

GRADE.
163
ROSE-CANON

PASTA

FIELD BOOK

No. 885

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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MICROFILMED

APR 9 1965

Walker
NE Hwy 11
Lacey
MoHoon 8-27-27

Note: for Alignment See Book 1325

STA + H.Z. -
Z + 50

Z + 39.37
BC.

Z + 00

+ 50

1 + 00

+ 50

0 + 00

0.63 19.94 19.31

45.95.
SW Balboa
+ Koble Canyon

A

Lt.

£

ft.

-4.2
31.1

-2.6
28.7

-1.9
27.7

-0.9
26.2

-0.3
25.3

+ 0.24 o/p

-2.5
1.24
18.70

-2.2
1.36
18.58

-1.6
1.48
18.46

-0.8
1.60
18.34

-0.2
1.72
18.22
18.94

18.10

0 1
-1.8
24.6

-1.4
25.7

-0.6
25.7

+0.4
25.2

+0.8
25.4

STH.	+	H.T	lt.	\$	Rt.
5+50				19.42	2
5+00				19.30	
38.24=EC 4+89.4=EC.					
+50			-5.3 32.8	-4.1 0.76 19.18	-2.2 28.1
4+00			X -5.4 32.5	-4.0 0.88 19.06	-2.4 28.4
+50			-4.8 32.0	-3.2 1.0 18.94	-2.1 28.0
3+00			-4.6 31.7	-3.1 1.12 18.82 19.04	-1.7 27.4

Not a Part of this Contract

+0.24%

Note: 0.04 per ft. Super in this case.

Sta.	+	H.I	-	Lt.	Σ	Rt.
9+00				+ 4.23 0/0 -6.0 33.8	-6.8 0.76 60.23	³ -1.7 36.4
+50				-7.1 32.5	-1.7 0.84 20.12	-5.3 32.8
7+00	8.47	20.96	7.45	12.49	20.96	
		19.94 - X Age 2				
8+00					20.00	
+50					19.88	
7+00					19.78	
+50					19.66	
6+00					19.54	

Not a part of this contact

STA.	H.I.		Lt.	ℓ	Rt.
13+00			-3.0 29.3	-3.1 4.47 21.15 25.62	4 -4.6 31.7
T.P.	7.62	25.62	2.96	18.00	
+50			-3.5 30.1	-3.3 +0.07 21.03	-4.9 32.2
12+00			-3.1 29.5	-3.9 0.04 20.92	-5.5 33.1
+50			-3.6 30.2	-4.4 0.16 20.80	-5.7 33.4
11+00			-3.6 30.2	-4.8 0.27 20.69	-6.4 34.4
+50			-3.9 30.7	-5.1 0.39 20.57	-6.5 34.6
10+00			-4.6 31.7	-6.0 0.46 20.46	-11.2 41.6
9+50	20.96		-5.2 32.6	-6.1 0.62 20.34 20.96	-11.3 41.8

↑
+0.23%

STA. 4 H.F.

16+00

73-86.
15+87.38-86.

+50

15+00

+50

4.28 29.74

T.P. on BM#1

0.14

25.46 = BM#1

0.02 = Error.
25.46 = BM
25.48

14+00

13+50

25.62

lt.

-1.9
27.2

-2.0
27.8

-2.2
28.1

-2.1
28.0

-2.7
28.5

-3.0
29.3

6
-0.9
7.24
22.50

-1.4
7.64
22.10

-1.5
7.97
21.77

-2.1
8.20
21.54
29.74

-2.5
4.24
21.38

-2.8
4.36
21.26
25.62

pt.
5
-6.9
35.2

-6.0
33.8

-6.4
34.4

-6.4
34.4

-6.8
35.0

-7.0
35.3

of $\frac{1}{2}$ in this curve

400 V.C.

+0.25%

Sta. + H.I. -

19+50

19+00

+50

18+00 = EVC

7.03 32.49

25.46

BM# 1.2 x 2" Hub,
63' H. Sta. 16+95

+50

17+00

16+50

+1.544%

400' V.C.

Lt.	C	Rt.
$\frac{+18.6}{39.3}$	$\frac{-0.2}{5.25}$ 27.24	$\frac{+0.2}{25.1}$ $\frac{+0.4}{25.2}$ 6
$\frac{+7.7}{28.9}$	$\frac{+0.1}{6.02}$ 26.47	$\frac{+0.2}{25.1}$ $\frac{+0.4}{25.2}$
$\frac{+3.9}{26.7}$	$\frac{+0.5}{6.73}$ 25.70	$\frac{-0.1}{26.5}$ $\frac{-0.2}{26.2}$
$\frac{+2.9}{26.5}$ $\frac{+2.8}{26.4}$	$\frac{+1.3}{7.56}$ 24.93 32.49	$\frac{+0.5}{25.3}$ $\frac{+0.6}{25.3}$
$\frac{+3.2}{26.6}$	$\frac{+1.0}{5.55}$ 24.19	$\frac{-0.3}{25.3}$
$\frac{+1.9}{26.0}$	$\frac{+0.4}{6.20}$ 23.54	$\frac{-3.7}{30.2}$
$\frac{-1.1}{24.5}$	$\frac{-0.4}{6.76}$ 22.98 23.74	$\frac{-7.0}{35.3}$

04' Super in this Curve

STN.	+	H.I	-	
23+00				
T.P	7.18	39.48	4.88	32.30
+50				
22+00				
T.P	4.88	37.18	0.19	32.30
+50				
21+00				
+50				
20+00				

32.49

17.1816
22.14
22.150

Lt.	±	Ht.
$\frac{4408 + 0.5}{453} = 25.3$	$\frac{-0.9}{6.83} = 37.65$ 39.48	$\frac{8.8}{37.9} = 57.6$
$\frac{4479 + 11.6}{459} = 25.8$	$\frac{-0.5}{530} = 31.88$	$\frac{-0.3}{38.8} = 38.5$
$\frac{4416 + 11.5}{458} = 28.7$	$\frac{-0.1}{6.08} = 31.10$ 32.18	$\frac{11.6}{25.7} = 23.7$
$\frac{4624}{456.2}$	$\frac{0.0}{2.16} = 30.33$	$\frac{0.7}{25.6} = 25.3$
$\frac{454.2}{452.1}$	$\frac{-0.2}{2.93} = 29.56$	$\frac{0.7}{25.9} = 25.6$
$\frac{453.9}{451.6}$	$\frac{-0.3}{3.70} = 28.79$	$\frac{0.7}{25.6} = 25.3$
$\frac{435.3}{43.7}$	$\frac{+0.5}{4.47} = 38.02$ 32.49	$\frac{40.1}{25.1} = 25.2$

+1.5344 96

of Supor in this Curve

STA. + H.I. -

29 + 00

+50

28 + 00

+50

27 + 00

+50

26 + 00

39.48

Lt.

$\frac{1532}{36}$

$\frac{1223}{31.2}$

$\frac{1178}{33.9}$

$\frac{1113}{30.7}$

$\frac{104}{29.2}$

$\frac{1103}{30.6}$

$\frac{184}{29.2}$

+1.544%

¢

$\frac{-4.7}{+2.43}$
41.91

$\frac{-4.5}{+1.66}$
41.14

$\frac{-3.9}{+0.89}$
40.37

$\frac{-4.1}{+0.12}$
39.60

$\frac{-3.9}{0.66}$
38.82

$\frac{-3.5}{1.49}$
38.05

$\frac{-2.8}{2.20}$
37.28
39.48

Rt.

9
 $\frac{-113}{47.3}$

$\frac{-11.6}{42.2}$

$\frac{-11.8}{42.5}$

$\frac{-12.0}{42.8}$

$\frac{-11.7}{43.4}$

$\frac{-10.9}{41.1}$

$\frac{-12.3}{43.3}$

STA.	+	M.I.	-
32+00			
+50			
31+00			
30+69 ^{.22} _{.37} = BC.			
+50			
T.P.	6.45	47.10	10.26 40.65
TP	0.94	50.91	12.04 49.97
30+00			
T.P.	12.07	62.01	0.17 49.94
TP	12.68	50.11	2.05 37.43
29+50			
		39.48	

Lt.	¢	Rt.
+38.6 +38.8 44.3 44.4	+9.1 15.47 46.54	<u>10</u> 33.9 38.7
+42.6 +42.8 46.3 46.4	+10.5 16.24 45.77	<u>6.7</u> 34.4 34.7
+43.4 +43.6 46.7 46.8	+11.3 17.01 45.00	<u>6.3</u> 34.2 35.5
+39.2 44.6	+9.7 17.78 44.23	<u>5.8</u> 33.5
+36.0 43.0	+8.0 18.55 43.46 62.01	<u>5.6</u> 33.2
+30.2 40.1	-3.8 +3.20 42.68 39.48	<u>7.3</u> 35.8

+1544.96

04 Super

on slab
10' LA 29+50
on slab
10' LA 29+50

Sta. + H.T. -

35 + 00

+ 50

34 + 00

+ 50

33 + 21.06
21 = EC.

33 + 00

T.P.
32 + 50

47.10

↑
+1.544%

Lt.

-2.1
27.9

-3.0
29.3

-3.8
30.5

-3.4
29.9

+3.2 (34.4)
42.1 (42.2)

+3.9 (43.1)
43.5 (43.6)

£

-13.8
+4.08
51.18

-11.4
+3.30
50.40

-10.0
+2.53
49.63

-7.6
+1.76
48.86

-5.4
+0.99
48.09

-1.3
+0.22
47.32
47.10

Rt.

11
-21.3
37.8

-17.3
50.8

-20.5
55.6

-18.8
53.0

(-17) (-16.9)
50.8 50.2

(-17.0) (-16.8)
50.8 50.0

↑
o.A. Super

STA.	+	H.I.	-	
38+50				
38+00 = Break.				
+50				
37+00				
+50				
36+00				
T.P.	13.73	56.44	0.26	42.71
35+50				
T.P.	7.97	42.97	12.10	35.00
		47.10		

Lt.	±	Rt.
$\frac{+3.6}{26.8}$	$\frac{-2.2}{+0.02}$ 58.46	12 $\frac{-13.8}{45.5}$
$\frac{+1.1}{25.6}$	$\frac{-4.0}{0.62}$ 55.82 ✓	$\frac{-18.0}{57.8}$
$\frac{+0.3}{25.2}$	$\frac{-5.5}{1.40}$ 55.04	$\frac{-19.5}{54.1}$
$\frac{-0.5}{25.6}$	$\frac{-3.4}{2.18}$ 54.26	$\frac{-20.3}{55.3}$
$\frac{-0.8}{22.0}$	$\frac{-3.4}{2.95}$ 53.49	$\frac{-22.1}{57.9}$
$\frac{-1.8}{27.7}$	$\frac{-3.6}{3.72}$ 52.72	$\frac{-22.0}{57.8}$
$\frac{-2.0}{26.8}$	$\frac{-10.2}{5.49}$ 51.25 56.44	$\frac{-18.9}{53.2}$

+1.544%

17 New File
00 84
Sta 35+00

JTA.	+	H.I.	-
42 + 00			
+ 50			
41 + 00			
+ 50			
40 + 00			
+ 50			
39 + 00			
T.P.	12.20	68.59	0.05 56.35
		56.44	

Lt.	¢	Rt.
+39.4 44.7	+6.4 7.61 60.98	13 +2.3 24.5
+22.6 36.3	+5.4 8.26 60.33	-6.2 34.1
+23.9 37.0	+4.2 8.90 59.69	-8.2 37.1
+20.7 35.7	+3.6 9.54 59.04	-9.0 38.3
+20.4 35.2	+3.4 10.19 58.40	-7.1 35.7
+22.6 36.3	+3.1 10.84 57.75	-8.0 36.0
+20.1 35.0	+2.4 11.48 57.11 58.53	-13.7 45.4

+1.29 %

STA.	+	H.I.	-
45 + 00			
44 + 52 = B.S. Lt.			
+ 50			
44 + 00			
+ 50			
43 + 00			
42 + 50			
T.P.	12.75	80.61	0.73 67.86
		68.59	

Lt.	¢	Rt.
+27.8 58.3	+10.8 15.76 64.85	14 +8.8 29.4
+28.0 39.0		
+21.5 35.8	+10.0 16.41 64.20	+9.4 29.7
+23.6 36.8	+9.1 17.05 63.58	+10.1 30.0
+30.9 40.5	+18.3 17.70 62.91	+9.6 29.8
+30.6 40.3	+17.9 18.34 62.27	+8.5 29.3
+37.6 43.8	+16.0 18.99 61.62 80.61	+8.2 29.1

+1.29%

at Super in this curve

Sta.	+	H.I.	-	↑	Lt.	£	Rt.
51+50					$\begin{matrix} +3.6 \\ 26.8 \end{matrix}$	$\begin{matrix} +1.6 \\ 12.0 \\ 73.23 \end{matrix}$	$\begin{matrix} +2.2 \\ 8.65 \\ 73.23 \end{matrix}$ 16 $\begin{matrix} +1.0 \\ 23.5 \end{matrix}$
51+00					$\begin{matrix} +4.9 \\ 27.2 \end{matrix}$	$\begin{matrix} +1.9 \\ 10.0 \\ 72.59 \end{matrix}$	$\begin{matrix} +2.1 \\ 9.29 \\ 72.59 \end{matrix}$ $\begin{matrix} +1.3 \\ 25.7 \end{matrix}$
+50					$\begin{matrix} +5.7 \\ 21.9 \end{matrix}$	$\begin{matrix} +2.6 \\ 10.0 \\ 71.94 \end{matrix}$	$\begin{matrix} +2.5 \\ 9.24 \\ 71.94 \end{matrix}$ $\begin{matrix} +1.6 \\ 25.8 \end{matrix}$
50+00					$\begin{matrix} +8.8 \\ 23.4 \end{matrix}$	$\begin{matrix} +7.5 \\ 13.0 \\ +6.2 \\ 17.0 \\ +5.7 \\ 8.0 \\ +4.2 \\ 5.0 \\ +4.0 \end{matrix}$	$\begin{matrix} +4.0 \\ 10.58 \\ 71.30 \\ 81.88 \end{matrix}$ $\begin{matrix} +3.1 \\ 26.6 \end{matrix}$
T.P.	3.89	81.88	11.15	77.99			
+50					$\begin{matrix} +11.9 \\ 31.0 \end{matrix}$	$\begin{matrix} +11.2 \\ 13.0 \\ 70.65 \end{matrix}$	$\begin{matrix} +5.4 \\ 13.49 \\ 70.65 \end{matrix}$ $\begin{matrix} +4.6 \\ 3.0 \\ 27.0 \end{matrix}$
49+00					$\begin{matrix} +13.8 \\ 31.9 \end{matrix}$	$\begin{matrix} +13.0 \\ 5.0 \\ 70.01 \end{matrix}$	$\begin{matrix} +11.2 \\ 13.13 \\ 70.01 \end{matrix}$ $\begin{matrix} +9.0 \\ 6.0 \\ +6.4 \\ 10.0 \\ 27.5 \end{matrix}$
48+85					$\begin{matrix} +15.5 \\ 32.7 \end{matrix}$	$\begin{matrix} +12.7 \\ 30.0 \\ 69.80 \end{matrix}$	$\begin{matrix} +13.8 \\ 13.34 \\ 69.80 \end{matrix}$ $\begin{matrix} +10.8 \\ 10.0 \\ +6.3 \\ 12.0 \\ 27.3 \end{matrix}$
48+50					$\begin{matrix} +18.3 \\ 34.2 \end{matrix}$	$\begin{matrix} +16.2 \\ 16.0 \\ 69.36 \end{matrix}$	$\begin{matrix} +15.3 \\ 16.0 \\ 69.36 \end{matrix}$ $\begin{matrix} +14.8 \\ 12.0 \\ +12.3 \\ 15.0 \\ +8.3 \\ 20.0 \\ 27.7 \end{matrix}$
48+25					$\begin{matrix} +19.0 \\ 34.5 \end{matrix}$	$\begin{matrix} +16.6 \\ 8.0 \\ +15.5 \\ 7.0 \\ +15.3 \end{matrix}$	$\begin{matrix} +15.3 \\ 20.10 \\ 69.04 \\ 89.14 \end{matrix}$ $\begin{matrix} +15.3 \\ 28.0 \\ 11.6 \\ 30.8 \end{matrix}$

+1.29%

89.4

JTA. + H.I. -

55+00

	Lt.		¢	Rt.
	$\frac{+10.8}{36.4}$	$\frac{+10.7}{24.0}$	$\frac{+14.8}{23.0}$	$\frac{+2.8}{9.98}$
				$\frac{+2.0}{26.0}$
				77.75

+50

	$\frac{+5.4}{27.7}$		$\frac{+13.4}{10.0}$	$\frac{+1.4}{10.63}$
				$\frac{+1.4}{25.7}$
				77.10

54+00

	$\frac{+5.9}{28.0}$		$\frac{+2.7}{15.0}$	$\frac{+2.5}{11.27}$
				$\frac{+1.7}{25.9}$
				76.46

+50

+129

	$\frac{+1.6}{25.8}$			$\frac{+1.6}{11.22}$
				$\frac{+1.5}{25.8}$
				75.81

53+00

	$\frac{+1.4}{25.7}$			$\frac{+0.8}{12.56}$
				$\frac{+0.5}{25.3}$
				75.17

+50

	$\frac{+1.0}{25.5}$			$\frac{+2.1}{13.21}$
				$\frac{+2.0}{26.0}$
				74.52

52+00

	$\frac{+1.7}{25.7}$			$\frac{+1.7}{13.85}$
				$\frac{+0.6}{25.3}$
				73.88
				87.73

10.43 87.73 4.58 77.30
 81.88

STA.	+	H.I.	-	
58+50				
58+00				
T.P.	3.48	96.95	0.21	93.47
+50				
57+00				
+50				
56+00				
T.P.	10.14	93.68	4.19	83.54
55+50				

87.73

LT.	±	RT.
+14.1 82.0	-1.2 14.65 82.26	18 -5.2 32.6
+28 29.9	-1.5 15.33 81.62 80.95	+0.7 25.3
+15.6 32.8	+0.2 12.71 80.97	+1.9 26.0
+12.0 31.0	+2.0 13.35 80.33	+2.2 26.1

+1.29%

End X. Sections

(+12.0) 31.0	+2.6 17.0	+3.2 16.0	+4.8 14.00	+4.7 6.0	+3.3 7.0	+2.8 22.0	+3.3 25.0	(+8.0) 26.5
(+7.8) 28.9	+6.7 25.0	+4.0 2.0	+3.5 7.0	+2.5 14.64 79.04 78.68		+2.8 25.0		(+6.7) 28.4
(+9.4) 29.7	+2.5 13.0	+2.3 11.0	+2.3 5.34 78.39 87.73					(+2.6) 26.3

STA.	+	H.I.	-	ht.	±	R.I.
62+00				$\frac{+13.7}{32.3}$	$\frac{+0.6}{4.41}$ 86.78	$\frac{19}{-2.7}$ 89.4
+50				$\frac{+14.1}{32.7}$	$\frac{-1.0}{5.06}$ 86.13	$\frac{-9.2}{38.6}$
61+00				$\frac{+20.1}{35.7}$	$\frac{+0.1}{5.70}$ 85.49	$\frac{-22.7}{58.9}$
+50				$\frac{+13.9}{32.2}$	$\frac{-2.7}{6.35}$ 84.84	$\frac{-25.9}{63.7}$
60+00				$\frac{+21}{29.7}$	$\frac{-4.0}{6.99}$ 84.20	$\frac{-25.5}{63.1}$
+50				$\frac{+8.8}{29.4}$	$\frac{-4.0}{7.64}$ 83.55 21.19	$\frac{-23.2}{59.6}$
T.P.	7.31	91.19	13.07	83.88		
59+00				$\frac{+11.8}{30.9}$	$\frac{-2.6}{14.04}$ 82.91 86.95	$\frac{-16.6}{49.7}$
		90.95				

+1.29%

STA.	+	H.I.	-
65+50			
cht. on d stub 66+50			
		2.3	$\frac{0.0 = \text{Error.}}{97.7 = \text{Elev. Stub.}}$ 97.7
65+00			
+50			
64+00			
+50			
63+00			
62+50			
TP	940	100.02 91.19	0.57 90.62

Lt.	C	Rt.
$\frac{+134}{31.7}$	$\frac{+4.9}{8.73}$ 91.29	20 $\frac{+0.0}{25.0}$
$\frac{+174}{33.7}$	$\frac{+5.0}{9.37}$ 90.65	$\frac{-6.1}{31.9}$
$\frac{+18.6}{34.3}$	$\frac{+5.6}{10.02}$ 90.00	$\frac{7.8}{35.6}$
$\frac{+13.2}{31.6}$	$\frac{+3.2}{10.66}$ 89.36	$\frac{-10.4}{40.4}$
$\frac{+8.1}{29.1}$	$\frac{+0.5}{11.31}$ 88.71	$\frac{-10.4}{40.4}$
$\frac{+14.1}{32.0}$	$\frac{+2.6}{11.55}$ 88.07	$\frac{-10.3}{40.3}$
$\frac{+6.1}{35.6}$	$\frac{+4.9}{12.60}$ 87.42 100.02	$\frac{-9.9}{39.7}$

STA.	+	H.I.	-	-
68+50				
68+00				
	+79.50			
67+77.95	=	B.C. LT.		
67+50				
67+00				
T.P.	10.31	109.85	1.00	99.54
+50				
TP	12.68	100.54	1.00	87.86
66+00				
	12.53	88.86		76.33

B.M. #4 2' x 2' 1/2"
140' x 66' x 26'

Lt.	£	Rt.
+132 37.6	+137 31.9	+21 71.69 95.16
+127 32.4	+152 32.6	+79 153.3 24.52
+162 33.1	+110.0	+5.3 27.7
+147 32.1	+84 16.62 93.23 109.85	+4.3 27.2
+112 30.6	+59 7.96 92.58	+2.3 26.2
+124 31.2	+58 8.60 91.94 100.54	+0.7 25.4

Note: in this curve
 Rt. Side 1.0' higher than L.
 Lt. " 1.0' lower " "

STA.	+	H.I.	-
71 + 50			
71 + 00			
70 + 50			
70 + 12.77 = E.C.			
70 + 00			
69 + 50			
T.P.	9.12	107.02	11.95 97.90
69 + 00		109.85	

Lt.	±	St. 22
$\frac{+78}{28.9}$	$\frac{-14}{7.99}$ 99.03	$\frac{-23}{28.3}$
$\frac{+92}{29.6}$	$\frac{-3.1}{8.63}$ 98.39	$\frac{-13.0}{44.3}$
$\frac{+124}{32.2}$	$\frac{-3.5}{9.28}$ 97.74	$\frac{-18.8}{53.0}$
$\frac{+148}{33.1}$ $\frac{+15.3}{32.7}$	$\frac{-44}{9.92}$ 97.10	$\frac{-22.9}{59.2}$ $\frac{-22.4}{58.4}$
$\frac{+143}{32.2}$ $\frac{+14.8}{32.4}$	$\frac{-2.9}{10.57}$ 96.45 97.02	$\frac{-21.2}{54.6}$ $\frac{-20.7}{55.8}$
$\frac{+160}{33.0}$ $\frac{+16.5}{33.3}$	$\frac{+1.0}{14.04}$ 95.81 109.85	$\frac{-14.9}{47.2}$ $\frac{-14.4}{46.4}$

+1.29%

Note: in this curve
 1/2" side 1.0" higher than E.
 1/4" 1.0" lower

STA.	+	H.I.	-
74 + 50			
74 + 00			
+ 50			
+ 11.59 73 + 10.19 = B.C.			
73 + 00			
72 + 50			
	14.54	120.42	114 105.88
72 + 00			
		107.02	

Lt.	E	Rt.
+27.6 38.8	+27.4 38.7	+6.8 77.52 102.90
+13.6 34.8	+13.4 34.7	+8.8 18.16 102.26
+22.1 36.0	+21.9 35.9	+13.1 18.81 101.61
+20.2 35.1	+13.6	0.0 daylight 38.5
+17.4 33.7	+14.5	0.0 } daylight 20.10 100.32 120.42
+12.3 31.2	+4.7	-1.5 27.0

+ 10.0%

23
106 + 0.4
25.3 25.2

-0.2
25.1

0.0 daylight
34.2

0.0 daylight
38.5

0.0 } daylight
20.10
100.32
120.42

-1.5
27.0

Note: in the Curve
of Super

STA.	+	H.I.	-
78+00			
+50			
77+00			
+50			
T.P.			
76+00	1.33	109.90	11.85 108.57
+50			
75+00			

120.42

L	E	Pt.
+10.5 30.3	+10.3 30.2	10.0 24 39.8 40.1
-5.2 32.6	(5.4) 32.9	(3.7) -34.9 72.6 72.8
-1.8 5.5	(2.0) 37.8	(7.4) -14.2 46.6 46.1
+21.2 35.6	(21.0) 35.5	+0.2 25.1 25.0
+31.3 41.0	(31.7) 40.5	+13.3 15.58 104.84
+36.0 43.0	(35.8) 42.9	+12.9 16.23 104.19
+33.6 47.8	(33.4) 41.7	+8.0 16.87 103.55 120.42
		(1.7) +1.5 25.8 25.8
		(0.7) +0.5 25.3 25.3

% G.S.I.

Note: in this curve of 'Support'

STA.	+	H.F.	-
81+50			
81+00			
+50			
80+00			
79+50			
T.P.	8.50	118.36	0.04 109.86
79+00			
78+50			
		109.90	

Lt	±	Pt
$\frac{+11.1}{30.6} \frac{+1.09}{30.5}$	$\frac{+0.8}{6.46}$ 111.90	$\frac{+0.7}{25.7} \frac{+0.5}{25.2}$
$\frac{+11.2}{30.6} \frac{+1.0}{30.8}$	$\frac{+0.9}{7.07}$ 111.29	$\frac{+1.2}{26} \frac{+1.0}{25.8}$
$\frac{+10.0}{30.0} \frac{+0.8}{29.9}$	$\frac{+1.1}{7.72}$ 110.64	$\frac{-0.0}{30.8} \frac{-0.2}{24.1}$
$\frac{+10.0}{30.0} \frac{+0.8}{29.9}$	$\frac{+1.4}{8.36}$ 110.00	$\frac{-1.9}{24.5} \frac{-1.9}{24.6}$
$\frac{+11.4}{30.7} \frac{+1.2}{30.6}$	$\frac{+0.9}{9.01}$ 109.35 118.36	$\frac{-2.6}{24.4} \frac{-2.6}{24.7}$
$\frac{+10.9}{30.5} \frac{+1.07}{30.4}$	$\frac{+0.2}{1.19}$ 108.71	$\frac{-4.0}{24.7} \frac{-4.2}{25.1}$
$\frac{+10.0}{30.0} \frac{+0.8}{29.9}$	$\frac{-0.8}{1.84}$ 108.06 109.90	$\frac{-3.1}{23.5} \frac{-3.3}{23.8}$

200 W.

+1.29%

Note: in this curve of sight.

STA. + H.I. -

+ 85.30
84 + 8836 = PCC

+50

84 + 00

+50

83 + 00

12.70 104.85

92.15 BM #5

85' Ht
84+8836
on RL

T.P. 11.69 116.18 0.36 104.49

+50

chk. on 2 sub. 83+00

5.1

0.0 = Error
113.3 = Sub.
113.3

82 + 00

11836

Lt.

£

Ht.

26

$\frac{-0.3}{25.3} = \frac{0.5}{25.6}$

$\frac{-2.8}{218}$
114.00

$\frac{13.2}{44.6} = \frac{13.4}{44.5}$

$\frac{+0.7}{25.7} = \frac{+0.5}{25.3}$

$\frac{-0.2}{246}$
113.72

$\frac{10.6}{40.7} = \frac{10.8}{41.0}$

+0.57 90

$\frac{75.0}{26.6} = \frac{+2.8}{26.7}$

$\frac{+0.2}{275}$
113.43

$\frac{6.4}{34.4} = \frac{-6.6}{34.7}$

$\frac{12.7}{26.3} = \frac{13.6}{26.8}$

$\frac{+0.2}{303}$
113.15
~~116.18~~

$\frac{5.1}{32.5} = \frac{-5.3}{32.8}$

$\frac{+6.8}{28.4} = \frac{+6.6}{28.3}$

$\frac{+0.4}{5.53}$
112.83

$\frac{-3.5}{38.1} = \frac{-3.7}{38.4}$

$\frac{+3.8}{29.9} = \frac{+2.6}{29.8}$

$\frac{+0.5}{5.96}$
112.40
11836

$\frac{-3.0}{29.3} = \frac{-3.2}{29.6}$

Note: 10 has same 94 Support.

STA.	+	H.I.	-
88+00			

Lt.	£
$\frac{41}{30.9}$ $\frac{43}{31.2}$	$\frac{7.0}{5.44}$ 116.00 121.44

Rt.
$\frac{-126}{43.7}$ $\frac{27}{-128}$ 44.0

T.P.	11.61	121.44	6.35	109.83
------	-------	--------	------	--------

$\frac{-14}{56.9}$ $\frac{-16}{27.2}$	$\frac{-6.7}{0.47}$ 115.71	$\frac{-11.8}{43.5}$ $\frac{-12.0}{42.8}$
---------------------------------------	-------------------------------	---

87+50

$\frac{-0.7}{25.9}$ $\frac{-0.9}{26.2}$	$\frac{-6.9}{0.75}$ 115.43	$\frac{-13.4}{44.5}$ $\frac{-12.6}{45.2}$
---	-------------------------------	---

87+00

$\frac{-0.1}{24.9}$ $\frac{-0.4}{25.4}$	$\frac{-7.9}{1.04}$ 115.14	$\frac{-14.5}{46.6}$ $\frac{-14.7}{46.9}$
---	-------------------------------	---

+50

+0.57%

$\frac{+0.2}{25.1}$ $\frac{0.0}{25.0}$	$\frac{-5.3}{1.32}$ 114.86	$\frac{-14.0}{46.7}$ $\frac{-14.8}{47.0}$
--	-------------------------------	---

86+00

$\frac{-0.2}{25.1}$ $\frac{-0.4}{25.4}$	$\frac{-4.6}{1.61}$ 114.57	$\frac{-14.2}{46.1}$ $\frac{-14.4}{46.4}$
---	-------------------------------	---

+50

$\frac{-0.4}{25.4}$ $\frac{-0.6}{25.7}$	$\frac{-3.6}{1.89}$ 114.29 116.18	$\frac{-13.0}{44}$ $\frac{-13.2}{44.6}$
---	---	---

85+00

116.18

Note: in the Curve 0.4' Supers

STA. + H.I. -

91+50

Lt.
 $\frac{-0.4}{25.4}$ $\frac{-0.6}{26.7}$

Σ
 $\frac{-5.4}{3.45}$
 117.99

28.1
 $\frac{-11.4}{41.9}$ $\frac{-11.6}{42.2}$

91+00

$\frac{0.0}{25.0}$ $\frac{0.1}{24.9}$

$\frac{-6.4}{3.73}$
 117.71

$\frac{-3.5}{39.1}$ $\frac{-2.7}{39.4}$

90+50

$\frac{-1.3}{26.8}$ $\frac{-1.5}{27.1}$

$\frac{-4.6}{2.02}$
 117.42

$\frac{-2.7}{39.4}$ $\frac{-2.9}{39.7}$

90+00

$\frac{-2.2}{25.2}$ $\frac{-3.1}{25.5}$

$\frac{-6.0}{4.30}$
 117.14

$\frac{-5.7}{39.4}$ $\frac{-9.9}{39.7}$

10.57%

+50

$\frac{-5.2}{22.6}$ $\frac{-5.4}{22.9}$

$\frac{-7.5}{4.59}$
 116.85

$\frac{-11.5}{42.1}$ $\frac{-11.7}{42.4}$

89+00

$\frac{-5.1}{22.5}$ $\frac{-5.8}{22.8}$

$\frac{-8.7}{4.87}$
 116.57

$\frac{-12.9}{44.7}$ $\frac{-13.1}{44.5}$

88+50

$\frac{-3.0}{29.3}$ $\frac{-3.2}{29.6}$

$\frac{-2.7}{5.16}$
 116.28
 121.44

$\frac{-12.9}{44.1}$ $\frac{-13.1}{44.4}$

121.44

Note: 12 hrs Curve 24" Super

STA.	+	H.I.	-
95+00 = P.V.C			
+50			
T.P.	11.20	142.50	131.30
94+00			
+50			
T.P.	12.44	132.56	120.12
93+00			
+50			
92+00		121.44	

200 V.C

Lt	±	#1	#2
+58.0 + 58.2 54.0 54.2	+21.6 22.51 119.99	-1.6 27.2	-1.8 27.5
+51.7 + 51.5 50.9 50.8	+16.9 22.80 119.70 142.50	-1.7 27.4	-1.9 27.7
+36.6 + 35.7 43.3 42.9	+12.1 13.14 119.42	-1.6 27.2	-1.8 27.5
+33.2 + 23.0 36.6 36.5	+6.0 13.43 119.13 122.56	-1.5 27.1	-1.7 27.4
+12.4 + 12.2 7.2 7.1	-1.5 2.59 118.85	-1.6 27.8	-1.9 27.1
+3.1 + 2.9 26.5 26.4	-1.6 2.88 118.56	-1.6 28.3	-1.8 28.6
-1.8 - 1.2 26.5 26.6	-4.1 3.16 118.28 121.44	-1.1 26.0	-1.3 26.3

+0.57%

Note: in this case of Super

STA.	+	H.I.	-
98+50			
98+00			
+50	12.57	112.97	100.40
97+00			
T.P.	1.28	120.02	11.99 118.74
+50			
96+00			
T.P.	0.69	130.73	12.46 130.04
95+50		142.50	

BM #6 = 2' x 2' 1/2" 4x6
46' Bl. 98135

300 V.C. 0.506%

Lt.	E	Rt.
$\frac{-42}{37.1} \frac{-47}{31.9}$	-2.9 +6.3 119.29	$\frac{-121}{43.0} \frac{30}{12.5} \frac{-16.3}{43.3}$
$\frac{-115}{42.0} \frac{-130}{44.3}$	-15.7 +6.57 119.54 112.97	$\frac{-126}{43.7} \frac{-16.6}{45.7}$
$\frac{-34}{29.9} \frac{-36}{30.2}$	-7.1 +0.22 119.80	$\frac{-108}{40.4} \frac{-10.6}{40.7}$
$\frac{-71}{26.5} \frac{-13}{26.8}$	-4.9 +0.03 120.05 120.02	$\frac{-108}{40.6} \frac{-10.7}{40.9}$
$\frac{+88}{29.4} \frac{+86}{29.3}$	-1.5 10.19 120.74	$\frac{-10.7}{40.9} \frac{-10.9}{41.2}$
$\frac{+166.8}{38.4} \frac{+26.6}{39.3}$	+3.3 10.44 120.29 120.73	$\frac{-11.4}{26.3} \frac{-16}{27.2}$
$\frac{+254}{47.7} \frac{+252}{47.6}$	+16.3 22.29 130.21 142.50	$\frac{-15}{27.1} \frac{-1.7}{27.4}$

Note: in this curve of Super Elevation

STA. + H.I. -

+59.14
101 +57.83 = E.C.

+50

T.P. 13.04 125.31 0.70 112.27

101 +00

+50

100 +00

+50

99 +00

112.27

Lt.

+2.2
26.1

+2.0
26.0

+2.0
26.0

+1.8
25.9

+1.5
25.8

+1.3
25.7

+1.4
25.7

+1.2
25.6

+1.1
26.4

+1.3
26.7

+1.4
31.4

+1.6
31.7

Rt.

-3.3
7.54

117.77

-6.8
+5.06

118.03

-7.6
+5.31

118.28

-5.3
+5.56

118.53

-6.3
+5.81

118.78

-9.6
+6.07

119.04

118.97

Rt.

31

-22.6
58.7

-22.8
59.0

-19.4
53.5

-19.6
54.2

-15.8
48.5

-16.0
48.8

-12.8
44.0

-13.0
44.3

-11.7
42.3

-11.9
42.6

-12.7
43.9

-12.9
44.2

Note: in this curve of Super

STA.	+	H.I.	-
104+50			
	11.18	135.62	0.87 124.44
104+00			
+50			
+34.78			
103+33 ²⁷ = B.C.			
103+00 = P.V.C.			
+50			
102+00		125.31	

Lt.	Σ	Rt.
131.9 + 32.4 41.0 41.2	195 138.4 115.78 135.62	32 40.9 + 7.4 25.2 25.7
+24.6 + 25.1 37.3 37.6	+56 7.01 116.30	-150 47.3 47.6
+20.6 + 21.1 38.3 35.5	+53 8.60 116.71	213 50.6 56.8 49
+15.5 32.8	+37 8.29 117.02	-22.1 57.9
+10.2 30.1	+0.4 8.04 117.27	-24.7 61.9
+1.9 26.6	-1.0 7.79 117.52 125.31	-24.5 61.6

600 V.C.

-0.506%

Note: in this curve
Rt. side 1.0 Higher than L.
Lt. " 1.0 Lower " " } And Cont. to E.C.

STA.

108+00

+50

107+00

7.12 114.83

107.71 110.84 107+00

+50

Re. chk. on 2 stub 107+00

15.5

0.2 error
113.5
113.6

106+00

TP 0.45 129.11 11.29 128.66

+50

105+00

5.59 140.65 0.56 135.06
135.62

Lt.

Rt.

Rt.

12.0
26.5

13.5
26.8

11.3
55.4
109.29

0.9
26.2

33
0.9
26.4

14.7
27.1

14.7
27.4

12.5
4.30
110.53

0.3
25.3

1.02
25.1

11.8
25.3

11.6
25.1

12.6
3.16
111.67
114.83

1.3
28.2

1.8
28.5

15.7
28.0

16.4
28.2

11.6
16.41
112.70

1.6
36.2

1.7
33.4

12.8
29.0

12.6
29.3

11.8
15.48
113.63
129.11

1.7
25.9

1.8
26.1

14.4
45.2

14.9
45.5

12.6
26.20
114.45

1.5
29.2

1.8
29.4

14.0
47.0

14.5
47.3

10.8
25.48
115.17
140.65

1.3
28.7

1.8
28.9

500' VC

Super Elev. = 0.4' per ft.
Note: 10' this curve
Rt. Side 1.0' higher than L.
Lt. " 1.0' lower " "

STA.	+	H.I.	-
111 + 50			
111 + 00			
T.P.	0.41	103.65	11.59 103.24
+ 50			
110 + 00			
+ 50			
109 + 00			
108 + 50			

114.83

LT.	ℓ	H.
$\begin{array}{r} +30 \\ 265 \end{array} \quad \begin{array}{r} +35 \\ 267 \end{array}$	$\begin{array}{r} +0.2 \\ 4.58 \\ 99.07 \end{array} \checkmark$	$\begin{array}{r} 34 \\ -26 \\ 287 \\ 27.9 \end{array}$
$\begin{array}{r} +31 \\ 265 \end{array} \quad \begin{array}{r} +36 \\ 268 \end{array}$	$\begin{array}{r} +0.3 \\ 3.15 \\ 100.50 \\ 103.65 \end{array} \checkmark$	$\begin{array}{r} +2.3 \\ 283 \\ 27.5 \end{array} \quad -7.8$
$\begin{array}{r} +29 \\ 265 \end{array} \quad \begin{array}{r} +32 \\ 267 \end{array}$	$\begin{array}{r} +0.9 \\ 12.83 \\ 102.00 \end{array}$	$\begin{array}{r} -1.9 \\ 277 \\ 26.9 \end{array} \quad -1.2$
$\begin{array}{r} +28 \\ 264 \end{array} \quad \begin{array}{r} +32 \\ 266 \end{array}$	$\begin{array}{r} +0.6 \\ 11.33 \\ 103.50 \end{array} \checkmark$	$\begin{array}{r} 22 \\ 281 \\ 27.7 \end{array} \quad -1.9$
$\begin{array}{r} +19 \\ 260 \end{array} \quad \begin{array}{r} +24 \\ 263 \end{array}$	$\begin{array}{r} -0.1 \\ 9.83 \\ 105.00 \end{array}$	$\begin{array}{r} -2.4 \\ 284 \\ 27.7 \end{array} \quad -1.9$
$\begin{array}{r} +0.8 \\ 254 \end{array} \quad \begin{array}{r} +1.3 \\ 257 \end{array}$	$\begin{array}{r} -0.4 \\ 8.33 \\ 106.50 \end{array}$	$\begin{array}{r} -2.8 \\ 290 \\ 28.3 \end{array} \quad -2.5$
$\begin{array}{r} +1.8 \\ 259 \end{array} \quad \begin{array}{r} +2.3 \\ 262 \end{array}$	$\begin{array}{r} +0.4 \\ 6.88 \\ 107.95 \\ 114.83 \end{array}$	$\begin{array}{r} -1.6 \\ 272 \\ 26.4 \end{array} \quad -7.1$

600 Y.C.

-3.00 %

Note: in this curve
 10' side 10' higher than
 10' lower than

STR.	+	H.F.	-
114 + 50			
114 + 00			
	9.15	95.82	86.67
			B.M. #8 520 P-36
113 + 81 ^{.10} ₃₄ = E.C.			
chk. 2 sub 114+00 +50		13.4	$\frac{0.0 = \text{Error.}}{90.2 = \text{Elev. Sta. 6}} \\ 90.2$
113 + 00			
+50			
112 + 00			
		10365	

1st	2	pt
$\frac{-30}{29.3}$	$\frac{-5.2}{2.07}$ 93.75	$\frac{35}{-6.8}$ 35.0
$\frac{-18}{27.5}$	$\frac{-4.0}{1.57}$ 94.25 95.82	$\frac{-7.2}{35.6}$
$\frac{-0.5}{25.6}$ (0.0) 25.0	$\frac{-3.1}{8.74}$ 94.91	$\frac{7.3}{35.8}$ -6.8 35.0
$\frac{+4.3}{25.2}$ (+0.8) 25.2	$\frac{-1.2}{7.93}$ 95.72	$\frac{5.7}{33.4}$ -5.2 33.6
$\frac{+7.4}{25.7}$ (+1.9) 26.0	$\frac{-1.1}{6.96}$ 96.69	$\frac{4.0}{30.8}$ -3.5 30.1
$\frac{25.4}{26.6}$ (2.9) 26.5	$\frac{-0.5}{5.84}$ 97.81 103.65	$\frac{3.6}{30.2}$ -3.1 29.5

600' V.C.

Note: in this Curve.
Pt. Side 1.0' Higher than
L. " 1.0' Lower " "

STA. + H.I. -

118 + 00

+ 50

117 + 00

+ 50

chf. on E stub 117+00

116 + 00

+ 50

115 + 00

13.00 99.67

1.4

95.82

BM # 8 - 2x14
86.67 100' H. 114+95

o.l. = Error.
94.5 - Stub
94.4

Lt

+ 0.67%

X

500' K.C.

$\frac{+3.5}{26.8}$

$\frac{+2.0}{26.0}$

$\frac{+3.0}{26.5}$

$\frac{+2.9}{25.5}$

$\frac{-2.4}{25.4}$

$\frac{-1.6}{27.2}$

$\frac{-2.1}{27.9}$

E

$\frac{+4.6}{54.9}$
94.18

$\frac{+0.5}{58.3}$
93.84

$\frac{+1.0}{61.6}$
93.51 ✓
~~93.67~~

$\frac{-0.9}{2.57}$
93.25

$\frac{-1.9}{2.67}$
93.15

$\frac{-3.1}{26.2}$
93.20

$\frac{-3.9}{2.43}$
93.39
95.82

H. 36

$\frac{-0.2}{25.1}$

$\frac{-0.9}{26.2}$

$\frac{-0.6}{25.7}$

$\frac{-2.4}{28.4}$

$\frac{-2.5}{30.1}$

$\frac{-4.8}{32.0}$

$\frac{-5.9}{33.6}$

STA.	+	H.I.	-
121+50			
121+00			
+50			
120+00			
+50			
T.P.	8.77	108.21	0.23 99.44
119+00			
118+50			
		99.67	

Lot	±	ff.
$\frac{+87}{294}$	$\frac{+5.1}{11.69}$ 26.52	37 $\frac{+8.6}{26.3}$
$\frac{+87}{294}$	$\frac{+5.9}{12.02}$ 26.19	$\frac{+3.6}{26.8}$
$\frac{+89}{295}$	$\frac{+5.9}{12.36}$ 25.85	$\frac{+4.0}{27.0}$
$\frac{+84}{292}$	$\frac{+5.7}{12.69}$ 25.52	$\frac{+3.3}{26.7}$
$\frac{+73}{286}$	$\frac{+5.2}{13.03}$ 35.18 108.21	$\frac{+2.9}{26.5}$
$\frac{+64}{282}$	$\frac{+4.6}{4.82}$ 24.85	$\frac{+2.6}{26.3}$
$\frac{+52}{276}$	$\frac{+3.6}{5.16}$ 24.51 99.67	$\frac{+1.4}{25.7}$

10.67%

STA.	+	H.I.	-
125+00			
+50			
124+00			
I.P.	5.01	100.81	12.41 25.80
+50			
123+00			
+50			
122+00			

108.21

Lt	±	38
$\frac{-47}{31.5}$	$\frac{-10.0}{7.94}$ 38.87	$\frac{-11.6}{42.2}$
$\frac{-34}{29.9}$	$\frac{-8.6}{2.28}$ 38.53	$\frac{-10.7}{40.8}$
$\frac{0.0}{25.0}$	$\frac{-3.5}{2.61}$ 38.20 <u>100.81</u>	$\frac{-8.3}{37.3}$
$\frac{+1.2}{25.6}$	$\frac{-1.0}{10.35}$ 37.86	$\frac{-7.5}{38.4}$
$\frac{+2.7}{26.4}$	$\frac{+0.5}{10.68}$ 37.53	$\frac{-1.8}{37.5}$
$\frac{+5.3}{27.7}$	$\frac{+2.6}{11.02}$ 37.19	$\frac{+1.0}{25.5}$
$\frac{+6.9}{28.5}$	$\frac{+4.1}{11.35}$ 36.86 108.31	$\frac{+2.0}{26.0}$

+0.67%

STA.	+	H.I.	-	Lt.	Σ	ft.
128+50				$\frac{-12}{76.6}$	$\frac{-2.8}{3.74}$ 101.21	39 $\frac{-4.7}{32.2}$
128+00				$\frac{-1.6}{57.6}$	$\frac{-3.1}{4.07}$ 100.88 104.25	$\frac{-5.6}{33.2}$
	10.99	104.35	93.96	B.M. #9 287.116 50' 81.66 128+11		
+50				$\frac{-2.9}{29.2}$	$\frac{-4.5}{0.77}$ 100.54	$\frac{-7.2}{35.6}$
	chk. on B.M. #9	6.86	$\frac{0.01 = \text{Error}}{93.96 - 87.10}$ 93.95			
127+00				$\frac{-1.6}{87.6}$	$\frac{-4.8}{0.60}$ 100.21	$\frac{-9.0}{38.2}$
+50				$\frac{-2.5}{28.6}$	$\frac{-2.1}{0.94}$ 99.87	$\frac{-11.5}{42.0}$
126+00				$\frac{-3.7}{30.4}$	$\frac{-8.9}{1.27}$ 99.54	$\frac{-11.8}{42.5}$
125+50				$\frac{-4.5}{31.4}$	$\frac{-10.6}{1.61}$ 99.20 100.81	$\frac{-12.0}{42.8}$
	100.81					

+ 0.67%

STR.	+	H.F.	-
131+50			
131+00			
+50			
130+00			
T.P.	12.54	114.14	335 101.60
+50			
129+00			
+57.31			
128+55.95			B.C.
			104.95

Nail in fence post
50' R+
130+50

10.67%

L4	E	FF.
$\frac{+18}{26.6} \frac{+36}{26.9}$	$\frac{+14}{1092}$ 103.22	$\frac{40}{25.3} \frac{8.9}{25.0}$
$\frac{+16}{25.9} \frac{+3}{26.1}$	$\frac{+0.4}{11.25}$ 102.89	$\frac{+1.8}{27.5} \frac{-1.3}{28.8}$
$\frac{+20}{25.5} \frac{+14}{25.7}$	$\frac{-0.8}{11.59}$ 102.55 102.12	$\frac{-3.1}{29.5} \frac{-7.6}{28.7}$
$\frac{+9}{25.0} \frac{+0.6}{25.3}$	$\frac{-1.7}{2.73}$ 102.22	$\frac{-4.5}{31.6} \frac{-4.0}{30.8}$
$\frac{+9}{25.0} \frac{+0.6}{25.3}$	$\frac{-2.1}{3.07}$ 101.88	$\frac{-1.0}{32.3} \frac{-4.5}{31.6}$
$\frac{-1.2}{25.1} \frac{+0.3}{25.1}$	$\frac{-2.1}{3.40}$ 101.55 104.95	$\frac{-5.2}{32.6} \frac{-4.7}{31.0}$

Note: in this curve
FF. stake is 1.0' Higher than E
L4 " " 1.0' Lower " "

Super = 0.4' per. ft.

STA. + H.I. -

134 +50

$\frac{+10.4}{30.2}$

$\frac{+17.4}{8.91}$
105.23

FA.
41
 $\frac{+15.3}{27.6}$

134 +00

$\frac{+12.2}{29.6}$

$\frac{+16.8}{9.24}$
104.90

$\frac{+14.6}{27.3}$

+50

$\frac{+17.8}{28.9}$

$\frac{+15.6}{9.58}$
104.56

$\frac{+13.6}{26.8}$

133 +00

+ 0.67 %
 $\frac{+17.3}{28.7}$

$\frac{+14.8}{9.91}$
104.23

$\frac{+12.6}{26.3}$

+9713
132+9577 EC.

+50

$\frac{+16.3}{28.2}$ (16.8)
28.4

$\frac{+13.4}{10.25}$
103.89

(10.6) $\frac{+11.8}{28.7}$
28.4

132 +00

$\frac{+4.1}{27.0}$ (4.6)
27.3

$\frac{+2.4}{10.58}$
103.56
114.14

(10.2) $\frac{+10.7}{25.4}$
25.1

114.14

STP. + H.F. -

138+00

+50

137+00

TP 4.89 116.44 2.59 111.55

+50

136+00

+50

135+00

119.14

Lt.

$\frac{+27}{76.4}$

$\frac{+151}{27.5}$

$\frac{+77}{28.7}$

$\frac{+83}{29.2}$

$\frac{+9.7}{29.9}$

$\frac{+109}{30.5}$

$\frac{+110}{30.5}$

0.67%

E

$\frac{+08}{8.87}$
107.54

$\frac{+25}{9.20}$
107.24

$\frac{+3.9}{9.54}$
106.90
116.44

$\frac{+5.1}{7.57}$
106.57

$\frac{+5.8}{7.91}$
106.23

$\frac{+7.5}{8.24}$
105.90

$\frac{+7.9}{8.58}$
105.56
114.14

Rt.
42

$\frac{-20}{27.8}$

$\frac{-0.3}{25.3}$

$\frac{+1.0}{25.5}$

$\frac{+2.1}{26.1}$

$\frac{+2.7}{26.4}$

$\frac{+3.9}{27.0}$

$\frac{+5.4}{27.7}$

STN.	+	H.I.	-
141+50			
141+00			
+50	6.12	115.92	109.80
			B.M. #10 2 1/2" hb 50' H. Sta. 144+00
140+00			
+50			
139+00			
			0.0 = Error 103.3 = Elev. Stub
	Chiron L. Sta 141+00		6.8 103.3
T.P.	5.45	110.14	11.75 104.69
138+50		116.44	

Lt	±	Rt
-50 32.3	58 6.16 109.76	43 -64 34.4
-53 32.9	62 6.37 109.55 115.92	-67 34.9
-46 31.7	54 4.89 109.25	-6.5 34.6
-38 30.5	46 1.73 108.91	-6.0 33.8
-32 29.6	45 1.56 108.58	-5.5 33.1
-17 27.4	42 1.90 108.24 110.14	-5.0 32.3
+03 28.2	1.5 8.53 107.91 116.44	-3.8 30.5

Sta.	+	H.F.	-	Lt.	℄	Rt.
145+00				$\frac{+6.3}{28.2}$	$\frac{+4.0}{4.69}$ 111.23	$\frac{44}{12.5}$ 76.3
+50				$\frac{+4.6}{27.3}$	$\frac{+2.6}{4.90}$ 111.02	$\frac{+4.2}{25.6}$
144+00				$\frac{+2.4}{26.2}$	$\frac{+0.9}{5.11}$ 110.81	$\frac{-0.4}{25.7}$
+50				$\frac{+0.3}{25.2}$	$\frac{-1.0}{5.32}$ 110.60	$\frac{-1.9}{27.7}$
143+00				$\frac{-1.5}{27.1}$	$\frac{-3.0}{5.53}$ 110.39	$\frac{-3.8}{30.9}$
+50				$\frac{-2.8}{29.0}$	$\frac{-4.0}{5.74}$ 110.18	$\frac{-4.7}{31.9}$
142+00				$\frac{-4.0}{30.8}$	$\frac{-5.0}{5.95}$ 109.97 115.92	$\frac{-5.6}{33.2}$
		115.92				

+ 0.42.90

STY.	+	H.F.	-
148+00			
+50			
147+00			
+61.43 146+59.99		B.C. FT.	
+50			
146+00			
145+50			
T.P.	9.30	124.12	110 114.82
		115.92	

Lt.	♀	#45
$\frac{761}{28.1}$ $\frac{+56}{27.8}$ $\frac{+50}{27.5}$	$\frac{14.7}{11.63}$ 112.49	$\frac{+43}{27.2}$ $\frac{+32}{26.6}$ $\frac{+37}{26.9}$
$\frac{+64}{28.2}$ $\frac{+58}{27.9}$ $\frac{+52}{27.6}$	$\frac{+51}{11.84}$ 112.28	$\frac{+47}{27.4}$ $\frac{+36}{26.8}$ $\frac{+41}{27.0}$
$\frac{+60}{28.0}$ $\frac{+55}{27.8}$ $\frac{+45}{27.3}$	$\frac{+4.6}{12.05}$ 112.07	$\frac{+51}{27.6}$ $\frac{+30}{27.0}$ $\frac{+45}{27.3}$
$\frac{+72}{28.6}$	$\frac{+40}{12.26}$ 11.86	$\frac{+20}{26.0}$
$\frac{+80}{29.0}$	$\frac{+5.5}{12.47}$ 11.65	$\frac{+34}{26.7}$
$\frac{+77}{28.9}$	$\frac{+5.1}{12.68}$ 11.44 124.12	$\frac{+33}{26.7}$

+0.42%

3.2 Super. in this course

STR.	+	H.I.	-
151+50			
151+00			
+50			
150+00			
+50			
T.P.	9.36	132.25	122.89
149+00			
148+50			

124.12

L.H.	\$	Pt.
$\frac{+11.8}{30.9}$ $\frac{+11.2}{30.6}$ $\frac{+10.6}{30.3}$	$\frac{+8.7}{18.29}$ 18.96	$\frac{+6.6}{28.9}$ $\frac{+5.6}{27.8}$ $\frac{+4.0}{28.0}$
$\frac{+1.6}{33.0}$ $\frac{+1.6}{32.3}$ $\frac{+1.0}{32.0}$	$\frac{+1.1}{18.50}$ 113.75	$\frac{+3.0}{33.5}$ $\frac{+2.4}{32.2}$
$\frac{+1.1}{33.6}$ $\frac{+1.4}{33.2}$ $\frac{+1.5}{32.9}$	$\frac{+1.2}{18.71}$ 113.54	$\frac{+3.9}{30.9}$ $\frac{+3.8}{29.4}$ $\frac{+2.8}{29.7}$
$\frac{+1.7}{33.5}$ $\frac{+1.4}{33.2}$ $\frac{+1.5}{32.9}$	$\frac{+1.2}{18.92}$ 113.33	$\frac{+1.4}{30.2}$ $\frac{+3.2}{29.6}$ $\frac{+2.8}{29.5}$
$\frac{+1.5}{33.8}$ $\frac{+1.5}{32.6}$ $\frac{+1.5}{32.3}$	$\frac{+1.1}{19.13}$ 113.12 132.25	$\frac{+2.7}{29.9}$ $\frac{+3.6}{29.3}$ $\frac{+2.1}{29.6}$
$\frac{+1.2}{31.0}$ $\frac{+1.5}{30.8}$ $\frac{+1.0}{30.5}$	$\frac{+1.9}{11.21}$ 112.91	$\frac{+8.3}{29.2}$ $\frac{+7.2}{29.6}$ $\frac{+7.7}{28.9}$
$\frac{+8.1}{29.1}$ $\frac{+7.7}{28.9}$ $\frac{+7.1}{28.6}$	$\frac{+6.7}{11.42}$ 112.70 124.12	$\frac{+6.0}{28.0}$ $\frac{+4.8}{27.4}$ $\frac{+3.4}{27.1}$

3.2' Super in this Curve (Left Right)

STA.	+	H.I.	-	Lt.	£	Rt.
158+50				-2.2 28.1	-1.5 3.50 116.90	48 -1.9 27.7

158+00				-3.0 27.3	-2.1 3.77 116.69	-0.9 26.2
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+50				-2.0 27.8	-0.8 3.98 116.48	-0.8 26.0
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157+00				-4.8 32.0	-2.7 4.19 116.27	-0.9 26.2
--------	--	--	--	--------------	------------------------	--------------

+67.0/ 156+65.57 E.C. +50				-5.8 32.8	-5.7 33.2	-6.5 34.3	-4.8 4.40 116.96	(3.9) 30.7	-5.0 32.9	-4.5 31.6
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156+00				-4.7 32.3	(5.2) 32.6	(5.5) 32.1	-5.7 4.61 115.85	(4.2) 31.1	-5.5 32.1	(4.8) 32.0
--------	--	--	--	--------------	---------------	---------------	------------------------	---------------	--------------	---------------

155+50				-5.1 32.4	(5.4) 32.9	(6.0) 33.8	-4.7 4.82 115.64 120.46	(5.7) 30.4	-5.1 32.5	(4.3) 31.3
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120.46

+0.42 9/6



Note: in this curve
 Pt. side 1.6 lower than
 Lt. + 1.0 Higher

STH.	+	H.I.	-
162+00			
+50			
161+00			
+50			
160+00			
+50			
TP 159+00	313	123.97 120.46	5.62 114.84

400' Y.C.

lot	\$	Rt
$\frac{-2.5}{28.6}$	$\frac{-9.6}{3.95}$ 128.02	49 $\frac{-10.8}{41.0}$
$\frac{-10.8}{41.0}$	$\frac{-5.9}{4.66}$ 119.31	$\frac{-2.6}{28.7}$
$\frac{-1.9}{2.9}$	$\frac{-1.9}{5.28}$ 118.69	$\frac{-2.1}{27.7}$
left out	$\frac{-2.1}{3.82}$ 118.15	$\frac{-2.0}{27.8}$
$\frac{-2.2}{28.1}$	$\frac{-1.4}{6.26}$ 117.71	$\frac{-1.7}{27.3}$
$\frac{-2.7}{28.3}$	$\frac{-2.6}{6.60}$ 117.37	$\frac{-0.9}{26.2}$
$\frac{-3.1}{29.5}$	$\frac{-2.9}{6.86}$ 117.11 123.97	$\frac{-1.2}{26.8}$

STA.	+	H.I.	-
165+00			
164+60			
164+50			
+16.33			
164+14.57 = BC Lt.			
164+00			
+50			
163+00 = E.V.C.			
T.P.	12.78	139.06	1.68
	11.03	127.96	
162+50			
chk. on 2 stakes 163+00			
		0.9	
			123.97

Lt.	±	Rt.
$\frac{+11.5}{30.7}$ $\frac{+12.0}{31.0}$	+7.2 13.50 125.56	$\frac{+3.4}{26.7}$ $\frac{+7.9}{26.9}$
$\frac{+10.0}{30.0}$ $\frac{+10.5}{30.2}$	+7.1 14.20 124.80	$\frac{+3.3}{26.7}$ $\frac{+3.8}{26.9}$
	Left out 14.45 124.61	
	Left out.	
$\frac{+5.7}{27.5}$	$\frac{+3.6}{15.39}$ 123.67	$\frac{+2.6}{26.3}$
$\frac{+5.8}{27.9}$	$\frac{+3.0}{16.34}$ 122.72	$\frac{+0.7}{25.3}$
$\frac{+1.9}{26.0}$	$\frac{+1.2}{17.28}$ 121.78	$\frac{-0.4}{25.4}$
$\frac{+7.47}{121.57} = 162+90$	121.06	
$\frac{-0.5}{25.6}$	3.13 120.84 123.97	$\frac{-8.5}{27.6}$

1.85%

400 Y.C.

Note: In this curve
the side is 1.0 ft. from
the " " " " " " " "

STN.	+	H.I.	-
168+50			
168+00			
+50			
167+00			
T.P.	3.85	152.62	1.14 148.77
166+50			
T.P.	12.94	149.91	2.09 136.97
166+00			
165+50			

139.06

Temp. P.M. on bench
20' H. 166+75

166+11

Let	±	Rt.
$\frac{+12.3}{30.8} / \frac{+23.6}{30.9}$	$\frac{+15.6}{20.45}$ 132.17	$\frac{+11.8}{27.8}$ $\frac{+11.8}{27.9}$
$\frac{+22.3}{30.6} / \frac{+22.8}{30.7}$	$\frac{+17.5}{21.39}$ 131.23	$\frac{+14.8}{28.7}$ $\frac{+15.3}{28.8}$
$\frac{+28.3}{32.1} / \frac{+28.8}{32.2}$	$\frac{+21.6}{22.34}$ 130.28	$\frac{+16.1}{29.0}$ $\frac{+16.6}{23.1}$
$\frac{+30.3}{32.6} / \frac{+30.8}{32.7}$	$\frac{+22.7}{23.28}$ 129.34 152.62	$\frac{+14.6}{28.7}$ $\frac{+15.1}{28.8}$
$\frac{+26.8}{31.7} / \frac{+27.3}{31.8}$	$\frac{+17.8}{21.52}$ 128.39 149.91	$\frac{+10.9}{27.5}$ $\frac{+10.5}{27.6}$
$\frac{+17.6}{29.4} / \frac{+18.1}{29.5}$	$\frac{+10.4}{11.61}$ 127.45	$\frac{+4.1}{26.0}$ $\frac{+4.6}{26.7}$
$\frac{+12.0}{31.0} / \frac{+12.5}{31.2}$	$\frac{+6.3}{12.50}$ 126.50 139.06	$\frac{+2.4}{26.3}$ $\frac{+2.9}{26.5}$

Note: cut slopes are 1:1

Note: this corner
cut side is 10' lower than
RT " 10' higher

STA.	+	H.I.	-	Lt.	Σ	Pt.
172+00				+1.7 28.9	+2.2 26.1	-2.6 13.83 38.79
						(6.7) -6.2 34.9 34.1
+50				+4.5 27.3	+5.0 27.5	-0.2 14.78 137.84
						(4.7) -4.2 31.9 31.1
171+00				+4.4 27.2	+4.9 27.4	+0.8 15.72 136.90
						on credit (7.1) -2.5 26.4 28.6
+50				+5.5 27.8	+6.0 28.0	+0.9 16.67 135.95
						(1.4) -0.9 26.9 26.1
170+00				+4.4 30.7	+4.9 30.6	+5.1 17.61 135.01
						(0.8) -0.3 26.0 25.3
+50				+1.7 29.4	+1.8 29.6	+9.9 18.56 134.06
						(4.1) +4.6 26.0 26.1
169+00				+2.0 30.2	+1.8 30.3	+13.6 19.50 133.12 152.62
						(2.1) +2.6 27.3 27.4

152.62

1.89%

Note: in this curve, cut slope 3:1
Left side is 1:0 Lower
Rt. side is 1:0 Higher

cut slopes:
3:1
3:1
3:1

STA.	+	H.I.	-
175+50			

$0.0 = \text{Error}$
 $151.0 = \text{Elev. Stub. Pinned}$

chg. on L cut stub 176+00 0.8 151.00
 T.P. 9.52 151.81 0.37 142.29

175+00

+50

174+00

+50

173+00

+ 51.03 2.11 142.66 12.07 140.55
 172+49.91 = E.C.
 152.62

LT.	±	RT.
$\frac{+81}{29.0}$	$\frac{-2.6}{6.21}$ 145.40 151.81	53 $\frac{-59}{33.6}$
$\frac{-15}{27.0}$	$\frac{-6.0}{71.80}$ 141.46	$\frac{-8.7}{37.1}$
$\frac{-24}{28.4}$	$\frac{-6.0}{70.85}$ 143.51	$\frac{-8.8}{38.0}$
$\frac{-44}{31.4}$	$\frac{-7.6}{80.9}$ 142.57	$\frac{-8.8}{38.0}$
$\frac{-5.9}{33.7}$	$\frac{-7.2}{70.4}$ 141.62	$\frac{-11.5}{42.0}$
$\frac{-6.5}{34.6}$	$\frac{-6.6}{71.98}$ 140.68	$\frac{-10.6}{40.7}$
$\frac{-1.8}{27.8}$	$\frac{-6.4}{2.93}$ 139.73 142.66	$\frac{-11.1}{41.2}$ -10.6 40.7

1.89

STA.	+	H.I.	-
179+50			
179+00			
+50			
178+00			
+50			
177+00			
+50			
T.P.	9.52	160.75	0.00 151.23
176+00			
	11.80	151.23	137.43

1.85%

B.M. #13. 2 1/2' high
on fence line
80' N. 176+60

LT.	±	RT.
$\frac{+57}{27.9}$	$\frac{-4.3}{7.79}$	$\frac{-3.9}{33.6}$
$\frac{+71}{28.5}$	$\frac{-3.1}{8.73}$	$\frac{-9.9}{37.6}$
$\frac{+10.9}{30.5}$	$\frac{+1.0}{9.68}$	$\frac{-5.6}{37.7}$
$\frac{+12.2}{31.1}$	$\frac{+3.4}{10.62}$	$\frac{-4.8}{32.0}$
$\frac{+14.1}{32.0}$	$\frac{+4.9}{11.57}$	$\frac{-1.0}{26.3}$
$\frac{+13.3}{31.7}$	$\frac{+6.9}{12.51}$	$\frac{+1.5}{25.8}$
$\frac{+16.0}{33.0}$	$\frac{+5.9}{13.46}$	$\frac{+3.2}{26.6}$
$\frac{+11.8}{30.9}$	$\frac{+4.7}{14.40}$	$\frac{-0.7}{25.1}$
	146.35	
	160.75	

STR.

+

H.I.

-

185+50

185+00

T.P. 13.16 176.73 8.69 163.57

+50

184+00

+ 88.12
183+86.72 = EC.

128 172.26 12.56 170.98

0.54 183.54

+50

183+00 ckt. on 2 stub. 184+00 3.8

165.40

0.1 = Error.

161.5 - stub.

161.6

Lt.

+0.5
25.3

+5.6
27.8

+6.5
28.3

+7.9
28.7

+4.2 (3.7)
27.1 (26.8)

+10.5 (9.1)
30.3 (29.6)

£

-7.9
8.66
168.07

-1.0
19.41
166.32

176.73

-1.9
7.58
164.68

-1.6
3.14
163.12

172.26

Leave out

-3.6
3.74
161.66

-0.5
5.12
160.28

165.40

Rt.
56

-10.3
40.3

-9.1
38.5

-11.6
42.2

-12.5
43.6

(-10.4) = 11.0
40.4 41.3

(-10.7) = 11.2
40.9 41.6

600' Y.C.

574' 14" = 2' 10" H.I.
On Price 4.100
64' 14" to 182' 14"

Note: In this curve
cut wide 16.10' Higher than I
the " " " " " " " " " " " "

STN.	+	H.I.	-
189+00			
+50			
188+00 = P.V.C.			
T.P.	13.75	190.09	0.39
			176.34
+50			
187+00 = E.V.C.			
+50			
186+00			
		176.73	

Lt.	Σ	Rt.
$\frac{+11.7}{28.0}$	$\frac{14.5}{8.11}$	$\frac{57}{28.1}$
	181.98	
600 V.C.		
$\frac{+1.0}{28.0}$	$\frac{-11.7}{10.04}$	$\frac{-3.2}{29.6}$
	180.05	
$\frac{+1.8}{25.9}$	$\frac{+3.1}{12.07}$	$\frac{2.0}{27.8}$
	178.02	
	190.09	
$\frac{+2.8}{26.4}$	$\frac{+0.9}{0.70}$	$\frac{-5.9}{33.6}$
	175.94	
4.15%		
$\frac{-0.3}{25.3}$	$\frac{-2.3}{2.86}$	$\frac{-3.4}{29.9}$
	173.87	
$\frac{+1.7}{25.9}$	$\frac{-3.4}{4.88}$	$\frac{-5.9}{33.6}$
	171.25	
600 V.C.		
$\frac{+1.1}{25.6}$	$\frac{-5.9}{6.82}$	$\frac{-8.2}{37.1}$
	169.91	
	176.73	

STP,	+	H.I.	-
192+50			
192+00			
TP	11.67	202.85	9.85
191+50			191.18
191+00			
+50			
190+00			
TP	12.35	201.03	141
189+50			188.68
		190.09	

Lt.	£	Rt.
$\begin{matrix} +12.9 \\ \underline{31.5} \end{matrix}$	$\begin{matrix} +3.6 \\ \underline{9.98} \\ 192.87 \end{matrix}$	$\begin{matrix} 58 \\ \underline{-7.0} \\ 55.3 \end{matrix}$
$\begin{matrix} +11.5 \\ \underline{30.7} \end{matrix}$	$\begin{matrix} +5.3 \\ \underline{11.25} \\ 191.60 \\ \underline{202.85} \end{matrix}$	$\begin{matrix} -0.6 \\ \underline{25.7} \end{matrix}$
$\begin{matrix} +12.9 \\ \underline{31.4} \end{matrix}$	$\begin{matrix} +6.1 \\ \underline{19.80} \\ 190.23 \end{matrix}$	$\begin{matrix} -5.3 \\ \underline{32.7} \end{matrix}$
$\begin{matrix} +12.0 \\ \underline{31.0} \end{matrix}$	$\begin{matrix} +4.9 \\ \underline{12.26} \\ 188.77 \end{matrix}$	$\begin{matrix} -2.7 \\ \underline{28.8} \end{matrix}$
$\begin{matrix} +8.3 \\ \underline{29.2} \end{matrix}$	$\begin{matrix} +3.9 \\ \underline{13.81} \\ 187.22 \end{matrix}$	$\begin{matrix} -4.1 \\ \underline{30.9} \end{matrix}$
$\begin{matrix} +9.9 \\ \underline{30.0} \end{matrix}$	$\begin{matrix} +3.7 \\ \underline{15.46} \\ 185.57 \end{matrix}$	$\begin{matrix} -4.2 \\ \underline{31.1} \end{matrix}$
$\begin{matrix} +11.9 \\ \underline{30.9} \end{matrix}$	$\begin{matrix} +4.8 \\ \underline{17.2} \\ 183.83 \\ \underline{201.03} \end{matrix}$	$\begin{matrix} -2.2 \\ \underline{28.1} \end{matrix}$

600 Y.C.

on 6x6x17 Ad
40' 5/4 on panels

STN. + H.I. -

196+00

+50

195+00

+50

194+00 = E.V.C.

193+50

193+01.74
 192+99.74 = B.C. Pt.

202.85

Lt
 +2.3
 26.2

+4.9
 27.4

+7.5
 29.7

+8.0
 29.0

+8.9
 29.5

+13.3
 31.6

+12.3
 31.2

£
 +0.1
 2.98
 199.87

+4.1
 3.92
 198.93

+4.8
 4.80
 197.99

+5.0
 5.80
 197.05

+4.5
 6.74
 196.11

+4.3
 7.73
 195.12

+4.0
 8.81
 194.04

202.85

Rt.
 59
 -7.3
 35.7

-6.3
 34.3

-3.6
 30.2

-2.7
 28.9

-2.5
 28.6

-5.9
 33.6

-8.5
 37.6

188%

X

600%

STA. + H.I. -

199+00

Lt.

$\frac{-24}{274}$

$\frac{72.9}{256}$
205.51

Rt.
60

$\frac{-18.1}{52.0}$

+50

$\frac{-27}{304}$

$\frac{-13.5}{3.50}$
204.57

208.97

$\frac{-18.3}{52.3}$

T.P. 12.13 208.07 6.91 195.94

198+00

$\frac{-47}{313}$

$\frac{-12.2}{+0.78}$
203.63

$\frac{-16.3}{49.3}$

+61.63
197+61.15 = E.C.

15.8%

+50

$\frac{-26}{287}$

$\frac{-9.2}{0.15}$
202.69

$\frac{-12.4}{43.4}$

197+00

$\frac{-10}{263}$

$\frac{-5.0}{1.10}$
201.75

$\frac{-8.4}{37.4}$

196+50

$\frac{+16}{258}$

$\frac{-2.5}{2.04}$
200.81

202.85

$\frac{-5.6}{33.2}$

202.85

STH.	+	H.I.	-	Lt.	£	Rt.
203+00				+122 31.1	+28 646 213.03	61 711 25.5
+50				+157 32.8	+46 7.40 212.09	+0.8 752
202+00				+131 31.5	-1.1 8.34 211.15 219.49	-7.0 35.3
T.P.	13.25	219.49	1.89	206.24		
					Set. temp. 27.1, 110 fms 23.5, 201 +75	
201+50				+42 27.1	-0.8 +2.14 210.21	-5.1 34.1
201+00				+18 25.9	-0.4 +1.20 209.27	-5.6 33.2
+50				-1.9 27.6	-1.4 +0.26 208.33	-6.3 34.3
200+00				-2.1 27.9	-8.3 0.68 207.99	-10.5 40.6
199+50				-2.1 27.9	-11.9 1.62 206.45	-14.8 47.0
		208.07			208.07	

1.88%

STP.	+	H.I.	-	Lt.	€	Rt.
206+50				$\frac{+196}{34.8}$	$\frac{+07}{76.84}$ 219.40 <u>230.24</u>	$\frac{62-82}{37.1}$
T.P.	11.21	230.24	0.46	219.03		
206+00				$\frac{+198}{79.9}$	$\frac{+04}{0.89}$ 218.60	$\frac{-10.6}{49.7}$
				$\frac{0.0}{25.0}$	$\frac{+04}{1.79}$ 217.70	$\frac{-7.8}{36.5}$
+50 = P.V.C.						
205+00				$\frac{+21}{76.0}$ $\frac{+133}{76.6}$	$\frac{+0.3}{2.71}$ 216.78	$\frac{-34}{29.9}$
				$\frac{+14}{25.7}$	$\frac{0.0}{3.64}$ 215.85	$\frac{-0.7}{25.8}$
+50						
204+00				$\frac{+67}{28.3}$	$\frac{0.0}{2.58}$ 214.91	$\frac{+14}{25.7}$
				$\frac{+78}{28.9}$	$\frac{+0.9}{5.52}$ 213.97	$\frac{+1.7}{25.8}$
203+50					<u>219.49</u>	
		219.49				

400' V.C.

1.88%

STA. + H.I. -

210+00

209+50

209+00

+50

208+00

+50

207+00

230.24

0.534%

400' Y.S.

+94
297

+77
289

+124
312

+151
326

+165
332

+122
311

+120
305

+

±

+30
7.41
222.83

+2.6
7.68
222.56

+2.6
7.99
222.25

+2.0
8.44
221.80

+1.7
8.86
221.38

+1.5
9.47
220.82

+1.3
10.14
220.10
230.24

63

-33
297

-42
311

-14
269

-40
308

-51
324

-155
480

-57
334

STG. + H.I. -

+2818
213+26.35 = BC. RT.

213+00

+50

212+00

+50

211+00

210+50

230.24

L.

+150
325

+147
323

+130
315

+142
321

+164
332

+93
297

€

+4.9
581
224.43

+5.4
608
224.16

+5.3
635
223.89

+5.1
661
223.63

+4.4
688
223.36

+3.7
715
223.09
230.24

Rt.

64

+3.8
269

+3.1
26.6

+3.5
26.7

+4.1
27.0

+3.1
26.6

-0.5
25.6

0.534%

STR. + H.I. -

216+50

216+00

+50

215+00

+50

T.P. 0.29 238.03 12.60 237.74

0.49 250.34 249.85 = BM #16

0.11 = Error

214+00

chk on BM #16 = 6224.56 216+20 0.49 249.74

T.P. 10.73 250.23 2.44 239.50

T.P. 12.54 241.94 0.84 229.40

213+50

230.24

Lt.

$\frac{+108}{304}$

$\frac{+110}{305}$

$\frac{+131}{315}$

$\frac{+151}{326}$

$\frac{+203}{352}$

$\frac{+297}{396}$

$\frac{+136}{318}$

Σ

$\frac{-0.4}{11.73}$
226.30

$\frac{+0.7}{12.00}$
226.03

$\frac{+1.4}{12.27}$
225.76

$\frac{+1.8}{12.53}$
225.50

$\frac{+5.3}{12.80}$
225.23

$\frac{+5.2}{13.07}$
224.96

$\frac{+5.6}{5.54}$
224.70
230.24

ft. 65

$\frac{-72}{356}$

$\frac{-26}{287}$

$\frac{+0.1}{250}$

$\frac{+0.6}{253}$

$\frac{+2.8}{264}$

$\frac{+4.3}{273}$

$\frac{+4.9}{274}$

0.534 %

Note: in this case
Left side is 1.0' higher than R.
Rt. side is 1.0' lower than L.

STA.	+	H.I.	-
219+84.47	} EC.		
219+69.54			
+50			
219+00			
+50			
218+00 ✓			
+50			
T.P.	277	228.69	1211 22592
217+00		238.09	

Pt. 66

Lt	±	±
-1.0 26.3	-5.9 0.79 227.90	-10.7 40.7
-1.4 26.9	-5.5 1.06 227.63	-11.5 42.0
-2.5 28.6	-8.7 1.32 227.37	-12.1 43.9
-1.9 27.7	-10.1 1.59 227.10	-16.0 48.8
-2.3 28.3	-10.8 1.86 226.83	-14.7 46.9
-0.4 25.4	-3.9 2.12 226.57 228.69	-10.9 41.2

0.534 %

STA.	+	HT	-
222+50			

TR 10.2 219.55 10.16 218.53

RRR +00

+50

+39.07
221+27.53 = B.C.

RR1 +00

+50

Set Temp BM. 60' Lt 220+50 0.90 227.79 on stub.

220+00

228.69

Lt.	±	Rt.
-8.9	-16.0	67
38.1	19.95	-20.8
	229.50	56.0
	219.55	

-7.5	-11.6	-17.2
36.0	+0.55	50.6
	229.24	

-3.2	-7.1	-12.3
29.6	+0.28	43.3
	228.97	

0.534%

-1.4	-3.2	-8.3
26.9	+0.01	37.3
	228.70	

-2.3	-4.2	-9.1
28.3	+0.26	38.4
	228.43	

-0.7	-5.8	-9.6
25.8	+0.52	39.0
	228.17	

228.69

Note: Rt. set 1.0' higher than Lt. } in this curve
Lt. 1.0' lower

STA.	+	H.I.	-
226+00			

T.P. 13.21 241.43 2.88 228.22

+50

225+00

+50

T.P. 11.66 231.10 0.11 219.44

224+00

+50

223+00

219.55

set temp.
511 fence
Post 75' out
113480

941 210.14

Lt.	±	Rt.
+171 33.5	+5.3 19.06 231.37 241.43	68 30 29.3

+169 33.5	-1.4 0.00 231.10	-84 37.4
--------------	------------------------	-------------

+193 29.6	-2.4 0.26 230.84	-13.9 45.6
--------------	------------------------	---------------

-2.2 28.1	-8.0 0.53 230.57 231.10	-23.7 60.3
--------------	----------------------------------	---------------

0.534%

-3.5 30.0	-17.8 +10.75 230.30	-24.1 60.9
--------------	---------------------------	---------------

-8.3 37.2	-22.7 +10.49 230.04	-24.3 61.3
--------------	---------------------------	---------------

-9.2 38.6	-19.4 +10.22 229.77 219.55	-23.7 60.5
--------------	-------------------------------------	---------------

STA.	+	H.I.	-
229+50			
229+00			
T.P.	10.04	264.20	0.13
+50			
T.P.	12.97	251.9	0.11
228+00			
+50			
227+00			
226+50			

241.43

Lt.	¢	Rt.
+65.0	+30.4	69
57.5	30.96	0.0 } daylight
	238.24	32.5 }
+54.6	+24.9	0.0 } daylight
52.3	31.23	32.8 }
	232.97	
	264.20	
+27.5	+15.0	-3.7
38.7	21.58	30.4
	232.71	
	254.29	
+7.9	+2.0	-3.8
28.9	8.39	30.5
	232.44	
+12.0	+1.3	-3.8
34.0	9.26	30.5
	232.17	
+8.7	+0.6	-2.9
29.4	9.52	29.2
	231.91	
+6.3	-1.8	-3.5
28.2	9.79	30.0
	231.64	
	241.43	

0.534 %

STR. + H.I. -

233+00

0.1 = Error
237.9 = Stub

chk on 2 stubs 233+50 46 238.00

+50

232+00

T.P. 0.38 242.59 10.70 242.21

+50

T.P. 1.05 252.91 12.34 251.86

231+00

+50

230+00 = PVC

264.20

LT \$

~~+27.0~~ 116
38.5 308

+1.1
6.6
236.00

-14.3
46.3

16.3
33.2

+0.8
7.16
235.43

-16.2
49.1

~~+11.6~~ 1229
30.8 365

+0.6
17.67
234.92

-17.4
50.9

+36.0
13.0

+13.3
18.45
234.46

-0.2
25.1

400' VC

+48.0
49.0

+21.5
30.16
234.06

-1.3
26.7

+48.0
49.0
23

+19.4
30.48
238.72

-2.3
28.2

+50.7
50.1

+24.3
30.78
233.42

0.0 } day 1944
30.7

264.20

Sta.	+	H.I.	-
236+00			
T.P.	1.89	246.52	12.73
+50			
235+00			
+50			
234+00 - E.V.C.			
+50			
T.P.	3.63	257.36	12.81
T.P.	5.39	266.54	12.81
+08.00 233+07.34 = E.C.			
	4.23	273.96	

Set. Temp
BM on stub
approx 50'
40.50 234+00

BM #18
2 x 2 Mt. Wood Nib
34' Lt. Sta. 233+36

140' up
400' V.C.

Lt.	±	Rt.
+0.9 25.5	-0.8 6.43 240.09	71.44 31.4
+0.5 25.3	-2.3 7.13 239.39 246.52	-5.6 33.2
+3.4 26.7	-1.8 18.67 238.69	-6.5 34.6
+8.2 29.1	+1.4 19.37 237.99	-7.5 36.3
+3.5 29.8	+1.7 20.07 237.29	-10.5 40.6
+2.0 29.5	+1.3 20.74 236.62	-12.0 42.8
	257.36	

Sta.	+	H.I.	-	LT.	℄	RT.
239+50				$\frac{-0.9}{26.3}$	$\frac{-2.2}{1.53}$ 244.99	$\frac{72-128}{44.0}$
239+00				$\frac{-0.9}{26.5}$	$\frac{-7.4}{2.23}$ 244.29	$\frac{-11.1}{41.5}$
+50				$\frac{-0.7}{26.0}$	$\frac{-5.8}{2.93}$ 243.59	$\frac{-8.6}{37.7}$
238+00				$\frac{-0.1}{25.1}$	$\frac{-3.4}{3.63}$ 242.89	$\frac{-6.5}{34.5}$
+50				140 o/o $\frac{+0.5}{25.3}$	$\frac{-1.2}{4.33}$ 242.19	$\frac{-4.2}{31.1}$
237+00				$\frac{+0.8}{25.7}$	$\frac{-1.1}{5.03}$ 241.49	$\frac{-3.8}{30.5}$
236+50				$\frac{+0.8}{25.7}$	$\frac{-0.8}{5.73}$ 240.79	$\frac{-3.8}{30.5}$
		246.52			246.52	

STA.	+	H.I.	-
243+00			
+50			
242+00			
+50			
241+00			
+50			
T.P.	9.32	254.45	1.39
240+00			245.13
		246.52	

Lt.	\$	73
+182 34.1	+0.6 4.56 249.89	1.2 26.6
+127 31.3	+0.6 5.26 249.19	-1.3 26.7
+156 32.8	+0.5 5.96 248.49	-6.2 34.1
+161 33.1	+0.1 6.66 247.79	-12.1 42.9
140 of +8.5 29.3	-0.3 7.36 247.09	-15.8 48.5
+0.5 25.9	-2.3 8.06 246.39	-16.2 49.2
	254.45	
-1.1 26.6	-5.2 0.83 245.69	-14.6 46.7
	246.52	

STN.	+	H.I.	-
246+00			
+50			
245+00			
244+75.83			
244+70.83 B.C.			
+50			
244+00			
T.P.	12.34	264.28	2.51 251.94
243+50			

254.45

Lt.	C	Rt.
+18.8 34.4	+3.6 10.19 254.09	74 24.8
+25.3 37.6	+9.2 10.89 253.39	+0.4 25.2
+15.3 32.6	+5.5 11.59 252.69	+0.8 25.4
	252.32	
14.0 of +9.0 23.5	+5.6 12.29 251.99	+3.1 26.1
+12.3 31.2	+2.6 12.99 251.29 264.28	+2.3 26.2
+20.0 35.0	+0.7 3.86 250.59 254.45	+0.8 25.4

STA.	+	H.I.	-	
249+50				
T.P.	2.41	277.07	2.25	274.66
249+00				
+50				
248+00				
+50				
+25 = P.V.C.				
247+00				
T.P.	12.65	276.91	0.02	264.26
246+50		264.28		

LT.	±	RT.
	+5.1 <u>71.86</u> 260.51	-1.0 25.3
	277.07	
	+25.9 <u>37.9</u>	-0.3 25.3
	259.21	
	+19.3 <u>34.6</u>	+0.1 25.0
	258.06	
	+17.7 <u>33.0</u>	+0.0 25.0
	257.06	
	+13.4 <u>46.7</u>	+0.7 25.5
	256.21	
	+11.0 <u>45.5</u>	-0.4 25.4
	255.43	
	+13.9 <u>41.9</u>	-0.1 25.0
	276.91	

600' V.C.

P.V.C.

140' o/p

Sta.	+	H.I.	-	
253+00				
+50				294.65 = BM.#20
chk. on BM #20 18' Lt. Sta. 250+90	2.98			294.65
T.P.	6.90	297.63	0.12	290.73
T.P.	13.26	290.85	0.25	277.59
252+00				
+50				
T.P.	12.31	277.84	11.54	265.53
251+00				251+50 on stub. 10' Lt.
+50				
250+00				

277.07

600' V.C.

Lt.	±	Rt.
+15.7 32.8	+0.5 23.82 273.81	-16.5 40.6
	297.63	
+20.2 35.1	+6.3 63.8 271.46	-17.7 51.4
+6.0 28.0	-1.2 8.58 269.26	-23.3 59.8
-0.5 25.5	-7.0 10.63 267.21	-17.7 51.4
	277.84	
+10.4 30.2	-4.2 11.76 265.31	-15.8 40.6
+11.8 30.9	-3.2 13.51 263.56	-3.7 30.3
+6.7 28.7	+2.5 15.11 261.96	-1.0 27.0
	277.07	

Rt.
76

STA.	+	H.I.	-	
256+00				
+50				
255+00				
+62.91				
254+60.33 E.C.				
TP	6.26	289.87	12.13	283.61
	1.09	295.74		294.65
+50				
254+00				
TP	0.16	272.52	12.87	272.36
	0.33	285.23	12.73	284.90
253+50				
253+25 = E.V.C.		297.63		

B.M. #20
78' 47" Sta. 250+90

500' 0"

↑ E.V.C.
34
35

Lt.		Rt.
$\frac{+4.8}{27.4}$	$\frac{-4.1}{1.08}$ 288.79	77 $\frac{-2.00}{54.8}$
$\frac{+1.6}{25.8}$ 26 27.8	$\frac{-2.2}{3.58}$ 286.29	$\frac{-20.9}{56.1}$
$\frac{-1.4}{26.9}$	$\frac{-9.6}{6.08}$ 283.79	$\frac{-28.2}{67.1}$
$\frac{-2.9}{29.1}$	$\frac{-13.4}{8.06}$ 281.81	$\frac{-34.6}{76.7}$
$\frac{-5.8}{33.5}$	$\frac{-15.3}{+8.77}$ 281.29	$\frac{-35.3}{77.7}$
$\frac{-13.9}{45.8}$	$\frac{-15.5}{+6.27}$ 278.79	$\frac{-32.7}{73.8}$
$\frac{-4.3}{31.6}$	$\frac{-13.8}{+3.77}$ 276.29	$\frac{-28.3}{67.2}$
	272.52	

Sta. + H.I. -

L

Rt.
78

259+50 Cont. in Grade Book - 164 Page 1

chk. on BM #21 2.53 $\frac{0.02}{315.95} = \text{Error}$
 315.93 5747.56, 258+63

T.P. 9.75 318.46 2.44 308.71

259+00

+2.9
26.4

-1.6
7.36
303.79

-8.8
38.0

+50

+4.3
27.2

-0.3
9.86
301.29

-10.3
40.4

T.P. 12.09 311.15 1.91 299.06

258+00

+6.4
28.2

-0.5
2.18
298.79

-11.4
41.9

+50

+5.6
27.8

-1.5
4.68
296.29

-12.7
43.8

257+00

+4.2
27.1

-2.7
7.18
293.79

-14.1
45.8

256+50

+4.7
27.3

-3.4
9.68
291.29

-14.9
47.1

T.P. 12.97 300.97 1.87 288.00
 289.87

300.97

Sta. + H.I. -

155.5 = B.M.
10.35 +
165.85 = π

286+00 Lt. & Rt. 149.5 150 150.5 50 - $\frac{10.3}{35.0}$

+50

287+00

+50

288+00

OID

288+51⁰² E.C.

B.M.[#] 23 10.0 404.98

50

5.0

394.98 = 131

(RL)

Emb.

Grade

(ht.)

cuts.

79

Λ

100 V.C.

X

+0.98%

V

Cor F.
Dist. out.

$\frac{0}{C23}$
 $\frac{5.5}{409.83}$

Cut or Fill
Dist. out.

Not set in culvert on South side pavt. - West Italian Villa Inn

404.98

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not level, the distance from side stake to slope stake and slope stake lower tangent to the amount if cut elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target.

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of correction. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{7}{8}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{15}{16}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
1	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet $\times .00019$ = miles
 Lineal yards $\times .0006$ = miles
 Square inches $\times .007$ = square feet
 Square feet $\times .111$ = square yards
 Square yards $\times .0002067$ = acres
 Acres $\times 4840$ = square yards
 Cubic inches $\times .00058$ = cubic feet
 Cubic feet $\times .03704$ = cubic yards
 Links $\times .22$ = yards
 Links $\times .66$ = feet
 Feet $\times 1.5$ = links
 $360^\circ = 21600' = 1296000''$
 Radius = arc of 57.2957790°
 Arc of 1° (radius = 1) = .017453292
 Arc of $1'$ (radius = 1) = .000290888
 Arc of $1''$ (radius = 1) = .000004843

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = $0.667 (\text{Dist. in miles})^2$

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = $R - R \sin^2 a + C \cos a$

Vertical Distance = $R \frac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

2M. V 19. = 27678
107' L- 238180

145 6143

29478
32
59.5

.61
2
1.22
.16
3 | 1.38
.46
2
.92