

GRADE:

157

PASTS

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FIELD BOOK

No. 385

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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
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CHICAGO, ILL.

MICROFILMED

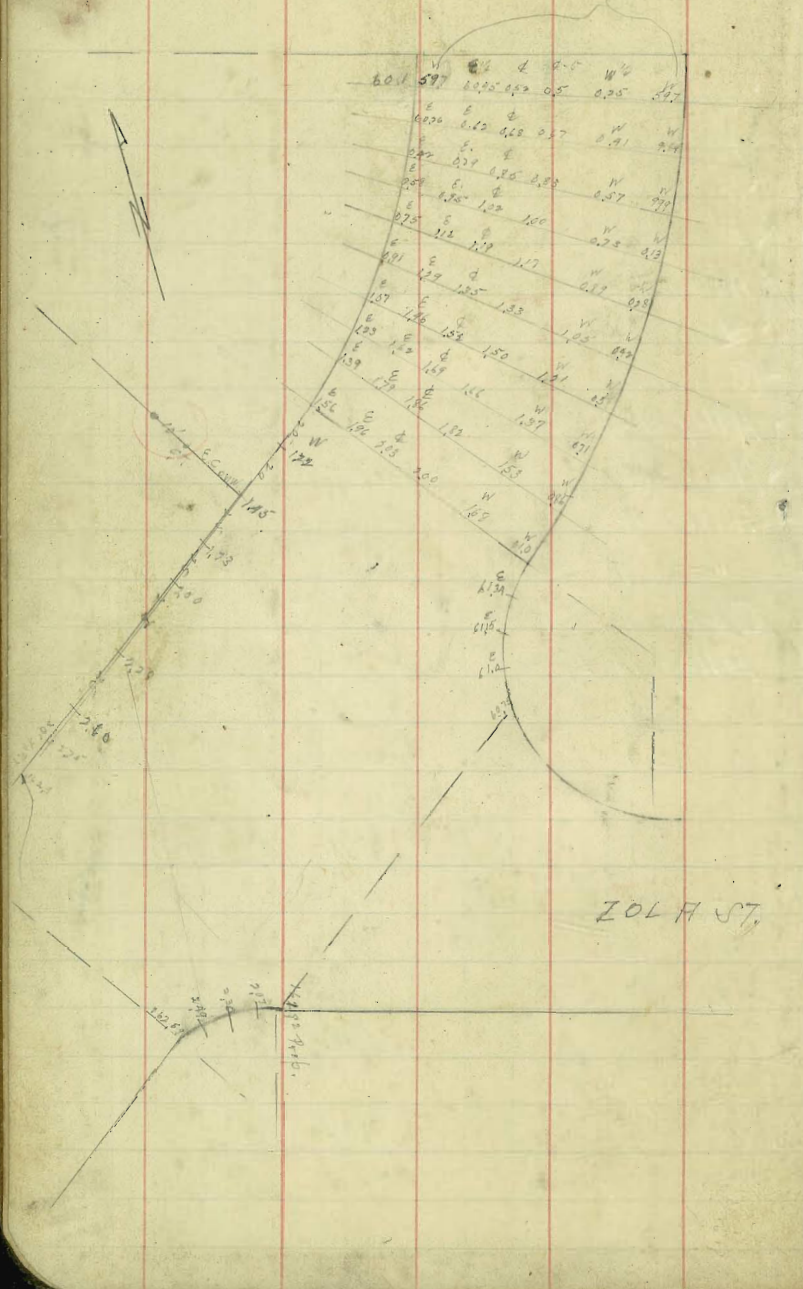
APR 9 1965

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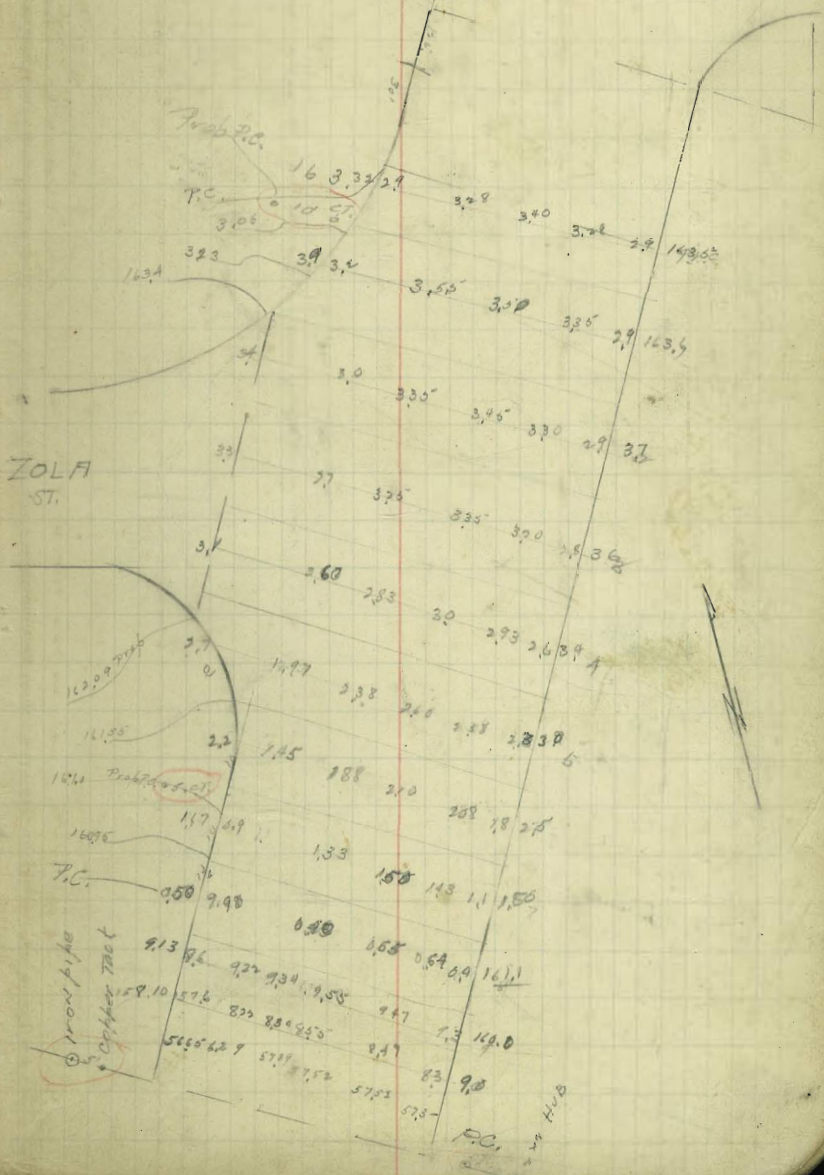
Sidewalk



ZOLA ST

01

ZOLA ST



ZOLA ST

iron pipe  
Copper Mat

100

CHATS WORTH Blvd

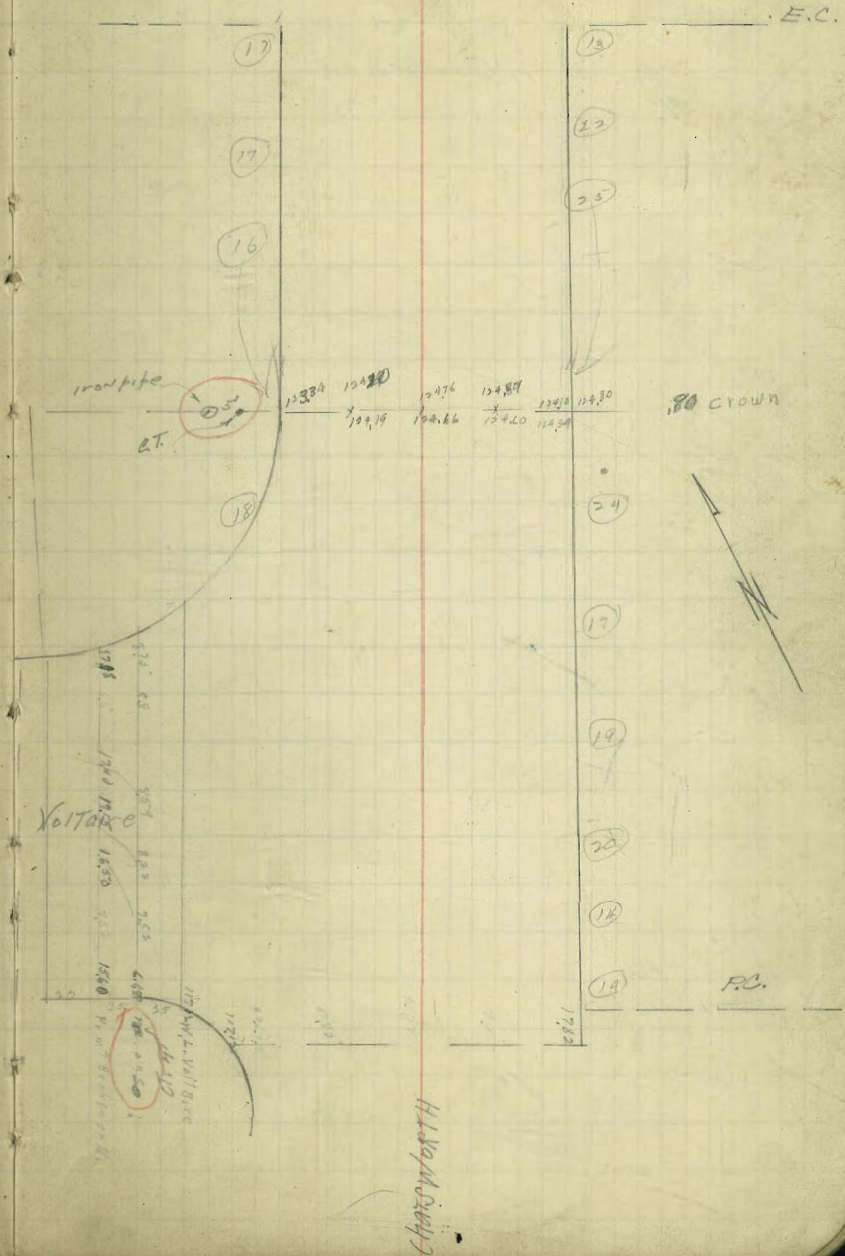
iron pipe 105

O.T. 1532

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iron pipe 105

O.T. 1532



Vol 179144 VT.

Villa Drive

3

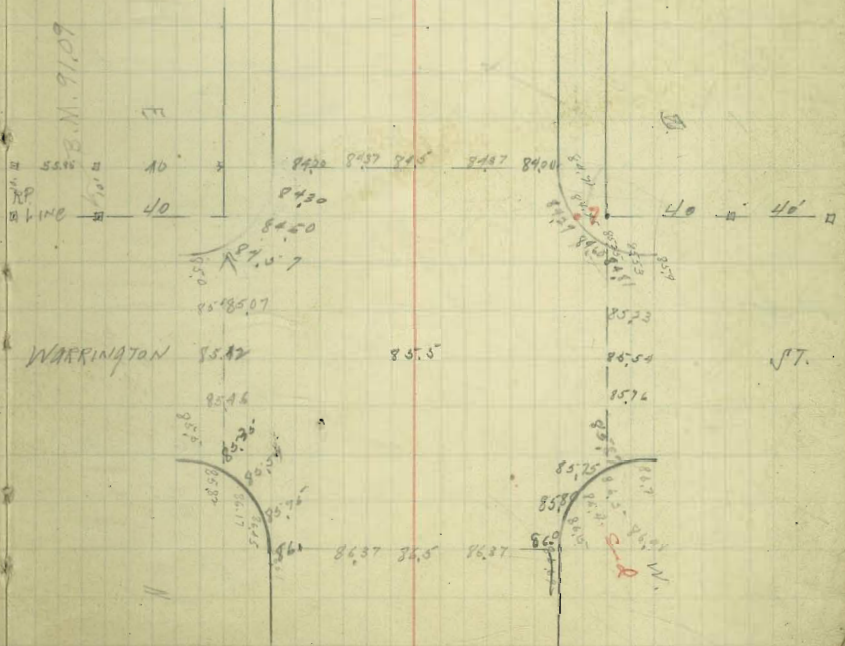
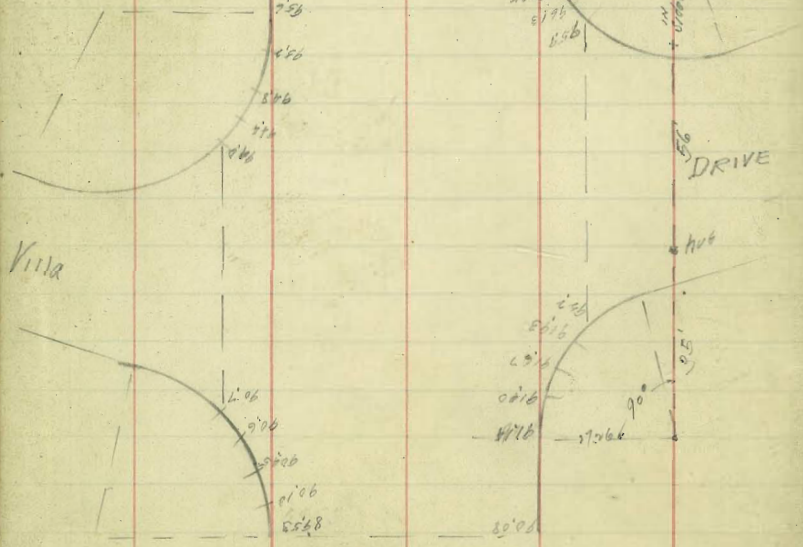
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Recorder 1460



1281	6.01	542	1281	6.01	542
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50.78

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32  
13

26.17  
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PC

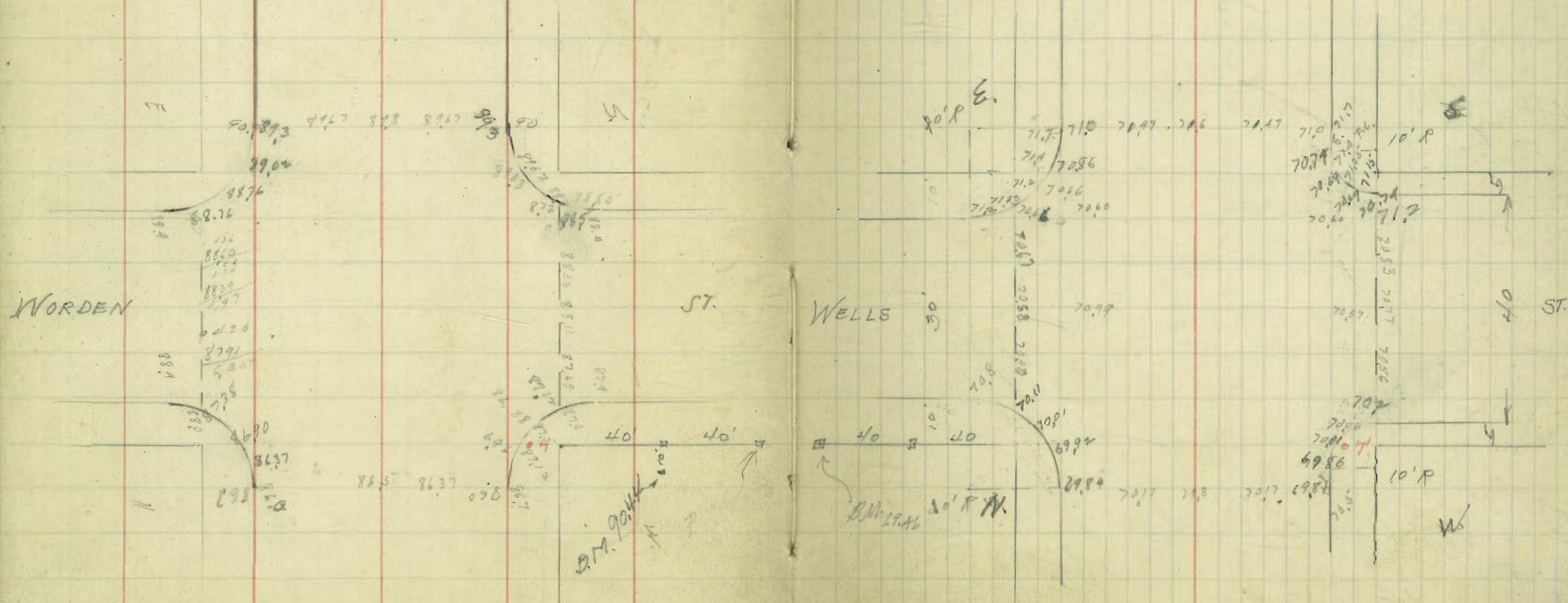
46.5  
76.4

B.M. 9109

XP  
LINE

WARRINGTON

VT.



VOITHAIRE ST.

7098 7077 7058 7017 6988

6970 6950 6930 6910 6890

6870 6850 6830 6810 6790

6770 6750 6730 6710 6690

6640 6620 6600 6580 6560

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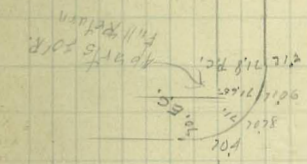
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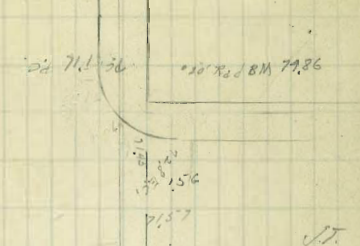
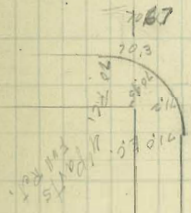
SAN CLEMENTE ST.

Voltaire ST

5



San Clemente



ST.

WABASKA DR.

C.S.  
Def. 5'00" 14  
9' 13" 20  
8' 18" 43  
8' 24" 02  
10' 31" 12  
Ch. 10.00

No. 35

30' C.S.R.

Catalina

Bldg

74.86  
6.88  
75.74





VOITARO UT

	S. Cb.		N. Cb.	
0700 = RC Reton N.	77.5	0700 = RC Ret	78.5	
0760.7 = End of Cb. Existing	77.0	1750.82	75.0	Δ E.L. Mendocino
1718.3 = W.L. Mendocino	75.36			
1750 = C Mendocino	74.30	1767.36	74.46	
2701.2	72.75	2718.46	72.77	
2752.40 = E.L. Mendocino Brk.	71.7	2769.66	71.08	B
1.	69.5	3723.06	69.31	B
2 ① 534	67.80	3776.46	67.54	
3.	66.10	4729.86	65.77	
4765.9 Brk	64.40	4783.76	64.0	Brk
4775.9 Brk	63.7	5713.26	63.0	Brk
5708.36 Brk	63.4	5725.72	62.8	Brk
5758.36 Brk	62.4	5775.72	61.9	Brk
5708.36 Brk	62.0	6725.72	61.3	Brk W. Catalina
6733.8 W.L. Catalina	61.9			

Mendocino E.Cb.

0700 712.	75.5	75.1
0720	76.8	76.2
0740	77.5	76.9
0760	77.7	77.1
0780 = E.C.	77.5	76.95
17106	78.35	
77200 = Δ End of Existing Cb.	75.2	

75.09  
6.2  
11.5  
6.7  
75.09  
2.2  
77.89  
11.2  
25.68  
3.8  
49.8  
12.44

N. 81.82 81.82  
77.5 77.5 75.0 7

S.	81.82	81.82	75.26	74.3	72.7	71.2	69.5	67.8	66.1
	77.0	77.1	61.5	7.5	7.1	10.6	7.9	9.2	11.3
	4.82	4.82	2.9	4.3	8.2	10.2	8.5	10.0	11.7
	2.186	4.10	+3.6	+3.2	+0.9	+0.9	-1.5	-1.4	-1.4

69.5	9.3	9.3	9.3	9.3	9.31
61.4	63.7	63.4	62.7	62.0	61.9
4.9	5.6	5.9	4.7	7.3	7.46
5.0	3.8	6.0	3.8	6.8	7.28
-1.1	-1.2	-1.1	+1.6	+1.0	+1.8

75.09 2M.  
7.01  
82.10  
5.25  
75

42.00  
4.20  
47.80  
3 23.3  
3 5.4  
3 20.3  
3 1.8  
4.12  
63.14

75.09  
1.25  
76.34

81.82	77.5	77.0	77.7	77.5	76.95
6.3	5.0	4.3	4.1	4.3	5.9
5.1	4.3	6.0	5.2	5.9	5.1
+1.2	-1.3	-1.7	-1.1	-1.1	-0.7

Voltaire VT

	66	66
EL Catalina Blvd	64.40	61.80
	63.10	62.74
	64.1	63.68
	64.9	64.62
	65.8	65.56
	66.7	66.50
	67.6	67.44
	68.5	68.38
	69.4	69.32
	70.3	70.26
WL	71.20	71.20
EL "	71.70	71.70
0+71 = P.C. Abbotts	72.0	72.0
1+01 = WL "	72.20	72.20
1+20	72.10	72.10
+80.6 EL "	71.42	71.42
2+00	70.77	70.77
3+40 PVC	70.10	70.10
3+70	69.80	69.80
3 = EVC	69.80	69.80
+5.0	70.25	70.25
4 = WL Wells	70.70	70.70
00 EL "	71.50	71.50

72.82  
 12.76  
 60.06  
 60.03  
 60.01  
 60.07  
 59.90  
 69.46  
 1.66  
 71.12  
 12.61  
 59.49  
 2.73  
 61.17  
 0.78  
 60.39  
 11.28  
 71.27  
 0.87  
 70.80  
 6.41  
 77.21  
 10.38  
 66.83  
 5.03  
 72.30  
 7.86  
 64.44  
 62.37  
 .08  
 S.M.R.  
 Voltaire  
 Catalina

8

N.	72.3	72.3	72.3	72.3	72.3	72.3	72.3	72.3	72.3
	61.8	62.7	63.3	64.6	65.6	66.5	67.1	68.1	68.9
	10.5	9.6	8.4	7.7	6.7	5.8	5.8	7.8	8.8
	10.43	13.8	12.5	6.2	5.7	6.0	8.7	7.2	7.2
	+7.87	-4.2	-3.9	+1.0	+1.0	-0.2	+1.1	+1.6	+1.6
S.	72.3	72.3	72.3	72.3	72.3	72.3	72.3	72.3	72.3
	63.2	63.1	64.0	64.9	65.8	66.7	67.6	68.5	68.5
	10.1	9.2	8.3	7.4	6.5	5.6	4.7	8.7	8.7
	10.0	9.0	8.9	8.5	6.3	4.9	0.8	3.3	3.3
	+4.1	+4.2	-0.6	-1.1	+0.2	+0.7	+3.9	+3.4	+3.4
N.	77.2	77.2	77.2	77.2	77.2	77.2	77.2	77.2	77.2
	69.3	70.3	71.2	71.7	72.0	73.2	73.1	73.7	70.1
	7.9	6.9	6.0	5.5	5.2	4.3	-11.3	-10.7	-10.0
	7.0	6.3	5.5	7.0	6.0	4.9	24.6	6.0	3.5
	+0.9	+0.6	+0.6	-1.5	-1.8	-10.7	-16.6	-17.3	-15.1
S.	77.2	77.2	77.2	77.2	77.2	77.2	77.2	77.2	77.2
	69.4	70.3	71.2	71.7	72.0	72.2	72.1	71.7	70.8
	7.8	6.9	6.0	5.5	5.2	5.0	5.1	1.3	-9.6
	+4.0	+3.6	+2.0	+1.3	+2.0	-1.6	-1.1	-2.7	-14.8
N.	60.1	60.1	72.8	72.8					
	64.8	64.8	70.3	70.7					
	-9.7	-9.7	2.5	2.1					
	6.0	-0.9	1.7	3.3					
	-15.7	-10.5	-3.2	3.4					
S.	61.2	61.2	61.2	61.2	71.1				
	71.0	69.7	69.8	70.3	70.7				
	-9.8	-9.6	-8.6	-9.1	.4				
	6.0	5.0	6.7	5.3	9.1				
	-16.0	-14.5	-15.9	-14.4	-8.4				



Voltaire ST

	N/cb	N/cb
2 (N)	83.5	83.5
8 T+69.7 = EVC	84.4	84.4
0	86.77	86.13
3 (V. 49.1) = NL	89.13	88.48
3 = PC Villa Dr. WL	91.5	90.5

Voltaire 9 C  
 116.39  
 123.28  
 130.2  
 110.26.1  
 110.96 T  
 12.71  
 78.25  
 0.56  
 78.81 T  
 12.73  
 86.08 TR  
 0.21  
 86.29  
 12.37  
 73.92  
 0.28  
 74.20  
 86.08 TR  
 0.98  
 87.06  
 11.51  
 75.55  
 0.12  
 75.67

Check e Voltaire 4. Villa Dr. S.E.P. 92.42 = 96.35 Bliss

10

N	90.5	88.5	86.3	86.3	74.2	89.5	84.5
	8.3	10.3	-1	1.9	-9.3	3.1	2.2
		11.7	1.9	5.2	7.1	4.6	6.0
		-1.7	-2.0	-4.0	-16.4	4.5	-3.8
S.	91.5	89.1	86.8	84.7	83.5		
	7.3	7.1	12.0	-8.7	-7.8		
	6.8	2.7	11.9	2.0	3.4		
	4.5	9	+12	-12.7	-17.2		

# Chatsworth St.

166.35T

11

Statistics  
N.1. Measurements.

	E. Cb.	W. Cb.
0+00	160.6	160.1
1.	160.74	160.54
2.	160.99	160.69
3.	161.03	160.83
4.	161.18	160.98
5.	161.32	161.12
6.	161.47	161.27
7.	161.61	161.41
8.	161.75	161.56
9. 1+60	161.9	161.7
1+96	162.28	162.08
2+46	162.81	162.61
2+96	163.39	163.14
3+10.89 - H.V.C.	163.5	163.32
1. (10) 200	163.6	163.4
2.	163.7	163.4
3.	163.6	163.3
4.	163.4	163.1
5.	162.9	162.7
6.	162.5	162.2
7.	161.8	161.5
8.	161.1	160.7
45.68		160.4
9.	160.2	159.8
10 E.V.C.	159.3	158.8

E.	163.5	3.6	3.7	3.6	3.4	3.9	3.5	1.8	1.1	60.2	57.3
	3.75	3.7	2.6	3.7	2.9	3.4	3.8	4.5	5.2	4.1	7.0
	2.0	2.7	2.7	2.0	2.9	2.9	3.4	3.0	3.5	2.9	5.8
	4.3	7.1	4.1	9.	9	7.5	7.7	7.5	7.7	7.2	7.2
W.	163.32	3.4	3.4	3.3	3.1	2.7	2.2	1.5	60.7	57.8	8.8
	2.77	2.85	2.9	2.0	3.2	3.6	1.1				
				2.1	3.0	3.3	2.0				
				1.1	1.2	1.3	1.1				



147.31  
 12.18  
 135.13  
 0.87  
 135.82  
 14.63  
 128.19  
 0.84  
 125.73  
 2.27  
 116.86  
 116.84  
 .02 Error

E 133.61	2.67	1.68	130.72	7.76	8.80	6.80	4.80	2.7	20.6	118.60
13.7	14.7	21.1	5.1	4.1	7.0	9.0	11.0	13.1	15.2	7.13
10.0	12.1	21.0	1.2	0.5	4.6	2.3	1.6	9.8	16.4	2.07
13.7	22.6	22.0	10.7	7.6	7.7	7.7	7.7	7.7	7.7	7.7

E.Cb                      W.Cb

25.	133.61	133.24
26.	132.89	132.31
27.	131.68	131.39
28.	130.72	130.45
29.	129.76	129.52
30 = E.C. Brk	128.8	128.6
+ 53	126.8	126.4
+ 06.54 Brk	124.8	123.8 = P.C. W. Ret.
122.7		
120.6		
+ 46.54 = St. Valtairc	118.6	



69.46 B.M. Wells Treat  
 2.70  
 72.16  
 11.23  
 60.93  
 67.83

Culvert #1

Fl. at existing Culvert 46.6  
 Fl. in let 47.7

8.12  
 7.02  
 5.95  
 1.97

46.6  
 8.24  
 54.44  
 17.70  
 6.94  
 5.84  
 1.3

72.16  
 69.9  
 2.26  
 8.39  
 13

14 39 20  
 34 11 20 30  
 140  
 128  
 12

Curb Inlet #3 119' W. of Wells St

Cb. Grade 69.9  
 Flowline box 57

10' E. Stake

72.16 72.16  
 69.9 57  
 2.26 15.16  
 11.78 11.78  
 -9.52 +3.38

10' W. Stake

67.85 67.85  
 69.9 57  
 -2.05 10.85  
 5.37 5.37  
 -7.42 +5.18

Curbinlet #4

Cb. Grade 69.9  
 Flowline Box 55.0

10' E Stake

72.16 72.16  
 69.9 55  
 2.26 17.16  
 8.44 8.44  
 -6.18 +8.72

10' W. Stake

72.6 17.16  
 80.4 8.04  
 -5.78 +9.12

9.91  
 9.12  
 19.03  
 55  
 74.03  
 55  
 18.03

160' E. of Warrington  
 Curb Inlet #1 (North Side) Top Cb. 81.9 Flowline 60.0

9240 E.M. 1/4  
 Drive  
 96.28  
 17.88  
 83.60 T.P.  
 0.34  
 83.74  
 12.30  
 71.51  
 5.72  
 77.26  
 79.71  
 68.50  
 11.69  
 80.24  
 7.78  
 72.46  
 12.29  
 85.45  
 6.71  
 84.74  
 10.32  
 95.06  
 91.05  
 91.05 E.M. Warrington

Curb Inlet #2 (South) 81.9 65.0

9240 E.M. 1/4  
 Drive  
 96.28  
 17.88  
 83.60 T.P.  
 0.34  
 83.74  
 12.30  
 71.51  
 5.72  
 77.26  
 79.71  
 68.50  
 11.69  
 80.24  
 7.78  
 72.46  
 12.29  
 85.45  
 6.71  
 84.74  
 10.32  
 95.06  
 91.05  
 91.05 E.M. Warrington

Culvert #2 intake outlet  
 20.5' (N. of N. line) 53.6 53.0

Culvert #6 57.1 56.5  
 20.5' (S. of S. line)

10' E. End Stake  
 83.74 83.74  
 51.7 60.  
 2.04 53.74  
 12.40 12.40  
 -10.36 +11.54

10' W. End Stake  
 77.26 77.26  
 81.7 60.  
 -7.84 19.76  
 8.71 8.71  
 -10.35 +8.55

8' End Stake  
 80.24 80.24  
 81.7 45  
 -1.66 75.74  
 8.33 8.33  
 -10.87 +5.71

W. End Stake  
 80.24 80.24  
 81.7 65  
 -1.66 15.24  
 7.78 7.78  
 -9.44 +7.46

53.6  
 53.7  
 57.17  
 55.17  
 5.82  
 73.8

56.5  
 56.5  
 65.76  
 57.1  
 8.66  
 8.66  
 74.88

Chatsworth Blvd  
Sewer Construction

150.55  
15.66  
169.21

97.98  
17.82  
85.16  
1.99  
87.15  
0.92  
86.23  
11.42  
77.65

F.L.  
151.40  
154.40  
154.45  
154.88  
155.21  
155.54  
155.88

WL Chatsworth Plugend + 8.30  
0 + 19.37 = M.H.#1 + 8.58

19 + 09.37 = DE  
5' S of Voltaire at Warrington 95.00  
@ Warrington = M.H.#3 74.90

9074 9074 9074 9074 9074  
75.15 75.02 75.88 76.25 76.62  
15.37 15.27 14.86 14.77 14.12  
6.25 6.29 6.28 6.31 7.23  
9.34 9.29 9.28 9.31 9.39

7 = 3 + 67 = DE  
@ Warrington = M.H.#3 95.42  
75.15 74.63 78.11 79.60  
20.37 8.77 17.81 15.79  
10.86 8.35 7.78 6.16  
4.41 4.43 4.53 4.56

6 (47.83)  
85.02 90.42 84.05  
81.08 83.56 77.37  
17.37 2.36 11.37  
92.14 9.22 5.17  
78.15 4.77 7.57

b = 2 + 87 = DE

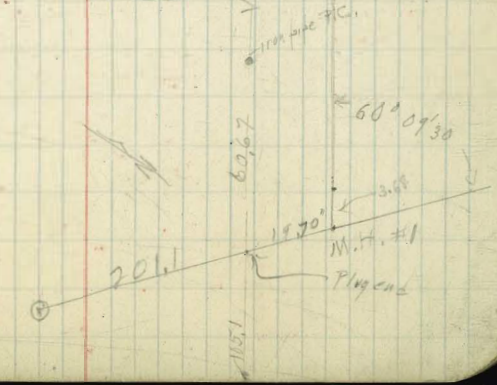
5/2/29 14000  
Flood  
Colpoul  
P20-10

5441	5453	5488	5521	5554	5585
13.50	75.64	78.33	79.00	79.87	79.83
5.09	8.18	4.84	5.23	5.80	6.33
79.73	81.48	8.49	7.78	8.87	6.00
87.15	87.15	75.52	75.88	76.25	76.62
73.08	12.0	11.58	11.27	10.95	10.73
2.23	8.54	5.83	4.57	4.53	4.37
21.75	48.34	16.10	12.10	10.57	10.09
76.63	78.11	79.60	81.08	82.56	84.05
21.35	19.77	18.38	16.90	15.59	13.98
15.92	8.07	6.10	4.57	3.57	3.70
48.45	40.40	12.28	12.38	12.00	10.23
84.66	84.57	84.36	84.36	84.36	84.36
12.97	13.81	13.29	14.14	14.14	14.14
5.42	4.57	3.78	4.57	4.57	4.57
77.57	78.41	79.51	80.61	81.71	82.81

SEBR  
96.22 Voltaire  
0.25 Villa Drive  
96.87  
17.21  
84.26  
6.43  
90.74

Sewer in Voltaire & Villa Drive

NL Voltaire 84.66  
M.H.#2 84.57  
SL Voltaire 84.36



Water Line Voltaire St

97.98  
 12  
 3.599  
 2.64  
 85.62

	K.L.
100' E of EL Wells = 00	79.0
+50	75.5
1	78.0
+50	80.5
2 = WL Worden	83.0
+int 2 "	84.8
+50 EL "	85.6
+50	86.7
3 10	87.2
+35	87.3
5 +50	87.4
+35	86.8
4 +10	86.4
+30	84.4
5 +50 = WL Warrington	82.4

73.0	75.5	78.0	80.5	83.0	84.8	85.6	86.7	87.2	87.3
15.5	15.1	10.8	17.5	15.9	14.2	12.8	12.3	11.8	11.7
72.5	9.3	4.8	2.7	6.3	5.2	4.4	3.5	5.2	3.2
13.0	77.6	76.1	77.2	78.9	79.0	77.7	78.8	78.6	78.0
87.2	84.8	86.4	84.4	82.4					
11.8	12.2	12.6	14.6	16.6					
3.9	4.6	5.4	7.8	13.4					
47.9	77.2	77.2	74.8	73.2					

WORDEN ST See Worden Profile  
BORROW

10' V	87.4	87.4
34' Voltare	87.4	88.4
50' S Voltare	87.4	86.3
100' "	87.9	83.7
150' S	80.3	81.1
200' S = NL Udal	77.8	78.5

R.P. 15' E+W of NL Hubs

St. Voltare Warrington, Borrow, Voltare to Udal

0400	W	E
0410	86.7	85.9
490	87.3	86.7
450	87.9	87.5
470	88.4	88.1
490	88.7	88.6
410	89.0	88.9
430	89.0	89.2
450	88.9	89.3
470	88.6	89.2
494	88.4	89.0
N NL Udal	88.0	88.9

R.P. 15' E+W on NL Udal ST

See Warrington profile

90.93  
10.01  
100.94  
12.50  
88.44  
90.64

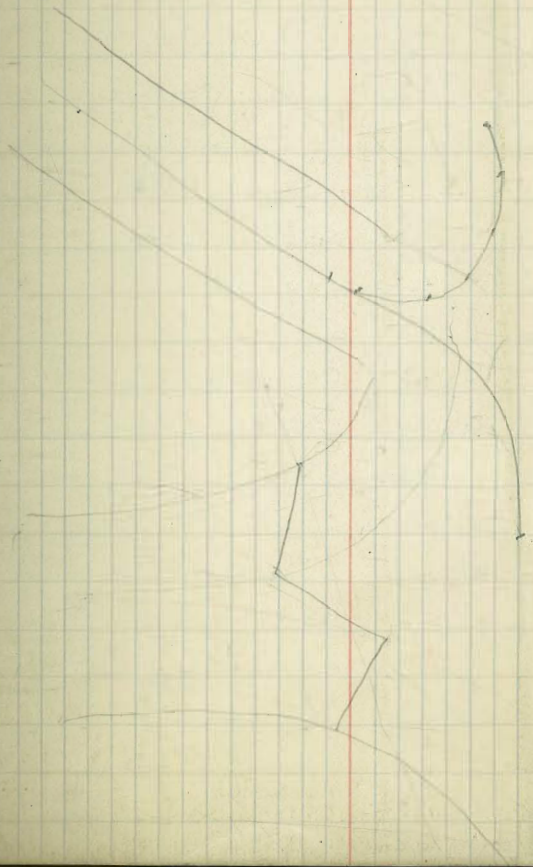
41.09  
7.94  
99.03

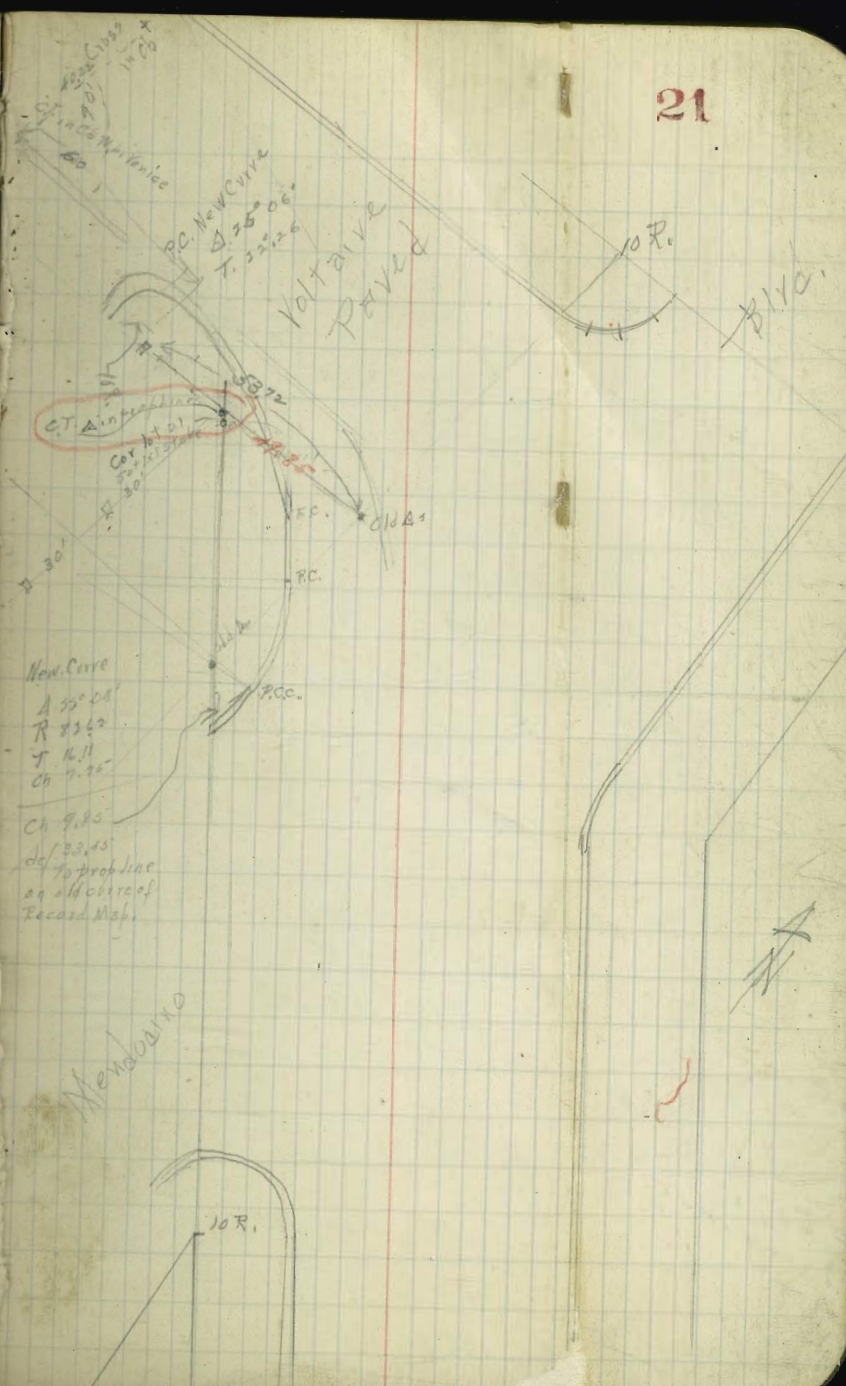
W	87.4	87.9	80.3	77.8				
	17.5	18.0	10.3	15.8				
	2.7	1.0	7.0	10.6				
	+7.8	+6.2	+3.3	+4.2				
E	86.3	83.7	81.1	78.5				
	14.6	17.4	9.4	12.1				
	1.5	7.2	3.3	8.3				
	+13.1	+10.0	+6.7	+3.8				
W	86.7	87.3	87.9	88.4	88.7	89.0	89.0	88.9
	14.3	11.7	11.1	10.6	10.3	10.0	10.1	10.1
	3.0	3.4	3.4	3.1	3.0	2.9	2.7	2.5
	+7.3	+8.3	+7.7	+7.5	+7.3	+7.1	+6.9	+6.2
E	85.9	86.7	87.5	88.1	88.6	88.9	89.0	89.3
	13.4	14.3	14.8	10.9	10.4	10.1	9.8	9.7
	4.4	4.2	5.0	4.8	4.9	5.9	3.7	3.9
	+7.6	+7.1	+6.8	+6.1	+5.5	+6.2	+6.1	+5.5
W	88.6	88.4	88.0					
	10.4	10.0	11.0					
	4.0	6.1	6.4					
	+6.0	+4.7	+4.5					
E	89.4	89.0	88.9					
	9.8	10.0	10.1					
	4.4	3.8	6.1					
	+5.4	+4.2	+4.0					

Warrington Borrow Voltair to Whittier

	E.L.	W.L.	
N.L. Voltairc	85.2	85.9	91.09 5.65
+ 10	85.0	85.5	96.74 12.76 83.98
+ 30	83.75	84.0	0.27 84.65
+ 40	82.0	82.0	11.98 72.77
+ 50	71.0	71.25	0.85 73.62
+ 70 = St. Whittier	60.0	60.5	

E 25.2	96.7 85.8 11.7 5.8 +5.9	96.7 83.7 13.0 6.2 +6.8	96.7 82.1 14.7 11.7 +3.0	84.65 71.1 13.6 8.5 +3.1	73.6 60.0 13.6 15.8 -2.2
W. 85.9	96.7 85.5 11.2 2.0 +8.7	96.7 84.1 12.7 3.6 +9.1	96.7 82.1 14.7 6.7 +8.0	84.6 71.3 13.3 3.1 +10.2	84.6 60.5 14.1 12.5 +1.6





Grading Harris, Cont.  
 Alley 1 Palm Heights

	W Side		E Side	
0+00 = N. Douglass St.	271.20	5.12 5.18 1.92	271.60	
0+10	271.6	1.67 +0.05		4.12
+20	272.00	1.82 1.88	272.2	3.10 +1.97
+30	272.6	1.72 3.04 +1.15	272.8	3.52 +1.22
+40	273.0	1.33 1.33 -1.23	273.2	3.12 +1.05
+50	273.1	3.22 0.22 1.30	273.8	3.12 +1.17
+60	273.0	1.33 1.33 +1.20	273.2	3.12 +1.22
+70	272.8	3.52 3.52 +1.05	273.0	3.12 +1.17
+80	272.6	3.72 3.72 +1.14	272.8	3.52 3.52 +1.40
+90			272.8	3.52 3.52
		N Side		
0+00 = N. Douglass St.	272.6	2.75 New stake 4.14 5.23 1.93 4.13	272.6	2.50 3.21 7.27
+15	269.8	5.10 7.05 +1.94	269.8	5.30 +1.04
+25	268.7	5.71 7.10 +1.39	268.7	5.60 +1.55
+35	267.8	7.20 8.59 +1.39	267.8	7.30 8.50
+45	267.10	1.37 0.37 +1.00	267.1	7.82 +1.32
+55	266.7	1.72 2.22 +1.15	266.7	7.40 11.31
+65	266.45	2.22 2.22 +1.17	266.45	7.00 11.00
+75	266.40	3.07 10.56 -2.49	266.40	10.44 -3.42
+85	266.53	1.84 10.15 -1.07	266.53	6.64 10.15
+95	6.66	4.51 8.56 7.65	6.66	5.51 +1.97
	6.79	6.38 5.33 +1.06	6.79	6.38 +1.73
	6.92	2.25 4.21 +1.44	6.92	4.21 +1.97
	267.05	6.12 4.20 +1.22	267.05	6.12 5.12 +1.00

S.W.B.P. Douglas St. Harris

370.53
5.77
271.37
3.12
272.90
2.20
273.10
1.08
225.02
3.45
248.47
2.46
266.07
7.10
223.17
6.70
227.17
1.45
249.13
6.94
247.99
268.25

272.6	269.8	268.7	268.8
5.23	8.03	7.13	10.03
4.25	6.97	8.40	9.56
7.28	11.24	4.68	-1.57
247.1	266.9	266.85	266.8
10.73	10.73	4.70	4.75
8.73	13.96		4.90
22.00	-8.03		5.57
			-6.7
266.6	4.77	4.92	7.05
4.95	4.76	4.63	4.50
4.29	4.10	3.84	3.50
4.64	+1.66	+7.7	+1.00

268.25 N.W. N.W. Br. St. & Douglas St. Harris

1465  
 8288  
 24788

Grades Changed to Meet New Culvert Location

	W Side		N Side
1+00	267.15		267.15
1+35	266.9	1.96 1.40 2.01	266.9
1+45	266.85	3.32 1.00	266.85
1+65	266.8	2.06 4.91 2.85	266.8
2+06.44	266.65	2.21 2.87 -1.14	266.65
2+21.34	266.6		266.6
			2.21 5.84 -3.63



6.7+1352	267.18	5.99 5.50 +1.46	267.18	5.99 5.50 +1.46
1+55.1 = Wly End.	267.30	5.97 5.43 +1.44	267.30	5.97 5.43 +1.44

### Colvert #1

S. Line  
N. Line  
C. Basin

*Changed by  
Survey 8/5/29*

262	5.97
260.8	5.50
266	5.97
	5.43
	+1.19

### Colvert #1 New Line Grade

0+00 = Top Grating	266.3	5.54 5.50 +1.00
Flow Line	263.3	5.54 5.50 +1.00
0+50 = Brk	258	10.36 11.35 +1.00
1+00	256.5	13.36 11.35 +2.00
1+30 = S. Washington = A	255.66	5.50 5.50 +2.11
1+49 = Connection to East	255.5	9.66 8.40 +1.00

N.W. 2nd Washington

Br. P. 264.47

17
264.66
5.76
258.90
10.00
268.90
12.86
281.76
252.47

4.18	3.61	320	3.08	312	263
3.12		418		823	215
7.30		748		233	481
3.65		371		8	260
3.49	294	260	245	251	343
2.51		345		260	446
5.147		608		5.14	789
2.99		301		2155	394
3.91	3.54	390	3.54	3.08	
3.50	2.46	342	3.42		
7.41	7.00	6.94	6.91		
3.90		3.44	3.44		







Froude St. Grades, Cont.

	E.Cb.		W.Cb.	
0+00 = N.A. Capella	76.64	13.25 13.25 2.33 2.33 10.00 10.00 +2.33	75.67	5.97 5.97 5.97 1.4 1.4 7.1 10.9 10.0 7.7 13.5 13.2 7.13
+50	74.12	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	73.15	10.9 10.0 7.7 13.5 13.2 7.13
1+	71.6	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	70.62	10.9 10.0 7.7 13.5 13.2 7.13
+50	69.06	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	68.09	10.9 10.0 7.7 13.5 13.2 7.13
2	66.54	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	65.56	10.9 10.0 7.7 13.5 13.2 7.13
+50	64.02	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	63.03	10.9 10.0 7.7 13.5 13.2 7.13
3+00 = S.L. Brighton	61.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	60.5	10.9 10.0 7.7 13.5 13.2 7.13
0+00 = N.A. "	60.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	59.5	10.9 10.0 7.7 13.5 13.2 7.13
1	58.25	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	57.25	10.9 10.0 7.7 13.5 13.2 7.13
+50	56.0	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	55.0	10.9 10.0 7.7 13.5 13.2 7.13
2	53.70	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	52.70	10.9 10.0 7.7 13.5 13.2 7.13
2+15 = S.L. Long Branch	51.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	50.5	10.9 10.0 7.7 13.5 13.2 7.13
0+00 = N.A. "	50.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	49.5	10.9 10.0 7.7 13.5 13.2 7.13
11	49.27	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	48.27	10.9 10.0 7.7 13.5 13.2 7.13
+50	47.25	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	47.25	10.9 10.0 7.7 13.5 13.2 7.13
	45.62	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	47.62	10.9 10.0 7.7 13.5 13.2 7.13
2+15 = S.L. Mill	48.0	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	49.0	10.9 10.0 7.7 13.5 13.2 7.13
0+00 = N.A. "	48.0	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	49.0	10.9 10.0 7.7 13.5 13.2 7.13
11	47.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	46.63	10.9 10.0 7.7 13.5 13.2 7.13
+50	47.	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	46.25	10.9 10.0 7.7 13.5 13.2 7.13
	46.5	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	45.87	10.9 10.0 7.7 13.5 13.2 7.13
1974 Ten E 202.58 on N	46.0	10.00 10.00 10.00 10.00 10.00 10.00 +2.33	45.5	10.9 10.0 7.7 13.5 13.2 7.13

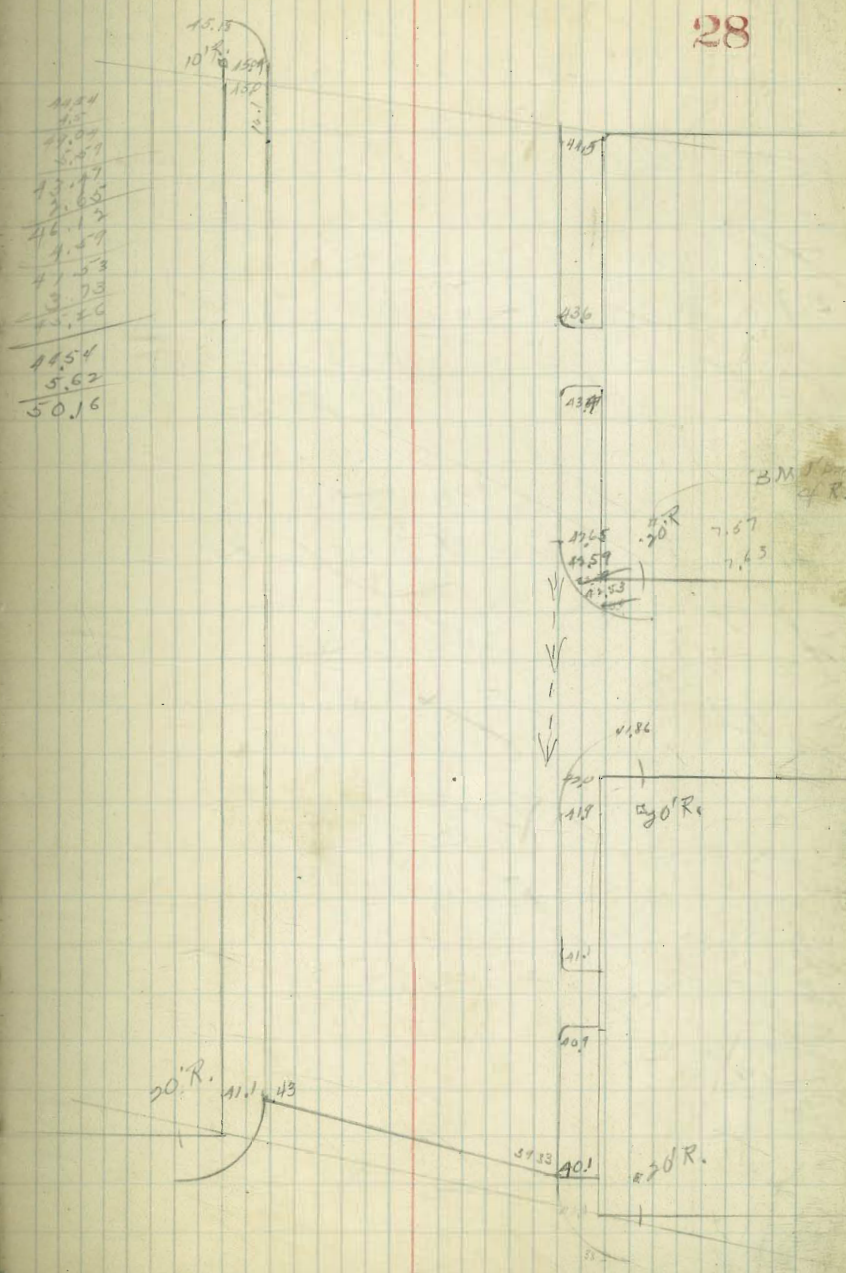
79.0  
 7.36  
 86.36

11.77 R.M. To N.W. of S.W.  
 Brighton

11.77 R.M. To N.W. of S.W.  
 Brighton

Fraude St. Grades, Cont.

	E. Cb.		W. Cb.
0+00 = Mt. Voltaire	15.0	$\frac{4.04}{4.04}$	44.5
1-53735 on R.	14.6	4.44	44.
4-54735 E	14.2	4.54	43.5
24 21.1 = St. Louis on E	13.8	5.00	43.
2+15 = St. Louis on W	13.4	5.72	42.5
150+00+100 = Mt. W	13.0	$\frac{3.12}{3.12}$	42.0
1-55135 on R.	12.5	3.62	41.5
1-55235 on R.	11.	4.12	41.
14 20 = St. Louis on E	11.5	4.62	40.5
14 15 = St. Louis on W	11.0	4.76	40.0



Sewer in Froude St  
Coronado to Santa Cruz

29

0+00 = N.L. Coronado	172.3	8.78	Connect to
+ 55	170.1	2.14	Existing Sewer
1+10 = Brk	167.9	2.18	
+ 70	160.96	6.97	172.77
2+30	154.03	6.93	4.31
+ 90	147.09	6.93	191.08
3+50 = M.H.#1	140.16	6.93	172.65
30' E of M.H.#1 plug	143.4	3.27	12.873
30' W of M.H.#1 plug	137.61	5.79	0.46

8/19/30  
 Flood  
 Station  
 Kauer

# Catch Basin at Sutter & 9bis

B.M.N.K.B.P.	0.50	262.50		262.00	Sutter & Sackdaw
	4.04	254.94	11.60	250.90	

W. End Catch Basin		250.90		7.29	
		247.67		7.36	
E " " "		247.67		7.29	
				7.18	
				-21	

Flow Line &		254.90		11.94	
		243.0			

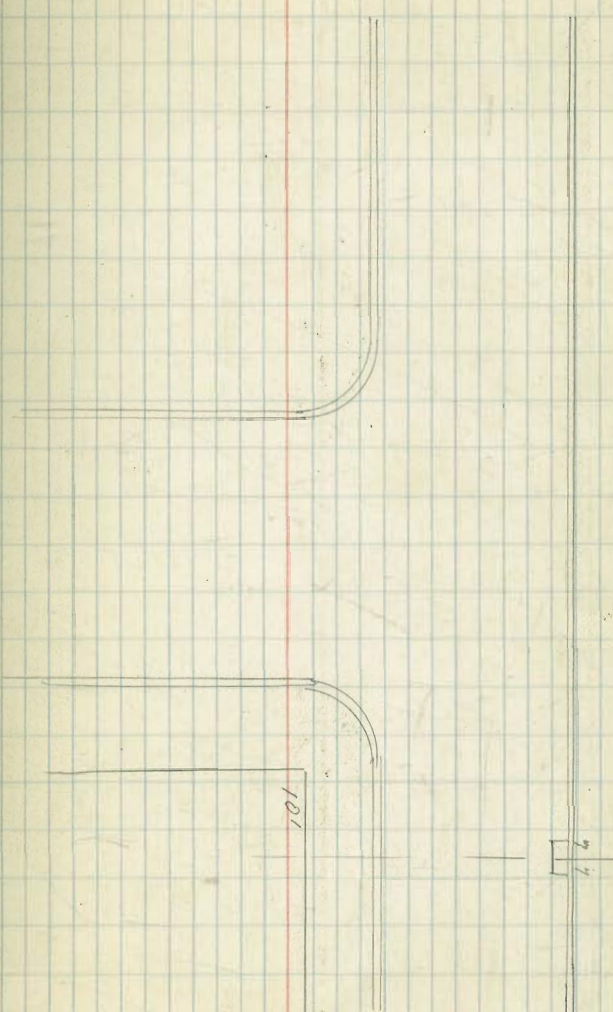
W End Flow		248.33		11.61	
------------	--	--------	--	-------	--

E End "		243.33		11.41	
---------	--	--------	--	-------	--

	208	
	571	
	39	

	254.94	
	6.08	
	248.86	









MADE  
FIELD  
TRIP  
RECORD  
RABBIT

Alley Paving  
BIT 7 Watkins & Middle  
" B Burlington

1200  
31<sup>st</sup> June, 19

	N	N	
			287.07
			7.40
E.L. 31 <sup>st</sup> = 0+00	290.71	290.97	288.47
			8.28
0+40 = PVC	291.40	291.70	291.23
			3.98
0+60	291.70	291.95	298.03
			6.33
0+80 = PVC	291.90	292.10	298.22
			2.30
1+20	292.07	292.27	295.33
			3.26
1+60	292.23	292.43	297.27
			3.96
2+00 = BREAK	292.40	292.60	293.71
			5.62
2+40	292.52	292.72	297.53
2+80	292.65	292.85	
3+20	292.77	292.97	
3+60 = BREAK	292.90	293.10	
4+00	293.45	293.65	
4+40 = BREAK	294.0	294.20	
4+70	294.15	294.40	
5+00 = BREAK	294.30	294.60	
5+50	294.65	294.97	
6	295.0	295.35	
+1.71 = WL 3 <sup>rd</sup> and 4 <sup>th</sup>	295.15	295.54	

WATSON CUTTON  
7/6/29

paving

	S	N	S	N	S	N
	90.71	91.40	91.70	91.90	92.07	92.23
	92.40	92.60	92.77	92.90	93.45	94.0
	92.72	92.85	92.97	93.10	93.65	94.20
	94.15	94.30	94.65	95.0	95.15	95.54
	94.40	94.60	94.97	95.35	95.54	95.94

7/12/07  
 Blue  
 Source  
 Kernmen  
 Xaniff

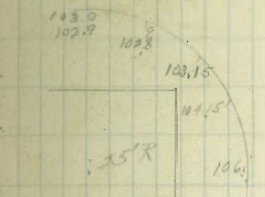
Quince St. Farming  
 Columbia to India

W. C. B. 11

	S. Cb.		N. Cb.
0-06 = W. Columbia			
0+00 = W. C.	150.8		152.2
0+14 = T. C. P. 100	148.0		148.5
1	137.5		137.67
+	127.		127.25
17.4	116.5		116.22
P+035 = T. C. P. 100	106.0		106.0
2-10.0	104.9		104.60
-16.5	93.5		93.8

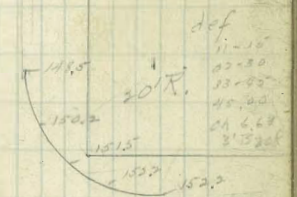
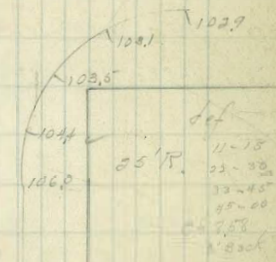
Handwritten notes and calculations in the lower section of the left page, including various numbers and small diagrams.

India St.  
 566 face .33 cr.



SE India

- 103.00
- 111.23
- 114.43
- 118.03
- 120.03
- 126.43
- 130.03
- 132.33
- 137.30
- 142.33
- 147.33
- 152.33
- 157.33
- 162.33
- 167.33
- 172.33
- 177.33
- 182.33
- 187.33
- 192.33
- 197.33
- 202.33



Columbia St.

9/14/29  
 Flood  
 Repair  
 Paving  
 Work

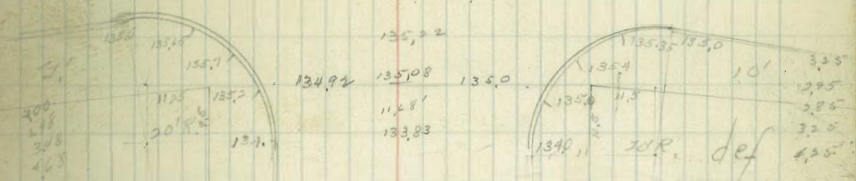
Oline St. Paving

Water & Sewer

	N. Cb.	S. Cb.
	135.5	135.0
	2.0	2.0
	2.0	2.0
	2.0	2.0
0700 = W. Columbia	135.3	135.2
0710 = W. Columbia	135.3	135.2
	124.35	124.35
	118.5	118.5
	110.75	110.75
1140 = W. Columbia	105.0	105.0
1145 = W. Columbia	101.7	101.7

100.96  
 6.12  
 107.08

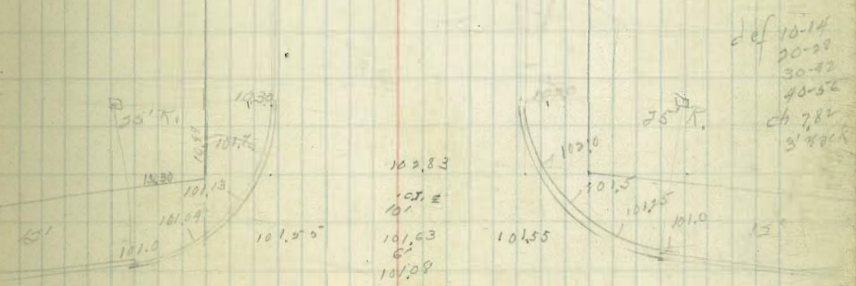
S.F. Ind. 2  
 100.76  
 12.84  
 113.80  
 0.153  
 118.29  
 12.33  
 135.40  
 0.12  
 135.46  
 12.11  
 157.60  
 157.85  
 155.77  
 12.03  
 172.82  
 4.22  
 145.57  
 143.56 N. Columbia  
 101.00



35

Columbia St.

50' face 33' cr



493  
 623  
 686  
 689  
 693

- 2.07

def 10-14  
 20-22  
 30-42  
 40-52  
 ch 782  
 5' 80' K

697  
 493  
 593  
 643  
 688  
 693

N.W. 1/4  
Flood  
Reserve  
Kanary

Alley Paving Bk 14 Fairmont  
& Bk 3 Mountain View  
20' wide

B.C. 1911

B.M. N.W. 1/4  
174 N.W. 1/4

N.W. 1/4 34307

36

0+00 = S.L. University

E. Side

W. Side

+ 40

342.95

7.61  
1.62  
1.01  
3.65  
2.60  
1.50

341.62

4.51  
4.51

342.64

3.49  
2.41  
1.00 Nail in

+ 80

343.45

6.80  
1.71  
5.83  
1.59  
1.24

343.66

2.47  
1.47  
1.00 Nail in

+ 20

344.42

5.83  
1.59  
1.24  
5.35  
4.35  
1.00

344.67

5.56  
1.11  
1.21

+ 40 = P.Y.C.

344.9

5.67  
1.25  
-0.10  
5.87  
4.65  
-0.11

345.2

5.05  
1.10 Nail in  
5.34  
1.77  
-0.05

+ 60

345.3

345.6

5.19  
5.28  
-0.09

+ 80 = E.Y.C.

345.5

345.8

5.13  
0.12  
+0.24

+ 20

345.68

345.78

5.06  
5.07  
-0.52  
4.70

+ 40

346.05

346.35

5.88  
-0.58

+ 60

346.41

346.71

4.33  
2.83  
-0.10

+ 20

346.78

347.08

3.97  
3.25  
+0.72

+ 60

347.14

347.44

6.56 Nail in  
5.60  
+1.26 Fence

+ 20

347.50

347.80

6.49 Nail in  
5.84  
+0.65 Fence

+ 40

347.87

348.17

6.13  
5.10  
+1.03

+ 60

348.23

348.53

5.76  
5.23  
+0.53

+ 20 = T.Y.C.

348.6

348.9

5.76  
5.63  
+0.13

+ 40

348.6

348.9

6.06  
5.04  
+1.02

+ 60

348.3

348.6

6.76  
6.88  
+0.18  
5.05

+ 80

347.6

347.9

6400 = E.Y.C. - No. 11 - 11/21/2011

346.7

343.108  
343.07 B.M. N.W. 1/4 Hand 7/11/11  
-0.01 5/1/11

11/16/29  
Flood  
Rear  
K 2899

Narragansett Ave  
Paving 53 Rd.  
Office  
50c.

	N. Cut.	S. Cut.
0+00 = W.L. Santa Barbara	217.0	217.9
0+60 = E.L. " " = 0+00	217.2	219.2
30	217.6	219.62
60	218.0	220.04
90	218.4	220.47
1+30	218.8	220.89
50	219.2	221.31
80	219.6	221.73
2+10	220.0	222.15
40	220.4	222.58
2+70 = P.V.C.	220.8	223.0
90	221.0	223.2
3+10	221.0	223.2
1+30	220.9	222.9
2+50	220.6	222.5
2+70	220.1	221.9
2+90 = B.V.C.	219.4	221.1
4+25	219.1	219.45
4+60 = P.V.C.	216.8	217.2
80	215.4	216.2
5+00 = E.V.C.	214.1	214.9
+ 30 = E.V.C.	213.3	213.06
+ 45.0	210.9	211.93
+ 66.8	207.1	207.86
6+00 = W.L. Venice	204.5	204.5

219.67 S.W. B.P. Narragansett 44 Santa Barbara  
 237.20  
 9.66  
 217.54  
 0.68  
 218.22  
 12.44  
 205.78  
 0.76  
 206.53  
 1.24  
 205.29 N.W. B.P. Venice & Narr.  
 1.84  
 206.53  
 12.10  
 194.43  
 0.35  
 194.78  
 12.19  
 182.59  
 0.37  
 182.96  
 10.19  
 172.77  
 0.62  
 173.39  
 12.88  
 160.51  
 0.12  
 160.63  
 0.15  
 157.48 N.E. B.P. Catalina & Narr.

219.67  
 6.01  
 204.66  
 2.83  
 202.83  
 1.22  
 204.09  
 13.70  
 211.39  
 0.28  
 211.67  
 5.52  
 206.15  
 0.78  
 205.94  
 12.91  
 193.03  
 3.23  
 190.54  
 12.46  
 183.03  
 2.185  
 180.93  
 11.26  
 174.47  
 2.25  
 177.42

# Narragansett Ave

10' Rd  
7' Cb face  
4' Cr.

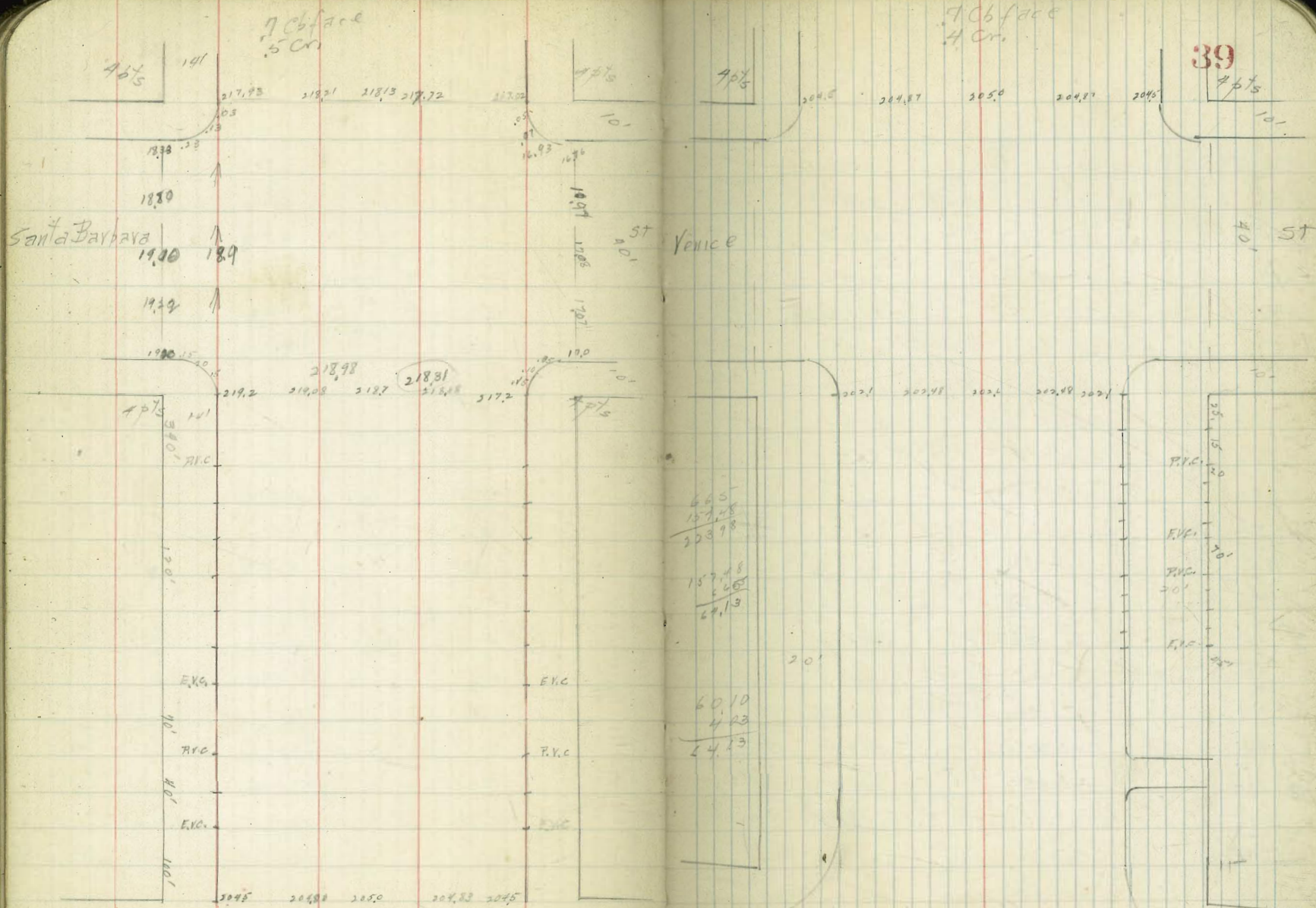
N. Gut      S. Gut.

0+00 = E.Venice	202.1	202.1
+35	201.1	201.1
+40 = P.V.C.	200.8 <sup>5</sup>	200.5
60	199.3 <sup>7</sup>	199.2
70	197.4 <sup>2</sup>	197.4
1+00	195.7 <sup>3</sup>	195.3
1+30 = E.V.C.	192.7	192.8
+55	188.05	188.1
1+90 = P.V.C.	183.4	183.4
3+10	181.0	181.0
+30	178.9	179.0
+50	177.4	177.4
2+70 E.V.C.	176.2	176.5
+92.5	175.25	175.55
3+15 = P.V.C.	174.7	174.6 <sup>9X</sup>
35	173.2	173.7
55	172.1	172.7
75	170.9	171.4
95	169.3	170.0
1+15	167.5	168.2
1+35 = E.V.C.	165.8	166.3

92.205  
+ 3.35  
= 95.555

5.22  
157.48  
162.70





Flood  
Tribice  
Kandy  
11/18/29

Alley 156 U. H. Carroll  
20' wide  
D sewer lat. 70's of St. Howard on W.

	East		West
0+00 = N.L. Polk	366.65	5.66 5.58 366.35	366.25
+ 20	367.0	5.33 +2.00 Nail 1.98 1.97	367.02
+ 81 = P.K.C.	367.35	4.93 +1.71 4.93	367.4
+ 100	367.5	4.95 -1.12 4.73 4.95	367.2
+ 20	367.6	4.73 -1.12 4.95	367.65
+ 40	367.6	4.73 -1.12 4.95	367.65
+ 60	367.5	4.73 -1.12 4.95	367.6
+ 80	367.4	4.73 -1.12 4.95	367.5
+ 100	367.2	4.73 -1.12 4.95	367.25
+ 20	366.9	4.73 -1.12 4.95	367.0
+ 40 = E.K.C.	366.6	4.73 -1.12 4.95	366.7
+ 85	365.87	4.73 -1.12 4.95	365.95
+ 30 = 45	365.15	4.73 -1.12 4.95	365.20
+ 75	364.39	4.73 -1.12 4.95	364.45
+ 20 = P.K.C.	363.65	4.73 -1.12 4.95	363.7
+ 40	363.40	4.73 -1.12 4.95	363.40
+ 60 = E.K.C.	363.25	4.73 -1.12 4.95	363.25
+ 85 = 3/	363.08	4.73 -1.12 4.95	363.13
+ 50 = 45	362.91	4.73 -1.12 4.95	363.01
+ 95 = B.K.	362.75	4.73 -1.12 4.95	362.9
+ 100	362.60	4.73 -1.12 4.95	362.9

S.E. B.P. OHIO & FOLK  
365.96  
5.95  
371.91

S.E. B.P. OHIO & FOLK 366.47  
S.E. B.P. " " Howard 361.01

40

364.47 S.E. OHIO & HOWARD  
3.46  
367.93  
4.60  
363.33  
6.00  
369.33  
3.93  
366.45  
5.17  
371.62  
3.33  
369.29  
4.04  
373.33

F1000  
 12/15/09

Paving  
 Alley 18 Fairmount Dock  
 0.03

	East.	<sup>332</sup> 312	West.	
0+00 = N2. Univ	346.81	4.37 2.87	347.15	4.88 6.38 +0.02
+10	346.8	6.38 5.74 +0.64	346.8	6.38 5.33 +3.00
+40	6.66	6.62 5.74 +0.78	6.66	6.52 6.105 +0.47
+70	6.51	6.67 5.50 +1.17	6.51	6.67 6.00 +0.67
1+00	6.37	6.81 6.23 +0.58	6.37	6.81 6.86 +1.95
+30	6.23	5.32 5.28 +0.06	6.23	5.22 3.28 +1.44
+60	6.08	5.37 5.61 -0.24	6.08	5.37 4.32 +0.78
+90	5.94	5.51 5.74 -0.23	5.94	5.51 4.23 +0.87
2+20 = Bk	346.8	5.65 5.63 +0.02	345.8	5.65 5.08 +0.57
+40	345.86	5.59 5.19 +0.40	345.86	5.59 4.94 +0.65
+70	5.95	5.30 5.30 +0.00	5.95	5.50 4.66 +0.84
3+0	6.04	5.41 5.04 +0.37	6.04	5.41 4.60 -1.19
+30	6.14	5.31 5.29 -0.02	6.14	5.31 5.26 -0.20
+60	6.23	5.02 5.65 -0.63	6.23	4.31 4.27 -0.04
+90	6.32	4.22 4.73 -0.51	6.32	4.22 2.32 -1.90
4+20	6.41	4.13 5.45 -1.32	6.41	4.13 5.02 -0.89
+50	6.51	4.03 3.88 +0.20	6.51	4.03 3.43 -0.40
+80 = Bk	346.6	3.94 3.89 +0.06	346.6	3.94 3.60 +0.34
5+00 = Bk	346.7	3.94 3.76 +0.08	346.7	3.94 3.83 +0.11
+40 = P.V.C.	347.6	6.27 5.85 +0.42	347.6	6.27 1.94 +0.51
+60	347.7	6.17 5.90 +0.27	347.7	6.17 5.90 +0.27
+80	347.5	6.37 4.52 +1.85	347.5	6.37 5.57 +0.80
5+90 <sup>85</sup> = P.V.C. S.A. P.V.S	346.83	7.04 7.01 +0.03	346.96	6.91 6.88 +0.04

3,86  
 3,86  
 1,81  
 41

B.M. N.V.B.P.  
 Manlo & Univ.

343.09 = 343.11 on new plug set	10.09	7.43
353.18	4.81	358.61
344.58	5.01	343.65
347.45	5.74	351.19
347.51	5.03	
347.71	5.00	
347.16	6.16	
348.87		

Storm Drain Alley 18 Fairmount,  
360' of 8" Concrete Sewer pipe

		W.	E.
0+00 = Catch Basin #1		7.75	7.75
2+20 N of N.L. Univ.	343.7	5.08	5.08
		-2.67	+2.12
+30 = Δ in pipe	343.59	7.86	
		4.82	
		3.04	
		9.76	
		5.22	
		2.80	
1 4-17-55	3.42	9.92	
		2.67	
		4.84	
		10.09	
		4.21	
		7.58	
3 -	3.09	10.33	
		5.33	
4 3+21 = Δ Cleanout #1	342.95	7.75	
		10.51	
		6.82	
		7.90	
1) 3-16-53	342.67	10.69	
		5.09	
		7.55	
7	342.49	10.18	
		9.63	
3 3+61 = W.L. Manhole	342.31	7.123	
		10.93	
3 3+76 = Ret on Manhole & Univ	342.26	10.21	
		-0.01	

Sewer Laterals Alley 18 Fairmount

#1 19976 N of Univ on E	340.9	10.55
		5.53
		46.02
#2 19932 N of Univ on E	341.1	10.35
		5.19
		45.17
#3 N of Univ on W	341.81	11.87
		5.19
		76.24
#4 N of Univ on W	342.11	10.07
		5.17
		45.67
#5 29954 N of Univ on E	341.19	10.26
		6.24
		45.57

Shortage of .75 ft partitioned among 24 lots

Water Services Alley 18 Fairmount

1 - 59.90 N of Univ on W	} Shortage of 0.75 ft partitioned to lots
2 - 119.80 " " " E	
3 - 169.80 " " " E	
4 - 219.70 " " " E	
5 - 279.60 " " " W	
6 - 329.60 " " " W	
7 - 20' S of Polk on W	
7 = N.L. Univ on E	

Flood  
 12/18/59  
 12/18/59

1 OCT

Coronado Ave Pmnt  
 Sunset Cliffs Blvd to EBERS

BUNW 97 40  
 Elev 50.06

Sunset Cliffs		20
5002 4854	0.82 506	5075 5110
5002 5000	51.8 516	5120 51.9

106.70  
 6.10  
 114.80  
 127.0  
 5.08

30'

40 01 30  
 89 55  
 179-56 30  
 3 30

104.8  
 104.8  
 50

103.7	10402	103.7	10402
105.13	10413	4.59	10450

Ebers

CORONADO

43

Ebers St

106.70	106.23	106.23	106.23	106.23
--------	--------	--------	--------	--------

107.0	106.93	106.59	106.59	106.59
107.85	107.28			

BMSW  
 Elev 105.40

10

133.5	132.63	132.72	132.42	132.42
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137.5	137.33	138.39	138.25	137.33
-------	--------	--------	--------	--------

169.0	168.33	168.39	168.25	167.33
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172.1	171.43	171.49	171.35	170.43
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174.7	174.03	174.09	173.95	173.03
-------	--------	--------	--------	--------

176.1	176.23	176.26	176.1	175.13
-------	--------	--------	-------	--------

178.0	177.83	177.84	177.65	176.63
-------	--------	--------	--------	--------

178.8	178.13	178.09	178.05	177.03
-------	--------	--------	--------	--------

179.4	179.03	179.44	179.29	178.03
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179.8	179.73	179.76	179.5	178.33
-------	--------	--------	-------	--------

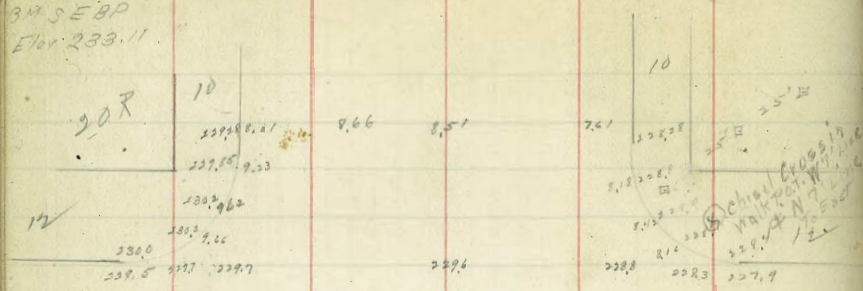
Froude St.

4 pts  
 7876  
 7891  
 7910  
 7930  
 7950  
 500

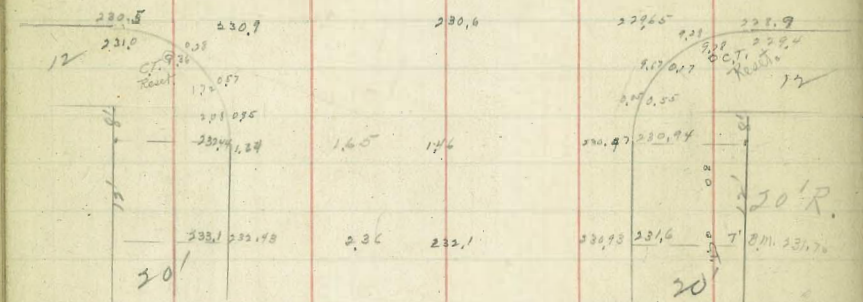


Coronado & Guizot St. Intersection

34 SE 80  
Elev. 233.11



Guizot  
229.88 230.1 230.7 230.2

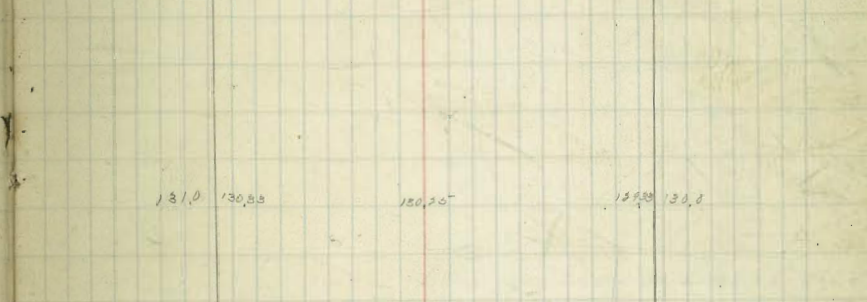
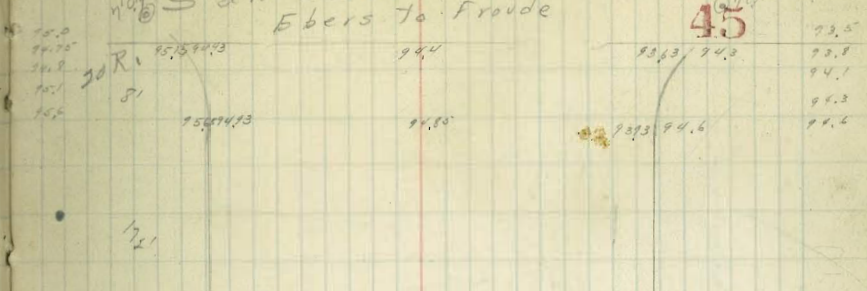


Coronado  
Santa Barbara

78991  
B.M. SIMMONS  
SW. 7 1/4 93.76

Santa Cruz Arc  
Ebers to Froude

45



Froude

- 93.96
- 7.68
- 101.60
- 0.24
- 101.36
- 12.34
- 113.70
- 0.68
- 113.02
- 12.95
- 126.07
- 0.41
- 125.66
- 7.81
- 135.87

- 144.3
- 147.22
- 148.15
- 149.00
- 150.00

- 144.3
- 147.22
- 148.15
- 149.00
- 150.00

Santa Cruz  
 Fronde St  
 BM SW 7' back  
 Elev 149.32

151.0  
 150.1  
 149.6  
 149.2  
 150.0

76.5  
 148.2 148.73  
 148.5  
 149.33 149.0  
 148.5  
 149.25  
 149.33 149.0  
 148.5

373.62

BRK  
 BRK

113.5 172.50  
 173.0  
 173.23 173.0

375.98

300.1  
 0.76  
 Hub road 4/4/30

0.96  
 0.76  
 126.23  
 106.76

50  
 50  
 50  
 2040.203.33  
 203.6  
 203.33 203.33

1001  
 140  
 211.58  
 212.6  
 212.6

Evizot St

Santa Cruz

46

2040.203.33  
 203.6  
 203.33 203.33

149.32  
 8.77  
 158.09  
 1.20  
 156.89  
 12.60  
 149.47  
 1.92  
 167.57  
 12.74  
 180.31  
 3.40  
 177.49  
 11.23  
 189.41  
 0.37  
 187.03  
 11.32  
 200.34  
 0.20  
 197.57  
 12.37  
 112.36

211.33 211.7  
 -0.36  
 212.04  
 -0.16  
 212.20  
 7.04  
 212.14  
 +1.20  
 211.75 212.6

218.0  
 217.33  
 218.12  
 218.12

8.15  
 0.25  
 219.90 - 217.70, 218.6  
 210.70 211.0

218.5  
 218.5  
 218.5



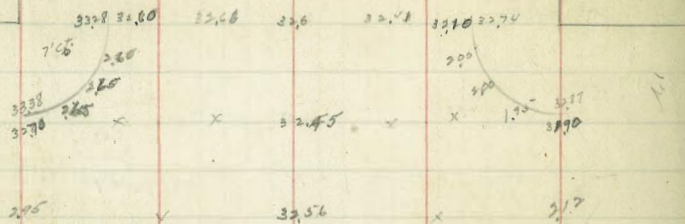


Del Mar & Cable

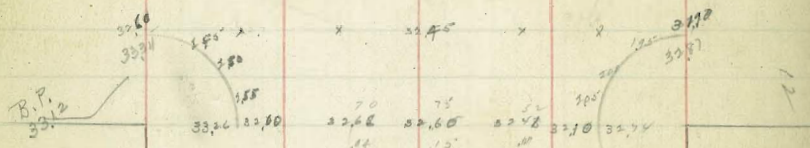
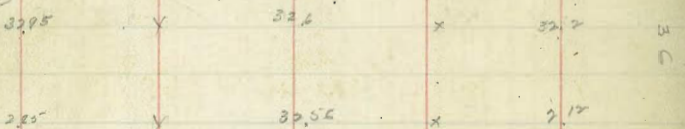
20

40

20



Cable St



Sunset Cliffs Blvd

Del Mar Cable

3326 3350

3240 3274

20'  
100'

20'  
100'



3490 500 530 530 3540

20

20

3570 3570 548 5570 572 3580 3621

100'

Sunset Cliffs

7 MI B.P.  
3619







Orchard 140' Net Cable to Sta East.

40

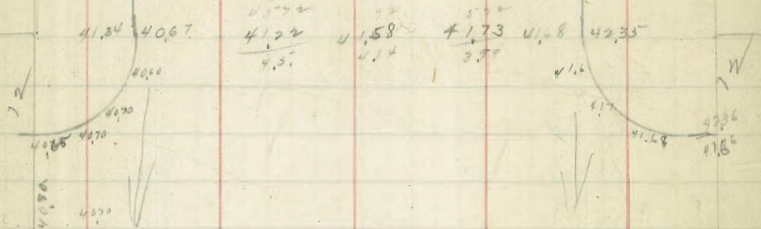
420 45.38 45.71 45.0 45.29 44.63 45.5 40. 44.55 45.24

40.70  
39.20  
42.42  
41.22

40.48  
40.32  
41.2  
40.6

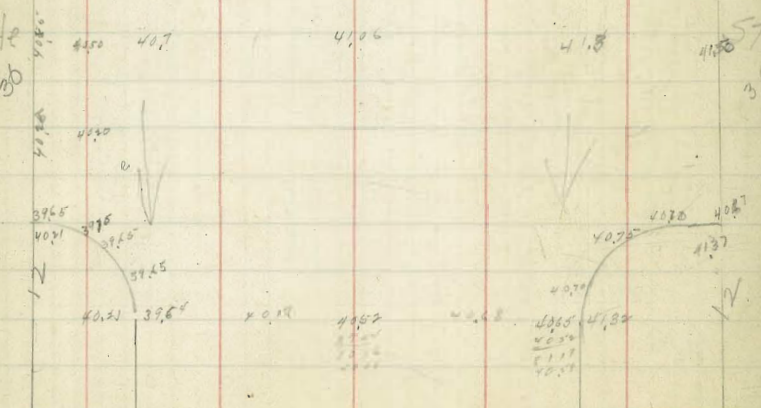
40.52  
40.32  
41.2  
40.6

40.52  
40.32  
41.2  
40.6



45.72 45.72 45.72 45.72 45.72  
41.22 41.58 41.73 41.8 42.35  
4.3 4.4 4.7 4.6

Cable 30



39.6 40.21 39.6 39.6 40.31 39.6  
40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7  
40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7

Orchard cable

52

20 40.1 39.54 40.18 40.52 40.18 40.32 20

29.41 30.22 30.28  
40 29.36 29.25 29.4 29.60 29.72 30.01

Sunset Cliffs

ORCHARD  
Sunset Cliffs

07-7.  
BM NW 7 tack  
Elev 30.21

30.38	29.96	30.71	30.20	31.33	20'
401	30.18		30.87		80'
60'				1.83	32.5
31.5	30.78	31.37	31.75		
401	22.9	31.53	32.09	32.43	33.2
401	33.4	2.78	33.27	3.45	37.3
401	35.1	4.43	34.97	5.20	39.3
40	37.2	6.53	37.07	7.45	39.2
40	39.7	9.03	39.59	9.95	40.7
40	42.9	12.33	42.79	13.15	43.7

49.83  
69.82  
117.83  
59.91  
40.01  
3.2  
36.9

600	9.33	10.01	0.5	0.53	61.5
-----	------	-------	-----	------	------

66.06	20	66.04	5.39	11.07	6.56	67.56	47.56
64.8		81.11				68.1	48.1
67.2		66.613		7.2		68.4	48.4
67.25						68.7	48.7
67.0						69.0	49.0

Ebers

ORCHARD  
Ebers

BM SW 7' c  
Elev 67.53

67.2	67.9	68.3	68.6	68.9	69.2	69.5	70.2	70.0	69.8	69.6
67.16	69.28	69.9		69.6		70.0	70.27	70.6	69.9	69.7
47.33	1.42	72.78	61.63	77.52	82.17	86.10	89.89	92.54	95.29	98.04
114.48	12.58	127.01	135.30	143.51	151.72	160.03	168.34	176.65	184.96	193.27
10.43	92.0	91.33	92.01	2.5	2.83	93.5				

53

50	50	102.1	5.48	132.14	6.25	203	127.7
50 R		127.0	6.33		7.33	203	127.1

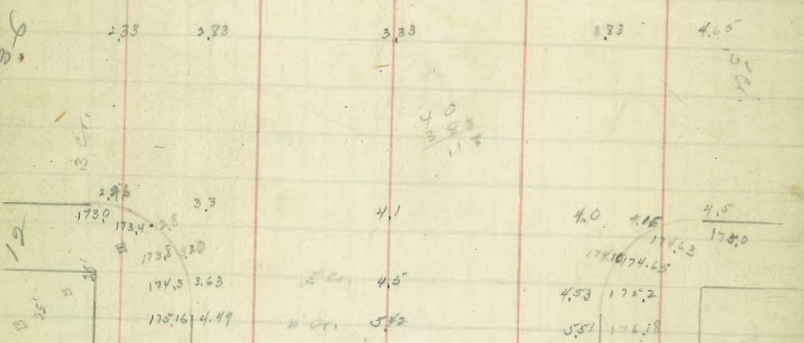
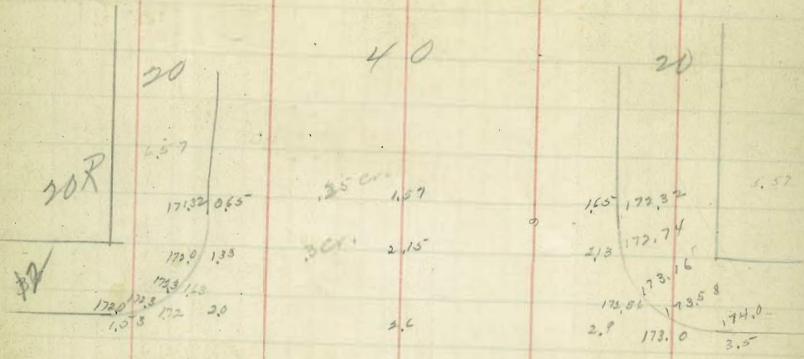
Froude

58  
272  
317  
826  
370





Orchard & Guizat Intersection



200.05  
4.01  
204.04  
12.82  
211.22  
215.44  
212.08  
12.73  
228.21  
1.21  
200.01

12 x 10  
343  
27

Santa Barbara

Orchard & Guizat

BM SE 25' tie  
Elev: 174.65

55

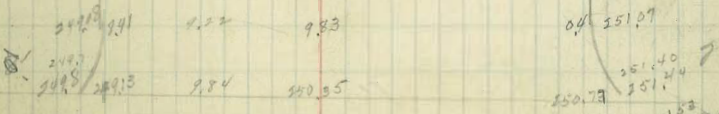


331

224.1	3.48	4.06	4.5	4.73	225.7
20'	206.8	2.18	4.81	7.3	209.3
20'	219.4	2.73	5.41	9.9	220.9
20'	231.6	3.93	6.21	2.43	233.1
20'	243.4	4.93	7.03	4.53	247.7

174.65  
174.28  
174.18  
174.05  
173.87  
173.71  
173.55  
173.39  
173.23  
173.07  
172.91  
172.75  
172.59  
172.43  
172.27  
172.11  
171.95  
171.79  
171.63  
171.47  
171.31  
171.15  
170.99  
170.83  
170.67  
170.51  
170.35  
170.19  
169.03  
168.87  
168.71  
168.55  
168.39  
168.23  
168.07  
167.91  
167.75  
167.59  
167.43  
167.27  
167.11  
166.95  
166.79  
166.63  
166.47  
166.31  
166.15  
165.99  
165.83  
165.67  
165.51  
165.35  
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165.03  
164.87  
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164.23  
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157.03  
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156.55  
156.39  
156.23  
156.07  
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155.11  
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154.79  
154.63  
154.47  
154.31  
154.15  
153.99  
153.83  
153.67  
153.51  
153.35  
153.19  
153.03  
152.87  
152.71  
152.55  
152.39  
152.23  
152.07  
151.91  
151.75  
151.59  
151.43  
151.27  
151.11  
150.95  
150.79  
150.63  
150.47  
150.31  
150.15  
150.00

170



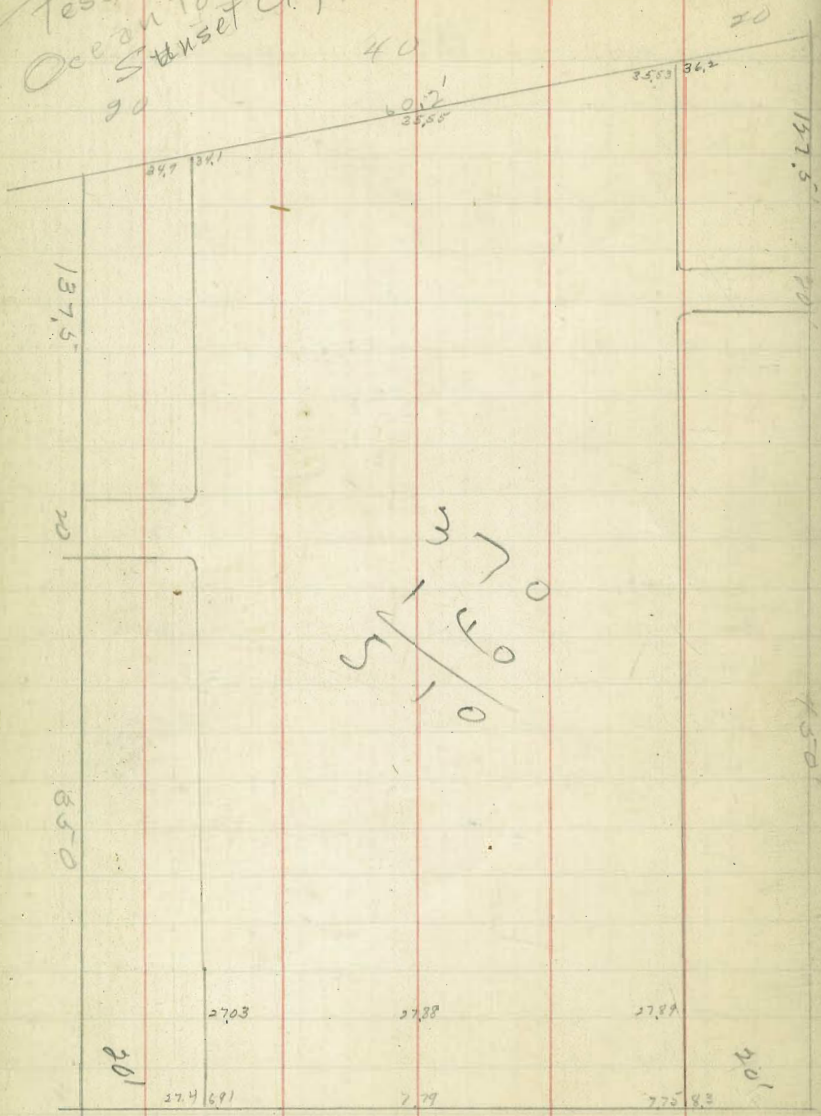
249.9  
249.7  
249.3  
249.0  
248.7

Santa Barbara BM SE BP Elev 250.05

40

10

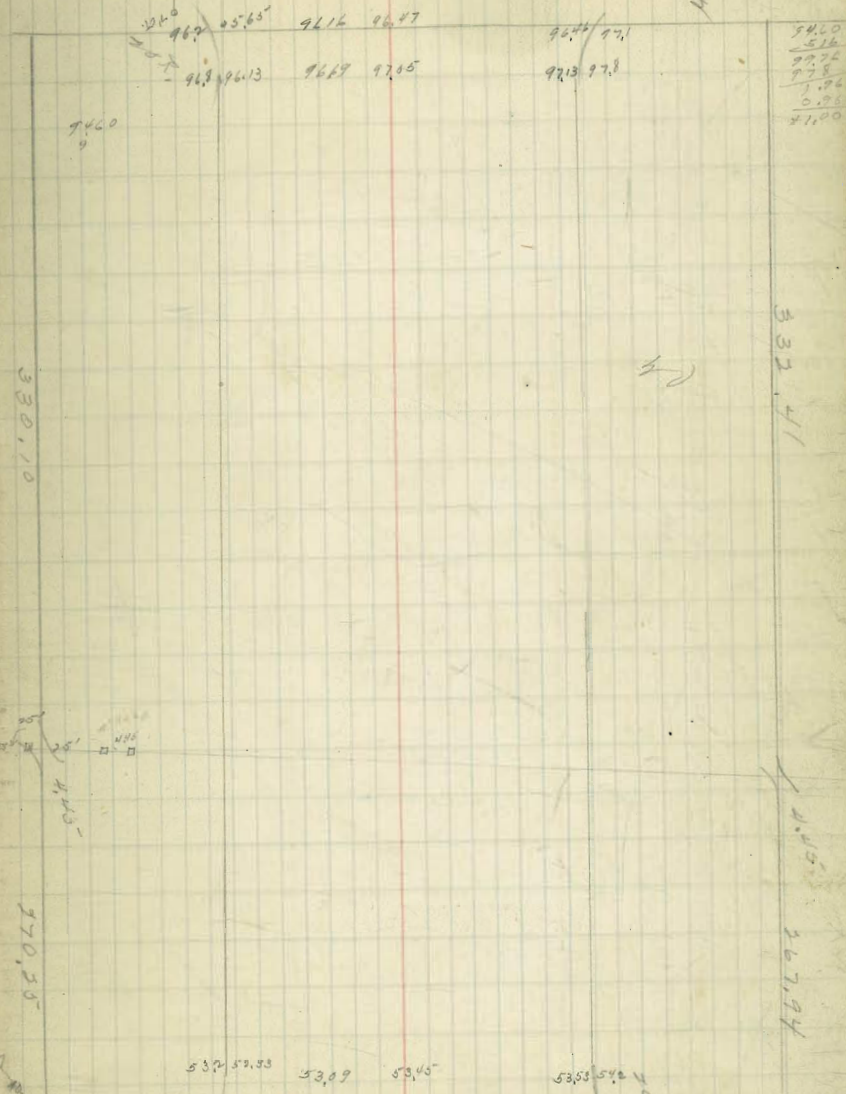
Pescadero  
Ocean to  
Sunset Cliffs



370  
510

Sunset Cliffs  
BM NW BP  
Elev 28.13

Pescadero  
Trough to Guizot  
BM SW BP  
Elev 94.60  
56

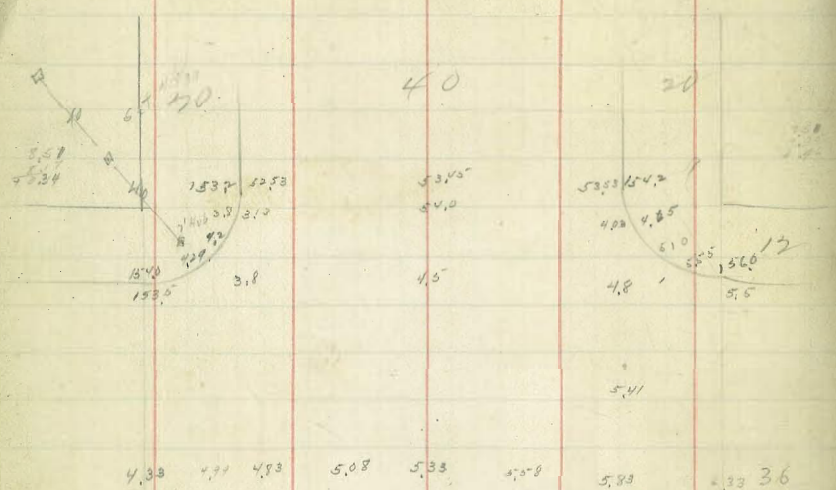


53.0, 50.33, 53.09, 53.45, 53.53, 54.0, 54.0, 54.7

Guizot

54.0  
51.6  
97.76  
97.8  
1.94  
0.18  
41.00

Pescadero & Guizot Intersection



4.33 4.77 4.93 5.08 5.33 5.58 5.83 6.08 6.33 6.58 6.83 7.08 7.33 7.58 7.83 8.08 8.33 8.58 8.83 9.08 9.33 9.58 9.83 10.08 10.33 10.58 10.83 11.08 11.33 11.58 11.83 12.08 12.33 12.58 12.83 13.08 13.33 13.58 13.83 14.08 14.33 14.58 14.83 15.08 15.33 15.58 15.83 16.08 16.33 16.58 16.83 17.08 17.33 17.58 17.83 18.08 18.33 18.58 18.83 19.08 19.33 19.58 19.83 20.08 20.33 20.58 20.83 21.08 21.33 21.58 21.83 22.08 22.33 22.58 22.83 23.08 23.33 23.58 23.83 24.08 24.33 24.58 24.83 25.08 25.33 25.58 25.83 26.08 26.33 26.58 26.83 27.08 27.33 27.58 27.83 28.08 28.33 28.58 28.83 29.08 29.33 29.58 29.83 30.08 30.33 30.58 30.83 31.08 31.33 31.58 31.83 32.08 32.33 32.58 32.83 33.08 33.33 33.58 33.83 34.08 34.33 34.58 34.83 35.08 35.33 35.58 35.83 36.08 36.33 36.58 36.83 37.08 37.33 37.58 37.83 38.08 38.33 38.58 38.83 39.08 39.33 39.58 39.83 40.08 40.33 40.58 40.83 41.08 41.33 41.58 41.83 42.08 42.33 42.58 42.83 43.08 43.33 43.58 43.83 44.08 44.33 44.58 44.83 45.08 45.33 45.58 45.83 46.08 46.33 46.58 46.83 47.08 47.33 47.58 47.83 48.08 48.33 48.58 48.83 49.08 49.33 49.58 49.83 50.08 50.33 50.58 50.83 51.08 51.33 51.58 51.83 52.08 52.33 52.58 52.83 53.08 53.33 53.58 53.83 54.08 54.33 54.58 54.83 55.08 55.33 55.58 55.83 56.08 56.33 56.58 56.83 57.08 57.33 57.58 57.83 58.08 58.33 58.58 58.83 59.08 59.33 59.58 59.83 60.08 60.33 60.58 60.83 61.08 61.33 61.58 61.83 62.08 62.33 62.58 62.83 63.08 63.33 63.58 63.83 64.08 64.33 64.58 64.83 65.08 65.33 65.58 65.83 66.08 66.33 66.58 66.83 67.08 67.33 67.58 67.83 68.08 68.33 68.58 68.83 69.08 69.33 69.58 69.83 70.08 70.33 70.58 70.83 71.08 71.33 71.58 71.83 72.08 72.33 72.58 72.83 73.08 73.33 73.58 73.83 74.08 74.33 74.58 74.83 75.08 75.33 75.58 75.83 76.08 76.33 76.58 76.83 77.08 77.33 77.58 77.83 78.08 78.33 78.58 78.83 79.08 79.33 79.58 79.83 80.08 80.33 80.58 80.83 81.08 81.33 81.58 81.83 82.08 82.33 82.58 82.83 83.08 83.33 83.58 83.83 84.08 84.33 84.58 84.83 85.08 85.33 85.58 85.83 86.08 86.33 86.58 86.83 87.08 87.33 87.58 87.83 88.08 88.33 88.58 88.83 89.08 89.33 89.58 89.83 90.08 90.33 90.58 90.83 91.08 91.33 91.58 91.83 92.08 92.33 92.58 92.83 93.08 93.33 93.58 93.83 94.08 94.33 94.58 94.83 95.08 95.33 95.58 95.83 96.08 96.33 96.58 96.83 97.08 97.33 97.58 97.83 98.08 98.33 98.58 98.83 99.08 99.33 99.58 99.83 100.08 100.33 100.58 100.83 101.08 101.33 101.58 101.83 102.08 102.33 102.58 102.83 103.08 103.33 103.58 103.83 104.08 104.33 104.58 104.83 105.08 105.33 105.58 105.83 106.08 106.33 106.58 106.83 107.08 107.33 107.58 107.83 108.08 108.33 108.58 108.83 109.08 109.33 109.58 109.83 110.08 110.33 110.58 110.83 111.08 111.33 111.58 111.83 112.08 112.33 112.58 112.83 113.08 113.33 113.58 113.83 114.08 114.33 114.58 114.83 115.08 115.33 115.58 115.83 116.08 116.33 116.58 116.83 117.08 117.33 117.58 117.83 118.08 118.33 118.58 118.83 119.08 119.33 119.58 119.83 120.08 120.33 120.58 120.83 121.08 121.33 121.58 121.83 122.08 122.33 122.58 122.83 123.08 123.33 123.58 123.83 124.08 124.33 124.58 124.83 125.08 125.33 125.58 125.83 126.08 126.33 126.58 126.83 127.08 127.33 127.58 127.83 128.08 128.33 128.58 128.83 129.08 129.33 129.58 129.83 130.08 130.33 130.58 130.83 131.08 131.33 131.58 131.83 132.08 132.33 132.58 132.83 133.08 133.33 133.58 133.83 134.08 134.33 134.58 134.83 135.08 135.33 135.58 135.83 136.08 136.33 136.58 136.83 137.08 137.33 137.58 137.83 138.08 138.33 138.58 138.83 139.08 139.33 139.58 139.83 140.08 140.33 140.58 140.83 141.08 141.33 141.58 141.83 142.08 142.33 142.58 142.83 143.08 143.33 143.58 143.83 144.08 144.33 144.58 144.83 145.08 145.33 145.58 145.83 146.08 146.33 146.58 146.83 147.08 147.33 147.58 147.83 148.08 148.33 148.58 148.83 149.08 149.33 149.58 149.83 150.08 150.33 150.58 150.83 151.08 151.33 151.58 151.83 152.08 152.33 152.58 152.83 153.08 153.33 153.58 153.83 154.08 154.33 154.58 154.83 155.08 155.33 155.58 155.83 156.08 156.33 156.58 156.83 157.08 157.33 157.58 157.83 158.08 158.33 158.58 158.83 159.08 159.33 159.58 159.83 160.08 160.33 160.58 160.83 161.08 161.33 161.58 161.83 162.08 162.33 162.58 162.83 163.08 163.33 163.58 163.83 164.08 164.33 164.58 164.83 165.08 165.

From St Roscadero to Coronado  
 BM SWBP  
 Elev. 94.60

From St BM SW Conference  
 Elev 125.05  
 Tully St 132.04 **58**

12

97.1	96.4	94.5	92.3	95.5	96.1
20'	18.2		17.03	17.2	

94.60  
 12.48  
 107.08  
 0.57  
 106.71  
 4.27  
 110.98

110.14

110.0	109.5	109.51	109.33	108.5	109.0
11.38				11.39	11.39

126.21

101	123.0	127.28	127.1	125.21	127.0
-----	-------	--------	-------	--------	-------

Orchard

130.5	0.2	0.27	0.15	9.0	134.5
10'	1.45		1.28		

100'

145.9	1.5	4.87	4.38	3.5	144.0
147.8	2.3	7.29	7.13	4.3	146.8
152.7	3.5	9.47	9.33	3.5	149.0
151.0	1.3	4.27	4.13	0.3	150.0
153.7	2.7	7.67	7.53	1.7	152.2
152.2	2.1	6.77	6.63		

100'

100.0	154.5	9.51	9.33	8.5	157.0
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Orchard  
 for intersection on Sec P. 54

Del Mar  
 for intersection Sec P. 50

Frovde St

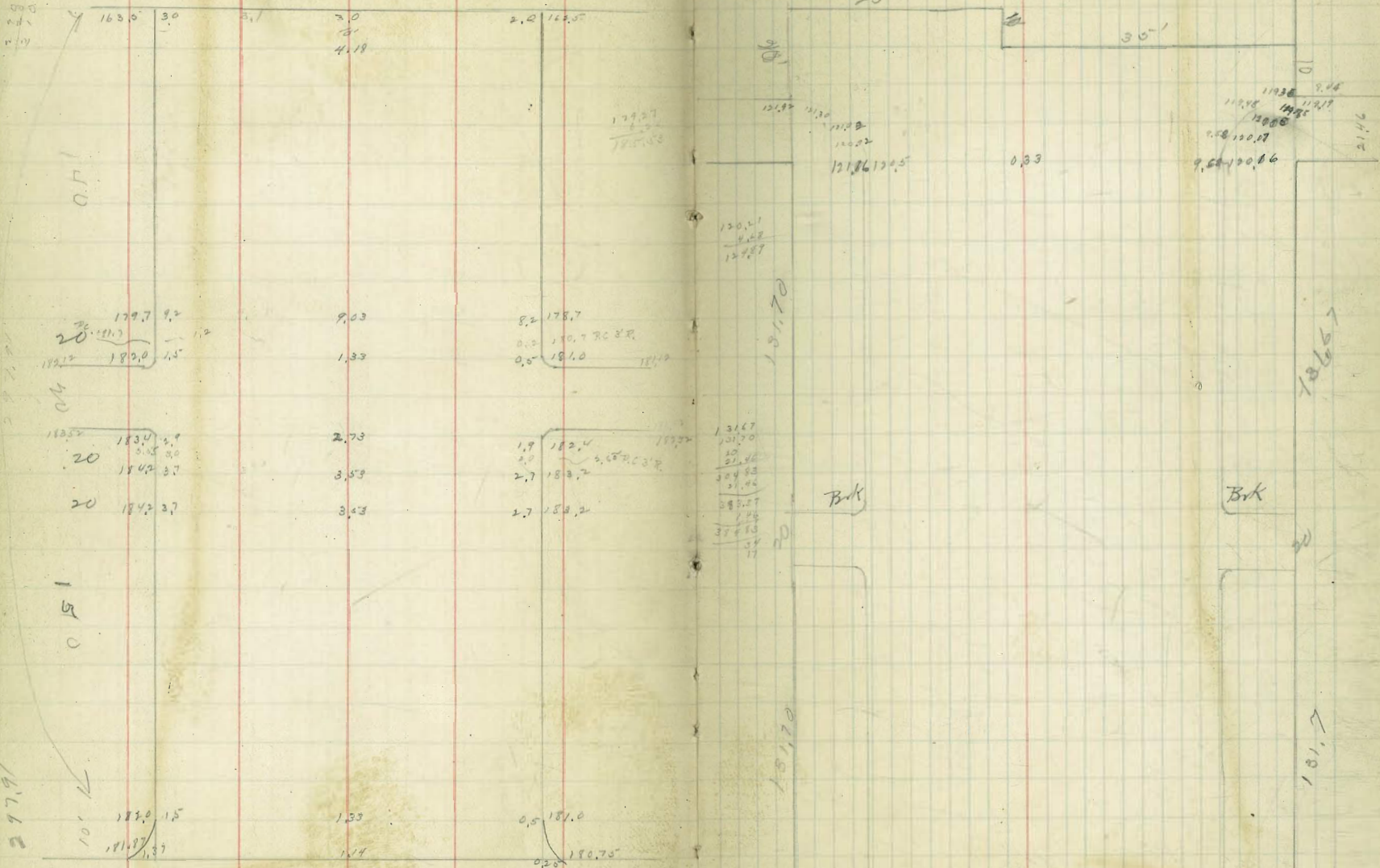
BM SW 25' tie  
Elev 157.51

Del Mar

GUIZOT ST PhLome Ave to Del Monie

PhLome

BM SE 3P  
Elev 120.21 **59**



29791  
20  
2174  
13896

Coronado  
BM 3' tie back NW  
Elev 178.27  
For intersection Sec P 44.

12 133.5' 3.88  
135.0 134.25 134.14  
12  
132.2  
133.2  
133.2  
133.2  
133.2  
133.2

Bermuda

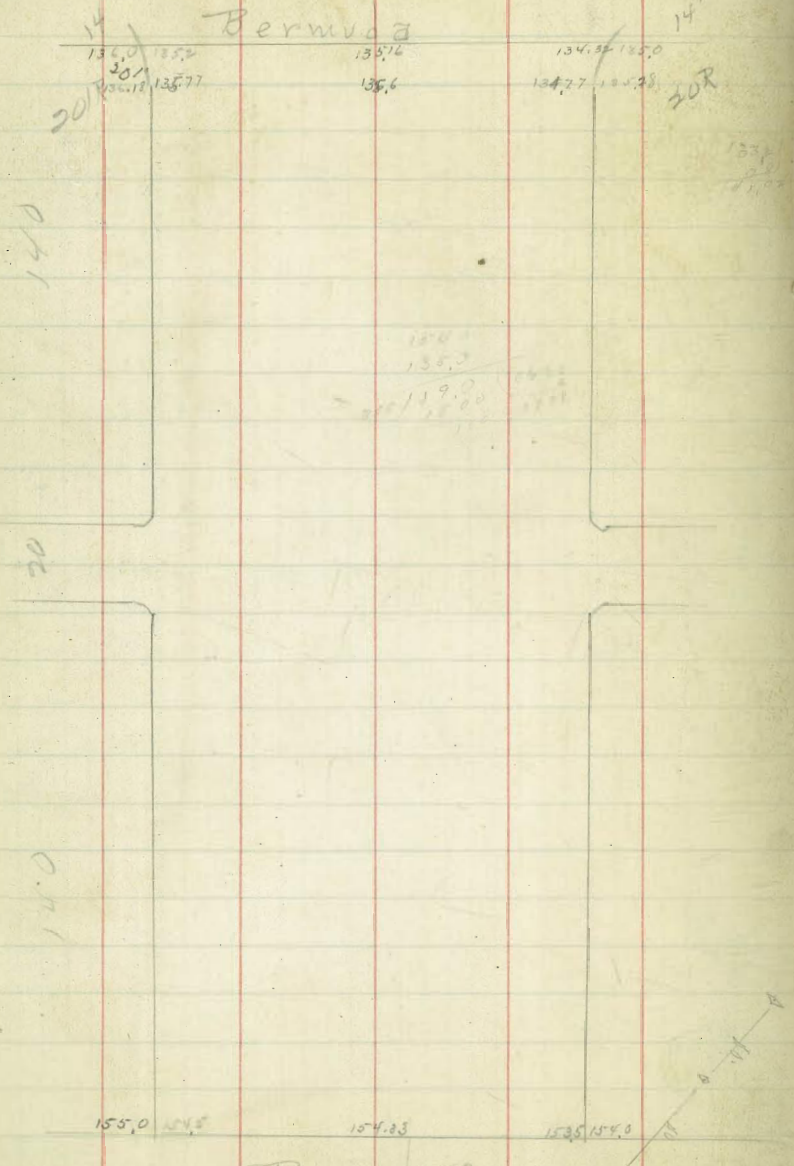
Guizot St B.M. S.W. 8.P  
Elev 133.21

B.M. S.W. 40'tie  
Elev. 151.44

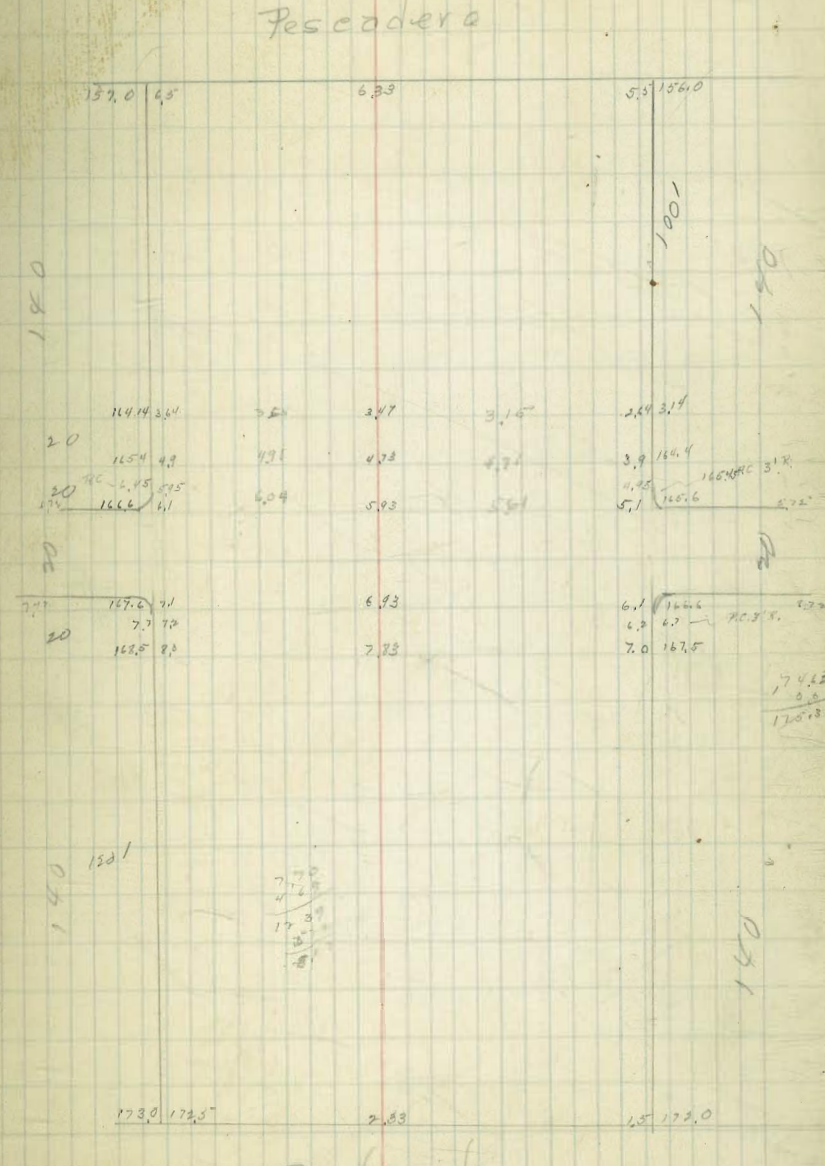
60

Bermuda

Pescadero



Pescadero.  
For Intersection See P. 57



Orchard  
For Intersection See P. 55

Guizot St

BM SE 25' 710  
Elev. 174.65

Orchard  
36

17	175.0	174.5	4.50	3.5	174.0
20	17	17	6.14	5.75	5.21

12

12

204.5 204.25

101 203.28

501 210.0 209.5

501

140

216.4 215.9

220.20  
220.30

219.2 221.2 200.7

201.5 221.5 221.0

222.3 223.4 222.9

37

225.5 225.0

150

228.2 227.8

601

231.0 229.5

Guizot St

BM SE 25' 710  
Elev. 204.09

61

Del Mar  
36

12

204.08

203.21

209.88

215.73

203.2 203.5

204.38

208.5 209.0

214.9 215.4

501

140

471

220.42  
220.52  
9.10

214.7 220.2 217.7

220.0 220.5 220.6

221.4 223.4 222.3

37

224.0 224.0

150

226.8 227.8

601

229.5 228.9

200.12 200.3 199.86 199.43 220 101

201.5 10

200.65

200.58 200.5

Del Mar

For Intersection See P. 57

229.88

230.1

Coronado

For Intersection See P. 45





Sewer lines Coronado, Froude to 310  
Exp (Guzot)

0+00 = N.L. Coronado & Froude	172.3	15.91 8.72 77.12	12.54 7.88 204.66	233.11 12.30 245.41
0+30 = & M.H. # 6 = & Froude & Coronado	173.5	14.71 7.98 11.65	19.47 7.47 12.13	245.73 12.30 258.03
1	176.56	8.59 2.19 72.40	13.29 2.12 +4.91	239.64 12.30 251.94
2	179.62	17.46 11.84 +6.42	10.00 6.36 +2.41	227.57 12.30 245.27
3	182.69	14.40 2.84 78.70	18.30 11.12 +7.14	239.64 12.30 251.94
4	185.75	11.84 2.84 78.70	15.24 6.36 +8.84	203.51 12.30 215.81
5	188.81	20.12 30.63 10.12	12.07 16.71 +10.55	191.43 12.30 203.73
6 3+60 = & M.H. # 5	191.98	17.31 10.12 +10.51	10.35 10.12 +9.18	192.29 12.30 204.59
3+60 = " " " "	193.30	14.20 5.84 +2.76	13.24 8.24 +5.04	182.55 12.30 194.85
1	198.48	7.08 0.80 +2.18	12.84 7.78 +5.06	179.15 12.30 191.45
2	202.53	16.45 2.12 +8.10	19.84 11.72 +5.72	179.15 12.30 191.45
3	208.65	11.35 2.12 +8.10	14.75 5.88 +8.88	179.15 12.30 191.45
4	213.76	17.54 8.92 +5.62	20.84 12.12 +9.84	179.15 12.30 191.45
5	218.88	12.51 6.70 +5.51	15.73 8.11 +7.62	179.15 12.30 191.45
6 6+90 = & M.H. # 4 = & Guzot	224.00	8.20 2.51 +5.76	7.97 7.03 +5.71	179.15 12.30 191.45
1	227.0	10.25 7.14 +5.91	17.85 11.84 +6.14	179.15 12.30 191.45
2	230.0	9.14 2.27 +6.54	11.84 7.78 +4.34	179.15 12.30 191.45
3	233.01	9.14 2.27 +6.54	11.84 7.78 +4.34	179.15 12.30 191.45
4	236.01	9.14 2.27 +6.54	11.84 7.78 +4.34	179.15 12.30 191.45
5	239.01	9.14 2.27 +6.54	11.84 7.78 +4.34	179.15 12.30 191.45
6 10+30 = Dead end.	242.02	6.74 0.80 +3.96	9.34 2.31 +5.94	179.15 12.30 191.45

Sewer line Santa Cruz to Alley 21

M.H. # 15 + 47.5	97.42	7.14 1.84 75.32	11.84 7.78 +4.34
+ 91.50	95.66	8.92 2.35 43.57	11.84 7.78 +4.34
4-47.55 + 142.5	93.90	10.68 4.60 +6.28	11.84 7.78 +4.34
+ 190 = & M.H. # 16	72.14	12.44 2.36 +5.28	11.84 7.78 +4.34

Sewer line Santa Cruz etc.

Alley 21

0+00 = & M.H. # 1 = & Guzot	208.8	15.80 2.12 7.14	177.06 12.30 189.36
1 1.45	208.4	31.25 1.87 7.37	204.65 11.71 216.36
2 0+90 = Bk	198.0	5.30 4.74 1.74	213.97 12.30 226.27
1	193.5	11.84 7.20 +3.57	208.11 12.30 220.41
2 5-47.5	189.12	5.17 2.04 +3.13	203.46 12.30 215.76
3	184.68	8.11 1.41 +6.70	197.22 12.30 209.52
4	180.12	10.50 1.05 -1.07	186.62 12.30 198.92
5 8+30 = & M.H. # 2	175.8	7.52 12.15 11.5	179.15 12.30 191.45
1	170.4	13.12 5.13 +8.99	166.23 12.30 178.53
2	165.0	6.66 12.30 12.30	153.93 12.30 166.23
3	159.8	14.16 10.24 +3.92	143.69 12.30 155.99
4	154.2	17.16 12.30 +4.86	131.39 12.30 143.69
5	148.8	10.65	120.74 12.30 138.44
6 6+30 = E.L. Froude existing	143.4		110.44 12.30 122.74
+ 60 = M.L. Froude			98.14 12.30 110.44
0+00	137.64		85.84 12.30 98.14
1	133.14		73.54 12.30 85.84
2 4-52.55	128.68		61.24 12.30 73.54
3	124.22		48.94 12.30 61.24
4 2+10 = & M.H. # 3	119.76		36.64 12.30 48.94
1	115.64		24.34 12.30 36.64
2 5-45.55	111.53		12.04 12.30 24.34
3	107.41		0.74 12.30 12.04
4	103.30		0.74 12.30 12.04
5 4+52 = & M.H. # 15	99.19		0.74 12.30 12.04

See Opposite Page Bottom 2/50 of 67

Sewer Line Orchard

100.85  
10.95  
136.71  
9.10  
136.71  
12.93

Drop	Station	Reading	Subtraction	Result
0+00 = M.H.# 14 = E. Froude	120.15	17.56	10.16	7.40
"	121.08	14.63	12.11	2.52
"	124.43	13.58	11.06	2.52
"	127.78	9.93	7.41	2.52
"	131.13	17.57	14.94	2.63
"	134.48	10.22	7.59	2.63
"	137.83	10.87	8.24	2.63
"	141.18	11.52	8.89	2.63
3+70 = M.H.# 13	144.54	16.05	13.42	2.63
"	147.89	12.70	10.07	2.63
"	151.24	9.35	6.72	2.63
"	154.59	12.37	9.74	2.63
"	157.94	15.02	12.39	2.63
"	161.29	11.67	9.04	2.63
"	164.64	12.84	10.21	2.63
6+70 = M.H.# 12 = E. Guizo	168.0	9.51	6.88	2.63
"	175.5	11.61	8.98	2.63
"	183.0	12.78	10.15	2.63
"	190.5	9.59	6.96	2.63
"	198.0	13.24	10.61	2.63
"	205.5	6.15	3.52	2.63
9+70 = M.H.# 11	213.00	18.91	16.28	2.63
"	218.72	17.30	14.67	2.63
"	224.44	11.63	9.00	2.63
"	230.16	12.01	9.38	2.63
"	235.88	12.01	9.38	2.63
12+50 = Dead End	240.00	6.29	3.66	2.63

Check for change

Sewer Line Del Mar.

Drop	Station	Reading	Subtraction	Result
0+00 = M.H.# 10 = E. Froude	153.75	15.71	13.18	2.53
"	156.21	13.25	10.72	2.53
"	158.68	10.29	7.76	2.53
"	161.14	11.99	9.46	2.53
"	163.61	10.09	7.56	2.53
"	166.07	17.42	14.89	2.53
"	168.53	10.01	7.48	2.53
3+45 = M.H.# 9	171.0	15.76	13.23	2.53
"	174.74	11.69	9.16	2.53
"	178.49	14.56	12.03	2.53
"	182.24	8.82	6.29	2.53
"	185.98	20.31	17.78	2.53
"	189.73	12.08	9.55	2.53
"	193.47	12.50	9.97	2.53
6+90 = M.H.# 8 = E. Guizo	197.22	17.27	14.74	2.53
"	204.14	10.43	7.90	2.53
"	211.16	15.98	13.45	2.53
"	218.13	9.01	6.48	2.53
"	225.10	13.29	10.76	2.53
"	232.07	16.66	14.13	2.53
10+30 = M.H.# 7	239.04	9.68	7.15	2.53
"	240.0	8.79	6.26	2.53
"	241.78	18.42	15.89	2.53
"	243.97	8.27	5.74	2.53
"	244.45	16.23	13.70	2.53
"	245.94	4.88	2.35	2.53
12+50 = Dead End	245.94	15.45	12.92	2.53

West East

# Sewer Froude St

Connect to Existing MH.

0+00 =	Alley S of Orchard St	99.25	12.07 13.25 13.55 3.29 + 2.11
1		104.17	20.18 9.10 + 10.64 14.96
2	U-47.55	109.7	3.27 11.20 20.31 17.80 + 2.44
3	& Orchard	114.92	14.16 8.22 + 2.94
4	1290 = & MH # 14	120.15	18.01 3.00 + 3.00
5		126.30	13.41 0.12 + 1.07
6	U-502	132.45	17.87 11.66 + 6.20
7		139.6	15.64 6.22 + 7.25
8		147.0	13.31 2.10 + 7.12
9	U-453	149.25	11.74 3.42 + 7.72
10		151.50	8.89 1.67 + 7.22
11	& Del Mar.		
12	5+70 = & MH # 10	153.75	

## Sewer Laterals Froude St.

# 147	135.9	1.61 9.29 + 6.34
# 146	151.2	11.23 6.22 + 7.01
# 145	150.7	11.81 3.26 + 5.49
# 141	131.5	18.96 9.53 + 9.39
# 74	155.1	12.03 1.60 + 11.23

## Sewer Laterals Guisot St

# 144	218.7	6.30 + 4.12
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## Sewer Laterals Pescadero Ave

# 148	29.3	38.31 9.0 + 4.4
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C6=341  
421  
3831

## Sewer Laterals Orchard Ave

# 122	129.0	5.71 2.71 + 2.99
# 123	134.7	14.0 8.21 + 5.20
# 124	141.9	2.77 1.72 + 5.08
# 125	143.6	16.99 12.22 + 2.69
# 126	146.6	13.97 2.25 + 2.24
# 127	148.8	11.72 3.22 + 7.94
# 128	152.3	9.28 1.05 + 5.51
# 129	156.2	12.76 12.44 + 4.32
# 130	160.4	13.52 1.61 + 3.16
# 131	164.16	8.36 2.11 + 5.10
# 132	171.4	15.91 2.37 + 9.12
# 133	178.8	8.81 2.02 + 10.79
# 134	186.4	15.39 7.32 + 6.04
# 135	193.8	17.80 16.22 + 7.25
# 136	201.4	10.55 2.22 + 8.00
# 137	208.7	15.27 17.15 + 6.70
# 138	216.2	7.22 0.51 + 7.25
# 139	223.5	10.57 2.84 + 6.23
# 140	229.2	15.49 11.20 + 6.77
# 141	234.0	15.44 0.55 + 7.44
# 142	238.6	8.27 3.19 + 6.10
Extra # 143	242.5	13.38 2.22 + 2.50

# Sewer Laterals Del Mar Ave

From to Guizot

N	From	To	S.	1903	13.83
# 75	1600	9.46 2.33 7.12	# 119	159.3	13.83 9.87 45.76
# 76	1645	16.45 10.57 5.88	# 118	161.8	11.33 9.12 22.45
# 77	1674	18.54 8.12 10.42	# 117	164.3	19.37 19.37 38.74
# 78	1713	21.69 3.12 18.57	# 116	167.3	16.37 2.24 18.61
# 79	1747	24.81 3.12 21.69	# 115	170.6	13.37 3.00 16.37
# 80	1786	27.93 3.12 24.81	# 114	173.7	9.87 3.00 12.87
# 81	1829	31.05 12.12 18.93	# 113	175.9	13.15 13.15 26.30
# 82	1867	34.17 19.21 14.96	# 112	179.3	15.75 8.22 23.97
# 83	1904	37.29 15.91 21.38	# 111	183.1	17.14 17.14 34.28
# 84	1941	40.41 12.27 28.14	# 110	186.9	12.88 7.13 20.01

Guizot to Santa Cruz Ave

# 85	2010	43.53 14.09 29.44	# 108	199.6	15.49 3.56 18.95
# 86	2071	46.65 20.04 26.61	# 107	205.7	9.39 4.47 13.86
# 87	2118	49.77 15.84 33.93	# 106	211.9	10.33 15.24 25.57
# 88	2166	52.89 21.69 31.20	# 105	218.0	20.37 12.87 33.24
# 89	2226	56.01 17.73 38.28	# 104	224.7	13.69 4.39 18.08
# 90	2310	59.13 13.65 45.48	# 103	231.2	17.53 12.10 29.63
# 91	2370	62.25 11.73 50.52	# 102	237.5	10.23 3.56 13.79
# 92	2427	65.37 14.09 51.28	# 101	245.4	14.50 9.50 24.00
# 93	2474	68.50 10.50 58.00	# 100	249.5	18.42 5.14 23.56
# 94	2501	71.62 7.80 63.82	# 99	251.4	1.50 5.41 6.91
# 95	249.2	74.74 5.10 69.64	# 98	250.1	8.80 3.34 12.14
# 96	242.8	77.86 13.80 64.06	# 97	248.1	11.10 5.14 16.24

# Sewer Laterals Santa Cruz Ave

# 28	108.0	7.24 1.87 5.37	# 7	213.3	21.85 12.80 9.05
# 29	111.1	15.25 8.12 7.13	# 6	217.6	17.35 8.12 9.23
# 30	115.0	11.33 3.72 7.61	# 5	221.6	13.35 1.50 14.85
# 31	119.0	12.87 2.24 10.63	# 4	225.7	9.12 2.12 11.24
# 32	123.5	14.09 1.50 12.59	# 3	229.8	15.69 7.12 8.57
# 33	125.6	12.87 1.50 14.37	# 2	233.9	12.59 2.12 10.47
# 34	128.1	10.37 2.24 12.61	# 1	237.6	7.88 3.56 4.32
# 35	133.3	16.37 7.87 8.50	# 22	177.7	14.03 3.56 10.47
# 36	138.4	14.09 2.24 11.85	# 24	184.7	17.87 7.12 10.75
# 21	145.5	17.44 3.56 13.88	# 26	192.6	19.21 11.24 8.97
# 20	151.7	18.63 1.50 17.13	# 27	204.9	21.69 3.56 18.13
# 19	157.6	25.37 7.87 17.50	# 17	166.7	21.69 3.56 18.13
# 17	166.7	21.69 8.30 13.39	# 16	171.8	21.69 3.56 18.13
# 16	171.8	21.69 3.56 18.13	# 15	174.6	21.69 3.56 18.13
# 14	179.6	24.81 4.17 20.64	# 14	179.6	24.81 4.17 20.64
# 13	183.6	27.93 5.14 22.79	# 13	183.6	27.93 5.14 22.79
# 12	187.6	31.05 6.12 24.93	# 12	187.6	31.05 6.12 24.93
# 11	191.6	34.17 7.13 27.04	# 11	191.6	34.17 7.13 27.04
# 10	195.7	37.29 8.12 29.17	# 10	195.7	37.29 8.12 29.17
# 9	200.7	40.41 9.12 31.29	# 9	200.7	40.41 9.12 31.29
# 8	202.9	43.53 10.10 33.43	# 8	202.9	43.53 10.10 33.43

14932 RMA FIVE  
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 93.95

271927  
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 157.57  
 13.82  
 170.33  
 1.34  
 168.99  
 11.32  
 180.34

Sewer laterals Coronado Ave

1869  
192.69

# 54	177.6	10.61 2.03 +8.58	# 56	179.4	8.51 4.02 +4.49
# 53	179.5	8.71 2.14 +6.57	# 57	182.2	6.01 1.01 +5.00
# 52	184.3	15.65 11.81 +4.84	# 58	185.0	15.00 12.28 +2.72
# 51	186.9	13.35 9.46 +3.89	# 59	187.8	12.80 4.10 +8.70
# 50	189.9	10.30 3.10 +7.20	# 60	190.6	22.00 12.10 +9.90
# 49	194.0	17.41 11.12 +6.29	# 61	196.0	16.41 6.24 +10.17
# 48	195.6	17.01 4.12 +12.89	# 62	201.2	11.41 3.52 +7.89
# 47	201.2	11.41 1.21 +10.20	# 63	205.1	19.88 11.33 +8.55
# 46	205.0	20.09 8.24 +11.85	# 64	209.1	15.98 7.87 +8.11
# 45	209.8	15.22 8.80 +6.42	# 65	213.7	14.38 2.66 +11.72
# 44	213.9	11.18 3.56 +7.62	# 66	218.4	12.06 10.20 +1.86
# 43	218.5	17.96 9.85 +8.11			
# 42	229.1	7.41 1.85 +5.56	# 67	227.3	7.21 5.17 +2.04
# 41	232.2	11.09 0.23 +10.86	# 68	231.5	8.01 0.23 +7.78
# 40	236.1	12.18 6.64 +5.54	# 69	234.2	14.05 8.22 +5.83
# 39	238.9	9.88 3.60 +6.28	# 70	235.2	13.08 1.07 +12.01
# 38	241.7	10.41 3.10 +7.31	# 71	237.8	10.48 2.43 +8.05
# 37	243.2	8.61 1.58 +7.03	# 72	240.5	7.78 0.32 +7.46
			# 73	242.8	9.31 3.02 +6.29

Sewer laterals Cable St

# 149	27.4	10.34 4.22 +6.12	# 152	27.4	8.34 4.22 +4.12
# 150	24.5	13.20 2.22 +10.98	# 153	29.4	8.34 2.88 +5.46
# 151	24.5	13.20 9.41 +3.79			

3812 S. 50th St  
462  
37.74

Sewer line Santa Cruz @ Vizo + East

67  
227.08  
12.87  
209.65  
0.80  
237.85  
6.68  
245.88  
12.16  
239.80  
1.50  
234.88  
11.97  
223.00  
1.07  
224.66

0 + 00 =	\$ N.H. # 1	208.8	15.85 8.11 +7.74
1.		212.0	11.80 9.19 +2.61
2.		216.8	17.06 11.27 +5.79
3.	6-505	220.8	14.85 7.25 +7.60
4.		224.8	10.05 3.22 +6.83
5.		228.8	16.47 10.54 +5.93
6.	3 + 00	232.8	12.88 2.65 +10.23
	3 + 00 = D.E.	236.0	4.28 4.20 +0.08

194.0	186.9	196.0
7.49	5.79	8.27
201.49	192.69	204.27
6.44		3.66
207.93		207.93
195.60		
12.33	12.33	
4.81	4.81	
7.52	7.87	

# Santa Cruz Ave Grades

Station	North	South
0+00 = E.A. Ebers		
Old Carb	94.3	95.1
0+08 = P.C.	94.6	95.6
1	97.7	98.7
2	100.8	101.8
3	103.9	104.9
4 1+80 Brk.	107.0	108.0
1	100.83	111.83
2	114.66	115.66
3	118.50	119.50
4	122.33	123.33
5	126.16	127.16
6 4+40 = Brk	130.0	131.0
7	135.17	136.17
8	140.34	141.34
9 5+92 = P.C.	145.5	146.5
6+00 = EX. CB PL. Froude	146.85	147.37
0+00 = EL. Froude	148.1	149.5
+08 = P.C.	149.0	150.0
1	155.0	155.87
2 4-48's	161.0	161.75
3	167.0	167.62
4 2+00 = Brk	173.0	173.5
1 6-50's	178.09	178.58
2	183.16	183.66

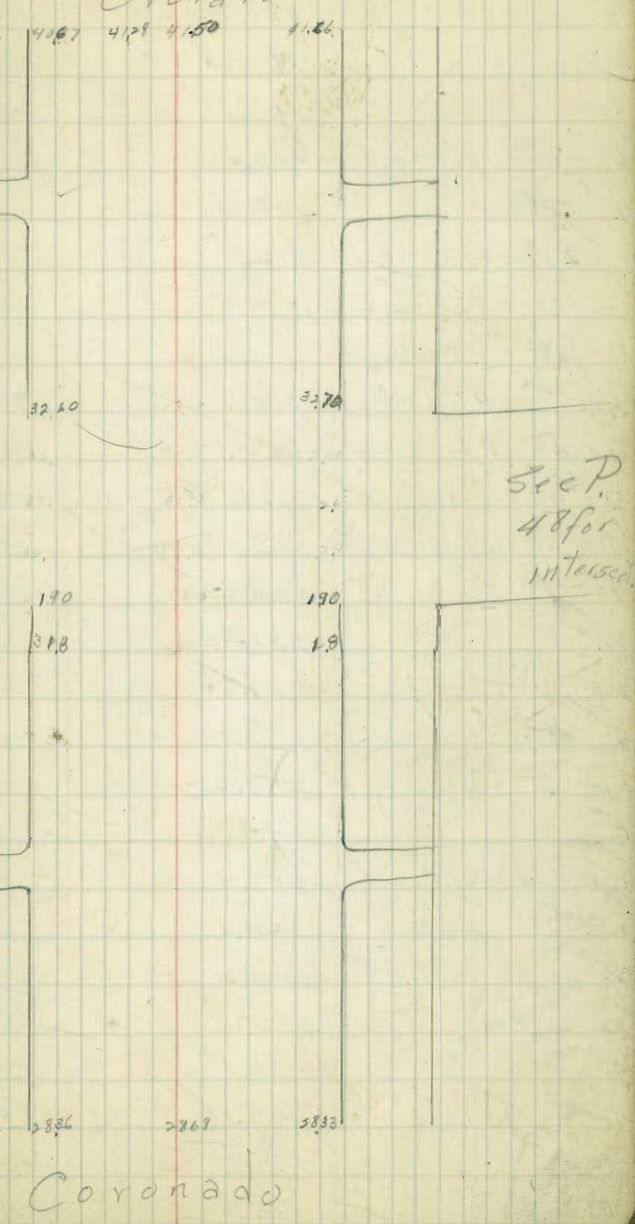
# Cable Pmt Orchard sec 10 for section 68

4067  
4 1.66  
8 2.33  
4 1.50  
4 0.67  
8 2.33  
3 1.17  
3 1.17

B.R.B.M.  
33.12

Del  
Mar

B.R.B.M.  
28.58



Coronado

	N		S	
3	188.25	$\begin{array}{r} 10.8 \\ 8.2 \\ +2.6 \\ \hline 5.8 \\ 4.1 \\ +1.7 \\ \hline 12.7 \\ 12.3 \\ +0.6 \\ \hline 7.8 \\ 7.2 \\ +0.1 \\ \hline 3.3 \\ 3.5 \\ -0.2 \end{array}$	188.75	$\begin{array}{r} 14.8 \\ 3.9 \\ +10.1 \\ \hline 2.8 \\ 4.5 \\ +0.3 \\ \hline 14.7 \\ 1.6 \\ +3.1 \\ \hline 10.2 \\ 8.6 \\ +1.6 \end{array}$
4 6-50s	193.33	$\begin{array}{r} 12.7 \\ 12.3 \\ +0.6 \\ \hline 7.8 \\ 7.2 \\ +0.1 \\ \hline 3.3 \\ 3.5 \\ -0.2 \end{array}$	193.83	$\begin{array}{r} 14.7 \\ 1.6 \\ +3.1 \\ \hline 10.2 \\ 8.6 \\ +1.6 \end{array}$
5	198.41	$\begin{array}{r} 10.8 \\ 8.2 \\ +2.6 \\ \hline 5.8 \\ 4.1 \\ +1.7 \\ \hline 12.7 \\ 12.3 \\ +0.6 \\ \hline 7.8 \\ 7.2 \\ +0.1 \\ \hline 3.3 \\ 3.5 \\ -0.2 \end{array}$	198.71	$\begin{array}{r} 14.7 \\ 1.6 \\ +3.1 \\ \hline 10.2 \\ 8.6 \\ +1.6 \end{array}$
6 5+00 = Rk R Cons	203.5	$\begin{array}{r} 3.3 \\ 3.5 \\ -0.2 \end{array}$	204.0	$\begin{array}{r} 15.14 \\ 12.1 \\ +2.0 \end{array}$
1 + 50	208.05	$\begin{array}{r} 10.8 \\ 8.2 \\ +2.6 \\ \hline 5.8 \\ 4.1 \\ +1.7 \\ \hline 12.7 \\ 12.3 \\ +0.6 \\ \hline 7.8 \\ 7.2 \\ +0.1 \\ \hline 3.3 \\ 3.5 \\ -0.2 \end{array}$	217.35	
6+80 = W.L. Guizotto S	212.6	$\begin{array}{r} 5.0 \\ 3.8 \\ +2.2 \end{array}$	217.7	
+6+60 = EL Guizotto S.	218.5	$\begin{array}{r} 2.5 \\ 0.8 \\ +1.7 \\ \hline 13.4 \\ 12.8 \\ +1.4 \end{array}$	218.0	
6+68 = R Cons.			220.63	
6+92 = P.C. on N	221.0	$\begin{array}{r} 10.3 \\ 8.4 \\ +1.9 \end{array}$	223.1	
7+00 = W.L. Guizotto N	221.9		225.56	
7+30 = old cons.			228.2	
7+60 = EL Guizotto N	225.0		231.4	
1	228.2		232.11	
2	231.4		235.39	
3 7-40s	234.6		238.67	
4	237.8		241.94	
5	241.0		245.22	
6	244.2		248.5	
7 10+40 = R.K. Cons.	247.4		249.8	
1.	249.0		251.1	
2.	250.6		252.1	
3 11-50s	252.2		253.0	
4.	253.2		253.7	
5.	254.1		254.2	
6.	254.8		254.6	
7.	255.3			

	N	S.
8.	255.6	255.0
9. 1/2 00	255.8	255.07
10.	255.9	255.07
11. 12+60 = W.L. Santa Barbara	256.0	255.0

8	232.47	214	2.92	2.47	230.24	R.C.
8.5	233.1	222.43	222.1	230.93	231.6	
8.10	233.1	222.43	222.1	230.93	231.6	

249.10  
11.70  
237.40

Coronado 57 Grades

0+00 = El. Ebers.	106.5	106.7
0+08	106.8	107.0
0+18	107.97	107.85
1.	112.04	112.09
2	116.12	116.33
3. 1-43 1/2	120.70	120.57
4	124.27	124.81
5	128.35	129.05
6 2+60 = Brk.	132.43	133.3
3+00 = Brk	138.0	139.10
11	145.5	146.5
2. 4-45 1/2	153.0	154.0
51	160.5	161.5
4 4+80 = R.V.C.	168.0	169.0
1.	171.1	172.1
2. 5-20 1/2	173.7	174.7
3.	175.8	176.9
41	177.3	178.5
5 5+80	178.4	179.8

242.0	241.33	1.29	1.05	237.93	240.6	
210	245.05	4.83	4.60	3.53	244.2	
20	246.5	5.83	5.86	5.70	4.73	245.1
20	247.4	6.73	6.76	6.60	5.63	246.3
20	248.2	7.63	7.59	7.55	6.63	247.2
20	249.2	8.13	8.19	8.05	7.13	247.8
20	249.7	8.53	8.59	8.40	7.53	248.2
20	249.8	8.93	8.74	8.65	7.83	248.5
20	249.4	8.73	8.79	8.65	7.73	248.8
20	249.2	8.53	8.59	8.40	7.53	248.2
20	248.7	8.23	8.14	8.15	7.23	247.9
20	247.8	7.13	7.29	7.30	6.53	247.2
20	247.0	6.133	6.49	6.45	5.73	246.4

B.M. SW B.P.  
340.10 B.P.

Santa Barbara



# Coronado Grades

	N.	S.
5+92 = P.C.	178.76	180.22
6+00 = W.L. Froode	179.0	181.0
0+00 = E.L. Froode	180.5	182.
0+08	180.96	182.44
1.	183.53	184.89
2. 3-44	186.10	187.34
3. 1+40 = P.W.C.	188.66	189.78
+60	189.95	190.95
+80	191.3	192.3
2+00	192.9	193.9
2+20	194.52	195.52
1.	198.74	199.74
2	202.96	203.96
3	207.18	208.18
4 8-4653	211.40	212.4
5	215.62	216.62
6	219.84	220.84
7	214.06	225.06
8 5+92 = P.C. Guizot	228.28	229.28
6+00 = W.L. Guizot	229.0	230.0
0+00 = E.L. Guizot	230.5	232.0
0+08 = P.C.	230.94	232.44
0+21.5 = Brk-odd. Cb	231.6	233.1

# Coronado Grades 71

	N	S
0+00 = E.L. Cliffs <sup>Sunset</sup>	51.14	50.27
0+10	57.7	50.92
1	56.26	55.36
2	60.63	59.81
3	64.99	64.25
4	69.36	68.7
5 12-48.55	73.72	73.14
6	78.09	77.59
7	82.45	82.03
8	86.82	86.48
9	91.18	90.92
10	95.54	95.36
11	99.91	99.81
12 5+92 = P.C.	104.28	104.26
6+00 = Ebers.	104.8	104.8

2.7  
-0.6

# Del Mar Ave Grades

	N.	S.	
0+00 = F.L. Sun Set cliffs	36.8	36.3	
1	37.97	37.35	
2	39.15	38.4	
3	40.32	39.45	
4. 2+00 = P.V.C.	41.5	40.5	
2+20	42.1	41.1	
+40	43.0	42.0	
+60	44.2	43.1	
2+80 = F.V.C.	45.7	44.5	
1	49.43	48.15	
2	53.16	51.8	
3	56.9	55.44	
+40	58.8	57.2	
4+60 = E.V.C.	61.38	59.88	
1	67.7	66.20	
2	74.02	72.52	
3	80.34	78.84	
6+00 = Ebers	81.35	79.9	
0+00 = E.L. Ebers	84.6	83.15	
0+08 = P.C.	85.62	84.12	
1	91.48	89.98	
2	97.34	95.84	
3	103.2	101.7	
4	109.06	107.56	

50.7 Total Ebers

80.75 P.M.

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Del Mar Grades  
N  
S.

73

5	114.92	113.42	2.0 2.0 -0.2
6	120.78	119.28	1.5 1.5 +0.5
7	126.64	125.14	1.5 1.5 +1.6
8.5+40 = Birk.	132.3	131.0	1.3 1.3 +0.9
1.	137.02	135.52	1.5 1.5 +0.5
2.	141.54	140.04	1.5 1.5 +0.5
3. L-42	146.07	144.57	1.5 1.5 +1.5
4	150.59	149.09	1.5 1.5 +1.5
5	155.11	153.61	1.5 1.5 +1.5
6. 5+92 = P.C.	159.64	158.14	1.5 1.5 +1.5
6+00 = W.L. Froude	160.4	158.85	1.5 1.5 +1.5

0+00 = F.L. Froude	163.5	161.8	
0+08 = P.C.	163.92	162.42	
1.	166.52	165.02	
2. L-48.75	169.12	167.62	
3.	171.71	170.21	
4.	174.31	172.81	
5.	176.91	175.41	
6. 3+00 = Birk	179.5	178.0	1.5 1.5 -1.5
1.	183.15	181.65	1.5 1.5 -1.5
2.	186.8	185.3	1.5 1.5 -1.5
3. L-48.75	190.45	188.95	1.5 1.5 -1.5
4.	194.1	192.6	1.5 1.5 -1.5
5.	197.75	196.25	1.5 1.5 -1.5
6. 5+92 = P.C.	201.4	199.9	1.5 1.5 -1.5
6+00 = W.L. Guizot	201.8	200.5	1.3 1.3 -1.3

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92.75

# Del Mar Grades

	N.		S.	
0+00 = El. Gvizot	204.5	12.1	203.1	$\frac{13.5}{13.5}$ - 0.0
0+08 = F.C.	205.46	$\frac{19.8}{12.1}$ + 4.8	204.01	
1. <del>SW. 1/4</del> 204.00	210.74	$\frac{19.8}{12.1}$ + 11.9	209.6	$\frac{7.0}{7.0}$ + 0.1
2. <del>SE. 1/4</del> 204.00	216.02	$\frac{13.6}{12.1}$ + 0.0	215.18	$\frac{1.2}{1.2}$ - 1.1
3. <del>SW. 1/4</del> 204.00	224.3	$\frac{16.0}{12.1}$ + 2.8	220.77	$\frac{7.5}{7.5}$ - 0.6
4. <del>SW. 1/4</del> 204.00	226.58	$\frac{16.0}{12.1}$ + 2.7	226.35	$\frac{11.0}{11.0}$ + 3.0 + 3.5
5. <del>SW. 1/4</del> 204.00	231.86	$\frac{16.2}{12.1}$ + 7.1	231.94	$\frac{5.4}{5.4}$ + 1.8
6. <del>SW. 1/4</del> 204.00	237.14	$\frac{11.0}{12.1}$ + 8.7	237.43	$\frac{10.0}{10.0}$ + 6.1
7. <del>SW. 1/4</del> 204.00	242.42	$\frac{15.5}{12.1}$ + 7.5	243.12	$\frac{5.0}{5.0}$ + 1.0
8. 3+60 = old C6. Bk.	247.7	$\frac{10.2}{12.1}$ + 6.3	248.7	$\frac{7.2}{7.2}$ + 8.7 + 6.0

# Froude St Grades

	E.		W.	
0+00 = N.A. P. ...	97.1		96.1	
1.	100.3		99.3	
2. 4-45	103.5		102.5	
3.	106.8		105.8	
4. 1+60	110.0		109.0	
1. 3-44.7	116.0		115.0	
2.	122.0		121.0	
3. 3+00 = S.L. Orchard	129.0	$\frac{10.2}{8.1}$ + 2.1	127.0	$\frac{7.6}{7.6}$ - 3.4
0+00 = N.A. "	130.5	$\frac{7.9}{8.1}$ + 3.0	129.5	$\frac{7.7}{7.7}$ + 6.1
1. 2-505	139.75		136.75	
2. 1+00 = F.C.	145.0		144.0	
+ 30	147.8		146.8	
+ 40	150.0		149.0	

# Froude St Grades

1+60	151.8	150.8
1+80 = F.C.	153.2	152.2
1	155.5	154.5
2. 3/405	157.7	156.7
3. 3+00 = S.L. Del Mar	160.0	159.0
0+00 = N.A. " "	163.5	162.5
1	168.9	167.9
2. 3/405	174.3	173.7
3. 1+20 = F.C.	179.7	178.7
+ 40	182.0	181.0
+ 50	183.4	182.4
+ 80	184.2	183.2
3+00 = F.C.	184.2	183.2
1. 2/405	183.1	182.1
3. 5+00 = F.C.	182.0	181.0
3+10 = S.L. Coronado	181.87	180.75

# Orchard Ave Grades

# Pescadero Ave Grades

	N.	S.
0700 = K.L. Sunset dffs	31.0	30.33
+50	31.75	30.91
1700 = Brk	32.5	31.5
1.	33.2	32.2
2. 6-40's	34.4	33.4
3. All Breaks	36.1	35.1
4	38.2	37.2
5.	40.7	39.7
6. 3+40 =	43.9	42.9
"	48.3	47.17
2. 4-50's	52.7	51.45
3.	57.1	55.72
4 5+40 = Brk	61.5	60.0
5+42 = P.C	67.56	66.06
6+00 = Ebers	68.1	66.8
0700 = E.L. Ebers	70.2	68.9
0708 = P.C.	70.67	69.16
1.	74.5	73.0
2. 6-45-33's	78.3	76.8
3	82.1	80.6
4.	85.9	84.4
5	89.7	88.2
6. 2+80 = Brk	93.5	92.0
1. 5-53's	99.2	97.7
2.	104.9	103.4

	N	S	N
0700 = F.L. Froude	96.2	96.2	97.1
"	100.85	100.85	101.85
"	105.7	105.7	106.7
"	110.5	110.5	111.5
"	115.3	115.3	116.3
"	120.2	120.2	121.2
"	125.0	125.0	126.0
"	129.8	129.8	130.8
"	134.7	134.7	135.7
"	139.5	139.5	140.5
"	144.3	144.3	145.3
"	149.15	149.15	150.15
" = W.L. Quizot	153.8	153.8	154.7
1400 = E.L. Quizot	158.4	158.4	157.0
"	161.7	161.7	162.6
"	167.3	167.3	168.33
"	173.0	173.0	174.00
"	178.7	178.7	179.67
"	184.3	184.3	185.34
"	190.0	190.0	191.01
"	195.7	195.7	196.67
"	201.3	201.3	202.34
"	207.0	207.0	208.02
"	212.7	212.7	213.68
"	218.35	218.35	219.35
"	223.7	223.7	224.9

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-6101.20  
-6107.35  
-6113.50  
-6119.65  
-6125.80  
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Orchard Ave

	N.		S.
3.	100.6	12.8 7.0 +5.3	109.8
4. 6-535	116.3	15.3 7.7 +10.5	114.7
5.	123.0	12.5 +7.9	130.4
6.			
7. 5+92 = P.C.	127.7		126.1
6+00 = W.L. Froude	128.1	10.1 2.6 +7.5	127.0
0+00 = E.L. Froude	139.83	8.4 4.7 +3.7	129.2
0+08 = P.C.	180.49		129.68
1. 3-465	134.60		133.6
2. 1+00 = P.I.C.	138.71		137.57
+20	140.2		139.1
+40	141.7		140.6
+60	142.9		141.9
1+80 = E.V.C.	144.13		143.18
1	146.6		145.6
2. 4-455	149.0		148.0
3	151.4		150.4
4. 3+60 = P.V.C.	153.87		152.87
+80	155.0		154.0
4+60	156.3		155.3
+20	157.8		156.8
4+40 = E.V.C.	159.4		158.4
1. 3-526	163.7		162.7
2	168.0		167.0
3. 5+92 = P.C.	172.32		171.32
6+00 = W.L. Guizot	172.8	7.9 2.6 +5.3	172.0

12.8  
7.0  
+5.3  
15.3  
7.7  
+10.5  
12.5  
+7.9  
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4.7  
+3.7  
7.6  
4.2  
+3.4

Orchard Ave Grades

'76

	N		S.
0+00 = E.L. Guizot	175.2	5.5 1.0 +4.1	174.3
0+08 = P.C.	176.18		175.16
1.	182.3	2.8 7.9 +5.1	181.3
2.	188.5	3.1 3.0 +7.1	187.4
3.	194.6	7.0 3.8 +1.7	193.5
4.	200.8	12.2 2.3 +7.9	199.6
5.	206.9	6.1 3.1 +3.7	205.8
6.	213.1	10.3 5.3 +5.0	211.9
7.	219.2	14.0 2.8 +7.2	218.0
8. 3+40 = P.I.C.	225.4	8.4 3.1 +4.5	224.1
+60	228.3	17.0 7.6 +7.4	226.8
+80 <i>sketch</i>	230.9	14.4 4.7 +9.7	229.4
4+00	233.1	12.2 2.6 +9.4	231.6
4+20 = E.V.C.	235.2	10.4 8.8 +9.4	233.6
1.	239.2	15.6 7.3 +8.3	237.5
3. 4-42.55	243.1	11.7 4.6 +7.1	241.3
3	247.1	7.7 2.7 +5.3	245.2
4. 5+90 = P.C.	251.07	3.7 3.0 +0.7	249.08
6+00 = W.L. Guizot	251.4	3.4 3.0 +0.6	249.8

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# Gulzot St. Grades

	E		W.	
0+00 = P.H. Loma = 255.41	121.0	$\frac{10.22}{19.29}$ $\frac{2.12}{-1.1}$	120.0	$\frac{11.28}{19.29}$ $\frac{-1.1}{-1.1}$
1.	123.33	$\frac{18.1}{17.7}$	122.33	$\frac{8.96}{2.62}$ $\frac{-1.74}{-1.74}$
2 6-47.33	125.66	$\frac{15.2}{6.2}$	124.66	$\frac{6.6}{-1.0}$ $\frac{-1.0}{-1.0}$
3	128.0	$\frac{13.4}{10.1}$ $\frac{-3.3}{-3.3}$	127.0	$\frac{4.2}{1.7}$ $\frac{-1.7}{-1.7}$
4	130.33	$\frac{11.1}{2.4}$ $\frac{-2.7}{-2.7}$	129.33	$\frac{1.7}{2.3}$ $\frac{-2.3}{-2.3}$
5	132.66	$\frac{21.0}{12.2}$ $\frac{-8.8}{-8.8}$	131.66	$\frac{0.8}{0.8}$ $\frac{-8.8}{-8.8}$
6 2+83.4 = SL Bermuda	135.0	$\frac{2.9}{2.9}$ $\frac{-1.0}{-1.0}$	134.0	$\frac{7.46}{2.56}$ $\frac{-1.04}{-1.04}$
0+00 = N.H. "	136.0	$\frac{2.45}{2.45}$ $\frac{-1.01}{-1.01}$	135.0	$\frac{6.00}{2.00}$ $\frac{-1.00}{-1.00}$
1.	139.16	$\frac{14.4}{11.3}$ $\frac{-3.1}{-3.1}$	138.16	$\frac{15.4}{11.7}$ $\frac{-3.7}{-3.7}$
2 6-50.5	142.33	$\frac{11.3}{7.0}$ $\frac{-4.3}{-4.3}$	141.33	$\frac{12.3}{10.9}$ $\frac{-1.4}{-1.4}$
3.	145.50	$\frac{9.1}{6.5}$ $\frac{-2.6}{-2.6}$	144.5	$\frac{9.1}{11.9}$ $\frac{-2.8}{-2.8}$
4	148.66	$\frac{5.0}{2.4}$ $\frac{-2.6}{-2.6}$	147.66	$\frac{5.9}{2.1}$ $\frac{-3.8}{-3.8}$
5	151.83	$\frac{13.9}{12.7}$ $\frac{-1.2}{-1.2}$	150.83	$\frac{14.7}{11.6}$ $\frac{-3.1}{-3.1}$
6 3+00 = SL P. S. B. Lero	155.0	$\frac{10.7}{5.7}$ $\frac{-5.0}{-5.0}$	154.0	$\frac{11.7}{10.5}$ $\frac{-1.2}{-1.2}$
0+00 = N.H. "	157.0	$\frac{5.7}{6.7}$ $\frac{-1.0}{-1.0}$	156.0	$\frac{10.0}{10.3}$ $\frac{-0.3}{-0.3}$
1 3-00	160.57	$\frac{3.1}{2.1}$ $\frac{-1.0}{-1.0}$	159.57	$\frac{6.1}{13.1}$ $\frac{-7.0}{-7.0}$
2 1+00 = P.C.	164.14	$\frac{10.4}{13.4}$ $\frac{-3.0}{-3.0}$	163.14	$\frac{11.4}{12.6}$ $\frac{-1.2}{-1.2}$
+20	165.4	$\frac{13.1}{14.8}$ $\frac{-1.7}{-1.7}$	164.4	$\frac{14.1}{12.2}$ $\frac{-1.9}{-1.9}$
+40	166.6	$\frac{11.2}{4.7}$ $\frac{-6.5}{-6.5}$	165.6	$\frac{12.2}{14.1}$ $\frac{-1.9}{-1.9}$
+60	167.6	$\frac{10.7}{18.4}$ $\frac{-7.7}{-7.7}$	166.6	$\frac{11.7}{13.7}$ $\frac{-2.0}{-2.0}$
+80 = P.C.	168.5	$\frac{10.0}{2.0}$ $\frac{-8.0}{-8.0}$	167.5	$\frac{11.0}{10.0}$ $\frac{-1.0}{-1.0}$
1	170.0	$\frac{8.5}{2.0}$ $\frac{-6.5}{-6.5}$	169.0	$\frac{9.5}{10.0}$ $\frac{-0.5}{-0.5}$
2 3-40's	171.5	$\frac{10.0}{10.0}$ $\frac{-8.5}{-8.5}$	170.5	$\frac{8.0}{10.0}$ $\frac{-2.0}{-2.0}$
3 3+00 = SL D. Orchard	173.0	<del><math>\frac{7.7}{11.1}</math></del>	172.0	<del><math>\frac{7.7}{10.4}</math></del>

	E		W.	
0+00 = N.H. Orchard	175.0	$\frac{5.7}{2.4}$ $\frac{-3.3}{-3.3}$	174.0	$\frac{6.7}{10.1}$ $\frac{-3.4}{-3.4}$
1	179.41	$\frac{7.9}{2.1}$ $\frac{-5.8}{-5.8}$	178.41	$\frac{9.1}{7.3}$ $\frac{-1.8}{-1.8}$
2	183.73	$\frac{18.7}{13.0}$ $\frac{-5.7}{-5.7}$	182.83	$\frac{4.9}{7.3}$ $\frac{-2.4}{-2.4}$
3	188.25	$\frac{11.2}{14.5}$ $\frac{-3.3}{-3.3}$	187.25	$\frac{4.0}{3.1}$ $\frac{-0.9}{-0.9}$
4 4-50's	192.66	$\frac{6.0}{2.0}$ $\frac{-4.0}{-4.0}$	191.66	$\frac{7.8}{11.2}$ $\frac{-3.4}{-3.4}$
5	197.08	$\frac{2.4}{2.6}$ $\frac{-0.2}{-0.2}$	196.08	$\frac{3.4}{5.6}$ $\frac{-2.2}{-2.2}$
6 3+00 = SL Del Mar	201.5	$\frac{19.6}{29.0}$ $\frac{-9.4}{-9.4}$	200.5	$\frac{1.8}{2.0}$ $\frac{-0.2}{-0.2}$
0+00 = N.H. "	204.5	$\frac{7.6}{2.7}$ $\frac{-4.9}{-4.9}$	203.5	$\frac{8.0}{2.0}$ $\frac{-6.0}{-6.0}$
+40 = B.K.	210.0	$\frac{14.4}{13.8}$ $\frac{-0.6}{-0.6}$	209.0	$\frac{15.4}{5.8}$ $\frac{-9.6}{-9.6}$
+90 = "	216.4	$\frac{17.8}{11.8}$ $\frac{-6.0}{-6.0}$	215.4	$\frac{7.0}{7.6}$ $\frac{-0.6}{-0.6}$
+40 = "	221.5	$\frac{12.7}{7.6}$ $\frac{-5.1}{-5.1}$	220.5	$\frac{3.9}{3.2}$ $\frac{-0.7}{-0.7}$
+90 = "	225.5	$\frac{8.7}{4.5}$ $\frac{-4.2}{-4.2}$	224.5	$\frac{1.1}{1.8}$ $\frac{-0.7}{-0.7}$
+40 = "	228.5	$\frac{5.8}{3.1}$ $\frac{-2.7}{-2.7}$	227.3	$\frac{6.9}{2.6}$ $\frac{-4.3}{-4.3}$
3+00 = " 70. Com. Rd.	231.0	$\frac{3.2}{2.0}$ $\frac{-1.2}{-1.2}$	230.0	$\frac{1.7}{2.0}$ $\frac{-0.3}{-0.3}$
3+10 = B.K. on W. Rd.	230.2		230.2	$\frac{4.0}{4.0}$ $\frac{-0.0}{-0.0}$
0+00 = N.H. Orchard	229.4	$\frac{3.0}{1.6}$ $\frac{-1.4}{-1.4}$	228.9	$\frac{3.5}{2.0}$ $\frac{-1.5}{-1.5}$
+10 = "	229.4	$\frac{4.7}{1.0}$ $\frac{-3.7}{-3.7}$	228.4	$\frac{5.1}{10.9}$ $\frac{-5.8}{-5.8}$
1	227.68	$\frac{1.0}{2.0}$ $\frac{-1.0}{-1.0}$	226.77	$\frac{5.0}{5.0}$ $\frac{-0.0}{-0.0}$
2 4-10's	225.96	$\frac{6.4}{3.4}$ $\frac{-3.0}{-3.0}$	225.15	$\frac{7.2}{10.4}$ $\frac{-3.2}{-3.2}$
3	224.24	$\frac{8.1}{2.0}$ $\frac{-6.1}{-6.1}$	223.52	$\frac{8.8}{10.1}$ $\frac{-1.3}{-1.3}$
4 1+70 = P.C. on W.	222.52	$\frac{9.8}{10.6}$ $\frac{-1.0}{-1.0}$	221.9	$\frac{10.4}{10.1}$ $\frac{-0.3}{-0.3}$
+40	220.8	$\frac{3.5}{2.0}$ $\frac{-1.5}{-1.5}$	220.8	$\frac{3.4}{10.1}$ $\frac{-6.7}{-6.7}$
2+10 = P.C. on W.	220.8	$\frac{11.5}{10.0}$ $\frac{-1.5}{-1.5}$	219.5	$\frac{4.7}{10.0}$ $\frac{-5.3}{-5.3}$
1 1+00 = 2' 55' 03" W.	218.8		218.8	$\frac{5.4}{11.4}$ $\frac{-6.0}{-6.0}$
2 0+30 = B.K. on W.	218.0		218.0	$\frac{6.0}{11.9}$ $\frac{-5.9}{-5.9}$



# Gvizo 7 St. Grades

	E.	W.	
1	10.50	217.1	7.1 4.2 7.2
2	3+50 = E.V.C. on W.	219.08	13.0 8.1 4.7
1		214.89	8.3 4.0 4.3
2		213.68	10.5 6.7 3.8
3		212.47	11.7 7.5 4.2
4	(E.L. 3+90)	217.36	12.7 8.4 4.3
5	11.50	210.05	14.1 8.1 6.0
6	3+40	208.84	5.4 1.2 4.2
7		207.63	6.6 2.8 3.8
8	(E.L. 3+10) Santa Cruz E	206.42	7.6 4.3 3.3
9		205.21	9.0 5.4 3.6
10	E.C. on Santa Cruz	204.0	10.2 5.0 5.2
11	0+00 = N.L. Santa Cruz	222.7	12.4 8.1 4.3
12	+40	224.32	11.0 6.8 4.2
13	+50	222.83	10.5 10.0 0.5
14	+80 = P.K. on E	224.45	10.8 7.3 3.5
15	+100	222.76	10.2 6.5 3.7
16	+30	224.3	11.0 7.1 3.9
17	+40	224.1	11.2 10.5 0.7
18	+60	223.8	

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1% If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table is same row and column by which distance from side stake to slope stake. If ground is not nearly level, the distance from side stake to slope stake and slope stake lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and distance in table. Set up rod at this point, and line of sight should cut target. (See also Table No. 2.)

## IMPROVED TABLES AND INFORMATION

TABLE No. 2  
To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given  $T$  may be found by dividing tangent (or external), opposite  $T$  by given tangent (or external).  
The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

6.89  
5.7  
7.16

6.11  
4.62  
10.73  
5.86  
5.50

5.90  
4.40  
10.86  
0.17  
5.27

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

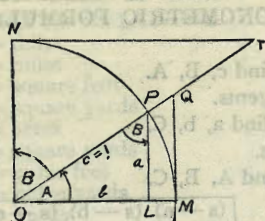


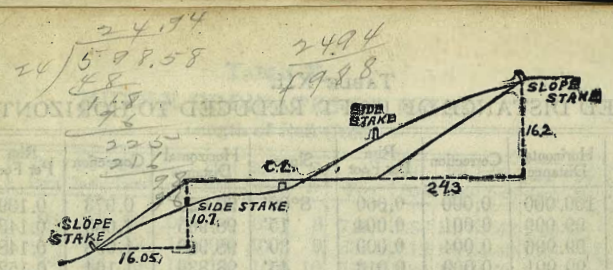
TABLE II

TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \end{aligned}$$

$$\begin{aligned} \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Sines} & \frac{\sin a}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

Handwritten calculations and diagrams on the right page. Includes numbers like 109, 1035, 573, 1733, 6164, 4, 8, 52, 6.60, 4.06, 5.73, 5.36, 5.54, 5.66, 12.26, 6.13, 285.17, 283.71, 125.771, 128.85, 128.62, 307.62, 162.5, 81.25, 1.21, 90.01, 89.55, 6.30, 16.25, 31/390, 24, 100, 144, 60, 48, 120, 277.62, 20, 277.62, 138.81, 10, 148.81.

To find

