

893
550
3.4

1234
105
2.2

12155
290
9.65

358.83
31.72
341.56
363.50
9.65
353.83
290
350.93

191.0
9.33
4.77

341.56
47.9
341.81
24.8

36348
12155
346.33
341.81
8.94

330.93
290
332.23
332.47

353.88
341.81
24.8
332.47

389.33
6.46
332.87
332.47

339.33
4.46
332.87
332.47

341.81
8.94
6.46
2.48
341.81
24.8
338.33

MADE IN U.S.A.

G-177

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book,) which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

MICROFILMED

APR 12 1965

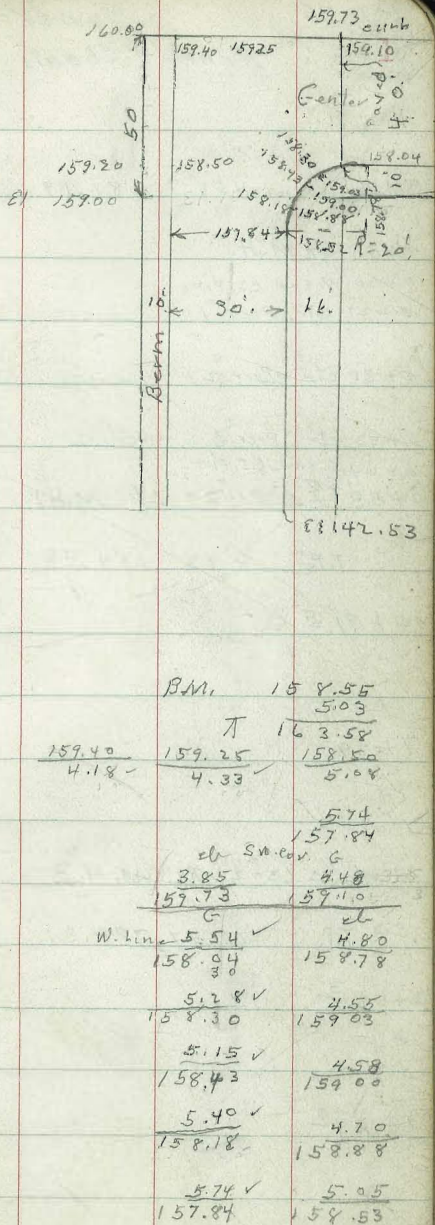
Girard Ave Grade 8-24-36

indexed
C.S.K.

BM. BP 4.77	163.52	158.75	Girard Center
New B.M. The old			
Set BM BP Taken out. New 20' Rad.	4.77	158.55	Girard Center
3+65.4	BC. 20' R Curve	158.57	W. cl
		4.9	
		5.1	
		-0.2	
3+82.7		157.14	
		6.4	
		4.3	
		+0.1	
3+00		155.71	
		7.8	
		8.3	
		-0.5	
2+50		153.51	
		10.0	
		9.6	
		+0.4	
2+00		151.32	
		12.2	
		12.0	
		+0.2	
1+50		149.13	
		3.9	
		3.9	
		0.0	
1+00		146.93	
		6.1	
		6.0	
		+0.1	
0+50		144.73	
		8.3	
		8.0	
		+0.3	
0+00		142.53	
		10.43	
		10.43	

E. Berlm

S.L. Center	160.00	
	2.5	
	1.8	
	+1.7	
N.L. Center	159.00	
	4.5	
	3.8	
	+0.7	
	163.52	
	12.83	
	150.69	
	2.27	157.14
	152.96	6.4
		3.0
		-1.6
		155.71
		7.8
		9.1
		-1.3
		153.51
		10.0
		11.1
		-1.1
		151.32
		12.2
		13.5
		-1.3
		149.13
		3.9
		5.1
		-1.2
		146.93
		6.1
		7.5
		-1.4
		144.73
		8.3
		9.2
		-0.9
		142.53
		10.43
		11.2
		-0.8



142.53

BM.	158.55
	5.09
+	163.58
159.40	159.25
4.18	4.33
	5.09
	5.74
	157.84
	3.85
	4.48
	159.73
	5.71
	157.02
W. line	5.54
	158.54
	5.28
	158.30
	4.55
	159.03
	5.15
	158.43
	4.58
	159.00
	5.40
	158.18
	4.70
	158.88
	5.74
	157.84
	5.05
	158.53

1-7-35
 Mills
 Walker
 Bliss

Sewer Grades
 Arnold & Choate P. L. B. Add.

Indexed
 C.S.K.

BM. & Stab	4.68	181.19		176.51	Station 0+53.88	5' offset. Rt.		Grade	5' offset. Lt.
0+00 Ex M.H.					172.00				
0+20 N. end. C.T. Pipe									
0+21 ctr. Pier #1	8.48		172.71	172.21	+0.50 ✓	10.02	171.17	172.21	-1.04 ✓
0+31 ctr. Pier #2	9.92		171.27	172.31	-1.04 ✓	11.06	170.11	172.21	-2.20 ✓
0+43 ctr. Pier #3	8.03		173.16	172.43	+0.73 ✓	9.22	171.97	172.43	-0.46 ✓
0+44 S. end. C.T. Pipe									
0+53.88 Δ 71-25 Lt. M.H. #	4.25		174.94	172.54	+4.40 ✓				
37.6 T.P.	4.93	184.48	1.64	179.55					
0+91.5			2.94	181.54	172.91	+8.63 ✓			
37.6									
1+29.1			1.50	182.98	173.29	+9.69 ✓			
37.6									
1+66.2 Δ 63-24 Rt. M.H. #2	4.58		179.90	173.47	+6.23 ✓				
35.4 T.P.	11.57	188.31	7.74	176.74	{ 1+66.2 # Hub.				
2+02.3			2.81	185.50	174.02	+11.48 ✓			
35.6									
2+38.0			2.23	186.08	174.38	+11.70 ✓			
35.6									
2+73.6 Δ 2-35 Rt. No M.H.	1.45		186.86	174.74	+12.12 ✓				

188.31

3

3+15⁶ 5.68 182.63 175.16 +7.47 ✓

42.
4
3+57⁶ 5.03 183.28 175.58 +7.70 ✓

42.
4
3+99⁶ 4.68 183.63 176.00 +7.63 ✓

42.
4
T.P. 9.59 189.06 8.84 179.47 4+41⁶³ 4.74 ✓

4+41⁶³ Δ38°34'30" Rt. M.H.3 7.53 181.53 176.42 +5.11 ✓

48.6
48
4+90³ 5.00 184.06 176.90 +7.16 ✓

48.6
48
5+38² 4.34 184.72 177.39 +7.33 ✓

48.6
48
5+87.5² ∠26°-18' Rt. M.H.4 3.89 185.17 177.88 +7.29 ✓

B.M. & Hub 9.74 205.58 195.84 4+70⁴⁴ 4.74 ✓

6+35 11.68 193.90 184.54 +9.36 ✓

6+70⁴⁴ ∠30°-21' Rt. M.H.5 7.50 198.08 189.52 +8.56 ✓

42.
4
7+13³ 0.27 205.31 198.10 +7.21 ✓

T.P. 12.54 217.85 0.27 205.31

217.85

7+56¹ 4.74 213.11 206.66 +6.45 ✓

112.9

T.P. 11.49 228.89 0.45 217.40

7+98⁷⁷ L 90°-00' M.H. 6 7.27 221.62 215.21 +6.41 ✓

8+19 Brk. 3.40 223.49 220.21 +5.28 ✓

T.P. 11.93 240.52 0.30 228.59

T.P. 12.80 252.98 0.34 240.18

8+58⁹⁷ L 25⁰28¹ No M.H. 13.22 239.76 236.21 +3.55 ✓

∅.Stub 8+58⁹⁷ 14.07 238.91 = 238.91

9+05⁵ DE. 1.95 251.03 246.00 +5.03 ✓

Line to S. of M.H. 6

∅ 100 = M.H. 6 221.62 215.21 +6.41 ✓

240.52

0+28⁸⁸ 8.70 231.82 229.65 +2.17 ✓

T.P. 12.80 252.98 0.34 240.18

0+57⁷⁵ 5.53 247.43 244.09 +3.34 ✓

2-27-35
Walker
Bliss.

SEWER GRADES
In Block 18 University Hts.
Bet. Arizona & Texas
" Madison And Adams Aves.

Indexed
C.S.K.

5

Station		El. stakes	El. Grade	cuts	offsets.
0+00 = E. Exist. Sewer	Madison		345.23		
			362.35		
2+14 = end exist. sewer		15.29	347.06	347.05	
+67		8.32	354.03	347.50	+ 6.53 2.0' RT.
3+20 = MH #1		6.87	355.48	347.95	+ 7.53 3.4' RT.
		7.06			
3+66		5.78	356.57	348.67	+ 7.90 4.4' RT.
4+12		3.67	358.68	349.39	+ 9.29 4.4' RT.
+58		2.49	359.86	350.11	+ 9.75 4.4' RT.
5+04		2.58	359.77	350.83	+ 8.94 1.8' RT.
+50	T.P.	368.74	6.95	361.79	351.55 + 10.24 4.4' RT.
+96			5.53	363.21	352.27 + 10.94 4.4' RT.
6+42 = MH #2	2' North St. Adams	10.75	357.99	353.00	+ 4.99 4' RT.
+81		10.86	357.88	353.50	+ 4.38 4' RT.
7+20 = D.E. N. Adams		10.60	358.14	354.00	+ 4.14 4' RT.

S.F.B.P. Madison + Texas = 346.03
 12.96 +
 358.99 x
 6.19 -
 352.80 TP
 9.55 +
 362.35 x
 2.18 -
 360.17 = TP
 8.57 +
 368.74 x

4-26-35
L.T.

Catch Basin Grades Par 1 Blvd.
Russ Blvd. North

Indexed
C.B.K.

Cut stakes 22' from ϕ
on edge of Berm.

W. edge C.B. +22	Par edge +15	+8	ϕ	+8	edge Par +15	R.T. +22 W. edge C.B. 6.72 LOW.
5.05	4.72	4.50	4.41	5.86	5.97	6.14

4'S. of ϕ C.B.	4' N. of ϕ C.B.
5.05	5.05
4.05	4.05
+1.00	+1.00

E. edge C.B. +22	Stk. 19+03 +15.5	+8.5	ϕ	+7.5	+14.5	E. C.B. +22
4.80	4.48	4.20	4.12	5.28	5.47	5.54

4'S. of ϕ C.B.	4' N. of ϕ C.B.
4.80	4.80
4.30	3.80
+0.50	+1.00

ϕ	+8.3	+15.3	C.B. +22
5.14	5.21	5.54	5.85

4'S. of ϕ C.B.	4' N. of ϕ C.B.
5.85	5.85
4.85	4.85
+1.00	+1.00

W. edge C.B. +22	+15.	+8.	ϕ
4.22	3.92	3.72	3.58

4'S. of ϕ C.B.	4' N. of ϕ C.B.
4.22	4.22
3.22	3.22
+0.50	+1.00

Station at an E.C.

ϕ	+7.8	+14.8	+22
2.72	2.79	2.95	3.25

4'S. of ϕ	4' N. of ϕ
3.25	3.25
2.25	2.25
+1.00	+1.00

E. Edge
C.B
+22

Edge
Pav
+15

24 + 17 $\frac{6}{6}$
+ 8 $\frac{6}{6}$

5.50 5.20 5.13 5.05

+22 +15.5 +8.5 $\frac{6}{6}$ +7.5 +14.5 +22
4.90 4.63 4.51 4.42 4.53 4.70 5.00

W. of Naval Hospital Entrance.

E of C.B.
+22.7
+8 +15
5.09 5.19 5.46 6.17
Low.

Excavation
+23.5 +15 +8 $\frac{6}{6}$
W. of Naval Hospital Entrance

4.85 4.54 4.41 4.36

4.85 4.85
3.85 3.35
+1.00 +1.50

4.5 of $\frac{6}{6}$ 4.1 N. of $\frac{6}{6}$
5.50 5.50
4.50 4.50
+1.00 +1.00

4.90 4.90 $\frac{6}{6}$ Pav 4.5 of $\frac{6}{6}$ 4.1 N. of $\frac{6}{6}$
4.40 4.40
+0.50 +0.50 5.00 5.00
4.00 4.00
+1.00

4-27-35 Grades Alley BIK. 54 City Hts

indexed
c.s.k.

8. Edg
C. B
+22
BM. B.P. 2.83 345.92 343.09
N. W. Cor
Wightman
+ 40.22
4.41 341.51

5.5
W. line
Wightman
0+00
341.20
4.72
4.72
0.0

12' E. of ϕ
341.20
4.72
2.20
+ 2.02

+22
0+20 Brk.
342.35
3.57
3.57
0.0

342.35
3.57
0.77
+ 2.80

4.90 T.P. 2.86 348.01 0.77 345.15

0+40 Brk
343.19
4.82
4.82
0.0

343.19
4.82
2.55
+ 2.27

0+60 Brk
343.73
4.28
4.28
0.0

343.73
4.28
2.44
+ 1.84

Excav
+23
4.8 0+80 Brk
343.97
4.04
4.04
0.0

343.97
4.04
2.73
+ 1.31

1+00
2+80 Brk.
344.05
3.96
0.0
344.80

344.05
3.96
2.51
+ 1.45

5-4-35

Grades North side Florida Court
E. of Georgia St.Indexed
C.S.K.

9

BM. BP.	H. L.	288.64	284.00	N.W. Cypress + Georgia	Prop. Grade + or -
				Ex. Curb. Grade	Prop. Grade + or -
0+00 = E. Line Georgia St.		2.20	286.44		
0+00 " " " "		2.07		Cor. Cmt. Ret.	
0+05 E. B. Stub		2.8	285.8		286.1 - 0.3
0+60 E.		17.1	271.5		273.4 - 1.9
1+00 E. B.					264.4

5-4-35

Proposed Location Light Standards

Per shing Drive

indexed
C.S.M.

15+62 L.S. #9 9' N. of Pav.

220'
13+42 culvert

13+37 L.S. #8 9' N. of Pav.

15'
215'

11+22 L.S. #7 9' N. of Pav.

220'
220'

9+02 L.S. #6 9' N. of Pav.

220'
220'

6+82 L.S. #5 9' N. of Pav.

E.C.

160'

5+22 L.S. #4 6' N. of Pav Toe Bank ctr. Curve

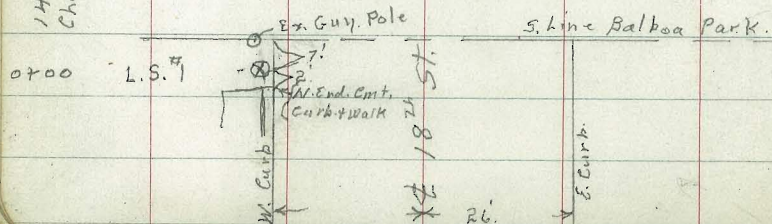
160'
chd. dist.

3+62 L.S. #3 9' N. of Pav B.C. Lt.

220'
chd. dist.

1+42 L.S. #2 9' N. of Pav 11' E. of 2. line 18th St

142'
Chd. dist.



31+63 L.S. #17 9' E. of Pav

220'
220'

29+43 L.S. #16 9' E. of Pav.

220'
220'

27+23 L.S. #15 9' E. of Pav. oh. Curve.

220'
220'

25+03 L.S. #14 9' E. of Pav B.C. Rt.

220'

23+74 = Culvert

22+83 L.S. #13 9' E. of Pav. E.C. Lt.

148'

21+35 L.S. #12 9' N. of Pav. E. of P.H.C. Rd.

213'
213'

19+22 L.S. #11 13' N. of Pav. W. of P.H.C. Rd

160'

18+15 E. End. Bridge 5' N. of Pav.

17+70 = W. End. Bridge 2.5' N. of Pav.

17+62 L.S. #10 9' N. of Pav.

200'

15+62

5D+83 #
L.S. 26 2' E. of Cl.
10' E. of Pav B.C. Lt.

R10
2' E. of Curb.
48+73 #
L.S. 25 10' E. of Pav

R10
2' E. of emb. d.
46+63 #
L.S. 24 10' E. of Pav

R200
45+86 = s. End. emb. d. 8' E. of E. Edge Pav.

R200
44+63 #
L.S. 23 7' E. of Pav. Foot of Bank.

R200
43+40 B.C. Rt.

R200
42+63 #
L.S. 22 9' E. of Pav.

R200
40+43 #
L.S. 21 9' E. of Pav

R200
38+23 #
L.S. 20 9' E. of Pav.

R200
36+23 #
L.S. 19 9' E. of Pav. ✓

R200
34+40 E.C.
33+91 Culvert

R200
33+83 #
L.S. 18 9' E. of Pav. on Curve

R200
31+63

69+95 #
L.S. 35 2' E. of cl.
10' E. of Pav B.C. Rt.

R200
67+75 #
L.S. 34 2' E. of cl.
10' E. of Pav E.C.

R200
65+55 #
L.S. 33 2' E. of cl.
10' E. of Pav

R200
63+90 Drive to Tool House

R200
63+35 #
L.S. 32 2' E. of cl.
10' E. of Pav.

R250
61+10 #
L.S. 31 2' E. of cl.
10' E. of Pav

R300
6+60 B.C. Lt

R300
58+80 #
L.S. 30 { 2' E. of cl. { E. End. of
10' E. of Pav (Laurel St. Extension)

R197
56+83 #
L.S. 29 2' E. of cl.
10' E. of Pav. E.C.

R200
54+83 #
L.S. 28 2' E. of cl.
10' E. of Pav

R200
52+83 #
L.S. 27 2' E. of cl.
10' E. of Pav

R200
50+83

88+6B Culvert

88+50 L.S. #44

10' E. of Pav. { opposite Road to
Municipal Pool

220

86+30 L.S. #43

10' E. of Pav. W. End Branches
of Pepper Tree

170

84+60 L.S. #42

9' E. of Pav. V Island North
of Redwood.

160

83+00 L.S. #41

2' E. of cb. S. side Redwood St.

205

80+95 L.S. #40

2' E. of cb.
10' E. of Pav.

98+73 Ex. Elec Pole { 2' S. of S. cb. of Upas St.
1' E. of E. line 28th St.

200

78+95 L.S. #39

2' E. of cb. } at Road to
10' E. of Pav. } Municipal Pool.

143

97+30 L.S. #48

2' S. E. of cb.
10' S. E. of Pav

230

76+65 L.S. #38

{ 2' E. of cb.
10' E. of Pav.

220

95+10 L.S. #47

2' E. of cb.
10' E. of Pav

230

74+35 L.S. #37

2' E. of cb.
10' E. of Pav E.C.

220

92+90 L.S. #46

10' E. of Pav opp. Intersection
Pershing Ave

220

72+15 L.S. #36

2' E. of cb.
10' E. of Pav

220

90+70 L.S. #45

10' E. of Pav.

220

69+95 L.S. #35

220

88+50

7-9-35 Sewer Grades. P.L. 174.
F.B. 1519 - P. 35.

Indexed
C.S.K.

13.

M.H. BM	12.19	131.27	119.08	Rim. M.H.					
0+00 = Ex. M.H.			12.19	119.08	114.83	+ 4.25	from. Pipe		
0+25			8.29	122.98	115.08	+ 7.90	5' off set. to Rt.		
0+50.			6.06	125.21	115.33	+ 9.88	" "		
0+88 ²⁰	M.H. Δ. 58°-23 Rt.		9.26	122.01	115.71	+ 6.30	" "	" " split. of L	
1+00			8.24	123.03	115.83	+ 7.20	" "	" "	
1+50			6.71	124.56	116.33	+ 8.23	" "	" "	
2+00			8.95	122.32	116.83	+ 5.49	" "	" "	
2+50			9.20	122.07	117.33	+ 4.74	" "	" "	
2+75			4.41	126.86	117.58	+ 9.28	" "	" "	
T.P.	9.51	137.23	3.55	127.72					
3+00			7.50	129.73	117.83	+ 11.90	" "	" "	
3+25			4.57	132.66	118.08	+ 14.58	" "	" "	
3+50			4.66	132.57	118.33	+ 14.24	" "	" "	
3+75			5.82	131.41	118.58	+ 12.83	" "	" "	
4+00			7.67	129.56	118.83	+ 10.73	" "	" "	
4+23 ¹⁰	M.H. L 62°-50 Rt.		11.55	125.68	119.06	+ 6.62	" "	" " split	14.0 123.2
4+50			7.36	129.87	119.33	+ 10.54	" "	" "	9.2 128.0
4+75			3.91	133.32	119.58	+ 13.74	" "	" "	6.0 131.2
5+00	D.E. bottom gully.		11.12	126.11	119.83	+ 6.28	" "	" "	14.2 123.0

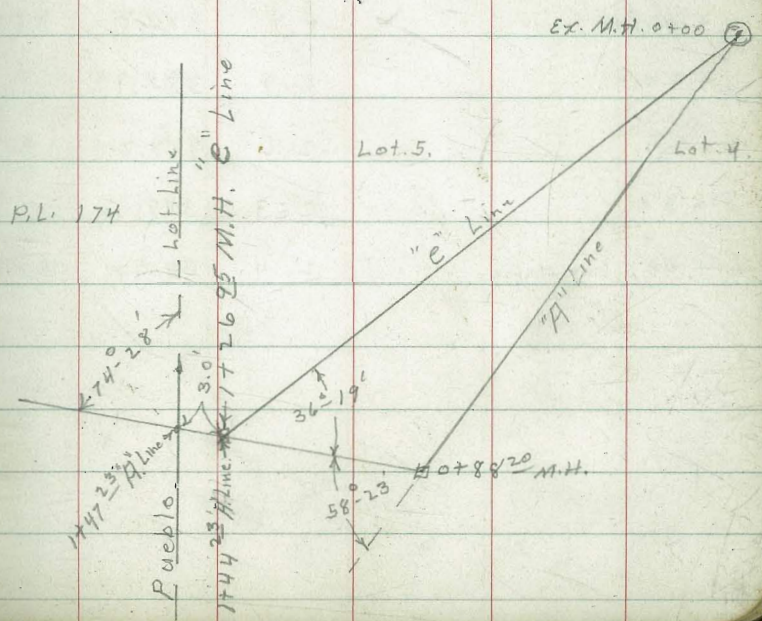
Profile from 4+23¹⁰
to D.E. 5+
H.I. 137.23

7-17-35
Miller
Walker
Bliss

Sewer in P.L. 174
change - "C" Line
see F.B. 1519 - P. 35

B.M.	16.17	135.25	119.08	M.H. Rim Sta 0+00 F.L. Grade		Profile	Elev.	
0+00 = Ex M.H.			16.17	119.08	114.83	+ 4.25 from Rim	135.25	118.8
0+03							18.2	117.0 Wash.
0+25		8.10	127.15	115.11	+ 12.04	Stub 5' offset to RT	10.4	124.8
0+50		3.76	131.49	115.40	+ 16.09	" " " "	5.5	129.7
0+75		4.94	136.31	115.69	+ 14.62	" " " "	6.0	129.2
1+00		7.72	127.53	115.97	+ 11.56	" " " "	9.0	126.2
1+25								
1+26.95 (M.H. = Sta 1+44.23 "C" Line) R. Line		11.05	124.20	116.27	+ 7.93	" " " "	12.30	122.95 stub.

14



7-27-35
Miller
Walker
Bliss

Water Grades Alley Brk. 60
Univ. Hts. Monroe to Madison
bet. Ohio & Illinois. 10" Main

Indexed
C.S.K.

15

BM.	6.98	391.82	384.84	Alley Grade	Grade Ballon Pins	± Alley = 5' offset to W. cuts.
0+00 = N. Line Monroe		5.7	386.1	385.8	382.20	+ 3.9
0+50		5.2	386.6		382.40	+ 4.2
1+00		5.4	386.4		382.60	+ 3.8
1+50		4.7	387.1		382.90	+ 4.2
2+00 Brk.		4.8	387.0	386.7	383.10	+ 3.9
2+50		4.3	387.5		383.30	+ 4.2
3+00		4.4	387.4		383.50	+ 3.9
3+50		4.1	387.7		383.70	+ 4.0
4+00		3.8	388.0		383.90	+ 4.1
4+40 Brk		3.4	388.4	387.7	384.10	+ 4.3
4+80		2.9	388.9		384.50	+ 4.5
5+20		2.6	389.2		384.90	+ 4.3
5+60		2.3	389.5		385.30	+ 4.2
6+00 S. Line Monroe		2.4	389.4	389.2	385.60	+ 3.8

8-17-35
Miller
Walker
Bliss.

Sewer Grades Talbot St

indexed
C.S.R.

Top of 6" Pipe at Δ
Sta 6+49 Xcul
Location M.H.

7.19
65.56
0.56
65.00
70.36 BM 16
2.39
72.75

← Grade Change

Grade of pipe at Δ

BM. & M.H. Connection 6+41 ⁰⁰	12.89	82.37	69.48	at Sta 6+41.00	65.50	+4.86	6+41	65.00	11.6 S. of Prop. Line.
6+00		12.01	70.36	67.43	+4.52	6+00	71.95	67.38	4.57
5+50		7.42	74.95	69.78	+5.17	5+50	74.95	69.75	+5.20
5+00		5.40	76.97	72.13	+4.84	5+00	No. change	72.13	+4.84
4+50 T.P.	12.21	93.85	0.73	81.64	74.48	+7.16			
4+00		12.93	80.92	76.83	+4.09				
3+50		10.05	83.80	79.18	+4.62				
3+00		Not in		81.53					
2+88 ³⁰ T.P.	M.H. L 8-25 Rt. 12.23	105.44	7.87	85.98	82.08	+3.90	4 stub	7.95	85.90 = 85.88
2+50			0.64	93.21	83.87	+8.49			
2+00			13.08	92.36	86.22	+9.08			
1+50			10.14	95.30	88.57	+5.90			
0+90			10.97	94.47	91.39	+10.48			
0+50 T.P.	7.25	111.98	3.57	101.87	93.27	+11.46			
0+14	D.M.H.		0.71	104.73	94.97	+11.37			
0+14			5.44	106.34	99.06	+7.28			
0+00 Connection			5.64	107.31	100.00	+7.31			
chk			5.22	106.76 = 104.70					

8-19-35
Miller
Walker
Bliss

Sprinkler Head Grades.
Municipal Golf Course

No. 1 Battery at Green.

Grade Rod	0.16	0.16	0.16	0.16	0.16
Rod	1.43		2.88	9.79	13.28
	F1.27		-2.72	-9.63	-13.12

No. 2 Battery

G. R.	0.50	0.50	0.50	0.50
R.	3.94	10.50	7.44	17.10
	F3.46	-10.00	-7.16	-13.60

No. 3 Battery

G. R.	0.12	0.12	0.12	0.12
R.	5.42	8.89	12.06	15.12
	-5.30	-8.77	-11.94	-15.00

No. 4 Battery

G. R.	0.51	0.51	0.51	0.51
R.	3.33	6.99	12.98	9.70
	-2.82	-6.48	-12.47	-9.19

No. 5 Battery

G. R.	0.92	0.92	0.92	0.92
R.	4.35	12.03	8.03	15.60
	-3.43	-11.11	-7.11	-14.68

No. 6 Battery

G. R.	0.80	0.80
R.	11.24	14.64
	-10.44	-13.84

No. 7 Battery

G. R.	1.23	1.23	1.23
R.	5.53	10.93	8.53
	-4.30	-9.70	-7.30

Indexed
C.S.K.

16.7
6.5

17

Laurel St Grades Kettner to Atlantic

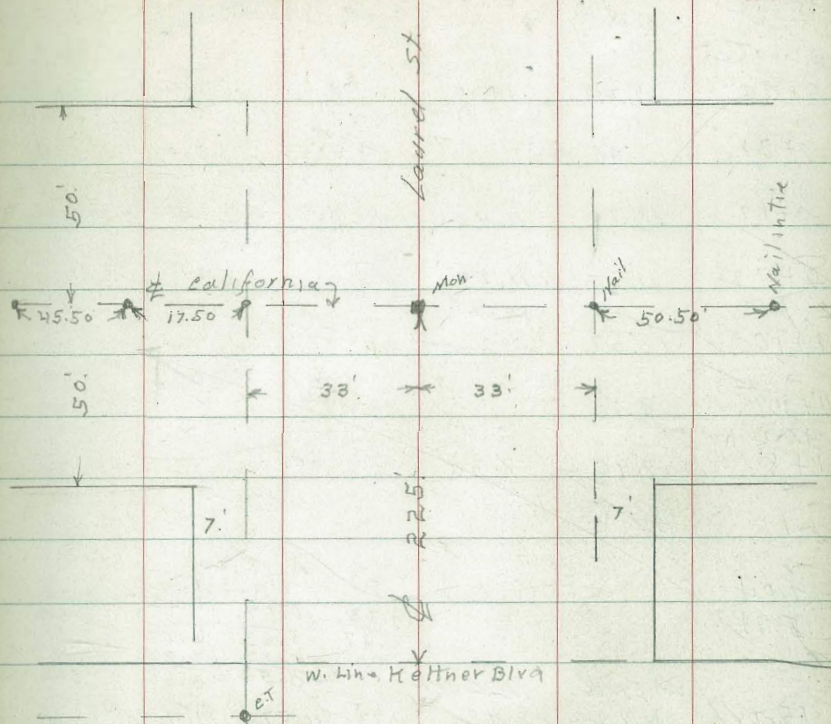
Grades.

W. Line Kettner	S. Edge & Pav.	S. Gutter	S. el.
0+00	31.25	31.04	31.62
0+20	30.12	29.90	30.50
0+40	28.56	28.45	29.05
0+60	26.70	26.54	27.16
0+80	24.51	24.40	25.00
1+00	22.41	22.32	22.92
1+20	20.65	20.59	21.19
1+40	19.37	19.38	19.98
1+60	18.53	18.41	19.01
1+75	17.92	17.73	18.33
cut. el.		16.55	17.15

BM 15.78	17.15	18.33	19.01	19.98	21.19	22.92	25.00
2.43	1.06	10.40	9.72	8.75	7.54	5.81	3.73
X 18.21	1.89	11.50	10.21	9.19	7.62	6.02	4.19
1.89	-0.83	-1.10	-0.49	-0.44	-0.08	-0.21	-0.46
16.32	27.16	29.05	30.50	31.62			
12.41	1.57	5.61	4.16	3.04			
X 28.73	2.07	5.99	3.93	3.03			
1.10	-0.50	-0.38	+0.23				
27.63							
7.03							
X 34.66							

Indexed
C.S.K.

18



Gutter Grades

15.78	16.55	17.73	18.41	19.38	20.59	22.32	24.40
12.16	11.39	10.21	9.53	8.56	7.35	5.62	3.54
27.94							
1.01							
26.93							
7.60	26.56	28.45	29.90	31.04			
34.53	1.38	6.08	4.63	3.49			

W. Line Cal	N. d.	
0+00	15.20	14.60
	11.75	
0+31	13.45	
	7.5	
0+62	11.70	11.40
0+72	11.40	11.20
38.67		10.85
1+10 67	10.57	
1+49 33	9.73	
P.C. 20' Rad		
1+88 P.C.	8.90	8.30

W. Line Cal	S. Gutter	S. d.
0+00	14.40	15.00
0+30		13.50
0+60	11.40	12.00
1+06	9.90	10.50
1+17	9.80	10.00
1+30 ⁺²²	9.00	
1+52.5		9.02
P.C. 20' Rad.		
1+88	7.40	8.05
2+00	7.20	
2+08		

A 18.20
Respt. 14.40

9.73	10.57	11.40	11.70
8.47	7.63	6.80	6.50
chk	8.13	7.38	7.10
	-0.50	-0.58	-0.60
		chk	

End Ex. ch.	N. Curp					
15.78	R 11.22	8.90	9.73	10.57	11.40	11.70
4.20	B 8.78	11.08	10.25	9.41	8.58	8.28
29.98 = A						8.84
						-0.60

S. ch.	S. ch.						
1998 = T	8.05	9.02	10.00	10.50	12.00	13.50	15.00
15.78	11.93	10.96	9.98	9.48	7.98	6.48	4.98
2.42			10.38	10.44			6.04
514.20			-0.40	-1.00			-1.10

continued Page 22.

15' E. of W. Line
Cal. Cornic
N. ch. Line Ply

Water Grades				
0+50	0+85	1+35	1+65	
10.2	8.5	7.3	6.5	
12.6	9.7	10.9	11.7	
5.6	6.1	7.4	8.2	
3.0	+1.9	+2.3	+2.5	
+2.6				

101 S. of E. +
12.5
5.7
4.0
+1.7
s. ch. line Ply

12.4	
5.8	
3.7	
+2.1	

2+15 = G.V. E. Line Pacific

Grades for 5' Sidewalk N. Side of
Sassafras St. bet. Pacific & Kettner Blvds

8-24-35
Miller
B. Liss

Indexed
C.S.K.

27

W. 0	BM Top Hyd	9.41	21.31	11.90	S. E. Pacific + Sassafras curb Grade	Grade of S. Edge Walk.	
	0+12 = 2' End Curb		11.93	9.38	9.27	7.33	+0.05
	0+46		11.85	9.46	9.61	9.67	-0.27
	0+80 B.		11.30	10.01	9.95	10.01	0.0
	0+90 B			Not set.	10.17		
	1+00 B		10.69	10.62	10.65	10.71	-0.09
	1+10 B			Not set.	11.36		
	1+20 B		9.52	11.79	12.33	12.39	-0.60
	1+30 B			Not set.	13.55		
	1+40 B		7.36	13.95	15.01	15.07	-1.12
	T.P.	12.93	32.96	1.28	20.03		
	1+92 B B.C. 20' Road		12.06	20.90	23.25	23.31	-2.41
	2+00		11.06	21.90	24.45	24.45	-2.55
	2+67		10.03	22.93	25.28	25.28	-2.35
	W. Rail						
	2+50 = A.T.S.F. R.R.		4.93	26.03	25.89		
	2+75 B		5.21	27.75	26.30	26.36	+1.39
	3+05		3.32	29.64	28.00	28.06	+1.58
	3+35 B		2.25	30.71	29.70	29.76	+0.95
	3+55 B		1.31	31.65	31.10	31.16	+0.49

30
17

32.96

Grade of S
Edge Walk

21

3+75 B.P.	13.67	46.38	0.25	32.71	32.80	32.86	-0.15
3+95 B			11.65	34.73	35.00	35.06	-0.33
4+15 B			8.56	37.82	37.60	37.66	+0.16
4+45			4.78	41.60		42.00	-0.40
4+75 = N. line Kettner ex. curb 0.25				46.16 = 46.16		46.35	

0.25
13
12.14
1.03
13.67
0.03
46.35
37.65
2 | 8.70
4.35
42.00
46.35

Laurel St. Grades. Indexed
C.S.K.

	N.G.	±	S.G.	
BM. 15.78 3.61 19.39	E Line Cal. 17.60 1.79 Pav.	18.16 1.23 Pav.	17.73	15.78 3.87 19.65
0+25	16.55 3.10 ✓	16.70 2.95 ✓	16.55	
0+40	16.10 3.55 ✓	16.15 3.50 ✓	15.95 3.70 ✓	
0+45 Track	15.96 3.69 ✓	15.88 3.77 ✓	15.80 3.85 ✓	
0+55	15.93 3.72 ✓	15.86 3.79 ✓	15.76 3.89 ✓	
0+75	15.50 4.15 ✓	15.40 4.28 ✓	15.30 4.35 ✓	
0+88	15.10 4.55 ✓	15.00 4.65 ✓	14.90 4.75 ✓	
W. Line Cal 1+00	14.60 5.05	14.50 5.15 ✓	14.40 5.25 ✓	

	N. Gutter	±	S. Gutter
W. Line Cal	14.60 ✓	0+00 ± 14.30 ✓	0+00 S 14.40
0+25 N	13.22 ✓	0+35 ± 12.80 6.85 ✓	0+30 S 12.90
0+50 N	11.85 ✓	0+70 ± 11.10 8.55 ✓	0+60 S 11.40
0+61 1/2 N	11.40 8.25 ✓	0+81 1/2 ± 10.75 8.90 ✓	1+03 S 10.10
Track		Track	Track
0+74 N	11.00 8.65 ✓	0+94 ± 10.36 9.29 ✓	1+16 S 9.70
0+89 N.B	10.40 9.25 ✓	1+00 ± 10.40	1+30 S 9.00
1+10 67	9.96 9.69 ✓	1+10 ± 10.20	1+59 S 8.20
1+49 33	9.20 10.45 ✓	1+20 ± 9.95 9.70 ✓	
		1+50 ± 9.17 10.48 ✓	
1+84 P.C.	8.30 11.38 ✓	1+80 ± 8.40 11.25 ✓	
	8.10	1+88 ± 8.20 11.45 ✓	1+88 S 7.30
2+00 P.C.	8.10	1+ 2+00 ± 7.90 11.75 ✓	2+90 S 7.05 Ex. Catch Basin
2+08	8.00	2+08 ± 7.80	2+08 S 7.55

10-17-35 Gutter Grades W. side 21st St.
 Miller
 Miller
 Bless
 E. St. to Broadway
 BM. BP. 7.49 121.94 114.45 N.W. Cor.
 21st & E.

Indexed
 C.S.K.

121.94

23

Return at N.W. Cor 21st & E.
 W. End

Gutter Pav 8.31
 " Grade 8.31 113.63
 14

G. Pav

0+20

8.00

G. Grade

7.88

114.06

0+34

Gutter Pav 8.10
 " Grade 8.10 113.84
 str.

G. P.

7.92

G. G.

0+40

Gutter Pav 8.00
 " Grade 8.00 113.94
 14

G.P.

7.96

G.G.

7.81

114.13

0+60

Gutter Pav 8.00
 " Grade 7.97 113.97
 0+00 = N. line E. St.

G. P.

7.90

G.G.

7.74

114.20

0+73

el. 7.50 114.44
 G. Pav. 8.04
 G. Grade 7.94 114.00

G.P.

7.95

G.G.

0+80

G. P.

7.92

G.G.

7.67

114.27

121.94
1+00
ch 7.22
G.P. 7.86
G.G. 7.60 114.34

1+20
G.P. 7.72
G.G. 7.54 ✓ 114.40

1+40
G.P. 7.56
G.G. 7.49 ✓ 114.45

1+46
G.P. 7.47
G.G. 7.47 114.47

1+60
G.P. 7.47
G.G. 7.44 ✓ 114.50

1+80
G.P. 7.47
G.G. 7.39 ✓ 114.55

121.94
2+00
ch 7.25
G.P. 7.52
G.G. 7.34 ✓ 114.60 High Pt.

2+20
G.P. 7.50
G.G. 7.39 ✓ 114.55

2+40
G.P. 7.49
G.G. 7.44 114.50

2+60
G.P. 7.45
G.G. 7.49 ✓ 114.45

2+80
G.P. 7.43
G.G. 7.54 114.40

3+00 - S. Line Rdw.
ch. 7.14
G.P. 7.32
G.G. 7.59 ✓ 114.35

121.94.

Return S.W. Cor. 21st + Bdw
1/4

G.P. 7.25
G.G. 7.62 114.32

center

G.P. 7.26
G.G. 7.65 114.29

1/4

G.P. 7.42
G.G. 7.68 114.24

W. End.

el 7.09

G.P. 7.67

G.G. 7.71 114.23

B.M. B.P. 7.04 114.86 S.W. Cor.
21st + Bdw

Gutter Grades 24st St 25

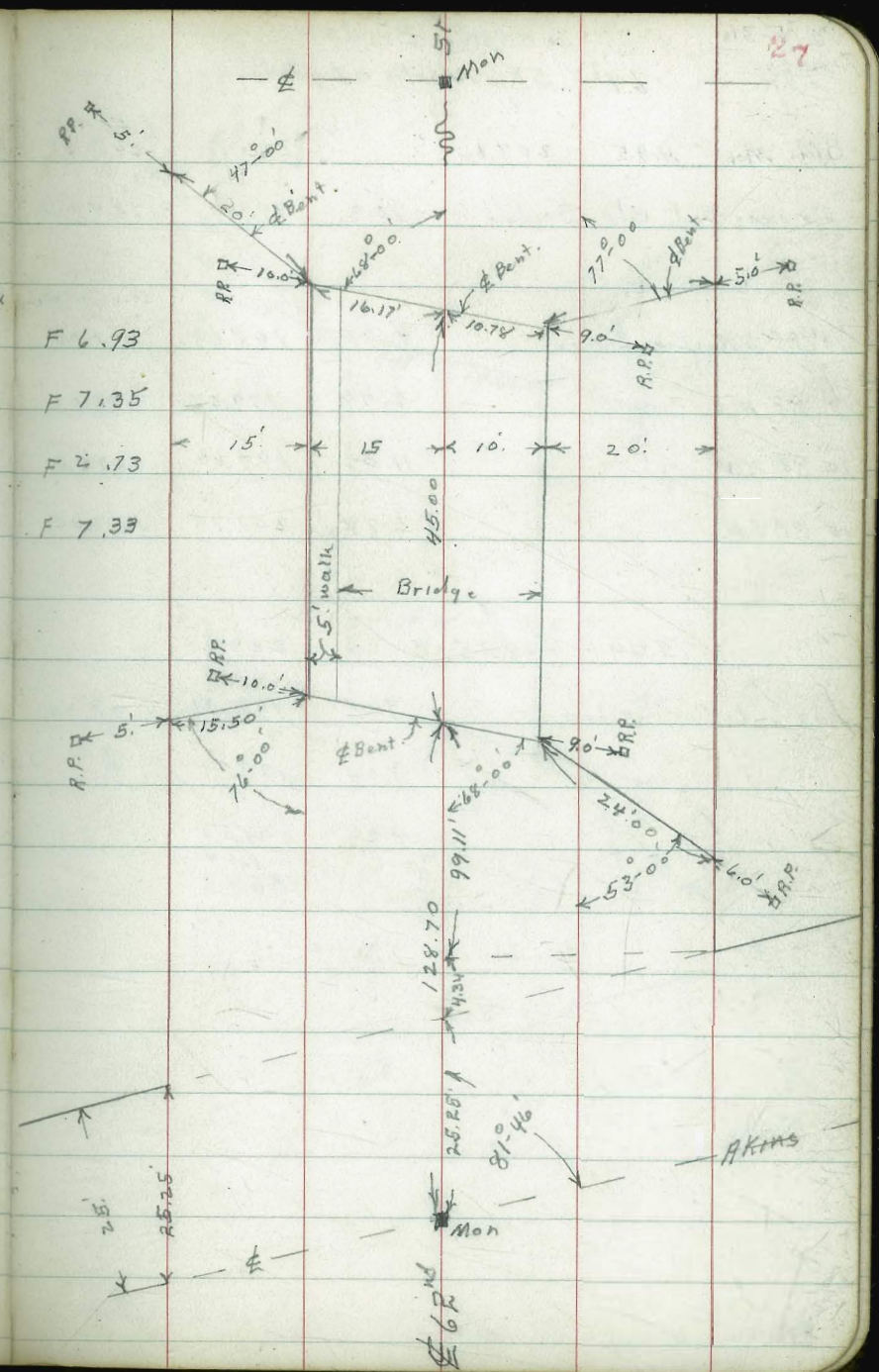
Grades for Fence
Golf Course Balboa Park.
Ground Rod.

Indexed
C.S.K.

26

		Grade Rod		Ground Rod.	Grade Rod
+40		5.1 ✓			
+20	2	6.3 x			
3		4.5 ✓	7	11.2	10.5 11.2 F 0.7
+80		5.8	+80	11.1	10.2 11.05 F 0.85
+60		3.9 ✓	+60		out 9.4 9.6 10.3
+40		5.3	+40	10.3 x	F 0.7 9.3
+20		3.3 ✓	+20		out 9.0 9.7 F 0.7
2		4.6	6	9.8 x	8.7
+80		2.7 ✓	+80		out 8.4 8.9 F 0.5
+60		4.0 x	+60	8.9	8.25 ✓
+40		2.1 ✓	+40	8.9	8.1 out
+20		3.5	+20	8.8	7.8 ✓
1		1.5 ✓	5		7.5 ✓
+80		2.4	+80	8.9 x	7.2 ✓
+60		0.9 ✓	+60		6.9 ✓
+40		1.5	+40	7.5 x	6.6 ✓
+20		0.3 ✓	+20		6.3 ✓
00 = N. End. Fence		0.9	4	7.1	6.0 ✓
			+80		5.7 ✓
	∏ 99.9 Assumed		+60	6.8	5.4 ✓

1-27-36	Encanto Bridge			Indexed	
Miller Walker Bliss	62nd St. N. of AKins St.			c.s.K.	
B.M. Mon	5.06	190.74	185.68	AKins 4	
Ex Stream Bed	ctr Bridge	9.0	181.7	62nd ST.	
				OK Profile	
9' R.P. S.E. Cor.	7.67	183.07	190.00	Grade	
9' R.P. N.E. "	8.09	182.65	190.00	Bridge Deck	
10' R.P. N.W. "	3.47	187.27	190.00		
10' R.P. S.W. "	8.07	182.67	190.00		



2-5-36
Indexed
C.S.K.

Encanto Bridge
64th St. North of AKINS

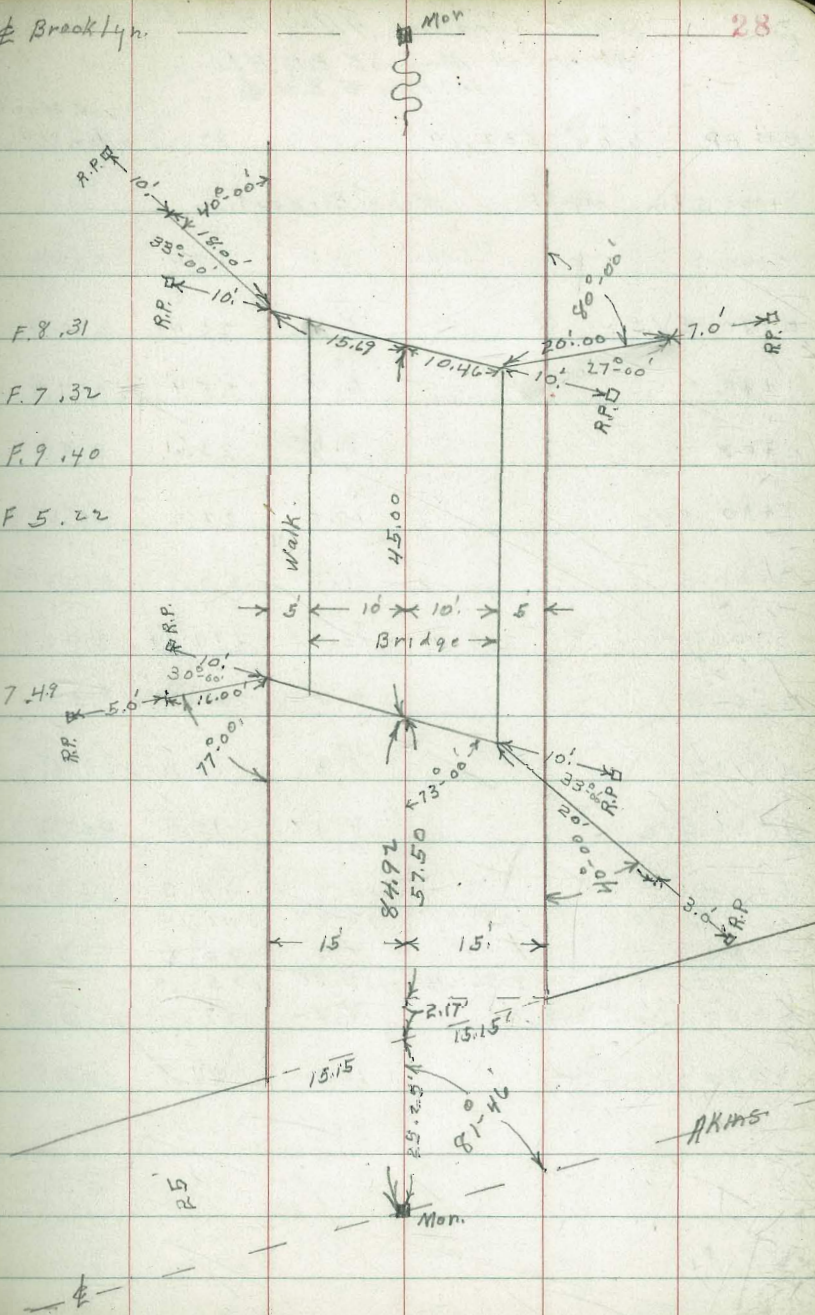
± Brooklyn

Mon

28

B.M. Mon	4.95	208.66	203.71	± AKINS + 64 th St.
Stream Bed, Ctr Bridge	10.3	198.4	= 198.4 Profile	
			Elev floor of Bridge	
10' R.P. S.E. Cor. Bridge	9.97	198.69	207.00	F. 8.31
10' R.P. N.E. " "	8.98	199.68	207.00	F. 7.32
10' R.P. N.W. " "	11.06	197.60	207.00	F. 9.40
10' R.P. S.W. " "	6.88	201.78	207.00	F. 5.22

B.M.	5.04	208.75	203.71
slab S.E. Cor Bridge	9.24	199.51	207.00
	9.24	199.51	
	4.24	204.51	
		1.64	
		206.15	



Water Grades Alley B/K 104. 4-15-36

Indexed
c/s/k.

Amended Map of City Hts.
10" Pipe 5' E. of Φ

BM.B.P. 6.08 332.19

326.11

N.W. Myrtle
+ Van Dyke.

0+00 = S. line - Myrtle Make Connection

0+40 B 4.8 27.4 322.4 +4.6

0+80 E.V.C. 5.8 26.4 322.8 +3.6

1+40 6.8 25.4 321.3 +4.1

2+00 8.6 23.6 319.9 +3.7

2+60 R.V.C. 10.0 22.2 318.5 +3.7

3+00 B 11.3 20.9 317.3 +3.6

3+40 B T.P. 0.68 319.87 13.00 319.19 315.4 +3.8

3+80 B 2.8 17.1 313.0 +4.1

4+20 B 5.3 14.6 309.8 +4.8

4+60 E.V.C. 8.4 11.5 305.8 +5.7

5+00 15.9 04.0 301.5 +2.5

T.P. 0.81 307.91 12.77 307.10

5+50 12.7 95.2 296.0 -0.8

T.P. 1.96 296.76 12.91 295.00

6+00 N. line - Thork. 8.8 88.2 290.5 -2.3

6+50 10'x10" T. 10.0 86.9 289.4 -2.3

Water Grades Thorn St

Indexed
C.S.K.

30

296.96

0+00 = 5' E. of Alley W. of 43rd St 187.

289.4

0+45 ⁴ B		16.2	280.8	285.9	-5.1
0+85 ⁴ B		17.3	279.7	283.8	-4.1
40					
1+25		19.7	277.3	285.3	-8.0
1+45 connection 2"					
1+65 ⁴ B		18.8	278.2	286.8	-8.6
45.5					
2+10 ²		+0.3	297.3	290.2	+7.1
45.5 TP	12.96	309.48	0.44	296.52	
TP	10.54	319.80	0.22	309.26	
2+56 ⁴ B		6.7	313.1	293.6	+19.5
3+14		7.1	312.7	298.5	+14.2
3+76		9.8	310.0	303.4	+6.6
4+36		7.3	312.5	308.3	+4.2
4+96 W. Line Fairmont		3.0	316.8	313.1	+3.7
5+36 T.				314.3	
T.P. B.M. B.P.	1.81	319.83	1.78	318.02	S.E. Thorn + Fairmont.
B.M. Mon			14.38	305.45	W. W. Glenfield + Fairmont + Poplar.
B.M.	2.54	320.56		318.02	S.E. Thorn + Fairmont.
0+00 = E. Line Fairmont		2.5	318.1	314.6	+3.5
0+50		3.3	317.3	312.3	+5.0
1+00		7.6	313.0	309.9	+3.1
1+40 Valve.		10.0	310.6	308.0	+2.6

Water Grades A Key B 1 K. 5
 City Hts Annex "2" Indexed
C.S.K.

BM. BP	5.52	346.41		340.89		
0+202 S.						
Line Dwight	Lowered	to meet pipe	3.9	342.5	337.3	+ 5.2 ✓
0+60 B			4.5	341.9	38.6	+ 3.3 ✓
1+00			4.8	341.6	38.4	+ 3.2 ✓
1+40			5.1	341.3	38.1	+ 3.2 ✓
1+80 B			5.3	341.1	337.9	+ 3.2 ✓
2+20 B			5.7	340.7	337.5	+ 3.2 ✓
2+60			6.0	340.4	37.0	+ 3.4 ✓
3+00			6.6	339.8	36.5	+ 3.3 ✓
3+40	2.40	341.71	7.10	339.31	36.0	+ 3.3 ✓
3+80			2.6	339.1	35.5	+ 3.6
4+20			3.1	338.6	35.0	+ 3.6
4+60			3.9	337.8	34.5	+ 3.3
5+00 B			4.6	337.1	334.0	+ 3.1
5+50 B			5.8	335.9	332.7	+ 3.2
6+00 B			8.2	333.5	330.1	+ 3.4
N. Line Myrtle						
E. ch.			8.3	333.4		

N.W. Dwight
+ Fairmont

Poplar St. Water Grades

Fire Hydrant Ely. Cor Columbine

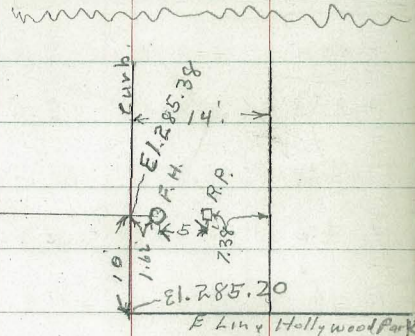
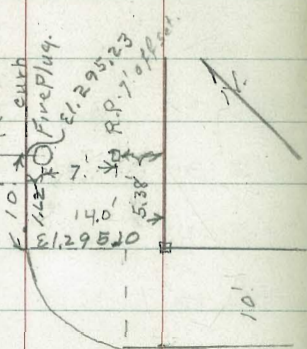
BM. Mon 305.45
+ Poplar

0.12
305.67
12.69
293.58
1.58
295.16
8.15
287.01
6.74
293.75

NW. Glenfield
+ Poplar

395.23
10.44
8.64
+ 1.76

247.01
4.08
291.09
285.38
5.71
5.34
+ 0.37

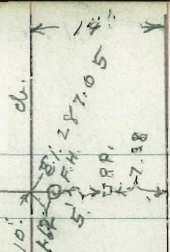
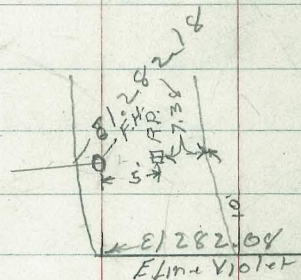


Indexed
C.S.K.

293.75
7.01
286.74
6.10
292.84
8.01
284.85
5.38
290.21
5.97
284.24 = 284.08

293.75
287.05
6.70
7.01
- 0.31
El. 287.00
Ely. Cor Columbine
BM. Pipe N.E. Violet

292.84
282.18
10.66
8.01
+ 216.5



Culvert Grades Webster Ave.

Indexed
C.S.K.

33

B.M. B.P.	1.14	63.07	61.93	N.W. Webster & Bancroft		
E. curb Bancroft						
S. cl Webster		Top. curb	4.87			
S. line "			5.07	58.00		
14. South "			4.86	- 6.00	Depth of C.B.	
					Fl. Grade	
S. cl. Line Webster = N. & S. C.B.			4.87	58.20	52.00	+6.20
0+50 = { clean out $\Delta 90^{\circ}-00$ Rt.						
-42.11 = { E. curb line = 4 R. of W to E.			3.83	59.24	51.50	+7.74
Profile 1+00			7.87	55.20	49.50	+5.70
1+50 Brk			11.07	52.00	47.50	+4.50
T.P.	0.33	50.50	12.90	50.17		
1+95 Brk			2.6	45.5	42.00	+3.5
T.P.	1.88	39.35	13.03	37.47		
2+22 Σ			6.95	32.40	32.4	0.0
T.P.	0.41	26.89	12.87	26.48		
2+60.			3.89	23.00	19.0	4.0
2+75 W. end Pipe	24" Diam		6.55	20.34 Top		
" " "				- 2		
				18.34 Fl.		
E. End above Pipe			9.23	17.66		
+46.5			9.09	17.80	17.40	+0.40
+93. W. End. Pipe under 33 rd St			9.85	17.14		

		26.89							
T.P. Hydr.	1.40	23.00	5.29	21.60					
0+00					Grade				
E. end 33rd st. Pipe			6.45	16.15	16.15				
0+40			4.89	18.11	15.95		+2.14		
0+80			5.30	17.70	15.75		+1.95		
1+20			5.66	17.34	15.55		+1.79		
1+60 W. end Pipe			FL. Pipe			Grade			
			7.06	15.94	To Belowward	5.05	17.95	15.35	+2.60 ✓
E. " "			FL. Pipe		" " "	5.40	17.60	15.10	+2.50 ✓
			7.41	15.59	" " "				
30' E. W	" "		7.72	15.28	" " "	5.63	17.37	14.90	+2.47 ✓
E. " "	" "		7.72	15.28 ✓	" " "	5.78	17.22	14.70	+2.52 ✓
0+50			6.54	16.46	14.40		+2.06 ✓		
1+00			6.25	16.75	14.10		+2.65 ✓		
1+50 W. end. Pipe			FL. Pipe		To Belowward	5.70	17.30	13.80	+3.5 ✓
			7.25						
E. " "			FL. Pipe		" " "	5.20	17.80	13.50	+4.30 ✓
			7.60	15.40	" " "				

Five House 8th 9 J. Sts

Indexed
c.s.k.

π 25.26

π 25.26

35

B.M. BP.

6.26

25.26

19.00

N.V. cor

" "

5.05

24.05

19.00

8th J. Sts

0+00 = E End = W. line 9th St.

line 9th St.

π 24.05

19.50

17.75

Floor

Bottom Footing S.

Floor S.

+1.50

4.55 ✓

+1.75

19.50

5.74 ✓

17.5

+2.0

19.50

5.76 ✓

0+14.2

17.75

+1.67

19.42

4.63 ✓

17.50

+1.92

19.42

5.84 ✓

17.25

+2.77

19.42

5.84 ✓

0+28.4

17.50

+1.83

19.33

4.72 ✓

17.25

+2.08

19.33

5.93 ✓

17.00

+2.33

19.33

5.93 ✓

0+42.4

17.25

+1.99

19.24

4.81 ✓

17.00

+2.24

19.24

6.02 ✓

16.75

+2.49

19.24

6.02 ✓

0+56.8

17.00

+2.16

19.16

4.89 ✓

16.75

+2.41

19.16

6.10 ✓

16.50

+2.66

19.16

6.10 ✓

0+71

16.75

+2.33

19.08

4.97 ✓

+74

16.50

+2.56

19.06

6.20 ✓

16.25

+2.83

19.08

6.18 ✓

0+85

W. End.

16.50

+2.50

19.0

5.05

16.25

+2.75

19.00

6.26 ✓

14.0

+3.00

19.0

6.26 ✓

19.00

Floor G

19.50

5.745

5.03

-0.50

G.R.

24.03

19.00

chk 4.55

19.48

See Page 5th.

1-28-36
Miller
Walker
Blair

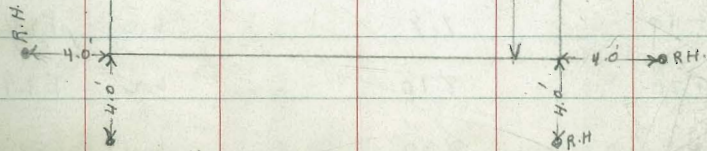
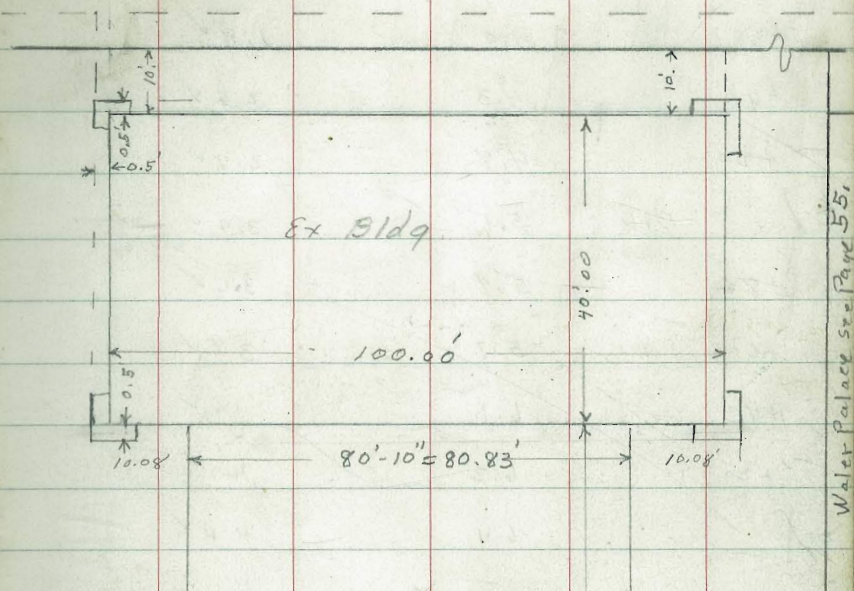
Building at City Yards 20th + B. St.

Indexed
C. S. K.

36

← W. Line 20th St. Produced. B. St.

BM, BP	0.83	71.07	70.24	S. E. 20 th + B. St.
		4.87	66.20	✓ Floor Elev Shop.
Plans		5.82	65.25	
Nail Elev Pole		5.50	65.57	✓ Floor Elev New Bldg
BM	0.86	71.10	70.24	
Floor Elev Shop.		4.90	66.20	✓
TP	4.69	70.26	5.53	65.57
466 464		4.69		
		4.65		
		4.61		



Store Room

120'-5" = 120.42'

Water Palace see Page 55

2-3-36

Grade for Fence at Golf Course
E. Side Pershing Drive S. of Redwood

Ground Rod

{ 2' above Grade }
Grade Rod

+60 4.0 1.9 ✓

+40 4.3 2.4 ✓

+20 4.8 2.9 ✓

3 Brk 5.1 — 3.4 ✓ —

+80 5.4 3.6 ✓

+60 5.7 3.8 ✓

+40 6.1 4.0 ✓

+20 6.2 4.2 ✓

2 6.4 4.4 ✓

+80 7.0 4.6 ✓

+60 7.1 4.8 ✓

+40 7.2 5.0 ✓

+20 7.3 5.2 ✓

1 +00 S. End. Fence 7.3 5.4 ✓

+80 7.4 5.6 F. 1.8

+60 7.5 5.8 F. 1.7

+40 7.8 6.0 F. 1.8

+20 8.10 6.2 F. 1.9 ✓ 4

0400 8.30 6.4 F. 1.9 ✓

Indexed
C.S.K.

37

Ground Rod

{ 2' above Grade }
Grade Rod

+60

+40

+20

5

+80

+60 N. End. Fence

1.5

+0.6 ✓

+40

2.2

+0.7 ✓

+20

2.7

0.4 ✓

4

3.0

0.9 ✓

+80

3.5

1.4 ✓

2-5-34

Ampludia Pav. Grades
La Jolla Ave to. Jefferson.

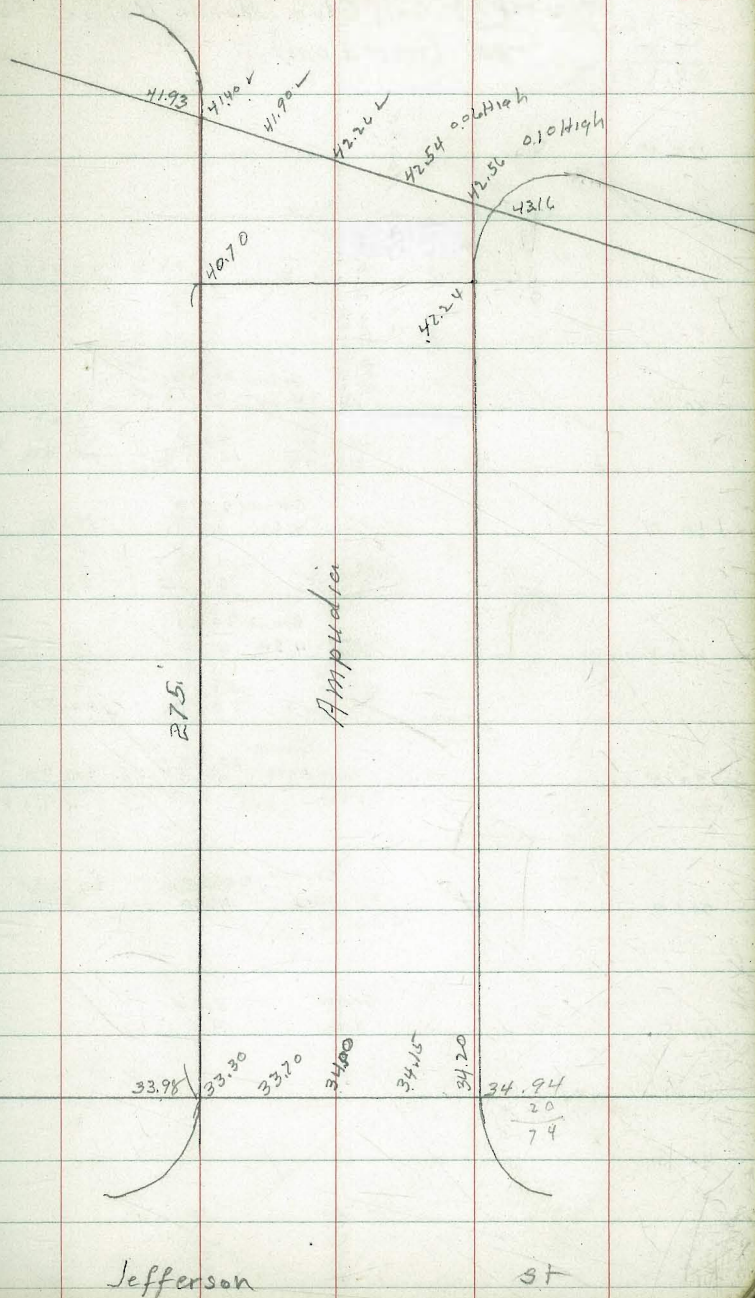
BM. B.P	2.21	45.96	43.75
E. el		2.80	43.16
E. G		3.40	42.56
1/4		3.42	42.54
E		3.70	42.26
1/4		4.06	41.90
N. G		4.56	41.40
W. el		4.03	41.93

N. line Jefferson

E. el	11.02	34.94
E. G	11.76	34.20
W. G	12.66	33.30
W. el	11.98	33.98

Indexed
C.S.K.

38



2-10-36

Grades for Parking Area

Municipal Golf Club. House Balboa Park.
pal (what a pal)

Indexed
C.S.K.

39

AM. 220.49
4.41
224.90

120' N

108' N

100' N

80' N

60' N

40' N

20' N

0+00

20' S

40' S

Cmt. Porch.
Golf Club. House.
FAM. Elev 220.49
Cmt. Porch.

Ground 20.10
4.60 4.80 ✓
5.20
4.80
+0.40

Ground 20.10
4.80 4.80
5.10
4.80
+0.30

Ground 20.20
4.50 4.70 ✓
5.00
4.68
+0.32

Ground 20.30
4.40 4.60
20.30 4.80
4.60 ✓
4.57
+0.23

Ground 20.40
4.40 4.30
20.40 4.30 ✓
20.60 4.80 ✓
4.30 ✓

Ground 4.2
Ground 4.0

0+00

20' S

40' S

60' S

80' S

100' S

120' S

20.10 ✓ 19.40
4.80 ✓ 5.10
4.74
+0.32

19.70 19.40
5.20 5.50
4.80 4.40
+0.70

19.80 19.50
5.10 5.40
4.80 4.80
+0.60

19.90 19.40
5.00 5.10
4.68 4.68
+0.42

20.30 20.10
4.60 ✓ 4.80
4.57
+0.23

20.40 20.60
4.30 4.80 ✓
4.30 ✓

19.50 219.00
5.40 5.90
4.92 4.78
+0.48

19.10 18.70
5.80 6.20
4.94 4.84
+0.86

19.40 19.30
5.50 5.60
5.02 5.02
+0.48

19.70 19.70
5.20 5.20
4.75 4.82
+0.45

20.10 220.10
4.80 4.80 ✓
4.65
+0.15

20.80 ✓ 20.90
4.10 4.00 ✓
20.90 ✓

5.90
4.78
1.12
18.70
6.20
4.84
+1.36

6.00 18.90
4.88 6.00
+1.12 5.06
+0.94

19.30 19.30
5.60 5.60
5.02 4.85
+0.58

19.70 19.70
5.20 5.20
4.82 4.92
+0.38

220.10 220.10
4.80 4.80 ✓
4.80 ✓

20.90 ✓ 220.90
4.00 4.00 ✓
4.00 ✓

218.30
6.60
5.50
+1.10

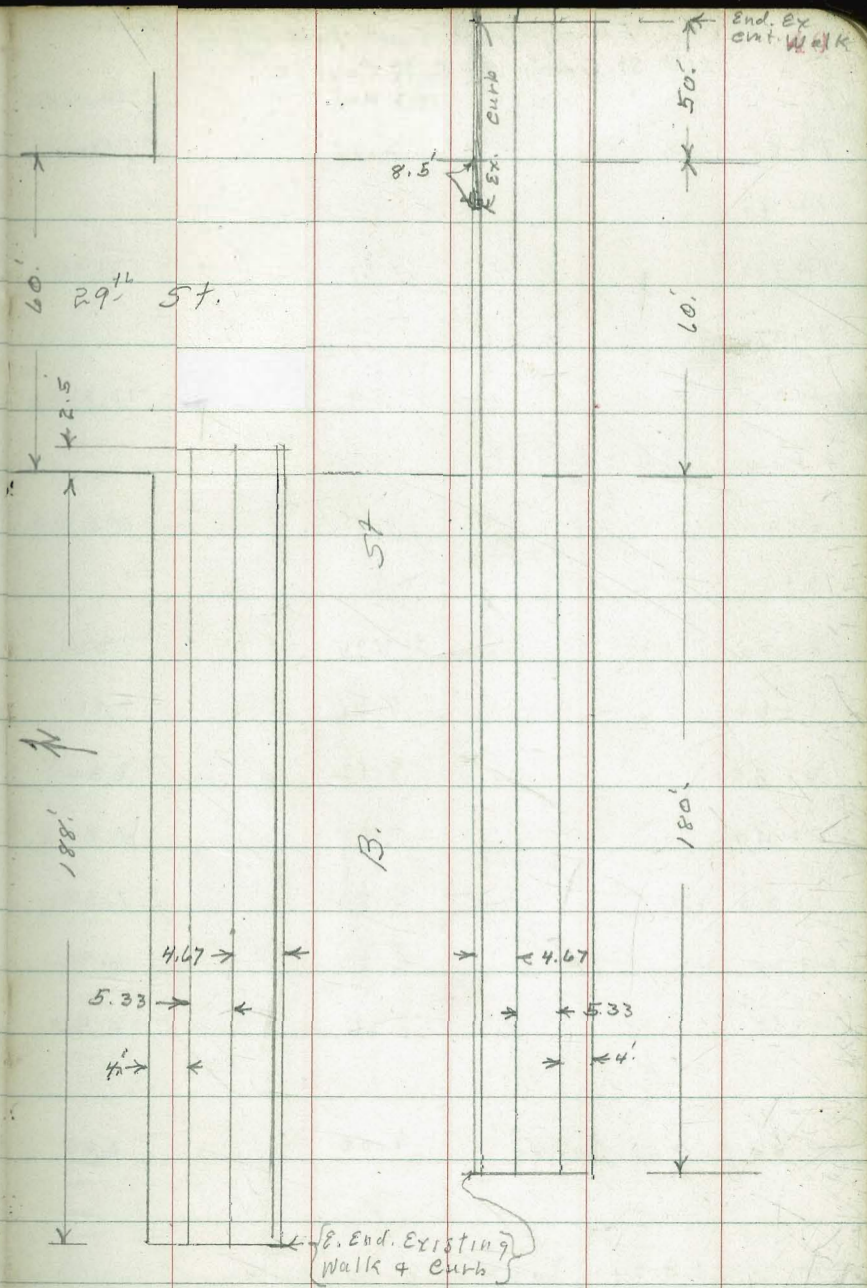
108' N

2-10-36 Side Walk & Curb Grades.
B. St. at 29th

Indexed
C.S.K.

5.40
4.87
53

4.60
54
5.14



Fence Grades at foot of
26th St. Grade at Golf Course.
stab Rod.

4-22-36

Indexed
c.s.k.

41

	stab Rod.	Grade Rod	
1+50	12.97	12.90	-0.07 ✓
1+40			
1+30	11.61	11.98	+0.37 ✓
1+20			
1+10	10.84	11.06	+0.22 ✓
1+00			
0+90	9.81	10.14	+0.33 ✓
0+80			
0+70	8.95	9.22	+0.27 ✓
0+60	8.51	8.76	+0.25 ✓
0+50	8.12	8.30	+0.18 ✓
0+40	7.58	7.84	+0.26 ✓
0+30	6.80	7.38	+0.58 ✓
0+20	6.66	6.92	+0.26 ✓
0+10	6.26	6.46	+0.20 ✓
0+00 = E. End. Fence	6.00	6.00	00

B.M. Assumed 8.34

E. End conc Head wall S. of Road.

Permit Grades Alliy BIK
 65 W.P. Herber's Afd. Bet. 39th
 + 40th S. of Monroe

Indexed
 c.s.Kr.

T.P. el

5.88

377.85

371.97

ent. el
 W
 pay

W

E

E

ent. el

1+60 B

OUT

372.83

373.03

S. Lm. Monroe

6.21

6.43

6.44

6.17

5.88

371.64 ✓

371.42 ✓

371.41 ✓

371.68 ✓

371.97 ✓

2+00.13

372.88

373.04 ✓

0+20 25 B

371.98

271.83

372.21

2+20 B

out

372.80

373.00

5.87
 4.87
 + 1.00

6.02

5.64
 4.98
 + 0.66

4.79
 4.20
 + 0.59 ✓

4.59
 4.45
 + 0.14 ✓

0+40 25 B

372.33

372.54

2+40 B

372.72

372.92

5.52
 4.85
 + 0.67

5.31
 4.92
 + 0.39

4.95
 4.29
 + 0.66 ✓

4.75
 4.06
 + 0.69 ✓

0+60 25 B

372.49

372.69

2+80

372.50

372.70

5.36
 4.70
 + 0.66

5.16
 4.16
 + 1.00

5.17
 4.99
 + 0.18 ✓

4.97
 3.95
 + 1.02 ✓

0+87 25

372.55

372.75

3+40

372.28

372.48

5.30
 5.12
 + 0.18

5.10
 4.10
 + 1.00

5.39
 4.64
 + 0.75 ✓

5.19
 5.45
 - 0.26 ✓

1+00 25

372.60

372.80

3+90 B

372.06

372.26

5.25
 5.01
 + 0.24

5.10
 4.10
 + 1.00

5.61
 5.30
 + 0.31 ✓

5.41
 5.24
 0.17 ✓

1+30 25

372.69

372.89

4+10 B

371.96

372.16

4.98
 4.98
 0.0

5.05
 4.05

3.42
 3.10
 + 0.32 ✓

3.22
 2.90
 + 0.32 ✓

X 377.67

4+30 B

371.81

372.00

3.57
 2.82
 + 0.75 ✓

3.38
 3.28
 + 0.10 ✓

Continued Page 64.

377.67

372.78
 4.89
 5.10
 - 0.21 ✓

5.19
 372.48
 2.90
 375.38 ✓

372.98
 4.79
 4.09
 + 0.70 ✓

Club House.
Police Pistol Range

5-17-36

Indexed
C.S.K.

43

All R.P.s 5'

BM. 50.00 on walk

4.80
54.80

50.50 Floorgrade

4.30

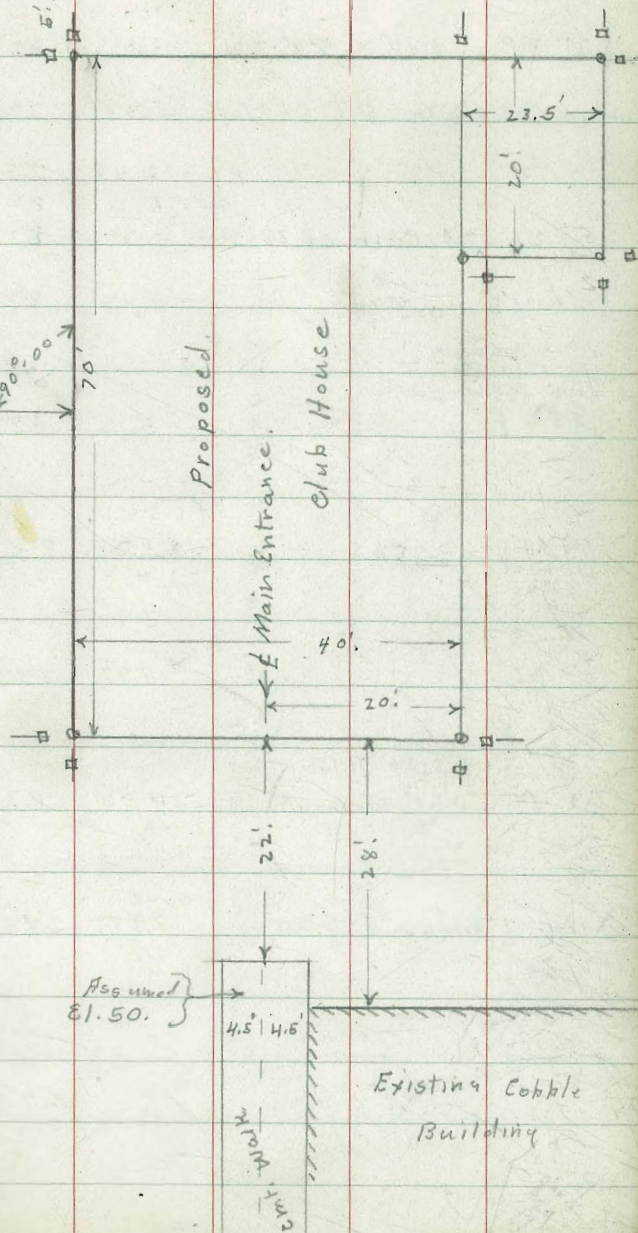
Main Bldy.

N.W. Cor	S.W. Cor	N.E.	S.E.
4.30	4.30	4.30	4.30
4.69	5.53	3.67	4.72
-0.29	-1.23	+0.63	-0.42

Wing

N.W.	S.W.	S.E.	N.E.
4.30	4.30	4.30	4.30
4.81	5.41	4.78	4.72
-0.51	-1.11	-.48	-0.42

Covered Pergola 25 yd. Range



Comfort Station
Memorial Play Grounds.

5-25-36

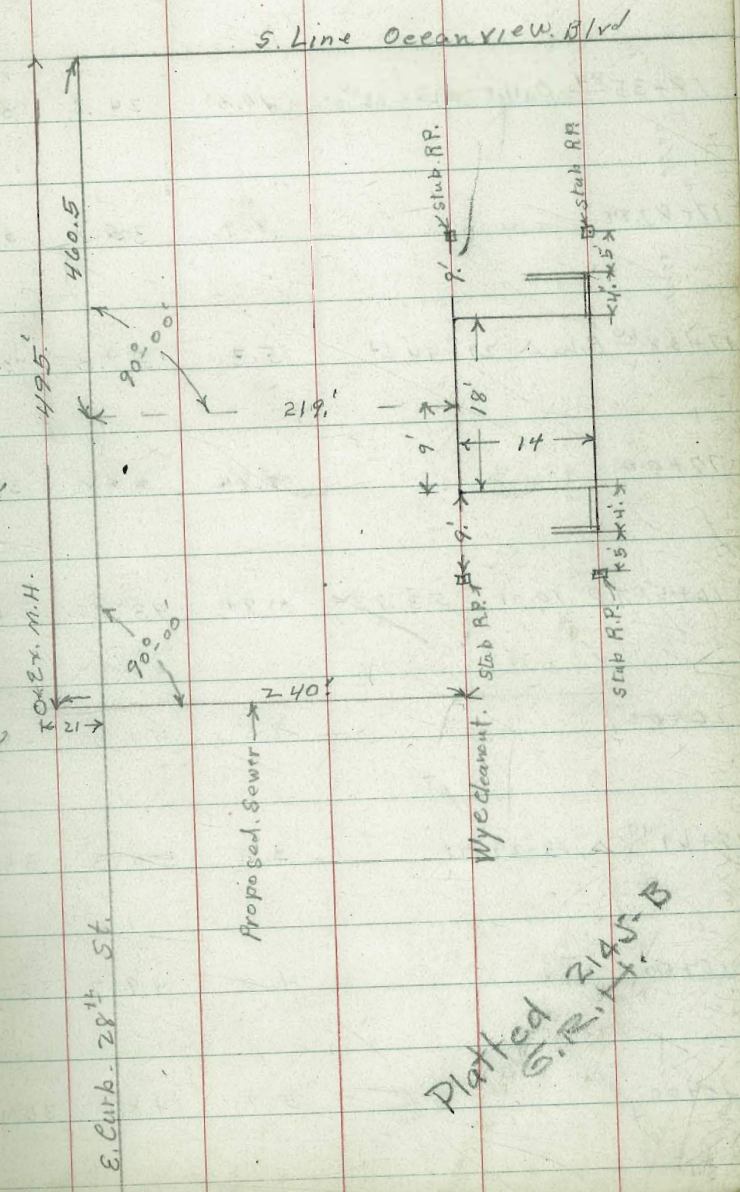
Indexed
C.S.K.

44

B.M. B.P. 1.17 88.22 87.05 ^{N.W. Stearns} & Harrison

0+00 = M.H. 1h. 28 th St. Top.	5.38	82.84	76.24	+6.60
" " " " F.L. 12.48 gutter 6.0		75.74	76.24	-0.50
0+21 = E. Curb of 28 th St. 5.30		82.2		
0+41	4.48	83.74	77.04	+6.70
0+91	5.16	83.06	78.04	+5.02
1+41	5.00	83.22	79.04	+4.18
1+91	4.97	83.25	80.04	+3.21
2+40 W. side Bldg. Wye. cleanout.	4.50	83.72	81.04	+2.68
Floor of Bldg.	2.82	85.40		

1/4" To the ft. = 2.0000'



Platted Right of Way

6-19-36

Southlook

Storm Drain
See Book 1505-40.See Book 182
Page 46Indexed
c.s.k.

45

BM. & stub	12.95	44.61	31.66	18+35.84		
18+35 ⁸⁴ Outlet = W. Line 36 th St.	10.31	34.3	31.60	FL. Grade	+2.7	
4862 17+87.22	8.9	35.7	32.8		+2.9	
4962 17+38 ⁴⁰ Brk Δ 21° 54' Lt.	5.3	39.3	34.00		+5.3	
17+00	4.8	39.8	34.4		+5.4	
16+50 T.P. 10.01	53.73	0.89	43.72	34.9	+8.8	
16+00	9.5	44.2	35.4		+8.8	
15+69 ⁴⁰ Δ 13° 29' Rt.	3.4	50.3	35.7		+14.6	
15+50	4.0	49.7	35.9		+13.8	
15+00	5.7	48.0	36.4		+11.6	

53.73

14+50 7.1 46.6 36.9 +9.7

14+00 8.0 45.7 37.4 +8.3

13+61¹⁰ # Curb inlet #10 8.4 45.3 37.8 +7.5

13+50 8.2 45.5 37.9 +7.6

13+00 7.3 46.4 38.4 +8.0

12+50 6.0 47.7 38.9 +8.8

T.P. 12.81 60.84 5.70 48.03 3 Nails Tel. Pole N.W. Ocean View + Olive Wood Terrace

12+42 ? cleanout on Ex. pipe from E.

11+74 # Curb inlet #9 12.81 48.0 39.7 8.3 ✓

↑ 36" Pipe

11+46²³ Cleanout #1 12.3 48.5 40.00 +8.5 ✓

↓ 30" Pipe

11+00 10.94 49.9 41.05 +8.9 ✓

60.84

10+50		9.16	51.7	42.16	+9.54	
10+00		7.64	53.2	43.27	+9.91	
9+50		5.15	55.7	44.38	+11.3	
9+	S. End Curto inlet	4.0	56.8	44.5	+12.3	
9+22 ²³	ch. inlet #8			45.00		
				47.00		
2	ch. inlet #7			51.0		
	S. End. ϕ Box, 3.5	57.3			+6.3	grade raised 4'
8+40		5.4	55.4	45.7	+9.7	
7+96 ²⁵	ch. inlet #6	7.0	53.8	46.30	+7.5	
59.3						
7+37		8.3	52.5	47.4	+5.1	
59.3						
	ch. inlet #5					
6+77.70		6.0	54.8	48.6	+6.2	
T.P.	10.10	65.31	55.21			

65.31

48

6+20² 9.1 56.2 49.7 +6.5

9.1 56.2 50.8 +5.4

5+63² 9.1 56.2 50.8 +5.45+07¹ 8.5 56.8 51.8 +5.04+50³ 7.7 57.6 52.8 +4.83+93⁵ W. Line Milbrae 6.0 59.3 53.8 5.5el. inlet ⁴/₄el. inlet ³/₃3+43⁵⁰ E. Line Milbrae 5.1 60.2 54.6 +5.6New. Grade
3+09 for change orig. Grade
55.9New. Grade
Ex. Pipe
57.202+89¹ 1.5 63.8 57.0 +6.8 58.3 +5.5 ✓

T.P. 13.25 77.79 0.77 64.54

2+34⁷ 11.4 66.4 59.4 +7.0 60.7 +5.7 ✓

77.79

1+80 $\bar{3}$			6.7	71.1	61.8	+9.3	63.1	+8.0
----------------	--	--	-----	------	------	------	------	------

1+25 $\bar{2}$			4.5	73.3	64.2	+9.1	65.5	+7.8
----------------	--	--	-----	------	------	------	------	------

0+71 $\bar{5}$ Δ			2.1	75.7	66.6	+9.1	67.9	+7.8
-------------------------	--	--	-----	------	------	------	------	------

ch. inlet $\bar{2}$

0+11 $\bar{5}$ ch. inlet $\bar{1}$ *

0+00 = Existing 15" Culvert

Profile
69.00 $\bar{6}$

B.M. B.P.			1.63	76.76	N. E. 38 th + Franklyn
-----------	--	--	------	-------	--------------------------------------

B.M. B.P.	4.15	80.91		76.76
-----------	------	-------	--	-------

Existing Pipe			Red 3.71	
			+ 7.90	
F.L. on Pipe			11.61	69.30

T.P.	1.07	70.05	11.93	68.98
------	------	-------	-------	-------

Sta. 3+09 F.L. Pipe			12.85	57.20
---------------------	--	--	-------	-------

8-7-36
Miller
Walker

Grades for Gutter
Penning Drive

1+79⁸ B.C.

15.8

1+64 E.C.

Def 4

27-41

1+43⁵

24-13.3

1+23

20-45.6

1+02⁵

$\Delta = 55^{\circ} 22'$ 17-18'

0+82

R 170' 13-50.4

T 89.18

0+61⁵

Chd, 20.52' 10-22.8

0+41

6-55.2

0+20⁵

3-27.6

0+00 = B.C.

10

BM

Indexed
o.s.k.

stake

50

20
3.6
58.0

3.61 57.98 57.45 +0.53 ✓

4.64 56.95 56.45 +0.50 ✓

20.17
5.9
55.7

5.63 55.96 55.10 +0.86 ✓

7.04 54.53 53.90 +0.63 ✓

20.17
7.8
53.8

8.61 52.98 53.10 -0.12 ✓

9.21 52.38 52.50 -0.12 ✓

20.17
9.3
52.3

9.51 52.08 52.00 +0.08 ✓

10.25 51.34 51.65 -0.31 ✓

10.00

10.14
51.45

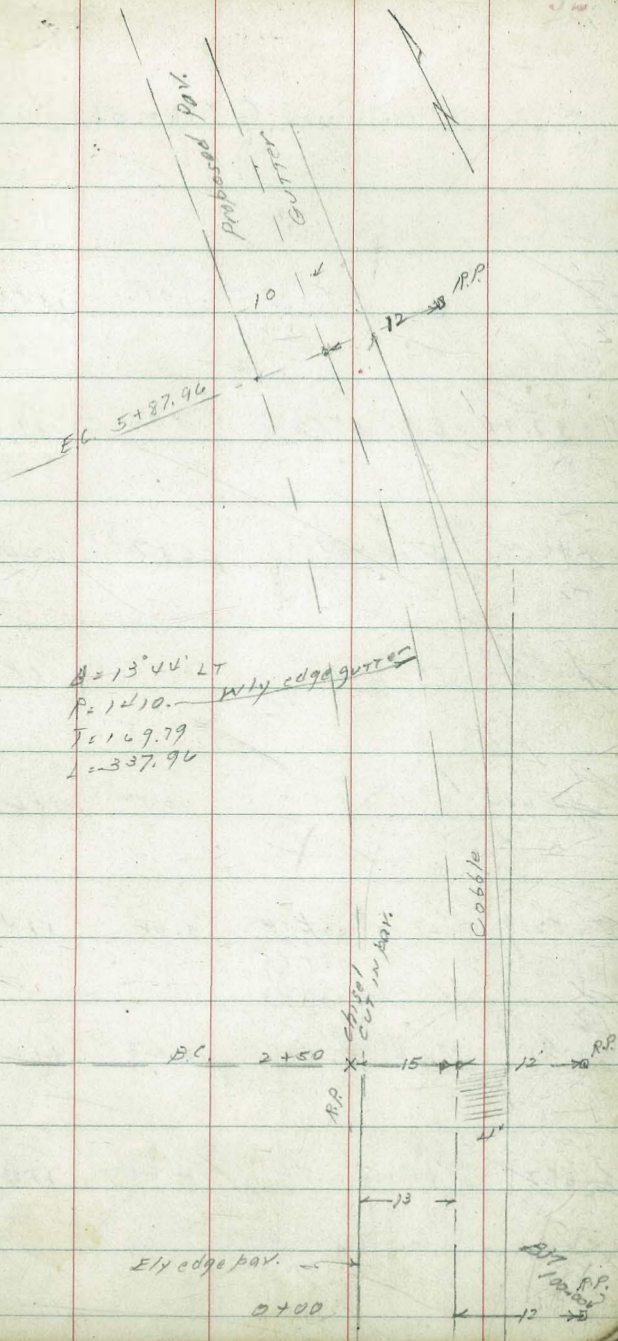
10.61 50.98 51.30 -0.32 ✓

50.00
assumed

						Stub				
4+89					1.42	18 ^W Pay 1.53 77.51	1.70	77.34	77.20	+0.14
4+39						74.12	5.49	73.56	73.82	-0.26
					T.P.	8.59	79.04	2.55	70.45	
3+89					2.25	2.25 ^{Pay} 70.75	2.55	70.45	70.45	-0.00
3+39						5.33 ^{Pay} 67.67	5.43	67.57	67.45	+0.12
2+89	EC	Def 2 11-10				12.5 Pay 8.24 64.76	8.62	64.38	64.45	-0.07
2+67.0		8-56				12.5 Pay 9.44 63.56	9.76	63.24	63.05	+0.19
2+45 ²	Δ = 22.20	6-42					10.67	62.33	61.65	+0.68
	R = 280				T.P.	12.06	73.00	0.65	60.94	
2+23 ⁴	J = 55.27	4-28				26 Lt. 0.9 60.7	0.65	60.94	60.25	+0.69
	L = 109.14									
2+01.6	chd. 21.78	2-14					2.26	59.33	58.85	+0.48
1+79 ⁸	BC					26 Lt. 3.6 58.0 41.59	3.61	57.98	57.45	+0.53

1/2 to 1 Cut
 Pershing Drive
 Gutter CONST. see G176-51
 E. edge Pav. Wedge
 Gutter Grade

Station	Angle	Dist	E. Edge Pav.	Wedge Gutter Grade	Notes
0+51.4	2°03'30"	6.50	108.32	108.10	C 18.0 0.5 OUT
0+17.6	1°22'30"	8.56	106.26	106.0	C 12.8 0.4 OUT
2+89.8	0°41'12"	10.00	104.22	104.0	C 14.4 4.7 OUT
+50 BC		1.65	102.05	101.75	C 14.1 7.0 OUT
2		4.90	98.74	98.44	C 12.4 0.2 OUT
+150		8.10	95.60	95.30	C 10.5 5.3 OUT
T.P.	12.51	114.84 0.67 114.17 13.41 126.56	102.31		
1		11.12	92.58	92.28	C 4.1 2 OUT
+50		13.90	89.80	89.50	C 5.9 4.0 OUT
0+00		16.80	86.90	86.60	C 13.0 6.5 OUT
0+00	370	103.70	100.0		12' OUT Pav. Stake assumed E.L.



Continued G 176-51.

T.P.		1.95	135.51	121.05	121.05	
	<u>137.46</u>					
5+87.94 = EC	6°52'	4.71	121.85	121.05	121.05	C 13.8 6.9005
5+54.2	6°10'48"	6.57	120.0	119.8	119.8	C 12.4 6.1005
5+20.4	5°29'36"	8.57	118.0	117.8	117.8	C 12.0 6.0005
+86.6	4°48'24"	10.52	116.0	115.8	115.8	C 11.7 5.8
4+52.8	4°07'12"	0.61	114.2	114.0	114.0	C 11.6 5.8005
	$\begin{array}{r} 126.50 \\ 1.01 \\ \hline 125.54 \\ 11.91 \\ \hline 137.46 \end{array}$					
4+19	3°26'	2.63	112.20	112.0	112.0	C 11.8 5.9005
3+85.4	2°06'48"	4.61	110.21	110.0	110.0	C 12.2 6.4005

G. 176-51.

T

Fire Engine House 8th + J.
Floor Grades.

Indexed
C.S.K.

BM.B.P.	5.19	24.19	19.00	N.W. 8 th + J. St.				
		0+50 ^N	0+44 ^N	0+38 ^N	±	0+12 ^N	N+06 ^N	0+00 ^N + 5. N. like J. St.
0.0 - 14. = Curb		4.53						5.19 El 19.00
0.0 - 4.5 inside Walk		4.32						5.00 El 19.19
0+00 =								
W. Line 8 th		<u>19.93</u> 4.26	<u>19.59</u> 4.60	<u>19.59</u> 4.60	<u>19.59</u> 4.60	<u>19.50</u> 4.69		El 19.25 4.94
T.P.	6.30	N 25.16	5.33	18.86				
0+09 ^W			<u>19.70</u> 5.46 ✓	<u>19.67</u> 5.49 ✓	19.67	<u>19.67</u> 5.49 ✓	<u>19.70</u> 5.46 ✓	
11								
0+20			<u>19.64</u> 5.52 ✓			<u>19.60</u> 5.56 ✓	<u>19.64</u> 5.52 ✓	
18								
0+38			<u>19.52</u> 5.64 ✓			<u>19.48</u> 5.68 ✓	<u>19.52</u> 5.64 ✓	
18								
0+56			<u>19.40</u> 5.76 ✓			<u>19.36</u> 5.80 ✓	<u>19.42</u> 5.74 ✓	
18								
0+74			<u>19.28</u> 5.88 ✓			<u>19.24</u> 5.92	<u>19.28</u> 5.88 ✓	<u>19.32</u> 5.84 ✓
11								
0+85			<u>19.17</u> 5.99 ✓	<u>19.12</u> 6.04 ✓		<u>19.17</u> 5.99	<u>19.23</u> 5.93	

Survey of Footings for Water Palace
at City Shops, 19th + B. Sts

12-30-36
Water
Alma

Indexed
C.S.K.

499

515

B.M. BP

70.23

70.23

5 E. 20th + B.

63.55
3.90
67.45
3.59

71.10
7.55
63.55
3.93
67.48

N. End
2+60

63.86
9.81
73.67
10.73
62.94
4.79

5. W. of W. Side
of Bldg
Grades 6"
below Floor Elev
73.67
66.60
7.07
1.53
+5.54

4 Bldg
10 E. of E. Side
66.60
7.07
5.16
+1.91

10 E. of E. Side

N. End

66.60
66.60
7.07
4.58
-3.70

2+60

2+40

67.73
4.14
63.55

66.40
7.27
1.84
+5.43

66.40
7.27
7.34
-0.07

66.40

2+40

66.40
1.08
4.74
-3.66

2+00

66.00
7.27
3.31
+4.36

66.00
7.67
8.59
-0.92

66.00

2+00

66.00
1.48
5.26
-3.78

B.M. BP. NW 1/4 + B. 5.26

68.37

Grades - W. wall Existing Shed.

B.M.

6.15

69.26

T.P.

7.62

70.04

4.84

62.42

63.11

6.58

69.79

Grades on plane

63.11

66.50

3.27

3.09

2.89

2.69

2.49

2.29

2.09

1.89

1.69

1.49

1.29

64.00

2.50

66.50

3.22

3.02

2.82

2.62

2.42

2.22

2.02

1.82

1.62

1.42

1.22

1.02

0.82

0.62

0.42

0.22

0.02

0.16

0.36

0.56

0.76

0.96

1.16

1.36

1.56

1.76

1.96

2.16

2.36

2.56

2.76

2.96

3.16

3.36

3.56

3.76

3.96

4.16

4.36

4.56

4.76

S. End Bldg =

0+00

64.00
9.67
10.73
-1.06

64.00
9.67
11.31
-1.64

64.00
3.48
4.85
-1.37

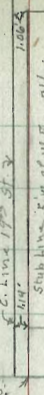
0+00 S. Bldg

64.00
4.4

0+00

67.50

1.76



125.0

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

5-8-37

Finish Floor Grades

- 63.11 B.M. -

5.84	65.48
169.00	3.93
6.81	169.41
62.49	
1.64	
171.15	
5.62	
65.48	

E. Wall

Top Wall

W. Wall

	2.50	
	66.50	
	64.50 E1	4.50
	4.50	4.91
0+20	4.30 ✓	4.71 ✓
0+40	4.10 ✓	4.81 ✓
0+60	3.90 ✓	4.31 ✓
0+80	3.70 ✓	4.11 ✓
1+00	3.50 ✓	3.91 ✓
1+20	3.30 ✓	3.71 ✓
1+40	3.10 ✓	3.25 ✓
1+60	2.90 ✓	3.05 ✓
1+80	2.70 ✓	2.85 ✓
2+00	66.50	4.65 ✓
2+20	66.70	4.45 ✓
2+40	81 66.90	4.25 ✓
2+60	81 67.10	4.05 ✓
	4.85	

64.50
2.40
66.90

62.49
4.78
67.27

66.50
0.77 ✓
66.70
0.57 ✓

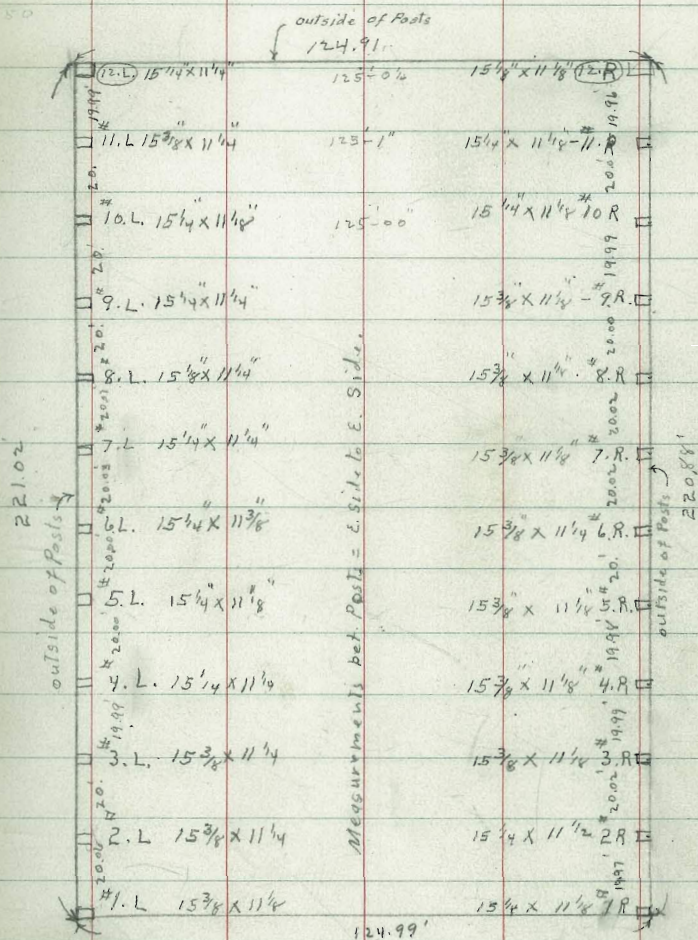
371
12
383

4.51

Park = E. End

79 C + B = N. End

56



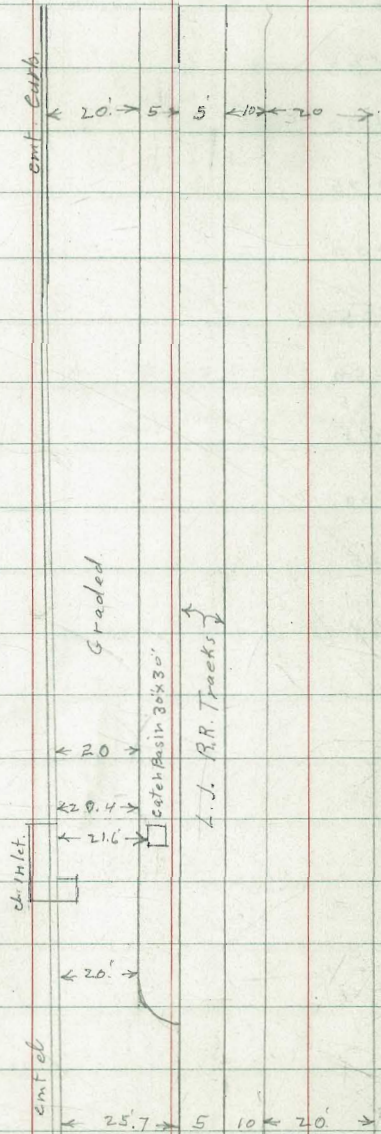
Park = N. End = S. End = 19 C + B. Sls

Grades for Oiled Pavmt Fay Ave
at La Jolla High School.

Indexed
C.S.K.

58

0+00
0+25
+50
+75
1+00
+25
+50
+75
2+00
+25
+50
+75
3+00
+25
+50
+60
+70
+75
4+00
+25
+50
+75



5+00

+25

+50

+75

6+00

+25

+50

+65

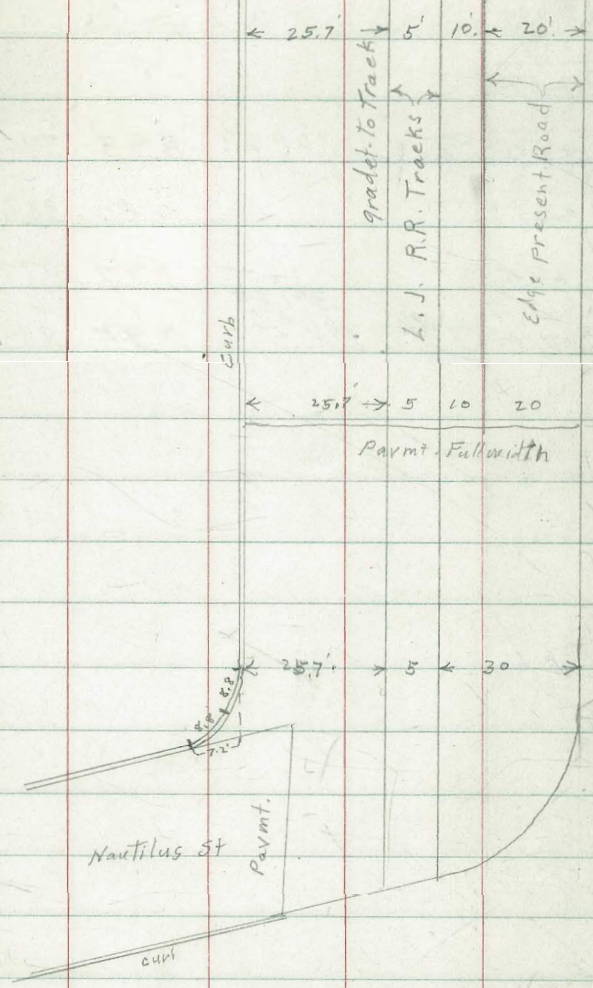
+75

7+00

+25

BC. Ret

+54



Construction Sewer
 From station 9+07 To M.H. #5 See Page 75

Station 9+15
 Elev. top Septic Tank by Miller = 378.94
 4.55+
 π 383.49
 0.15-
 T.P. 383.34
 8.49+
 π 391.83

9+07				367.89		
8+50	383.49	8.93	374.56	368.12	+6.44	
8+27		0.80	382.69	368.21	+14.48	
7+75			3.77	379.72	368.42	+11.30
7+41.71 = 7+71.53	equation M.H. #5	391.83	2.95	388.88	368.55	+20.33

39th St. Grades

8-

Indexed
C.S.K.

61

304.76

E. Line

W. Line

BM. Nail Pole 13.27 285.24

271.97 F.B. 1519-P.55 3+40 Brk

296.0
8.8
6.6
+ 2.2

295.5
9.3
7.5
+ 1.8

E. Line W. Line

281.2 280.2

S. Line Guinea

4.0 5.0

1.9 4.8

4+00 Brk

297.2
7.6
5.6
+ 2.0

296.7
8.1
6.0
+ 2.1

+ 1.1 + 0.2

T.P. 12.19 297.00 0.43

284.81

N. Line Guinea

283.2 282.2

73.8 74.8

9.3 15.3

4+40 Brk

+ 4.5 - 0.8

298.2
6.6
4.3
+ 2.3

297.7
7.1
4.4
+ 2.3

0+50

285.0 284.1

12.0 12.7

7.2 15.2

4+80 Brk

298.9
5.9
3.1
+ 2.8

298.4
6.4
4.3
+ 2.1

+ 4.8 - 2.3

1+00

284.8 286.0

10.2 11.0

5.8 13.3

5+20

299.5
5.3
3.0
+ 2.3

299.0
5.8
4.1
+ 1.7

+ 4.4 - 2.3

1+50

288.6 287.9

8.4 9.1

4.2 10.0

5+60

300.1
4.5
2.0
+ 2.5

299.6
5.0
4.1
+ 0.9

+ 4.2 + 0.9

2+00

290.4 289.8

6.6 7.2

2.6 7.4

S. Line Redwood

6+00

300.7
4.1
2.2
+ 1.9

300.2
4.6
4.0
+ 0.6

+ 4.0 - 0.2

2+50

292.2 291.7

4.8 5.3

1.3 4.8

BM. T.P.

N. Line Redwood

8.77

310.43

310 301.66

301.2
9.2
6.6
+ 2.6

300.7
9.7
7.7
+ 2.0

+ 3.5 + 0.5

T.P. 9.29 304.76 1.53 295.47

3+00

out. out.

0+40

302.6
8.4
6.2
+ 2.2

301.7
8.7
7.2
+ 1.5

3+20 Brk

294.8 294.2

10.0 10.6

7.2 10.0

0+80

302.8
7.6
5.5
+ 2.1

302.7
7.7
6.4
+ 1.3

+ 2.8 + 0.6

310.4

E. Line W. Line

1+20 Brk

203.6	303.7
6.8	6.7
<u>5.0</u>	<u>5.7</u>
+1.8	+1.0

1+60 B

204.2	304.7
6.2	5.7
<u>4.9</u>	<u>5.4</u>
+1.3	+0.3

2+00 B

204.7	305.2
5.7	5.2
<u>4.7</u>	<u>4.8</u>
+1.0	+0.4

2+40 B

205.1	305.6
5.3	4.8
<u>4.7</u>	<u>4.6</u>
+0.6	+0.2

2+80 Brk

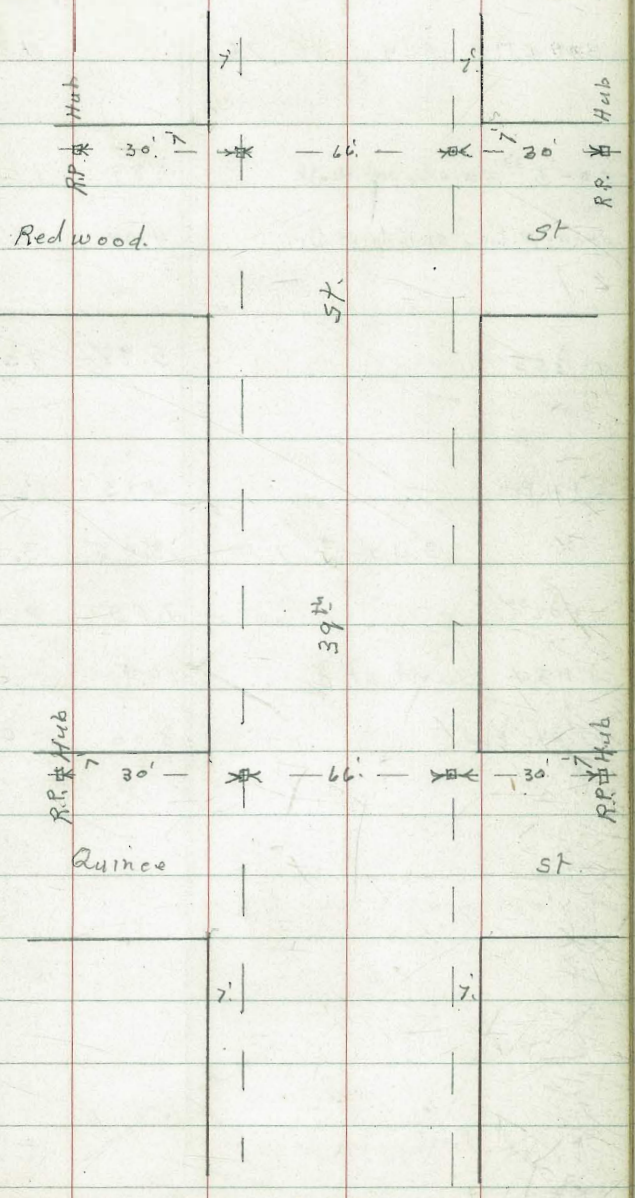
205.5	306.0
4.9	4.4
<u>4.7</u>	<u>4.3</u>
+0.2	+0.1

3+20

305.7	306.2
4.7	4.2
<u>4.5</u>	<u>4.2</u>
+0.2	0.0

3+60 B

305.8	306.3
4.6	4.1
<u>4.4</u>	<u>3.9</u>
+0.2	+0.2



Grades for 6' Path S. of Spindrift Inn. 8-14-36
 See F.B. 1503-P. 61. miles

Indexed
 C.S.K.

63

BM. C.T. a'	5.14	16.75	11.61	N. Line E. End 6' Walk	
				Grade	
00-5 ³³ = w. edge cont. Walk	4.89	11.86	11.86	00	
0+00 = N. line spindrift. Dr.	4.00	12.75	11.61	+1.14	
0+35.5	5.98	10.77	9.80	+0.97	
0+71. Brk	4.13	12.62	8.00	+4.62	
	3.40	7.10	13.05	3.70	
1+02 ⁵⁰	7.05	0.05	2.30	-2.25	
1+34 sand. at $\frac{1}{2}$	10.4	-3.3			
1+34 End.	8.00	-0.90	-3.4	+2.5	

Grades Alley BIK 65.
W. P. Herberts Add.

Continued from Page 42

W. Lin. 375.38 E. Lin.

64

4+50 B	$\begin{array}{r} 371.62 \\ 3.76 \\ \hline 3.53 \\ + 0.23 \checkmark \end{array}$	$\begin{array}{r} 371.79 \\ 3.59 \\ \hline 3.34 \\ + 0.20 \checkmark \end{array}$
--------	---	---

4+70 B	$\begin{array}{r} 371.40 \\ 3.98 \\ \hline 3.82 \\ + 0.16 \checkmark \end{array}$	$\begin{array}{r} 371.54 \\ 3.84 \\ \hline 3.44 \\ + 0.40 \checkmark \end{array}$
--------	---	---

4+90 B	$\begin{array}{r} 371.12 \\ 4.26 \\ \hline 3.90 \\ + 0.26 \checkmark \end{array}$	$\begin{array}{r} 371.25 \\ 4.13 \\ \hline 3.98 \\ + 0.15 \checkmark \end{array}$
--------	---	---

5+20 B	$\begin{array}{r} 370.65 \\ 4.73 \\ \hline 4.64 \\ + 0.09 \checkmark \end{array}$	$\begin{array}{r} 370.73 \\ 4.65 \\ \hline 4.01 \\ + 0.64 \checkmark \end{array}$
--------	---	---

5+40 B	$\begin{array}{r} 370.36 \\ 5.62 \\ \hline 5.02 \\ - 0.10 \checkmark \end{array}$	$\begin{array}{r} 370.40 \\ 4.98 \\ \hline 4.14 \\ + 0.80 \checkmark \end{array}$
--------	---	---

5+60 B	$\begin{array}{r} 370.12 \\ 5.26 \\ \hline 5.46 \\ - 0.20 \checkmark \end{array}$	$\begin{array}{r} 370.12 \\ 5.26 \\ \hline 4.82 \\ + 0.44 \checkmark \end{array}$
--------	---	---

5+80	$\begin{array}{r} 369.95 \\ 5.43 \\ \hline 5.89 \\ - 0.46 \checkmark \end{array}$	$\begin{array}{r} 369.90 \\ 5.48 \\ \hline 4.93 \\ + 0.55 \checkmark \end{array}$
------	---	---

6+00 N. Lin. Mead.	$\begin{array}{r} 369.84 \\ 5.54 \\ \hline 5.54 \\ \text{Pay } 5.54 \end{array}$	$\begin{array}{r} 369.75 \\ 5.63 \\ \hline 5.62 \\ \text{Pay } 5.62 \end{array}$
-----------------------	--	--

Normal H₂S Sewer

8-20-36

Indexed
C.S.K.

B. Line Pump House North.

B.M. 2 ¹ Pipe	0.20	<u>363.48</u> ✓		363.28	s. side E. End Collier Ave.		
58+03 ⁹³	Pump House				F.L. Grade		
					328.25		
57+93 ⁹³					328.30		
57+50			8.63	354.85	328.47	+26.38 ✓	
T.P.	2.90	<u>353.83</u> ✓	12.55	350.93 ✓			
57+00			5.02	348.81	328.68	+20.13 ✓	
T.P.	0.05	<u>341.56</u>	12.32	341.51 ✓			
56+71 ⁸⁶	M.H. 35	∠ 66° 21' R	5.91	335.65	328.78	+6.87 ✓	
56+50			5.44	336.12	328.88	+7.24 ✓	
T.P.	14.10	<u>346.33</u>	9.33	332.23			
56+00			9.06	337.27	329.09	+8.18 ✓	
55+50			7.81	338.52	329.30	+9.22 ✓	
55+00			9.06	337.27	329.50	+7.77 ✓	
54+50			8.37	337.96	328.69	+8.27 ✓	
54+39 ⁶²	M.H. 34	∠ 82° 19' R	11.02	335.31	329.73	5.58 ✓	

T.P. 54+39 ⁶²	4.02 M.H. 34	346.33 <u>339.33</u> ^v	11.02 6.72	335.31 ^v 332.61 = 332.5 ^v ϕ Hub			
54+00			0.00	339.33	329.89	+9.44 ^v	
53+55 ²²	M.H. 33	\angle 51-52 Rt	2.76	336.57	330.08	+6.49 ^v	
T.P.	8.94	<u>341.81</u> ^v	6.46	332.87 ^v			
53+00			1.44	340.37	330.30	+10.07 ^v	
52+50			3.69	338.12	330.50	+7.62 ^v	
T.P.	5.50	<u>338.38</u> ^v	8.93	332.88 ^v			
52+00			1.41	334.97	330.51	+6.46 ^v	
51+62 ¹⁰	M.H. 32	ϕ Hub	4.63	333.75 = 333.74			
51+62 ⁶⁰	M.H. 32	\angle 8-01-30 Rt	1.80	336.58	330.87	+5.71 ^v	
T.P.	10.82	<u>348.42</u> ^v	0.78	337.60 ^v			
51+00			7.77	341.25	331.12	+10.13 ^v	
50+50			7.47	340.95	331.33	+9.62 ^v	
50+00			9.58	338.84	331.54	+7.30 ^v	
49+53 ⁶⁰	M.H. 31	\angle 41-34 Rt	11.67	336.75	331.72	+5.03 ^v	

348.42

N.H. Sewer.

63

49+00			4.23	342.19	331.92	+10.27 [✓]
48+50			5.00	343.42	332.13	+11.29 [✓]
47+99 ⁹⁸	M.H. #30	$\Delta 14^{\circ}-45'$	9.75	338.67	332.35	+6.32 [✓]
" "	" "	ϕ Hub	12.42	336.00	336.01	
47+50			5.13	343.29	332.55	+10.74 [✓]
47+00 ⁵	M.H. #29	$\Delta 80^{\circ}-35'$	2.47	345.95	332.76	+13.19 [✓]
T.P.	5.23	351.20 [✓]	2.45	345.97 [✓]		
46+57 ⁷²	M.H. #28	$\Delta 67^{\circ}-09'$	5.81	345.39	332.94	+12.45 [✓]
46+00			4.83	344.37	333.17	+11.20 [✓]
45+59 ⁵⁰	M.H. #27	$\Delta 49^{\circ}-32'$	9.23	341.87	333.34	+8.53 [✓]
(45+05 ³⁰) Equation	M.H. #26	$\Delta 68^{\circ}-18'$	7.56	343.64	333.56	+10.08 [✓]
44+36 ⁶²	" " "	ϕ Hub	11.05	340.15	340.14	
T.P.	5.82	349.46		343.64		
44+00			1.60	347.86	333.71	+14.15
43+50			1.22	348.24	333.91	+14.33 [✓]

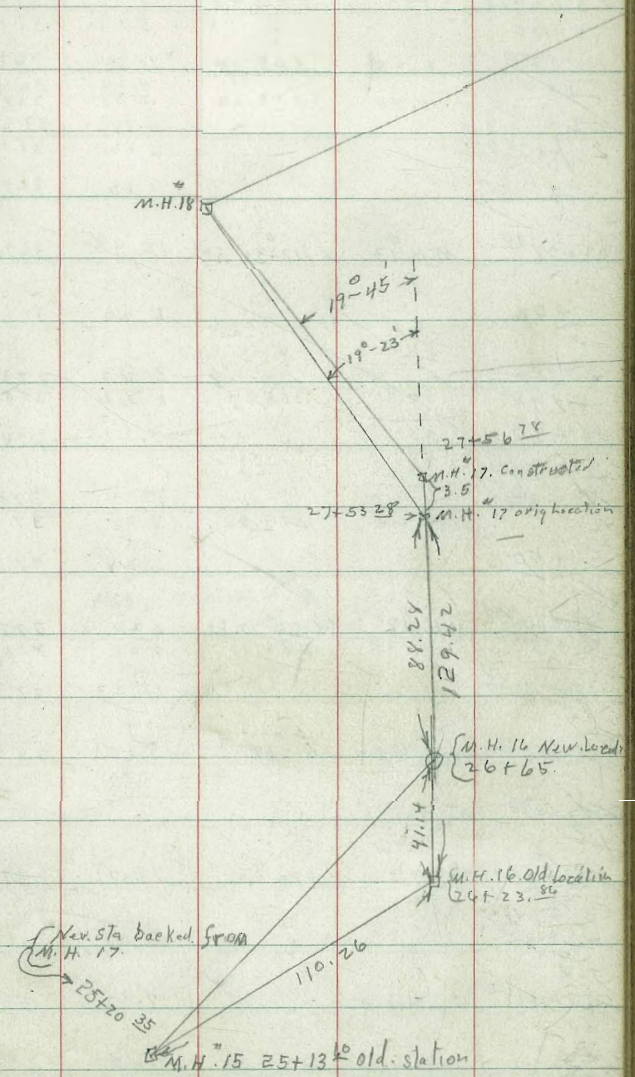
		349.46						
43+23 ¹⁴	M.H. #25	24°-57' Lt.	10.90	338.56	334.02	+4.54 ✓		
T.P.	9.82	<u>352.20</u>	7.08	342.38				
43+00			15.09	337.11	329.11	+3.00 ✓		
+50			0.70	351.50	334.31	+17.19 ✓		
42+00			1.46	350.74	334.52	+16.22 ✓		
41+87 ²⁶	M.H. #11	54°-50' Lt.	8.00	344.20	334.57	+9.63 ✓		
12.22 T.P.	0.15	<u>339.55</u>	12.80	339.40				
41+70 ²³	End. C.I. Pipe						Base of Pier	
12								
41+58 ²⁴	Pier #6		9.71	329.84	334.70	-4.86 ✓	6' Lt	328.0
12		<u>329.50</u>						
+46 ²⁴	" #5		4.35	325.15	334.75	-9.60 ✓	6' Lt	323.0
12								
+34 ²⁴	" #4		9.24	320.26	334.80	-14.54 ✓	6' Lt	318.0
12								
+22 ²⁴	" #3		5.32	324.18	334.84	-10.66 ✓	6' Lt	318.0
12		<u>339.55</u>						
+10 ²⁴	" #2		10.80	328.75	334.89	-6.14 ✓	6' Lt	326.0
12								
40+98 ²⁰	" #1		6.02	333.53	334.94	-1.41 ✓	6' Lt	330.0
12.24 T.P.	11.90	<u>350.10</u>	1.35	338.20				
40+86	End. C.I. Pipe							
14								
40+84 ²⁴	M.H. #24	Δ 87°-16' Lt.	11.47	338.63	335.00	+3.63 ✓		4 Hub 40+71.72 335.20
0.41%								
+50			8.03	342.07	335.22	+6.85 ✓		
0.65%								
40+00			3.97	346.13	335.55	+10.58 ✓		
39+64 ²⁹	M.H. #23	Δ 11°-26'-30" Lt.	1.37	348.74	335.74	+13.00 ✓		± Hub 345.07
T.P.	12.33	<u>357.40</u>	5.03	345.07	± Hub M.H. 23			
+50			8.15	349.25	335.84	+13.41 ✓		

357.40

-39 ⁰⁰			8.13	349.27	336.04	+13.23 ✓	
+86 ⁴¹	P.O.T. Hub.						± Hub. 349.00
+50			9.50	347.90	336.25	+11.65 ✓	
38			6.91	350.49	336.45	+14.04 ✓	
+50			9.33	348.07	336.65	+11.42 ✓	
0.41 ⁴¹							
+28 ⁴⁴	M.H. 22	Δ 57-25 RT	12.08	345.32	336.74	+8.58 ✓	± Hub. 341.81
TP			12.08	345.32			
37					336.85		
50					337.05		
36					337.26		
50					337.46		
35					337.67		
+68 ⁴¹	M.H. 21.	Δ 41-14 RT.			337.81		± Hub. 343.42
+50					337.88		
+21 ⁰⁹	P.O.T				338.08		
34					338.29		
+50					338.47		± Hub. 349.33
33+05 ⁴⁹	M.H. 20	Δ 86-31 RT			338.70		
+50					338.90		
32					339.00		
31+75 ⁸⁵	D.M.H. 19	Δ 78-27 LT.			353.00		
"	"	Line to West					

+50							
31							
+50							
30	292.86						
+50							
B.M.	7.92	359.83		351.41			
29 +359.5	M.H. 18	$\Delta 106^{\circ} 25' R$			346.01		
28 +98			4.58	354.75	347.13	+7.62	
+44			1.50	357.83	348.61	+9.22	
T.P.	9.80	369.01	0.12	359.21			
27 +98			8.76	360.25	350.08	+10.17	
4 th 25.6.25	M.H. 17	N $19^{\circ} 45'$	9.76	359.25	351.29	+7.96	
35 th 453.28	M.H. 17	$\Delta 19^{\circ} 23' L$			351.34		
42 nd	M.H. Moved 3.6' E. to avoid end steps						
27 +15			8.55	360.46	351.88	+8.58	
+65			8.71	360.80	352.58	+7.72	
4 th			3.85	365.16	353.16	+12.00	
+23.86	M.H. 16	$\Delta 38^{\circ} 45' L$					
26			5.00	364.01	353.50	+10.51	
5 th T.P.	7.99	372.87	4.11	364.90			
+5.0			4.89	368.00	354.20	+13.80	
T.P.	4.33	372.12	5.10	367.79	4 th M.H. 15		
+13.60	M.H. 15	$\Delta 76^{\circ} 54' L$	0.67	371.45	354.70	+16.75	
25			4.92	365.20	354.90	+10.30	
T.P.	12.58	371.65	13.65	359.07			
+50			11.20	360.45	355.60	+4.85	
+30			8.34	363.31	255.84	+7.43	
T.P.	8.30	379.04	0.91	370.74			
24 +08.5			10.14	368.90	356.20	+12.70	RO.T.H. 4b.
23 +88.5			7.22	371.82	356.30	+15.52	

Grade change
See page 72



		379.04							
+53 ¹⁶	M.H. #74	∠26°-38' RT	12.29	366.75	356.95	+9.80		Hub	362.40
23+29 T.P.	5.48	376.45	8.07	370.97	257.30	+13.67			
23+00			5.29	371.16	357.70	+13.46			
T.P.	2.35	368.15	10.68	365.80		+5.71			
+50			4.04	364.11					
2.2 T.P.	11.80	377.60	2.35	365.80	358.40	+13.72			
			4.78	372.82	359.10				
+70 ³⁵ P.O.T.			6.16	371.44	359.52	+11.92			
+40			8.13	369.47	359.94	+9.53			
21+08 ⁹⁰	M.H. #73	∠117°-28' RT	10.45	367.15	360.37	+6.78			
+72			6.20	371.40	360.88	+10.52			
20+35			3.62	373.98	361.40	+12.58			
19+98 T.P.	10.01	385.85	1.76	375.84	361.92	+13.92			
19+39			7.21	378.64	362.75	+15.89			
18+88			15.60	370.25	363.46	+6.79			
	2.28	379.08	9.05	376.80					
+50			2.28	376.80	363.98	+12.82			
18+36 ⁶¹	M.H. #12	∠26°-22' RT	1.26	377.82	364.17	+13.65		Red. & Hub. M.H. #12	
= +38 ⁰⁷	15.10	386.17	8.01	371.07				4.50	374.58 = Hub 374.58
T.P.									
17+92 ¹⁴			12.23	373.94	364.35	+9.59			
17+46 ²¹	M.H. #10 new	∠41°-34' Lt	3.15	383.02	364.54	+18.48			
17+28 ⁰⁹	P.O.T. Nail								
16+90 T.P.	6.76	380.22	12.71	373.46	364.76	+8.70			
45									
16+45			11.48	368.74	364.94	+3.80			
35									
16+11 ²²	P.O.T. Hub. &		7.92	372.30	365.07	+7.23			
T.P.	3.16	371.36	12.02	368.20					

359.33

29+35 ²⁵	M.H. 18	Δ 106-25 RT.			346.01		
28+98			4.58	354.75	346.39	+ 8.36 ✓	
28+48			1.50	357.83	346.89	+ 10.94 ✓	
27+98	T.P.	9.80 369.01	0.12	359.21			
27+56 ²⁵	M.H. 17	New. Location	9.76	359.25	347.80	+ 11.45 ✓	
27+15			8.55	360.46	348.22	+ 12.24 ✓	
26+65	M.H. 16	New. Location T.P.	8.71	360.30	348.72	+ 11.58 ✓	
26+35		2.73 363.03		360.30			
26+16			4.96	358.07	349.02	+ 9.05 ✓	
25+95			14.8	348.2	349.22		
25+78			4.09	356.94	349.42	+ 7.52 ✓	
25+65	T.P.	14.32 372.48	13.8	349.2	349.57	pipe exposed	
25+40			4.87	358.16	349.72	+ 8.44 ✓	
25+20 ³⁵			1.93	370.55	349.97	+ 20.58 ✓	
25+13 ⁴⁰			1.03	371.45	350.17	+ 21.28 ✓	
					354.70	+ 16.75 ✓	

Levels for change

π 369.01

26+65¢ 9.8 359.2
π 363.03

26+35¢ 6.0 357.0

26+18¢ 12.7 350.3

26+16¢ 14.8 348.2

26+14¢ 13.0 350.0

25+95¢ 7.0 366.0

25+78¢ 13.6 349.4

25+75¢ 13.1 ✓ 349.2

25+70¢ 13.5 349.5

25+65¢ 8.0 355.0
π 372.48

25+40¢ 4.0 368.5

25+20³⁵ New =
= 25+13⁴⁰ old 4.49 362.79

76' Sewer Lateral N. of M.H. 24

0+00	B.M.	16.96	351.96	335.00	F.L.M.H. 24		
				335.50			
0+22	¢ ground		3.4	48.6	46.6		
T.P.	12.86	364.54	0.28	351.68			
0+44	stab & ¢ ground		3.01	361.53	57.80	3.73	
T.P.	14.55	378.36	0.73	363.81			
0+73	stab & ¢		2.42	375.94	72.50	3.44	

N.H. Sewer

371.36

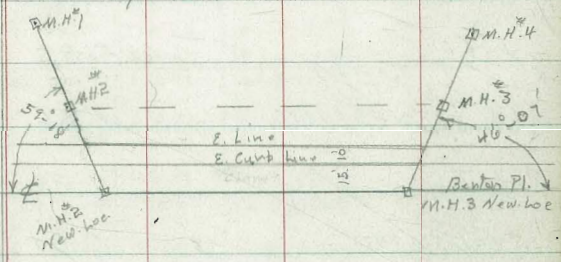
15+90 ⁴² Pier #5	10.20	361.16	365.16	-4.00 ✓
15+78 ⁴² Pier #4	9.63	361.73	365.21	-3.48 ✓
15+66 ⁴² Pier #3	9.29	362.07	365.26	-3.19 ✓
15+54 ⁴² Pier #2	8.87	362.49	365.20	-2.81 ✓
15+42 ⁴² Pier #1	9.60	361.76	365.35	-3.59 ✓
T.P. 11.70	380.35	2.71	368.65	
14+90 ⁴² M.H.#9	3.00	377.35	365.56	+11.79 ✓
38.42				
14+52	6.26	374.09	365.71	+8.38 ✓
35				
14+17 M.H.#8	See Page 75		365.85	

383.17
7.80
392.97

46.8	64.1	393.8	73
35.2	38.1	78.4	
373.8	26.0	47.26	
		38.1	
		530.7	
		26	
		556.7	
		61.15	
		44.10	
		165.28	

2-16-38

Change in line bet. M.H.#2 & M.H.#3.



B.M.L. R.P.	9.80	392.97	383.17	M.H.#2	
3+53 ⁴ M.H.#2			6 R.P. 21	Grade Fl.	
13+70 Top of Bank			383.17	370.32	+12.85
3+82 ³ E. Curb. Benton					
3+99 ⁸ New M.H.#2					
4 Benton Place	Δ 59°-18' Rt.	4.90	388.07	370.14	+17.93 ✓
4+56		4.20	388.77	369.93	+18.84 ✓
New M.H.#3 Benton Place					
4+98 ⁶	Δ 46°-07' Rt.	3.82	389.15	369.78	+19.37 ✓
5+19 ³ E. curb. Benton Pl.					
5+36 ² Top. Bank					
5+62 ²					
5+20 Sold M.H.#3	11.53	381.44	369.51	+11.93	see Page 74

Red. Change Elev. Change

> 4.8	388.2
> 4.82	388.15
4.7	388.3
3.9	389.1
3.5	389.5
3.50	389.47
3.2	389.8

Walker
Bliss
2-3-38

JENNER Construction
North of Adams And East Mt. View Drive
Between South Line 35th to MH #5

Indexed
C.S.K.

74

See Drawing 5179 L Profile 5181 L

Stake 35th		Elev. stake	Elev. Floodline	Cuts	offsets	
-0+00	π	391.53	385.07	371.63	+13.44	
+50		360	387.93	371.43	+16.50	
1+00		4.43	387.10	371.23	+15.87	
+50		5.83	385.70	371.03	+14.67	
1+66.25	M.H. #1 Δ R/L 89°56'	11.56	379.97	370.97	+9.00	
2+17		6.30	385.23	370.77	+14.46	
+52.83	P.P.T.	6.51	385.02	370.62	+14.40	
2+85	π	7.46	384.07	370.49	+13.58	
3+25		389.87	13.23	376.64	370.33	+6.31
3+53	M.H. #2 Δ 61°15' L/L	6.70	383.17	370.22	+12.95	
4+00	π	391.42	9.47	381.95	370.03	+11.92
4+50		9.49	381.93	369.83	+12.10	
4+85		9.58	381.84	369.69	+12.15	
5+20	M.H. #3 Δ 44°10' L/L	9.98	381.44	369.55	+11.89	
5+50		16.61	374.81	369.43	+5.38	
5+83		12.29	379.13	369.30	+9.83	
6+15		389.09	1.77	387.32	369.17	+18.15
6+56	Nail on line	1.51	387.58	369.01	+18.57	
6+87	M.H. #4 Δ 81°34' R/L	11.99	377.10	368.89	+8.21	

Book 1404-15
N.Y.R.P. 35th. Millstone

385.54

+5.99

π 391.53

19.72

371.81

Grade Change	at 001	M.H. #2	2-17-38
0+00	(C.R.P.)	(F.L. Grade)	
0+50	(C.R.P.)	(F.L. Grade)	
1+00	387.10	371.26	+15.84
1+50	385.70	371.07	+14.63
1+66.25	379.97	371.01	+8.96
2+17	385.23	370.81	+14.42
2+52.83	385.02	370.62	+14.40
2+85	384.07	370.51	+13.56
3+25	376.64	370.42	+6.22
3+53	383.17	370.32	+12.85
4+00			

π 391.53

6.43

TP = 385.10

4.77

π 389.87

1.77

TP 388.10

3.32

π 391.42

3.25

TP 388.17

0.92

π 389.09

10.16

chk. on Cor. Septic Tank P-75
" " by miller = 378.94
difference 0.01

change in grade M.H. #3 to M.H. #4
6' R.P. E1. F.L. Grade

381.44 369.51 +11.93

374.81 369.40 +5.41

379.13 369.28 +9.85

Hub 14+90	M.H. 9264-474	5.10	375.63 = 375.65	6' offset stub
Hub 14+17	M.H. #8	6.91	373.82	FL. Grade
14+17	M.H. #8	2.86	377.87	365.85 + 12.02
14+00		1.80	378.93	365.92 + 13.01
13+70		2.34	378.39	366.04 + 12.35 ✓
13+50		9.45	371.28	366.12 + 5.16 ✓
13+00		4.66	374.39	366.32 + 8.07 ✓
12+50		0.65	379.80	366.52 + 13.28 ✓
12+00		0.67	372.60	366.72 + 5.88 ✓
11+95	S. line lot 37			Grade Base of Piers
11+95	S. End Trestle		366.75	But to Base of Piers 368.7 + 2.0
11+83	Pier #2	8.86	364.41	366.79 - 2.38 360.00 + 4.4
11+71	Pier #1	5.50	367.77	366.83 + 0.94 360.00 + 7.8
11+59	N. End Trestle			366.87
11+50		3.88	376.42	366.92 + 9.50 ✓
11+47	N. Line lot 37	6.1	373.7	366.93 + 6.8 ✓
11+47	P.O.T. Hub.	6.88	382.82	367.01 + 15.81 ✓
10+90		5.34	384.36	367.16 + 17.20 ✓
10+49	M.H. #7	14.87	374.83	367.32 + 7.51 ✓
10+30	P.O.T. Hub.	4.57	385.13	367.40 + 17.73 ✓
10+00		13.27	376.43	367.52 + 8.91 ✓
9+63		3.74	385.96	367.67 + 18.29 ✓
9+23		0.37	389.33	367.83 + 21.50 ✓
9+07	M.H. #6	3.28	386.50	367.89 + 18.61 ✓
8+50		15.25	374.53	368.12 + 6.41 ✓
8+27		7.13	382.65	368.21 + 14.44 ✓
7+75		10.06	379.72	368.42 + 11.30 ✓
7+41	Equation M.H. #5	0.92	388.86	368.55 + 20.81 ✓
7+35		12.79	376.30	368.70 + 7.60 ✓

Grade Base of Piers
But to Base of Piers

Rod

B.M. of Hub.
10+49.87
372.58

11+27 POT Hub
379.52
0.28
379.80
12.90
366.90
6.37

373.27
0.63
372.64
7.81
380.45
7.89
372.56
8.17

380.73

Hub 11+27
379.52
10.18

389.70
10.76
378.94
10.84
389.78

Hub 372.55
Hub 384.44

4.1
373.7 C.6.8

T.P. Sample Tank

New cut stub for M.H. #6
N.W. of M.H. #6
384.34
367.89
16.43
5.34
+ 11.09
384.32
367.89
16.43
6.85
+ 9.58

Levels Perun see p. 60

Hub
14+17
374.52

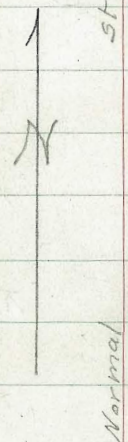
Continued on Page 74

11-21-36 Tie Points Normal & Blaine indexed

Muller
Walker
Bliss

C.S.K.

plotted on Tie point sheet
11-20-43
C.S.K.



9-17-36 Grades Alley BIK 153.264

indexed
C.S.K.

F.B. 1519-59

BM
S.L. Howard Ave
= 6+00

3.78 376.18

372.40

Nail Pole N
End. Alley

W.
371.68
4.50

E.
371.47
4.71

5+70

371.56
4.12
4.14
+0.98

371.35
4.83
0.10

Blaine Ave

5+35

371.42
4.76
0.0

371.21
4.87
4.73
+0.24

5+00

371.24
4.90
4.74
+0.16

371.07
5.11
4.25
+0.86

4+65

371.14
5.04
4.56
+0.48

370.93
5.25
4.25
+1.00

See G.186-P54.

0+70

369.56

369.36

Sl. Gutter	Track	2' Soffit	♀	Gutter	BM Lull... SA	Indexed	Rosecrans Paymt. Grades				
						2.5.R.	Track	2' Soffit	♀	Gutter	
51. Lullors	40.00	39.88 8.26 Pav		38.96 X 7.28 ✓ 006	41.75 6.39						
at 50 B.	41.12	40.89 7.37 7.25 Reset to fit Track.		39.70 X 8.74 ✓ 006	48.14 1.50	44	54.38	54.32 = 54.25	53.88 X 5.42 F 0.20	59.30 9.15 50.15 3.31	
N.L. Kingsley											
2+00	43.65	43.50 4.64 ✓ 00		42.47 X 5.67 ✓		♀ Ipsen	54.55	54.48 = 54.33	54.13 X 5.17 50 F 0.50	53.46 1.95 51.51 RM. AN Home	
2+35											
♀ Kingsley		4.01 ✓		4.81 ✓		44	54.35	54.29 = 54.18	53.83 X 5.47 ✓		
S.L. Kingsley						S. Linn/Ipsen					
2+70	44.87	44.76 3.38 ✓ 00		44.00 7006 4.14 4.14 -2.04		8+10	54.05	53.90 5.40 5.65 F 0.25	53.50 5.80 ✓		
3+20 B	45.87	45.64 2.46 ✓ 00		45.06 7+24 3.08 8.36 F 0.28		N.L. Horner 10+10	50.41	50.39 8.91 8.91 00	50.00 10 9.30 9.40 -0.10	9.95 ✓	
N.L. James					59.30						
4+70	48.79	48.72 10.58 ✓ 00		48.26 X 11.04 ✓ 0.0		S.L. Horner 10+80	49.49	49.38 9.92 0.0	48.70 X 10.60 14.60 00		
♀ James		9.72 ✓		10.18 10.32 0.14		12+30 B	47.03	46.90 6.56 6.06 0.050	51.01 46.90 4.11 7.39 7.44 -0.05	46.07 4.94 46.07 X 7.39 7.44 -0.05	53.46 3.48 49.98 Hyd SW. Goldsmith
S.L. James						N.L. Goldsmith					
5+40	50.50	50.44 8.86 ✓		49.98 020 9.32 9.51 -0.19		12+80	46.77	46.62 4.39 ✓	51.59 46.62 4.97 0.4 4.69	46.07 4.94 46.07 X 7.39 7.44 -0.05	49.94 1.50 51.74 46.90 4.88
5+90 B	51.64	51.60 7.70 8.00 -0.30		51.21 X 8.09 ✓			4.40		5.38 5.34	49.94 1.03 51.03	
N.L. Ipsen						S.L. Goldsmith					
7+40	54.16	54.08 5.22 ✓ 0.0		53.63 102 5.67 5.74 F 0.07		13+50	46.72	46.59 4.42 ✓	46.07 5.34 1.00		

Station	Track	2.8	BM 49.28	Track	4.584d	Gutter	78
S. Line Goldsmith 13+50	46.72	$\frac{46.59}{5.08}$	$\frac{47.08}{7.74}$ 45.67	S. Line Freeman 16+20	49.18	Lowered to Fit $\frac{48.22}{6.60}$	454.82
13+75		$\frac{46.71}{7.38}$	BM 49.28 $\frac{1.41}{51.59}$	+45			
14+00 B	46.95	$\frac{46.83}{4.76}$		+70			
+25		$\frac{47.07}{4.52}$		+95			
N. End Switch +40		$\frac{47.23}{4.36}$ $\frac{47.23}{6.93}$	gutter O.K.	17+14	49.65	49.02	
+75		$\frac{47.58}{6.58}$	RM Hyd S.W. Goldsmith 49.98 4.18 54.16 0.63 53.53	Drive	5.17	4.51	
15+00		$\frac{47.83}{6.33}$	Top Hyd S.W. Elliot	+55	0.0	4.38	
+25		$\frac{48.07}{6.09}$		+70	49.91	49.21	
N. Line Freeman +50	48.44	$\frac{48.31}{5.85}$		+95	4.91	4.25	
4+85		$\frac{48.69}{5.47}$			0.0		
				18+20	50.00	49.16	
				18+55d	50.15	4.01	
				N. Line Elliot 18+20	50.42	50.31	49.65
					3.85		
					50.27	3.87	49.62
				S. Line Elliot 18+90	50.14	4.02	49.44

Pav. Grades at City Shops
20th + B

Indexed
C.S.K.

Grades for Elec. Conductivity
Box
13' N. of N Line B. St

BM. B.P. 2.05 72.28 70.23 S.E. 20th
+ B St.

36' W. of 00 67.16
5.12
4.62
+0.50

0+00 = N. Line B. St.

44' W. of 00 67.40
4.88
4.38
+0.50

90' W. 80' W. 70' W. 60' W. 30' W. 15' 0+00 15' E

65.99 66.65 67.40 67.81 68.6 71.60
6.29 5.63 4.88 4.47 3.7 0.7
2.7
+1.0

0+18 N.

66.1 66.26 66.70 67.6 68.0 68.2
6.18 5.58 4.68 4.3 4.1
+0.2
+4.5

0+34 N.

66.0 66.16 66.1 66.7 67.3 67.7
6.24 6.12 6.18 5.6 5.0 4.7
4.6
+1.0
+0.4
+5.0

0+50.5 N

floor
64.19

66.0

65.70 66.02 65.70 66.3 66.9 67.2
6.58 6.58 6.0 5.4 5.1
5.58 5.0 0.6
+1.00
+4.5

72.24

	90W	80W 0+78N	70W S-End. Machine Shop	60W 38W	30W
BM Floor	75.60 65.60 6.8	65.40 6.88	65.74	65.40 6.88	65.6 6.57 6.8
T.P.	5.24	71.08 0+91N	6.44	65.84	6.00 5.90 4.90 4.10
65.55	65.60 5.48	65.30 5.78	65.58	65.30 5.78	65.50 5.58
65.55		1+12N			
	65.5 5.58	65.1 5.98	65.38 5.70	65.10 5.98 5.88 +0.10 on par.	65.17 5.91
65.55		1+40N			
	65.30 5.78	64.90 6.18	65.18	64.90 6.18	
90W Top Boy	89W Top Boy	82W Top Boy	1+63.6		
65.0 6.08	64.74 6.30	64.8 6.28	64.73 6.35	64.83	64.80 6.28
T.P.	3.39	69.01	5.46	65.62	

0+00	15.8	0.19 66.60 1.91 68.70	5.2 3.5 1.4 4.7	38 5 43
66.0 6.28 6.8 5.60 5.40 4.60 4.10	66.20 6.08 6.8 5.40 3.40 4.20	66.0 2.7 6.9 3.6 3.8 1.1	66.6 2.1	1.3 E -01 4.2 4.8 5.7 4.0 4.7
Top of 4.60 4.10	floor office 65.35	5.6 3.1 4.1	4.6 4.1 5.7 1.6	6.4 1.9

IMPROVED TABLES AND INFORMATION

70.23 0.66 70.89	64.70 4.38 4.26	64.90 4.11
------------------------	-----------------------	---------------

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

33rd N. E.

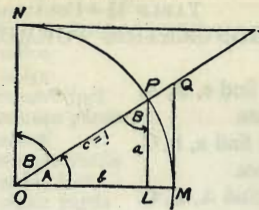


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

5.60
5.54
5.54
5.62
5.47
5.35

76
59
17

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360°	= 21600'	= 1296000"
Radius	= arc of 57.2957790°	
Arc of 1° (radius = 1)	= .017453292	
Arc of 1' (radius = 1)	= .000290888	
Arc of 1" (radius = 1)	= .000004848	

$$\pi = 3.141592654$$

$$\frac{\pi}{4} = 0.785398163$$

$$\frac{\pi}{6} = 0.523598776$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{\pi}{6} = 0.523598776$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$\sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\pi^2 = 9.869604401$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

2.1
1.3
+ 0.8
0.3
2.2
+ 0.8
- 2.0
2.4

4.50
4.42

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

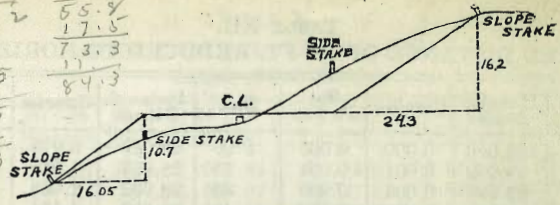
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.023	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	18 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

20.5 34.2
 17.7 17.6
 38.2 55.9
 17.8
 73.3
 11
 84.3
 34.5
 14
 20.5
 11.2
 9.3



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

48.31 41
 46.83 16
 0166
 25
 830
 332
 4150
 4938
 2.21
 411
 2.62
 820
 3.04
 413
 3.45
 424
 3.87
 3590.28
 34
 3.95
 386
 .42
 19.30 7.7
 21 14
 1947 9.1
 1964
 17
 1981 4.27
 98
 40
 1998 17.92
 4.69
 5.0
 3.2
 1.8
 72.24
 4.98
 67.30
 69.30
 1.3
 68.0
 63.8
 334.5
 289.1
 3.6
 45.4
 13200
 3178
 080
 20
 160
 3.09
 2.89
 20
 25.4
 08
 4220
 4086
 57.0
 54.6
 2.4
 76.76
 4.15
 80.91
 1166
 63.8
 1.6
 454
 2.400
 2270
 1300
 053
 20
 1060
 57.0
 53
 25.4
 53
 762
 62.2
 2.89
 68.0
 55.9
 1.3
 55.9
 1.3
 13462
 1.1
 546
 24
 71
 469
 41
 8
 68.4
 66.7
 66.7
 66.7
 .03
 16
 3
 48
 24
 7.2
 66.7
 1.08
 68.50
 515
 67.12
 19.030
 14
 167
 120
 1.8
 12
 5838
 89
 2.4
 512
 67
 33
 67
 00

Wightman + 400 343.07

50
23
17.7

10 30
8.25
6.05
8 30

72.13
65.00
0.475
1.7.13
6.0
1.13
1.05
80

10.46
523
15.69

12.40
1.98
14.38

75993
9.09

33.1
323
2 65.4
32.7

9.15
9.25
4.72

0475
5
23750
6500
237
67.38
69.75
238
72.13

290.21
5.95
284.26

530
473
57

18.2
45
3
4.2

5.17

220
240
500

09
72
37

66
14
8.0

372.84
4.83
377.67

273.40
3.87
277.67

180
260
280
460
140

80
68
34
13
46
34
80

712
688
4.4 12.40
105
240

0.5
2
10

19.25
67
19.42
17.59
17
19.76
19.93

4730
175 215.17
250

5.21 5.4 280 372 250 441
5.9 5.9 330 422 514 485
11.14 11.32 14 784
5.57 5.66 208 397 532 463
72 478.0 3780 50 288.64 114.23
99 195 260 23.10 2.00 25
12 690 32 286.44 115.08

800 13.24 119.1 60 115.33
11.70 4663 122.01 119.1 46 115.71
15.20 77 135.25 135.2 7 2036
2690 4586 19.02 17 734

134537.2 16.17 1.44
11.6 60 114.83
72 25.6 46 1.44
12 20.0 46 116.27
89 37.7 106
99 13.4 .01143

11.40 23.9 126 1.44
5.90 37.2 126
2.50 14.2 180
83 23.0 38.67 126 540
119.06 110.67 504
77 149.33 360
119.83 38.67 378

188.00 0.01143 27 280 13.17
12.165 1.95 5.4 2286 480 1.95
995 840 14.10 30860 15.12
2155 77 12.22 11.23 1.4 160
17 3.38 343 1.54 12

730 29 275
159 30 140
188 25 15
40 415
8.20 8.15 7.40
7.75 730 900
40 45 1640
9.20

11.45 4933
14.60 4933
26.45 12
13.22 6133
11.45 11067
1.37 4933
21.60 160.00