+0.2 +0.16 -1.44 -1.1 -0.64 +0.8

N 3718 3614 3510 = E.L. Arista
8.04 9.08 10.12

4522 = T P-1
1080
3442 = TP
292+
3734 = T

Finish stakes

PC = WLY Line Arista

N 3493 3476 3459 3442 3400 3380 3360 3340 3320 3323 3326
241 258 275 292 3.34 354 374 394 414 411 408
214 131 314
+1.40 +2.43 +1.00

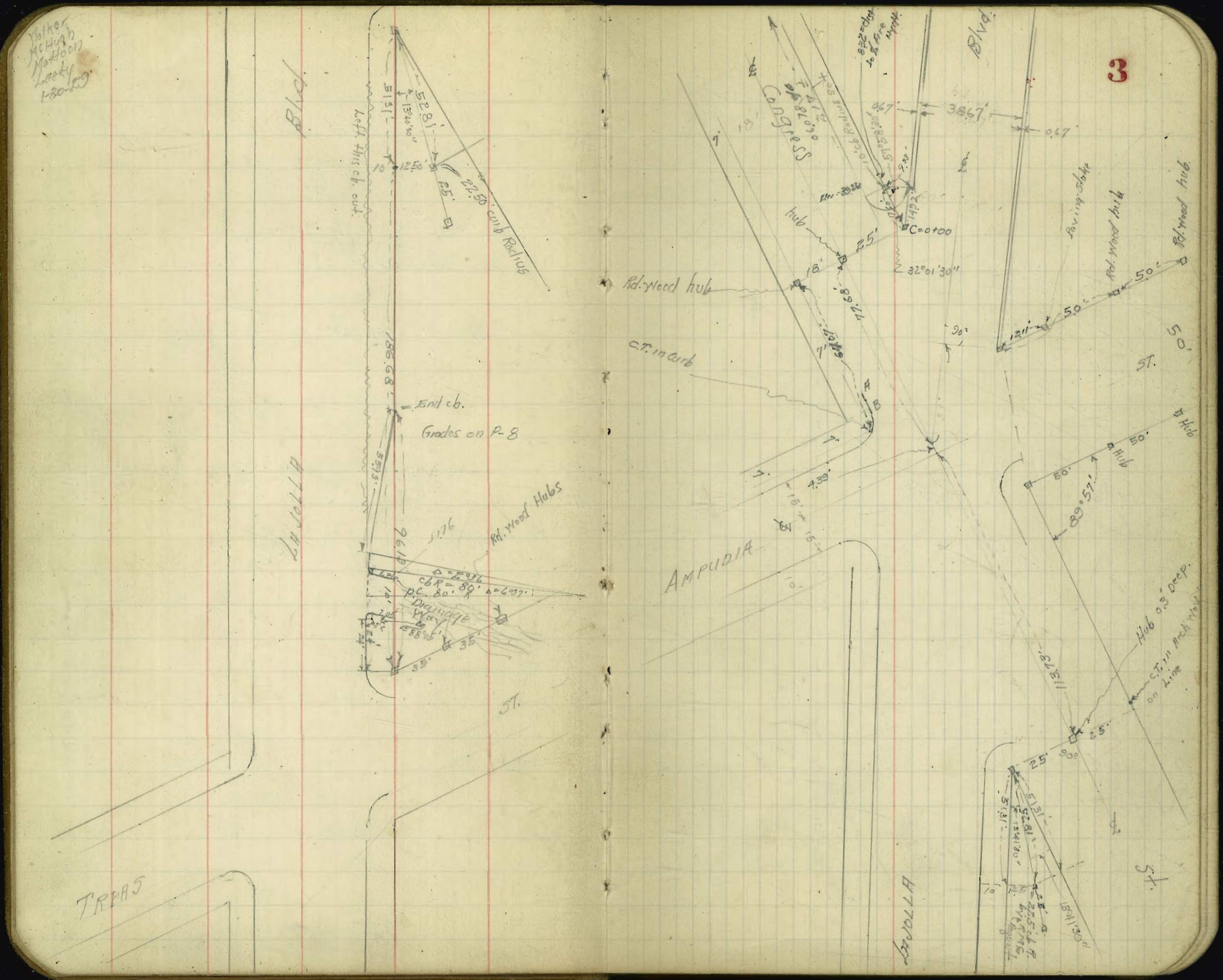
S 3234 3231 3228 3220 3216 3203 3187 3180 3150 3158
500 503 506 476 480 493 509 516 546 538

3519 = T P-5
3696 = T P-5

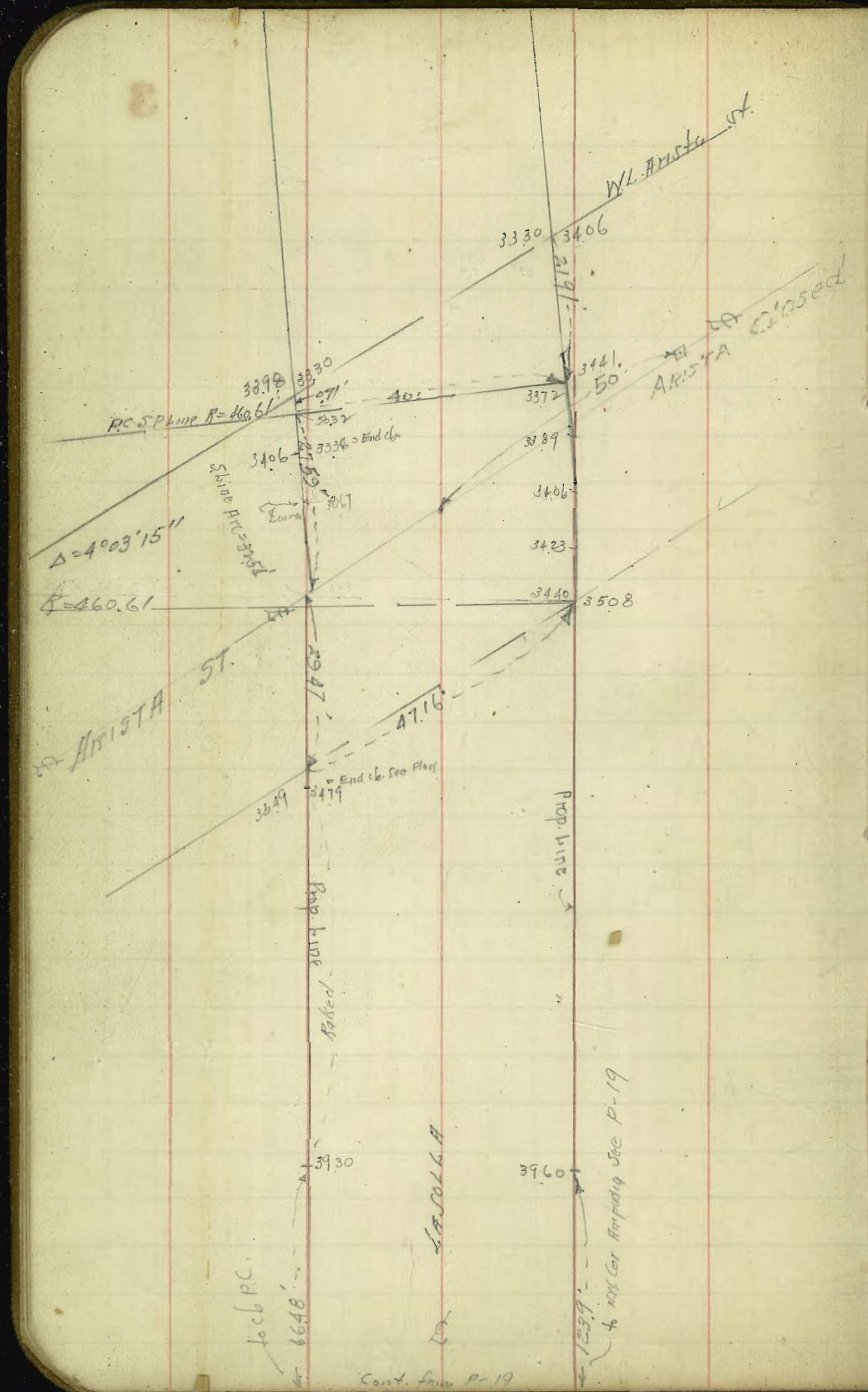
N 3340 3320 3320 3330 3346 3350 3330 3325 3313 3304 3300
3.56 375 376 366 350 346 366 371 383 392 396

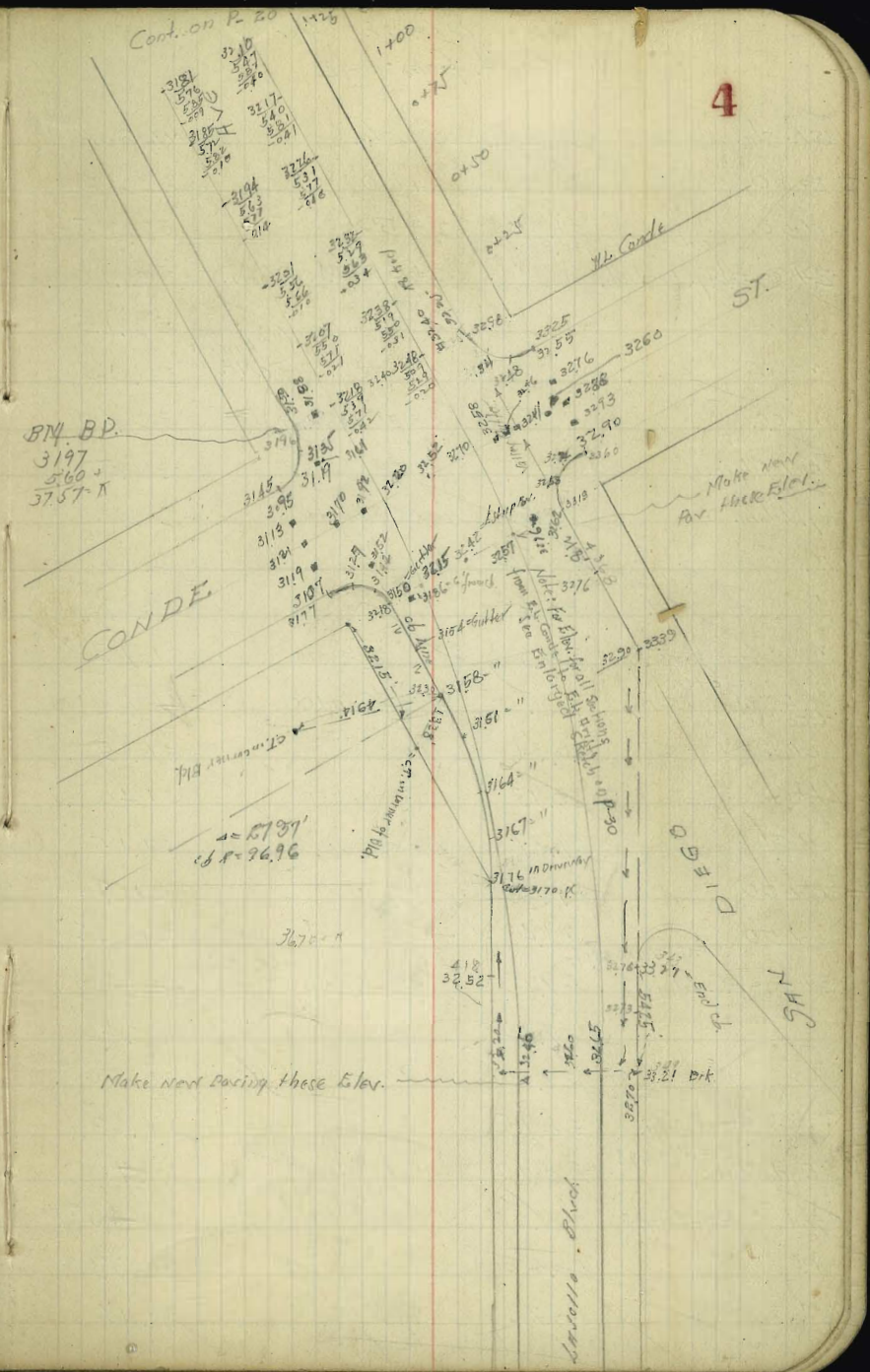
S 3180 3193 3200 3179 3157 3136
516 503 496 517 539 560

N 3285 3270 3255
411 249 264



Walker McHugh Mattoon Leeky 1-30-29
3
Blvd.
Left this cb. out
52.81'
13°40'30"
12.50'
25'
22.50' curb Radius
186.68'
End cb.
Grades on P-8
Rd. Wood Hubs
Drainage Way
35'
ST.
TREAS
Congress
38.67'
0.67'
C=0+00
32°01'30"
hub
25'
18'
Rd. Wood hub
C.T. in curb
77.68'
4.39'
AMPUDIA
Paving stake
Rd. Wood hub
50'
Hub
89°57'
Hub 0.3' deep
C.T. in Arch Way on Line
113.73'
25'
90°
ST.


W.L. Arista St.
Arista Closed
P.C.S.P. Line R=460.61'
Δ=4°03'15"
R=460.61
Arista St.
Prop. Line
Raked
Lasolla
Cont. from P-19


Cont. on P-20
W.L. Conde
Conde
St.
BM. BP.
3197
Make New Pav. these Elev.
Make New Paving these Elev.
Lasolla Blvd.
San Diego

San Diego Ave

Cont. from P-2

S.L. Sta.	S.L. Grade	N.L. Sta.	N.L. Grade
	31.14		
1+00	31.23	1+00	32.40
	30.93		
+50	31.03	2+50	32.25
	30.88		
2+60 = beg. Exist. Cb.	30.99	3+00 = P.C. Return.	32.10
		'	32.15
		'	32.25
		3 = E.C. Return	32.40
		End "	32.50
beg. Return.	30.50	beg. Return	32.30
P.C. "	30.52	P.C. "	32.23
'	30.60	'	32.07
'	30.61	'	31.93
3 = E.C. Return on San Diego (50' ℄)	30.60	③ = E.C. = 0+00	31.90
0+50	30.36		31.65
1+00	30.13		31.40
+50	29.89		31.15
2+00	29.66		30.90
+50	29.43		30.65
3+00 = P.C. Return	29.20	P.C. Return	30.40
'	29.15	'	30.40
'	29.05	'	30.50
3 = E.C. Return.	28.95	3	30.63
End Return.	28.90	End Return	30.70
End " S.W. twigg's	28.60	End " N.W. twigg's	30.40
P.C. " " "	28.63	P.C. " " "	30.33
'	28.72	'	30.17

Note decimal

Harney S.W.

Harney N.E.

Stations same as South

S.E. Cor. Twiggs St.

S.E. Cor. Twiggs St.

N.E. Twiggs

N.E. Twiggs

Cont. on P-6

3722 - T from P-2
673-
3049 = T.P.
676-
3725 = T

S 3123 3103 3099 3060 3036 3013 2989 2966 2943
60 67 623 689 717 736 76 787
67 631 633 691 540 681 638 656
-09 -02 0.9/Lnk 0.02 +1.7 +0.55 +1.2 +1.76

N 3240 3225 3210 3190 3165 3140 3115 3090 3065
4.87 4.97 5.17 6.32 5.57 5.81 6.07 6.32 6.57
3.51 3.67 3.51 3.51 3.41 3.71 3.68 3.42 3.91
+1.3 +1.79 +1.6 +1.8 +2.16 +2.07 +2.4 +2.90 +1.6

S 2920
805
676
+1.1

N 3040
6.87
4.38
+2.49

S.D. Ave + Mason P.78

2307 = B.M. SET tack FINISH STAKES
8424
3149 = T

S 3114 3098 3088 3050 3052 3060 3061 3060 3036 3013 2989 2966
582 476 431 459 483 506 530 553
424 428 481
002H 008H 002H

30.62 - 8" Sta. Harney
457
3519 = T
197-
3322 = T.P.
474
3696 = T

N 3240 3225 3210 3215 3225 3240 3250 3230 3223 3207 3195 3190
279 294 309 304 294 279 269 289 296 312 326 329

cont'd on P-2

P.C. ① ② ③ End

S 2943 2950 2915 2905 2885 2890 2860 2863 2877
576 529 534 544 558 549 569 586 579

N 3145 3140 3115 3090 3065 3040 3040 3050 3063 3070 3040 3033 3017
354 379 404 429 454 109 109 099 086 078 109 116 132

SAN DIEGO Ave.
Cont. from P-5

SL. Sta.	SL. Grade	N.L. Sta.	N.L. Grades
2	28.75	2	30.00
SW. Twiggs 3=E.C.=0+00 (50') 3	28.70	N.W. Cor. Twiggs 3=E.C.=0+00 (50') 6	29.90
0+50	27.74	0+50	28.81
1+00	26.77	1+00	27.73
+50 = beg. Exist. cb.	25.80	+50	26.64
		2+00	25.56
SW. Cor. Mason. ~~End. cb. Return.~~	~~22.30~~	+50	24.48
P.C. " "	22.30	3+00 = Brk.	23.40
1	22.35	+50 = " (37.5') 2	22.40
2	22.35	3+87.5 = E.L. Mason St.	21.40
3=E.C. "=0+00 (37.5') 2	22.30	4+25 = End of Job	20.40
0+36.4	21.37		
+75 = End Job.	20.40		

37.25 = π from P-5
12.30 −
24.95 = TP
2.37 +
27.32 = π
0.51
26.81 = TP
10.32 +
37.13 = π
6.51
30.56
30.62
0.06 = E

2732
181
25.51 = BM. S.E. top Hydt. Mason & San Diego Back 12-19-16
25.56
0.05 = Error

6

S 28.70 27.74 26.77 25.80 = 1+50
8.55 9.51 10.48 11.45
7.72 8.58 9.92
+0.83 +1.0 +0.56

22.30 21.35 20.40
5.02 5.97 6.92
6.13 6.03 7.20
−1.1 −0.1 −0.3

N 29.90 28.81 27.73 26.64 25.56 24.48 23.40 = Brk. 22.40 = Brk. 21.40 20.40
7.35 8.44 9.52 10.61 11.7 12.77 13.85 14.92 15.92 16.92
3.80 4.30 6.83 8.47 9.7 11.70 12.72 3.56 4.63 5.92
+3.55 +4.14 +2.7 +2.14 +2.0 +1.07 +1.13 +1.36 +1.3 +1.00

31.49 = π P-5 Finish stakes
23.07 = BM. S.E.
3.25 +
26.32 = π

S 28.75 28.70 27.74 26.77 25.80 22.30 22.35 22.35 22.30
2.74 2.79 3.75 4.72 5.69 4.02 3.97 3.97 4.02
5.68
0.01 H.

N 30.00 29.90 28.81 27.73 26.64 25.56 24.48 23.40 22.40 21.40
1.49 1.59 2.68 3.76 4.85 5.93 7.01 8.09 9.09 10.09

S 21.37 20.40
4.95 5.92

N 20.40
11.09

Walker
McHugh
Leiby
Mathoop
2-19-29

SEWER Const. in Lapolla Ave.
Bet. Ampudia and Trias st.

Const. M.H. in L Ampudia =0+00	54.16	16.20	37.96	38.00	
+47		7.20	44.96	39.18	+5.78
+94		8.21	45.95	40.36	+5.59
1+41		7.15	47.01	41.54	+5.47
+88 1-50'		5.91	48.25	42.73	+5.54
2+38=P.E.		3.79	50.37	44.00	+6.37

B.M. S.W. Pole P.1 = 53.84
0.32-1
54.16=T

2-21-29 Walker

SEWER Const. in L Lapolla Blvd.
Bet. ARISTA And Ampudia

M.H.#1 & Arista st. =0+00	40.88	6.83	34.05	27.57	+6.78
+52		5.75	35.13	28.31	+6.82
1+04		4.56	36.32	29.35	+6.97
+56		3.48	37.40	30.29	+7.01
2+08		2.26	38.62	31.43	+7.19
+60 P.E.		1.68	39.20	32.47	+6.73

B.M. S.E. Pole P.1 = 35.16
.572
40.88=T

7

Walker 3-21-29

Change in Alignment Lafolla Ave
from cb E.C. P-1 on North side

	N.L. Grades
cb P.C. P-1	
= 0+00	53.50
cb R = 80'	
+28.26 = P.C. Rt. 9°13'	52.80
ctr. of curve	52.64
E.C. = 0+41.13	52.48
0+69.03	51.78
+96.93 = End cb. N.L.Y Prop line Lafolla Ave	51.08

5384 = B.M. P-1
353 +
57.37 -x

8

53.50	52.80	52.64	52.48	51.78	51.08
3.87	4.57	4.73	4.89	5.59	6.29
				4.59	2.82
				+1.00	+3.47

San Diego Ave. And Taylor St. Paving Etc.

{Griffith Co. Courts}

S.L. Sta.	S.L. Grades	N.L. Sta.	N.L. Grades
W.P.L. Wallace Produced SLY to S.L. San Diego = 0+00	13.50 Sec P-23	W.P.L. Wallace = 0+00	14.26
+38.42	13.60		14.80
0+76.85 = 4.33' E.E.L. Wallace = cb P.C. 5° Radius	13.05	+34.25	13.65
	12.49	+68.5 Brk.	13.00
E.S. on Wallace SLY Cor.	12.38		
P.C. on Wallace WLY Cor	12.02	WLY Line Wallace Produced NLY to NLY Line San Diego = 0+00	Leave Out
E.C. = 0+4.33 (48.98') 0+06' = 11.96 = E. Fire Ly. St.	11.96	+4.33 = opposite P.C. on S	12.51
0+52.9	11.19		11.57
1+01.5	10.42		10.65
1+50.1	9.65		9.72
+98.7	8.88		8.80
2+47.2 cb	8.11		7.87
+95.8	7.34		6.95
3+44.4	6.57		6.02
+93 = Brk. (685.1')	5.80	= cb. P.C.	5.10
4+21.5	5.75	(1)	5.03
+50 = P.C. 4° Radius = 1229'	5.70	(V)	4.96
(1)	5.72	(3)	4.89
(V)	5.74	(4)	4.82
(3)	5.76	(5)	4.75
(4)	5.78	(6)	4.68
(5) = E.C.	5.80	(7)	4.61
(135)' = End cb.	5.80	(8)	4.54
		(9)	4.47
		(10) = cb E.C. = 0+00	4.40
		r-45' 0+45	4.18

Station Same as South

+2933' ↑

E.L. Taylor, St.

Cont. on P-11

2556 = B.M. S.L. N.W.H. Watson & S.D. Ave Book 1218-16

0.12 ↑

2568 = A

1028-

1540 = T.P.

3037

1843 = T

5.60-

1279 = T.P.

1.56

1435 = T

See P-11

1843 = T

579-

1264 = B.M. S.W. Cor Wallace and S.D. Ave

= 0+43.33

S 1360 1305 1249 1238 1202 1196 1119 1042 965 888 811 734

483 647 722 801 878 955 634 701

842 729 678 761 725 772 702 757

-06 +08 +044 +04 -047 -017 -078 -06

= Brk

N 1430 1365 1300

413 543

423 434

-01 +057

= 0+433

1351 1157 1065 972 880 787 695

592 686 778 463 555 646 740

503 574 626 136 399 820 735

+089 +172 +172 +327 +156 -174 -20

= Brk. = cb P.C. = End Improvement at Santa Fe. R.R. Way

S 657 580 575 570 580

778 855 860 865 855

10.00 11.27 10.86 10.83 11.92

-2.22 -2.72 -2.26 -2.18 -5.37

= Brk - cb P.C.

N 607 510

833 925

10.66 10.67

-2.33 -1.37

= cb E.C.

440

775

1106

-121

1787 = T

1369

418

+053 on Switch

1247 = B.M. P-79

3267

1878 = T

1000-

5.80 = T.P.

234

815

683

183 = Brk on B.M.

185 = Brk

627

6.17 = T

FINISH STAKES

	P.C.	E.C.	P.C.	E.C.		P.C.
N.	1430 1431 1430 1426	1313 1300	1288	1451	← opp E.C.	Brk. 510 503 496
	357 357 357 361	474 487	499	537	← Brk 80	+1078 3.14 3.21
	361 -016 +004					

	P.C.	E.C.	P.C.	E.C.		Brk.	P.C.
S.L.	1350 1335 corr 1337	1249	1238	1185	1196	580 575	570
	437 467 487 512	538 549	903	3.92	← Station	+1008 circle	247
	827 -075						

							EC	
N	489	482	476	468	461	454	447	440	418
	3.28	3.35	3.41	3.49	3.56	3.63	3.70	3.79	3.77

1267 = B.M.

5267

2.87 = T

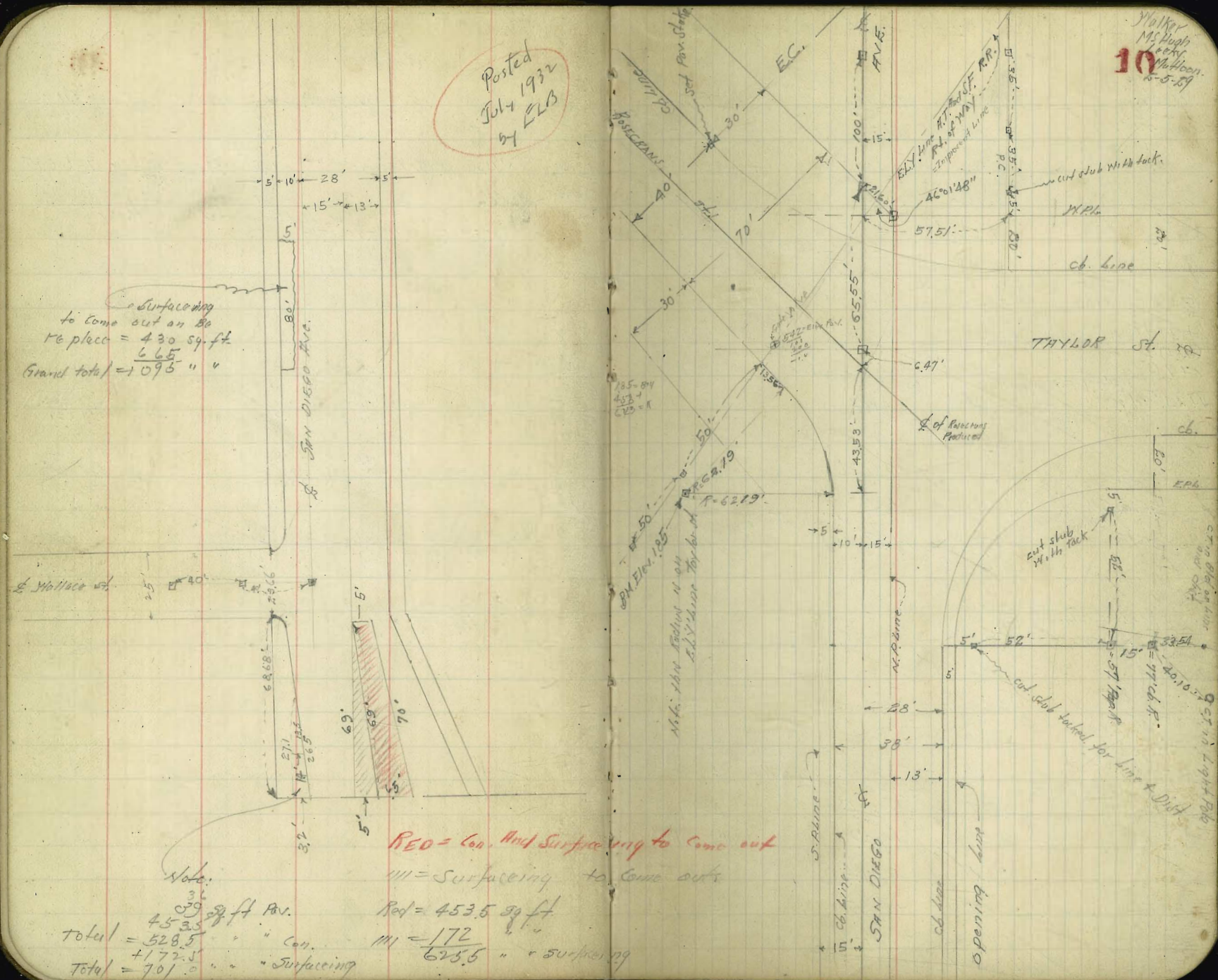
SL 572 574 576 578 580 580

243 243 241 239 237 237

Posted July 1932 by ELB

Walker McHugh Leeky Mulloon 2-5-29

10



RED = Con. And Surfaceing to Come out

//// = Surfaceing to Come out

Note:
36
39 sq ft Pav.
453.5
Total = 528.5 " " Con.
+172.5
Total = 701.0 " " " Surfaceing

Red = 453.5 sq ft
//// = 172 " "
625.5 " " Surfaceing

TAYLOR St Paving &c.

W.L. Sta.	W.L. Grade	E.L. Sta.	E.L. Grade
beginning cb EL'y line RT and SE RR. R'l way	5.75	15'SSL Calhoun 0+90 = cb P.C.	3.95
① def. = 2°29'58"	5.70	1	3.91
② 5°09'46"	5.66	2	3.92
③ 7°44'39"	5.62	3 = E.C. SE Calhoun	3.95
④ 10°19'32" 12°54'11"	5.58	P.C. on Calhoun.	4.11
⑤ = E.C. = 0+00	5.54	1	4.09
+47.49 = 8'sf. opp cb PC, on E (485)	5.40	2 NE Cor Calhoun.	4.07 4.06
0+96 = 8'SSL Calhoun. on W	4.57	4 = E.C. = 0+00 (454')5	4.05
1+44.5 = cb P.C.	3.74	0+45.4	4.17
①	3.70	+90.8	4.29
②	3.65	1+36.2	4.41
③ = E.C. on Calhoun. N.W.	3.60	1+81.6	4.53
P.C. on Calhoun	3.63	13' SSL Jaun 2+27 = cb P.C.	4.66
①	3.70	1	4.70
②	3.77	2	4.73
= 8' N.W.L. Calhoun.		SE Cor. contact	4.76
③ = E.C. = 0+00 (414)5	3.83	3 = E.C. on Jaun St. N.E. Cor.	4.80 4.86
0+41.4	3.98	P.C. on Jaun	
+82.8	4.13	1	4.84
1+24.2	4.28	2	4.83
+65.6	4.43	NE = 13' N.E. Jaun = 0+00 3 = E.C. on taylor (47.12)8	4.83
10' SSL Jaun St. 2+07 = cb PC	4.57	0+47.12	4.97
1	4.62	+94.2	5.11
2 S.W. Cor.	4.67	1+41.4	5.25
3 = E.C. on Jaun St. N.W. Cor.	4.72	+88.5	5.39
P.C. on Jaun	4.78	2+35.6	5.54

Conf. on P- 12

794 = π from P16

1438 = π from P9

969 = P.T.

4.72 = P.T.

403 +

875 = π

191

600 = T.P. N.E. top Wyatt Jaun

317+

1001 = π

= N.W. Prop. Cor. San Diego Ave

= cb E.C.

= cb P.C. = 0+00

W 575 570 554 540 457 374 383 398 413 428 443

300 305 371 335 418 501 492 477 462 447 432

785 708 814 765 838 911 892 875 832 798 793

-49 -40 -493 -43 -3.18 -41 -13 -20 -17 -151 -16

E 440 418 395 405 417 429 441 453

taylor 435 457 480 470 458 446 434 422

578 588 580 470 611 593 550

-143 -13 -10 000 -165 -16 -13

= cb P.C. = 10' SSL Jaun St. = 0+00

W 457

418

611

-20

= 10' SSL Jaun St

= cb P.C. = 0+00

= 2+37.5

E 466 483 497 511 525 539 554

409 518 504 490 476 462 447

520 561 586 581 573 430 541

-111 -05 -082 -09 -10 +0.8 -094

817 = π P-9

FINISH STAKES

= E.C. = B.M. = cb P.C. 8' SSL Calhoun. = E.C. = P.C.

W.L. 576 570 566 562 558 554 540 457 374 370 365 360 363

147 247 251 255 259 263 277 360 413 417 452 457 454

= E.C. 8' N.W.L. Calhoun. P.C. 10' SSL Jaun = E.C. S.W. = P.C. N.W. Jaun.

W.L. 370 377 389 398 413 428 443 457 462 467 472 478

447 440 434 364 549 534 519 505 500 495 490 482

920 = π from P-16

PC = S.E. Return = E.C. on Calhoun = P.C. = N.E. Calhoun = P.C.

E.L. 395 391 387 395 407 411 409 407 406 417 429 441 453 466

473 476 477 427 410 411 491 930

971 = π

960 = π

962 = π

= S.E. Cor Jaun = N.E. = E.C. 13' N.W.L. Jaun

E 470 473 476 486 484 483 483 497 511 525 539 554

477 474 449 446 432 411

472 = P.I. Jaun to Taylor

424 +

896 = π

TAYLOR St.

Cont. from P-11

M.L. Sta.	M.L. Grade	E.L. Sta	E.L. Grade
1	4.79	2+82.8	5.68
2	4.81	3+29.9	5.82
N.W. for Taylor & Jean		10'SSW Sunset.	
3 = E.C. = 0+00	4.83	3+77 = cb P.C.	5.95
(46.67') 6			
0+46.67	4.97	1	5.99
+93.34	5.11	2 S.E. Cor.	6.03
1+40	5.25	3 = E.C. on Sunset Blvd.	6.07
+86.7	5.39	P.C. N.E. Cor. on Sunset.	6.13
2+33.4 10'SSL Sunset.	5.53	1	6.10
+80 = cb P.C.	5.66	2	6.13
1	5.70	3 = E.C. = 0+00	6.13
2 S.W.	5.74	(45)'4	
3 = E.C. on Sunset N.W.	5.78	0+45	6.26
P.C. on Sunset	5.83	+90	6.39
1	5.83	1+35 10'S.S.L. Whitman	6.52
2	5.83	+80 = cb P.C.	6.66
NW Sunset		1	
3 = E.C. = 0+00	5.83	2	6.70
(46.67') 6		S.E.	
0+46.67	5.97	3 = E.C. on Whitman	6.74
+93.34	6.11	N.E. P.C. on Whitman	6.78
+40	6.25	1	6.83
+86.7	6.39	2	6.80
+33.4 10'SSL Whitman	6.53	N.E. 3 = cb E.C. = 0+00	6.83
+80 = cb P.C.	6.66	(46.67') 6	
1	6.70	0+46.67	6.98
2	6.74	+93.34	7.14
3 = E.C. on Whitman	6.78	1+40	7.29
		+86.7	7.45

Cont. on P-13

10.01 - π from P-11

319

682 - TP 3 Nails in Pole SE. Whitman & Taylor

491.1

1173 = π

293 -

880-812

889 - Seasons Whitman Stephen

293

11.82 - π

Sunset Blvd. **12**

= 0+00 = cb P.C. 10'SSL. = 0+00

W	483	497	511	525	539	553	566	583	597	611	625		
	518	504	490	476	462	448	435	418	404	390	376		
	512	461	516	537	539	✓	387	425	408	398	394		
	-.001	+040	-026	-061	-087		+0.5	-0.1	-00	-0.1	-018		

= cb P.C. = EC

E	568	582	595	613	626	639	652	666
	433	419	406	398	375	362	349	335
		428	414	361	342	312	288	330
		-029	-088	+137	+033	+05	+06	00
				+06	-0.4	00	-01	

Reset.

W	639	653	666
	367	348	507
	281	361	477
	-03	-013	+03

= 0+00

E	683	698	714	729	745
	499	484	468	453	437
	574	577	576	542	511
	-07	-093	-10	-09	-08

FINISH STAKES

= EC. = P.C. 10'SSL Sunset = EC SW = PC. NW

W	479	481	483	497	511	525	539	553	566	570	578	578	583	583
	481	479	488	474	460	446	433	418	421	401	397	393	388	505

= cb PC 10'SSL Sunset = EC SE. = PC. NE. on Sunset = EC. = 0+00

E	568	582	595	599	603	607	613	610	613	613	626	639	652
	403	389	493	489	485	481	475	478	475	475	462	449	436

1088 - π P-13

507 -

581 = TP

390.1

971 = π

361 -

610 = TP

460 -

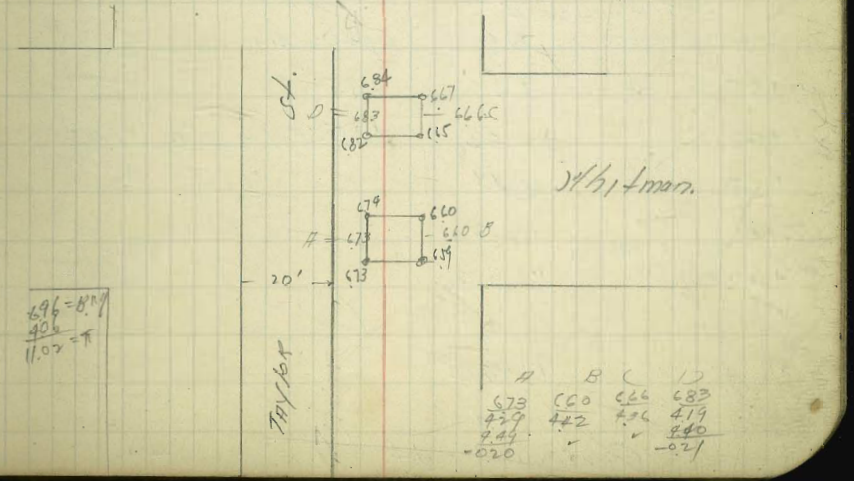
760 = π

= EC NW Sunset = cb PC 10'SSL Whitman = EC.

W	583	583	597	611	625	639	653	666	670	674	678		
	505	505	491	477	463	449	435	422	418	414	410		

= PC. 10'SSL Whitman SE = PC. NE on Whitman = EC NE Whitman

E	666	670	674	678	683	680	683	683	698	714	729	745	
	422	418	414	410	405	408	405	405	507	491	476	460	



696 = 8.04

405

11.02 = π

TAYLOR St.
Cont. from P-12

W.L. Sta.	W.L. Grade	E.L. Sta.	E.L. Grade
N.W. Cor. P.C. on Whitman	6.83	2+33.4	7.61
1	6.83	10' S.S.L. chesnut +80 = cb P.C.	7.76
2	6.83	1	7.84
10' N.N.L. Whitman 3 = E.C. = 0+00	6.83	2	7.92
(4667)6 0+46.67	6.98	S.E. 3 = E.C. on chesnut	8.00
+93.34	7.13	N.E. P.C. on chesnut	8.50
1+40	7.28	1	8.40
+86.7	7.4	2	8.50
2+33.4	7.60	10' N.N.L. chesnut 3 = E.C. = 0+00	8.70
10' S.S.L. chesnut +80 = cb P.C.	7.76	(4834)6 0+48.34	9.75
1	7.80	+96.68	10.80
2	7.84	1+20 = End of full width grading on E. 1+45	11.32 +17 at 5' E.G.L. 11.85
S.W. 3 = E.C. on chesnut	7.88	+93.4	12.90
N.W. P.C. on chesnut	8.40	2+41.7	13.95
1	8.40	2+90 = S.L. Hickory	15.00
2	8.50	1-50 = N.L. Hickory = 0+00	16.00
N.W. = 10' N.N.L. chesnut 3 = E.C. = 0+00	8.68	0+20 = Bk.	16.30
0+50	9.60	+55 = "	16.80
1+00	10.52	+85 = End of Work	17.03
+50	11.44		
2+00	12.36		
40' S.S.L. Hickory +50 = cb P.C.	13.28		
1	13.49		
2	13.70		
3	13.91		

1.84 %

Cont. on P-14

1182 = π from P-12
1.56 −
10.26 = T.P.
10.64 +
20.90 = π
0.77 −
20.13 = T.P. BM. Sand Bridge
R117 = π from P-78

W 683 698 713 728 744 760 776 868 960
5 4.84 4.69 4.54 4.38 4.22 4.06 3.14 2.22
5.3 5.48 5.26 5.32 5.41 5.40 4.49 4.82 4.42
−0.3 −0.64 −0.57 −0.78 −1.0 −1.2 −0.43 −1.68 −2.2
= E.C. = 0+00 = cb P.C. = 0+00

E 761 776 870 975 1080 1132 1185 1290 1395 1500
4.21 4.06 3.12 2.07 1.02 9.53 9.05 8.00 6.95 5.90
3.65 3.40 2.67 2.89 1.06 9.70 8.26 7.6 2.6 6.14
+0.56 +0.66 +0.45 −0.82 −0.1 +0.8 +0.4 +95.5 +1.20

1259 = P.C. cut stack on W
643 +
1902 = π

W 1052 1144 1236 1323 1344 1365 1500 Grade fire Hydt
10.65 9.73 8.81 7.94 4.02
13.68 13.38 10.77 8.58 1.23
−3.0 −3.65 −1.96 −0.64 +2.79
= cb P.C.

E 1600 1630 1680 1703
4.90 4.60 4.1 3.87
10.7 1.59 1.5 3.78
+15.8 +2.05 +5.6 +0.1

6.96 = BM. Page 79 S.W. Whitman & Taylor
3.92 +
10.88 = π

FINISH STAKES

W 683 683 683 683 698 713 728 744 760 776 780 784
4.05 4.05 4.05 4.05 4.47 4.32 4.17 4.01 3.85 4.29 4.25 4.21
= P.C. N.W. Whitman = 10' N.N.L. Whitman = P.C. 10' S.S.L. chesnut

E 761 776 784 792 800 850 840 850 870 975 1080 1185
4.44 4.29 4.21 4.13 4.05 3.55 3.65 3.55 3.35 6.57 5.52 4.47
= P.C. = P.C. S.E. chesnut = P.C. N.E. chesnut = E.C. 10' N.N.L. chesnut

871 = BM. P-78
334 +
1205 = π
518 −
687 = T.P.
458 +
1145 = π

W 788 840 840 850 868 960 1057 1144 1236 1305 1326 1347
4.17 7.19 6.27 5.75 4.88 3.96 3.27 3.06 2.85
3.73
−0.88
= E.C. P.C. = N.W. = E.C. 10' N.N.L. chesnut = 1+03 = cb P.C. 40' S.S.L. Hickory

E 1290 1395 1500
3.42 2.37 1.32

871 = Above BM.
716 +
1587 = π
303 −
1284 = T.P.
348 +
1632 = π
223 −
14.09 = T.P.
7.13 +
21.22 = π

W 1368 840 840 850 868 1328 1349 1370 1391
2.64 3.64 3.64 3.54 3.36 4.15 3.94 3.73 3.52
3.89 5.05 4.95 3.67 4.02 4.61 4.93
−1.25 −1.41 −1.31 −0.13 −0.08 −0.88 −1.41

1721 = BM. = 40
022
1743 = π
871 = BM.
333 +
1204 = π

TAYLOR St. Cont. from P-13

W.L. Sta	on St. Hickory	W.L. Grade
		14.12
℄ = Encl cb on W.L. Taylor		
1-50' = 0+00 = W.L. Hickory		15.00
0+35		15.80 = Pav. Grade = cb Grade
+55 Encl Sta.		16.20 = " " = " "
		= " "
0+85 = Encl Work		16.74 = " "

W	1407	1500	1580	1620	1674
	710	617	537	497	443
	856	617	582	676	392
	-146	-085	-045	-03	+051

1632 = ℄ P-13
1743 = ℄

Finish Stakes

W	1389	1412
	243	331
	377	478
	-154	-147

TAYLOR St.

Storm Drain #1

Location 13' West of East Property Line

				Flow Line Grades	Cuts
N.L. Whitman	9.72	4.09	5.63		+1.73
=0+00	~~10.47~~	~~4.78~~	~~5.69~~	3.90	+1.79
+50		4.12 ~~4.82~~	5.60 ~~5.65~~	3.45	+2.15 ~~+2.20~~
1+00		3.97 ~~4.65~~	5.75 ~~5.82~~	3.00	+2.75 ~~+2.82~~
+50		4.10 ~~4.78~~	5.62 ~~5.69~~	2.55	+3.07 ~~+3.14~~
2+00		4.30 ~~4.99~~	5.42 ~~5.48~~	2.10	+3.32 ~~+3.38~~
+50		4.45 ~~5.14~~	5.27 ~~5.33~~	1.65	+3.62 ~~+3.68~~
=S.L. Sunset on E. 3+00 = Brk.		4.89 ~~5.59~~	4.83 ~~4.88~~	1.20	+3.63 ~~+3.68~~
+50		4.82 ~~5.50~~	4.90 ~~4.97~~	1.05	+3.85 ~~+3.92~~
4+00 = ℄ Cleanout #TYPE "F"		4.97 ~~5.65~~	4.75 ~~4.82~~	0.90	+3.85 ~~+3.92~~
+50		4.80 ~~5.48~~	4.92 ~~4.99~~	0.75	+4.17 ~~+4.24~~
5+00		4.97 ~~4.92~~	4.75 ~~5.55~~	0.60	+4.15 ~~+4.95~~
+50		5.32 ~~6.01~~	4.40 ~~4.46~~	0.45	+3.95 ~~+4.01~~
6+00		5.83 ~~6.46~~	3.89 ~~4.01~~	0.30	+3.59 ~~+3.71~~
+50		5.44 ~~6.11~~	4.28 ~~4.36~~	0.15	+4.13 ~~+4.21~~
=Beginning Con. Section 7+00 = End 8" Con. Sewer Pipe		5.96 545	~~4.51~~		9.27 ~~+4.51~~
		= E.L. Jaun St.	4.27	0.00	

483' offset
6' offset East.
Note All these stakes
Reset 3-15-29 Top ℄ cleanout = Elev. = 5.85
4.66
5.75
− 1.09 = top ℄ cleanout.

483' offset East ℄
~~9' offset~~

Book 1219-37

B.M. S.W. Top Hydt. Whitman + Taylor = 8.89 = B.M.
1.58 +
10.47 = π
5.39 −
5.08 = T.P.
2.86 +
See P-16 — 7.94 = π

S.E. B.P. Jaun + Taylor = 4.72
5.00
9.72 = π

4.72 = B.M.
5.79
10.51 = π

Storm Drain #1 Concrete Section

591' " " −0.1

7+00 Above =0+00	10.47	5.96	4.51	−0.00	+4.51
+47		5.39	5.08	−0.13	+5.21
+94 T.P.	7.94	4.98	2.96	−0.27	+3.23
1+41		4.91	3.03	−0.41	+3.44
+88		4.88	3.06	−0.54	+3.57
2+35		4.93	3.01	−0.68	+3.69
2+82		4.80	3.14	−0.81	+3.95
3+29		4.23	3.71	−0.94	+4.65

Cont. on P-16

TAYLOR St. Storm Drain

Cont. from P-15

7.94 = π

			Flow Line Grades
3+76	6.00	1.94	-1.08
4+23	6.52	1.42	-1.21
+65.95 = ℄ Cleanout. Type A. = Δ R46°01'48"	6.90	1.04	-1.34
(45.76)3 5+11.7	4.86	3.08	-1.47
+57.47	6.74	1.20	-1.58
6+03.23 = End. = NELY Line Santa Fe. Rt. Way	6.59	1.35	-1.72

CULVERTS

No 1 20' of 6" Sewer Pipe	
0+00 = End	2.30
+20 = ℄ Storm Drain	-0.50
No 2 = 25'-6" Sewer pipe	
0+00	3.80
+25 = ℄ Storm Drain	0.00
No 3 = 25'-6" Sewer Pipe	
0+00	5.40
+25 = ℄ Storm Drain	1.60
No 4 = 25'-6" Pipe	
0+00	5.70
+25 = ℄ Storm Drain	3.80

+3.02	Chk. on B.M. Pole Taylor San Diego
+2.63	
+2.38	
+4.55	
+2.78	
+3.07	

7.94 = π
4.95
2.99
2.94 = B.M.
20V = diff.

7.94 = π
2.86
5.08
4.12 +
9.20 = π

Location 11.83 West E Line Taylor And W 7' Line Rosecrans St. 2-27-29

10' Storm Drain Restaked.

6+03.23 = End on opp. Page = 0+00

				Flow Line	Cuts
= 0+00	6.92 = π	8.64	-1.72	-1.72	✓
+27.45	6.43	8.08	-1.65	-1.65	✓
+54.90		8.00	-1.57	-1.57	✓
+82.35		7.92	-1.49	-1.49	✓
1+09.8		7.84	-1.41	-1.41	✓
1+38.9 = Δ = 0+00 = ℄ Cleanout 46°01'48" Lt.	7.81 = π 4.50 = top ℄ cleanout 3.31 5.58 -2.27	7.76	-1.33	-1.33	✓
0+23.87		7.69	-1.26	-1.26	✓
+48.87		7.62	-1.19	-1.19	✓
+73.87		7.55	-1.12	-1.12	✓
+98.87		7.48	-1.05	-1.05	✓
1+21.87		7.42	-0.99	-0.99	

B.M. P-78 = → 1.85
5.07 +
6.92 = π
5.07 -
1.85 = T.P.
4.58 +
6.43 = π

π 10.47

3+16.33	5.70	4.77	-0.29	
4+14.33 = SL Sawn.	10.61	-0.14	-0.14	+5.06

SEWER Const. in San Diego Ave
Bet. Taylor and Wallace sts

MH # 1	10.43	6.24		0.80	3.39
= 0+00 = ℄ Exist Sewer in Taylor St.			4.19	0.59	+ 3.60
(50.62') 8				2.83	
0+50.62		6.38	4.05	1.12	+ 2.93
1+01.24 Brk.		5.31	5.12	1.65	+ 3.47
+51.86		4.32	6.11	2.18	+ 3.93
2+02.48		3.44	6.99	2.70	+ 4.29
+53.10		2.53	7.90	3.23	+ 4.67
3+03.7		1.81	8.62	3.75	+ 4.87
+54.3		0.94	9.49	4.28	+ 5.21
4+05 = DE.		0.08	10.35	4.80	+ 5.55

TAYLOR St. Storm Drain {Restaking}
Cont. from P-16

8.49 = ⊼
4.20 = top MH cover
4.29 = ⊼
4.31
-0.02

B.M. on 62.29' Radius hub P-10 = 1.85
8.58 +
10.43 = ⊼

1.14
1.16

1.85 = B.M.
6.64 +
8.49 = ⊼

WATER Services Grades on Lasalla Blvd.
Bet. Trias And Conde St.

S.L. sta	S.L. cb Grades	N.L. sta.	N.L. cb. Grades
200' W.W.L. Trias		~~200' W.W.L. Trias~~	
= 0+00 = ℄ Water Service	+0.7	~~= 0+00 = Water Service~~	
+50 = " " "	+0.5	~~0+50 = " "~~	
S.W. Cor. Congress = 0+00		W.L. Ampudia = 0+00	
+52.29 = ℄ " "	40.43	+73.86 = ℄ Water Service	41.24
1-80'			
1+32.29 = " " "	38.86	1+23.86 = " " "	40.30
	1.12	1-80'	
+82.29 = " " "	37.74	2+03.86 = " " "	38.50
1-57	36.50	1-105'	
2+37.29 = " " " = 49' E.E.L. Arista		2+08.86 = " " = 45' E.E.L. Arista	36.13
W.L. Arista = 0+00		90' W ℄ Arista = Water.	33.69
+25 = ℄ Water Service	33.85		
+75 = " " "	33.54		
1+25 = " " "	33.23		

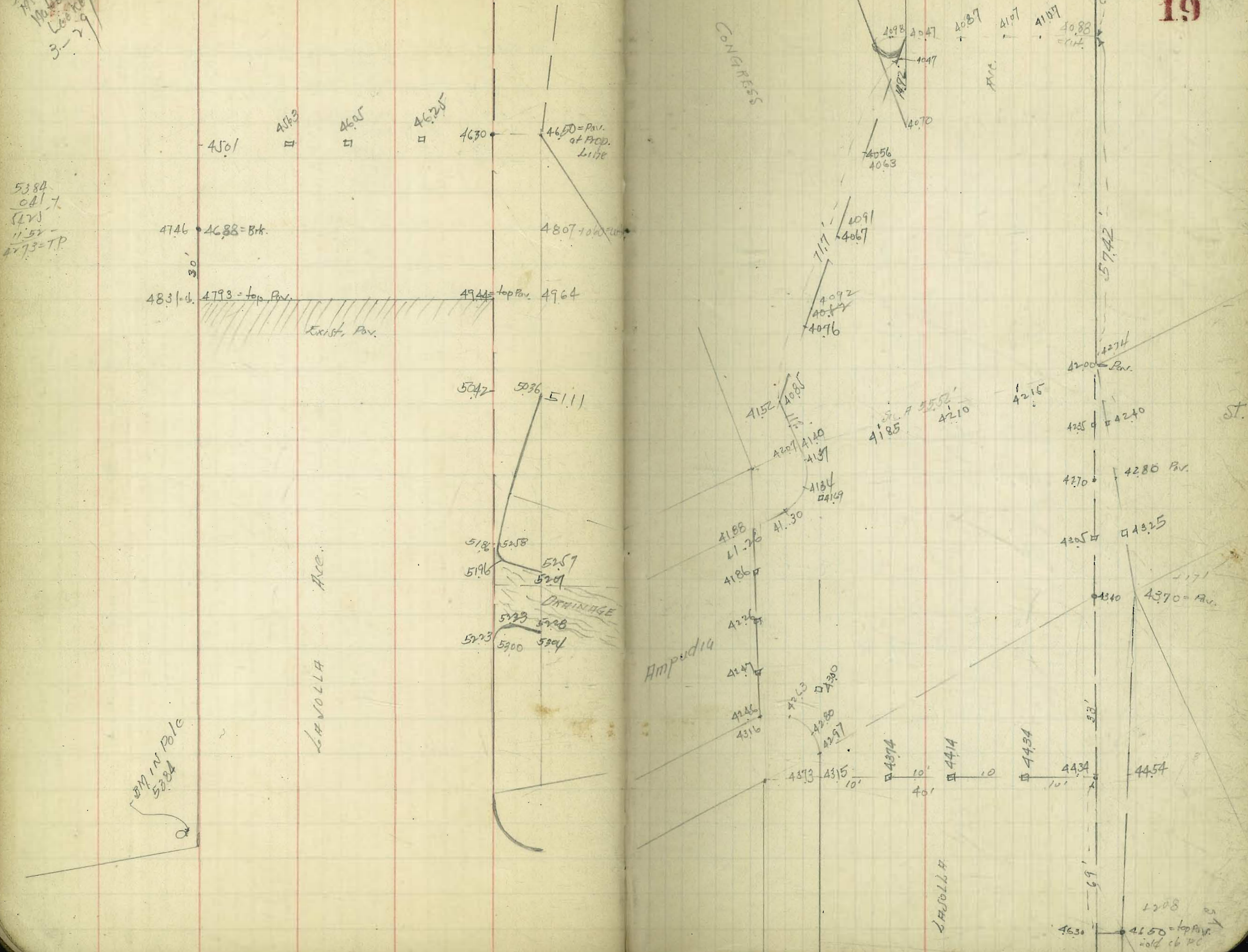
Raked

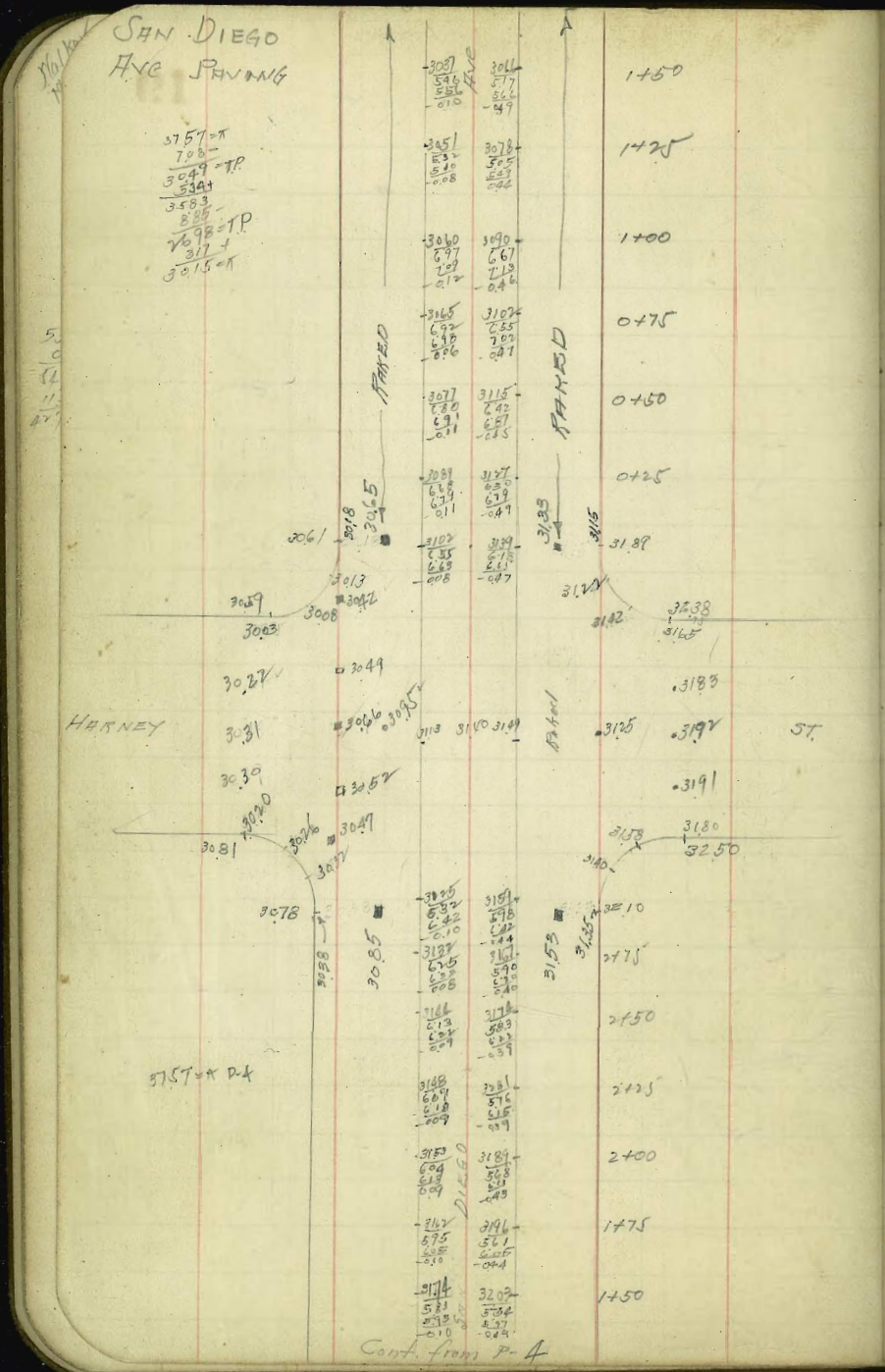
35.16 = BM. S.E. Pole Lasalla + Arista
5.59 +
40.75 = π

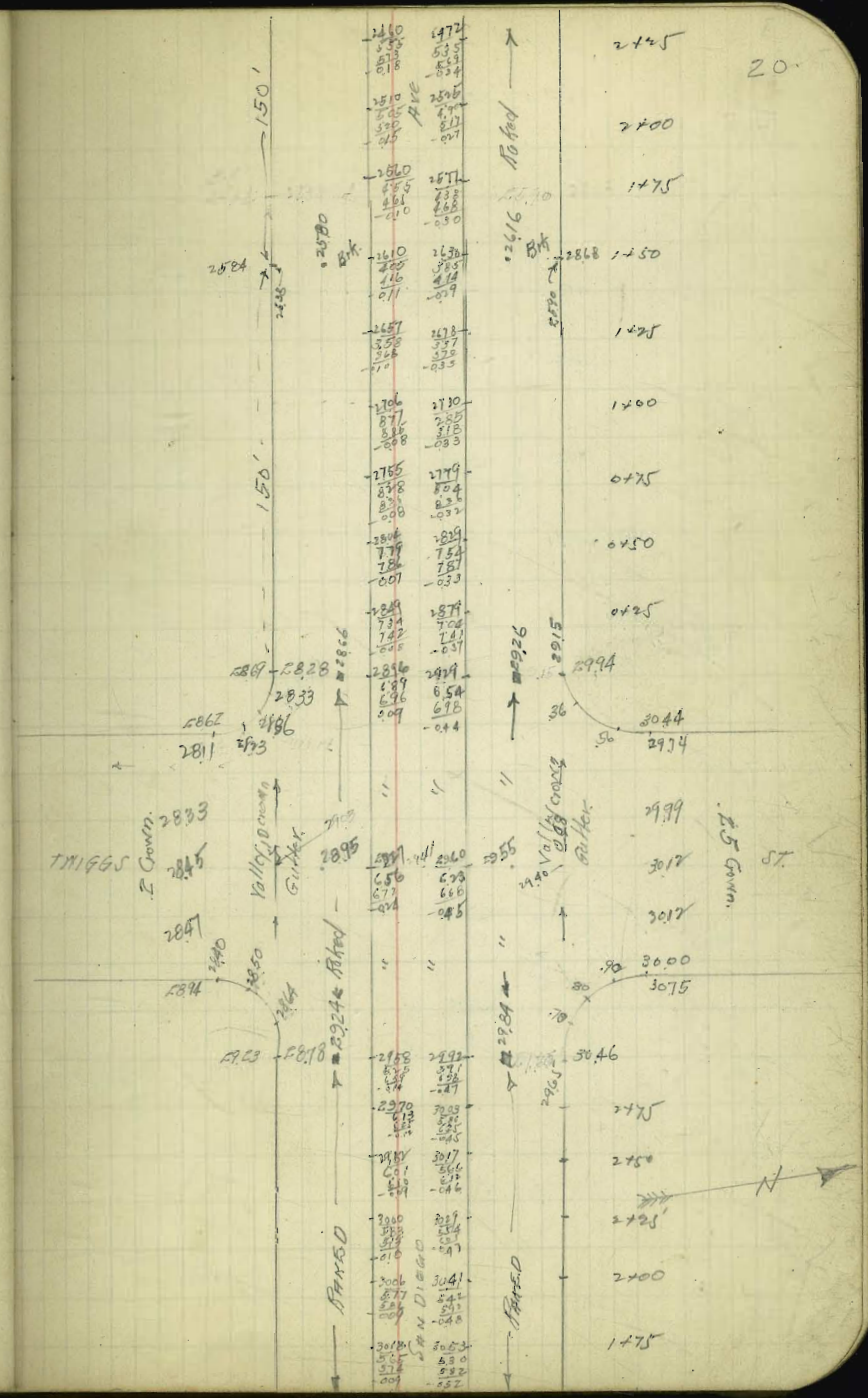
S	40.43	38.86	37.74	36.50	33.85	33.54	33.23
	0.32	1.89	3.01	4.25	6.90	7.21	7.52
	1.26	5.07	6.79	7.25	9.61	10.19	9.93
	−0.94	−3.18	−3.78	−3.00	−2.71	−2.98	−2.41
N	41.24	40.30	38.50	36.13	33.69		
	+0.49	0.45	2.25	4.62	7.06		
	+.23	1.30	3.58	7.27	6.11		
	−0.26	−0.85	−1.33	−2.65	+0.95		

LaJolla Ave Paving

Cont. on P-4
" " P-30

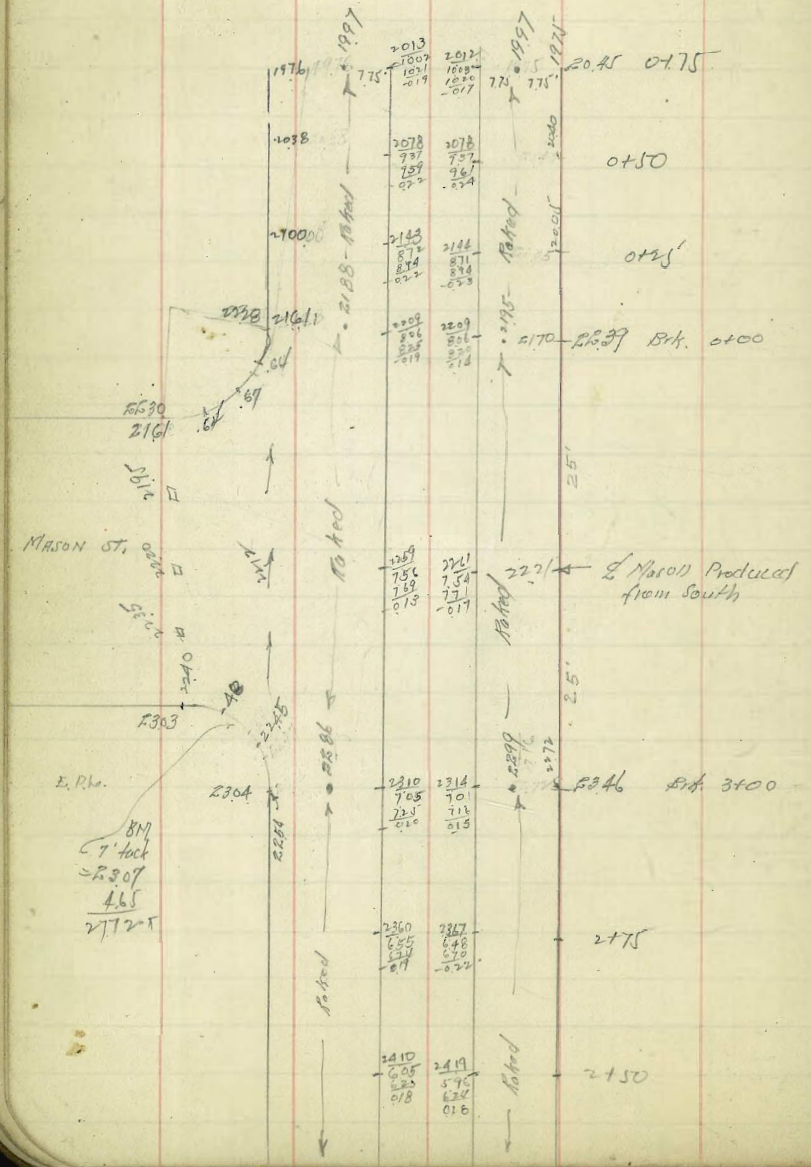



SAN DIEGO
AVE PAVING
HARNEY
ST.
RAKED
DIEGO
Cont. from P-4


20
TRIGGS
ST.
Valley Crown
Gutter
Raked
SAN DIEGO
N

San Diego Ave.

Paving.



Walker
McHugh
Leeker
Mahoon
3-27-29

LEVELS ON EXIST. PAVING {STRIP}
SAN DIEGO AVE
Bet. Conde And Mason st. on North.

	5.10	36.08		30.98	B.M. S.W. Conde & San Diego
	W.L. Conde = 0+00				
N			3.78	32.30	
℄			3.96	32.12	
S			4.25	31.83	
		0+25			
S			4.25	31.83	
℄			4.05	32.03	
N			4.03	32.05	
		0+50			
N			4.17	31.91	
℄			4.09	31.99	
S			4.19	31.89	
		0+75			
S			4.30	31.78	
℄			4.21	31.87	
N			4.33	31.75	
		1+00			
N			4.35	31.73	
℄			4.26	31.82	
S			4.34	31.74	
		1+25			
S			4.39	31.71	
℄			4.30	31.78	
N			4.41	31.67	

36.08

	1+50		
N		4.51	31.57
℄		4.37	31.71
S		4.44	31.64
	1+75		
S		4.58	31.50
℄		4.48	31.60
N		4.59	31.49
	2+00		
N		4.65	31.43
℄		4.55	31.53
S		4.65	31.43
	2+25		
S		4.70	31.38
℄		4.61	31.47
N		4.70	31.38
	2+50		
N		4.77	31.31
℄		4.67	31.41
S		4.74	31.34
	2+75		
S		4.86	31.22
℄		4.72	31.36
N		4.85	31.23
	3+00 = East Line Harney		
N		4.95	31.13

36.08

L			4.83	31.25
S			4.93	31.15
T.P	4.46	35.13	5.41	30.67
		L HARNEY		
S			4.16	30.97
L			4.07	31.06
N			4.12	31.01
		N.L. HARNEY = 0+00		
N			4.20	30.93
L			4.11	31.02
S			4.21	30.92
		0+25		
S			4.40	30.73
L			4.24	30.89
N			4.38	30.75
		0+50		
N			4.17	30.66
L			4.37	30.76
S			4.51	30.62
		0+75		
S			4.57	30.56
L			4.47	30.66
N			4.60	30.53
		1+00		
N			4.14	30.39
L			4.59	30.54

35.13

S		4.65	30.48
	1+25		
S		4.72	30.41
L		4.67	30.46
N		4.83	30.30
	1+50		
N		4.99	30.14
L		4.85	30.28
S		4.88	30.25
	1+75		
S		5.07	30.06
L		4.99	30.14
N		5.14	29.99
	2+00		
N		5.21	29.92
L		5.09	30.04
S		5.18	29.95
	2+25		
S		5.14	29.89
L		5.19	29.94
N		5.16	29.97
	2+50		
N		5.43	29.70
L		5.31	29.82
S		5.43	29.70
	2+75		

35.13

S			5.59	29.54
L			5.45	29.68
N			5.57	29.56
	3+00 = E.L. TWIGGS			
N			5.71	29.42
L			5.58	29.55
S			5.71	29.42
T.P.	3.89	32.90	6.12	29.01
	L TWIGGS			
S			3.86	29.10
L			3.66	29.34
N			3.77	29.13
	E.L. TWIGGS = 0+00			
N			4.08	28.82
L			3.99	28.91
S			4.06	28.84
	0+25			28.39
S			4.51	27.39
L			4.40	28.50
N			4.50	28.40
	0+50			
N			4.97	27.93
L			4.81	28.09
S			4.96	27.94
	0+75			
S			5.45	27.45

23

L			5.33	27.57
N			5.47	27.43
	1+00			
N			5.93	26.97
L			5.79	27.11
S			5.94	26.96
	1+25			
S			6.44	26.46
L			6.31	26.59
N			6.47	26.43
	1+50			
N			6.91	25.99
L			6.81	26.09
S			6.94	25.96
	1+75			
S			7.42	25.48
L			7.33	25.57
N			7.44	25.46
	2+00			
N			7.95	24.95
L			7.87	25.03
S			7.95	24.95
	2+25			
S			8.48	24.42
L			8.36	24.54
N			8.44	24.46

		32.90			
		2+50			
N			8.98	23.92	
℄			8.91	23.99	
S			9.00	23.90	
		2+75			
S			9.47	23.43	
℄			9.41	23.49	
N			9.45	23.45	
		3+00 = E.L. Mason on S			
N			9.90	23.00	
℄			9.86	23.04	
S			9.98	22.92	
T.P.	3.16	26.24	9.82	23.08	SE. 7' tack R 78 Mason + S Diego
		℄ Mason on South			
S			3.82	22.42	
℄			3.74	22.50	
N			3.86	22.38	
		N.L. Mason on South = 0+00			
N			4.32	21.92	
℄			4.24	22.00	
S			4.36	21.88	
		0+25			
S			5.08	21.16	
℄			4.99	21.25	
N			5.07	21.17	
		0+50			

	26.24		
N		5.76	20.48
℄		5.64	20.60
S		5.73	20.51
	0+75 = End Job.		
S		6.31	19.93
℄		6.22	20.02
N		6.34	19.90

Walter McHugh Leeky McHoon 3-29-29

X. Section 38.67 Roadway & 20' Exist Pav. Strip Lajolla Ave.
from station 0+81.4 Page 1 this Book
to E.L.Y. Line Conde st.

S.E. B.P. Ampudia & Lajolla Page 78

	0.92	44.67		43.75
	0+81.4 Page 1 = 0+00 = End Exist Paving			
N top cb.			4.39	40.28
" curb cut.			5.06	39.61
" edge Pav.			5.24	39.43
℄ "			5.05	39.62
S edge "			5.17	39.50
S curbcut.			5.37	39.30
	0+35.5			
S top cb.			5.44	39.23
" Gut.			6.17	38.50
S edge Pav.			6.05	38.62
℄ "			5.90	38.77
N " "			6.06	38.61
N Gut.			5.88	38.79
	0+68.5			
N "			6.63	38.04
N edge Pav.			6.81	37.86
℄ " "			6.69	37.98
S " "			6.83	37.84
" Gut.			6.91	37.76
	1+01.5			
" "			7.65	37.02
" edge Pav.			7.58	37.09
℄ "			7.44	37.23

	44.67		
N edge Pav.		7.57	37.10
" Gut.		7.36	37.31
	1+34.5		
" "		8.10	36.57
" edge Pav.		8.22	36.45
℄ "		8.13	36.54
S " "		8.24	36.43
" Gut.		8.38	36.29
	1+67.5		
" "		9.11	35.56
S edge Pav		8.94	35.73
℄ "		8.82	35.85
N " "		8.98	35.69
" Gut.		8.86	35.81
	2+00.5 = End cb on South 4' E.E.L. Arista		
N top cb		8.94	35.73
" Gut.		9.59	35.08
N edge Pav.		9.70	34.97
℄ "		9.55	35.12
S " "		9.69	34.98
S Gut.		9.87	34.80
" top cb.		9.18	35.49
T.P. 202	37.52	9.17	35.50
	2+30 = P.C. on N		
S edge Pav.		3.17	34.35
℄ "		3.02	34.50

37.52

N edge Pav.		3.16	34.36
" Gut		3.10	34.42
" top cb.		2.42	35.10
	2+47.8 on N		
" Gut.		3.43	34.09
Gut + 9.5 = N edge Pav.		3.50	34.02
℄ on Rim M.H.		3.20	34.32
" " Pav.		3.38	34.14
S edge Pav.		3.51	34.01
	2+76 on N = E.C.		
S top cb.		3.51	34.01
" Gut.		4.21	33.31
" Gut + 9.3 = S edge Pav.		3.91	33.61
℄ Pav.		3.71	33.81
N "		3.81	33.71
+ " + 9.4 = N Gut.		3.78	33.74
N top cb		3.10	34.42
	2+88 = Rt. Δ to N W.L. Ansta on N = 0+00		
N top cb		3.43	34.09
" Gut.		4.18	33.34
N Pav.		4.04	33.48
℄ "		4.01	33.51
S "		4.18	33.34
" Gut.		4.35	33.17
	0+30.5		
" "		4.53	32.99

37.52

S. Pav.		4.34	33.18
℄ "		4.21	33.31
N "		4.33	33.19
N. Gut.		4.33	33.19
	0+55.5		
N "		4.43	33.09
" Pav.		4.46	33.06
℄ "		4.34	33.18
S "		4.52	33.00
S Gut.		4.69	32.83
	0+80.5		
S "		4.84	32.68
" Pav.		4.66	32.86
℄ "		4.52	33.00
N "		4.63	32.89
" Gut.		4.52	33.00
	1+05.5		
" Gut.		4.62	32.90
" Pav.		4.78	32.74
℄ "		4.68	32.84
S "		4.79	32.73
" Gut.		5.00	32.52
	1+30.5		
S "		5.16	32.36
" Pav.		4.96	32.56
℄ "		4.83	32.69

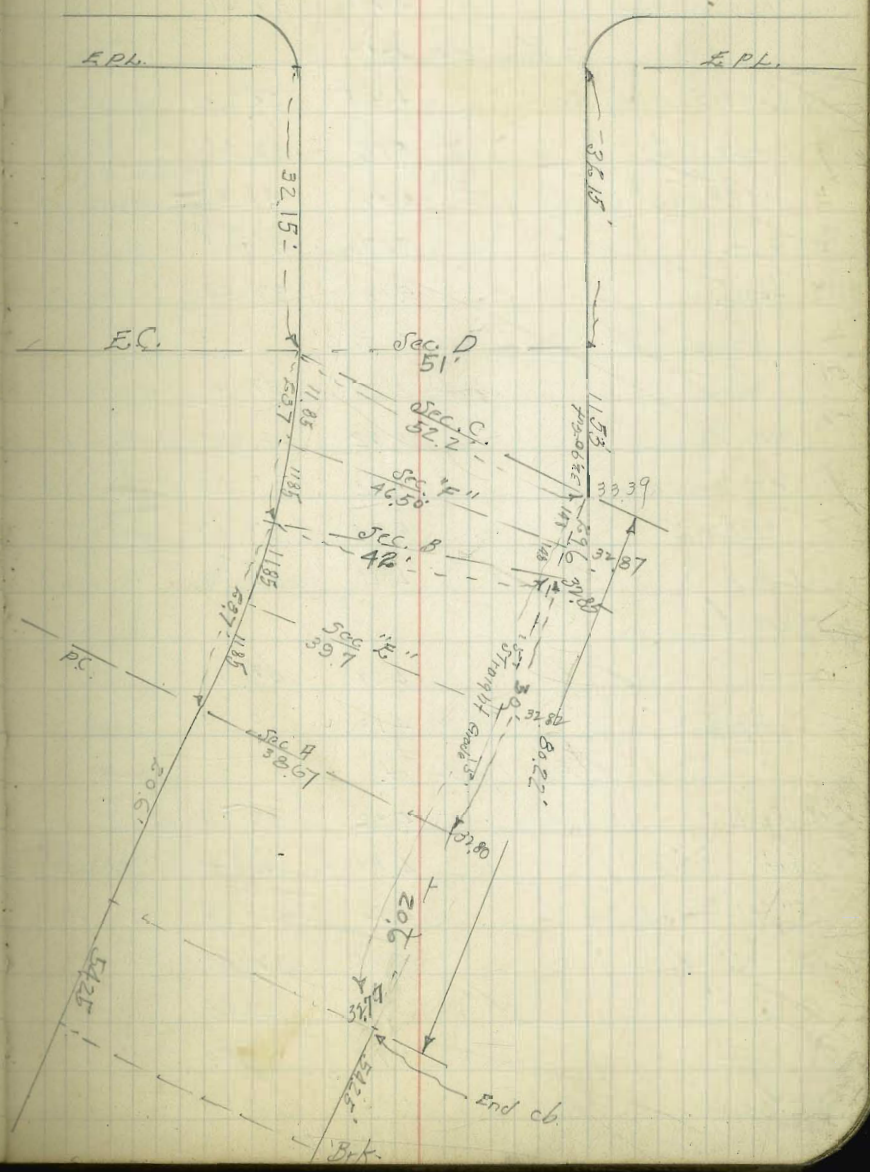
3752

N Pav.		4.96	37.56
" Gut.		4.72	37.80
	1+35.5 = Brk. on N Page 2		
N top cb.		4.30	33.22
" Gut.		4.81	37.71
" Pav.		4.99	37.53
L "		5.02	37.50
S "		5.25	37.27
" Gut.		5.32	37.20
" top cb.		4.62	37.90
	1+82.87		
" Gut.		5.49	37.03
" top Pav.		5.39	37.13
L "		5.15	37.37
N "		4.94	37.58
" Gut.		4.78	37.74
	2+10 = End cb. on N		
N top cb.		4.24	38.28
" Gut.		4.75	37.77
N Pav.		4.92	37.60
L "		5.21	37.31
S "		5.62	31.90
" Gut.		5.67	31.85
" top cb.		4.99	37.53
	Section A = P.C.		
" Gut.		5.81	31.71

Note. Make Cross Valley Gutter to S. this Section

CONDE

57



37.52

S Gut + 4.5' = S edge Pav.	5.59	31.93
" " + 15.8 = ℄ Exist Pav.	5.08	32.44
" " + 27.1 = N edge "	4.91	32.61
Section B = 42'		
N cb + 15.5 = N edge Pav.	4.89	32.63
" " + 27 = ℄ "	5.16	32.36
" " + 38.5 = S " "	5.57	31.95
S Gut.	5.87	31.65
" top cb.	5.18	32.34
Section C = 52.2		
" " "	5.21	32.31
" Gut.	5.92	31.60
" " + 6' = S edge Pav.	5.72	31.80
" " + 18.75 = ℄ "	5.20	32.32
" " 30.5 = N " "	4.96	32.56
N Gut.	4.59	32.93
" top cb.	4.13	33.39
E.P.L. Conde st.		
N top cb.	4.32	33.20
" Gut.	4.89	32.63
" " + 16.5 = N edg Pav.	4.94	32.58
27.7 = ℄ "	5.20	32.32
38.9	5.67	31.85
S Gut.	5.99	31.53
" top cb.	5.33	32.19

Additional Cross Sections
For Section "E" And "F" Sketch

6.65	38.62		31.97 SSY. B.P. Conde San Diego
Sec. "E" = 39.7			
S Gut.		6.96	31.66
+ 3.3 = S pav.		6.66	31.96
+ 14.9 = ℄ "		6.30	32.32
+ 19.8 = ℄ St. on Pav.		6.19	32.43
+ 26.5 = N Pav. Exist		6.01	32.61
+ 39.7 = N. Pav. Proposed			32.82
Sec. "F" = 46.5			
S. Gut.		7.00	31.62
+ 4.2 = S pav.		6.74	31.88
+ 16 = ℄ Pav.		6.34	32.28
+ 23.25 = ℄ St. on Pav.		6.13	32.49
+ 27.7 = N. Pav.		6.03	32.59
+ 46.5 = " "			32.87
℄ Conde			
5.19	37.16		31.97 = Above BM
S Gut.			
S Pav		5.28	31.88
℄ Pav.		4.91	32.25
N "		4.61	32.55
N Gut.			

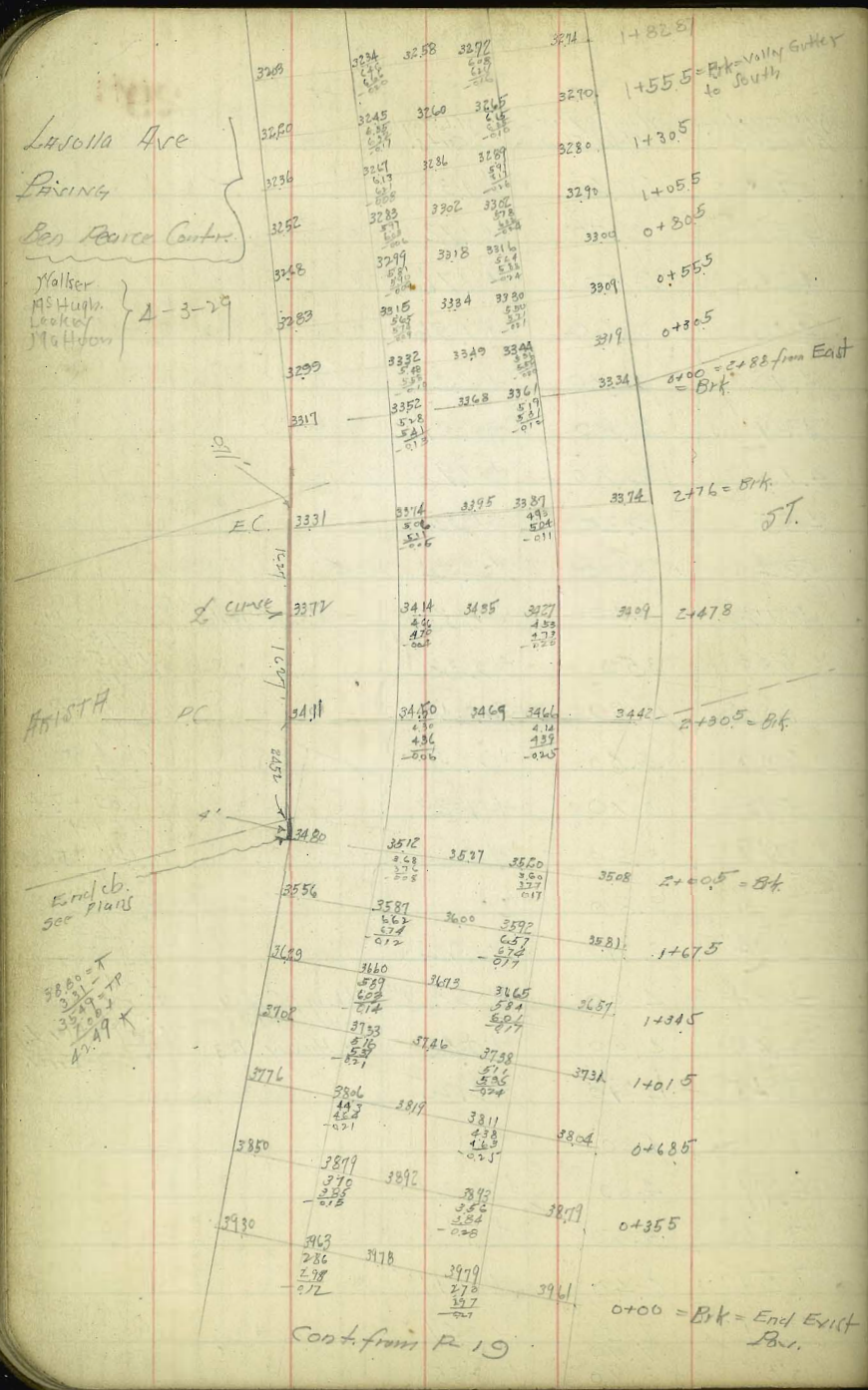
Sewer Laterals in Taylor St. Bet. Calhoun & Hickory St.

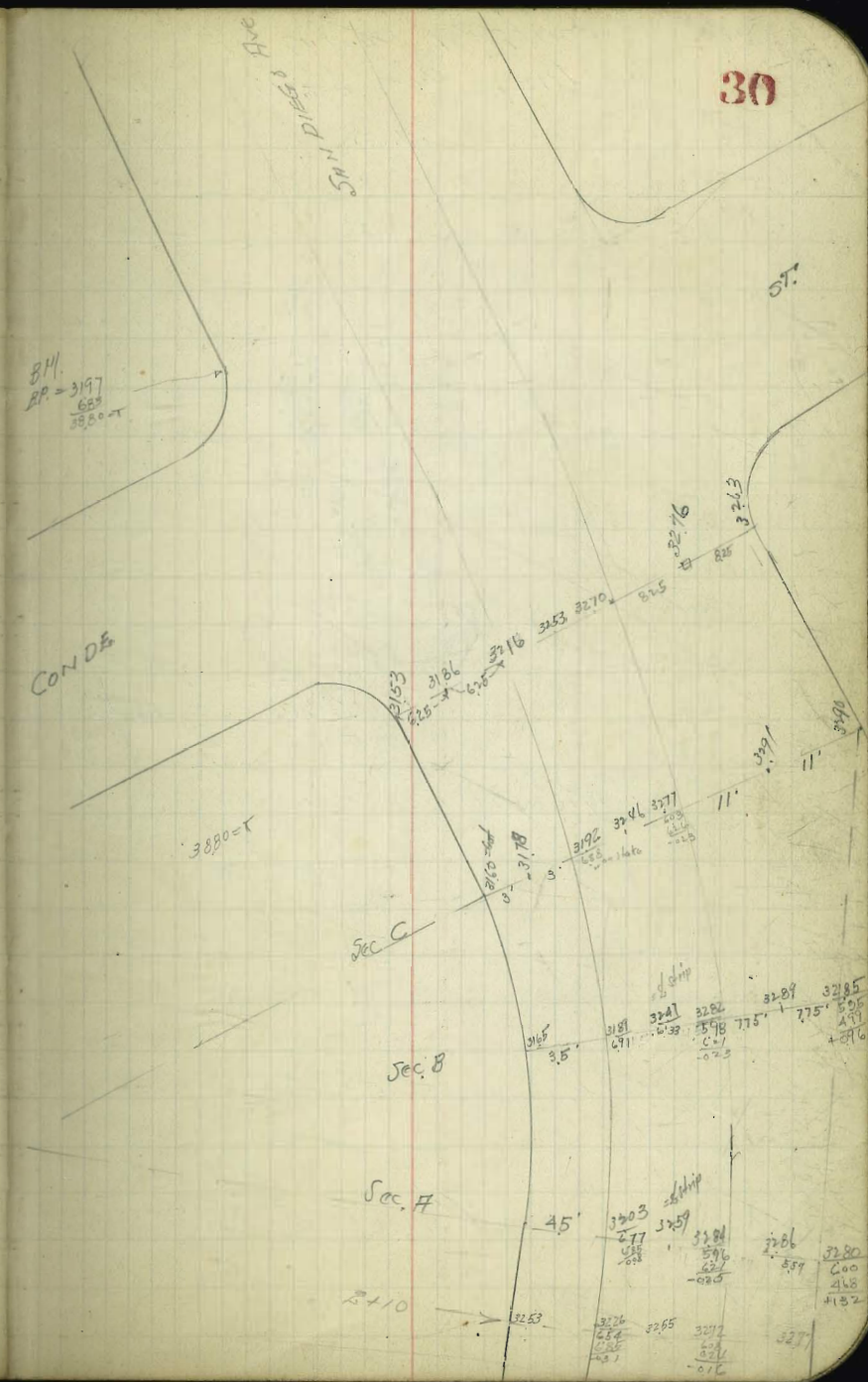
Note. 0+00 on each lateral = ℄ Trunk line
Sta. 0+37.5 Sta. 0+37.5 Sta. 0+37.5

Lateral No.	Rods	Elev. Stub.	Elev. Flow line	Cuts	W.L. Taylor Rocks	W.L. Taylor Elev. Stub.	W.L. Taylor Elev. Flow	W.L. Taylor Cuts
#53	5.28	3.94	1.65	+2.29	5.44	3.78	2.40	+1.38
#51	5.11	4.11	1.75	+2.36	5.00	4.22	2.50	+1.72
#49	5.00	4.22	1.75	+2.47	4.96	4.26	2.50	+1.76
#47	4.85	4.37	1.85	+2.52	5.06	4.16	2.60	+1.56
#45	4.57	4.65	1.95	+2.70	4.80	4.92	2.70	+2.22
#43	4.23	4.99	2.05	+2.94	4.33	4.89	2.80	+2.09
#41	4.10	5.12	2.05	+3.07	4.44	4.78	2.80	+1.98
6" Special	3.89	5.33	2.30	+3.03	4.67	4.55	3.20	+1.35
#35	Note Leave out this one				3.68	5.54	3.30	+2.24
#33			2.65		4.90	5.75	3.40	+2.35
#31			2.75		4.77	5.88	3.50	+2.38
#29			2.85		4.59	6.06	3.60	+2.46
#27			2.85		4.56	6.09	3.60	+2.49
#25			2.95		4.72	5.93	3.70	+2.23
#23			3.05		3.28	7.19	3.80	+3.39
#21 Left out.			3.05				3.80	
#19			3.15		4.53	6.14	3.90	+2.24
#17			3.25		5.16	6.24	4.00	+2.24
#15 Moved to #13=60' S/L. Chestnut St.			3.25		5.00	6.40	4.00	+2.40
			3.43 3.35		4.95	6.45	4.20	+2.25
#11 Left out			3.45				4.20	
#9 " "			3.85		4.41	6.99	4.60	+2.39
#7 " "			4.75		10.17	7.26	5.50	+1.76
#5 =6"			5.60		9.92	7.51	6.40	+1.11
#3 Leave out			6.65		9.62	7.81	7.40	+0.41
#2 =6"			7.70		7.53	9.90	7.90	+2.00
#1 = Leave out			8.15		4.98	12.45	8.90	+3.55

Sta. B.P. Taylor & Jason 4.72 - BM.
5.98 +
10.65 - T
3.94 -
6.71 - TP
3.96
10.67 = T
3.84 -
6.83 - TP
4.57 +
11.40 = T
+1.41 -
6.99 - TP
10.44 +
17.43 = T
4.84
12.59
12.59 = Elev. Stub
000 - Error

chk. on P.C. Stub on W. = at 10' S of W. cor. Hickory & 3


Lasolla Ave
Paving
Ben Pearce Contr.
Wallser
McHugh
Leakey
Mattoon
4-3-29
1+82.87
1+55.5 = Brk = Valley Gutter to South
1+30.5
1+05.5
0+80.5
0+55.5
0+30.5
0+00 = 2+88 from East = Brk.
2+76 = Brk.
ST.
E.C.
℄ curve
ARISTA
P.C.
2+30.5 = Brk.
End cb. see plans
2+00.5 = Brk.
1+67.5
1+34.5
1+01.5
0+68.5
0+35.5
0+00 = Brk = End Exist Pav.
Cont. from P 19


San Diego Ave
ST.
BM.
BP. = 3197
CONDE
Sec C
Sec B
Sec A
2+10

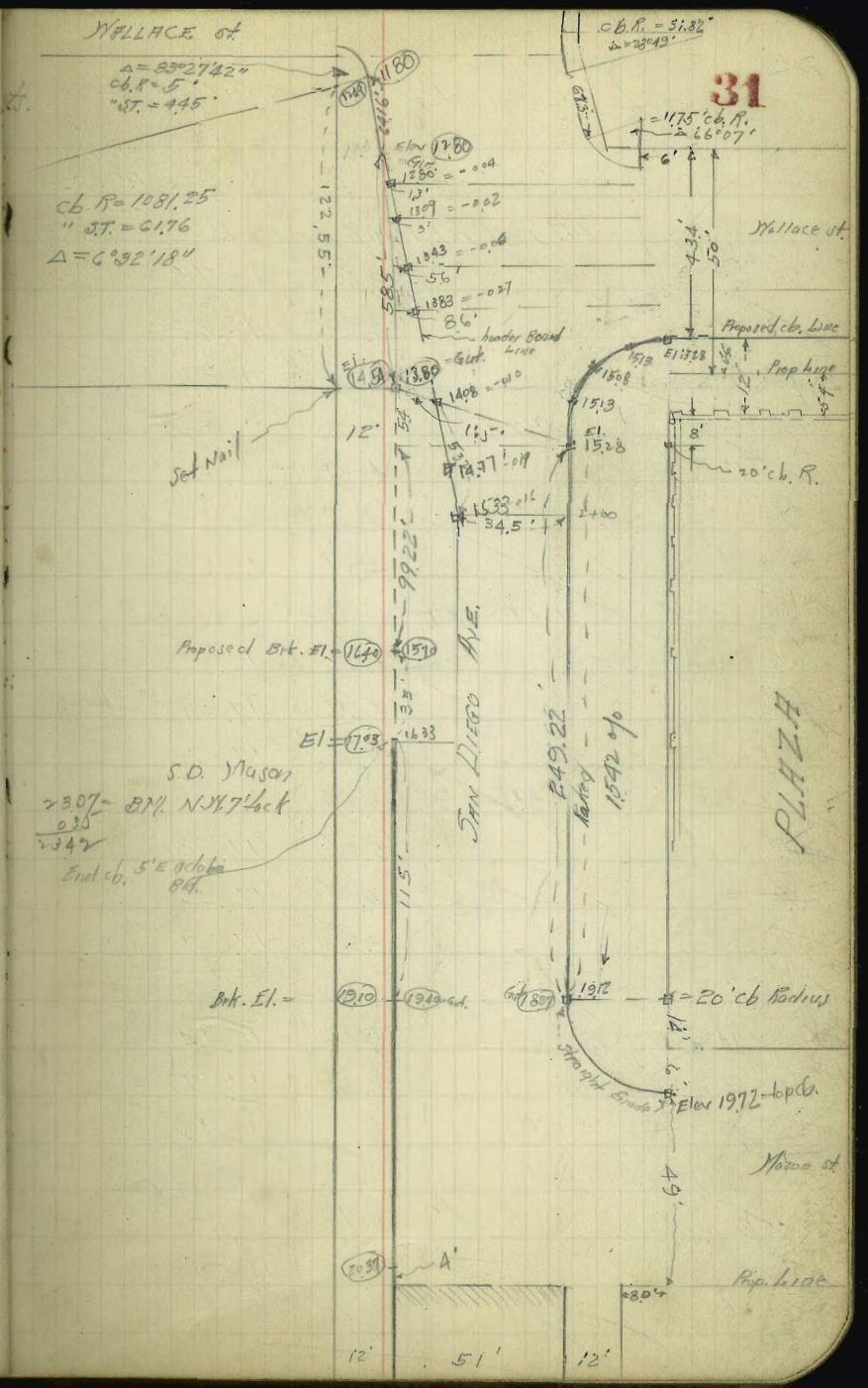
GRADING and PAVING of
SAN DIEGO AVE. bet. Mason & Wallace St.

	N.L. Sta.	N.L. Grade
c.b. P.C.		19.72
1		19.57
2		19.42
3		19.27
0+12 = c.b. R.		19.17
0+38.62		19.10
0+68.8		18.29
1+08.62		17.48
1+48.67		16.67
1+88.67		15.87
2+28.67 = 8'E EL Wallace		15.20
2+68.67 = c.b. P.C.		15.06

For Grades See sketch Page 12

19.17 19.10 18.29 17.48 16.67 15.87 15.06

G-155



X. Section Exist. PAVING
on SAN DIEGO Ave.
Bet. Mason St. on North & Wallace St. on South

	3.33	22.45	19.12

Elev. cb = P.C. P-31
P-31 P.C. = 0+00

14' West M.L. Mason on North = cb

Ncb +15.5 N=on Pav.		3.70	18.75
℄ Pav.		3.62	18.83
S "		3.76	18.69
	0+25		
S "		4.17	18.28
℄		4.07	18.38
N "		4.16	18.29
	0+50		
N "		4.59	17.86
℄ "		4.56	17.89
S "		4.62	17.83
	0+75 = P.C. Pav.		
S "		5.07	17.38
℄		5.01	17.44
N		5.08	17.37
	1+00		
Ncb +14.8 = N. Pav.		5.51	16.94
℄ "		5.38	17.07
S "		5.53	16.92
	1+25		
S Pav.		5.97	16.48
℄ "		5.86	16.59
N Pav. - cb - 14'			

	2+45		
	1+50		
Ncb. +12.9 = N. Pav.		6.39	16.06
℄ Pav.		6.27	16.18
S "		6.41	16.04
	1+75		
S "		6.85	15.60
℄ "		6.69	15.76
Ncb - 11.9		6.79	15.66
	2+00		
Ncb +10.6 = Pav.		7.17	15.28
℄ "		7.18	15.27
S "		7.32	15.13
	2+25		
S "		7.89	14.56
℄		7.58	14.87
Ncb -		7.51	14.84
	2+55 = opp cb. on N		
Ncb +11.1		7.67	14.78
℄		8.13	14.32
S		8.39	14.06
TP 344	18.72	7.17	15.28
	Sec A		
Ncb + 3.5 = Nedge Pav.		3.86	14.86
+18.5 = ℄ Pav.		4.14	14.58
+27' = ℄ Sec A		4.45	14.27
+28.5 = Sedge Pav.		4.48	14.24

18.72

Sec B = 54.4'

N Gut		
+10.7 = N edge Pav.	4.19	14.53
+20.7 = ℄ "	4.43	14.29
+27.2 = ℄ Sec B.	4.69	14.03
+30.7 = S edge Pav.	4.87	13.85

Sec. C = 55.6'

N Gut. + 11.8 = N edge Pav.	4.39	14.33
" " +21.8 = ℄ "	4.67	14.05
+27.8 = ℄ Sec C	4.93	13.79
+31.8 = S edge Pav.	5.13	13.59

Sec D = 57.4

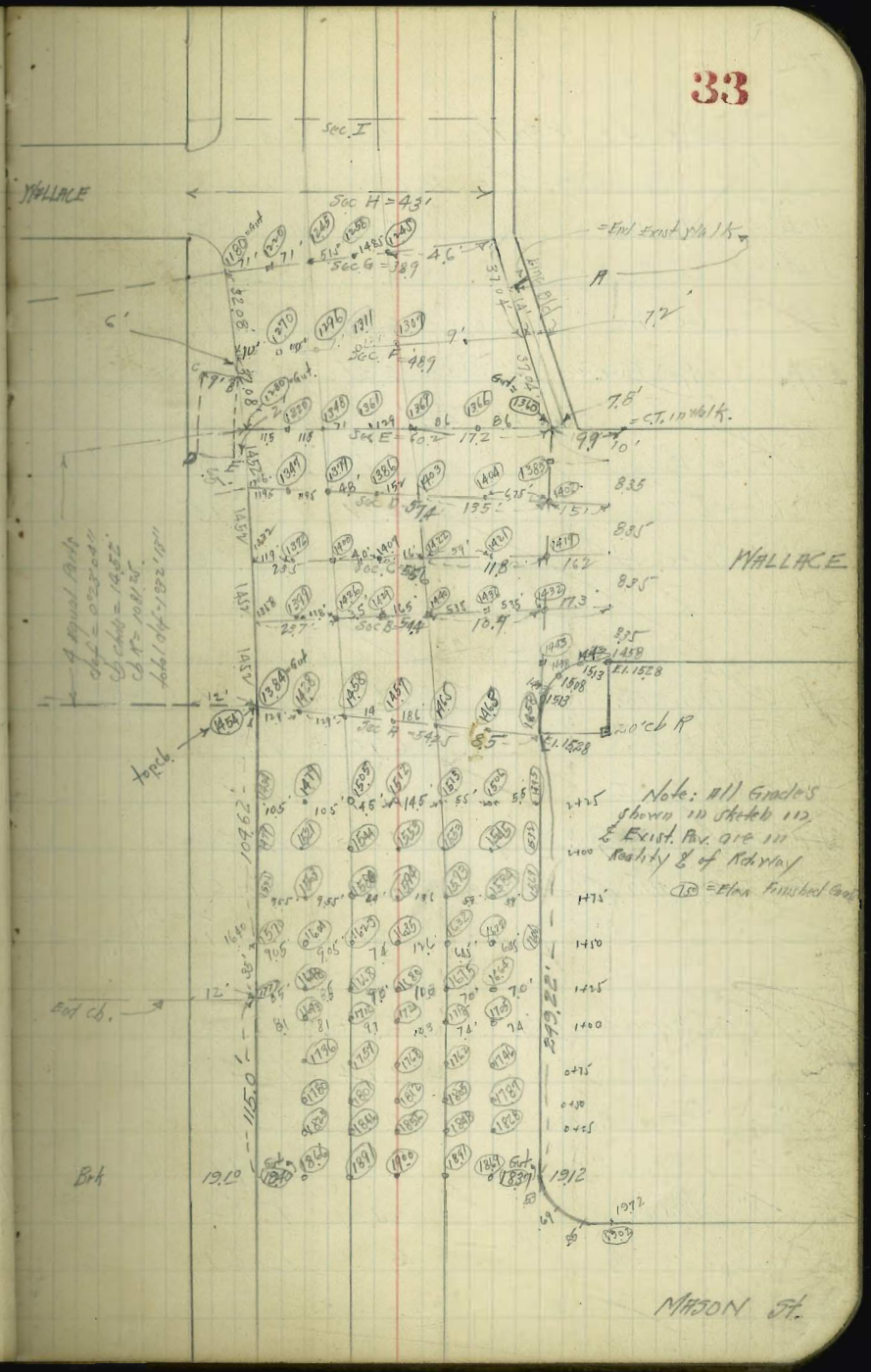
N Gut		
+13.5' = N edge Pav.	4.57	14.15
+23.5 = ℄ "	4.87	13.85
+28.7 = ℄ Sec D	5.13	13.59
+33.5 = S edge Pav.	5.36	13.36

Sec. E = 60.2'

N Gut		
− 4' = top Exist Walk.	4.46	14.26
N. Gut		
+17.2 = N edge Pav.	4.84	13.88
+27.2 = ℄ "	5.14	13.58
+30.1 = ℄ Sec E	5.28	13.44
+37.2 = S edge Pav.	5.71	13.01

Sec F = 48.9

N. Gut.		
− 3.3 = top Walk	4.41	14.31
N. Gut.		
+9' = N edge pav.	5.40	13.32
+19 = ℄ "	5.66	13.06
+24.45 = ℄ Sec F	5.86	12.86
+29 = S edge Pav.	6.02	12.70



1872

A on End Exist Walk on N	4.50	14.22
Sec. G = 38.9		
N. Gut		
+4.6 = N edge Pav.	6.37	12.35
+14.6 = ℄ "	6.30	12.42
+19.45 = ℄ Sec. G	6.31	12.41
+24.6 = S edge Pav.	6.37	12.35
Sec. H = 43'		
Next +7.6'		
- N edge Pav	6.79	11.93
+17.6 = ℄ "	6.57	12.15
+21.5 = ℄ Sec. H	6.52	12.20
+27.6	6.50	12.22
Sec. I = 43' (?)		
South Gut		
+6' = S edge Pav.	6.69	12.03
+16 = ℄ Pav.	6.90	11.82
+21.5 = ℄ Sec. I	7.10	11.62
+26 = N edge Pav.	7.32	11.40
chk. on S.W. BM S.D. Wallace	6.11	12.61
		12.67 = BM
		0.01 = Error.
B. on Con. Drive to o/l Stu.	6.28	12.44
C " " " " " "	6.24	12.48
C " " Pump Stands.	5.76	12.96
D " " " "	5.73	12.99
D " " Drive	6.08	12.64
E " " "	6.03	12.69

Cross Section Exist. Paving on San Diego Ave and Taylor St. 34

Walker McHugh

BM. 3 Nails in Pole S.D. & Wallace

110	13.72	12.62
0+33 = 33' West W.L. Wallace		
Scb+12.2 = S edge Pav.	2.39	11.33
℄ Rd. Way	2.76	11.02
+2.5' = N edge Pav.	2.84	10.88
+66		
S Pav.	3.00	10.72
℄ Rd. Way	3.40	10.32
+1' = N. Pav.	3.44	10.28
0+99		
Scb+10.2 = S edge Pav.	3.67	10.10
℄ Rd. Way.	3.97	9.75
+0.8 = N " "	4.00	9.72
1+32		
Scb+10.2 = S edge Pav.	4.33	9.39
℄ Rd. Way	4.54	9.18
+0.8 = N edge Pav.	4.56	9.16
1+44.5 = Beginning full Width Strip		
Scb = Sdge Pav.	4.60	9.12
℄ Rd. Way	4.60	9.12
+10' = on Pav.	4.77	8.95
1+65		
S. Pav.	4.96	8.76
℄ Rd. Way.	4.90	8.82
N. Pav.	5.10	8.62

	1372	S. Diego Ave.	
	1+98		
S Par		5.52	8.20
℄ Rd. way		5.41	8.31
N Par.		5.53	8.19
	E+31		
S "		6.09	7.63
℄ Rd. way		6.00	7.72
N Par.		6.13	7.59
	2+64		
S Par		6.71	7.01
℄ Rd. way		6.55	7.17
N Par.		6.64	7.08
	E+97		
S "		7.28	6.44
℄ Rd. way		7.17	6.55
N Par.		7.27	6.45
	3+30		
S Par		7.88	5.84
℄ Rd. way		7.73	5.99
N Par.		7.80	5.92
	3+63.		
S "		8.43	5.29
℄		8.30	5.42
N		8.43	5.29
	3+783		
S Par		8.64	5.08
℄ Rd. way.		8.58	5.14
N Par.		8.74	4.98

	1372	Taylor St.	
℄ 13	7.41	8.04	5.28
40' S.S.L. Calhoun st.			
E Par.		3.86	3.55
℄ "		3.69	3.77
W "		3.80	3.61
15' S.S.L. Calhoun = opp ch. P.C. on E			
W "		3.88	3.53
℄		3.66	3.75
E		3.83	3.58
31.0' N of S.ch. P.C. on E.			
E		3.70	3.71
℄		3.80	3.91
W		3.60	3.81
61' N of S.ch. P.C. on E.			
W		3.59	3.82
℄		3.44	3.97
E		3.63	3.78
93' N " S.ch. P.C. on E = opp ch P.C. on W. at N. Calhoun st = 0+00			
E		3.44	3.91
℄		3.34	4.07
W		3.47	3.94
0+25			
W		3.47	3.94
℄		3.33	4.08
E		3.46	3.95
0+50			

7.41

E		3.34	4.07
℄		3.23	4.18
W		3.37	4.04
	0+75		
W		3.35	4.06
℄		3.20	4.21
E		3.30	4.11
	1+00		
E		3.20	4.21
℄		3.05	4.36
W		3.23	4.18
TP	4.84 2.90	2.95	4.16
	1+25		
W		5.11	4.19
℄		4.93	4.37
E		5.08	4.23
	1+50		
E		5.02	
℄		4.83	
W		5.01	
	1+75		
W		4.94	
℄		4.83	
E		4.93	

9.30

	1+25		
W		5.01	4.29
℄		4.83	4.47
E		5.02	4.28
	1+50		
E		4.92	4.38
℄		4.82	4.48
W		4.94	4.36
	2+04 = opp ch. PC. S.E. Cor Juan St.		
W		4.77	4.53
℄		4.66	4.64
E		4.77	4.53
	℄ Juan St.		
E		4.70	4.60
℄		4.61	4.69
W		4.67	4.63
	0+00 = opp. ch. PC. N.E. Cor Juan St.		
W		4.51	4.79
℄		4.49	4.81
E		4.55	4.75
	+25		
E		4.51	4.79
℄		4.34	4.96
W		4.42	4.88
	0+50		
W		4.37	4.93

9.30

℄		4.31	4.99
E.		4.44	4.86
	0+75		
E.		4.35	4.95
℄		4.28	5.02
W		4.32	4.98
	1+00		
W		4.25	5.05
℄		4.21	5.09
E.		4.25	5.05
	1+25		
E.		4.21	5.09
℄		4.10	5.20
W		4.16	5.14
	1+50		
W		4.02	5.28
℄		4.00	5.30
E.		4.07	5.23
	1+75		
E.		4.01	5.29
℄		3.94	5.36
W		3.97	5.33
	2+00		
W		3.96	5.34
℄		3.86	5.44
E.		4.00	5.30

9.30

	2+25		
E.		3.90	5.40
℄		3.80	5.50
W		3.87	5.43
	2+50		
W		3.80	5.50
℄		3.72	5.58
E.		3.84	5.46
	2+77 = opp. cb. P.C. S.W. Cor Sunset Blvd.		
E.		3.74	5.56
℄		3.65	5.65
W		3.71	5.59
	℄ Sunset on West.		
W		3.64	5.66
℄		3.63	5.67
E.		3.68	5.62
T.P. 440	10.26	3.44	5.86
	opp. cb. PC N.W. Sunset.		
E.		4.50	5.76
℄		4.40	5.86
W		4.49	5.77
	opp. cb. PC on S.E. Sunset.		
W		4.38	5.88
℄		4.32	5.94
E.		4.48	5.78
	℄ Sunset on E.		

10.26

E	4.31	5.95
L	4.24	6.02
W	4.35	5.91
0+00 = opp. cb. PC NE Cr. Sunset		
W	4.24	6.02
L	4.14	6.12
E	4.20	6.06
0+25		
E	4.14	6.12
L	4.09	6.17
W	4.20	6.06
0+50		
W	4.12	6.14
L	4.01	6.25
E	4.12	6.14
0+75		
E	4.05	6.21
L	3.93	6.33
W	4.05	6.21
1+00		
W	3.98	6.28
L	3.86	6.40
E	3.98	6.28
1+25		
E	3.92	6.34
L	3.82	6.44

W.	3.95	6.31
1+50		
W.	3.84	6.42
E	3.75	6.51
E	3.83	6.43
1+80 = cb. PC. 10 SSL. Whitman		
E	3.73	6.53
L	3.64	6.62
W	3.76	6.50
L Whitman.		
W.	3.70	6.56
L	3.53	6.73
E	3.66	6.60
0+00 = 10' N NL. Whitman = cb PC		
E	3.52	6.74
L	3.43	6.83
W.	3.57	6.69
0+25		
W	3.49	6.77
L	3.37	6.89
E	3.49	6.77
0+50		
E.	3.45	6.81
L.	3.33	6.93
W.	3.39	6.87
0+75		

		1026		
T.P.	399	11.87	E.38	7.88
W.			4.96	6.91
L.			4.83	7.04
E.			4.96	6.91
		1+00		
E.			4.86	7.01
L.			4.75	7.12
W.			4.88	6.99
		1+25		
W.			4.83	7.04
L.			4.70	7.17
E			4.79	7.08
		1+50		
E.			4.78	7.09
L.			4.61	7.26
W.			4.66	7.21
		1+75		
W.			4.62	7.25
L.			4.53	7.34
E.			4.69	7.18
		2+00		
E.			4.58	7.29
L.			4.47	7.40
W.			4.57	7.30
		2+25		
W.			4.51	7.36

		1187		
L.			4.93	7.44
E.			4.59	7.28
		2+50		
E.			4.44	7.43
L.			4.31	7.56
W.			4.45	7.42
		2+80 = ob. P.C. 10' S.S.L. chestnut		
W.			4.25	7.62
L.			4.15	7.72
E.			4.25	7.62
		L. chestnut		
E			3.83	8.04
L.			3.67	8.20
W.			3.78	8.09
		10' N.N.L. chestnut = ob P.C. = 0+00		
W.			3.15	8.72
L.			3.05	8.82
E.			3.20	8.67
		0+33		
E.			2.56	9.31
L.			2.44	9.43
W.			2.56	9.31
		0+66		
W.			1.98	9.89
L.			1.86	10.01
E.			1.95	9.92

11.87

~~0+99 out~~

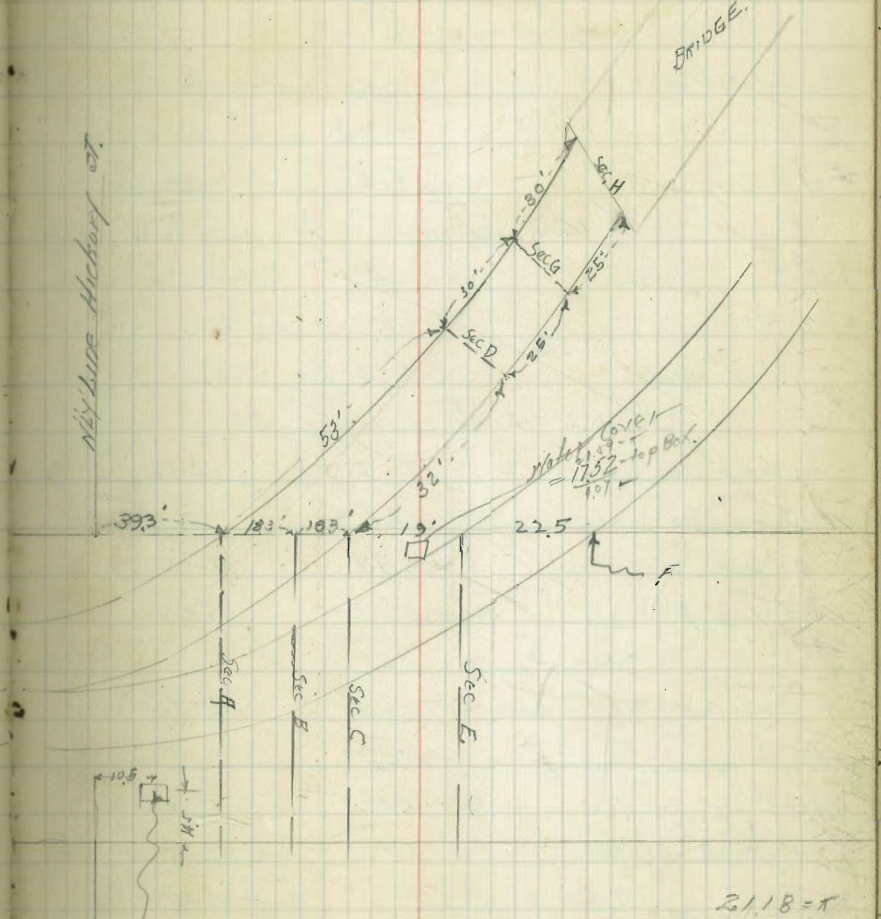
1+32

E.			0.75	11.12
℄			0.62	11.25
W.			0.84	11.03
		~~1+65~~		
T.P.	8.77	19.10	1.54	10.33
		1+65		
W			7.38	11.72
℄			7.24	11.86
E			7.40	11.70
		1+98		
E.			6.76	12.34
℄			6.62	12.48
W.			6.75	12.35
		2+31		
W			6.16	12.94
℄			6.06	13.04
E.			6.17	12.93
		2+50 = opp cb.		PC ~~S.St.~~ Hickory on W
~~E~~			5.74	13.36
~~℄~~			5.67	13.43
~~W~~			5.86	13.24
T.P.	4.00	21.21	1.89	17.21

top. on Fire Hdt. SE. Hickory & Poplar

(?) → 2+40 = 40' SSL. Hickory St. = cb PC

E			8.09	13.12



2121

℄ Rd. Way	8.00	13.21
W Pav.	8.17	13.04
E+90 = S.L. Hickory		
W Line + 37' = W Pav.	7.65	13.56
℄ Rd. Way	7.12	14.09
+10' = E Pav.	6.80	14.41
℄ Hickory St.		
W+31.3' = W edge Pav.	7.49	13.72
℄ Rd. Way.	6.55	14.66
+9.8' = E Pav.	6.14	15.07
W L.Y Line Hickory		
W+22' = W Pav.	7.05	14.16
+37' on Pav	6.66	14.55
℄ Rd. Way.	5.97	15.24
+8.3 = E edge Pav.	5.65	15.56
Sec. A		
W = on Pav.	6.03	15.18
"b " "	5.89	15.32
W b+15' on "	5.42	15.79
" " +29.1 = E edge Pav.	4.90	16.31
Sec. B.		
W. on Pav.	5.18	16.03
+16.2' = East edge of West strip Pav.	5.16	16.05
+21.8' = West " "East " "	5.29	15.92
+35' on Pav.	4.72	16.49
+43.4' "East edge of E Strip Pav.	4.44	16.77

2121

Sec. C		
East edge East strip Pav.		
W on Pav.	4.25	16.96
+45 = "	4.83	16.38
+339 = East edge East strip Pav.	4.12	17.09
Sec E.		
West edge Pav.	4.54	16.67
+298 = E edge Pav.	3.74	17.47
Rod on Point F	2.98	18.23
Sec. D 21.6'		
Lt. on Pav.	3.58	17.63
℄ " "	3.29	17.92
Rt. " "	3.08	18.13
Sec. G = 20.6'		
Rt. on Pav.	2.10	19.11
℄ " "	2.24	18.97
Lt. " "	2.28	18.93
Sec. H. = End Bridge = 22'		
Lt.	2.02	19.19
℄	1.91	19.30
Rt.	2.08	19.13
	1.15	20.06

20.07 = BM P-78
0.01 = Error

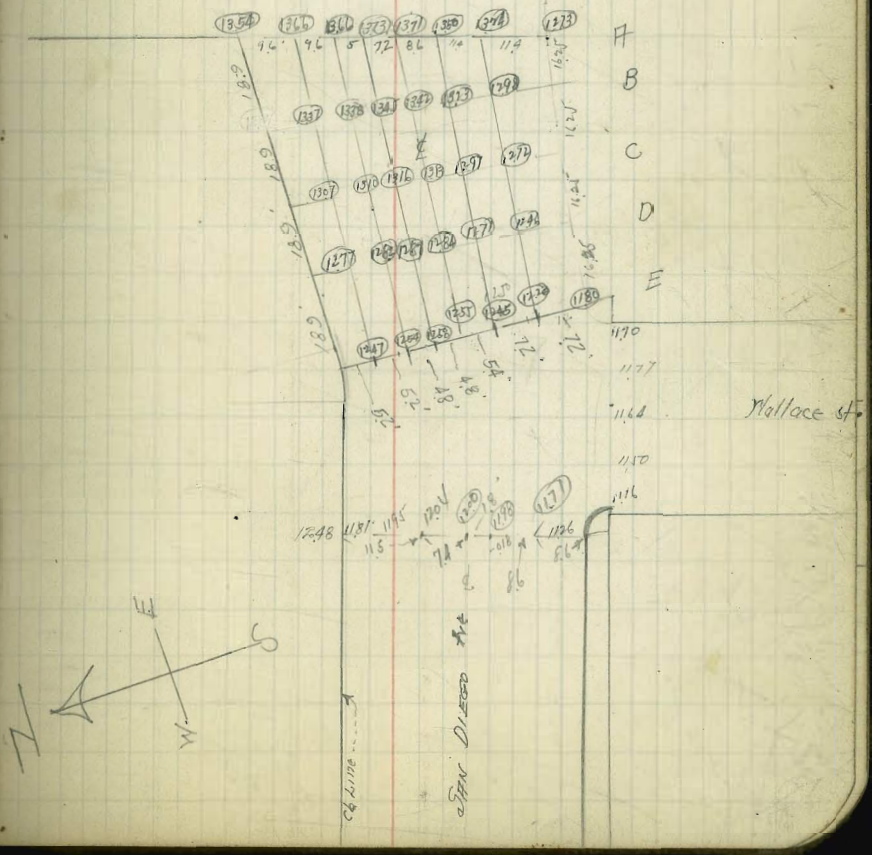
Walker
5-7-29

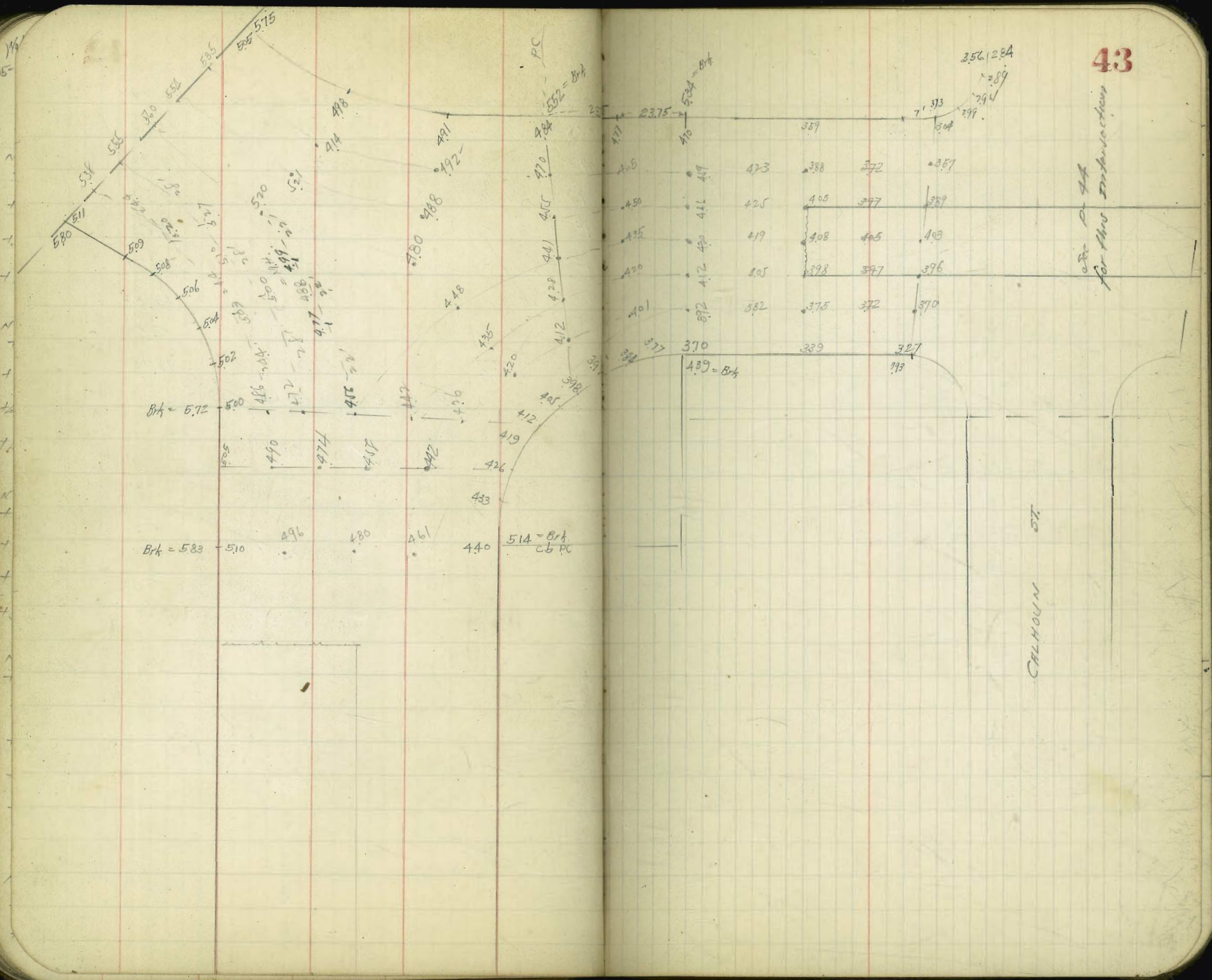
Additional X. Section. Exist. Pav.
Intersection. Wallace & San Diego Ave.

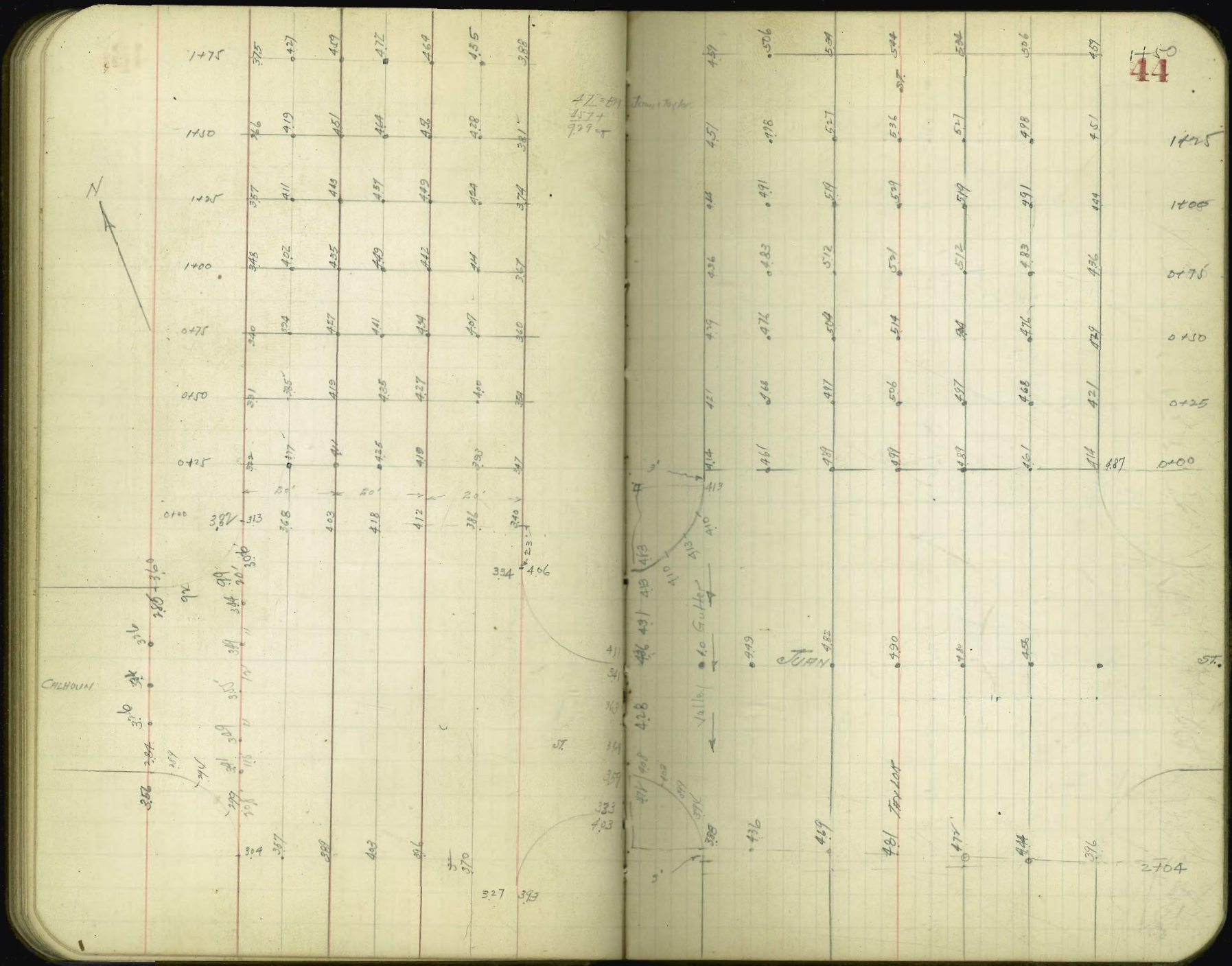
	π		
4.87	17.43		12.62 = B.M.
	Sec E		
N cb			
+5.2 = N edge Pav.		5.00	12.43
+10		5.02	12.41
+19.8 = ℄ Sec E.		5.02	12.41
+25.2 = S Pav.		5.09	12.34
	Sec D = 44'		
N cb.			
+6.5 = N Pav.		4.58	12.85
+11.5 on "		4.62	12.81
+22' = ℄ Sec D		4.79	12.64
+26.7 = S Pav.		4.96	12.47
	Sec C = 50'		
N cb.			
+10 = N edge Pav.		4.16	13.27
+15		4.23	13.20
+25 = ℄ Sec. C		4.54	12.89
+31 = S. Pav.		4.73	12.70
	Sec. B = 57'		
N cb.			
+13' = N Pav.		3.84	13.59
+18		3.93	13.50
+23		4.12	13.31
+28.5 = ℄ Sec. B.		4.32	13.11
+34.8 = S edge		4.57	12.86
	Sec A = 62.8		
N Gut on New Pav.		3.89	13.54
+19.2 = N edge old Pav.		3.57	13.86
+19.2 on New Pav.		3.77	13.66

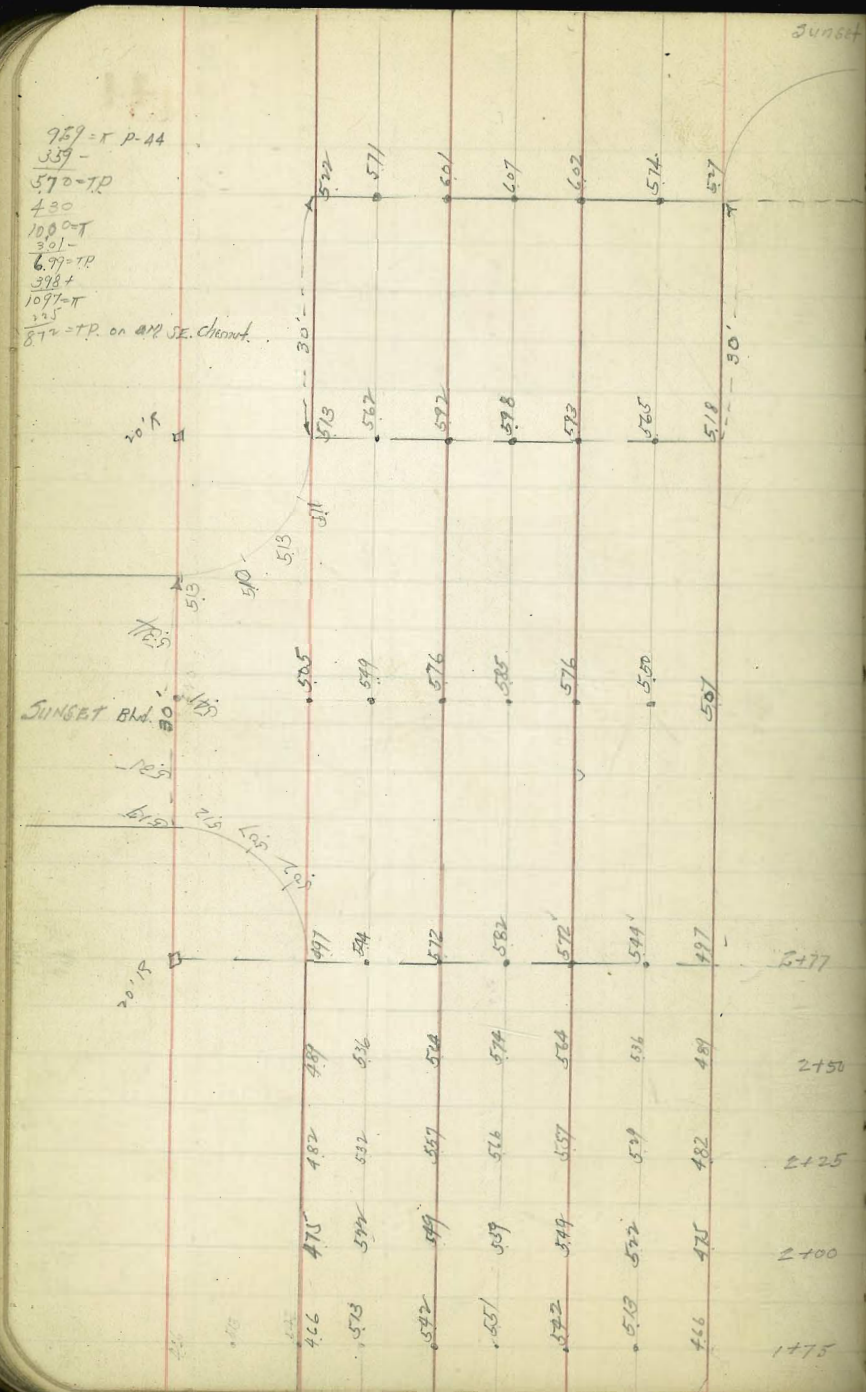
17.43

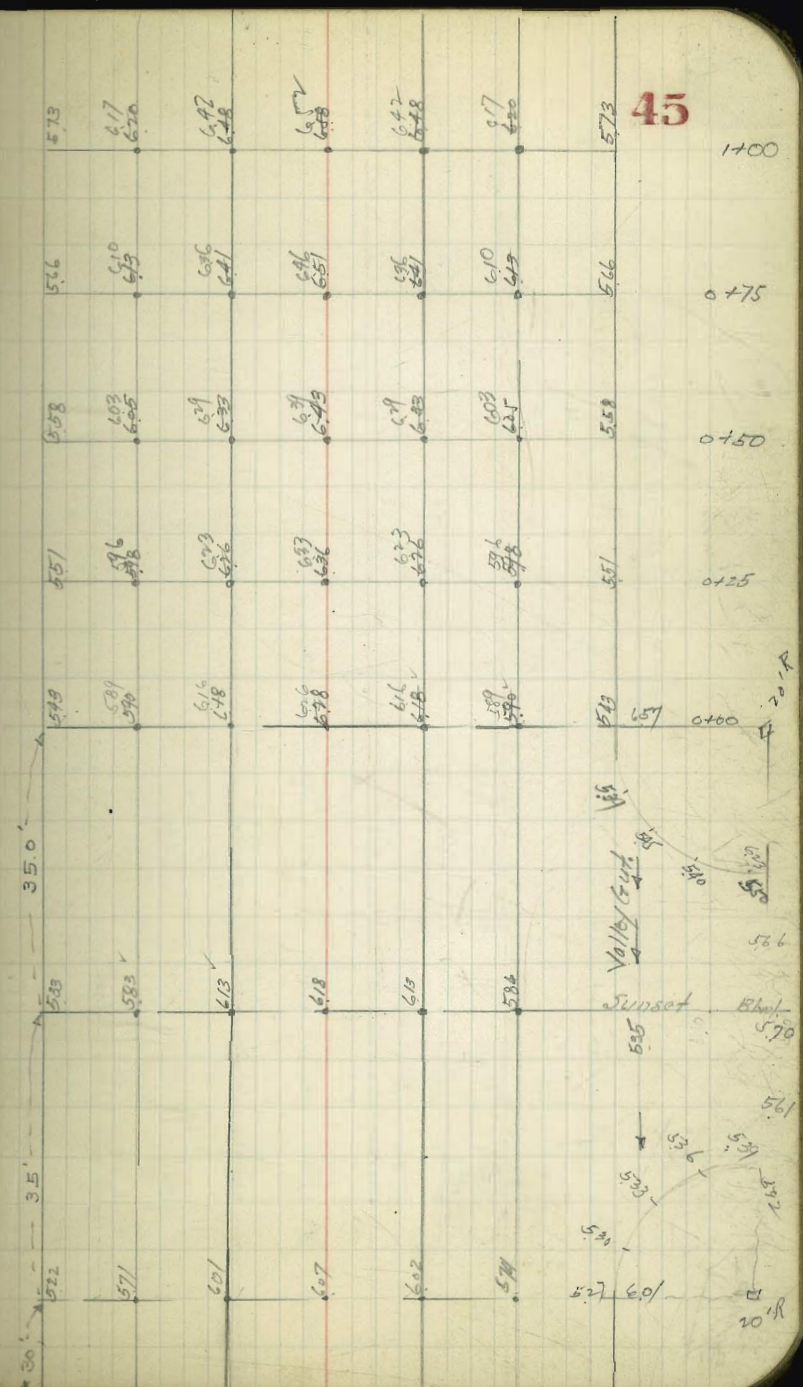
+24.2 on old Pav.	3.64	13.79
+24.2 " New "	3.77	13.66
+29.2 " " "	3.70	13.73
+29.2 on old "	3.84	13.59
+31.4 " " "	3.90	13.53
+31.4 " New "	3.72	13.71
+40 " old Pav.	4.40	13.03
+40 " New	3.93	13.50
+62.8 " Pav.	4.70	12.73

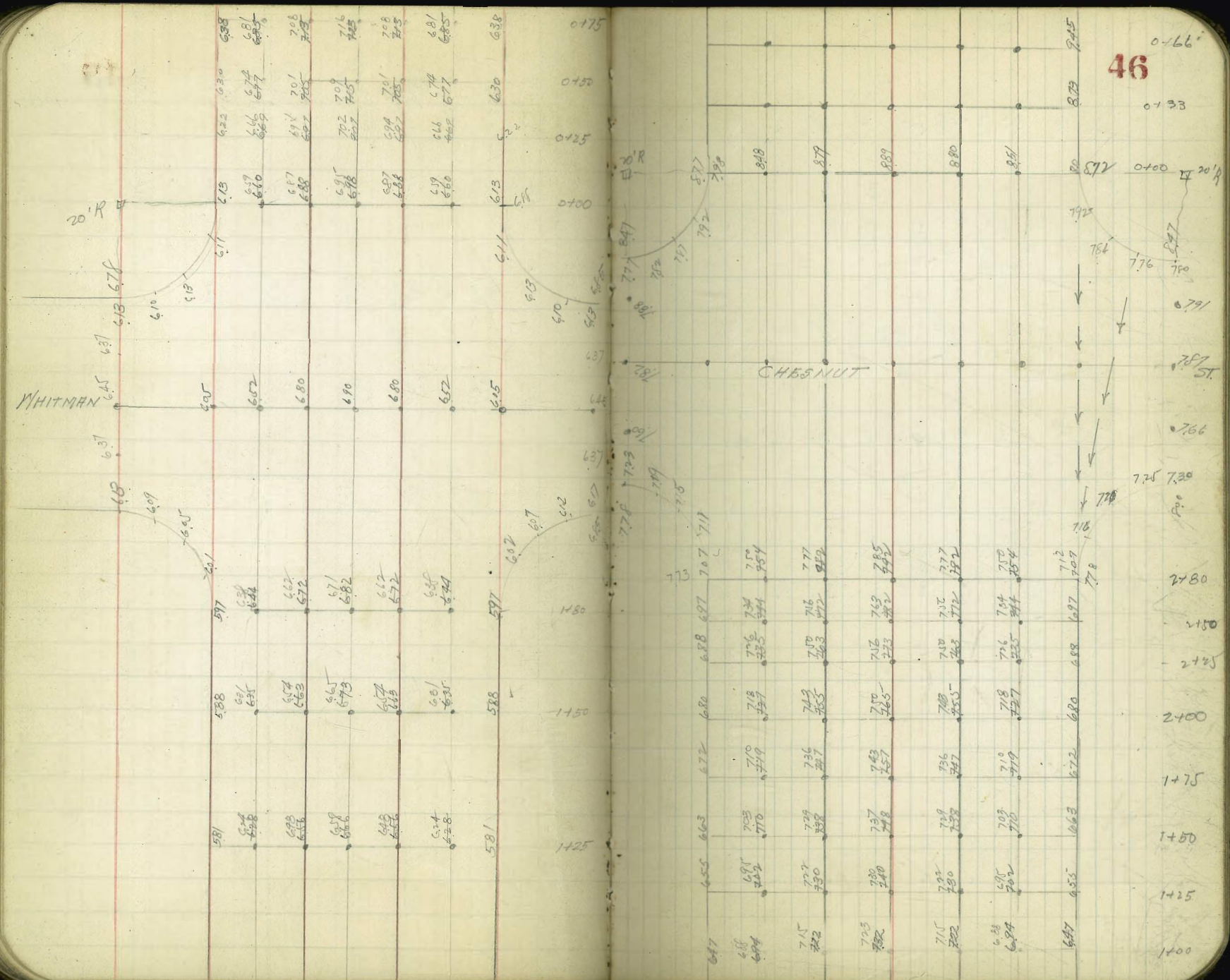


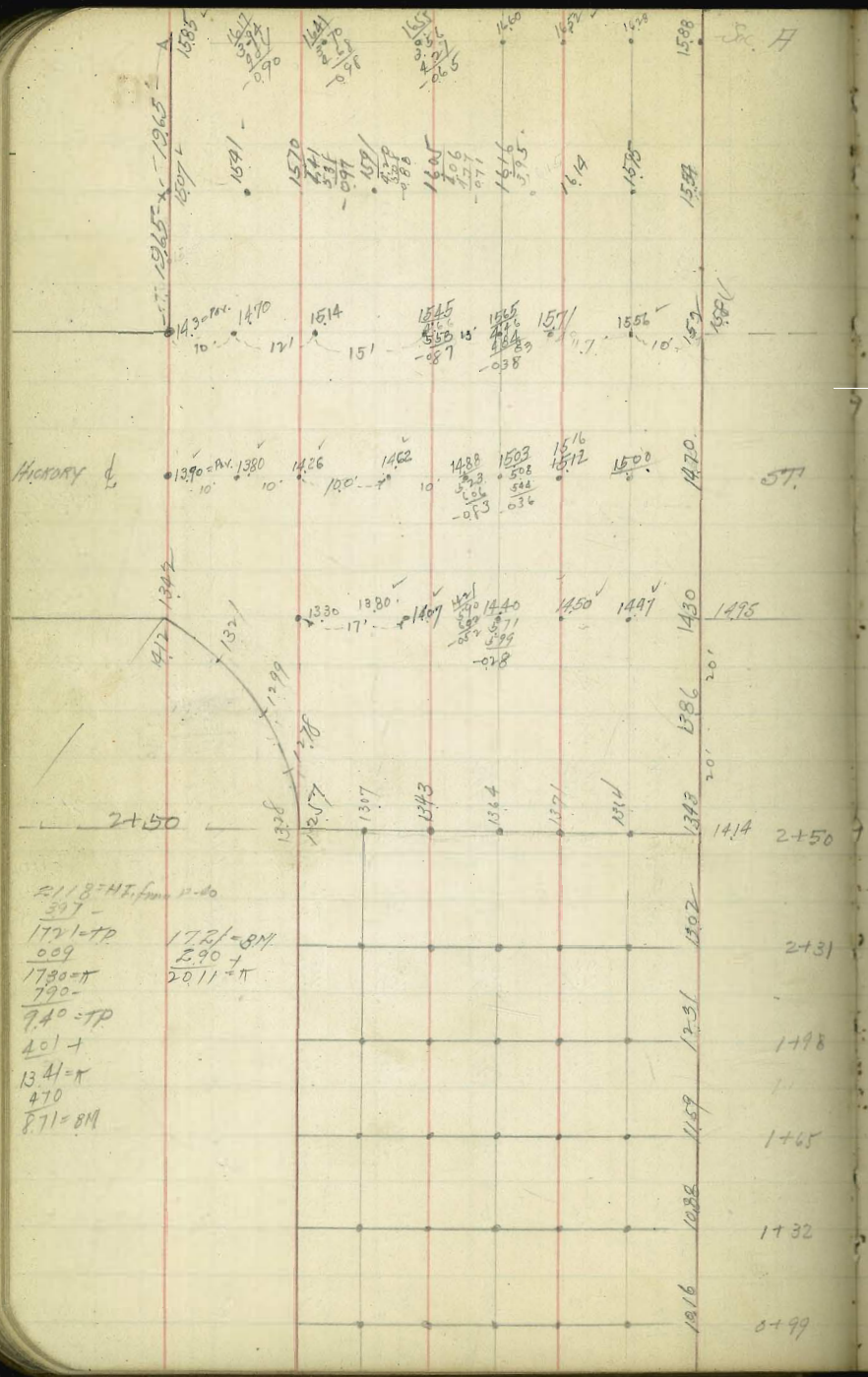

Brk = 5.72
Brk = 5.83
5.14 = Brk
cb PC
5.52 = Brk
5.34 = Brk
4.39 = Brk
CALHOUN ST.
See p. 44 for this intersection

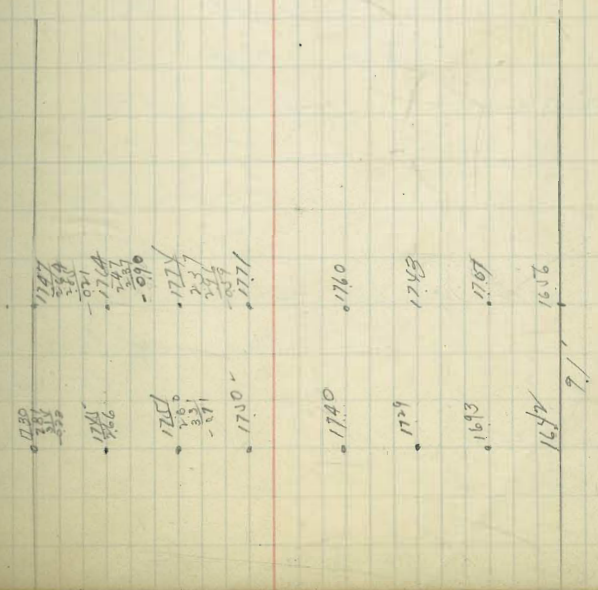

N
CALHOUN
JUAN
ST.
Valley
Gutter
1+75
1+50
1+25
1+00
0+75
0+50
0+25
0+00
2+04


Sunset
969 = π P-44
359 -
570 = T.P.
430
1000 = π
301 -
699 = T.P.
398 +
1097 = π
225
872 = T.P. on ⊕ M. S.E. Chemnut.
30'
30'
20' R
SUNSET Blvd.
30'
20' R
2+77
2+50
2+25
2+00
1+75


1+00
0+75
0+50
0+25
0+00
20' R
35.0'
Valley Gut.
Sunset Blvd.
35'
30'
20' R


WHITMAN
CHESNUT
ST.
20'R
0+75
0+50
0+25
0+00
1+80
1+50
1+25
0+66
0+33
0+00
2+80
2+50
2+25
2+00
1+75
1+50
1+25
1+00


Sec. A
HICKORY ℄
ST.
2+50
2+31
1+98
1+65
1+32
0+99
2118 = HI. from 12-40
397 -
1721 = TP
009
1730 = π
790 -
9.40 = TP
401 +
13.41 = π
470
8.71 = BM
1721 = BM
2.90 +
20.11 = π


Sec. C

Walker
145 Hwy.
Monhoon
Lockey
1929

LaSalle Blvd. STORM DRAIN Const.

Location See plan sheet 2257-L
Profiles " " 3679-L 3788-L

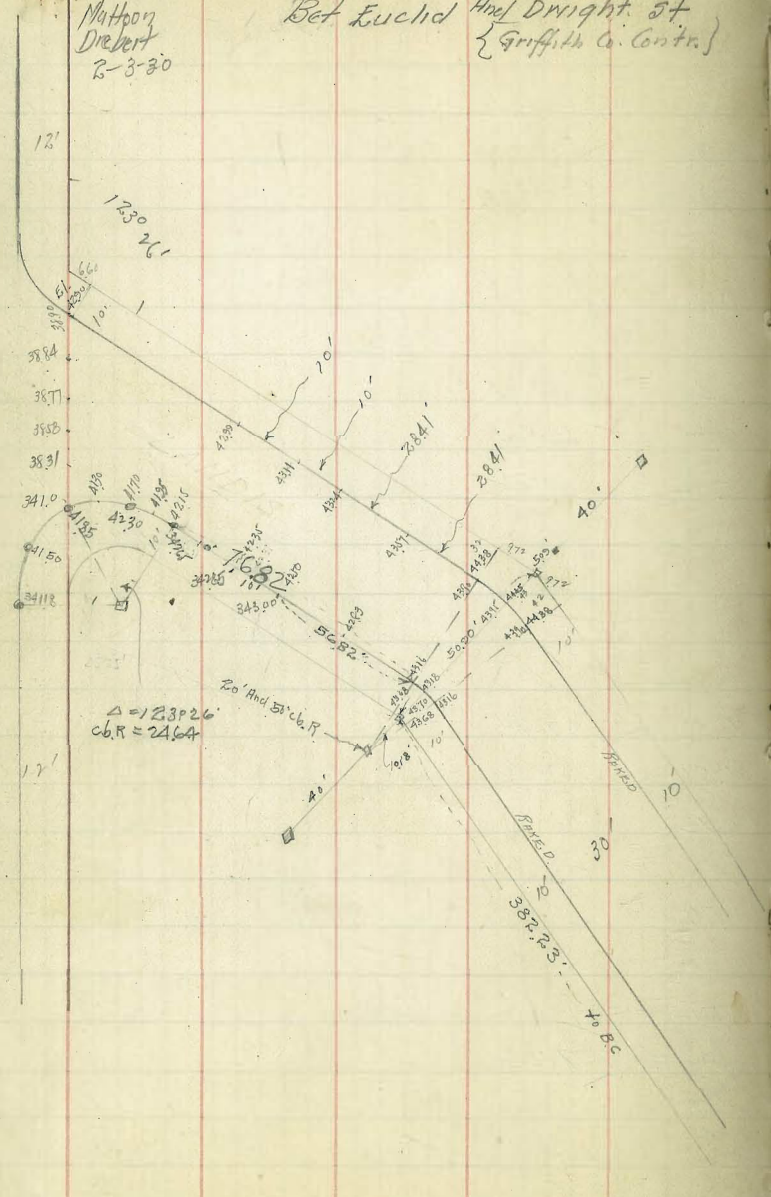
				Flow Line GRADES		Offsets	
		Culvert #11					
cb Inlet #12 = 0+00	77.52	2.59	74.93	69.00	+5.93	7' N.E.	
cb Inlet #13 =		1.76	75.76	68.00	+7.76	7' S.E.	
		Culvert #12					
cb Inlet #13 = 0+00		1.76		68.00			
+50		4.38	73.14	66.74	+6.40	7' Rt.	
1+00		7.34	70.18	65.47	+4.71	7' Rt.	
+50		8.22	69.30	64.21	+5.09	7' Rt.	
+94 = ℄ Storm Drain Cleanout #7		10.53	66.99	63.10	+3.89	cbk. on above B.M.	71.98
		STORM DRAIN #5					
℄ cleanout #7 = 0+00		10.53		63.10			
+50		11.25	66.27	60.18	+6.09	7' Rt.	
1+00	68.80	9.99	58.81	57.25	+1.56	" "	
+35 = ℄ Catch Basin #1		12.88	55.92	55.2	+0.72	" "	
1+67.5		9.97	58.83	5337	+5.46	" "	
2+00		5.50	63.30	51.54	+11.76	" "	
+33.5 = ℄ Lt. Line Lasalle Blvd.		6.66	62.14	49.66	+12.48	" "	
✓ 80.68 Δ 23°37' Lt.	58.58	~~10.46~~	~~48.12~~	~~47.00~~	+1.12	" "	
3+00		~~9.06~~	~~49.52~~	~~45.79~~	+3.15 +~~3.59~~	7' Lt.	
+50		~~10.89~~	~~47.69~~	~~43.72~~	+2.95 +~~4.57~~	" "	
+94.88 = Δ 35°55' Rt.		~~10.37~~	~~48.21~~	~~40.59~~	+4.94 +7.62	" "	
4+32.3 = Δ 30°51' Rt. ℄ 27°20'		7.87	50.71	~~38.79~~	+8.66 +~~11.92~~	" "	
+60.40 = Δ 15°04' Rt. 5°50'		~~12.53~~	46.05	~~36.91~~	+4.82 +7.74	" "	
4+94.7 = End.	End-Raised	~~14.54~~	44.04	~~35.06~~	+4.04 +7.04	" "	

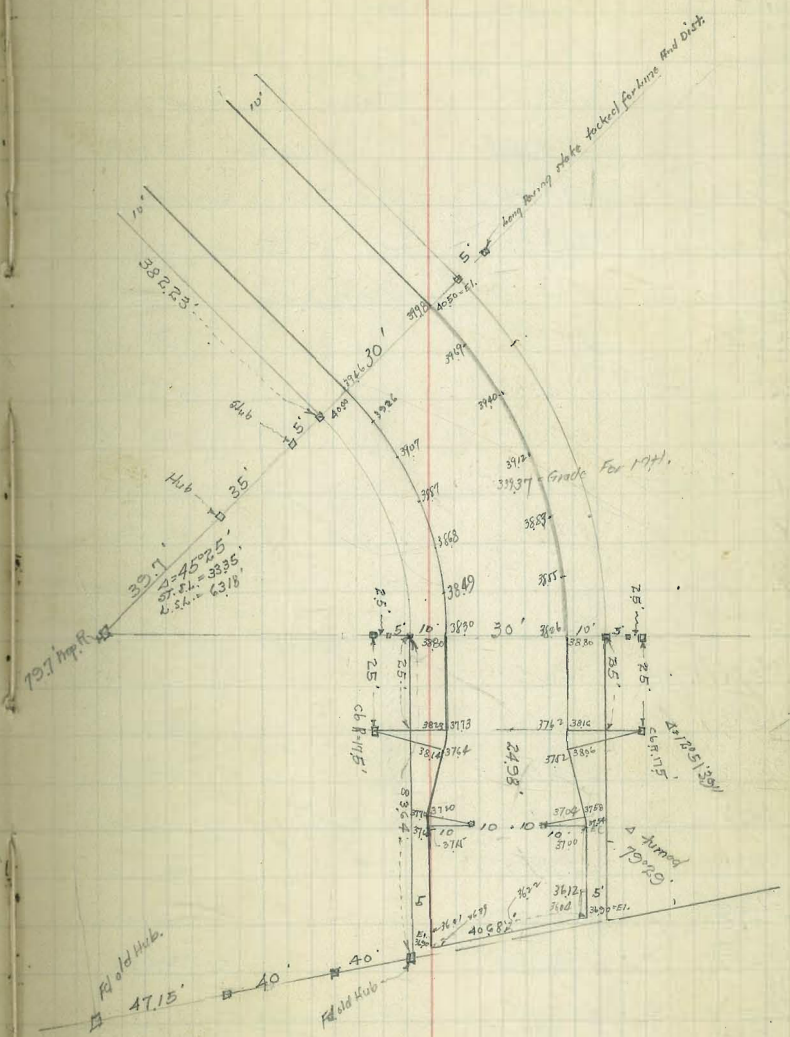
St. & R.R. Bm. Flr. Lasalle Blvd. = 7201
55 +
77.52 = π
11.77 −
6475 = T.P.
4.01 +
6880 = π
12.69 −
56.11 = T.P.
2.47 +
58.58 = π
1.48 −
5710 = T.P.
12.37 +
6947 = π
139 −
6808 = T.P.
669 +
74.77 = π
2.79 −
71.98
7201 = B.M.
0.83 = Error.

Walker
Wm Bliss
Mattson
Drebert
2-3-30

CASTLE ST. PAVING

Bet Euclid Ave. and Dwight St.
{Griffith Co. Contrs.}





Walker
2-3-30

CASTLE St. GRADING. And Paving
From Euclid St. East.

N.L. Station	N.L. Grades	S.L. Station	S.L. Grades
E.L. Euclid		P.C. on Castle	341.18
=0+00	342.92	①	341.50
		② = Center Return	341.85
+45.41	343.28	③	342.30
+90.82	343.64	④ = E.C. cb Return	342.65
1+36.24 = Brk.	344.00	10' East Above E.C. Brk.	342.85
+45.96 = Brk. = △	344.05	20' " " " " = Brk.	343.00 ok
		48' " " " "	343.34
+55.68 = Brk.	344.00	opp. 1+55.68 on N = △ on Sulk	343.50
(47.74')8			
2+03.42	343.56		343.06
+51.16	343.13		342.63
+98.9	342.69		342.19
3+46.64	342.25		341.75
+94.38	341.82		341.32
4+42.13	341.38		340.88
+89.87	340.94		340.44
5+37.64 = Brk = B.C. Rt.	340.50	B.C.	340.00 ok
+54.78 = ①	340.22		339.80
+71.92 = ②	339.94		339.60
+89.06 = ③	339.66		339.40
6+06.20 = ④	339.37		339.20
+23.34 = ⑤	339.09		339.00
+40.48 = E.C.	338.80	E.C.	338.80
(37.25')2			
6+77.73	337.85	(41.82)2	337.85
	337.54 = E.C.		337.65 = E.C. cb Return 10' Radius
7+14.98 = End of Work	336.90	End Work	336.90

opposite N.L. Stations

340.46 = N.L. B.P. Lantana Dr. + Euclid Ave.
8.07 +
348.53 = π
5.12 -
343.41 = T.P. on 13.59' Prop. Radius S.E. Cor. Castle + Euclid.
5.50 +
348.91

50

N.L. 342.92 | 343.28 | 343.64 | 344.00 | 344.05 | 344.00 | 343.56 | 343.13 | 342.69
599 | 563 | 527 | 486 | 535 | 578 | 622
6.01 | 4.15 | 4.26 | 3.94 | 4.06 | 4.20 | 4.52
+1.5 | +1.4 | +1.0 | +0.9 | +1.3 | +1.5 | +1.7 +1.4
+0.2 | +1.4 | +0.7 | +0.5 | +0.9 | +1.3

S.L. 342.50 | 343.0 | 343.25 | 343.5 | 343.06 | 342.63 | 342.19
6.41 | 5.91 | 5.66 | 5.41 | 5.85 | 6.28 | 6.72
5.12 | 4.62 | 4.46 | 4.94 | 5.31 | 5.51 | 5.85
+1.9 | +1.3 | +1.1 | +0.3 | +0.5 | +0.7 | +0.8
+1.3 | +1.3 | +1.1 | +0.3 | +0.3 | +0.5 | +0.8

343.41 B.N.
5.36
348.77

N.L. 342.25 | 341.82 | 341.38 | 340.94 | 340.50 | 340.22 | 339.94 | 339.66 | 339.37
6.66 | 7.09 | 7.53 | 7.97 | 8.41 | 8.69 | 8.97 | 9.25 | 9.54
4.92 | 5.55 | 6.40 | 7.17 | 7.85 | 8.23 | 8.40 | 8.70 | 9.47
+1.74 | +1.54 | +1.1 | +0.8 | +0.6 | +0.46 | +0.57 | +0.55 | +0.1
+1.5 | +1.4 | +1.0

S.L. 341.75 | 341.32 | 340.88 | 340.44 | 340.0 | 339.80 | 339.60 | 339.40 | 339.20
7.16 | 7.6 | 8.03 | 8.47 | 8.91 | 9.11 | 9.31 | 9.51 | 9.71
6.05 | 6.53 | 7.14 | 8.23 | 8.32 | 8.53 | 9.23 | 9.57 | 8.04
+1.1 | +1.1 | +0.9 | +0.2 | +0.6 | +0.6 | +0.1 | 0.0 | -0.1
+1.0 | +1.0

Storm Drain = 0+00 on Sulk
336.62
5.11 +
341.73 = π

N.L. 339.09 | 338.80 | 337.85 | 336.90 | Finish Stakes N.L. 337.54 | 336.90
9.82 | 10.11 | 11.06 | 12.01 | 4.19 | 4.83
9.75 | 10.46 | 11.20 | 12.17
+0.1 | -0.3 | -0.1 | -0.2

S.L. 339.00 | 338.80 | 337.85 | 336.90 | 337.65 | 336.90 | 336.90 | 336.90
9.91 | 10.11 | 11.06 | 12.00 | 4.08 | 4.83 | 4.83 | 4.83
10.11 | 10.45 | 11.31 | 13.3 | | | 3.48
-0.2 | -0.3 | -0.3 | -1.3 | | | +1.35

342.90 = top cb on N
6.03 +
348.93 = π
6.75 -
342.18 = T.P.
3.24 +
345.42 = π

Finish Stakes Set 4-7-30

348.77
6.07
342.70

S.L. 341.18 | 341.58 | 341.85 | 342.30 | 342.65 | 342.85 | 343.34
7.75 | 7.40 | 7.08 | 6.63 | 6.28 | 6.08 | 5.65
7.63 | 7.56
.006 High | .016

= P.C. ← curb Return → = E.C.

N 342.92 | 343.41 | 343.90 | 344.38 | 344.45 | 344.38
6.01 | 5.52 | 5.03 | 4.55 | 4.48 | 4.55 ← Raked
6.03
.002 Low

= P.C. | ℄ curve | = E.C.

Grade Change
Feb. 18-30
Sisson

S.L. 343.68 | 343.70 | 343.68 | 343.24 | 342.77 | 342.31 | 341.85 | 341.39 | 340.92 | 340.46
5.25 | 5.23 | 5.25 | 5.69 | 6.16 | 6.62 | 7.08 | 7.54

← RAKED to BC →

N.L. 343.91 | 343.42 | 342.98 | 342.45 | 341.96 | 341.48 | 340.99
5.02 | 5.51 | 5.95 | 6.48 | 6.97

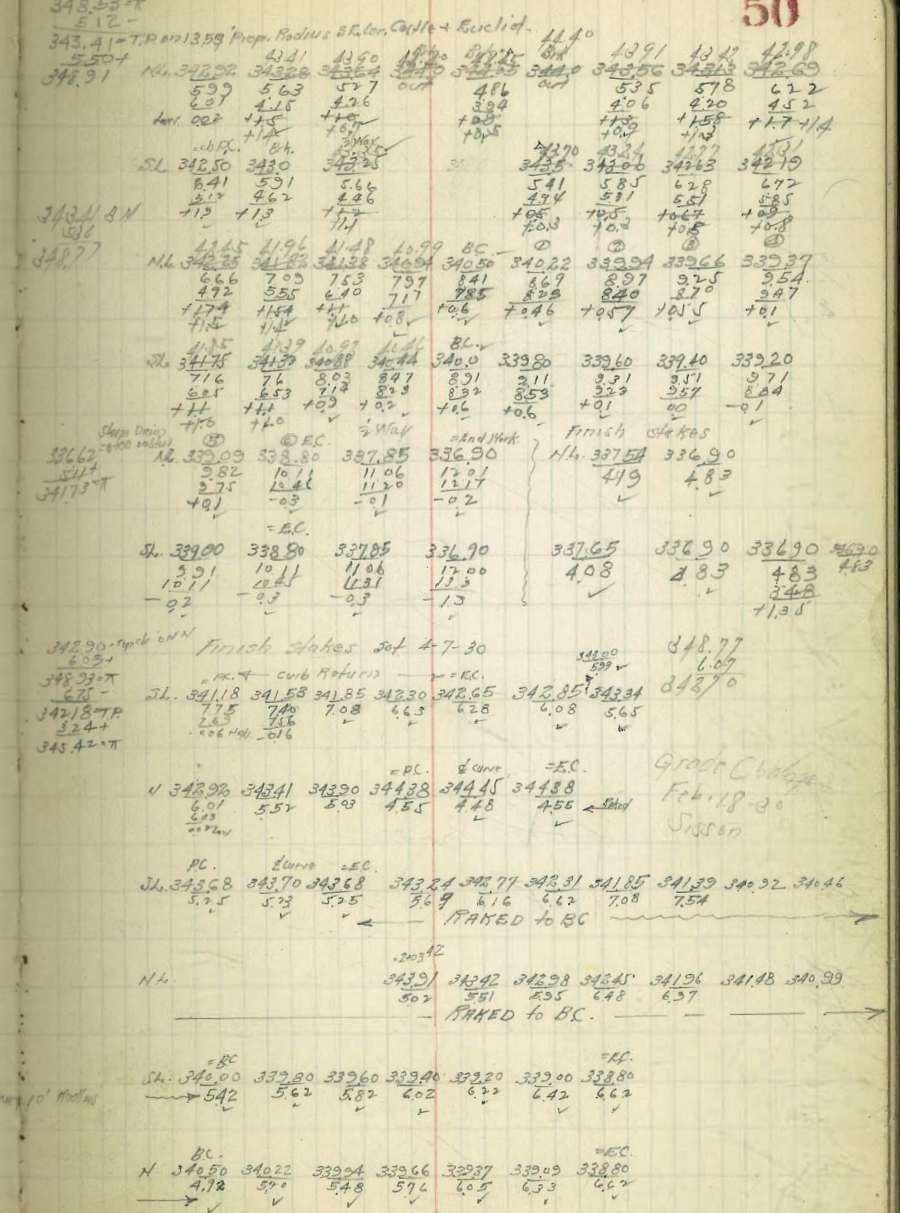
← RAKED to B.C. →

S.L. 340.00 | 339.80 | 339.60 | 339.40 | 339.20 | 339.00 | 338.80
5.42 | 5.62 | 5.82 | 6.02 | 6.22 | 6.42 | 6.62

= B.C. | = E.C.

N 340.50 | 340.22 | 339.94 | 339.66 | 339.37 | 339.09 | 338.80
4.92 | 5.20 | 5.48 | 5.76 | 6.05 | 6.33 | 6.62

= B.C. | = E.C.



CASTLE ST. SEWER LATERALS

LATERAL #	⊼ 350.42			Flow Line Elev. GRADE	Cuts	offsets
① on North		5.37	345.05	337.00	+8.05	2' N
② " South		7.46	342.96	335.00	+7.96 ✓	2' S
③ " North		5.69	344.73	338.90	+5.83 ✓	
④ " South		6.48	343.94	338.40	+5.54 ✓	
⑤ " North		5.47	344.95	338.70	+6.25 ✓	
⑥ " "		5.81	344.61	338.00	+6.61 ✓	
⑦ " South		7.45	342.97	337.00	+5.97 ✓	
⑧ " North		7.73	342.69	336.70	+5.99 ✓	
⑨ " South		9.02	341.40	336.00	+5.40 ✓	
⑩ " North		9.05	341.37	336.30	+5.07 ✓	
⑪ " South		10.75	339.67	336.50	+3.17 ✓	
⑫ " North		9.92	340.50	336.40	+4.10 ✓	
⑬ " "		11.83	338.59	336.80	+1.79 ✓	
⑭ " South	341.97	1.00	337.97	337.00	+0.97 ✓	2' S
⑮ " " Line		4.80	337.17	332.30	+4.87 ✓	2' S

LEVELS For 6" Con Sewer.

Inter-Section. 4" Cast Iron Lateral					Cuts	offsets
=0+00 = Beginning 6" Pipe	341.97	5.25	336.72	331.10	+5.62 ✓	5' E
+36.73		6.23	335.74	329.66	+6.08 ✓	5' W
+73.46		6.66	335.31	328.23	+7.08 ✓	5' W.
1+10.19 = End Pipe = N.h. Dwight		7.79	334.18	326.80	+7.38 ✓	5' W.

LEVELS For 12" Storm Drain

cb. Face				Flow Line		offsets
=0+00	341.97	5.35	336.62	333.00	+3.62 ✓	5' E
+50.33		6.85	335.12	332.50	+2.62 ✓	6.75' E
1+00.67 = End Pipe N.h. DWIGHT	339.57	5.55	334.02	332.00	+2.02 ✓	6.75' E

Elev. 1.857 Prop. R. on P-50 — 341.41 + 7.01 = 350.42 - ⊼ − 12.07 = 338.35 - TP + 3.62 = 341.97 - ⊼ − 7.79 = 334.18 + 5.39 = 339.57 - ⊼ − 1.96

chk. on cut & stub. 1st stub North end Castle on Sh. — 337.61 + 337.55 = Stub, 0.06

Walker
Wm Bliss
Drebert
Mattoon 3-17-30

WATER MAIN 10'S ℄
on CASTLE St.
Bet. Euclid AND DWIGHT.

Griffith Co
Contr.

Elev. top cb. on N. Page 50 — 342.90
3.94+
346.84 = ⊼

				Grade Bottom Pipe	Offsets	
℄ Tee in Euclid =0+00	346.84	4.67	342.17	339.5	+2.67	℄
+23.96 = ℄ Gate Valve		4.83	342.01	339.3	+2.71 ✓	℄
+60.73 = opp. cb P.C. on South		3.85	342.99	339.70	+3.29 ✓	10' Right
1+00.6		3.18	343.66	340.20	+3.46 ✓	" "
+40.45 = Δ 22° Rt. Brk.		2.95	343.89	340.70	+3.19 ✓	" "
(48.11) 8 1+88.56		3.55	343.29	340.23	+3.06 ✓	" "
2+36.7		4.05	342.79	339.75	+3.04 ✓	" "
+84.8		4.41	342.43	339.28	+3.15 ✓	" "
3+32.9		4.77	342.07	338.80	+3.27 ✓	" "
+81.0		5.20	341.64	338.32	+3.32 ✓	" "
4+29.11		5.60	341.24	337.85	+3.39 ✓	" "
+77.2		6.37	340.47	337.35	+3.12 ✓	" "
5+25.32 = Brk. opp B.C.		6.93	339.91	336.90	+3.01 ✓	" "
+42.38 = Δ 22°43'		7.36	339.48	336.60	+2.88 ✓	" "
83.86 +~~80.46~~ = Δ 22°43'		7.86	338.98	335.~~90~~ 85	+3.13 ✓	" "
6+01.06 5+99.56 = opp E.C. Brk.		8.45	338.39	335.60	+2.79 ✓	" "
40.45² ~~6+40.01~~ 6+41.51		9.54	337.30	334.60	+2.70 ✓	" "
6+81.96 +80.46 = End Pipe		9.97	336.87	333.60	+3.27 ✓	" "

Walker
Wm. Bliss
Drebert
Mattoon
Sommeyer
4-29-30

Collier St. Water Main

Bet 33rd And Hawley Blvd.
Location = 20' North of South Line Collier.

G.R. Daley Corp.
Contractors

B.M. Book 1380-41
= N.E.B.P. Collier And Felton

389.96
5.00 +
394.96 - π

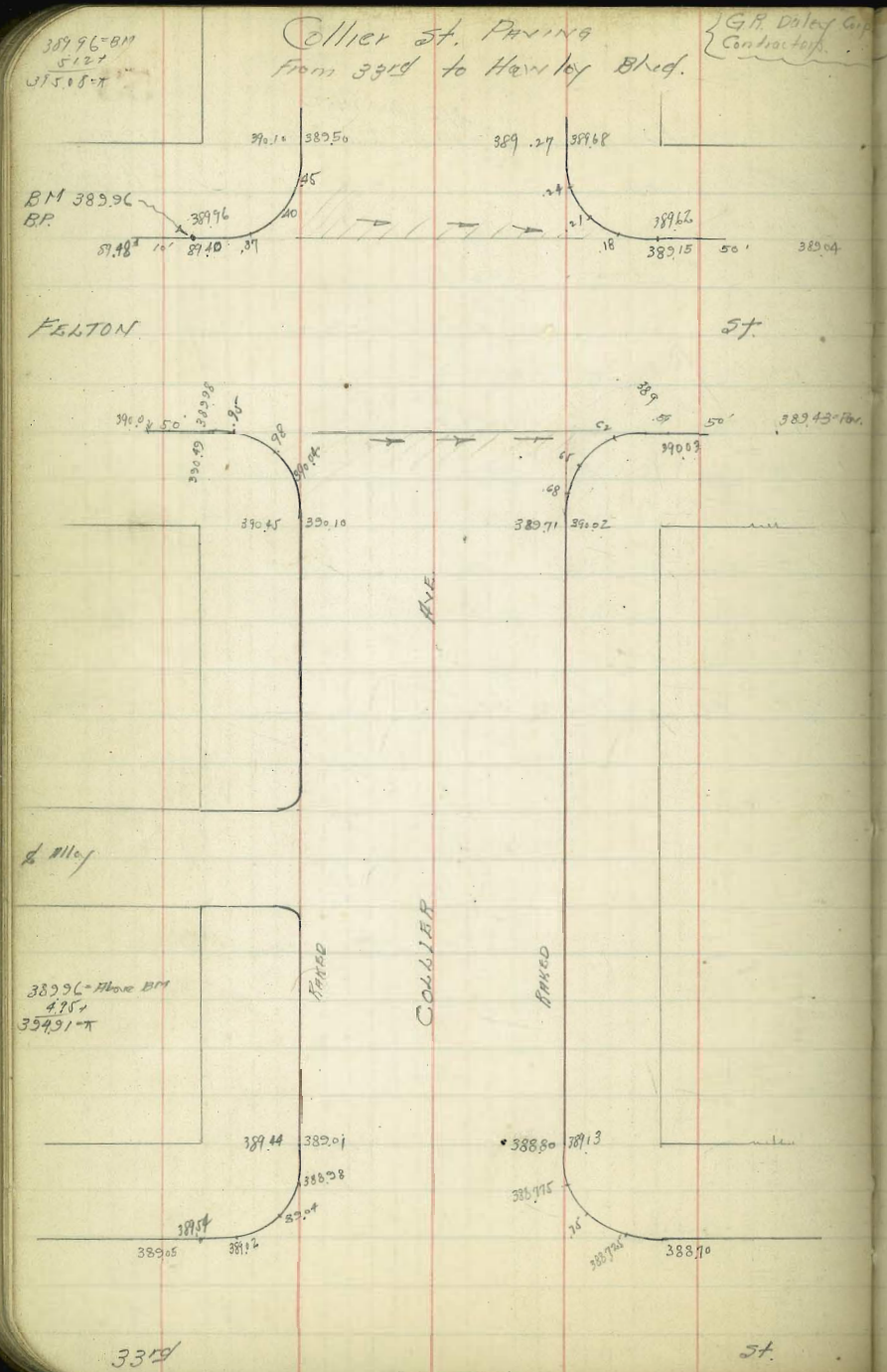
	π	–	Elev. Stake	Elev. Flow	Cuts	Offsets
E.L. 33rd St.						
=0+00	394.96	5.75	389.21	336.30	+2.91	9' South
+50		5.77	389.19	336.48	+2.71	" "
1+00		5.72	389.24	336.64	+2.60	" "
+45.5 = ℄ Tee 2.5' West E Line Alley on North		5.56	389.40	336.78	+2.62	" "
2+00		5.23	389.73	336.96	+2.77	" "
+50		5.15	389.81	337.11	+2.70	" "
+81.09 = W Line Felton St.		4.97	389.99	387.20	+2.79	" "
3+21.09 = ℄ Tee to South. East Line Felton St.		5.35	389.61	386.87	+2.74	" "
=0+00		5.16	389.80	386.70	+3.10	" "
+50		5.00	389.96	386.93	+3.03	" "
1+00		4.68	390.28	387.16	+3.12	" "
+45.5 = ℄ Tee 2.5' West E Line Alley		4.65	390.31	387.37	+2.94	

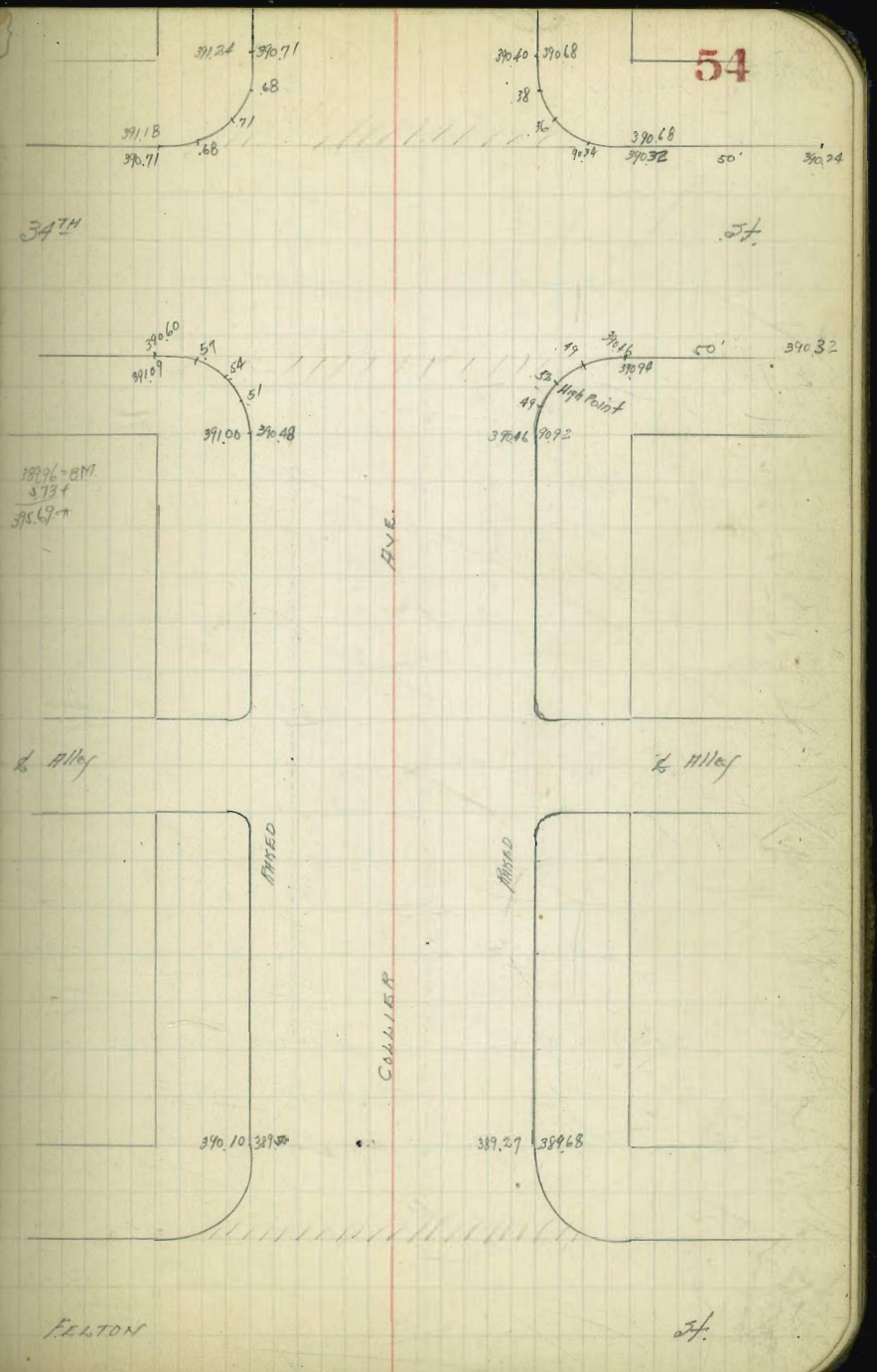
20' South Above Tee

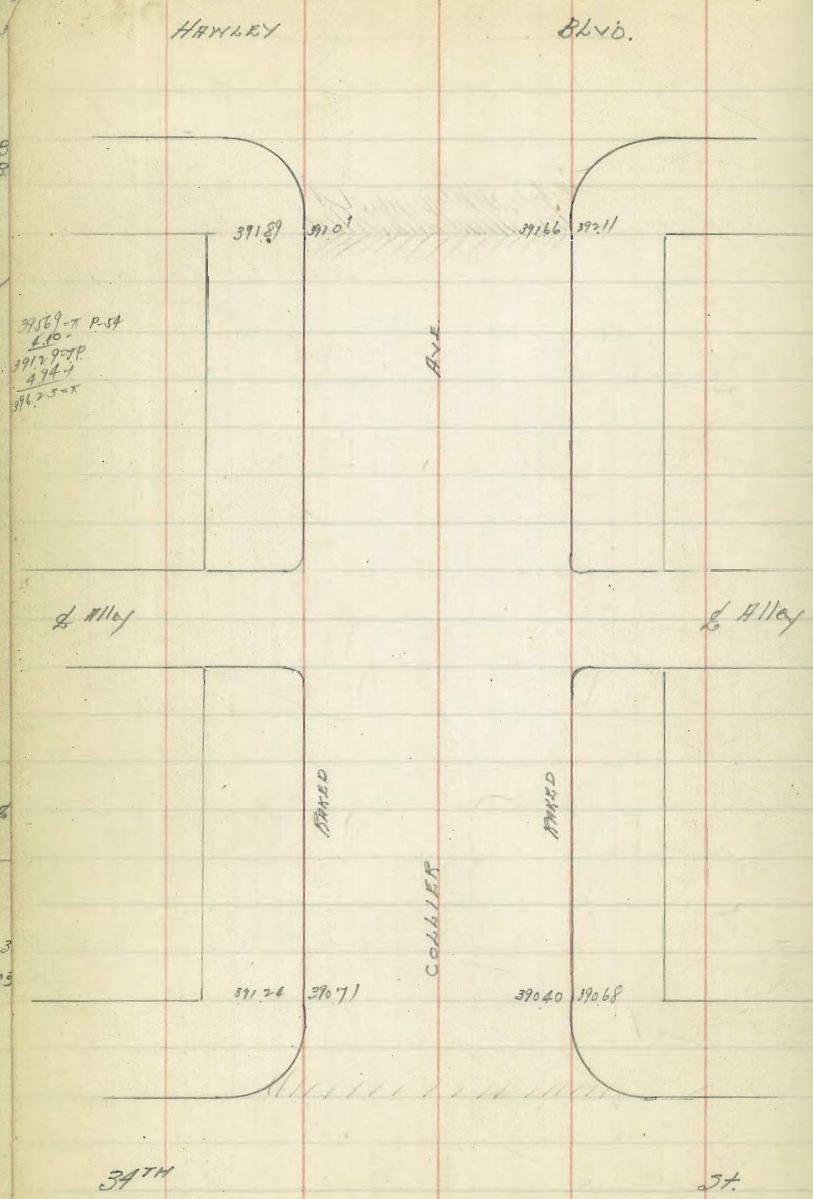
40' North " "

Collier St. Paving
From 33rd to Hawley Blvd.

{G.R. Daley Co. Contractors

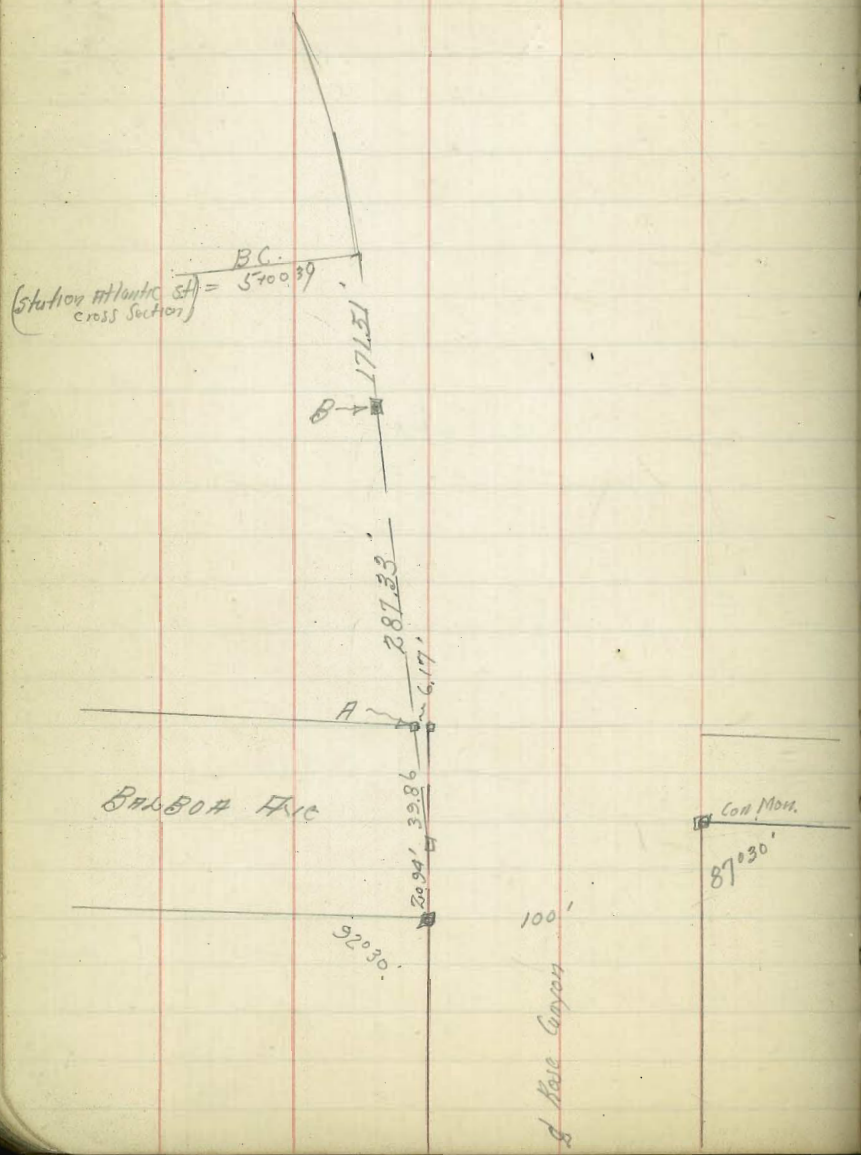





HAWLEY
BLVD.
391.89
391.0
391.66
392.11
39569=π P-54
4.10
391.29=TP
4.94
396.25=π
AVE
℄ Alley
℄ Alley
BAKED
BAKED
COLLIER
391.24
390.71
390.40
390.68
34TH
St.

Walker
Bliss
Drabeit
Mattoon
6-24-30

GRADES For opening LINE
BALBOA Ave And Atlantic St Ext.
Note: these Grades Are only Approx. as there is No Est. Grade on Atlantic St



U.S.G.S B.M. Balboa + Rose Canyon.
19.31 = city Datum
5.96 +
25.27 = ⊼

GRADES Bet. A & B Grades Are top cb.

	0+50	1+00	+50	2+00	2+50
19.76	19.26	18.76	18.26	17.76	17.26
5.51	6.01	6.51	7.01	7.51	8.01
5.19	4.46	4.80	5.05	5.36	6.37
+0.32	+1.55	+1.71	+1.96	+2.15	+1.64

Walker
Bliss
Drebert.

C-st GRADING And PAVING
Bet. India And Kettner Blvd.

Station	N.L. Grade	S.L. Station	S.L. Grade
0-21.46 = Brk.	11.83	0-23.8	11.70
0-18.44 = Brk. = West Rail	~~11.85~~ 11.71	0-18.44 = W. Rail	11.69
0-13.72 = Brk. East Rail	~~11.85~~ 11.71	0-13.72 = E. Rail	11.70
East Line Kettner =0+00	12.33	0+00	12.23
+6.36 = W. Rail	12.55	+6.33 = W. Rail	12.45
+11.08 = E "	12.55	+11.05 = E "	12.45
+19.06 = W "	~~12.70~~	+19.20 = W " Leave out	~~12.60~~
+23.78 = E "	~~12.70~~	+23.92 = E " " "	12.60
+36.31 = Brk.	12.90	+45.25 = Brk.	13.10
+41.54 = "	12.90	+59.07 = "	13.10
+80.0	13.87	80.0 = "	13.87
+95 = End Flat Section	13.87	+95 = End Flat Section	13.87
1+00 = cb Grades →	14.34 (89)	1+00 = cb Grade	14.32 (85)
+37.5	15.23	+37.5	15.17
+75 = Brk.	16.12	+75	16.03
2+00	16.25	2+00 = W.L. India	16.10
End of Imp 3' N.N.L. India	15.98	E.C. Return on India	1600

16.90 = NE 3P C- And India
0.41 -1
17.31 = ⊼

N.L. 11.83 11.71 11.71 12.33 (=0+00) 12.55 12.55 12.70 ~~12.70~~
4.98 4.76
5.14 4.80 to Fit Rail
-0.16

S.L. 11.70 11.69 11.70 12.23 (=0+00) 12.45 12.45 ~~12.60~~ ~~12.60~~
5.08 4.86 0.17
5.29 4.89
-0.15 -0.03 to Fit Track
-0.12 to Fit Track

N.L. 12.90 12.90 13.87 13.87 14.34 15.23 16.12 16.25 15.98
4.41 4.41 3.44 3.44 2.97 2.08 1.19 1.06
4.89 4.77 3.37 3.88 1.97 0.08 0.19 0.06
-0.48 -0.36 +0.07 +0.56 +1.00 +2.00 +1.00 +1.00

S.L. 13.10 13.10 13.87 13.87 14.32 15.17 16.03 16.10 EC 16.00
4.21 4.21 3.44 3.44 2.99 2.14 1.28 1.21 1.31
4.22 3.31 3.27 3.18 2.79 2.06 1.29 1.33
-0.01 +0.13 +0.17 -0.19 -0.65 -0.78 -0.08 -0.02

Grades for Light Poles. 8-25-30 Mills.

	S.	N.
BM. 16.90	chk W. End curbs 14.34	14.34
2.81	5.37	5.37
19.71	5.41	5.34

	S	N
0+01.5 W. Light Pole	12.17 / 7.54	
0+00 = E. Line Kettner	12.23	12.33
0+31 E		12.83 / 6.88 Light Pole
0+36.31 B.		12.90
0+80 Light Pole	13.87 / 5.84	

Walker
Bliss
Drebert
10-11-30

"T." – ALLEY BLOCK 110 UNIV. HTS.

GRADING AND PAVING
(EAST AND WEST ALLEY)

CARROL Contr.

Stations	S.L. Grade	N.L. Grade
0+00 – 14' = W.cb 30th W.L. 30th		
=0+00		364.80
+34.91		364.97
+69.82		365.15
1+04.73		365.32
+39.63 = E.L. N & South Alley = Brk.		365.50
+59.63 = W " " " Brk. (43.21') =		365.60
2+02.85		366.20
+46.06		366.80
+89.27 = Brk.		367.40
2+99.27 = E.L. KANSAS St.		367.40

North And South Alley Blk. 110 Univ. Hts.

S.L. Meade Ave.	E.L. Grade	W.L. Grade
=0+00	366.25	366.30
+40	366.43	366.47
+80	366.62	366.63
1+20 = Brk.	366.80	366.80
+70	366.60	366.62
2+20	366.40	366.44
+70	366.20	366.26
3+20	366.00	366.08
+70	365.80	365.90
4+20	365.61	365.71
+50 = N.L. Line East + W. Alley	365.50	365.60

366.78 = S.E. B.P. MEADE & Kansas Sts.
416+
370.94 = π
520 –
365.79 = T.P.
436+
370.10 = π
421 –
365.89 = T.P.
6.18+
372.07 = π

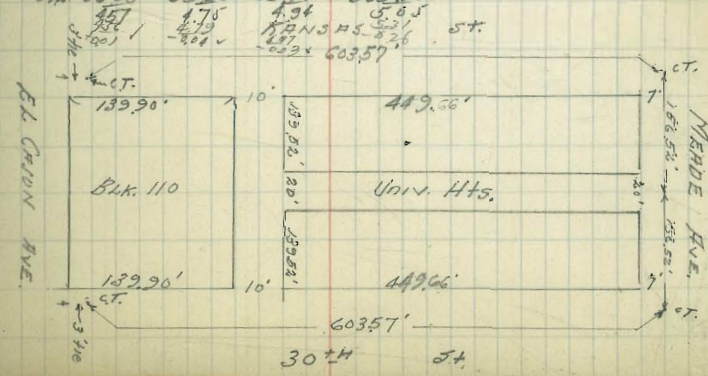
East & West Alley

S.L.	64.80	64.97	65.15	365.32	365.50 = E.L. Alley	365.60 = W.L. Alley	366.20
	5.30	5.13	4.95	4.78	4.60	4.50	3.90
	4.69	4.52	4.80	4.80	4.85	4.75	4.43
	+0.61 ✓	+0.61 ✓	+0.15 ✓	−0.02 ✓	−0.25 ✓	−0.20 ✓	−0.53
N.L.	64.80	64.97	65.15	65.32	65.50	65.60	66.20
	5.30	5.13	4.95	4.78	4.60	4.50	3.90
	4.91	4.76	4.78	4.60	4.37	4.77	4.53
	+0.39 ✓	+0.37 ✓	+0.17 ✓	+0.18 ✓	+0.23 ✓	−0.27	−0.63
S.L.	66.80	67.40	67.40	367.37 (Chk. on = Sissons)			
	5.27	4.67	4.67	4.70			
	5.45	4.46	4.43	4.71			
	−0.18	+0.21	+0.24	0.01 = Error.			
N.L.	66.80	67.40	67.40				
	5.27	4.67	4.67				
	5.12	4.59	3.85				
	+0.15	+0.08	+0.82				

366.78 = Above B.M.
3.87+
370.65 = π

North & South Alley

E.L.	66.25	66.43	66.62	66.80 = Brk.	66.60	66.40	66.20
	4.40	4.22	4.03	3.85	4.05	4.25	4.45
	4.39	4.72	4.54	5.30	5.15	4.77	4.75
	+0.01	−0.50	−0.51	−1.45	−1.10	−0.52	−0.30
W.L.	66.30	66.47	66.63	66.80	66.62	66.44	66.26
	4.35	4.18	4.02	3.85	4.03	4.21	4.39
	4.37	4.68	5.11	4.82	4.79	5.58	4.75
	−0.02	−0.50	−1.09	−0.97	−0.76	−1.37	−0.36
E.L.	66.00	65.80	65.61	65.50			
	4.65	4.85	5.04	5.15			
	4.74	4.32	4.04				
	−0.09	+0.53	+1.00				
W.L.	66.08	65.90	65.71	365.60			
	4.57	4.75	4.94	5.05			
	4.56	4.79	4.97	5.31			
	+0.01	−0.04	−0.03	5.26			

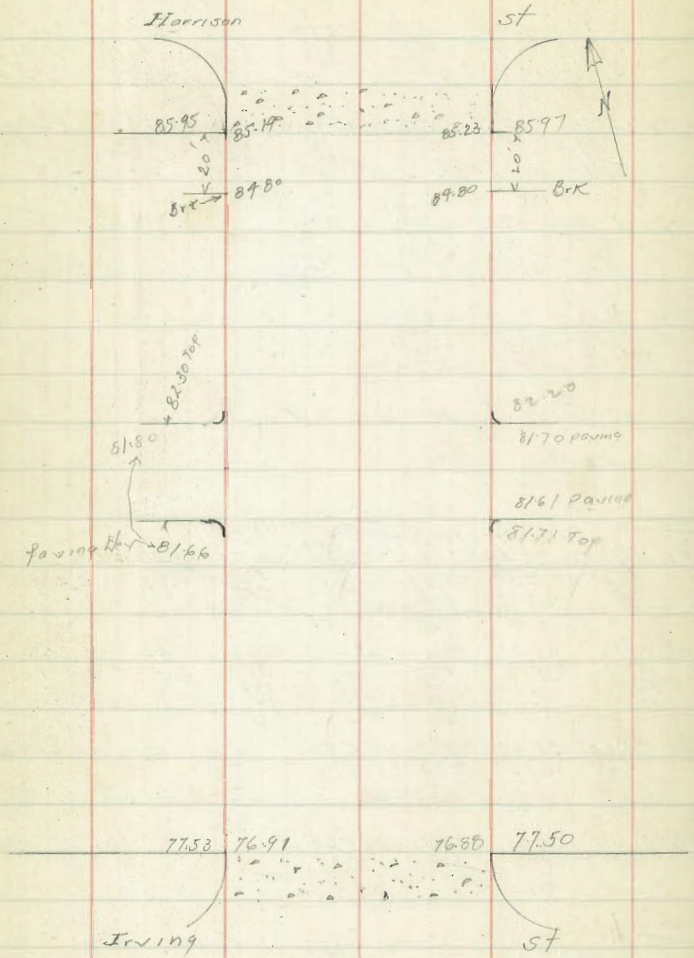


Walker
Bliss
Driebert
Pierce

Oct 15, 1930

Sicard St Paving
Between Harrison & Irving Streets

Daley Corp.
Contractors



77.56 N.W.B.P. Sicard & Irving
9.69+
67.25 H.I.

Walker
Bliss
Drebert
Isobell
10-22-30

GRADES for PAVING

10' Alley Blk. 1 - Roberts Sub.

Bet. PARK BLVD. AND GEORGIA
From El Cajon Ave to Meade Ave
(Plan - 4550-L)

Station		W.L. Grade	El. Station	El. Grade
N.L. -20'	top cb. =	328.30	N.L. -20	cb =
N.L. -20'	PAV. =	327.76	N.L. -20'	PAV. = 327.14
N.L. -12.5 = Blk.	in cb. =	328.55	N.L. -5'	" = 327.70
N.L. -7.5' = "	" " =	328.60		
N.L. El Cajon = 0+00	cb =	328.60		
0+00	PAV. =	328.00	N.L. El Cajon = 0+00	PAV. = 328.00
+40		328.20		328.20
+80 = Blk.		328.40		328.40
1+00 = Blk.		328.80		328.80
+20 = "		329.65		329.65
+40 = "		331.05		331.10
+50 = " on East only			Blk. = S.L. E.+W. Alley	332.10
+60 = "		333.30	Blk. = N.L. " " "	333.40
+80 = "		335.70	Blk.	335.85
2+00 = "		337.50		337.70
+20 = "		338.80		339.00
+40 = "		339.60		339.80
+90		340.80		340.90
3+40 = Blk.		342.00		342.00
+90		342.52		342.57
4+40		343.05		343.15
+90		343.57		343.73
5+40 = Blk.		344.10		344.30

Cont. on P-61

343.58 + 88 = 4 Normal Dr. + Pk. Blvd.
1471
345.05 = T
1303 -
332.62 TP
280 +
334.32 = T
2.19 -
332.13 = TP
12654
344.78 = T
4.05 -
340.73 = TP
5334
346.06 T
2.72 -
343.34 TP
4.07 -
347.43 = T

		cb.	-Pav.	cb.	0+00 -cb.	0+00 Pav.			
W.	28.30	27.76	28.55	28.60	28.00	28.20	28.40	28.80	
	6.02	6.56	5.77	5.72	6.32	6.12	5.92	5.52	
		6.50			5.72	9.48	8.31	7.96	
		+0.06			+0.60	-3.36	-2.44	-2.44	
		-20'	-5'		0+00				
E.		27.14	27.70		28.00	28.20	28.40	28.80	
		7.18	6.62		6.32	5.12	5.92	5.52	
		7.14	6.57		0.01		6.43		
			+0.07				+1.49		

W	29.65	31.05		32.30	35.70	37.50	38.80	39.60	40.80
	4.67	3.27		1.02	1.08	7.28	5.98	5.18	3.98
	2.78	4.98		1.95	10.98	6.88	6.18	5.50	3.75
	-2.09	-1.71		-0.93	-1.86	+0.40	-0.70	-0.32	-0.23
E.	29.65	31.10	32.10	33.40	35.85	37.70	39.00	39.80	40.90
	4.67	3.27	2.27	0.97	8.93	7.08	5.78	4.98	5.16
	1.90	3.91	2.55	1.18	7.93	6.43	5.38	4.77	4.87
	+2.77	-0.69	-0.33	-1.06	+1.00	+0.65	+0.40	+0.21	+0.29

W	42.00	42.52	43.05	43.57	44.10
	5.43	3.54	4.38	3.86	3.33
		2.54	4.33	3.84	3.15
		+1.00	+0.05	+0.02	+0.18
E.	42.00	42.57	43.15	43.73	44.30
	4.06	3.49	2.91	2.33	3.13
	3.06	2.99	1.91		
	+1.00	+1.00	+1.00		

Alley 1 Cont. from P. 60

Alley Station		Alley Grades	Ex. Station		Ex. Grade
5+50 = BK.		344.15		BK.	344.35
+60 = "		344.10		"	344.25
+70 "		343.90		"	344.05
+80 "		343.71/60		"	343.93/80
+90. "		343.44/20		"	343.66/40
+99.4 = 52. Meade		342.92/60	92 = Exist Pav.	"	43.18 = Exist Paving 342.80

Above change made to Meet exist. Paving

CULVERT #				Flow Line	Flowl. Cuts
0+00 = Alley		334.37	8.96	325.36	324.80	+0.56
+15 = El Alley			7.82	326.50	324.50	+2.00

35' N Nly. El Casein.

Location New Culvert to Meet Exist 6" Drain.

					Flowl. Line	Flowl. Cuts
		30.26				
0+15			5.96	24.30	24.30	
T.P	1.65	29.85	2.06	28.20		
			4.65	25.20	24.80	+0.40

28.20 = Elev. Grade Stake 0+40 on E
2.06
30.26 = T
Flow Line Cuts.

34743 = T
313
34430 = TP
459
345.89 = T
4

				4371	4344	42.92		
N	44.15	44.10	43.90	43.60	43.26	42.60	43.92	
	3.28	3.79	4.29	5.17	5.45	6.29		
	2.28	2.62	4.64	4.58	4.36	3.87		
	+1.00	+0.17	+0.35	+0.59	+1.09	+0.32		
				4393	4346	43.18		
E	44.35	44.25	44.05	43.80	43.40	42.90	43.18	
	4.53	4.64	4.84	4.96	5.23	6.09		
	4.57	4.37	3.84	3.96	4.23	5.71		
	+0.07	+0.32	+1.00	+1.00	+1.00	+0.38		

2+00	233.03
+50	235.78
+95.15 = cb. P.C. S.E. Cor Juniper on 6th	238.27
①	238.70
②	239.10
③	239.40
④ = Cb. E.C. S.E. Cor. Juniper on Juniper.	239.60
= cb P.C. N.E. " " " "	240.20
①	240.05
② " "	240.00
③ " "	240.05
④ = cb. E.C. on 6th N.E. "	240.15
= 0+00 = 6' N.W.L. Juniper	241.40
+50	242.65
1+00	243.90
+50	245.15
2+00	246.40
+94 = Blk. = S.L. Kalmia Produced	247.50
S. Kalmia " "	248.00
N.L. " "	248.50
= 0+00 = Blk.	248.95
+50	249.40
1+00	249.85
+50	250.31
2+00	250.63
+34.85	250.94
+69.7 = beg. Exist. cb.	

241.75 = π from P 62

E	233.03	235.78	238.27	238.70	239.10	239.40	239.60
	2.72	2.97	2.48	3.05	4.92	4.67	4.42
					-5.18	-4.89	
					-0.26	-0.27	

E	240.20	240.05	240.00	240.05	240.15	241.40
	3.82	3.97	4.02	3.91	3.87	11.60
		-0.50	-0.30			

					Blk.	
E	242.65	243.90	245.15	246.40	247.50	248.00
	10.25	9.10	7.85	6.60	5.50	5.00

	Blk.					= Blk.	
E	248.50	248.91	249.33	249.74	250.16	250.55	250.94
	4.50	4.09	3.67	3.26	2.84	2.45	2.06

251.99 = N.W.L. B.P. 6th Mod Laurel
1.07 +
253.00 = π
1.01 -
240.03 = T.P.
3.99 -
244.02 = π

those Grades are according to Profile Plan. but were Changed to Meet Exist cb. 313' S.S.L. Laurel by Permission - Chas Moore
See New Notes below.

Elev. Station 0+00 see above

248.50	E	248.50	248.95	249.40	249.85	250.31	250.63	250.94
5.15			4.70	4.75	3.80	3.32	3.02	2.71
= 253.65 = π								

6TH ST.
PAVING E. 1/2
bet. DATE AND LAUREL

FIR ST.

ELM

DATE

HAWTHORNE

GRAPE

.72 Crown.

.7 Crown.

.78 Crown.

6TH

164.26

161.29

152.04

149.88

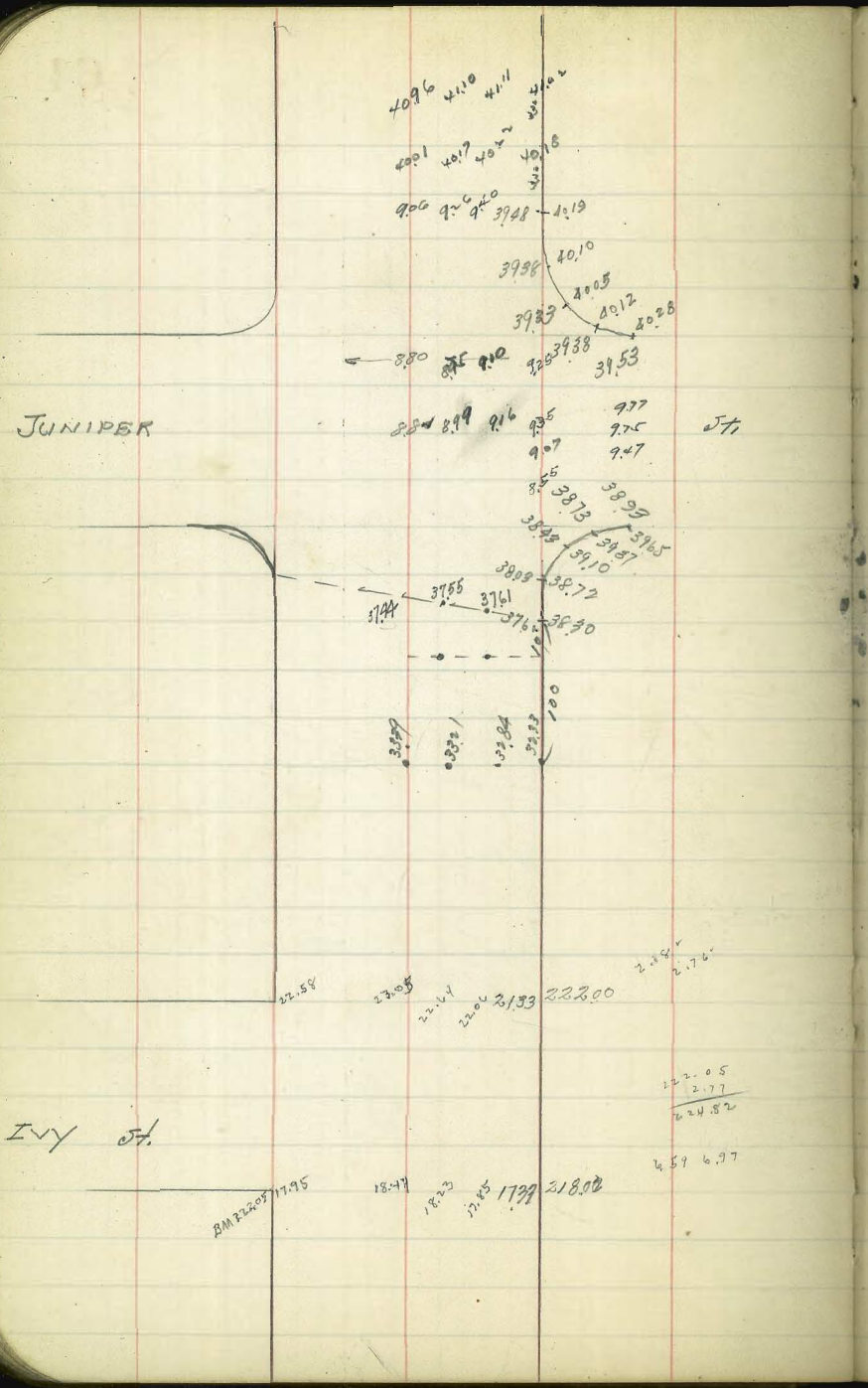
166.6

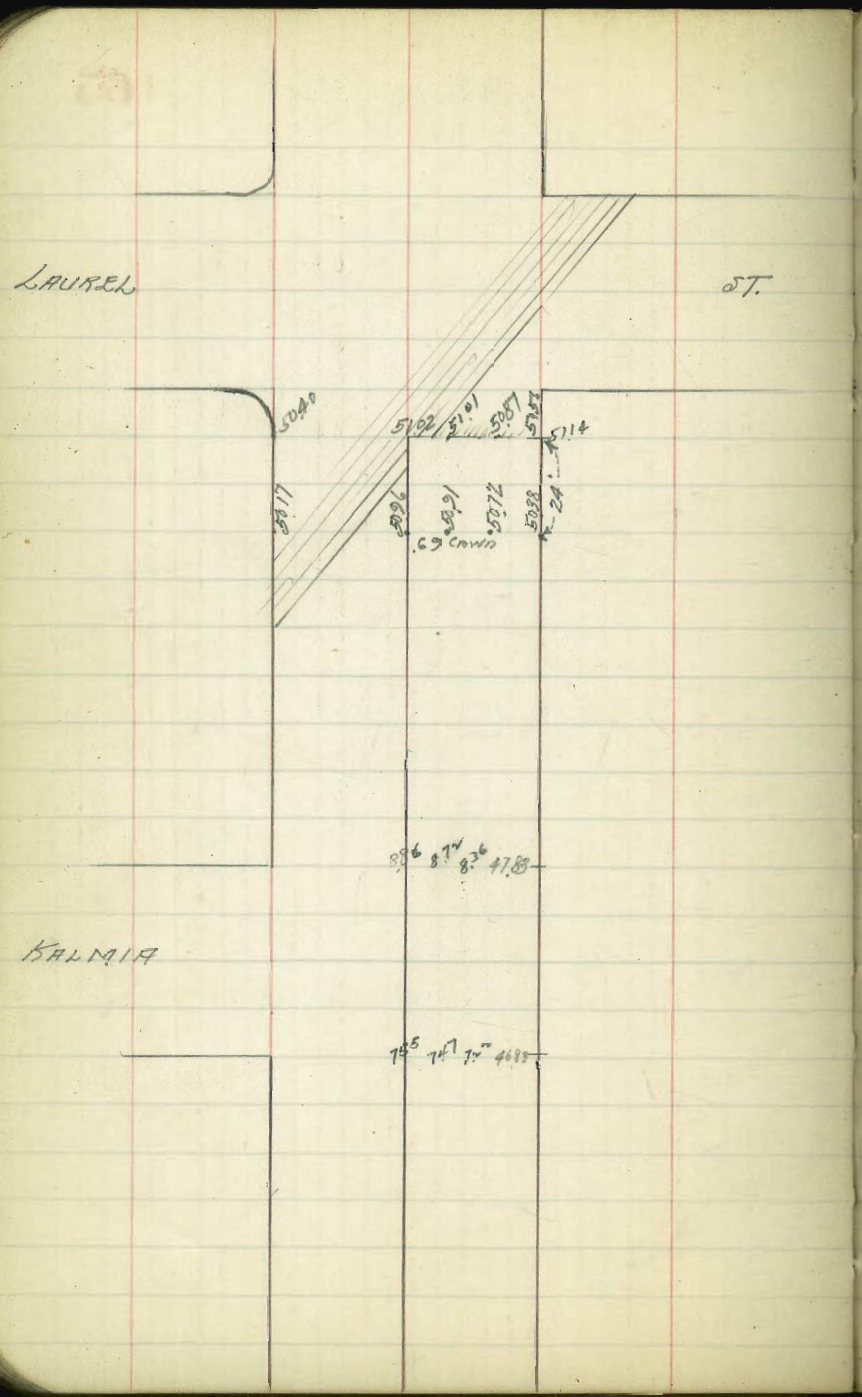
143.95

180.04
0.13
180.19
12.61
167.58
1.37
168.95
180.06
0.21
180.27
180.06
11.59
191.65
12.57
204.22

202.33
203.00
198.70
183.50
179.00
172.00

BM 180.06
S.W. Fire Hydt.
top.


JUNIPER
IVY ST.


LAUREL
ST.
KALMIA
50.40
51.02
51.01
50.87
51.14
50.17
50.96
50.91
50.72
50.38
24
.69 crown
8.86
8.72
8.36
47.83
7.55
7.47
7.22
46.83

Walker
Bliss
Flood

GRADING Alley Blk. 8 Reed + Hubbell's Add to Logan and National

Bet Logan and National
From El. 29th to Nl. 30th
DRAWING No - 4554-L

Stations El. 29th St.	N.L. Grade	Fl. Grade
=0+00	64.60	64.60
+50	64.85	64.85
1+00	65.10	65.10
+50	65.35	65.35
2+00	65.60	65.60
+50	65.85	65.85
3+00	66.10	66.10
+50	66.35	66.35
4+00	66.60	66.60
+50	66.85	66.85
5+00	67.10	67.10
+50	67.35	67.35
6+00 = Nl. 30th	67.60	67.60

SEWER LATERALS For Above Alley

				Flow Line	
Lat #1	69.41	2.30	67.11	60.30	+6.81 ✓
" #2	71.41	5.01	66.40	60.66	+5.74 ✓
" #3	73.30	5.67	67.63	61.84	+5.79 ✓

9th + Nd

6104 = Nl. 8th Nat'l. + 29½
1471
69.41 = A
2.24
67.17 = TP
4.24 +
71.41 = A
3.37 -
68.04 = TP
5.26 +
73.30 = A
5.45 -
6785
527
7306

67

Nl.	64.60	64.85	65.10	65.35	65.60	65.85	66.10	66.35
	4.81	4.56	4.31	4.06	5.81	5.56	5.31	5.06
	4.55	2.56	2.60	2.30	5.98	4.56	5.07	4.06
	+0.26 ✓	+2.00 ✓	+1.71 ✓	+1.76 ✓	+1.83 ✓	+1.00 ✓	+0.24 ✓	+1.00 ✓
Sl.	64.60	64.85	65.10	65.35	65.60	65.85	66.10	66.35
	4.81	4.56	4.31	4.06	5.81	5.56	5.31	5.06
	4.72	3.67	3.31	2.71	4.61	5.63	5.99	5.58
	+0.09 ✓	+0.89 ✓	+1.00 ✓	+0.35 ✓	+1.20 ✓	-0.07 ✓	-0.68 ✓	-0.52 ✓

Nl.	66.60	66.85	67.10	67.35	67.60
	4.81	4.56	6.20	5.95	5.70
	3.31	3.56	5.01	4.95	5.64
	+1.00 ✓	+1.00 ✓	+1.19 ✓	+1.00 ✓ 7306 = A	+0.06 ✓
Sl.	66.60	66.85	67.10	67.35	67.60
	4.81	6.43	6.20	5.77	5.70
	3.67	5.17	4.45	5.89	5.63
	+1.14 ✓	+1.28 ✓	+1.75 ✓	-0.18 ✓	+0.07 ✓

Sewer Const.
Presidio Ridge
Drawing No 4544-L

				Flow Line	Cuts	offsets	B.M. Pine & Ansta N'E'L'Y' 7' tack
M.H. No. 1							
= 0+00	253.20	12.19	241.01	234.28	+6.73	10' Rt. +10' Rt. (stub)	
+42.8		7.93	245.27	236.03	+9.24	5' Lt. "	
+85.6		6.19	247.01	237.78	+9.23	5' Lt. "	
				239.53	+9.07		
1+28.5 = ℄ Drop MH#2 = ℄ Ansta = Δ 90° Lt.		4.60	248.60	241.00	+7.60	Production ℄ Chisel Mk. on cb. East.	
+63.95		3.35	249.85	242.95	+6.90	12' Rt ℄ " " " "	
+99.40 = ℄ MH#3 = Δ 90° Rt		2.00	251.20	244.90	+6.30	12' " " " " " "	
2+52.4	261.48	8.07	253.41	247.81	+5.60	5' " " Stub.	
3+05.40 = ℄ MH#4 = Δ 90° Lt.		4.75	256.73	250.73	+6.00	115' N ℄ Chisel Mark. in Wall	
+48.9		3.48	258.00	253.12	+4.88	5' Lt ℄ Stub.	
+92.4 = D.E.		0.18	261.30	255.52	+5.78	" " " "	

Line South of M.H. #4

MH#4 = 0+00				250.73		
0+44.82 = End Sewer Line	261.62	5.39	256.23	251.69	+4.60	Chisel Mark.

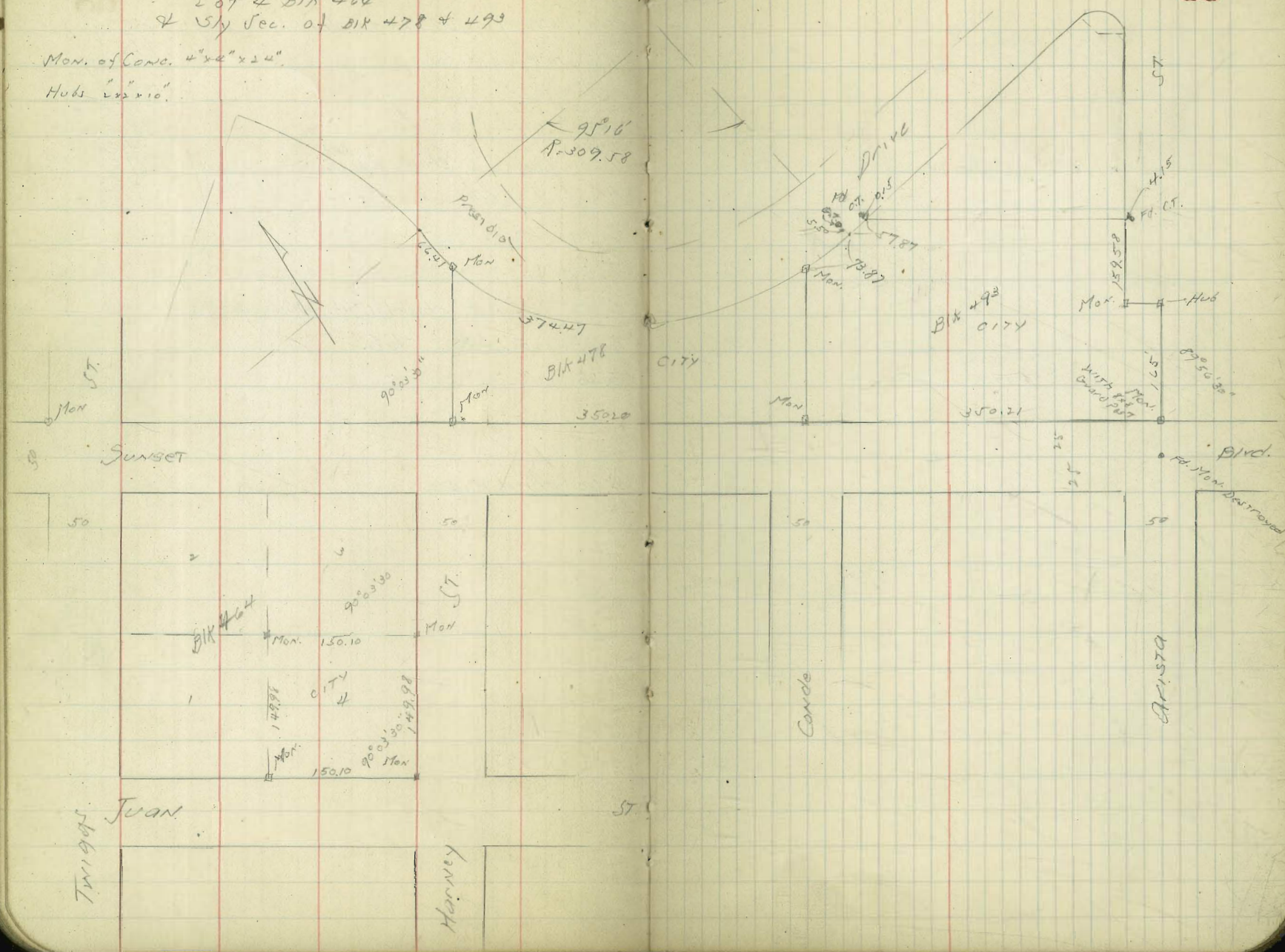
245.94
7.26 +
253.20
1.91 −
251.29 = T.P.
10.19 +
261.48 = x
4.44 −
257.04 = T.P.
4.58 +
261.62 =

Survey of City Property
in Old Town
Lot 4 Blk 464
& Sly Sec. of Blk 478 & 493

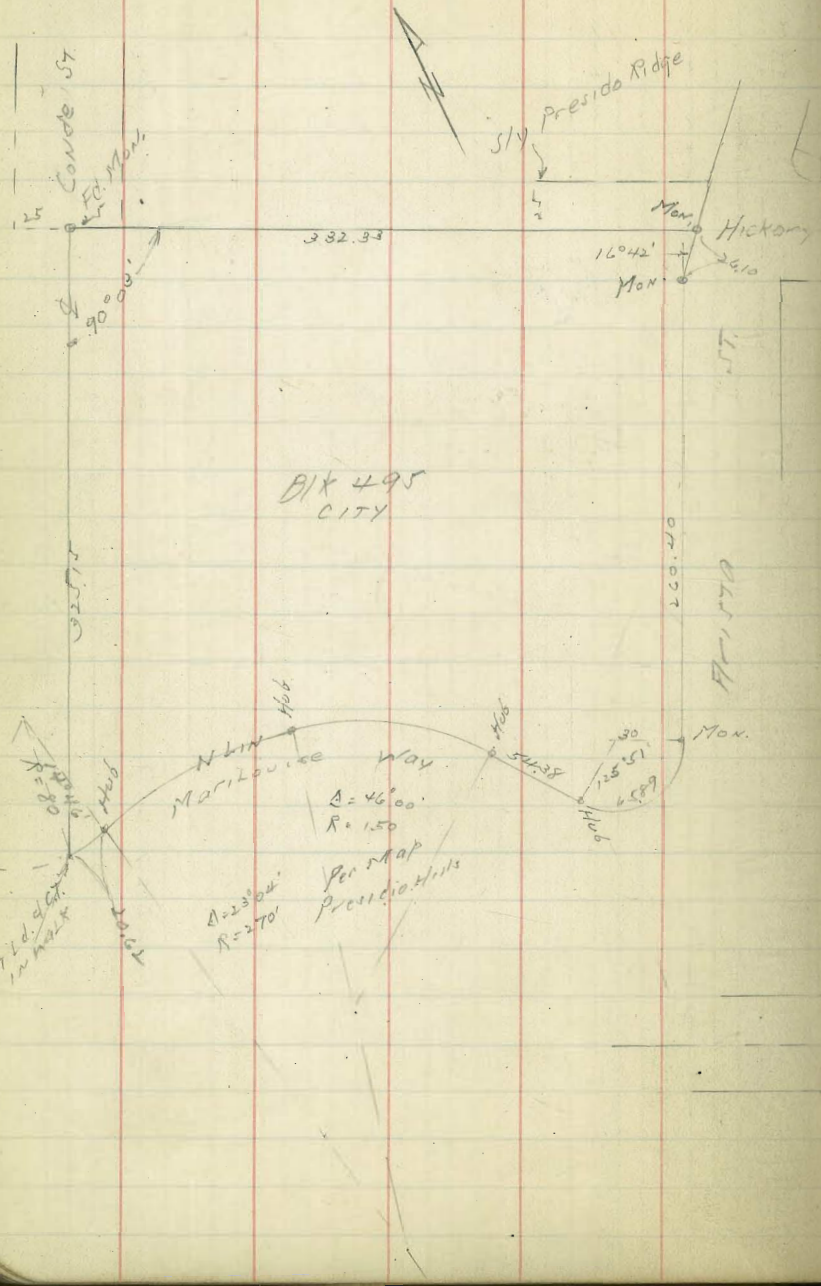
Moore, Sib. Nor. 2-25-37

Indexed C.S.K. Plotted - TPS - 516 4-5-48 - McQ

Mon. of Conc. 4"x4"x24".
Hubs 2"x2"x10".



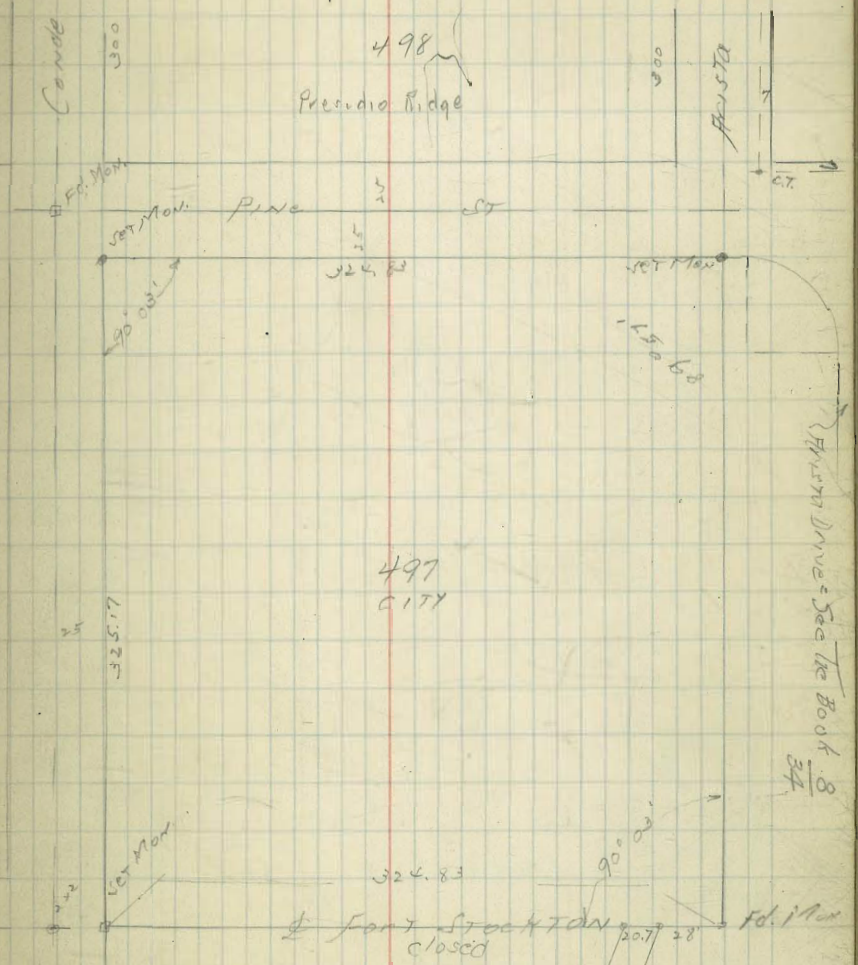
Survey City Prop. Moore
Blk 495 Old Town 2-37



Indexed
C.S.K.

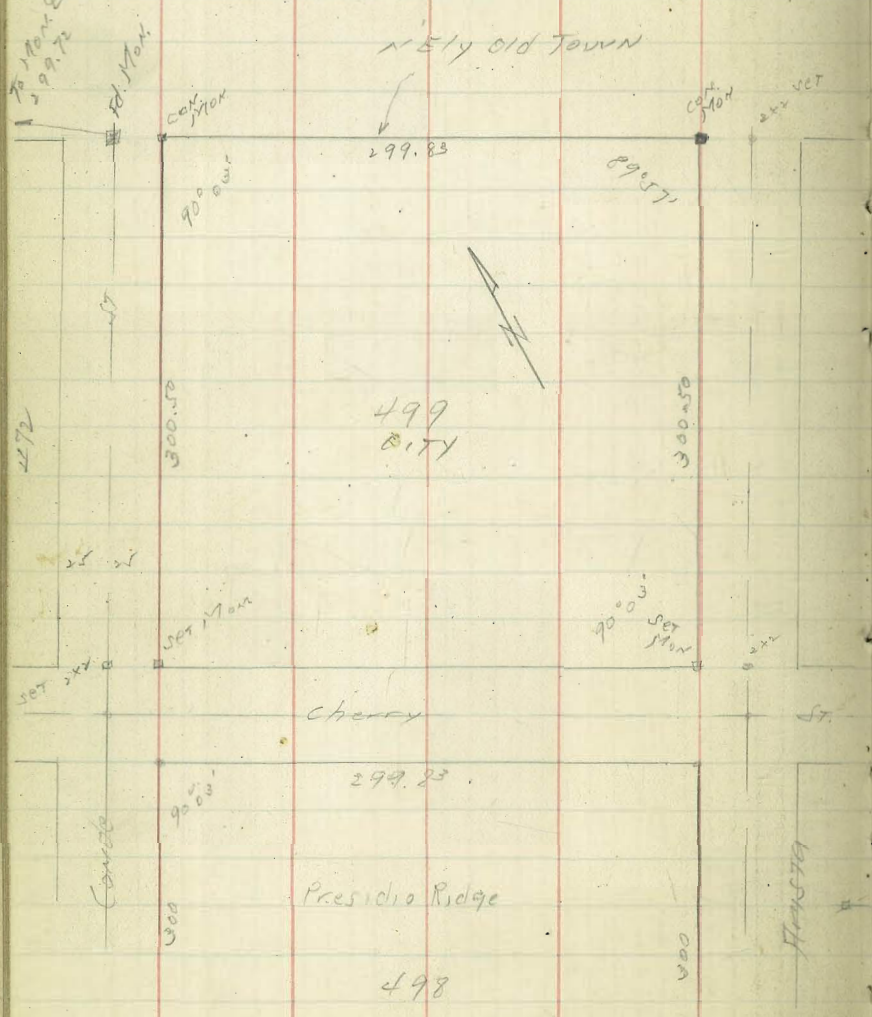
70

Survey Blk 497 Old Town
Plotted TPS 506
4-8-48-MRR



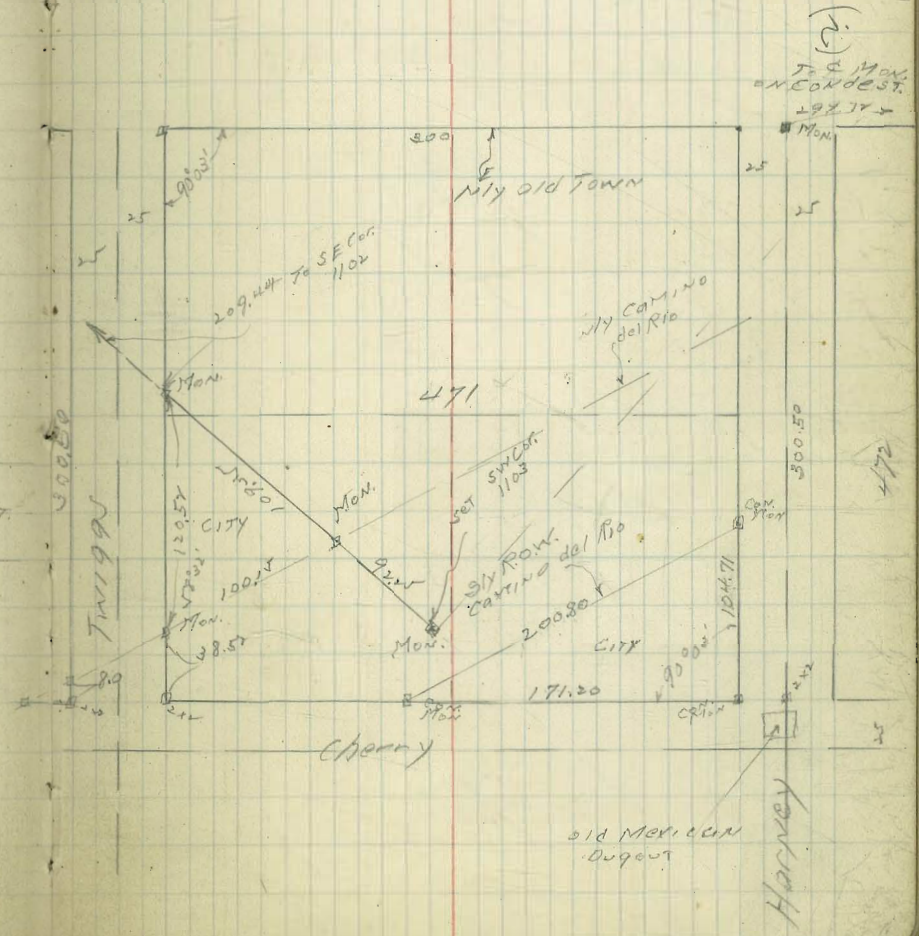
Plotted TPS 501
McQ - 4-9-48

Survey Blk 499 Old Town



Indexed
C.S.K.

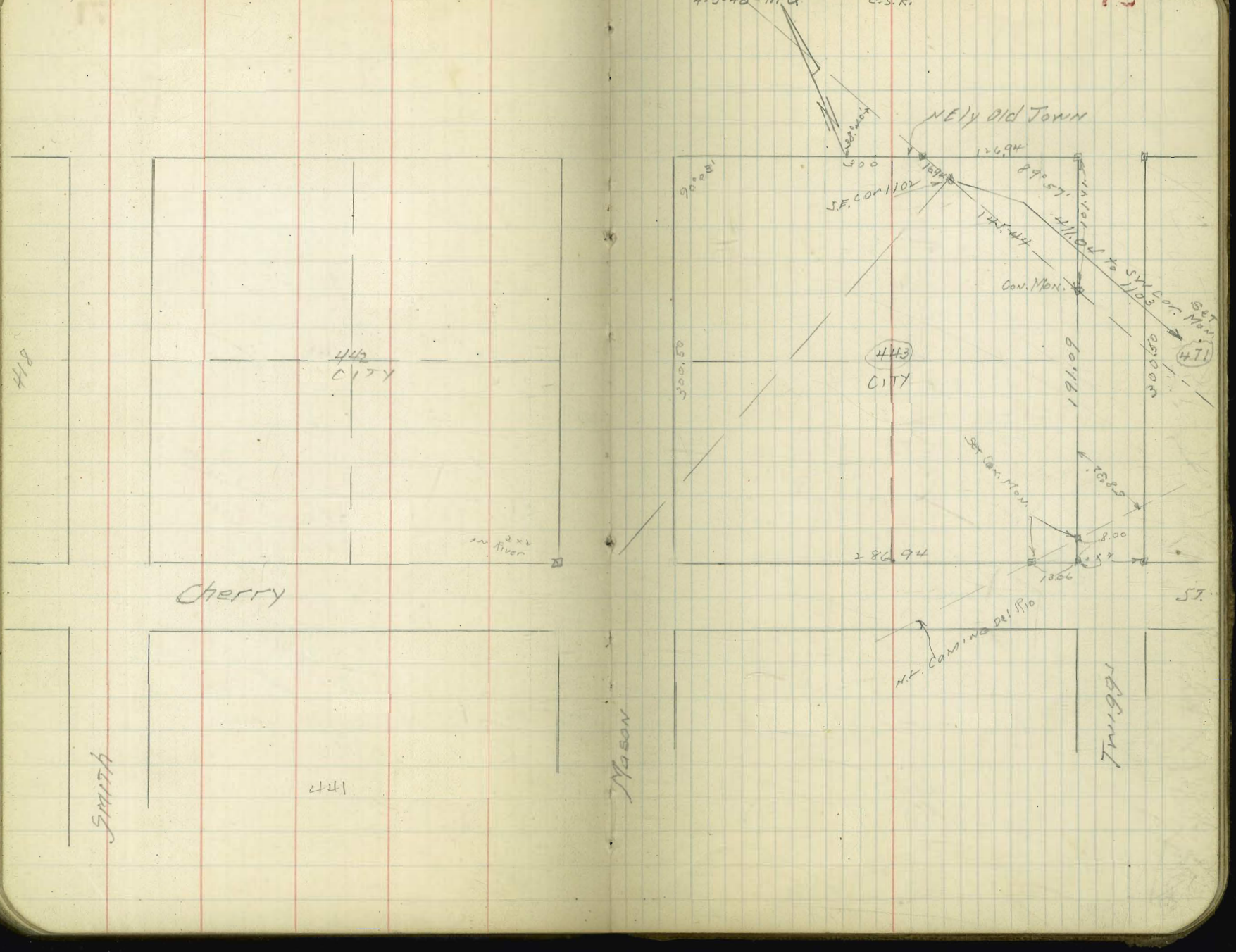
Plotted TPS-502
4-9-48 McQ

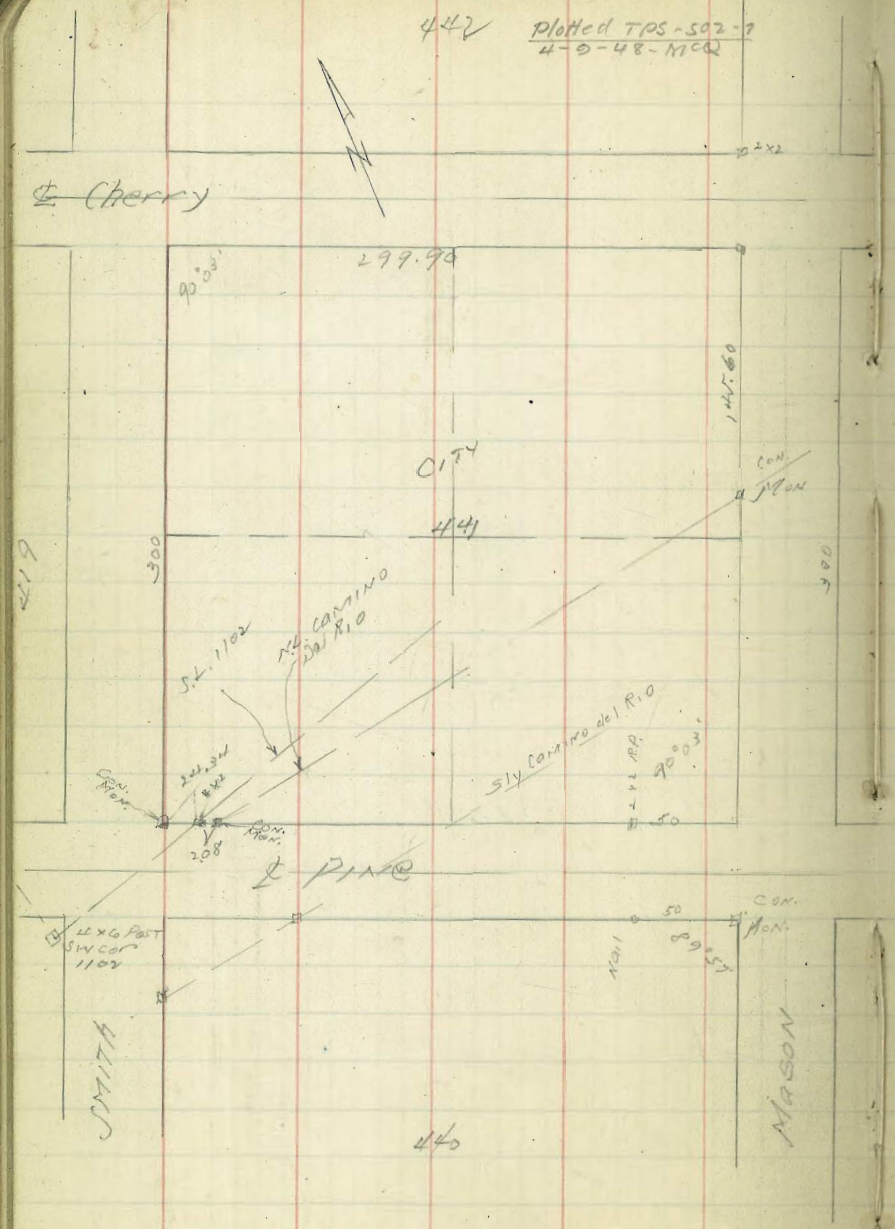


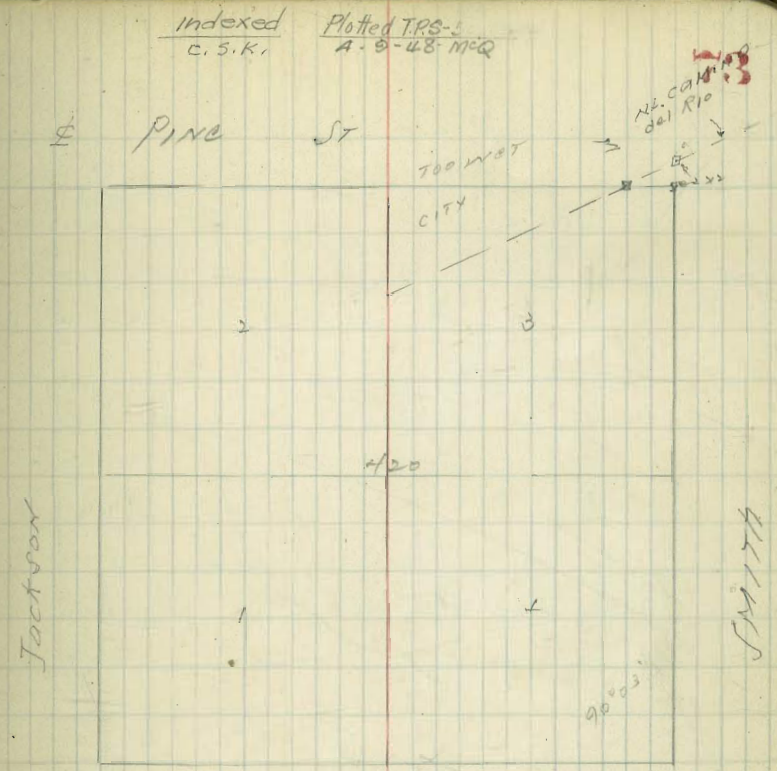
Plotted TPS-502
4-9-48-MCQ

Indexed
C.S.K.

72



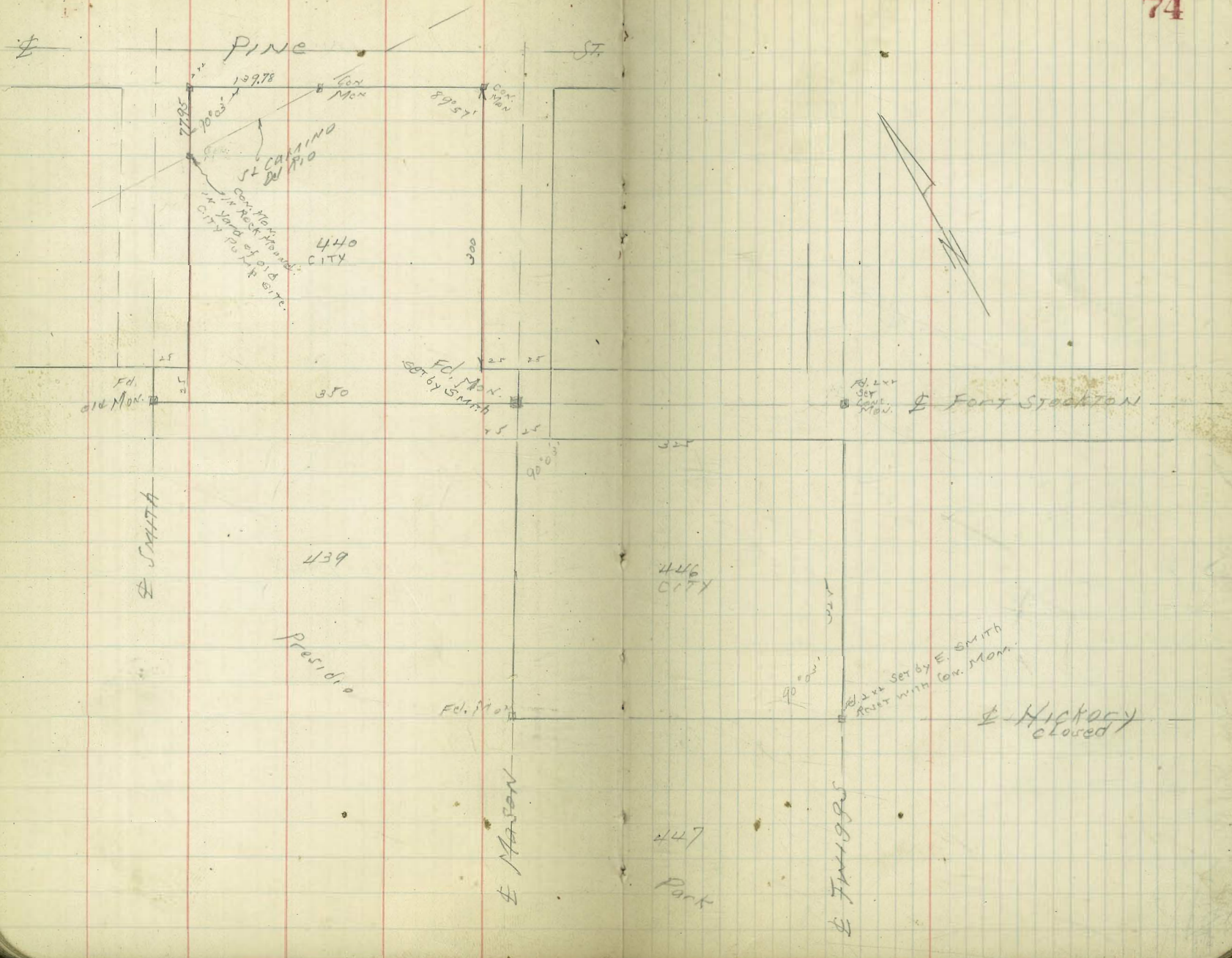

442
Plotted TPS-502-1
4-9-48-McQ
℄ Cherry
299.90
90°03'
145.60
CITY
441
CON. MON.
300
419
S.L. 1102
N.L. Camino del Rio
Sly Camino del Rio
90°03'
50
208
℄ Pine
4x6 Post SW Cor 1102
50
CON. MON.
89°57'
Nail
Smith
Mason
440


Indexed
C.S.K.
Plotted T.P.S-
4-9-48-McQ
℄ Pine St
Too Wet
City
N.L. Camino del Rio
2
3
420
1
4
90°03'
Jackson
Smith
Fort Stockton St.

Indexed
C.S.K.

Plotted T.P.S. 507
4-8-48 MHQ

74

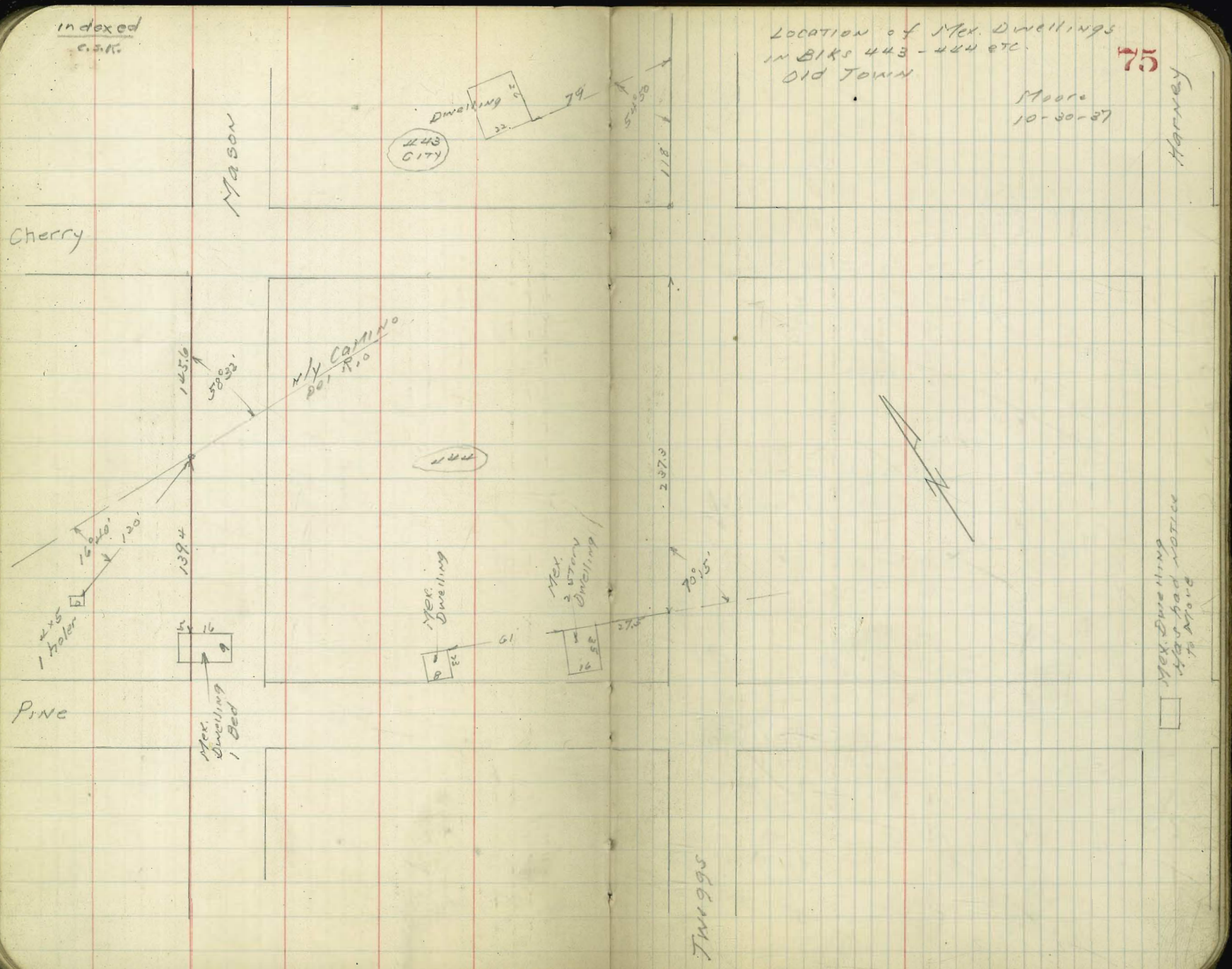


indexed
C.S.R.

LOCATION of Mex. Dwellings
IN BLKS 443 - 444 ETC.
OLD TOWN

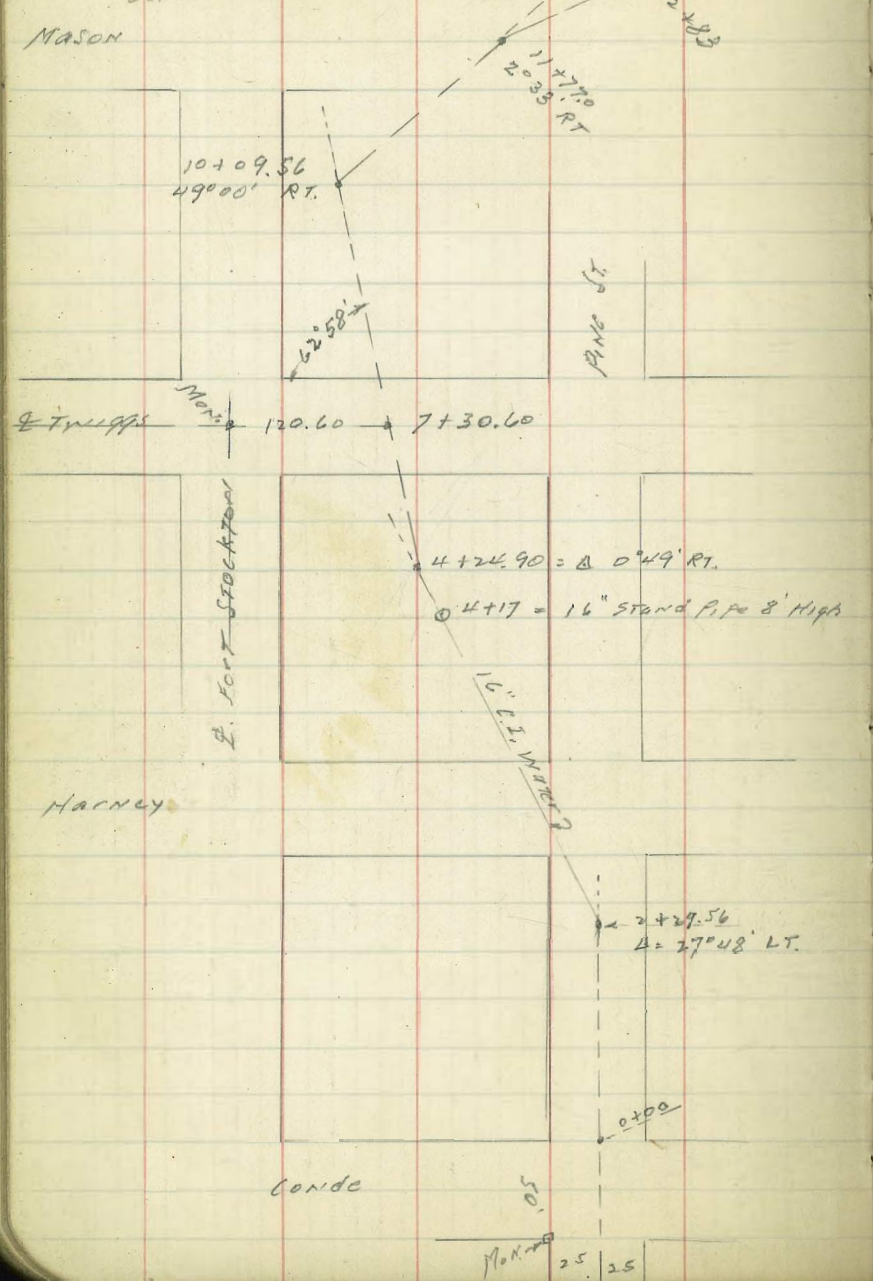
75

Moore
10-30-37



Location of 16" C.I. Water Main

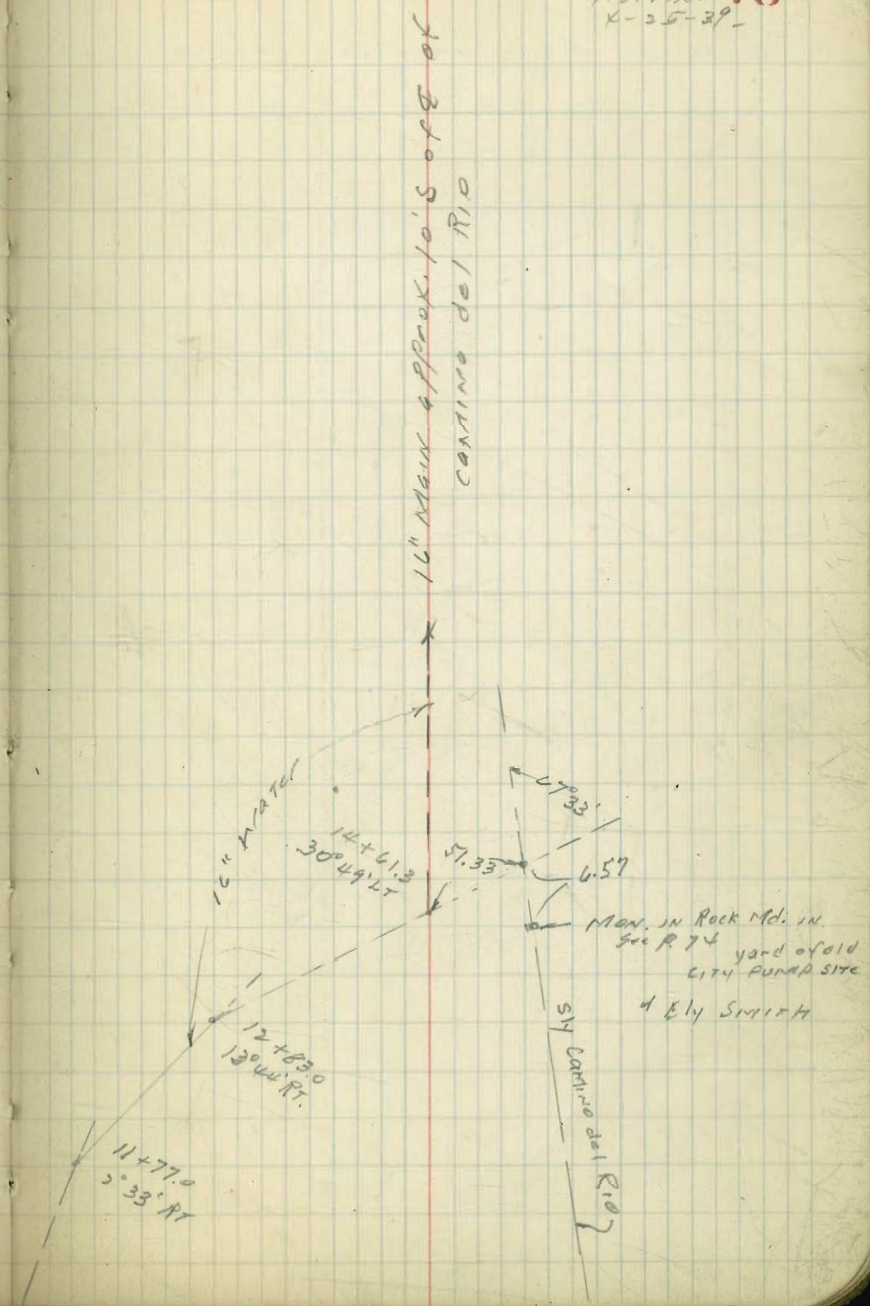
Pine & Conde to Mason & Camino del Rio



Indexed
C.S.K.

Moore
Sisson
Northern
4-25-39

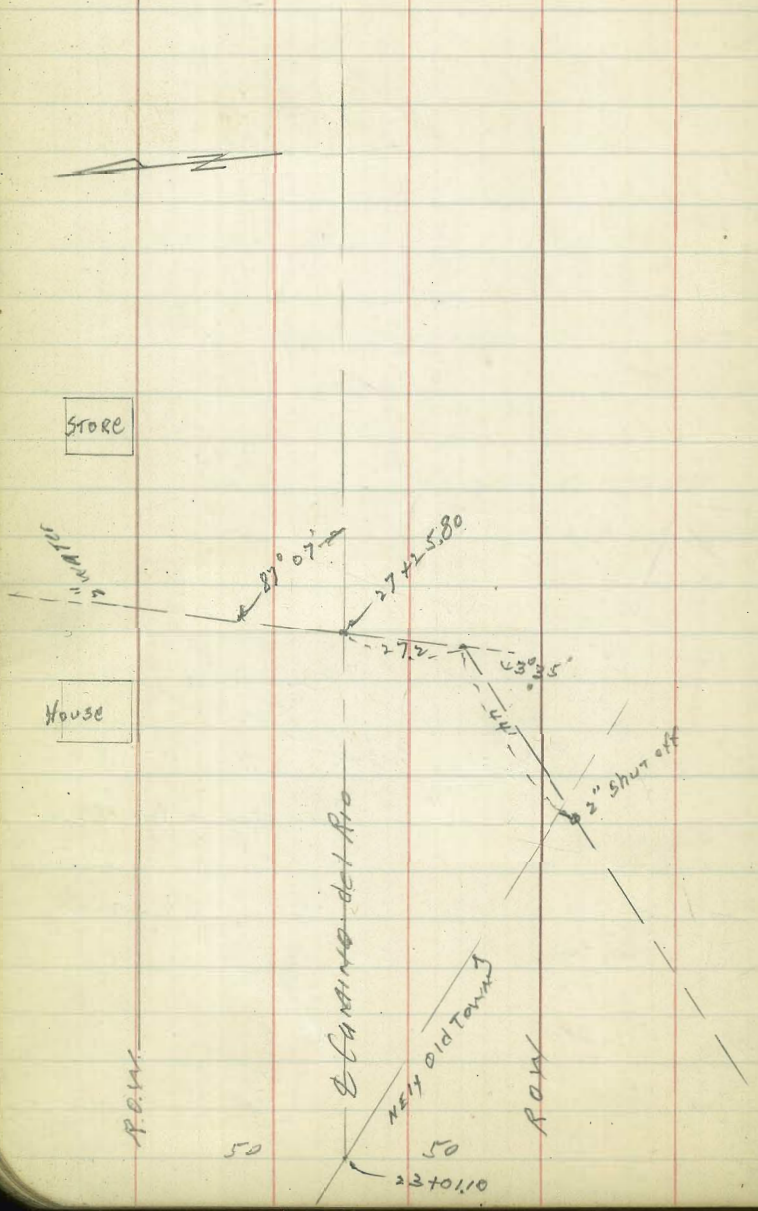
76



Indexed
e.s.k.

77

Location of 2" water line P.L. 11+20



Walker
Mt Hugh
Mottoon
Lee of
5-20-29

BENCH MARKS
SAN DIEGO Ave And TAYLOR St.
Bet. Harney and old Town Bridge

	3.79	34.41		30.62	✓ S.W. B.P. San Diego & Harney
T.P.	0.11	25.66	8.86	25.55	S.E. Top Hdyt. S.D. & Mason.
			2.59	23.07	✓ S.E. 7' tack S.D. Ave & Mason
T.P.	2.48	17.98	10.16	15.50	
			5.36	12.62	✓ B.M. 3 nails in Pole S.W. S.D. Ave. Wallace
T.P.	2.62	8.64	11.96	6.02	
			New Location = 1.46		on 62.19 Radius hub S.D. Ave & Taylor. S.E.
			~~6.79~~	~~1.85~~	
			5.69	2.95	✓ 3' Nails Pole S.W. S.D. Ave & Taylor
T.P.	5.77	10.49	3.92	4.72	✓ S.E. B.P. Taylor And Jaun St.
		2 Nails in Bld. S.W. Taylor & Whitman = 6.96			~~S.W. Top Hydt.~~
~~T.P.~~	~~3.89~~	~~12.72~~	~~1.66~~	~~8.83~~	~~Taylor And Whitman~~
			5.87	6.85	
			4.01	8.71	✓ S.E. B.M. 3 nails in Pole Taylor & Chesnut St.
TP	9.61	21.17	1.16	11.56	
			1.10	20.07	✓ B.M. B.P. S.L.Y. End Bridge

S.W. 7' tack S.D. Ave & Harney = ✓ 30.67

S.E. Brass Plug Lapolla & Arista St. ✓ 35.48

S.E. " " " " Ampudia ✓ 43.75

S.W. " " CONDE And SAN DIEGO ✓ 31.97

Sketch Page 10

Walker McHugh McHoon 2-26-29

CURB. LEVELS on SAN DIEGO AVE
50' West Harney to 40' E Harney

S. Diego

5.20	35.82		30.62 – BM. S.W. Harney
50' W.W.L. Harney = 0+00			
S top Walk at Store.		5.15	30.67
cb		5.42	30.40
0+13.5 = ℄ Doorway			
cb.		5.35	30.47
+11		5.07	30.75
+12 = S in Doorway on Walk		4.97	30.85
0+37			
S in Doorway		5.00	30.82
cb.		5.24	30.58
0+50 = W.L. Harney			
cb.		5.20	30.62
S at Bld. on Walk		4.97	30.85
E.L. Harney			
S at Bld. on Walk		4.79	31.03
cb.		5.04	30.78
0+40 = End Exist. Walk			
cb.		4.92	30.90
S on Walk at Bld		4.59	31.23

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IMPROVED TABLES

AND

INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

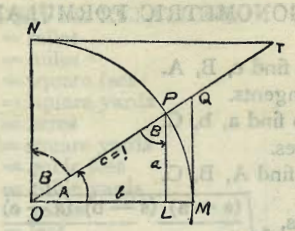


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot P = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$

Table II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.
Use Law of Tangents.

Given A. B. c; to find a, b, C.
Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \quad \sqrt{\frac{(s-a)\ (s-b)\ (s-c)}{s}} = r$$

$$\text{also } \tfrac{1}{2}A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \tfrac{1}{2}A = \frac{r}{s-a}$$

$$\tan \tfrac{1}{2}B = \frac{r}{s-b}$$

$$\tan \tfrac{1}{2}C = \frac{r}{s-c}$$

Area of a triangle:

Area $= \tfrac{1}{2}$ ab Sin C

Area $= \sqrt{s\,(s-a)\ (s-b)\ (s-c)}$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}(B+b+4M)$$

h = altitude; b, B = bases; M = midsection

Table III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/16
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	3/16
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	1/4
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	5/16
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	3/8
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	7/16
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	1/2
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	9/16
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	9688	5/8
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	11/16
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	3/4
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	13/16
7/8	.0729	.1563	.2396	.3229	4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	7/8
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	15/16
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

Table IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

360° = 21600′ = 1296000″

Radius = arc of 57.2957790°

Arc of 1° (radius = 1) = .017453292

Arc of 1′ (radius = 1) = .000290888

Arc of 1″ (radius = 1) = .000004848

$\pi = 3.141592654$ $\qquad \sqrt{\frac{1}{4}} = 0.564190$

$\frac{\pi}{4} = 0.785398163$ $\qquad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$

$\frac{\pi}{6} = 0.523598776$ $\qquad \pi^2 = 9.869604401$

$\sqrt{\frac{4}{\pi}} = 1.128379167$ $\qquad \frac{1}{\pi^2} = 0.101321184$

$\frac{\pi}{6} = 0.523598776$ $\qquad \sqrt{\pi} = 1.772453851$

$\frac{4.\pi}{3} = 4.188790205$ $\qquad \frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

Probable error of a single observation $= 0.6754\sqrt{\frac{\Sigma v^2}{n-1}}$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance $= R - R \sin^2 a + C \cos a$

Vertical Distance $= R\ \tfrac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

Table X.

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

Table XI.

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

Table XII.

INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

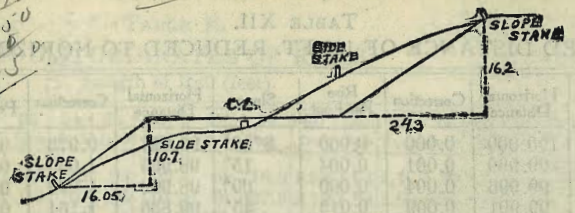
Table XIII.

MINUTES IN DECIMALS OF A DEGREE.

0 30″	.00833	10′ 30″	.17500	20′ 30″	.34167	30′ 10″	.50833	40′ 30″	.67500	50′ 10″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

C ° ′	R Feet
0–20	1718
0–40	859
1–0	573
1–20	429
1–40	343
2–0	286
2–20	245
2–40	214
3–0	191
3–20	171
3–40	156
4–0	143
4–20	132
4–40	122
5	114
6	955.
7	819.

To find leng



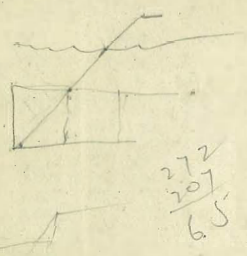
DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

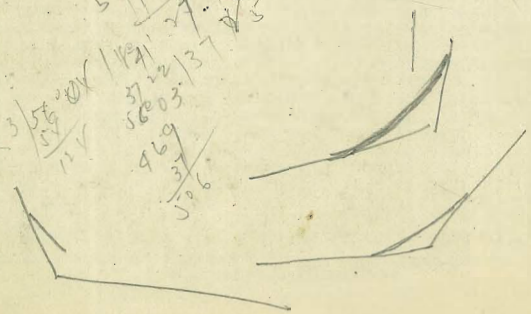
SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

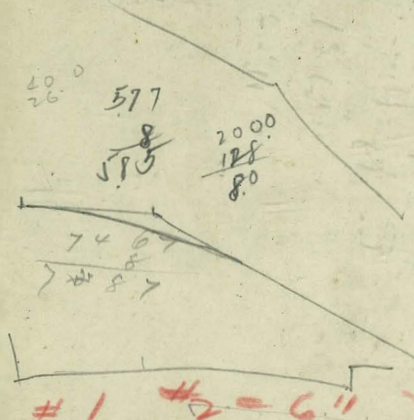
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6 75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24 60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44.25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47 25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49 50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51 75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

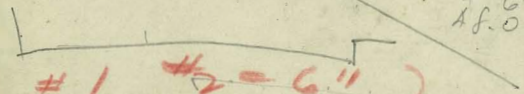
Computed by L. Leland Locke.

Lots 3 and 4
Blk. M. Montclair
add.
Preston









#1 #2 = 6"
#3
#5 = 6"
#7
#9

Taylor