

GRADE Book 176



EMERALD BOOK

1907

925230
1854500

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
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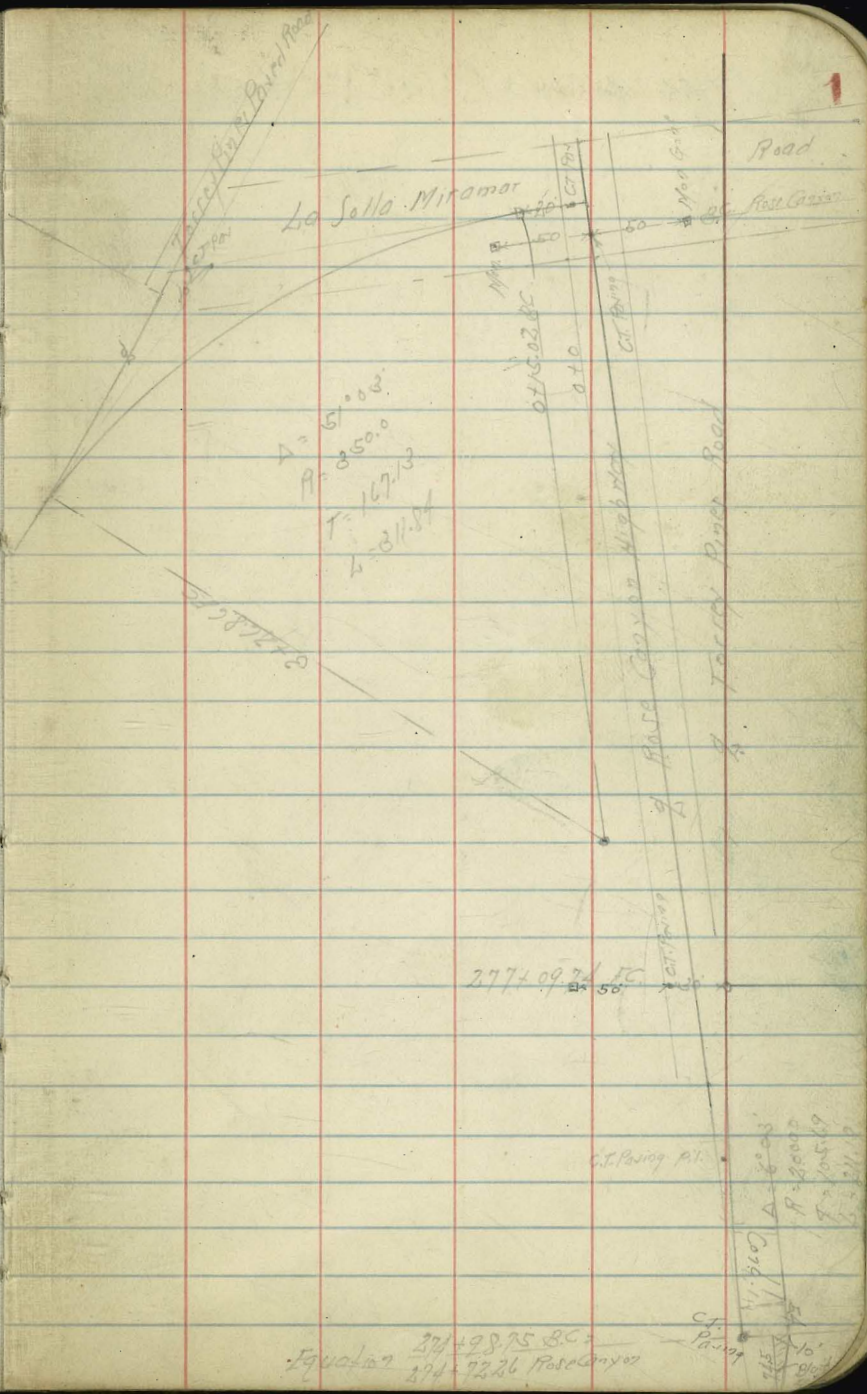
MICROFILMED

APR 12 1965



Torrey Pines Mesa Road
 Rose Canyon Highway Road
 La Sella-Miramar Road

indexed
 c.c.k



Equation $277 + 09.21 BC$
 $274 + 22.26 Rose Canyon$

C.T. Pines Pt.
 Rose Canyon
 Torrey Pines
 277 + 09.21
 274 + 22.26

Tim Torrey Pine Meadow Road
Rose Canyon to Torrey Pine Grade

Indexed
C.S.K.

299
288 976
10024

1313

1314

50

2 x 12" deep

2 x 12" deep

Gran. Mon

1312

1311

Torrey Pine Meadow Road

Rose Canyon Highway

W Lane

E Lane

12-18-40

C.T. 10 50
Posing

Mon 50
Mon 50

FC Rose Canyon

Most of
Dinner
Northward

A = 28° 45'
R = 15000
T = 30863
L = 60781

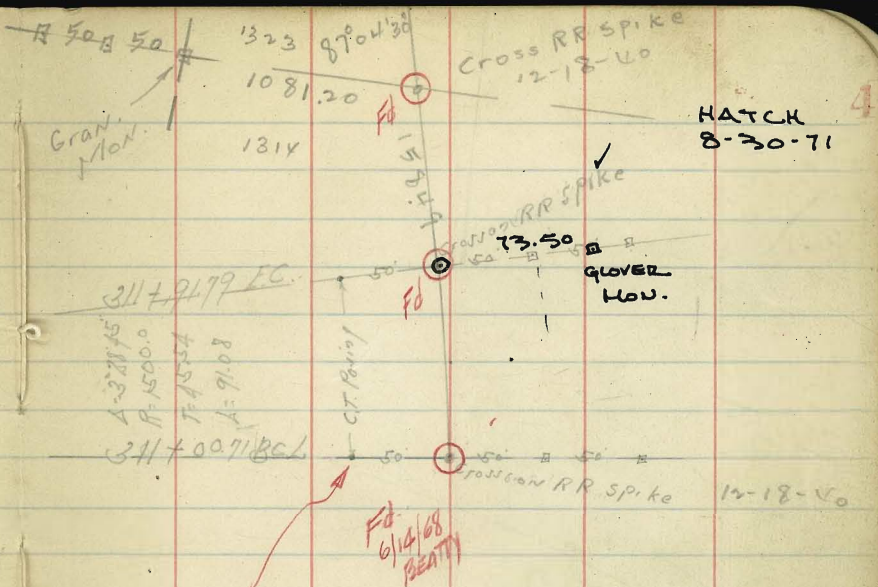
check this

set points
at 100 ft
intervals
along
the
road

28819988 FC

29910 POT

C.T. Parry 50 50 50 50



HATCH
8-30-71

C.T. pav.
NOT Fd.
(20 CONC. pav. NOT
covered with)
AC.
RTS should be there
unless get in 10 CONC
orig. pav.

3 29 45
1 44 22
89 59 60
88 15 38

0 30.34
3000
9102000

330 x 0 POT

330 x 0 POT

1000

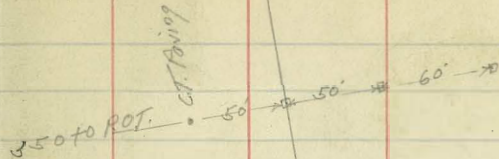
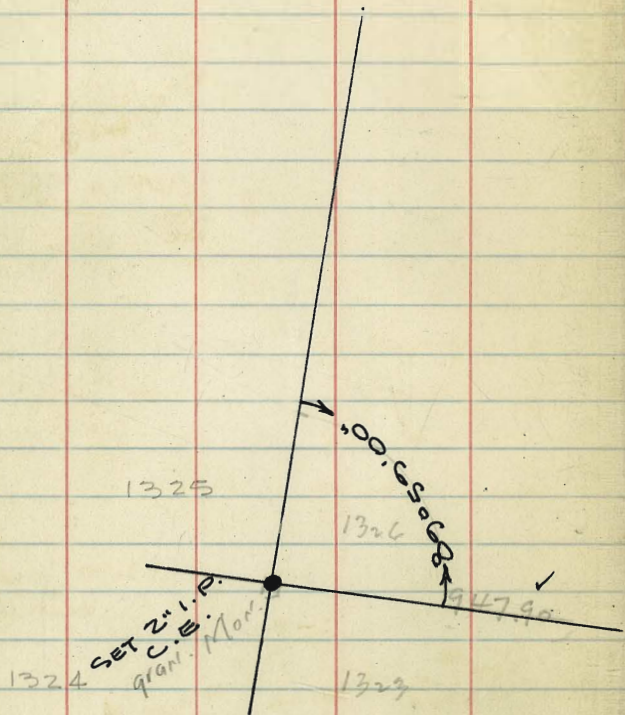
50 * 50 * 50 *

33070 POT

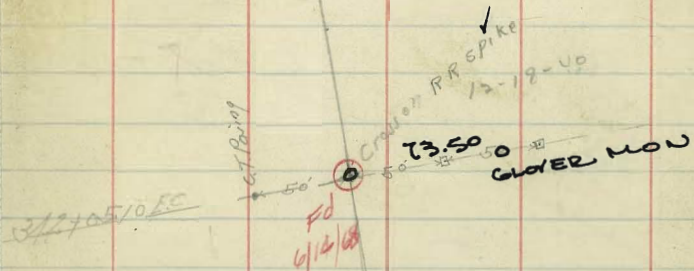
33070 POT

CT/Baria

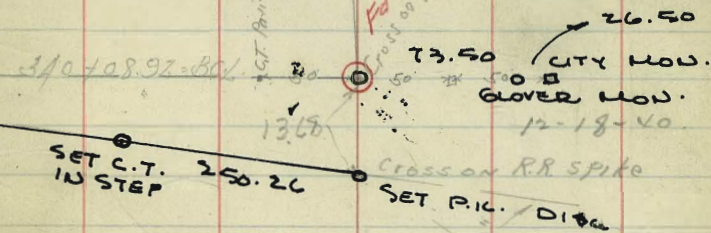
50 50 50 50



HATCH
8-30-71



$\Delta = 7^{\circ}30'00''$
 $R = 1500'$
 $T = 98.315$
 MEAS. 98.18



394+00. Alt. $0^{\circ}15'00''$
 39400
 39261.24
 138.76

392+61.24 Int. of P.h.
 79°34'
 138.76

390+0 P.O.T.

380+00 P.O.T.
 497.75 371.2624
 488.9 366.7756
 448.38

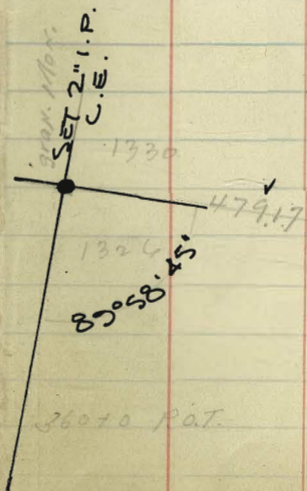
371+26.04 Alt. $0^{\circ}02'00''$

366+77.66 Int. P.K.

360+0 P.O.T.

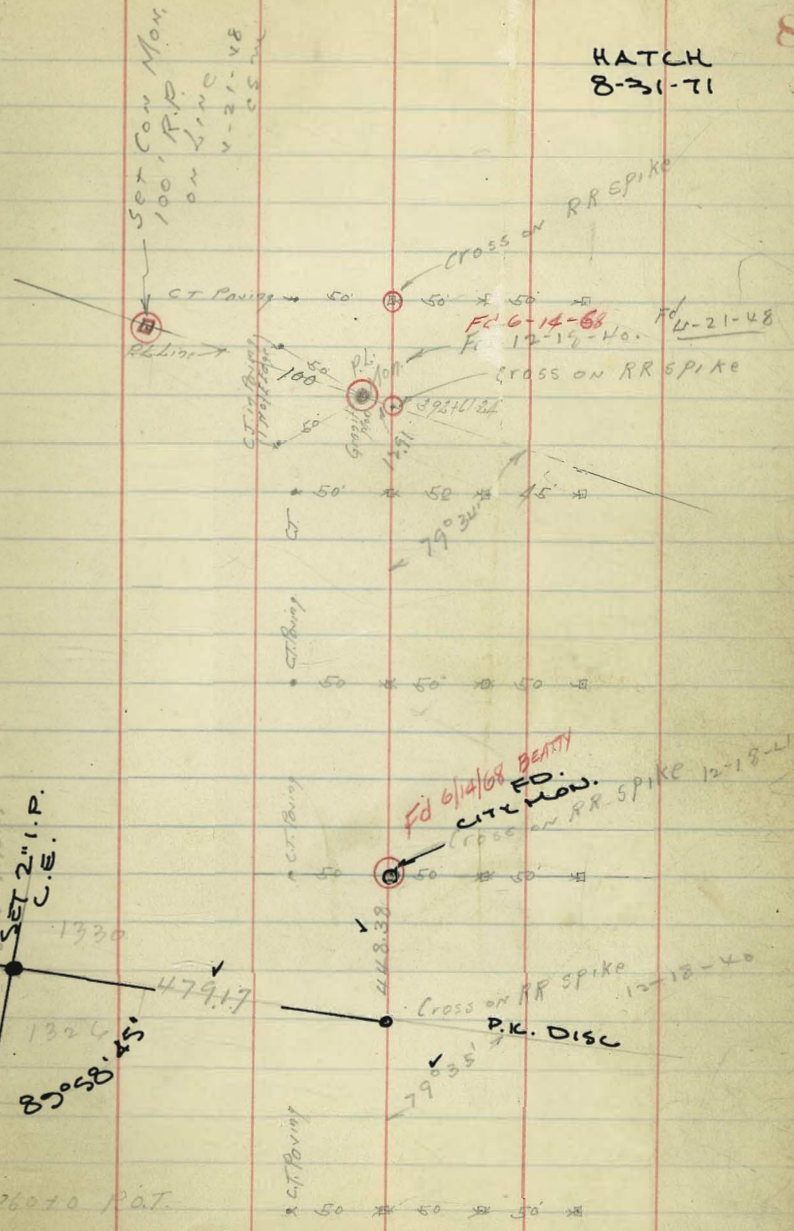
1331

1325



360+0 P.O.T.

HATCH
 8-31-71



Tins-Torrey Piped Mesa Road

3997 99.18 FC
Foot of Old Road

51226.64 FC

11204.88 FC

41712.45 FC

418135.92 End of Layout

9

Reservoir

404100 P.O.T

C.T.B.M.

45

75

39970 P.O.T

C.T.B.M.

45

45

45

45

45

45

45

45

45

$\Delta = 234.9$
 $R = 1500$
 $T = 315.87$
 $L = 122.65$

1105.68

Torrey Piped Road BC

3997 99.71 Foot Torrey Piped Grade

411401.80 BC

411401.80 BC

Ed
Ld. C.T.
P.C. Mon

Culvert 356+00

52# CMP #1

2 Type 82 1/2 ft

Flow Line

0+0 Inlet

412.10 ^{5.38}
+0.38

BM 417.68 ⁺⁶
7.12
418.80

356+07.5 Inlet

416.71 ^{+11.0} 416.0 Top ch Grad

356+02 Culvert

95 | 11 | 175

0+33.5 = Highway

355+81.5 Inlet

416.92 ^{+16.25} 416.82 Top ch Grad

0+59 Outlet

408.30 ^{10.50}
10.96
-0.46

Left

416.71
7.09
6.36
-8.97

416.92
1.88
6.13
-4.25

Right

416.61
2.19
9.07
-6.88

Culvert 364+00

68# CMP

Flow Line

0+0 Inlet

414.80 ^{5.55}
+0.77

BM 417.68 ⁺⁶
8.57
422.25
421.14
+15.21
419.35

0+16.87 = Grating Rt 421.31

2.94
12.11
-9.17

0+27.77 = Highway

0+46.61 = Grating Lt

421.31
15.04
13.93
-8.88

0+71.48 = Outlet

16.45
16.68
-0.23

364+00

Inlet

16.87 | 13.87 | 16.87 | 24.87

Culvert 377+10

50# CMP

Flow Line

0+0 Inlet

411.50 ^{7.77}
5.28
+3.39

BM 422.97 ⁺⁷ 416.79 ⁺³⁷⁺⁹⁰

11.00
11.97
12.24
+17.22
+17.92
419.27

0+10.87 = Grating Rt

411.30 414.57
17.0
6.52
-7.87

0+27.77 = Highway

0+46.61 = Grating Lt

410.50 ^{8.77}
8.15
-3.88

0+53.48 = Outlet

2.86

377+10

12.87 | 13.87 | 16.87 | 10.87

0+0

Culvert 316+10
 0+0 - Inlet
 0+148.2 Grating
 0+277.4 Highway
 0+446 Grating
 0+624.8 - Outlet

6" of 24" CMP
 Flow Line
 19.80
 20.5
 21.6
 22.5
 23.4

RT Grating
 25.54
 26.5
 27.4

18.70

Culvert 322+75
 0+0 - Inlet
 0+275 Highway
 0+690 - Outlet

6" of 24" CMP
 Flow Line
 13.20
 13.87
 14.54
 15.21
 15.88

BM 426.47 #1
 0.28
 426.19
 415.36
 416.07

107.10
 897
 925
 953

Culvert 332+88
 0+0 - Inlet
 0+255 Highway
 0+610 - Outlet

54" of 24" CMP
 Flow Line
 120.00
 669
 587
 505

BM 426.47
 0.28
 426.19

115.80
 1089
 1102
 1115

2 Type D Catch Basins
 316+10
 148.2
 157
 168.7
 18.87

427.698
 1.11

2 Type B2 Inlets
 322+91 - 5' of Inlet
 322+75 Culvert
 322+68 - 5' of Inlet

418.94
 125
 11
 18
 23.5
 418.89
 187
 187

418.84 Top of Grade
 418.79 Top of Grade

Left
 118.94
 2.87
 2.84
 -6.64

Right
 118.79
 2.73
 2.63
 -9.95

2 Type B2 Inlets
 332+07 - 5' of Inlet
 332+88 Culvert
 332+81 - 5' of Inlet

424.62
 115
 14
 18
 17.5
 424.36
 424.26

424.52 Top of Grade
 424.26 Top of Grade

Left
 424.62
 2.07
 2.55
 -5.78

Right
 424.26
 2.13
 2.59
 -8.42

Culvert 295+50

544' of 24" CMP

Flat Line

0+0 = Inlet

414.00

5.81
5.54
-0.27

417.71 ^{on 24"} 1125750
3.12
419.83

0+25.5 = Highway

0+11.0 = Outlet

410.00

9.83
9.57
-0.26

2 Type B3 Inlets

295+69 = 54' of Inlet

419.97

X

418.47

-419.27

Top Curb Grades

295+50 = Culvert

11.5

11

18

295+43 = 55' of Inlet

419.97

418.37

418.97

Top Curb S

418.37

419.07

0.76

0.76

0.22

0.82

-0.58

-0.06

Top Curb S

419.27

418.97

0.56

0.96

7.56

8.06

-7.00

-7.12

Highway

Culvert 305+15

114' of 24" CMP

Flat Line

0+0 = Inlet

423.60

6.06
2.69
-1.37

429.66 T. Right

2 Type D Catch Basins

305+15

429.50

429.00

428.70

16.97

12.87

14.97

32.87

0+16.87 = Grating

429.50

21.6
2.23
7.07

0+29.74 = Highway

419.80

0+46.6 = Grating

Grating

429.40

0.76
8.92
-8.66

0+69.48 = Outlet

418.50

11.16
11.99
-0.83

Grades - Terry Pine Mesa Road
 Rose Canyon to Terry Pine Grade

Indexed
 C.S.K.

	Left	2	Right				
280+40	394.31	393.61	394.31		144 4.5 1.5 198	2	Right 46 4.0 215
+90 P.V.C.	393.12	392.42	393.02		5.7 -0.7 18.1		58 -1.3 215
+50	392.05	391.35	391.95		4.8 1.0 195		6.8 4.0 215
279+0	390.71	390.01	390.61		391.95 x 1.25 387.63 389.71	81 5.0 190	12.2 -1.7 217
+59.71	388.25	388.95	389.55		7.9 1.0 160		1.2 4.0 215
278+09.71	387.35	387.61	388.22		34		2.5 1.0 215
+59.94	386.14	386.28	386.93				3.8 0.0 215
+09.91 P.C.	384.97	384.95	385.65				5.1 1.0 215
277+0 0° 8' 32"	384.71	384.68	385.40				2.1 0.0 215
+50 P.V.C. 51° 30"	383.51	383.35	384.10				3.2 1.0 215
276+0 1° 34' 28"	382.24	382.05	382.81				4.4 1.7 215
275+50 P.V.C. 2° 17' 26"	380.76	380.61	381.26				6.2 1.0 215
274+98.75 82° 01' 30"	379.05	379.03	378.73				5.8 0.0 215

392.82
 389.86
 390.76
 18.73
 380.63

390.75
 379.27
 377.8

385.79
 387.23

385.10
 380.7

	Left	Left	Right	Left	Right	
+50	6° 51' 39"	402.89	402.25	401.45		
286+0	5° 55' 31"	402.09	401.45	400.65		
+50	4° 58' 03"	401.44	400.80	400.00		
285+0	3° 40' 45"	400.69	400.05	399.25		
+50	3° 03' 27"	400.00	399.36	398.56		
284+0	2° 06' 09"	399.31	398.67	397.87		
+89.82	1° 54' 36"	399.18	398.54	397.74		
283+39.82	0° 57' 18"	398.29	397.82	397.06		
+89.82 BC		397.47	397.15	396.49		
282+39.82		396.48	396.47	395.91		
+89.82		395.57	395.99	395.31		
281+39.82		394.81	395.11	394.91		
280+90: F.V.C		395.13	394.43	395.03		

Top
41.30
H 40

100' Curve
41.44
H 30

Left
10.9
10.9
9.6
76.0

Right
13.1
13.1
11.8
81.8

11.9
11.9
9.6
76.0

13.1
13.1
11.8
81.8

12.3
12.3
10.4
76.4

13.1
13.1
11.8
81.8

13.1
13.1
11.8
79.5

14.5
14.5
13.2
83.2

13.7
13.7
12.5
78.5

15.1
15.1
13.8
80.8

6.6
6.6
5.3
79.8

8.9
8.9
7.6
80.4

6.6
6.6
5.3
80.0

8.9
8.9
7.6
80.4

7.6
7.6
6.3
80.7

8.9
8.9
7.6
80.4

8.5
8.5
7.2
80.1

9.9
9.9
8.6
80.6

9.5
9.5
8.2
79.8

10.0
10.0
8.7
80.0

10.6
10.6
9.3
79.4

10.6
10.6
9.3
79.4

10.0
10.0
8.7
79.0

11.1
11.1
9.8
80.4

3.7
3.7
2.4
79.5

3.8
3.8
2.5
80.2

112580.1
1171500.9

11325.11
9.79
13.0
403.08
10.9
405.21
10.2
BM 395.70

110.78
12.16
378.69
401.65
4.12
397.51
399.95

T.P.
EC. EAST

395.70
302
398.821

Nov 24-31
Start Sub

15

	Left	±	Right	Left	±	Right	
293+0	414.55'	414.85'	411.45'	5.8 2.4 +2.5 18.5		5.8 2.4 +2.5 20.7	BM 11 409.60 10.15 419.75 412.66 417.09 419.02
+150	413.75'	414.05'	413.65'	6.2 2.2 +3.4 19.4		6.1 3.2 +2.7 22.0	409.60 6.52 416.12 7.15 414.85
292+0	412.80'	413.10'	412.70'	1.0 6.2 1.0 +2.0 20.0		7.3 3.7 +3.7 20.7	T.P. Cont'd 292+00 714.85
+150	411.85'	412.15'	411.75'	7.0 1.2 +2.2 20.2		8.0 1.8 +2.2 22.0	409.60 7.18 410.78
291+0	410.90'	411.20'	410.80'	8.0 1.5 +2.3 20.0		8.0 1.5 +2.3 20.7	
+150	409.95'	410.25'	409.85'	9.8 5.0 +2.8 20.8		9.9 4.0 +2.8 20.6	
290+0 - F.V.C.	408.98'	409.20'	408.77'	12.8 2.7 +5.7 21.2		14.9 2.9 +5.9 23.7	
289+18.81	408.21'	408.30'	407.67'	14.8 2.7 +5.3 22.8		15.1 2.9 +5.7 23.7	
+9763 - F.C. 1136.20	407.52'	407.20'	406.54'	12.3 2.7 +5.1 20.1		13.3 2.7 +5.0 21.0	BM 11 409.60 10.15 419.75
288+47.63 10°39'07"	406.76'	406.20'	405.43'	2.9 2.7 +2.3 20.0		8.7 2.7 +2.6 20.0	
+9763 9°41'49"	405.84'	405.20'	404.40'	7.9 4.6 +3.3 19.3		9.3 2.3 +2.5 20.5	
+150 8°47'15"	404.89'	404.35'	403.45'	8.0 2.7 +2.2 20.2		10.5 2.7 +2.2 20.2	
287+0 - F.V.C. 7°49'57"	403.89'	403.25'	402.45'	9.9 9.1 +0.8 10.8		11.3 9.7 +1.6 22.6	

	Left	2	Right	Left	2	Right	
+50	122.85	122.15	122.75 ✓	6.0 12.5 18.5		7.0 13.0 20.0	410.02 B/F 71.97 P 417.71 12.06 397+0 397.77 X
299+0	122.26 ✓	122.56	122.16 ✓	7.5 8.9 30.9		7.1 8.5 28.1	429.55 X 5.05 421.50
+50	121.67	121.97	121.57 ✓	8.1 9.7 30.4		8.3 9.5 27.5	T.P. West 397+50 414.85 T.P. 5.66 423.51
298+0	121.10	121.40	121.00 ✓	8.3 9.7 30.2		8.8 10.0 30.8	
+50	120.50	120.80	120.70 ✓	9.3 10.6 30.1		8.6 9.8 30.1	
297+0	120.91	120.21	120.71 ✓	8.9 9.9 30.7		1.8 3.3 30.0	429.97 X 2.36 427.47 B/F 427.48 817 X 320.00
+50	120.23	119.63	120.23 ✓	1.3 2.4 30.4		1.3 2.5 29.2	
296+0	119.74	119.04	119.11 ✓	3.7 4.7 30.7		3.6 4.6 30.9	
+50 = E.V.C. Culvert	119.15	118.45	119.05 ✓	0.1 1.2 30.5		0.0 1.0 30.0	
295+0	118.55 117.55	117.85	118.45 ✓ 117.45	0.5 1.5 30.3		0.6 1.7 30.7	
+50	117.85 116.85	117.15	117.75 ✓ 116.75	1.3 2.7 30.2		1.3 2.7 30.0	
294+0	117.10 116.10	116.40	117.00 ✓ 116.00	1.9 3.3 30.5		1.9 3.0 30.5	
293+50	115.35	115.65	115.25 ✓	3.0 4.4 30.4		3.8 5.0 30.9	

30670 Left $\frac{1}{2}$ Right
431.50' 430.80' 431.40'

Left $\frac{1}{2}$ Right
 $\frac{3.2}{3.2}$
 $\frac{3.2}{3.2}$
 $\frac{3.2}{3.2}$

429.77
3.03
426.74
429.66
429.73
422.43
12.30
434.73

750 430.90' 430.20' 430.80'

$\frac{3.8}{1.2}$
 $\frac{1.2}{1.2}$
 $\frac{3.8}{3.8}$

30510 430.22' 429.62' 430.22'

$\frac{0.8}{6.0}$
 $\frac{6.0}{6.0}$
 $\frac{0.8}{8.8}$

750 429.73' 429.03' 429.63'

$\frac{8.6}{5.6}$
 $\frac{5.6}{5.6}$
 $\frac{8.6}{8.6}$

435.07 x 25
5.26
430.21
435.42 x

30410 429.15' 428.45' 429.05'

$\frac{9.5}{1.6}$
 $\frac{1.6}{1.6}$
 $\frac{9.5}{2.9}$

750 428.55' 427.85' 428.45'

$\frac{1.1}{3.1}$
 $\frac{3.1}{3.1}$
 $\frac{1.1}{2.0}$

30310 427.97' 427.27' 427.87'

$\frac{1.7}{2.2}$
 $\frac{2.2}{2.2}$
 $\frac{1.7}{1.1}$

750 426.38' 426.68' 426.28'

$\frac{5.3}{3.3}$
 $\frac{3.3}{3.3}$
 $\frac{5.3}{8.2}$

428.5
428.57
429.55

30210 425.79' 426.09' 425.69'

$\frac{1.0}{1.0}$
 $\frac{3.1}{3.1}$
 $\frac{1.0}{1.4}$

750 425.20' 425.50' 425.10'

$\frac{1.6}{0.2}$
 $\frac{0.2}{0.2}$
 $\frac{1.6}{2.0}$

30110 424.62' 424.92' 424.52'

$\frac{5.8}{0.2}$
 $\frac{0.2}{0.2}$
 $\frac{5.8}{2.0}$

750 424.03' 424.33' 423.93'

$\frac{5.8}{0.2}$
 $\frac{0.2}{0.2}$
 $\frac{5.8}{2.0}$

30010 423.45' 423.75' 423.25'

$\frac{6.3}{0.8}$
 $\frac{0.8}{0.8}$
 $\frac{6.3}{2.15}$

$\frac{5.8}{0.2}$
 $\frac{0.2}{0.2}$
 $\frac{5.8}{2.0}$

312+0 Left 2 Right
 433.02' 433.55' 433.95'

Left 2 Right
 433.02
 +53
 380

311+91.79 50.1°44'22" out

+50 0°56'35" 433.37' 433.95' 434.55'

11.0
 +7.3
 383

9.7
 +7.1
 380

434.73
 1.84
 433.89
 17.83
 416.06
 439.57
 16.21
 439.787

311+00:71.86 433.73' 434.25' 434.65'

10.7
 +6.5
 352

9.7
 +6.0
 357

+50 434.05' 434.45' 434.85'

10.6
 +8.8
 348

9.7
 +6.1
 356

< 30.19
 1.21
 436.70
 2.36
 434.02
 4.63
 438.67

310+0 434.15' 434.45' 434.15'

10.3
 +7.9
 389

10.3
 +7.9
 387

+50 434.05' 434.35' 433.95'

10.6
 +6.4
 324

10.5
 +3.4
 336

309+0 433.75' 434.05' 433.65'

10.2
 +10.3
 203

10.8
 +12.2
 218

+50 433.35' 433.65' 434.25'

11.6
 +8.5
 281

9.5
 +1.8
 23.5

308+0 = P.V.C. 433.85' 433.15' 433.75'

9.9
 +1.6
 281

10
 +1.2
 282

+50 433.26' 432.56' 433.16'

8.5
 +2.2
 203

6.4
 +1.7
 287

307+0 432.67' 431.97' 432.57'

8.6
 +3.8
 332

7.6
 +3.5
 311

306+50 432.02' 431.32' 431.92'

8.1
 +7.0
 250

7.6
 +7.1
 329

	Left	±	Right
+50	121.55'	121.15'	121.75'
31840	122.70'	122.00'	122.60'
+50. P.V.C.	123.70'	123.00'	123.60'
31740	124.75'	124.05'	124.65'
+50	125.80'	125.10'	125.90'
31640	126.85'	126.15'	126.75'
+50	127.90'	127.20'	127.80'
31540	128.95'	128.25'	128.85'
+50	130.00'	129.30'	129.90'
31440 - F.V.C.	131.05'	130.35'	130.95'
+50	130.90'	131.30'	130.80'
31340	131.80'	132.15'	131.85'
312450	132.49'	132.90'	132.90'

	Left	±	Right
	121.55 -0.2 121.35		121.75 -0.2 121.55
	122.70 -0.2 122.50		122.60 -0.2 122.40
	123.70 -0.2 123.50		123.60 -0.2 123.40
	124.75 -0.2 124.55		124.65 -0.2 124.45
	125.80 -0.2 125.60		125.90 -0.2 125.70
	126.85 -0.2 126.65		126.75 -0.2 126.55
	127.90 -0.2 127.70		127.80 -0.2 127.60
	128.95 -0.2 128.75		128.85 -0.2 128.65
	130.00 -0.2 129.80		129.90 -0.2 129.70
	131.05 -0.2 130.85		130.95 -0.2 130.75
	130.90 -0.2 130.70		130.80 -0.2 130.60
	131.80 -0.2 131.60		131.85 -0.2 131.65
	132.49 -0.2 132.29		132.90 -0.2 132.70

129.701311m
 135.19
 139.61
 141.56
 142.30
 127.49
 127.691
 131.2
 141.57
 145.76
 125.3311m
 129.90 T
 128.2
 128.96
 127.90
 127.66
 125.80 T P

139.70
 139.61
 139.51
 139.43
 139.35
 139.27
 139.19
 139.11
 139.03
 138.95
 138.87
 138.79
 138.71
 138.63
 138.55
 138.47
 138.39
 138.31
 138.23
 138.15
 138.07
 137.99
 137.91
 137.83
 137.75
 137.67
 137.59
 137.51
 137.43
 137.35
 137.27
 137.19
 137.11
 137.03
 136.95
 136.87
 136.79
 136.71
 136.63
 136.55
 136.47
 136.39
 136.31
 136.23
 136.15
 136.07
 136.00

	Left	Z	Right
+50	422.30	422.60	422.90
331+0	422.00	422.30	422.90
+50	421.70	422.00	422.60
330+0 PVC	421.45	421.75	421.35
+50	421.20	421.50	421.80
329+0	420.94	421.24	420.81
+50	420.69	420.99	420.59
328+0	420.44	420.74	420.34
+50	420.18	420.48	420.08
327+0	419.93	420.23	419.83
+50	419.67	419.97	419.57
326+0	419.42	419.72	419.32
325+50	419.17	419.47	419.07

Left	Z	Right
3.51 1.5 1.5 1.5	1.31	3.61 1.3 1.0 1.3
4.01 1.5 1.5 1.5	4.51	3.91 1.6 1.3 1.0
5.3 1.5 1.5	4.01	4.2 1.3 1.0
5.36 1.5 1.5 1.5	5.06	4.46 1.6 1.3 1.0
6.3 1.5 1.5 1.5		5.4 1.3 1.0
6.6 1.5 1.5 1.5	6.3	5.7 1.6 1.3 1.0
6.8 1.5 1.5 1.5	6.5	6.2 1.3 1.0
7.1 1.5 1.5 1.5	6.8	6.5 1.6 1.3 1.0
7.3 1.5 1.5 1.5	7.3	7.1 1.3 1.0
7.6 1.5 1.5 1.5	7.6	7.4 1.6 1.3 1.0
7.9 1.5 1.5 1.5	7.9	7.7 1.3 1.0
8.2 1.5 1.5 1.5	8.2	8.0 1.6 1.3 1.0
8.5 1.5 1.5 1.5	8.5	8.3 1.3 1.0
8.8 1.5 1.5 1.5	8.8	8.6 1.6 1.3 1.0

429.328 81.500

Dec 14-1
426.47
427.53
427.53

429.32
429.32
429.32

421.17
421.17
421.17

	Left	#	Right
33870 = EVC	12045	12075	12035

+50	12055	12085	12045
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33770	12975	12905	12965
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+50	12885	12815	12875
-----	-------	-------	-------

32670	12810	12740	12800
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+50	12740	12670	12730
-----	-------	-------	-------

32520	12670	12600	12660
-------	-------	-------	-------

+50	12615	12545	12605
-----	-------	-------	-------

32410	12565	12495	12555
-------	-------	-------	-------

+50	12505	12435	12495
-----	-------	-------	-------

32320	12455	12385	12445
-------	-------	-------	-------

+50	12405	12335	12395
-----	-------	-------	-------

32220	12370	12300	12360
-------	-------	-------	-------

Left	#	Right
833 +83 750	914	831

157 -15 142	81	227
-------------------	----	-----

-16 -23 39	207	307
------------------	-----	-----

327 -23 304	83	327
-------------------	----	-----

-01 -12 11	102	172
------------------	-----	-----

172 -50 122	86	543
-------------------	----	-----

153 -102 51	543	612
-------------------	-----	-----

597 -66 531	66	667
-------------------	----	-----

34 -13 21	617	717
-----------------	-----	-----

707 -20 687	717	777
-------------------	-----	-----

39 -16 23	757	827
-----------------	-----	-----

807 -50 757	877	877
-------------------	-----	-----

38 -16 22	811	381
-----------------	-----	-----

Right	#
833 -83 750	931

167 -15 152	83
-------------------	----

-16 -23 39	217
------------------	-----

337 -23 314	83
-------------------	----

833 -83 750	112
-------------------	-----

482 -61 421	87
-------------------	----

154 -102 52	552
-------------------	-----

607 -66 541	66
-------------------	----

35 -13 22	657
-----------------	-----

717 -20 697	717
-------------------	-----

34 -16 18	767
-----------------	-----

812 -50 762	87
-------------------	----

39 -16 23	381
-----------------	-----

1275211
833
418
428.05
428.65
1275211
1280711

129501
512
13076
123121
879
12333
308
126811

	Left	±	Right
+50	115.20	115.50	116.10 F
357+0	116.25	115.55	116.15
+50	116.45	115.75	116.25
356+0	116.75	116.05	116.65
+50	117.20	116.50	117.10
355+0	117.75	117.05	117.65
+50	118.25	117.65	118.25
354+0 - RYE	119.20	118.50	119.10
+50	119.08	119.38	119.98 F
353+0	119.95	120.25	119.85
+50	120.83	121.13	120.73
352+0	121.71	122.01	121.61
351+50	122.60	122.90	122.50

Left	±	Right
6.3 2.9 +1.9 7.9	5.08	4.78
2.03 ✓ 5.2 -0.5 78.3	4.73	1.13 5.2 ✓ 3.1 35.2
5.8 2.9 -1.9 30.4	3.83	1.53
	4.7	3.93 5.6 ✓ -5.5 32.8
		4.8
	4.23	
4.3 2.7 -3.9 33.2	3.08	3.78
2.53	10.6 10.6 -7.8 33.0	3.23
19.0 1.2 -1.9 26.1	1.93	2.63
1.08	9.1 16.0 -10.9 78.9	1.78
9.1 8.3 +0.8 16.9	1.20	0.90
8.86	8.2 8.2 +1.9 11.9	8.56
7.5 6.5 -1.5 78	7.98	7.68
7.10	6.6 6.6 +1.9 78.9	6.80
5.7 2.0 -1.9 79.0	6.21	5.91

421.475
3.78
117.698 M/L31.2 417.18
16.265 M/L 387.18422.201 F/L
12.11
415.53
421.477 F/L120.201
0.30
412.28
8.83
422.8117.6
7.6
-1.5
31.57.20
6.7
+1.8
31.85.8
4.7
-1.7
21.7

+50	422.4°	421.72	422.30	1.9 2.2 2.8 28.6	4.52	5.22	1.1 1.2 1.2 3.5	4.62	1-14-32 36+50	26
364+0	Left	±	Right	1.9 2.2 2.8 27.9	5.05	5.75	1.0 1.2 1.2 3.5	5.15	421.47X 31.50 3.75 418.32 419.28 421.30T 425.08 ± 446 421.23 ± 31.20 1.26 423.68T Ford	
+50	421.89	421.19	421.79	5.58	1.0 2.2 2.8 26.4	6.21	5.68	1.4 1.2 1.2 3.5		
363+0	421.36	420.66	421.26	1.8 2.2 2.8 24.1	6.11	6.81	1.9 2.2 2.8 3.0	6.21		
+50	420.83	420.13	420.73	6.64	2.1 2.2 2.8 20.7	7.04	6.74	2.5 2.2 2.8 26.8	423.45T	
362+0	420.30	419.60	420.20	3.9 3.3 4.0 76.1	8.17	7.87	3.9 3.6 4.0 22.9	7.87		
+50	c 418.77	419.07	419.67	8.70	4.4 4.2 4.8 78.7	8.40	8.80	4.5 4.2 4.8 21.4	421.94T 8.77 418.17 421.11T 3.51 81/417 65.6 47.68	
361+0	418.24	418.54	418.14	5.0 4.5 5.0 20.5	3.45	3.15	5.1 4.6 5.0 22.5	3.55		
+50	417.71	418.01	417.61	3.98	5.5 5.0 5.5 21.5	3.68	4.08	5.6 5.1 5.5 23.5		
360+0 = FIC	417.18	417.48	417.08	3.7 3.3 4.1 22.4	4.51	3.85 4.21 4.37	4.1 3.6 4.1 22.4	4.61		
+50	416.65	416.95	416.55	4.13	1.0 1.2 1.2 21.7	3.83	4.33	1.0 1.2 1.2 3.5	31/4 21.8 HL 2.6 420.38T	
259+0	416.15	416.45	416.05	4.3 3.8 4.3 21.2	4.48	4.18	5.8 5.4 5.8 22.6	4.58		
+50	415.80	416.10	415.70	4.83	6.8 6.2 6.8 20.3	4.53	4.93	6.1 5.6 6.1 21.9		
358+0	415.45	415.75	415.25	6.3 5.8 6.3 19.0	4.98	4.68	6.3 5.8 6.3 21.0	5.08		

	Left	±	Right
371+0	125.25	125.55	125.15
+50	125.45	125.75	125.25
370+0	125.80	126.10	125.90
+50	125.80	126.10	125.90
369+0	125.90	126.00	125.60
+50	125.75	125.95	125.35
368+0	125.05	125.25	124.95
+50 - P.V.C.	125.60	124.90	125.50
367+0	125.07	124.37	124.97
+50	124.54	123.84	124.44
366+0	124.01	123.31	123.91
+50	123.48	122.78	122.38
365+0	122.95	122.25	122.85

Left	±	Right
13.5 2.5 +8.2 34.2	0.78	13.5 2.5 +9.0 39.0
13.2 2.2 +8.2 34.6	0.58	13.3 2.2 +8.7 38.7
13.8 2.8 +8.6 34.0	0.23	12.9 2.9 +8.2 37.2
13.8 2.8 +8.6 33.8	0.23	12.9 2.9 +8.2 36.2
6.9 1.9 +5.0 31.0	0.33	7.0 2.2 +5.2 34.4
7.1 2.7 +5.7 34.4	0.58	7.8 2.8 +5.2 32.2
7.5 2.5 +5.0 31.9	0.98	7.6 2.7 +5.7 36.7
10.6 2.9 +8.7 38.6	2.04	14.4 2.6 -2.1 34.7
-1.6 0.6 -2.2 20.8	1.87	2.57
2.40 -1.4 -3.5 28.8	3.10	2.50 -1.0 -4.2 28.8
-0.6 2.5 -5.1 26.2	2.93	3.63
3.4.6 0.0 -5.9 26.4	4.1	3.56 -0.1 -8.0 33.5
-0.5 1.3 -1.8 37.7	3.99	2.69
		0.6 9.8 -9.2 35.8

122.60 T.O.F. Fin
0.35
122.33
1.12
123.45 X
123.10
122.85
9.75
122.60 X
0.25
122.72
121.82
438.63 X Fall

124.33 X
126.27
125.39
127.10
126.94 X

	Left	±	Right		Left	±	Right	
377+0	11588	11518	11579		115 147 152 353	109	178	115 87 23 250
+50	11691	11621	11681		305 715 59 263	395	315	51 80 34 251
376+0	11794	11724	11784		11 92 54 256	302 206 70	172	15 17 23 250
+50	11897	11827	11887		009 199 70	34 28 38 232	169	109 53 23 227
375+0	11999	11929	11889		34 42 22 37	936 100 70	1004	35 39 26 306
+50	12002	12032	11992		931 23 90 70		901	94 87 27 217
374+0 = E.V.C.	12105	12135	12095		138 117 171	889	798	120 104 55 225
+50	12210	12240	12200		783 77	117 781	693	733 118 125 222
373+0	12290	12320	12280		109 92 73 79.5	613	613	110 150 150 250
+50	12365	12395	12355		518 104 52 459 21.0		538	578 103 88 76.5 262
372+0	12435	12465	12425		95 37 22	498	418	91 119 277 277
+50	12485	12515	12475		448 90 7.4 254		418	408 91 66 285 285
371+2604 100°02'18"	12504	12534	12494		136 52 72 328	449	399	137 26 190 390

ASBUT & F
9.55
BM 439.08 #7

BM 439.07 #7
4.78
4338.51
121.41
121.93
122.37 #7

419.61
2.56
419.93
129.331

BM #7
439.07 #7
29.12 371.79

513 00 24.6

750
Left 401.95 402.25 Right 401.85

Left 8.54 8.00
 8.00
 7.60
Right 8.24 8.64
 8.64
 8.15

122.371 31.60
70.88
416.70
415.281
415.277
P 409.56 38000
109.91 A Ford

382+0
750
Left 402.85 403.15 Right 402.75

7.10 7.64 7.34 7.74 7.74
 7.00
 7.15
 7.15

750
Left 403.75 404.05 Right 403.65

6.74 6.24 6.44 6.84 6.34
 6.00
 6.00
 7.00

382+0
750
Left 404.70 405.00 Right 404.60

5.54 5.99 5.99 5.34 5.89
 5.00
 7.00
 8.14

100.90 P
26.91
410.91
410.97
11.22 show
P 408.75 38000
11.22
419.96 A

750
Left 405.65 405.95 Right 405.55

4.84 4.34 4.54 4.94 4.44
 4.00
 4.00
 7.00

382+0 = AVG
750
Left 406.65 406.95 Right 406.55

3.34 3.84 3.54 3.04 3.94
 3.00
 7.00
 8.14

750
Left 407.62 407.99 Right 407.59

2.80 2.24 2.50 2.90 2.34
 2.00
 7.00
 7.60

380+0
750
Left 408.71 409.01 Right 408.61

6.64 6.14 6.44 6.74 6.24
 6.00
 7.00
 7.00

750
Left 410.74 410.04 Right 410.64

9.22 8.74 9.94 10.32 9.84
 8.00
 7.00
 7.99

379+0
750
Left 411.77 411.07 Right 411.67

3.54 3.04 3.34 3.64 3.14
 3.00
 7.00
 8.14

750
Left 412.80 412.10 Right 412.90

7.14 6.64 7.84 7.34 7.84
 7.00
 7.00
 7.00

378+0
750
Left 413.83 413.13 Right 413.73

8.54 8.04 8.84 8.34 8.84
 8.00
 7.00
 7.00

377+50
750
Left 414.85 414.15 Right 414.75

5.11 4.61 5.81 5.31 5.81
 5.00
 7.00
 7.00

	Left	#	Right
39070	399.05	399.35	398.95
+50	398.40	397.70	398.30
38970	398.05	397.35	397.95
+50	397.90	397.20	397.80
38870	397.95	397.25	397.85
+50	397.00	397.30	396.90
38770	397.30	397.60	397.20
+50	397.70	398.00	397.60
38670	398.25	398.55	398.15
+50	398.95	399.25	398.85
38570	399.10	399.90	399.50
+50	100.35	100.65	100.85
38470	101.10	101.40	101.00

	Left	#	Right
	10.11	10.84	10.81
	1.1	0.84	1.54
	2.4	0.89	1.89
	1.0	1.34	5.04
	4.89	1.99	4.39
	2.8	5.24	4.94
	4.94	4.64	5.04
	2.6	4.54	4.64
	3.99	3.69	4.09
	1.69	3.39	2.99
	3.64	2.34	2.74
	2.6	1.59	2.6
	1.14	0.84	1.64

109.91
10.40
399.57
399.83
399.87 Ford

119.19
10.40
398.57
400.24
400.98 TP

BM # 8
396.58
Hub 828-35722

399.84
399.84
BM 396.60 # 8

402.24
5.65
BM 396.59 # 8

	Left	±	Right
39640	41395	41435	41385
+50	41238	41268	41228
39540	41082	41112	41072
+50	40925	40955	40915
+820	Out	40867	
39410 = Δ 0° 15' 00" 64°	40768	40798	40858
+50	40712	40642	40702
39340 = Δ 10'	40555	40485	40545
+50	40405	40335	40325
39240	40275	40205	40265
+50	40165	40095	40155
39140	40055	39985	40045
390450	39970	39900	39960

Left	±	Right
11.3 7.6 3.7 19.7	5.65	5.95
7.33 13.8 13.3 19.3	6.92	7.32
3.1 1.3 1.8	8.78	8.48
10.35 5.9 3.9 14.7	10.05	10.45
6.6 5.5 1.1 17.1	11.27	11.62
4.97 7.6 8.0 18.9	2.77	3.17
8.3 10.3 2.0 30.5	3.14	4.34
5.14 8.5 3.4 21.1	6.34	5.84
11.2 4.3 6.9 31.9	6.44	7.14
7.56 2.5 5.0 22.8	8.84	7.64
3.6 7.2 3.6 20.7	8.14	9.34
9.49 4.5 8.7 23.8	10.19	9.59

1-29-32
390450 **31**
399 413.8
399 414.3
399 413.8
399 412.3
399 412.7
399 412.2
399 410.8
399 411.1
399 410.7
399 409.2
399 409.5
399 409.1
399 408.6
399 408.5
399 408.6
399 408.7
399 408.8
399 408.9
399 409.0
399 409.1
399 409.2
399 409.3
399 409.4
399 409.5
399 409.6
399 409.7
399 409.8
399 409.9
399 410.0
399 410.1
399 410.2
399 410.3
399 410.4
399 410.5
399 410.6
399 410.7
399 410.8
399 410.9
399 411.0
399 411.1
399 411.2
399 411.3
399 411.4
399 411.5
399 411.6
399 411.7
399 411.8
399 411.9
399 412.0
399 412.1
399 412.2
399 412.3
399 412.4
399 412.5
399 412.6
399 412.7
399 412.8
399 412.9
399 413.0
399 413.1
399 413.2
399 413.3
399 413.4
399 413.5
399 413.6
399 413.7
399 413.8
399 413.9
399 414.0
399 414.1
399 414.2
399 414.3
399 414.4
399 414.5
399 414.6
399 414.7
399 414.8
399 414.9
399 415.0

	Left	±	Right	
150	429.80	430.10	430.70	
10270	429.40	429.70	430.30	F
150	428.90	429.20	429.80	
10140	428.20	428.50	429.10	
150	427.30	427.60	428.20	
10040	426.65	426.55	427.15	
150	425.85	425.15	425.75	F
39940 P.V.C	423.35	423.65	423.25	
150	421.79	422.09	421.69	
39940	420.22	420.52	420.12	
150	418.65	418.95	418.55	
39940	417.09	417.39	416.99	
399450	415.52	415.82	415.72	

Left	±	Right	
3.7 3.4 70.3 76.3	2.96	3.06	3.3 3.2 3.5 3.8
4.1 3.6 70.7 76.7	3.36	3.36	3.3 3.2 3.5 3.8
4.1 3.5 71.7 77.1	3.86	3.86	3.7 3.5 3.8 4.1
5.3 4.2 70.9 76.9	4.56	4.56	4.4 4.3 4.6 4.9
5.7 4.2 70.7 76.7	5.16	5.16	5.3 5.2 5.5 5.8
7.3 6.5 70.8 76.8	6.56	6.56	6.4 6.3 6.6 6.9
8.1 7.2 71.1 77.1	7.96	7.96	7.8 7.7 8.0 8.3
1.9 0.3 71.6 77.6	9.76	9.76	9.8 9.7 10.0 10.3
9.0 7.5 78.9 84.9	8.76	8.76	8.6 8.5 8.8 9.1
5.9 2.3 78.3 84.3	10.58	10.58	10.5 10.4 10.7 11.0
13.15 3.6 83.8 89.8	11.85	11.85	12.25 12.1 12.4 12.7
8.3 5.1 83.1 89.1	2.51	2.51	2.3 2.2 2.5 2.8
1.8 0.2 89.6 95.6	3.78	3.78	3.8 3.7 4.0 4.3

425.217 B. find
0.27 on 41.500
422.97
9.56
423.537 find

433.537
3.1
430.437

BN 430.437
Nail Loop Plug
1000 ft. 1000 ft. 1000 ft.

Finish Station

BN 130.437
2.63
133.061 find

3.70-82

430.437
0.37
430.807
1.8.97
0.66
419.607

	Left	±	Right
10970	124.10	123.40	123.00
+50	125.05	124.35	123.95
10870	125.85	125.15	124.75
+50 - P.V.C.	125.65	125.95	125.55
10770	126.31	126.61	126.21
+50 Last Popular Sedan	126.97	127.27	126.87
10670	127.63	127.93	127.53
+50	128.29	128.59	128.19
10570 = F.V.C.	128.95	129.25	128.85
+50	129.45	129.75	129.35
10470	129.85	130.15	129.75
+50	130.05	130.35	129.95
10370	130.05	130.35	130.95

	Left	±	Right
	126.56 8.5 8.5 1.3 19.5		126.16 4.5 8.7 70.8 20.8
	7.5 1.7 20.1	7.04	8.1 7.44 10.5 20.5
	6.54 6.6 7.6 19.7	6.32	6.14 7.8 10.3 20.3
	6.9 6.0 16.0	5.72	7.3 7.07 20.7
	5.08 6.5 10.8 16.0	4.78	5.11 6.3 7.0 20.8
	5.1 2.4 10.9 16.9	4.13	4.18 5.7 1.8 20.0
	3.76 4.9 6.6 17.0	3.26	3.86 5.5 2.3 21.7
	4.3 3.7 17.4	3.10	3.5 3.3 1.7 20.1
	4.11 3.6 2.5 17.1	3.81	3.7 1.5 1.8 20.2
	3.1 1.3 17.0	3.31	3.3 1.3 1.9 20.9
	3.21 3.7 3.5 10.7 16.9	2.91	3.31 3.8 3.6 2.6 20.6
	3.5 3.5 1.5 17.5	3.71	3.6 3.3 10.3 20.3
	3.01 3.5 1.4 16.4	3.71	3.11 3.6 3.9 1.4 20.3
			433.53 T. Bl. Fair 2.73 P. 130.81 12.74 432.55 T
			433.06 T. Bl. Fair 1.94 130.13 1.27 431.39 T 7.04 432.35 6.04 424.66 T. Fair

Lif & R96

41813592 = End of Kayak
 393 = 5568 - 5013 = 555
 385.25 385.55 385.15 -0.40

41812415 386.76 387.09 386.79 -0.30

41717415 389.00 389.41 389.41 0.00

41712445 = FC 11°53'30" 391.21 391.73 391.13 +0.60

41617415 10°56'13" ^{394.05}
~~393.75~~ 394.05 394.77 +0.70 0.70

41612415 9°58'56" ^{396.38}
~~395.74~~ 396.38 397.32 +0.90 0.90

402367 81/100
 396.77 0.00
 117.11 1.00

401117

9.9°	$\frac{11}{60}$	9.85	9.88	$\frac{10}{60}$
	$\frac{11}{60}$			$\frac{10}{60}$
				$\frac{10}{60}$
8.3	7.06	7.06	$\frac{7}{60}$	6.34
$\frac{8.3}{7.6}$			$\frac{13.0}{33.7}$	
1.83	$\frac{6.0}{7.6}$	1.83	1.77	$\frac{5.0}{3.2}$
	$\frac{6.0}{7.6}$			$\frac{1.8}{3.2}$
	$\frac{6.0}{7.6}$			35.2

Culvert 389+0 ALFA CMP

0+0 = Inlet
 0+23.5 = High bridge
 0+53.0 = Outlet
 E. Endline
 394.60 ^{5.59} 70.71
 94.18
 396.58
 400.17
 397.00 ^{4.19} 70.6
 71.23
 402.31

389+19 = 5' Inlet
 389+0
 388+93 = 5' Outlet
 398.18
 398.08
 398.03
 397.93
 95 | 11 | 18 | 115
 397.98
 397.02

Left S
 2.18
 -3.02
 398.18
 2.01
 3.06
 -3.06
 398.03
 2.11
 4.91
 -3.78
 2.05
 2.78
 Right S
 398.08
 2.11
 3.09
 397.93
 2.26
 4.85
 -3.89
 1.38
 2.88
 -3.82

Culvert 298+20 28' 34' CMP

0+0 = outlet 21' Gas Pipe
 0+25 = outlet 10' 11' CMP
 70' 10"

Lo Solla-Miramar Road

Indexed
c.s.k.

12-3-31

4-1-32
Finish Grade

Left L Right

Left Right

B/M 395.70
6.96
402.56

3+26.86	53°30'30"	398.84	98.55 398.30	399.54	84 395.70 5.71 401.41
3+76.86	21°25'30"	398.41	97.55 397.88	399.32	
3+126.86	12°30'30"	397.98	97.02 397.98	399.98	397.16 Edge of Pav 0.74
1+89.58	15°19'16"	397.68	96.83 397.18	398.68	
1+53.30	11°14'11"	397.38	96.51 396.88	398.38	
2c. 372.6					2580-39.92
1+15.02	8°11'06"	397.08	96.33 396.58	398.09	
0+65.02	1°05'22"	396.69	96.00 396.16	397.60	
2c. 499.6					2580-53.53
0+15.02	BC 350.4	396.29	95.67 395.75	397.00	
0+0	1/4 Edge of Pav Pav	395.11	96.16 395.86	396.16	Edge of Pav 0.74

2.35	2.57	3.55			
2.78	2.00	4.00	3.50	3.00	
3.21	3.15	4.1	4.11	3.4	4.25
3.51	3.73	4.7	4.32	3.7	4.25
3.81	4.03	5.0	4.63	4.0	4.36
4.11	4.33	5.3	4.86	4.3	4.51
4.50	4.73	5.7	5.19	4.8	4.76
4.92	5.13	6.1	5.52	5.4	4.96

B/M 409.60
1.82
410.82
11.22
399.60
1.59
401.19

5'
3'22"
3'22"
3'22"
5'

0.11
0.11

Torrey Pines Lodge Road
14 Lt

Index
c.s.k.
18 Rt

Left ± Right

3770.48 396.32 395.62 396.22

3720.48 398.08 397.38 397.98

3770.48 399.83 399.13 399.73

3738.08 400.98 400.28 400.88

2705.68 402.12 401.42 402.02

1755.68 404.43 403.15 403.42

1705.68 - FC 406.74 404.90 404.82

0782.12 407.47 405.73 405.65

0758.56 408.21 406.56 406.48

0735 - BC Pt 408.95 407.39 407.31

0705 - 1/4 Mile Old Parking 409.62 408.62 409.22

Left ± Right

11.40 4.8
9.1
4.8
24.0

3.9 9.64 10.34 3.1 9.74
2.7
5.7
26.1

7.89 1.3
8.0
6.7
24.6

9.1 6.74 7.54 0.6
7.0
28.0

5.6 7.0
6.5
7.5
28.8

-3.3 3.39 1.57 2.8
4.5
17.8
29.2

0.98 6.4
14.3
9.9
29.4

5.7 10.67 13.41 7.5 13.49
11.7
5.1
25.6

9.93 5.05
6.5
19.8

4.3 9.19 10.75 5.8
11.1
17.5

2-5-32

41

R 411.43 11410
1.75
413.781
12.90
400.38
0.73
401.71 1 For

Field Grain
2-15-32

419.88 11410
0.32

418.74

405.75

407.72

394.27

398.07

Left L Right

Left L Right

40.11 21.500

328.017

5+26.64 = EC 7'41"30 390.13 390.13 390.13

$$\begin{array}{r} 11.0 \\ 11.0 \\ 9.0 \\ \hline 16.0 \end{array} \quad 7.88$$

$$\begin{array}{r} 11.0 \\ 9.2 \\ 4.7 \\ \hline 21.7 \end{array}$$

4+91.26 5'07"40 391.38 391.38 391.38

$$\begin{array}{r} 6.63 \\ 8.7 \\ 8.7 \\ 6.0 \\ \hline 16.0 \end{array} \quad 6.63$$

$$\begin{array}{r} 6.6 \\ 8.7 \\ 8.7 \\ 2.0 \\ \hline 21.0 \end{array}$$

4+55.87 2'33"50 393.62 393.62 393.62

$$\begin{array}{r} 7.5 \\ 9.2 \\ 1.7 \\ \hline 20.1 \end{array} \quad 4.39$$

5.39

$$\begin{array}{r} 7.5 \\ 8.7 \\ 0.2 \\ \hline 22.4 \end{array} \quad 4.39$$

4+20.48-8c 394.86 393.86 394.86

$$\begin{array}{r} 3.15 \\ 1.2 \\ 8.2 \\ 1.2 \\ \hline 22.1 \end{array} \quad 4.15$$

$$\begin{array}{r} 3.15 \\ 6.3 \\ 0.8 \\ \hline 22.7 \end{array}$$

Crosby St.
10ft Gutter National to H. Line of Alley
on East Side Crosby

Indexed
c.s.K.

Feb 23 33
Moore 43

Log 97

	39.72		
	39.41	39.73	39.82
			39.35
Brk	37.95	38.27	37.96
		38.37	
	37.50	37.72	37.86
			37.32

Crosby

National

Moses St Grade
S.L. Congress to AT&SF R.R. P.P. & W

Indexed
c.s.K.

2-10-30
Moore
Sisson
Hortbarb 14

	F Curb Grade	W Curb Grade	
S.L. Congress	19.00	18.50	BM 21.35 5.12 26.53
50's	19.25	18.75	
100's	19.50	19.00	
150's	19.75	19.25	
200's	20.00	19.50	
250's	20.25	19.75	
300's = All Jefferson	20.50	20.00	BM 21.35

S.L. Jefferson	18.50	18.75	2.83 2.77 24.65 12.13 12.25 1487.1
65's	13.15	13.77	
130's = P.V.G.	7.80	8.00	
150's	6.60	6.65	
170's	6.20	6.20	

F	19.00	19.25	19.50	19.75	20.00	20.25	20.50
	7.5	7.3	7.0	6.8	6.5	6.3	6.0
	6.7	6.3	6.1	5.9	5.5	5.3	5.0
	+0.8	+1.0	+0.9	+1.3	+1.2	+1.7	+2.0

W	18.50	18.75	19.00	19.25	19.50	19.75	20.00
	8.0	7.8	7.5	7.3	7.0	6.8	6.5
	7.4	6.5	6.2	6.2	5.6	5.3	5.2
	+0.6	+1.3	+1.3	+1.2	+1.4	+1.5	+1.3

F	18.50	13.15	7.80	6.60	6.20
	8.0	7.0	7.1	6.3	6.5
	5.4	4.8	4.7	4.5	4.2
	+0.4	+0.7	+1.6	-0.2	

W	18.75	13.77	8.00	6.65	6.20
	7.8	7.4	6.9	6.2	6.5
	6.8	3.4	5.9	4.1	4.9
	+2.8	+7.0	+1.0	-0.9	

Jefferson St. Grade
47' E of E.L. Mason From So. to AT&SF RR Ref. N

	S	N	
47' E of E.L. Mason From So.	21.00	23.50	21.53 N 12.35 14.18 3.28 17.90 N
E.L. Mason From N	19.25	19.75	
H.L. Mason	19.50	20.00	
50' N	19.75	20.25	
100' N = E.L. Mason From N	20.00	20.50	
H.L. Mason	19.50	20.00	
40' N = P.C.	17.90	18.40	
60' N	16.80	17.20	
80' N	15.00	15.30	
100' N = F.V.C.	12.70	13.10	
120' N	10.00	10.20	
140' N	7.80	8.00	
160' N	6.50	6.50	

indexed
c.s.k.

45

N	23.50	19.75	20.00	20.25	20.50		
	3.0	6.8	6.5	6.3	6.0		
		2.0	1.3	1.0	1.0		
		4.8	2.2	2.0	2.8		
S	21.00	19.25	19.50	19.75	20.00		
		7.3	7.0	7.8	6.5		
		5.2	5.0	4.8	4.9		
		11.7	12.0	12.0	11.7		
N	20.00	18.40	17.20	15.20	13.10	10.20	8.00
	1.5	2.1	2.3	1.3	1.1	1.3	1.5
	17.3	16.3	16.3	16.3	16.4	16.5	16.5
		1.0	1.1	1.4	1.6	1.8	1.9
		1.0	1.1	1.4	1.6	1.8	1.9
S	19.50	17.90	16.80	15.00	12.70	10.00	7.80
	7.0	8.1	8.7	11.5	13.8	16.5	10.2
	6.9	5.9	6.1	6.8	7.4	8.0	11.8
	12.0	12.7	13.6	14.7	16.4	17.5	16.6

Garbage Disposal Plant 5/9/23

P. Lot 1175

Moore
Sisson
Northern

B.M.	O.P.P.	100.88	100.00	0.7 Hubs 12" of W Edge
0+0			100.0	
+8		0.9	98.5	
+12		2.4	97.2	
+12		3.7	91.9	
+15		9.0	89.9	
+25		11.0	84.0	
+35		16.9	79.9	

1.00 101.00 100.0

Bench level = Pl. 85.50
Top = 98.50

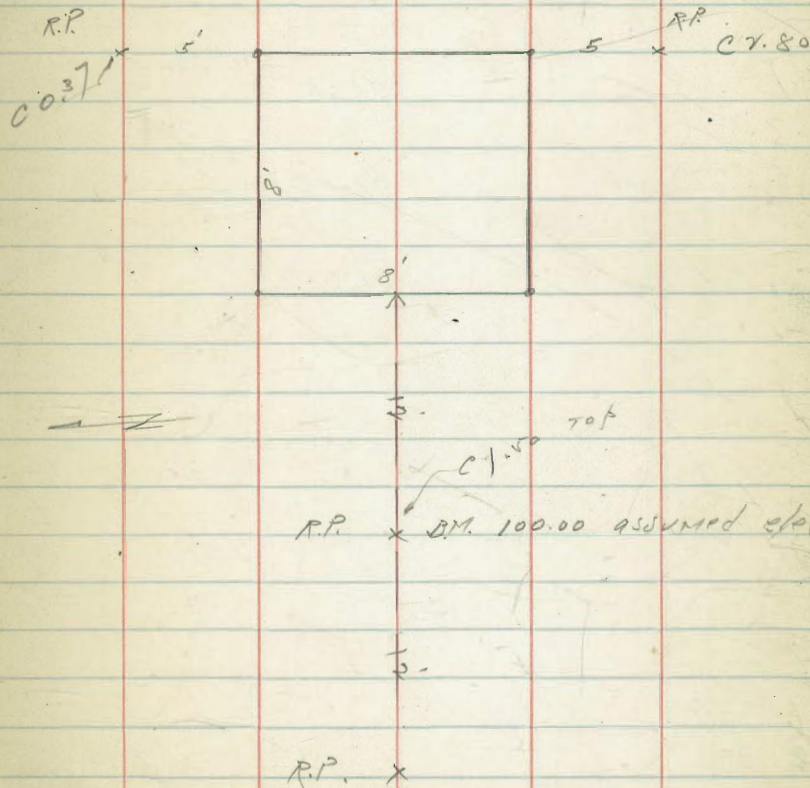
Indexed
C.S.K.

15.50
15.13
+0.37

101.00
98.50
2.50
+1.5

101.00
85.50
15.50
12.70
+2.80

5.9.23 46
Moore
Sisson
Northern



Columbia & Chalmers
Toe Hall

Indexed
C.S.K.

5-10-33
Moore 47

Stakes 3' E of E Side Toe Hall

S.F.B.P
Chalmers
Columbia

B.M. 5.28 102.39 97.11

N Edge Conc Gutter Top of Toe Hall 96.26 6.13

H 14 96.55 5.84

L 96.65 5.74

S 14 96.54 5.85

Edge Sol Gutter 96.20 6.19

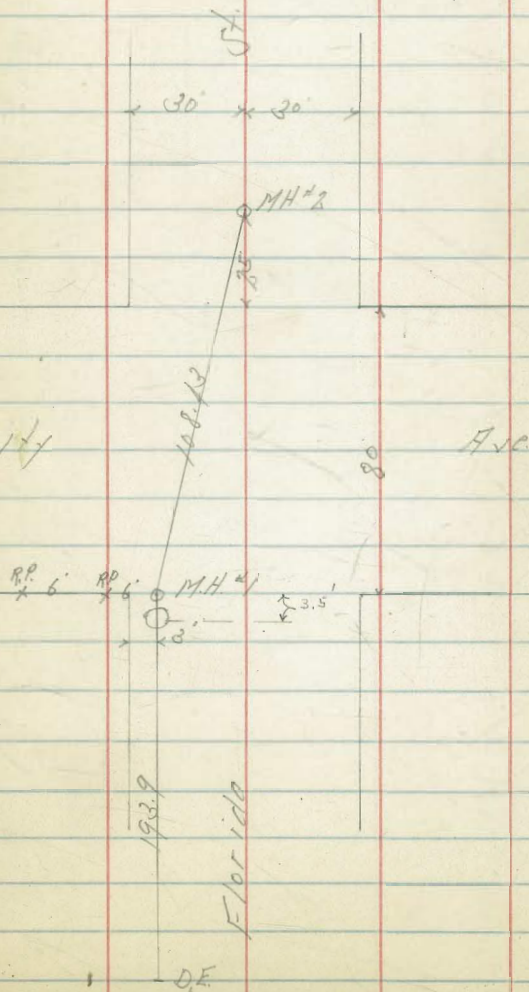
Florida St. A. University Fin.
 Sewer Construction

M.H. #2 - 25' N of M.H. Univ 2' Florida	278.50	18.03 14.68 +6.35	17.75 10.21 +7.54
15' S	278.78	17.48 9.55 +7.93	17.20 9.31 +7.89
30' S	279.05	16.93 9.33 +7.60	16.85 9.17 +7.68
45' S	279.33	16.37 9.05 +7.32	16.03 8.81 +7.22
60' S	279.60	14.53 8.81 +5.72	13.28 8.05 +5.23
75' S	279.88	10.03 4.77 +5.26	7.78 2.16 +5.62
90' S	280.16	5.53 0.36 +5.17	
108.43' S D.M.H. #2 - St. Univ 3' 2" of M.H. Florida	280.50		
	282.00		
156.90' S	284.25		
205.38' S	286.50		
253.86' S	288.75		
302.33' S - D.F.	291.00		

Indexed
 C.S.K.

6-1-33
 Mount
 Sisson 48
 Northway

B.M. 28709 S.W. B.P.
 University of Florida
 2.45
 298.531



Main St.
R. of Way Survey.

9-24-36
Miles
Walker
Bliss

Indexed
C.S.K.

49

				Grade N. curb El	Grade N. Line El	Gr. Rd
B.M. Hub R.P.	8.08	12.07	3.99	9.06	9.18	
4+30.94						
3+62.5	W. Side Bldg				9.04	3.63
3+30	E. side Bldg					
0+72.79				8.35	8.47	3.09

Pershing Drive. Slope stakes
Continued from G 177-53

Grade w. edge
Gutter = E.
= bottom
Bank.

1/2 to 1 Slope

Indexed
C.S.K.

22. R.P.	B.M. 5187	1.28	136.79	135.51	E. Edge Ex Pav.	121.85	121.6	R.P. Hub. 22 E. of E. Edge Ex Pavmt. G 177-53.
E.C.								145.0
6+00							122.1	8.8 136.2 122.1 +14.1 out. 7.0
+50		11.32	125.47	125.2				153.8 12.3 141.5 125.2 +17.3 out. 8.7
7+00		8.44	128.35	128.2				5.9 147.9 128.2 +19.7 out. 9.8
+50		5.40	131.39	131.2				1.8 152.0 131.2 +20.8 out. 10.4
8+00		2.37	134.42	134.2				166.31 10.3 156.0 134.2 +21.8 out. 10.9
T.P.	11.58	147.67	0.70	136.09				7.1 159.2 137.2 +22.0 out. 11.0
+50		10.27	137.40	137.2				
+ 47 1/2 POT.								
9+00		7.15	140.52	140.3				5.3 141.0 140.3 +10.7 out. 10.3
+50		4.05	143.62	143.4				3.8 142.5 143.4 +19.1 out. 9.5
10+00		1.27	146.40	146.2				2.8 143.5 146.2 +17.3 out. 8.6
T.P.	12.80	160.17	0.30	147.37				176.22 11.4 164.2 148.6 +15.6 out. 8.1
+50		11.40	148.77	148.6				
11+00		9.13	151.04	150.9				10.3 165.9 150.9 +15.0 out. 7.5
+50		7.07	153.10	152.9				9.2 166.9 152.9 +14.0 out. 7.0

160.17

π 176.22

1/2 to slope

12+00 5.08 155.09 154.9

8.3
167.9
154.9
+13.0 out. 6.5

+50 3.34 156.83 156.6

7.6
168.6
156.6
+12.0 out. 6.0

13+00 1.60 158.57 158.4

6.3
169.9
158.4
+11.5 out. 5.7

T.P. 11.03 171.08✓ 0.12 160.05✓

+50 10.83 160.25 160.0

5.4
170.8
160.0
+10.8 out. 5.4

14+00 9.20 161.88 161.7

5.2
171.0
161.7
+9.3 out. 4.6

+50 7.58 163.50 163.3

4.7
171.5
163.3
+8.2 out. 4.1

15+00 6.12 164.96 164.7

5.2
171.0
164.7
+6.3 out. 3.2

T.P. 5.20 176.22✓ 0.06 171.02✓

T.P. 0.72 166.31✓ 10.63 165.59✓

T.P. 0.09 153.77 12.63 153.68✓

T.P. 3.58 144.98✓ 12.37 141.40✓

Moore
4-19-29

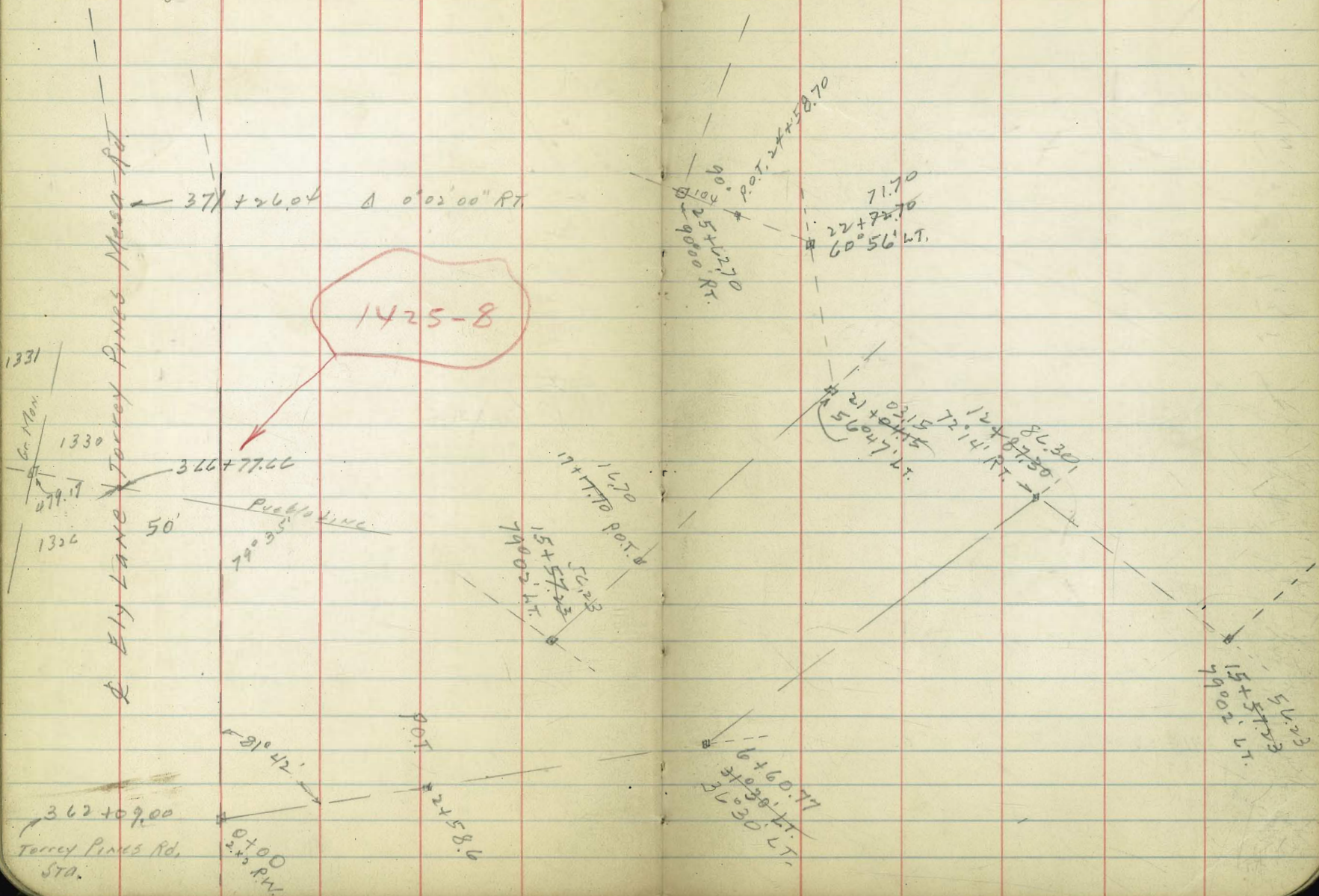
Survey for lease for
U.S. Agric. Exp. Sta.

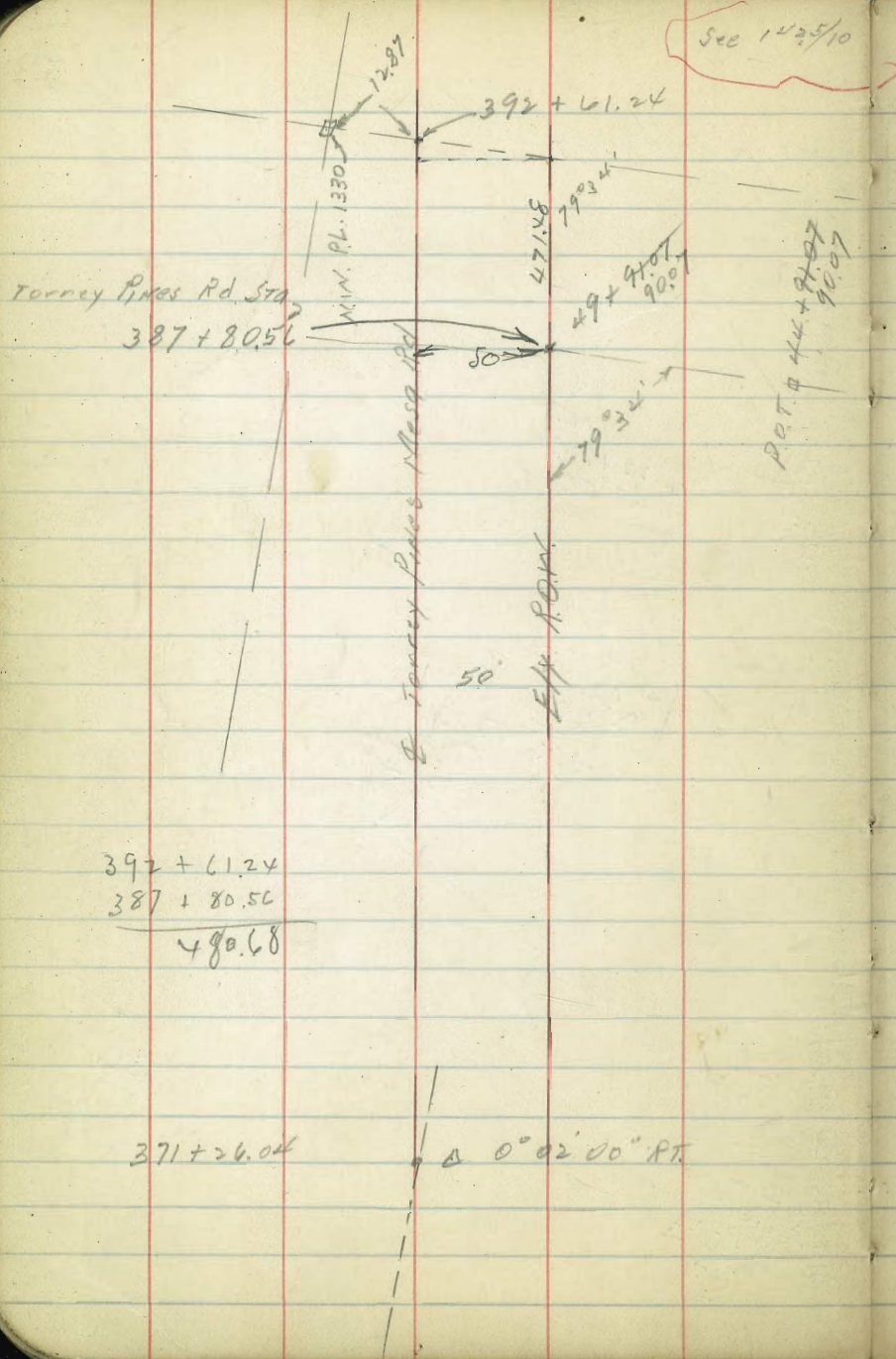
Indexed
C.S.R.

Cont. P. 54

53

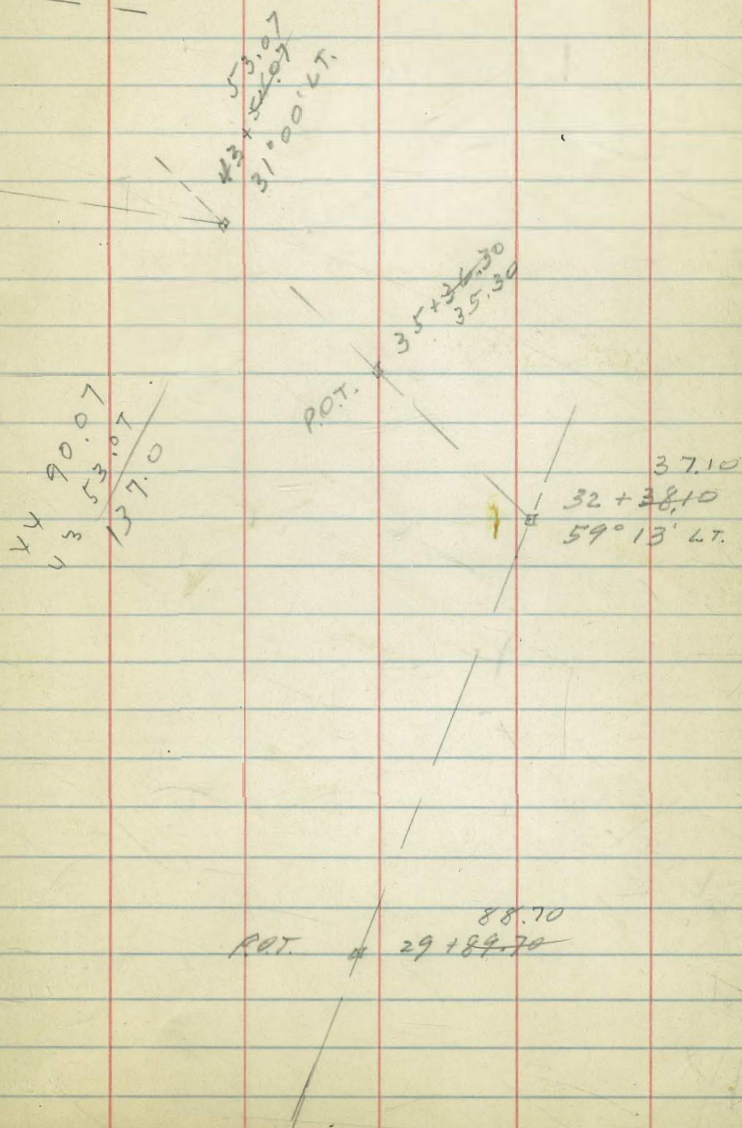
P.O.T. # 29+88.70





392 + 61.24
387 + 80.56
490.68

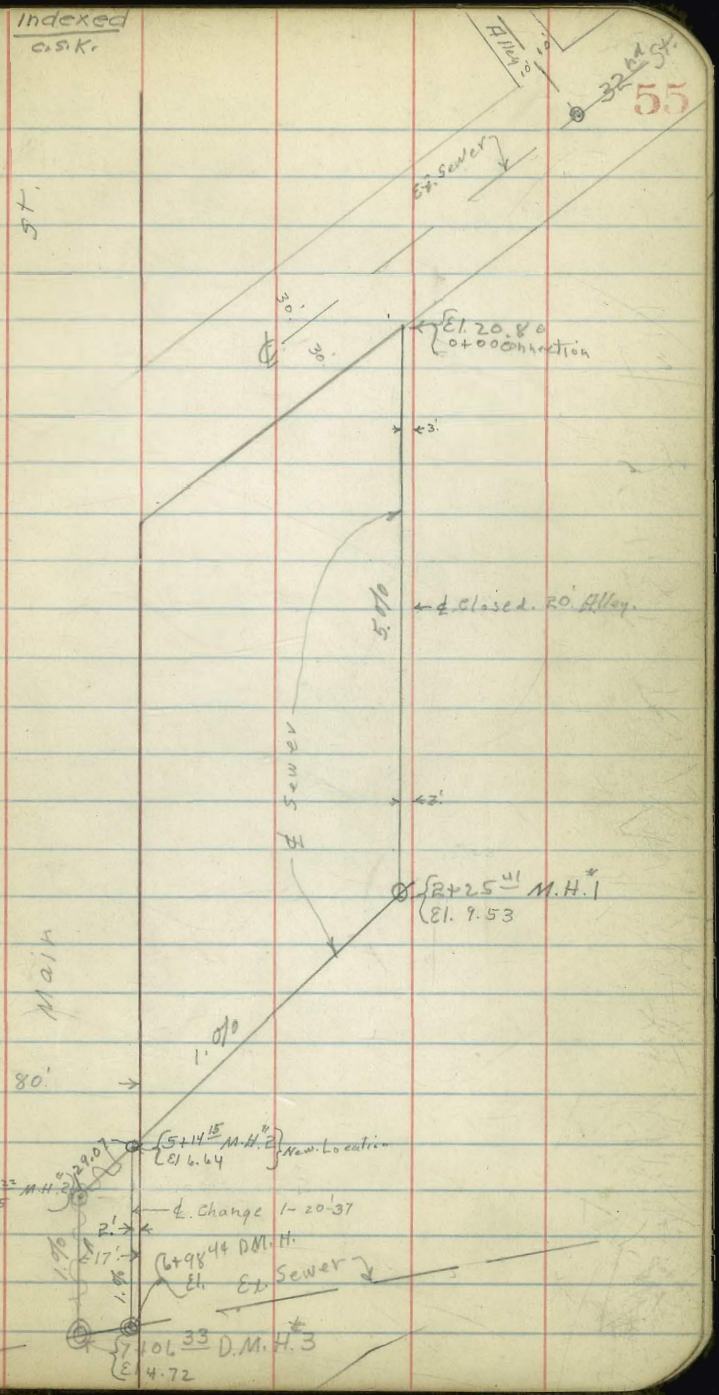
Survey Lease
U.S. Agr. Exp. Sta.



1-19-27
Miller
Walker
Bliss

Sewer Construction.
BIRs 248 + 249 South Chollas. Add.

BM	BF	1.20	40.06	38.86	s.w. 32 nd Main	
connection	0+00 = 8. Line 32 nd St.		1.02	39.04	20.80	+18.24 ✓
0+25		6.74	33.32	19.55		13.77 ✓
0+50		9.64	30.42	18.30		+12.12 ✓
T.P.	0.95	28.36	12.65	27.41		
1+00		2.58	25.78	15.80		+9.98 ✓
+50 T.P.	5.79	21.87	12.28	16.08	18.30	+2.78 ✓
2+00		7.91	13.96	10.80		+3.16 ✓
+25 th M.H. #1		8.34	13.53	9.53		+4.00 ✓
+50		9.04	12.83	9.28		+3.55 ✓
3+00		8.27	13.60	8.78		+4.82 ✓
+50		11.31	10.56	8.28		+2.28 ✓
4+00		11.91	9.96	7.78		+2.18 ✓
+50		11.97	9.90	7.28		+2.62 ✓



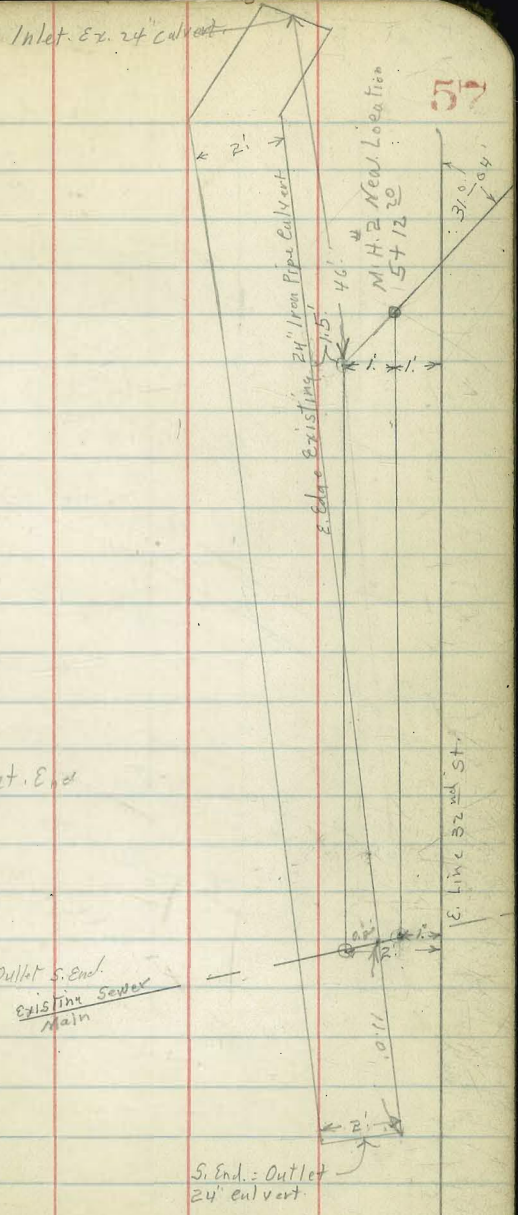
120-37. change of Alignment

T.P. Page 56	2.66	19.63	16.97			
M.H. 2 New Location						
5+12 ²⁰		1.59	18.04	6.64	+11.401	
5+50		2.84	16.79	6.28	+10.511	
6+00		5.05	14.54	5.78	+8.801	
6+50 T.P.	7.70	20.37	6.96	12.67	5.28	+7.391
6+98 ⁴⁴ D.M.H. 3		9.40	10.97	4.80	+6.171	
Connection Ex Main						

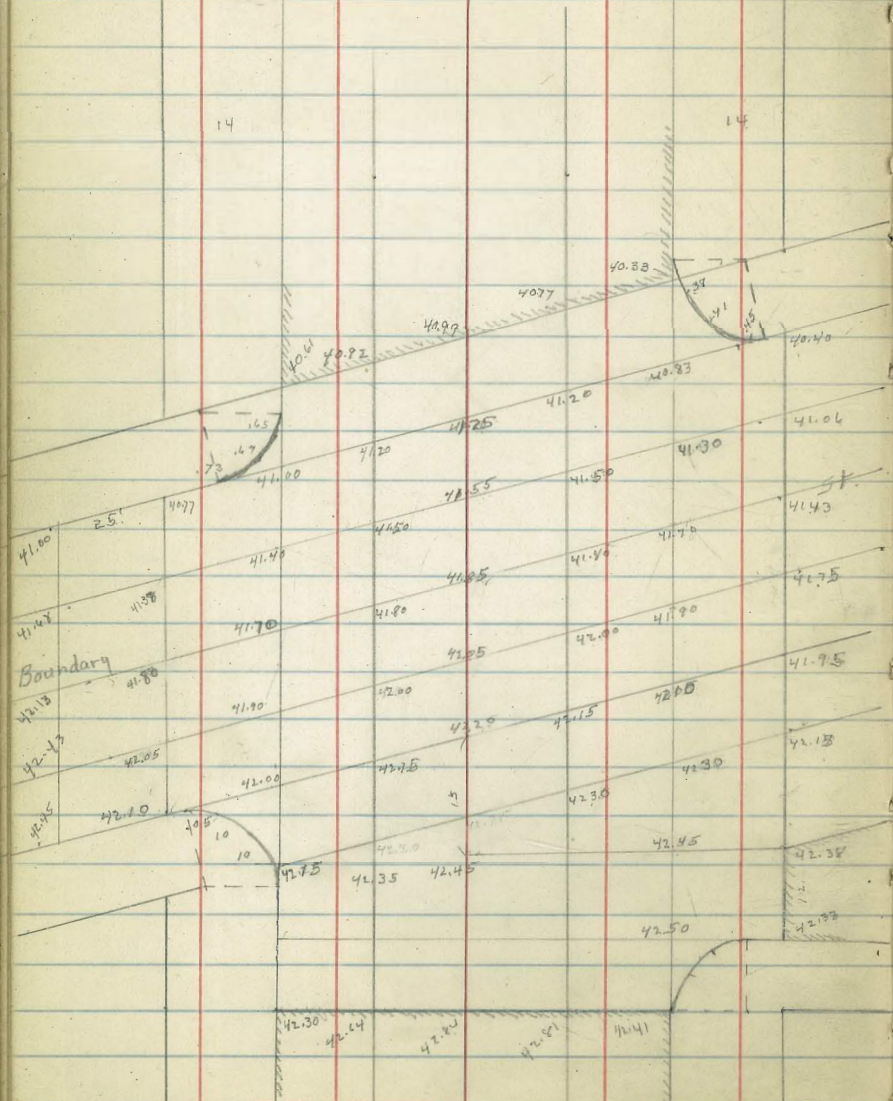
5-1-37. M.H. 2 + 3 covered with dirt.
Will locate later.

B.M. 18.04
4.86
22.90
13.2
9-7 F.L. Ex. 24" Culvert. Inlet. End

B.M. 11.0
6.0
17.0
13.7
3.3 F.L. Ex. 24" Culvert. Outlet S. End.
EXISTING SEWER MAIN



57



Running Track at
Herbert Hoover High School

10-20-36
Miller
Walker
Bliss

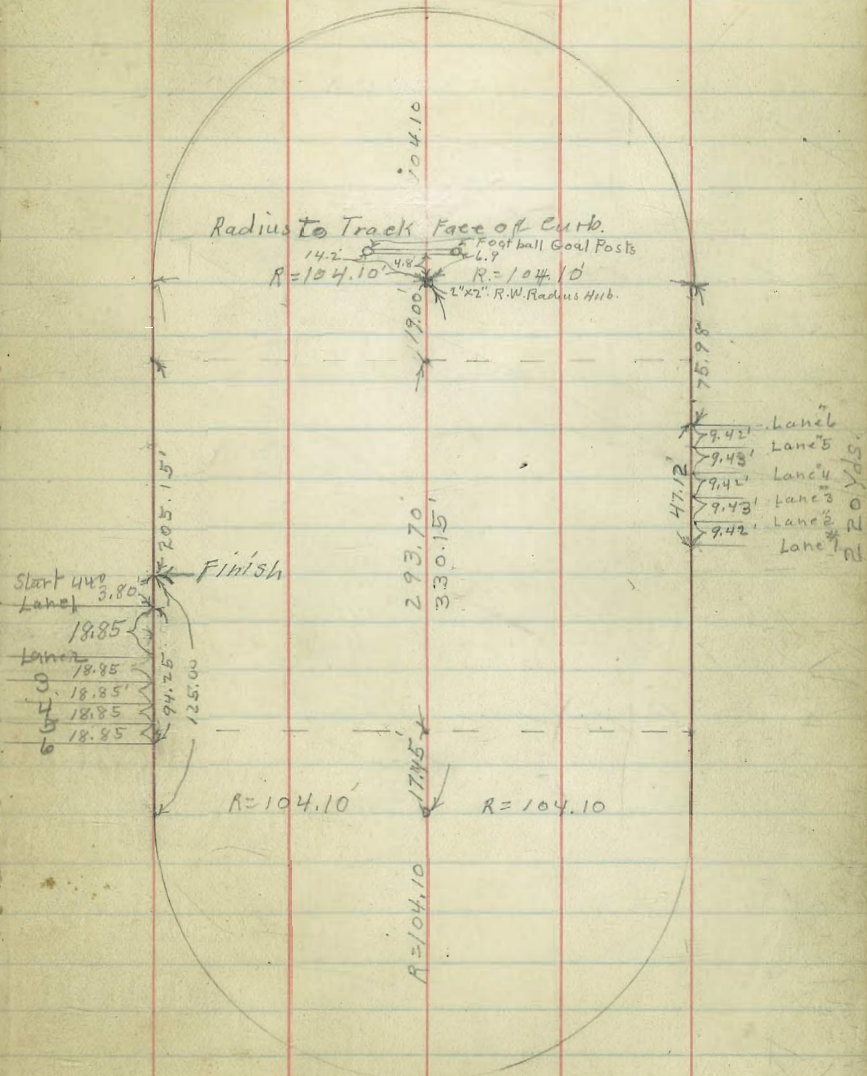
Indexed
C.S.K.

R-104.85	Length Track Face Inside Curb	1319.09'
"	0.9 from Curb	1320.00
# Lane 1	Rad. 105.6'	L. 1. Curve 331.75
"	" 2 " 108.6'	" " " 341.18
"	" 3 " 111.6'	" " " 350.60
"	" 4 " 114.6'	" " " 360.03
"	" 5 " 117.6'	" " " 369.45
"	" 6 " 120.6'	" " " 378.88

Inside Markers for 220 Low Hurdles

Lane #	Lane 2 Start	Lane 3	Lane 4	Lane 5	Lane 6
H1	60'	60'	60'	60'	60'
H2	120'				

123.10-8E	113.68BC	104.26BC	94.83BC	85.40BC	75.97BC
	6.32	15.74	25.17	34.60	44.03
H2	176.39.7	171.54.5	167.24.5	163.08.5	159.04.9
H3	65.90	145.00.4	141.06.3	137.24.7	133.54.6
H4	149.07.8	113.21.1	110.18.1	107.24.9	104.40.6
H5	116.73.4	81.41.8	79.30.1	77.25.1	75.26.7
H6	84.01.1	51.27.7	48.41.7	47.25.3	46.12.4
H7	51.27.7	18.54.5	18.23.2	17.53.5	17.25.5
	16.58.8	16.33.4			
H8	205.152E	E.E	E.C	E.C	E.C
H9	180'	180'	180'	180'	180'
H10	120'	120'	120'	120'	120'
H11	60'	60'	60'	60'	60'



Finish

Richmond St. Grades Indexed
Brookes Ave North. c.s.K.

B.M. BP	3.11	292.24		289.13	S. E. Brookes & Herbert.
T.P. Hydt.	3.52	283.76	12.04	280.20	S. E. Brookes & Richmond.
10' N.M. Line	Brookes Top. el		4.50	279.26	
T.P.	1.22	272.18	12.80	270.96	

2+60			10.68		61.50
2+90			11.08		61.10
3+25 N. = S. End. Curb. Inlet.		10.53		261.65	Top. el
" " " " "		11.50		260.68	gutter

Main St. Fire Hydr. To Lt. of E

Siva St.

Station 37+29.77

29.5 To Lt. of E.

BM Hub. #7	4.95	6.41	1.46	70' Rt. 37+85.77
Top. of 37+32.77 B.C. Ch. Rd.			5.53	
37+29.77 Fire Hydr.	4.58	1.83	5.53	F. 3.70

Thor St.
This BM. to be removed.

BM #6 B.P. Ch.	4.84	12.00	7.16	43' Lt. of Sta. 30+92.97
Ch. Gr Sta 30+62.07			8.00	
" " 30+72.07		4.20	7.80	
Set. BM. B.P. 58 Lt. of Sta 30+92.97		4.89	7.11	

Una St.

Fire Hydr. 1.3 from Face New Curb did not Move

This BM. to be removed.

B.M. #5 B.P.	4.64	18.19	13.55	44' Lt. of Sta. 24+32.60
Set New BM B.P. in Curb		4.65	13.54	55' Lt. of Sta 24+32.60

Vesta St.

This BM. will be removed.

B.M. B.P. #4	3.46	18.66	15.20	42' Lt. Sta. 17+71.56
17+51.56 B.C. Rd.		2.69	15.97	15.47 +0.50
Set New BM. 56 ³ Lt. of 17+71.56		3.76	14.90	B.P.

Indexed

C.S.R.

Woden St

This BM. to be Removed.

BM. B.P. #3	3.69	14.23	10.54	41' Rt. of Sta. 11+51.09
Top. Curb 11+71.09 at F.H.		3.48	10.75	10.25 +0.50
New BM. B.P. #3		3.58	10.65	56.5 Rt. of Sta. 11+51.09

gamma St.

B.M. B.P. Hub.	7.23	11.22	3.99	65' Lt. of Sta. 4+83.94
Top. of 4+30.94		5.65	5.57	8.57 -3.00

64

Cutter Grades 34th St Adams South
for Drainage

indexed
c/s.K.

499

65

BM.BP	4.75	394.00	W. gutter	389.25	S.W. 34 th Adams	394.00	E. gutter	Top	Curb		
0+00 =	S. Line Adams		5.25	388.75	4.66	389.34	0+00 = S. Line Adams	5.04	388.96	4.43	389.57
+25			5.22	388.78	4.73	389.27	+25	4.84	389.16	4.47	389.53
+50			5.18	388.82	4.70	389.30	+50	4.94	389.06	4.57	389.43
+75			5.22	388.78	4.83	389.17	+75	4.98	389.02	4.57	389.43
+100			5.24	388.72	5.00	389.00	+100	5.05	388.95	4.68	389.32
N.L. Alley +25			5.30	388.70	5.07	388.93	+25	5.05	388.95	4.75	389.25
S.L. " +42			5.41	388.59	5.21	388.79					
+50			5.40	388.60	4.76	389.04	+50	5.01	388.99	4.54	389.46
+75			5.43	388.57	5.03	388.97	+75	5.14	388.86	4.74	389.26
+200			5.32	388.68	4.84	389.16	+83	5.21	388.79	nd drive	
+25			5.40	388.60	4.89	389.11	+200	5.18	388.82	4.73	389.27
+50			5.42	388.58	4.95	389.05	+25	5.23	388.77	4.79	389.21
+75			5.53	388.47	5.16	388.84	+50	5.32	388.68	4.95	389.05
+300			5.53	388.47	5.13	388.87	+75	5.36	388.64	4.99	389.01
+20			5.60	388.40	5.20	388.80	+300	5.46	388.54	5.04	388.96
+25			5.63	388.37	5.20	388.80	+25	5.43	388.57	5.03	388.97
+50			5.65	388.35	5.20	388.80	+50	5.52	388.48	5.00	389.00
+75			5.63	388.37	5.21	388.79	T.P.	4.98	394.00	4.98	389.02
+400			5.59	388.41	5.22	388.78	+75	5.54	388.46	5.10	388.90
T.P.	4.98	394.00	4.98	389.02			+400	5.58	388.42	5.10	388.90
							+25	5.60	388.40	5.05	388.95
							+38	5.66	388.34	5.23	388.77
							+50	5.64	388.36	5.21	388.79
+25			5.62	388.38	5.25	388.75	+60	5.71	388.29	5.21	388.79
+50			5.65	388.35	5.20	388.80	+75	5.64	388.36	5.17	388.83
+75			5.67	388.33	5.26	388.74	+93	5.67	388.33	5.21	388.73

393.03

N. ch. Madison con.

W-50'	Top. ch	5.47	387.56
" "	gutter	6.05	86.98
W-25'	" "	5.92	87.11
" "	Top. ch	5.35	87.68
W. Line	" "	5.00	88.03
" "	gutter	5.55	87.48
+12' =	W. ch. Lin -	5.22	87.81
+21 =	" "	4.75	88.28
+30 =	¢	4.55	88.48
+39 =	E. 1/4	4.72	88.31
+48 =	E. ch. line = N+S. Gutter	4.90	88.13
+40 =	E. Line gutter	4.82	88.21
" "	Top. ch	4.34	88.65
E+25'	" "	4.38	88.65
" " "	gutter	4.66	88.37
E+50'	" "	4.54	88.49
E+50'	Top. ch.	4.22	88.81
E+100'	" "	4.34	88.69
" " "	Top. ch.	3.96	89.07
	9' S. of N. ch = N 1/4		
E. ch. Line = N+S. gutter		5.06	87.97
	18' S. of N. ch = ¢ Madison		
E. ch. line = N+S. Gutter		5.22	87.81

393.03

34 1/2 ST

66

E. ch. Line = N+S. Gutter		5.24	
	9' S. of ¢ = S. 1/4		
	18' S. of ¢ = S. ch. line - Madison		
E-100'	Top. ch	4.45	388.58
" "	gutter	4.85	88.18
E-50'	" "	4.71	88.32
" "	gutter	5.08	87.95
E-25'	" "	5.26	87.77
" "	Top. ch	4.85	88.18
E. Line	" "	4.90	88.13
" "	gutter	5.27	87.76
E. ch. Line = N+S. Gutter		5.29	87.74
+9 = E. 1/4		5.10	87.93
+18 = ¢		4.87	88.16
+27 = W. 1/4		5.01	88.02
W. ch. Line		5.34	87.69
W. Line	Top. ch.	5.05	87.98
" "	gutter	5.42	87.61
W+25'	" "	5.74	87.29
" " "	Top. ch	5.28	87.75
ctr. S.W. Return	Top. ch.	4.94	
" " "	gutter	5.31	
ctr. S.E. Return	gutter	5.27	
" " "	Top. ch.	4.99	

393.03
S. Line Madison

W. ch	4.85
W. gutter	5.32
E. "	5.49
E. ch	5.05

0 + 25 South

E. ch	5.18
E. gutter	5.60
W. "	5.39
W. ch	4.92

0 + 50 South

W. ch	4.84
W. gutter	5.32
E. "	5.66
E. ch	5.19

0 + 75 South

E. ch.	5.32
E. gutter	5.74
W. "	5.32
W. ch	4.97

1 + 00 South

W. ch	5.09
W. gutter	5.48
E. "	5.74
E. ch.	5.21

393.03

T.P.	4.19	391.52	570	387.33
B.M.B.P. 5 E	34 th + Monroe	3.11	388.41	= 388.36

67

Pershing Drive Gutter Grades

Indexed
c.s.K.

BM 10000
3.66
69
103.64
14.67
88.97
2.65
71.62

B.M. RP 0100 2.24 102.24 100.00 G 177.52

102.28

Reset

102.66

Stab. 1. E. Edge Pav.
2. of Exp. Pav.

Stab 2. offset. W. of Gutter

Gutter Grade

+ or -

2+50 B.E

0.23

102.05

13.0

✓

101.75
0.53 ✓

0.0

101.75

2.66
-0.77

2+00 S

✓

98.44
3.84 ✓

0.0

98.44
5.22 ✓

1+50 S

✓

95.30
6.98 ✓

0.0

95.30
8.36 ✓

1+00 S

✓

92.24
10.00 ✓

0.0

92.24
11.38 ✓

T.R

0.24

89.58

12.94

89.34

89.58

0+50 S

89.50
0.08 ✓

0.0

89.50
14.16
0.53

0+00 = 3+43 S

2.68

86.90 ✓

11.0

86.60
2.98
3.17 ✓

-0.20

86.60
5.92
5.22
-0.20

3+00 0

12.5

84.12
5.46 ✓

0.0

2+70

13.5

82.38
7.20 ✓

0.0

2+40

8.64

80.94

14.4

80.64
8.94 ✓

0.0

2+10

15.2

78.77
10.81 ✓

0.0

1+80

15.8

76.90
12.68 ✓

0.0

T.R

0.13

76.80

12.91

76.67

76.80

1+50

16.2

75.03
1.77 ✓

0.0

123.82

4786⁶ DL 4-40-24 7.62 116.20 115.80 +0.405420⁴ DL 5-29-36 5.82 118.00 117.80 +0.205454² DL 6-10-44 3.94 119.88 119.70 +0.185487² EC DL 6-52 2.61 121.21 121.60 -0.39T.P. Nail RP
Header Board1.98 121.84 Sta 5487² ECEC. { RP 5 tabs 12" E. of
w. edge gutter.
R.P. Nail in Header 10" W.
w. of w. edge gutter

71

10-6-38

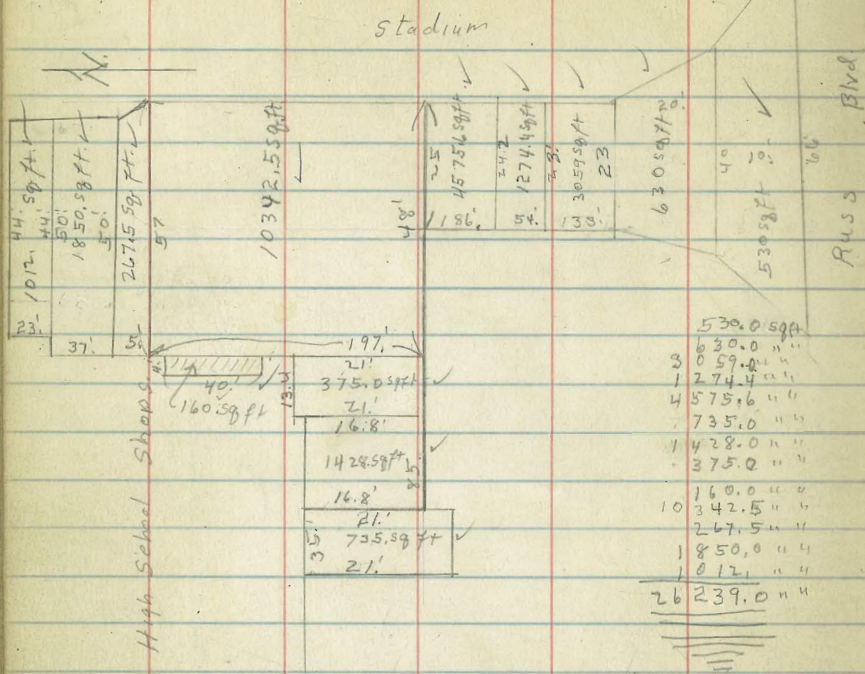
Area of Pav. Road. W. of Stadium
North of Russ. Blvd.

10-7-38

Pav. Area Boundary st. S. of Thorn

indexed
c.s.K

72

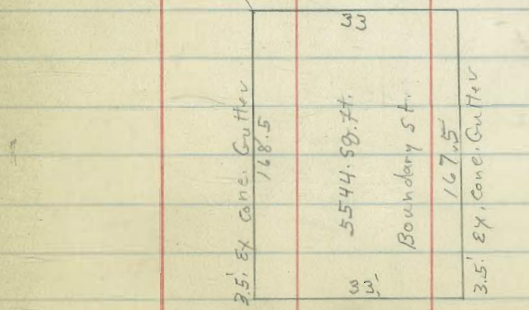
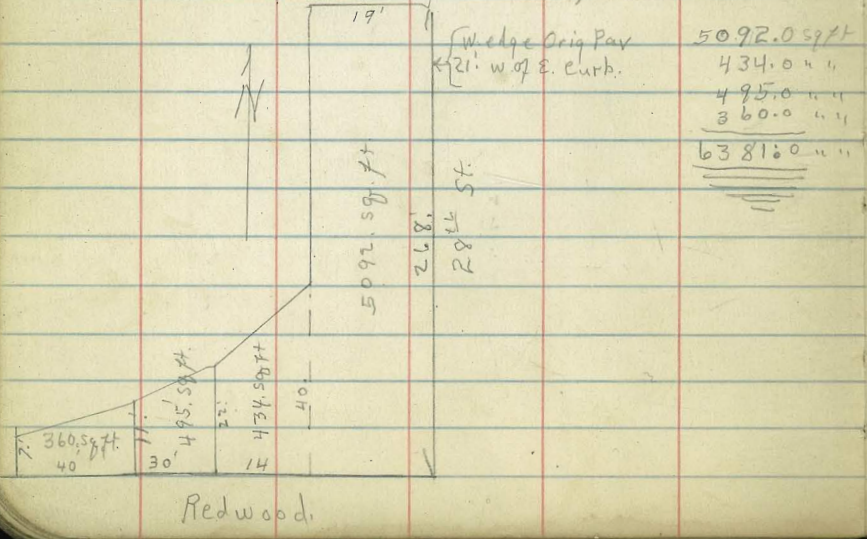


10-7-38

Pav. Area 28th St. N. of Redwood

Redwood St
Little Flower St

Pav. Area Boundary st
S. of Little Flower



5544.50 sq ft

Thorn St

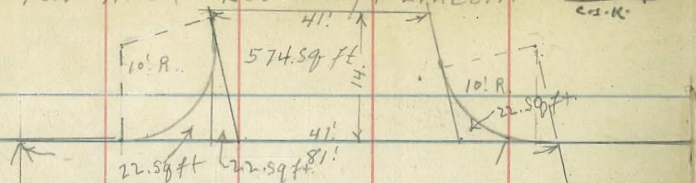
24, 450.0 sq ft
30.0 " "
252.0 " "
384.0 " "
443.0 sq ft
120.0 " "
25679.0 "

10-7-38

Pav. Area. Boundary + Lincoln

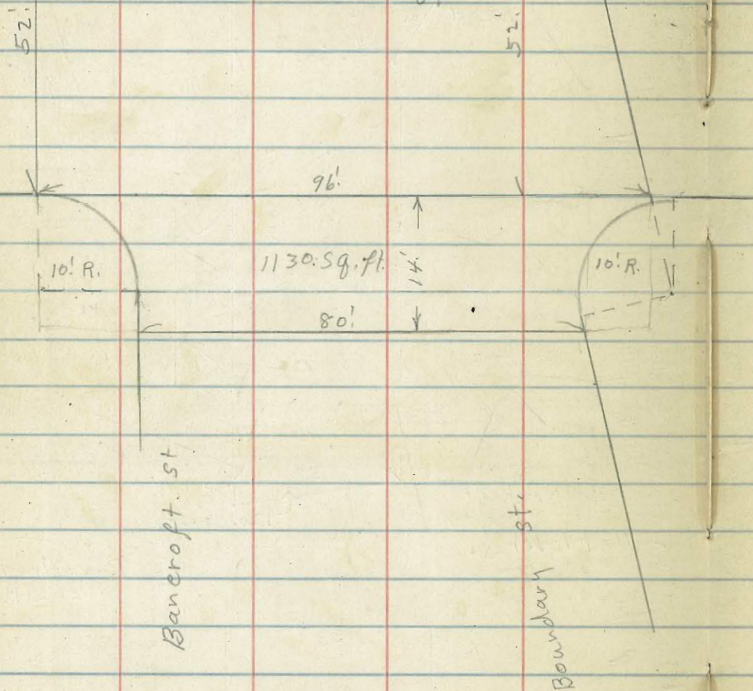
Indexed
as R.

73



Lincoln Ave.

4602.0 sq ft.



4602.0	sq. ft.
574.	" "
66.	" "
1130.	" "
6372.	" "

1-2-38 Curb Grades Diamond Haines Inq.

	d	Gutter	Par.	
-1.1		5.98		
B.C. 0+00	5.02	5.65	33	
1	4.87 ¹⁵	5.50	5.35	5.20
2	5.00 ¹³	5.56	5.48	5.05
3	5.13 ¹³	5.73	5.65	5.15
E.C. 4	5.26	5.90	5.40	5.30
0+00	0.85			

Indexed
O.S.K.

446.6
11.63
3.85
53
352
17
15013.20

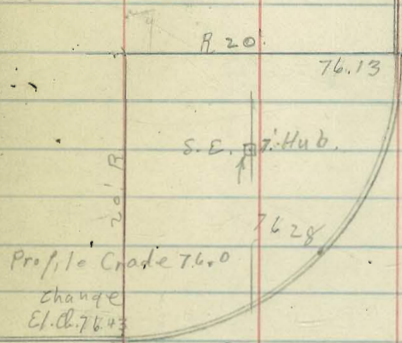
75

Return S.E. Cor Diamond + Haines

1+50	3.85			
1+75	4.35 ⁵⁰	5.02		
2+00	4.70 ³⁵	5.35		
1+25	4.87 ¹⁷	5.54		
+50	5.01 ¹⁴			
+75	5.19 ¹⁸			
3+00	5.34 ¹⁵			
+25	5.50 ¹⁶			
5+87	6.65	7.32		

B.M. School Step
N.W. Ingraham
Emerald 74.11

6.64
84.77
2.54
82.21
1.04
83.30
6.87
76.43
3.52
79.49
9.64
70.30
2.50
72.80
7.62
65.18
2.81
67.99
9.15
58.84
1.01
59.85
10.41
49.44
2.61
52.05
18.00
42.05
3.12
45.22
5.84
39.36



B.M. B.P.W.
Gresham +
Diamond } 71.31
8.27
79.58
S.V. Curb 3.15
76.43
Curb. stat 3.28
76.30
Clt. Ret 76.24
3.30
2.23
+1.07
S. End. Ret 76.13
3.45
2.48
+0.97
Diamond.

Ret. N.W. Cor Inq + Emer

78.11 B.M.				
0.96	N. Lin. - exd	ctr. 20 R	W. Lin.	
79.07		Ret	Ingraham	
	3.27	75.72	76.00	
	75.85	3.15	3.07	
		3.95	4.07	
		-0.80	-1.00	
0+55 W	0+93	1+24	2+05 W	
75.78	75.63	75.50	75.18	
3.29	3.44	3.57	3.89	
4.40	4.53	4.25	5.05	
-1.13	-0.89	-0.68	-1.16	

B.M. B.P.W.
Emerald + Garnett

N.E.T. Hub

5/5/37

Grades for Rogue Court

B.M.	1.50	219.11	217.61
		0+00 = W. Line	0+86 = E. Line
0+85 N = N. End. Court = S. side 8' Path		211.00 8.11 5.26 +2.85	211.00 8.11 4.78 +3.33
0+42 E ⁰ N = Center		211.00 8.11 11.24 -3.13	211.00 8.11 9.28 -1.17
0+90 = S. End. Court N. side 8' Walk		211.00 8.11 10.98 -2.87	211.00 8.11 8.52 -0.41

N.W. Cor.
Top of oxen219.11
4.85
214.26

78

Orange

Ave.

Barnett
St.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 \times to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not to cut or fill and find distance in table. Set up rod at this point and line of sight should cut target. **IMPROVED TABLES AND INFORMATION** necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

17.28 $\frac{43}{28}$ 2947
 31414 178.7
 20 160
 16.5 $\frac{925}{14}$ 2628320 93
 13 785 31.41 492 77
 29.5 10 4.51 76
 10.5 5678 41
 4324 55.5
 1423 0.00 31185 27
 1025 17.02 51.50
 398 17.25 37 + 29.77
 15.5 7.77
 4 2.09 7.13
 54.5 5.00 553
 898 3.04 61.01.60
 2.26 500 522 3.04
 11.24 522 1.70
 3.99 4.80 3.04
 7.25 2.89
 11.24 4.90 6.77
 8.57 1.91 4.38 7.80
 2.65 2.42 51.97 2.7
 7680 6.90 27399.6
 11.04 56 2.64 85
 11.36 40
 65.44 33
 66
 40
 106
 53